SEE SHEET 3 FOR PLAN SHEET LAYOUT AT TIME OF INVESTIGATION

CONTENTS

78000

REFERENCE

4936

<u>LINE</u>	<u>STATION</u>	<u>PLAN</u>	PROFILE
-L-	10+00.00 - 54+14.00	4-7	NA
-YI-	10+50.00 - 17+04.48	5	NA
-YIA-	10+11.00 - 12+25.00	5	NA
-Y2-	12+50.00 - 14+54.98	6	NA
-Y3-	10+40.00 - 12+40.00	7	NA
-DRI-	10+15.00 - 12+28.59	5	NA
-DR2-	10+38.56 - 11+71.37	7	NA

CROSS SECTIONS

<u>LINE</u>	<u>STATION</u>	<u>SHEETS</u>
-L-	10+00.00 - 53+00.00	8-27
-YI-	10+50.00 - 17+00.00	28-31
- YIA -	10+50.00 - 12+25.00	32
-Y2-	12+50.00 - 14+50.00	33-34
-Y3-	10+50.00 - 12+00.00	35
-DRI-	10+00.00 - 12+00.00	36-37
-DR2-	10+94.91 - 11+45.44	26

APPENDICES

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Α	LABORATORY	TEST	RESULTS	38-40

STATE OF NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT

ROADWAY SUBSURFACE INVESTIGATION

COUNTY WAKE

PROJECT DESCRIPTION WIDENING SR 1006 (OLD STAGE ROAD) FROM SR 2736 (ROCK SERVICE STATION ROAD) TO SR 3884 (ROLLING MEADOWS DRIVE) **INVENTORY**

STATE PROJECT REFERENCE NO. HL-00081

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (1991) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BORCHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS INCLORDED TO CLIMATIC CONDITIONS INCLORDED TO CLIMATIC CONDITIONS INCLORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GLARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, OR THE INTERRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO PERFORM INDEPENDENT SUBSURFACE INVESTIGATIONS AND MAKE INTERPRETATIONS AS NECESSARY TO CONFIRM CONDITIONS ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

- NOTES:

 1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.

 2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

K. HAVEN

M. DANIELS, GIT B. WORLEY, PG

M. G. MOSELEY

J. MOSELEY

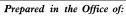
INVESTIGATED BY _SUMMIT DES

DRAWN BY __M. LEAR, PG

CHECKED BY __M. DANIELS, GIT

SUBMITTED BY M. LEAR, PG

DATE __*JUNE*, 2024





Hillsborough, NC 27278-855 Volce: (919) 732-3883 Fax: (919) 732-6776



DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED

SIGNATURE

PROJECT REFERENCE NO. SHEET NO.

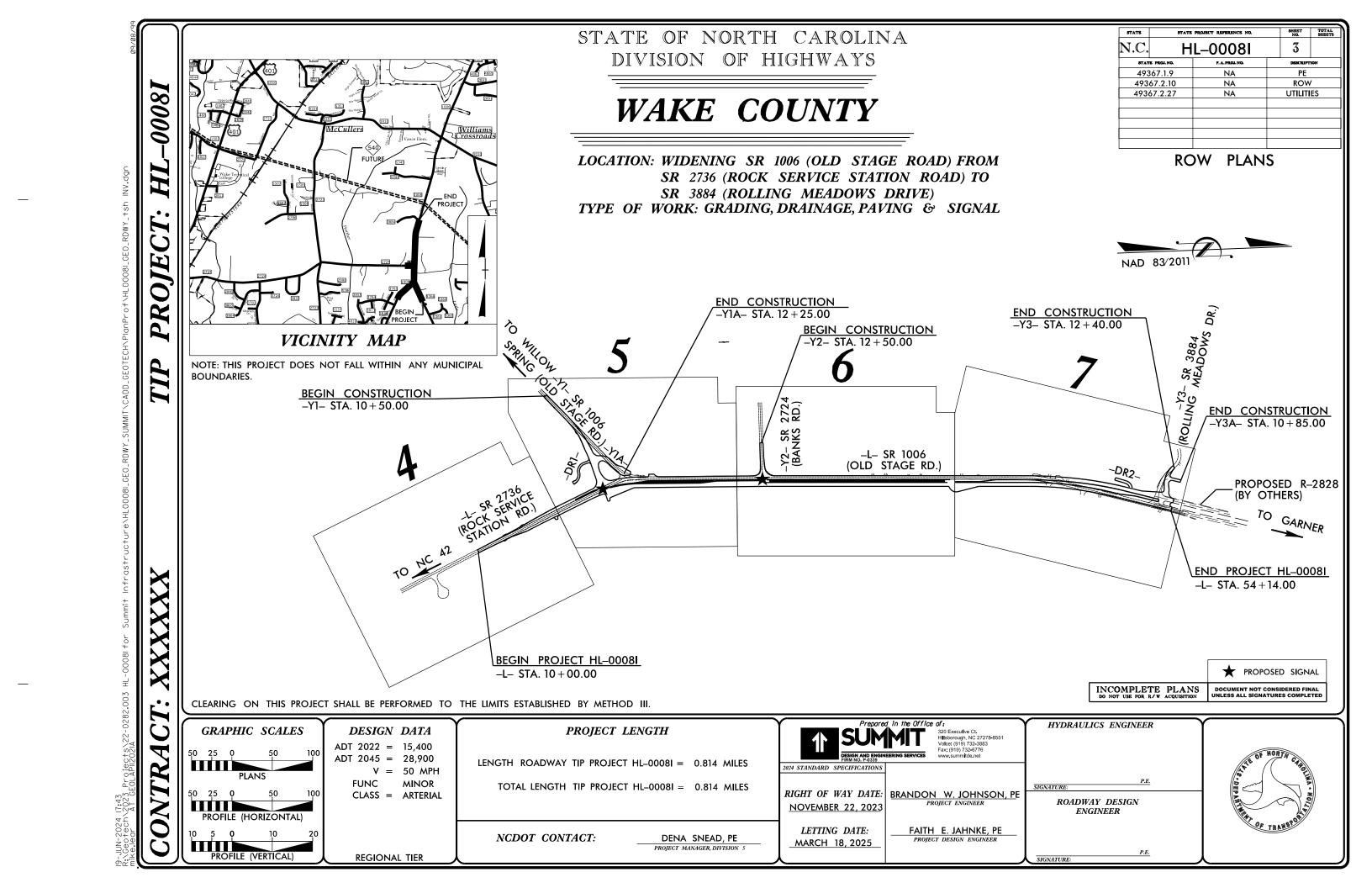
HL—00081
2

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION	GRADATION	ROCK DESCRIPTION HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED	TERMS AND DEFINITIONS
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT	WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.	ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL.	ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING:	GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.	SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN	AQUIFER - A WATER BEARING FORMATION OR STRATA.
CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE,	ANGULARITY OF GRAINS	REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:	ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING
VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6	THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS:	WEATHERED WILL NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES >	A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.
SOIL LEGEND AND AASHTO CLASSIFICATION	ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.	ROCK (WR) 100 BLOWS PER FOOT IF TESTED.	ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT
GENERAL GRANULAR MATERIALS SILT-CLAY MATERIALS ORGANIC MATERIALS	MINERALOGICAL COMPOSITION	CRYSTALLINE FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT	WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
LLASS. (\$\(\sigma\) 7ASSINU *200) (> 334 PASSINU *200)	MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.	ROCK (CR) WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.	CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5 CLASS. A-1-0 A-1-b A-2-4 A-2-5 A-2-6 A-2-7 B-2-6 A-2-7 A-3 A-6, A-7	COMPRESSIBILITY	NON-CRYSTALLINE FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YELLD SPT REFUSAL IF TESTED.	COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM
SYMBOL 0000 d0000 d	SLIGHTLY COMPRESSIBLE LL < 31	ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.	OF SLOPE.
7. PASSING	MODERATELY COMPRESSIBLE LL = 31 - 50 HIGHLY COMPRESSIBLE LL > 50	COASTAL PLAIN COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SEDIMENTARY ROCK SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED	CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
*10 50 MX GRANULAR CLAY MUCK,	PERCENTAGE OF MATERIAL	CCP) SHELL BEDS, ETC. WEATHERING	DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT
*40 30 MX 50 MX 51 MN PEAT *200 15 MX 25 MX 10 MX 35 MX 35 MX 35 MX 35 MX 36 MN 36 MN 36 MN 36 MN 36 MN	GRANULAR SILT - CLAY ORGANIC MATERIAL SOILS SOILS OTHER MATERIAL		ROCKS OR CUTS MASSIVE ROCK.
MATERIAL MATERIAL	TRACE OF ORGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10%	FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING, ROCK RINGS UNDER HAMMER IF CRYSTALLINE.	DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE
PASSING *40 SOUS WITH	LITTLE ORGANIC MATTER 3 - 5% 5 - 12% LITTLE 10 - 20% MODERATELY ORGANIC 5 - 10% 12 - 20% SOME 20 - 35%	VERY SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN,	HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE
LL — — 40 MX 41 MN 40 MX 41 MN 40 MX 41 MN 40 MX 41 MN LITTLE OR HIGHLY	HIGHLY ORGANIC > 10% > 20% HIGHLY 35% AND ABOVE	(V SLI.) CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.	LINE OF DIP, MEASURED CLOCKWISE FROM NORTH,
GROUP INDEX 0 0 0 4 MX 8 MX 12 MX 16 MX NO MX AMOUNTS OF	GROUND WATER	SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO	FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE
USUAL TYPES STONE FRACS ORGANIC	✓ WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING	(SLI.) 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR	SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
OF MAJOR GRAVEL AND FINE SILTY OR CLAYEY SILTY CLAYEY MATTER MATERIALS SAND GRAVEL AND SAND SOILS SOILS	STATIC WATER LEVEL AFTER 24 HOURS	CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS. MODERATE SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN	FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.
CEN RATING FAIR TO	→ PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA	(MOD.) GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS	FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.
AS SUBGRADE EXCELLENT TO GOOD FAIR TO POOR POOR UNSUITABLE		DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.	FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30	- OM← SPRING OR SEEP	MODERATELY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED, IN GRANITOID ROCKS, ALL FELDSPARS DULL	FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE
CONSISTENCY OR DENSENESS	MISCELLANEOUS SYMBOLS	SEVERE AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH	FIELD.
PRIMARY SOIL TYPE COMPACTNESS OR RANGE OF STANDARD RANGE OF UNCONFINED PENETRATION RESISTENCE COMPRESSIVE STRENGTH	ROADWAY EMBANKMENT (RE) 25/025 DIP & DIP DIRECTION	(MOD, SEV.) AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK, ROCK GIVES "CLUNK" SOUND WHEN STRUCK, IF TESTED, WOULD YIELD SPT REFUSAL	JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO
CONSISTENCY (N-VALUE) CONFRESSIVE STRENGTH	₩ITH SOIL DESCRIPTION → OF ROCK STRUCTURES	SEVERE ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT	ITS LATERAL EXTENT.
GENERALLY VERY LOOSE < 4 CONTROL LOOSE	— SOIL SYMBOL STATE TEST BORING SLOPE INDICATOR INSTALLATION	(SEV.) REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN.	LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
MATERIAL MEDIUM DENSE 10 TO 30 N/A	图	IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF	MOTILED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTILING IN SOILS
(NON-COHESIVE) DENSE 30 TO 50 VERY DENSE > 50	ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT AUGER BORING CONE PENETROMETER TEST	VERY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE SEVERE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK	USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE
VERY SOFT < 2 < 0.25	— — INFERRED SOIL BOUNDARY — CORE BORING ● SOUNDING ROD	(V SEV.) REMAINING, SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR	OF AN INTERVENING IMPERVIOUS STRATUM.
GENERALLY SOFT 2 TO 4 0.25 TO 0.5	MWO MOUNTABLING MEN TEST BORING	VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <u>IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF</u>	RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
SILT-CLAY MEDIUM STIFF 4 TO 8 0.5 TO 1.0 MATERIAL STIFF 8 TO 15 1 TO 2	WITH CORE	COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS	ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF
(COHESIVE) VERY STIFF 15 TO 30 2 TO 4 HARD > 30 > 4	→▼▼▼→ ALLUVIAL SOIL BOUNDARY △ PIEZOMETER INSTALLATION — SPT N-VALUE	ALSO AN EXAMPLE.	ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
TEXTURE OR GRAIN SIZE	RECOMMENDATION SYMBOLS	ROCK HARDNESS	SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT
U.S. STD. SIEVE SIZE 4 10 40 60 200 270		VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK, BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.	ROCK,
OPENING (MM) 4.76 2.00 0.42 0.25 0.075 0.053	UNDERCUT UNCLASSIFIED EXCAVATION - UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF	HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY, HARD HAMMER BLOWS REQUIRED	SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO
BOULDER COBBLE GRAVEL COARSE FINE SILT CLAY	SHALLOW UNCLASSIFIED EXCAVATION - UNDERCUT UNDERCUT UNCLASSIFIED EXCAVATION - EMBANKMENT OR BACKFILL	TO DETACH HAND SPECIMEN.	THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
(BLDR.) (COB.) (GR.) (SE. SD.) (F SD.) (SL.) (CL.)	ABBREVIATIONS	MODERATELY CAN BE SCRATCHED BY KNIFE OR PICK, GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE HARD EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK, HAND SPECIMENS CAN BE DETACHED	SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
GRAIN MM 305 75 2.0 0.25 0.05 0.005	AR - AUGER REFUSAL MED MEDIUM VST - VANE SHEAR TEST	HARD EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK, HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.	STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF
SIZE IN. 12 3	BT - BORING TERMINATED MICA MICACEOUS WEA WEATHERED	MEDIUM CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT.	A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL
SOIL MOISTURE - CORRELATION OF TERMS	CL CLAY MOD MODERATELY γ - UNIT WEIGHT CPT - CONE PENETRATION TEST NP - NON PLASTIC γ_a - DRY UNIT WEIGHT	HARD CAN BE EXCAVATED IN SMALL CHIPS TO PEICES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.	TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
SOIL MOISTURE SCALE FIELD MOISTURE GUIDE FOR FIELD MOISTURE DESCRIPTION	CSE COARSE ORG ORGANIC	SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS	STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY
(ATTERBERG LIMITS) DESCRIPTION OF THE DISTANCE DESCRIPTION	DMT - DILATOMETER TEST PMT - PRESSUREMETER TEST SAMPLE ABBREVIATIONS DPT - DYNAMIC PENETRATION TEST SAP SAPROLITIC S - BULK	FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.	TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
- SATURATED - USUALLY LIQUID; VERY WET, USUALLY (SAT.) FROM BELOW THE GROUND WATER TABLE	e - VOID RATIO SD SAND, SANDY SS - SPLIT SPOON	VERY CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK, PIECES 1 INCH	STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY
LL LIQUID LIMIT	F - FINE SL SILT, SILTY ST - SHELBY TUBE FOSS, - FOSSILIFEROUS SLI SLIGHTLY RS - ROCK	SOFT OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY	THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
PLASTIC SEMISOLID; REQUIRES DRYING TO	FRAC FRACTURED, FRACTURES TCR - TRICONE REFUSAL RT - RECOMPACTED TRIAXIAL	FINGERNAIL.	TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
(PI) PL PLASTIC LIMIT ATTAIN OPTIMUM MOISTURE	FRAGS FRAGMENTS w - MOISTURE CONTENT CBR - CALIFORNIA BEARING HI HIGHLY V - VERY RATIO	FRACTURE SPACING BEDDING TERM SPACING TERM THICKNESS	BENCH MARK: ELEVATIONS DETERMINED FROM PROVIDED ELECTRONIC FILE (h10008i_is_tin,tin)
	EQUIPMENT USED ON SUBJECT PROJECT	VERY WIDE MORE THAN 10 FEET VERY THICKLY BEDDED 4 FEET	ELEVATION: N/A FEET
OM OPTIMUM MOISTURE - MOIST - (M) SOLID; AT OR NEAR OPTIMUM MOISTURE SL _ SHRINKAGE LIMIT	DRILL UNITS: ADVANCING TOOLS: HAMMER TYPE:	WIDE 3 TO 10 FEET THICKLY BEDDED 1.5 - 4 FEET MODERATELY CLOSE 1 TO 3 FEET THINLY BEDDED 0.16 - 1.5 FEET	
REQUIRES ADDITIONAL WATER TO	CME-45C CLAY BITS X AUTOMATIC MANUAL	CLOSE 0.16 TO 1 FOOT VERY THINLY BEDDED 0.03 - 0.16 FEET	NOTES:
- DRY - (D) ATTAIN OPTIMUM MOISTURE	CME-55 G' CONTINUOUS FLIGHT AUGER CORE SIZE:	VERY CLOSE LESS THAN 0.16 FEET THICKLY LAMINATED 0.008 - 0.03 FEET THINLY LAMINATED < 0.008 FEET	FIAD = FILLED IMMEDIATELY AFTER DRILLING
PLASTICITY	X 8 HOLLOW AUGERS	INDURATION	
PLASTICITY INDEX (PI) DRY STRENGTH	X CME-550 HARD FACED FINGER BITS	FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.	
NON PLASTIC 0-5 VERY LOW	TUNGCARBIDE INSERTS	RUBBING WITH FINGER FREES NUMEROUS GRAINS: FRIABLE GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.	
SLIGHTLY PLASTIC 6-15 SLIGHT MODERATELY PLASTIC 16-25 MEDIUM	VANE SHEAR TEST CASING W/ ADVANCER POOR NOTES OF SHEAR		
HIGHLY PLASTIC 26 OR MORE HIGH	PORTABLE HOIST TRICONE STEEL TEETH X HAND AUGER	MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.	
COLOR	TRICONE TUNGCARB. SOUNDING ROD	GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE;	
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN. RED. YELLOW-BROWN, BLUE-GRAY).	CORE BIT SOUNDING ROU	INDURATED DIFFICULT TO BREAK WITH HAMMER.	
MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.	THINK SILLAN (ES)	EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE;	2.55
		SAMPLE BREAKS ACROSS GRAINS.	DATE: 8-15-1





320 Executive Court, Hillsborough, NC 27278 Phone // 919.732.3883 Web // www.summitde.com

June 19, 2024

WBS Number: 49367.1.9
TIP Number: HL-0008I
County: Wake

Description: Widening of SR 1006 (Old Stage Road) from SR 2736 (Rock Service Station Road) to SR 3884

(Rolling Meadows Drive)

SUBJECT: Geotechnical Report - Roadway Subsurface Inventory

Project Description

The proposed 0.814-mile-long project is located approximately seven miles southeast of the town of Garner, in Wake County, North Carolina. The core of the project involves the widening of SR 1006 (Old Stage Road) from SR 2736 (Rock Service Station Road) to SR 3884 (Rolling Meadows Drive) from a two-lane road to a four-lane divided roadway. The proposed widening will be primarily to the east side of the existing Old Stage Road at the start of the project and will shift widening to the west side of the existing roadway at the north end of the proposed alignment. Improvements will be made at intersecting secondary roadways to accommodate the planned widening and will include realignment of the intersection of Old Stage Road and Rock Service Station Road and the intersection of Rolling Meadows Drive and Old Stage Road. Proposed signals will be added at the intersection of Old Stage Road and Rock Service Station Road and at the intersection of Old Stage Road and Banks Road. In general, the proposed earthworks are minor throughout the project corridor, with the proposed grade located within a few feet of the existing grade of Old Stage Road and other intersecting secondary roads and access driveways. The proposed roadway alignment passes through sparsely wooded residential areas and open fields with few commercial facilities.

The geotechnical investigation for this project was primarily conducted during late October and early November of 2023. Twenty-eight (28) total borings were advanced using 3.25-inch hollow stem auger and hand auger drilling methods to depths ranging from 6.1-feet to 15.0-feet. Most of the borings were advanced using a CME-550X ATV drill rig equipped with an automatic hammer. Standard Penetration Tests (SPT) were performed at approximately 2.5-foot to 5.0-foot intervals at these locations to provide subsurface information for roadway foundation and slope design/construction. Representative soil samples were collected for visual classification in the field and selected samples were submitted for laboratory analysis.

All borings were advanced by North Carolina Licensed Drillers (Certified Well Contractors - CWC). All borings were logged by a North Carolina Licensed Geologist (LG/PG), Geologist in Training (GIT), Engineer Intern (EI), or other professional geotechnical field staff deemed qualified by NCDOT. All investigations and reporting were performed in accordance with the NCDOT Geotechnical Engineering Unit's 2021 "Geotechnical Investigation and Recommendations Manual."

Where possible, borings were left open for a minimum of twenty-four (24) hours to collect groundwater data. In some instances, the 0-hour measurements were used in lieu of the 24-hour measurements due to borings being

backfilled immediately after drilling when near active roadways or per property owner request. A total of forty (40) soil samples were submitted to Summit's soils laboratory for classification and moisture content testing. Based on the subsurface conditions encountered within the project corridor, no bulk samples or undisturbed samples were deemed necessary to obtain and submit to the laboratory for testing.

The following alignments, totaling approximately 0.814 miles, were explored. Subsurface cross sections of these alignments are included in this report.

<u>Alignment</u>	<u>Station (±)</u>
-L-	10+00.00 – 54+14.00
-Y1-	10+50.00 – 1704.48
-Y1A-	10+11.00 – 12+25.00
-Y2-	12+50.00 – 14+54.98
-Y3-	10+40.00 – 12+40.00
-DR1-	10+15.00 – 12+28.59
-DR2-	10+38.56 – 11+71.37

Physiography, Geography, and Geology

The project area is located along the eastern margin of the Piedmont Physiographic Province. The topography within this province is best characterized as gently rolling, well-rounded hills and long low ridges with a few hundred feet of elevation difference between the hills and valleys. The topography within the project corridor is best described as flat to gently rolling. A relative topographic low of approximately 370 feet above sea level occurs within the south end of the project corridor near the intersection of Old Stage Road/Rock Service Road (-L-) and Old Stage Road (-Y1-). From this area, the project ascends gently in both directions to a relative topographic high of 397 feet above sea level at the north end of the project corridor near the intersection with Rolling Meadows Drive (-Y3-). The ultimate topographic low of approximately 360 feet above sea level can be found at approximate -L- station 24+00 between the intersections of Old Stage Road/Rock Service Station Road and Old Stage Road/Banks Road (-Y2-).

The project area is located within the Neuse River Basin, between the drainages for Panther Branch and Little Creek. Panther Branch and Little Creek flow to the south into Middle Creek, which continues southeast and eventually empties into the Neuse River. Surface drainage within the project corridor would be expected to follow the slightly rounded peak-shaped terrain, mostly flowing from the topographic highs near the middle of the project alignment to the developed drainages west and east of the project corridor.

The project area is located within the Raleigh Belt. A geological belt is a typically fault-bounded fragment of Earth's crust that shares a common geologic history distinguishing it from surrounding belts or areas. The Raleigh Belt consists of mostly metamorphosed igneous rocks. These rocks were once part of a large chain of ancient volcanic islands. More specifically, in the deeper subsurface, the project corridor is primarily underlain by Biotite Gneiss and Schist, which has been repeatedly intruded by numerous dikes and sills of Granite. This rock unit has been mapped by the North Carolina Geological Survey (NCGS) as "Biotite Gneiss and Schist (Map Symbol: CZbg)." At the project site, the surface and shallow subsurface sediments belong to the Inner Coastal Plain Province. According to the Geologic Map of North Carolina, these sediments belong to the Cretaceous aged Middendorf Formation (Map Symbol: Km) characterized by laterally discontinuous beds of unconsolidated sand,



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sandstone, clay, and mudstone. These Coastal Plain sediments overlie the Piedmont residual soils and bedrock of the Raleigh Belt within the subsurface.

Soil Properties

Soils encountered during this geotechnical investigation have been divided into two categories based on origin, including Roadway Embankment and Undivided Coastal Plain sediments.

Roadway Embankment soils are present in limited quantities along the project corridor, at the north end of the project alignment and appear to be related to the recent and on-going roadway widening and construction of the adjacent NCDOT project (I-540 interchange at Old Stage Road). Where encountered, these soils consist of ± 2 feet of red, moist, soft, silty clay (A-7).

Undivided Coastal Plain sediments were found throughout the project corridor at the surface and in the subsurface to the depths investigated. The surficial Undivided Coastal Plain sediments consist mostly of brown and orange, dry to moist (locally saturated), very loose to medium dense, silty and clayey, fine to coarse sand (A-2-4, A-2-6, A-2-7), occasionally with trace organics such as root fragments; and locally consist of red, orange, and tan, dry to moist, slightly to moderately plastic (locally highly plastic), stiff to very stiff, fine to coarse sandy and silty clay (A-6, A-7-6), and brown and orange, moist, non-plastic, medium stiff, fine to coarse sandy silt (A-4), occasionally with trace gravel. Within the subsurface the Undivided Coastal Plain sediments consist of thinly to very thickly interbedded, red, orange, gray, brown, and tan, dry to moist, slightly to moderately plastic (locally highly plastic), medium stiff to hard, fine to coarse sandy and silty clay (A-6, A-7-5, A-7-6), locally with trace gravel; tan, red, orange, and gray, dry to moist, medium stiff to very stiff, non-plastic, sandy silt (A-4); and red, brown, orange, gray, and tan, dry to saturated, very loose to very dense, silty and clayey, fine to coarse sand (A-2-4, A-2-6), locally with trace gravel. The interbedded Undivided Coastal Plain sediments do not appear to be laterally continuous over more than few hundred feet in any one direction. In general, apparent weathering decreases with depth and soil consistency or denseness increases with depth. All Undivided Coastal Plain sediments showed signs of oxidation and traces of iron staining.

Laboratory Testing

Laboratory testing was conducted on collected Undivided Coastal Plain soil samples located near and above the proposed grade throughout the project corridor. In total, forty (40) samples were submitted to Summit's laboratory. Of those, seventeen (17) were AASHTO classified as either A-7-5 or A-7-6. In general, A-7 classified soils are composed of clay with moderate amounts of fine to coarse sand. They may be highly elastic and may have moderate to high plasticity indexes. The table below provides a summary of the results of the laboratory testing for the A-7 classified soils:

	<u> Liquid Limit (L.L)</u>	<u>Plastic Limit (P.L.)</u>	<u>Plasticity Index (P.I.)</u>	<u>Natural Moisture</u>	Passing # 200 Sieve
LOW	41	22	15	14.0%	42%
HIGH	77	53	39	26.9%	80%
AVERAGE	51	29	22	19.9%	58%

Seven (7) of the forty tested samples of Undivided Coastal Plain soil were AASHTO classified as A-6. In general, A-6 classified soils are composed of silt and clay with moderate amounts of fine to coarse sand. The table below provides a summary of the results of the laboratory testing for the A-6 classified soils:

	<u> Liquid Limit (L.L)</u>	Plastic Limit (P.L.)	Plasticity Index (P.I.)	<u>Natural Moisture</u>	Passing # 200 Sieve
LOW	29	15	12	10.5%	37%
HIGH	40	26	20	16.7%	78%
AVERAGE	35	20	15	14.3%	50%

Three (3) of the forty tested samples of Undivided Coastal Plain soil were AASHTO classified as A-4. In general, A-4 classified soils are composed of fine to coarse sand with moderate amounts of silt and clay. The table below provides a summary of the results of the laboratory testing for the A-4 classified soils:

	<u> Liquid Limit (L.L)</u>	<u>Plastic Limit (P.L.)</u>	<u>Plasticity Index (P.I.)</u>	<u>Natural Moisture</u>	Passing # 200 Sieve
LOW	16	12	4	10.8%	38%
HIGH	25	21	5	19.3%	46%
AVERAGE	20	16	4	15.1%	41%

The remaining thirteen (13) tested samples of Undivided Coastal Plain soil were classified as non-cohesive or granular materials. The AASHTO results for these samples were as follows: ten (10) samples were classified as A-2-4, and three (3) samples were classified as A-2-6/A-2-7. The results showed that most of the granular soils within the project corridor contain silt and clay binder materials. For additional laboratory information on these samples and all samples tested within the project corridor, please refer to Appendix A "Laboratory Test Results" sheets 38-40 of this report.

Groundwater Properties

The geotechnical investigation was conducted during a period of average rainfall. Groundwater was encountered in six (6) of the borings, with most of the borings showing as dry 24 hours after boring completion. Where encountered, groundwater depths ranged from 0.5 feet to 12.2 feet below existing ground surface and elevations ranged from 359.9 feet to 368.4 feet above sea level. Areas that showed wet to saturated soils and shallow groundwater were typically adjacent to existing ponds along the project alignment. Approximate locations where groundwater may be present within six feet of proposed grade are noted in the section, "Areas of Special Geotechnical Interest."

A visual reconnaissance of springs, seeps, ponds, or lakes was also conducted. In addition, a visual reconnaissance for water wells was conducted throughout the project corridor. This was used in conjunction with the final survey file to attempt to identify water wells within or immediately adjacent to the proposed right of way of the project. Some water well locations are well hidden, and it is possible that some wells were missed or misidentified by the final survey and/or visual reconnaissance. Approximate locations of ponds and wells present close to or within the proposed right of way are noted in the section, "Areas of Special Geotechnical Interest."

Areas of Special Geotechnical Interest

<u>Highly Plastic Soils</u> – The following areas contain highly plastic soils within areas of proposed cut or proposed subgrade which have the potential to cause embankment/subgrade and/or slope stability problems during construction:



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<u>Alignment</u>	<u>Station (±)</u>	<u>Offset</u>
-L-	25+75.00 – 27+75.00	Right

<u>High Groundwater</u> - During the geotechnical investigation, wet to saturated soils and/or shallow groundwater was encountered in a few areas of the project corridor and adjacent to existing ponds along the proposed alignment. The following approximate locations listed below show areas where groundwater is believed to be present within six (6) feet of proposed grades:

<u>Alignment</u>	<u>Station (±)</u>	<u>Offset</u>
-[-	15+25.00 – 18+25.00	Right
-L-	23+60.00 – 25+75.00	Left

<u>Ponds</u> – Three ponds occur within proximity to the proposed right of way on this project at the following locations:

<u>Alignment</u>	<u>Station (±)</u>	<u>Offset</u>
-L-	14+98 to 18+36	47' to 175' Right
-L-	23+47 to 23+96	23' to 101' Right
-L-	23+98 to 25+64	60' to 230' Left

<u>Wells</u> – Residential water supply wells were observed close to or within the proposed right of way on this project at the following locations:

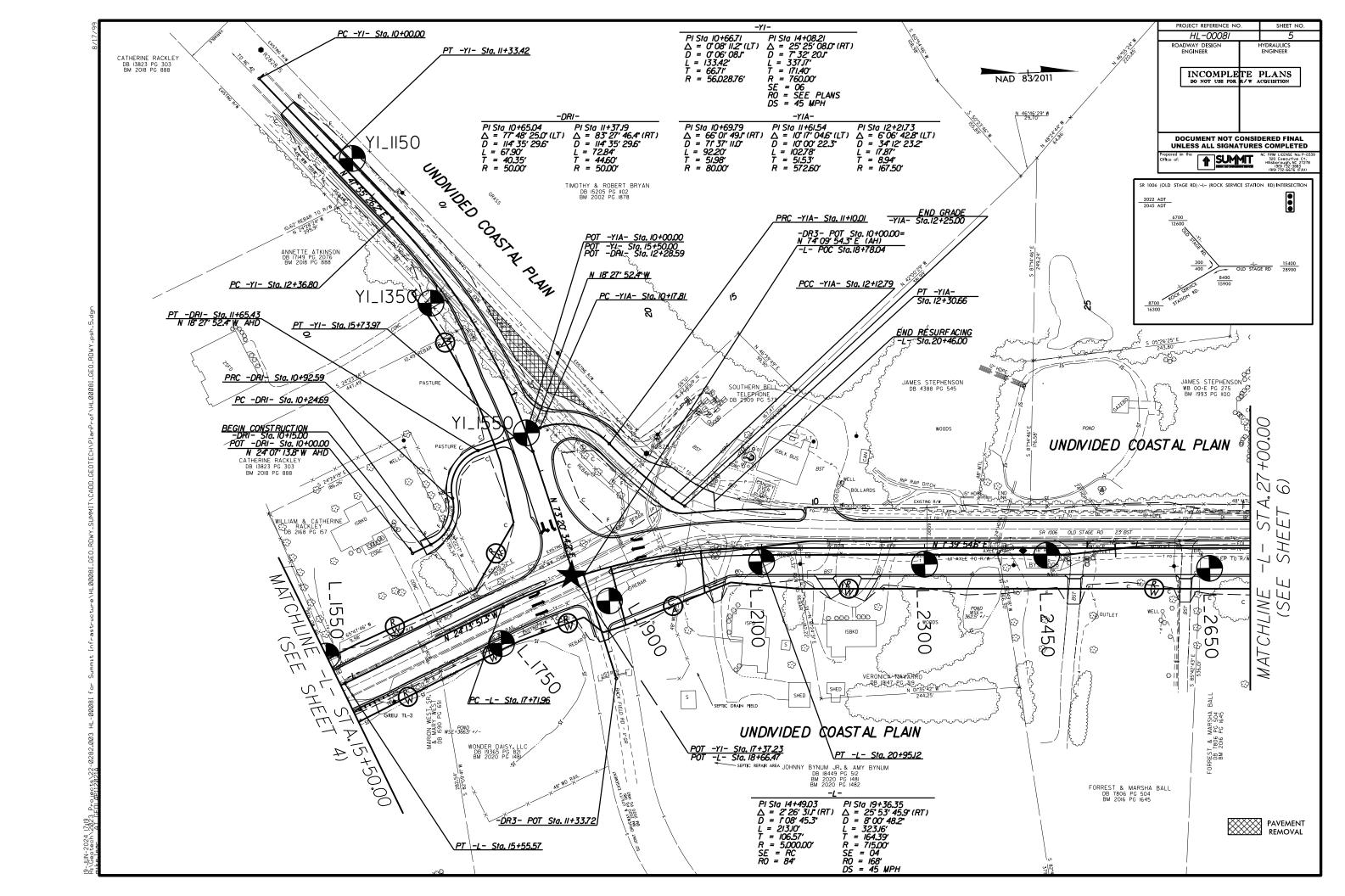
<u>Alignment</u>	<u>Station (±)</u>	<u>Offset</u>
-L-	25+93	78' Right
-L-	28+03	59' Right
-L-	49+06	24' Left

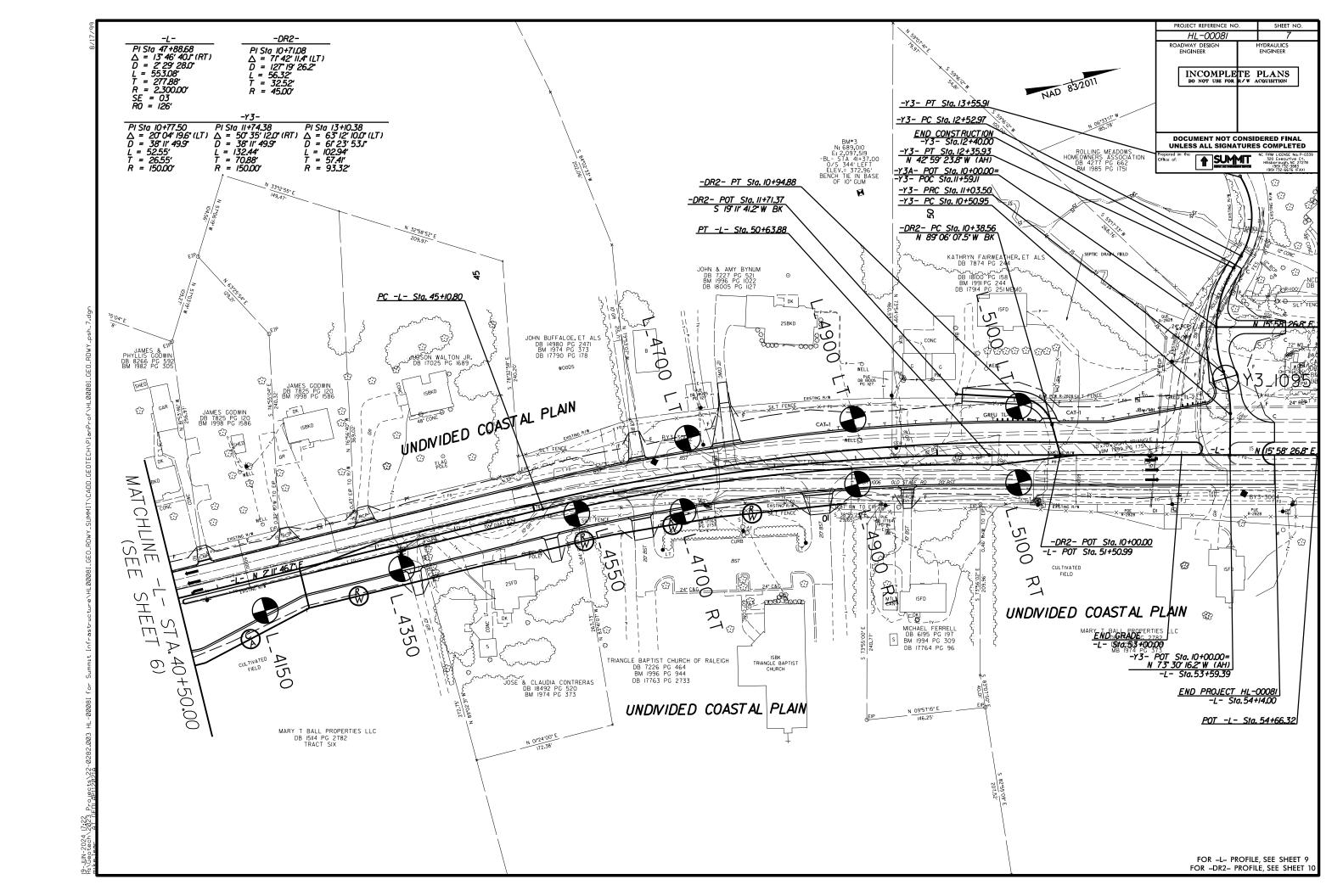
Respectfully Submitted,

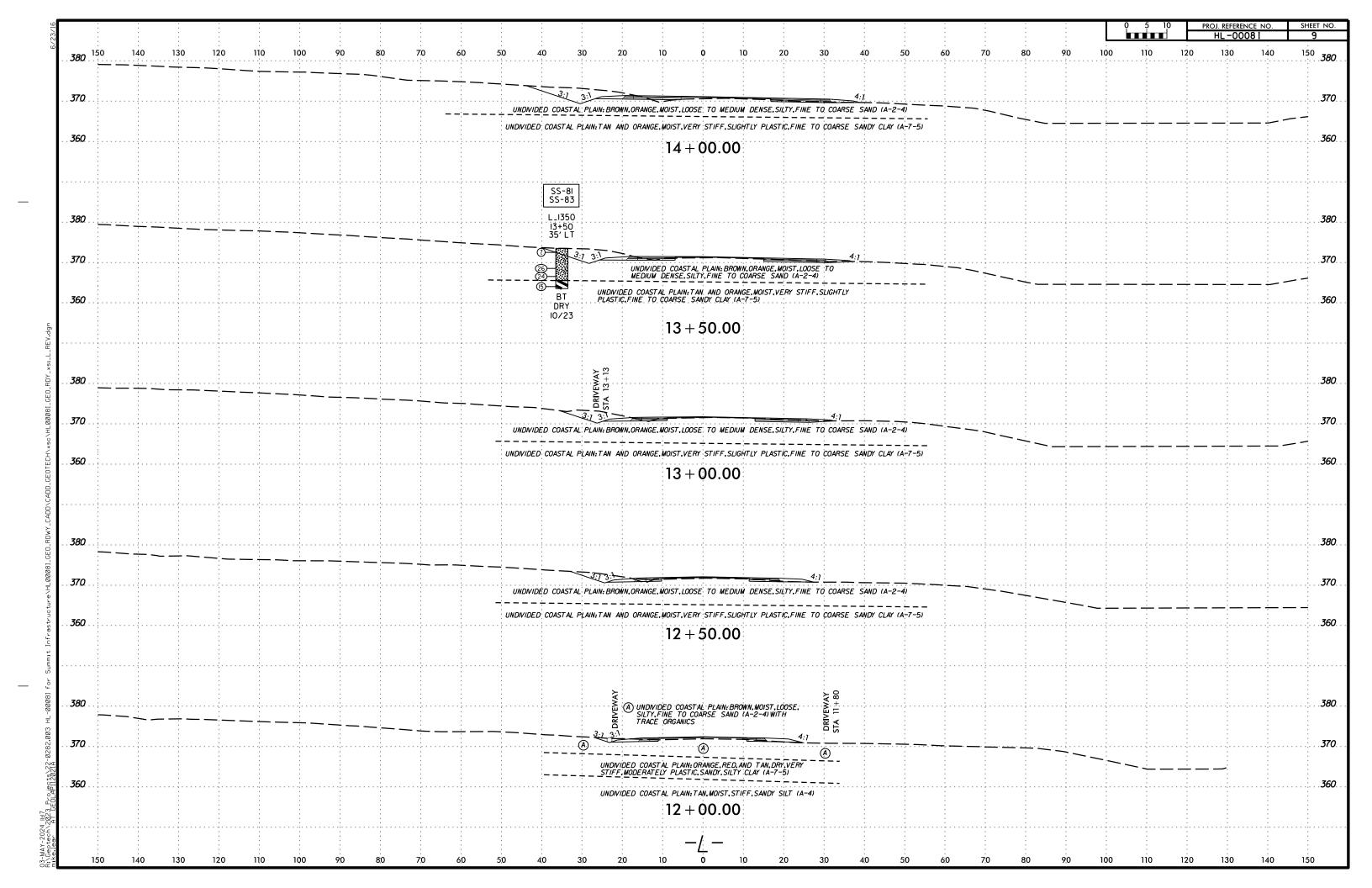
Michael B. Lear, PG Senior Geologist

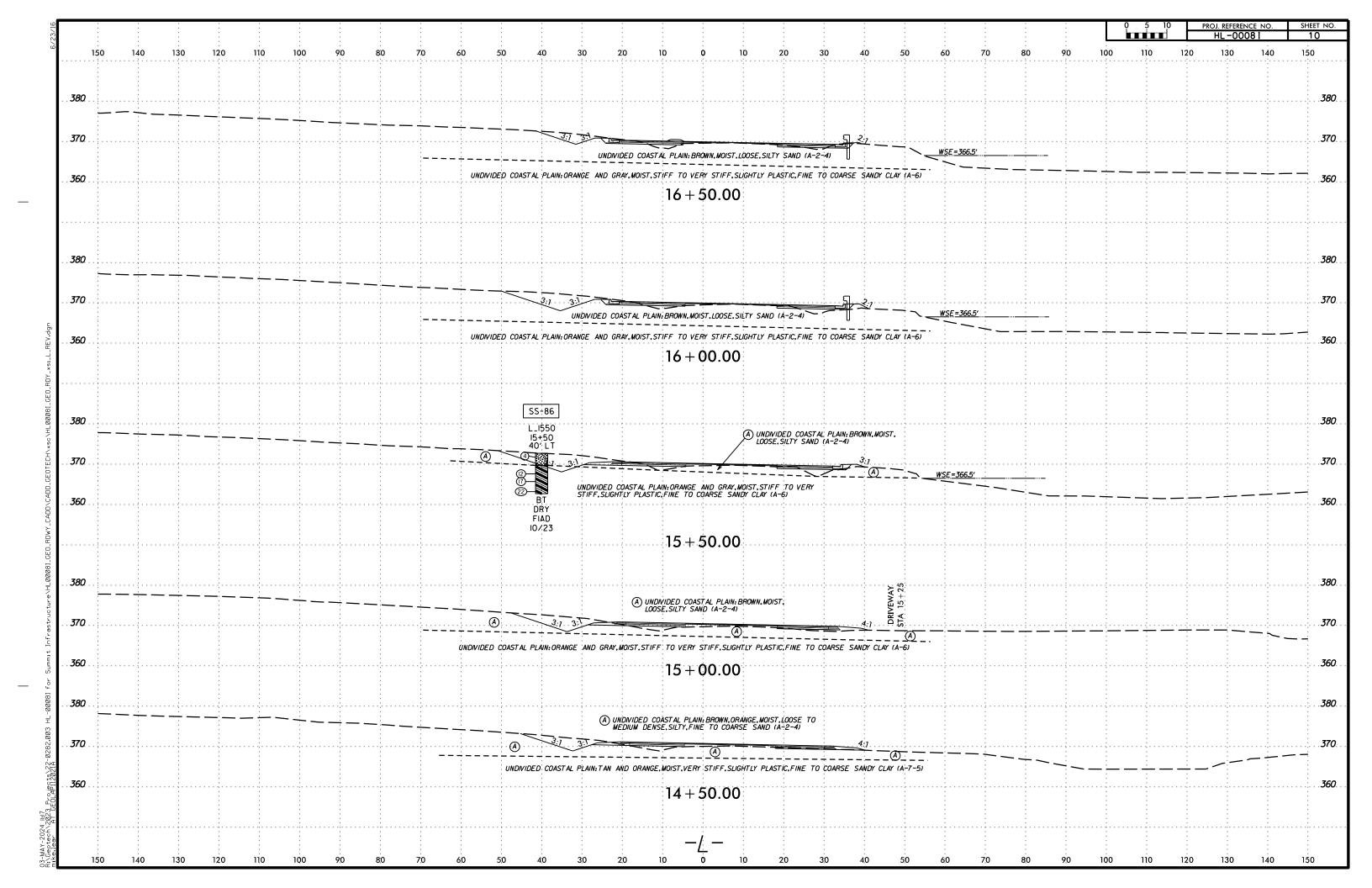
Summit Design and Engineering Services, PLLC

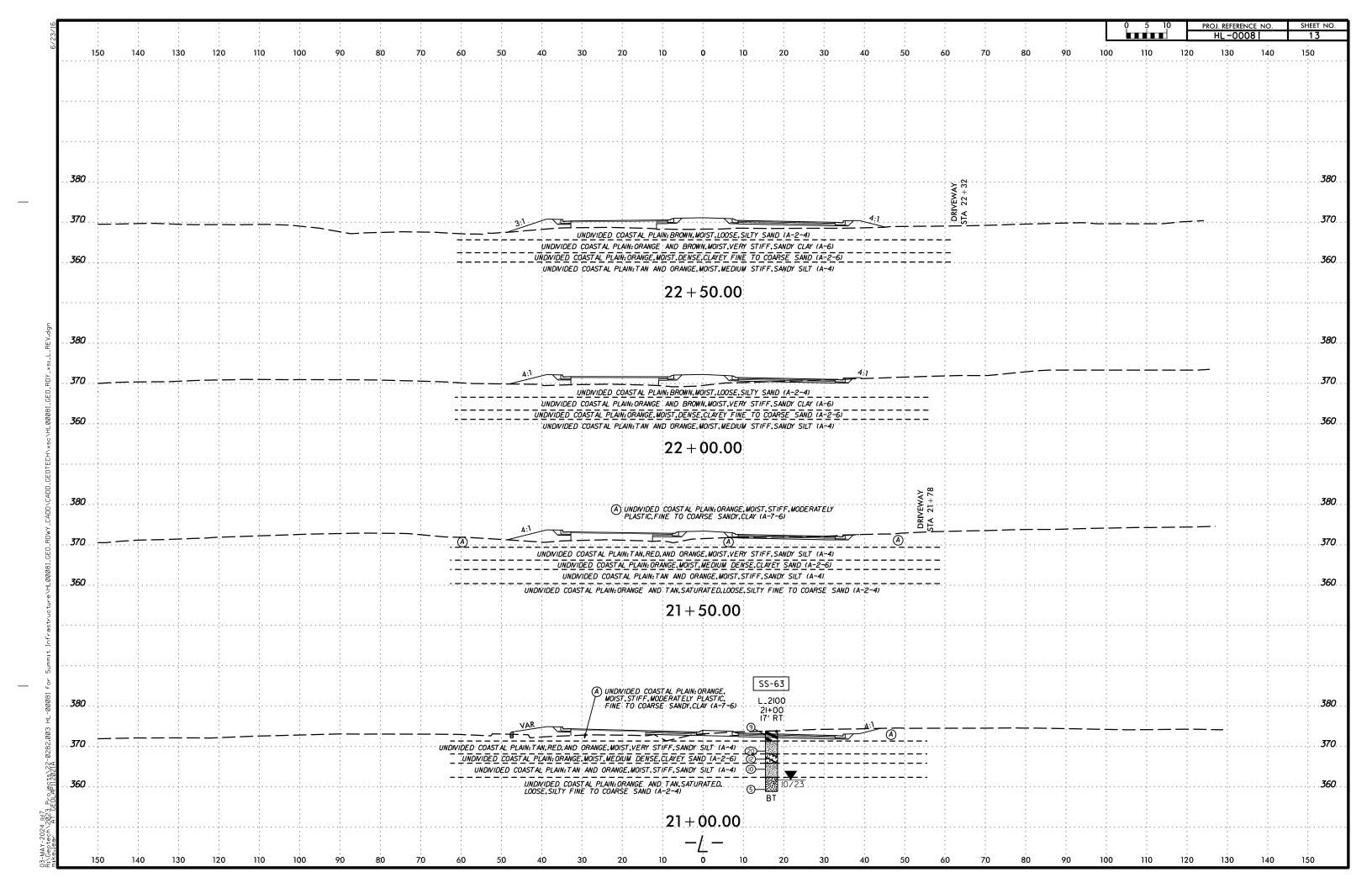
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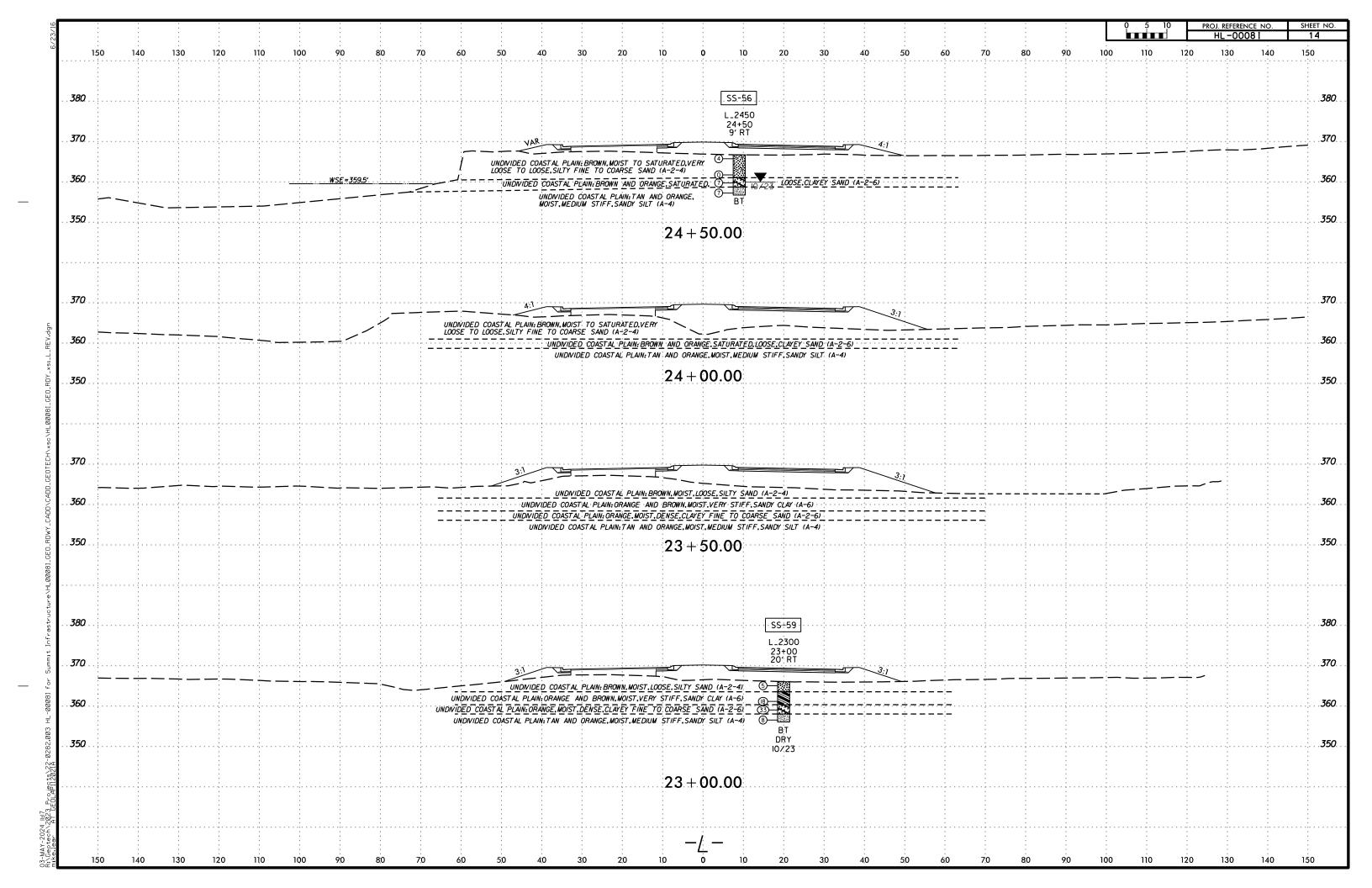


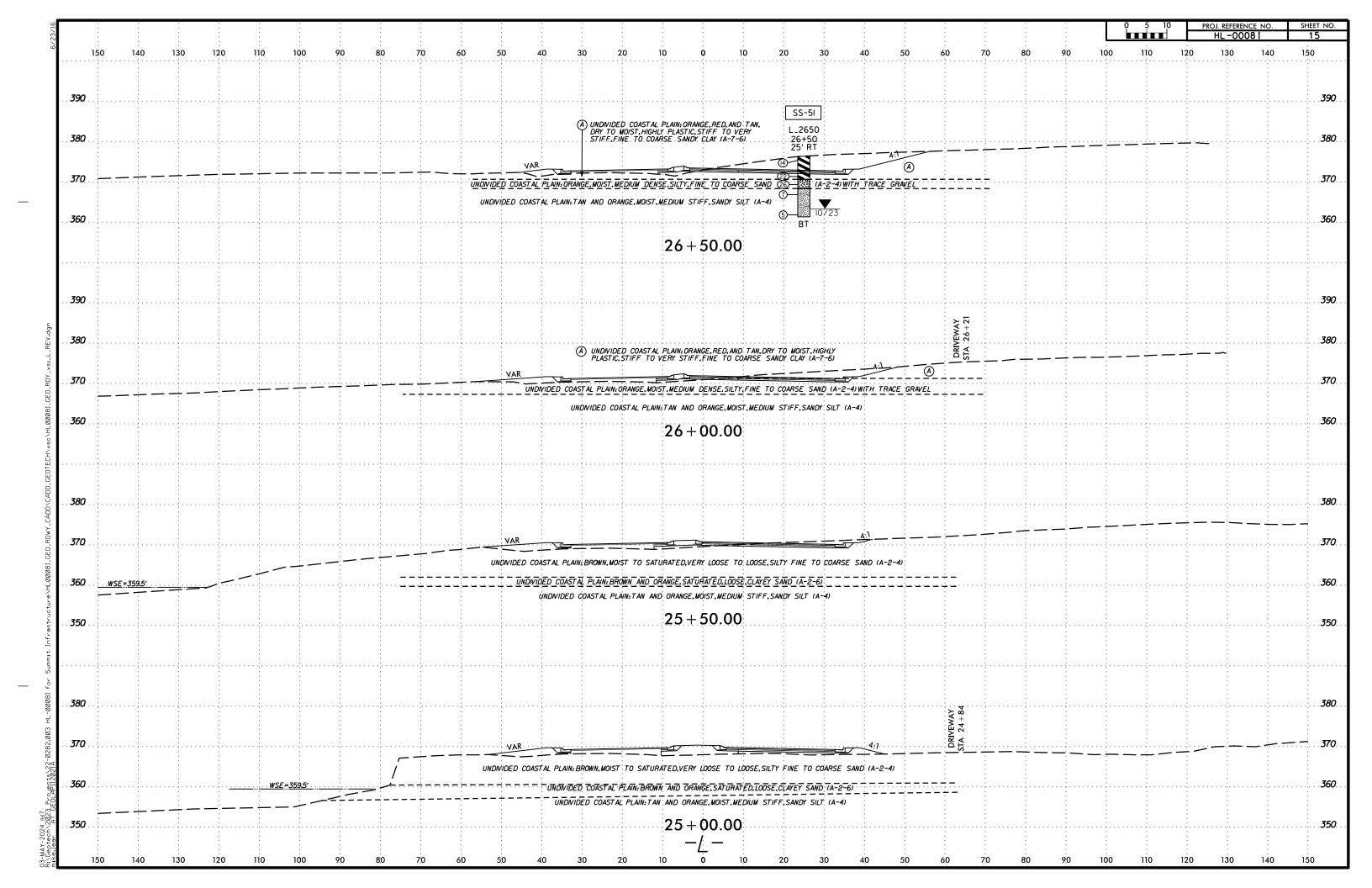


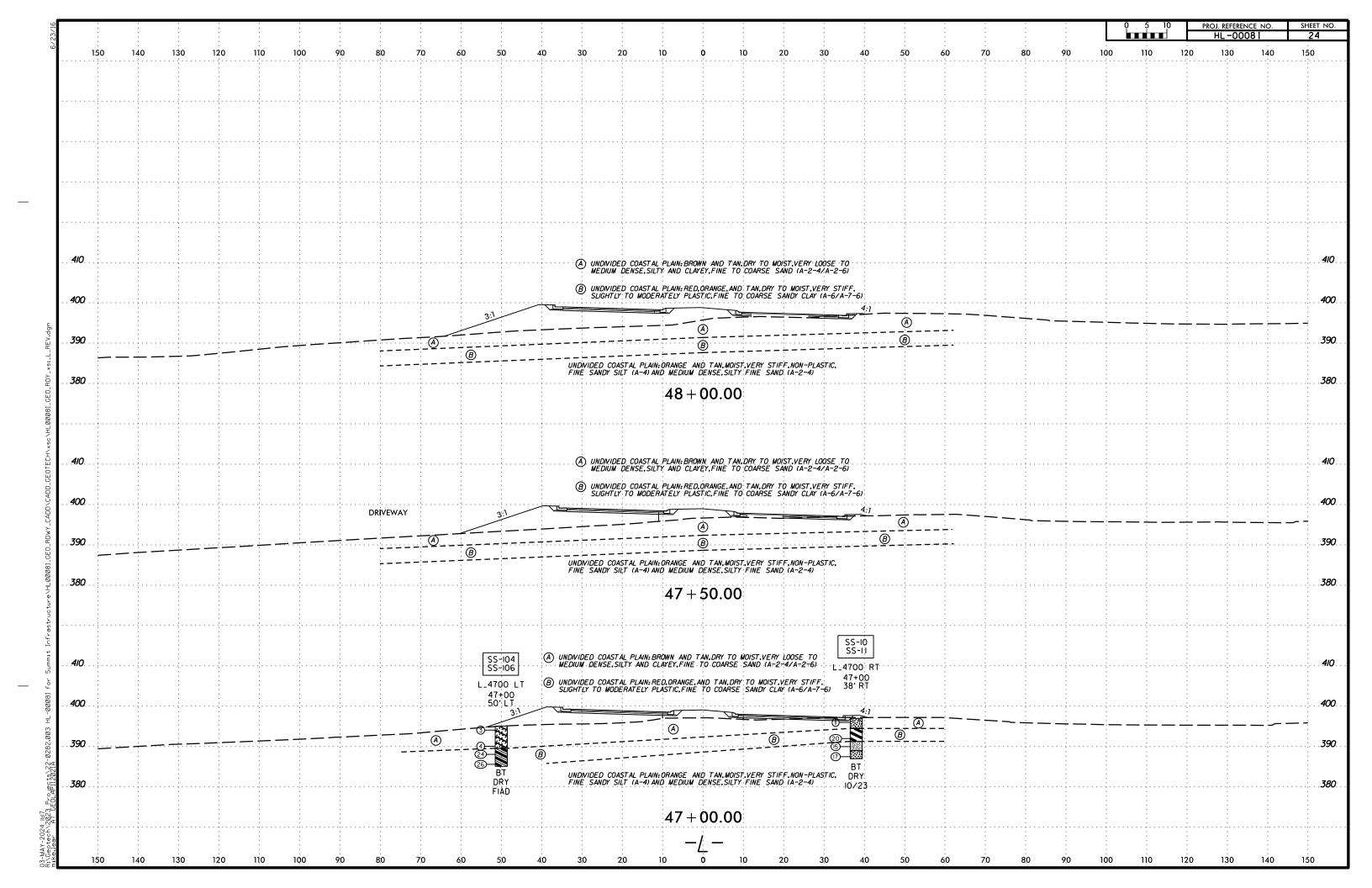


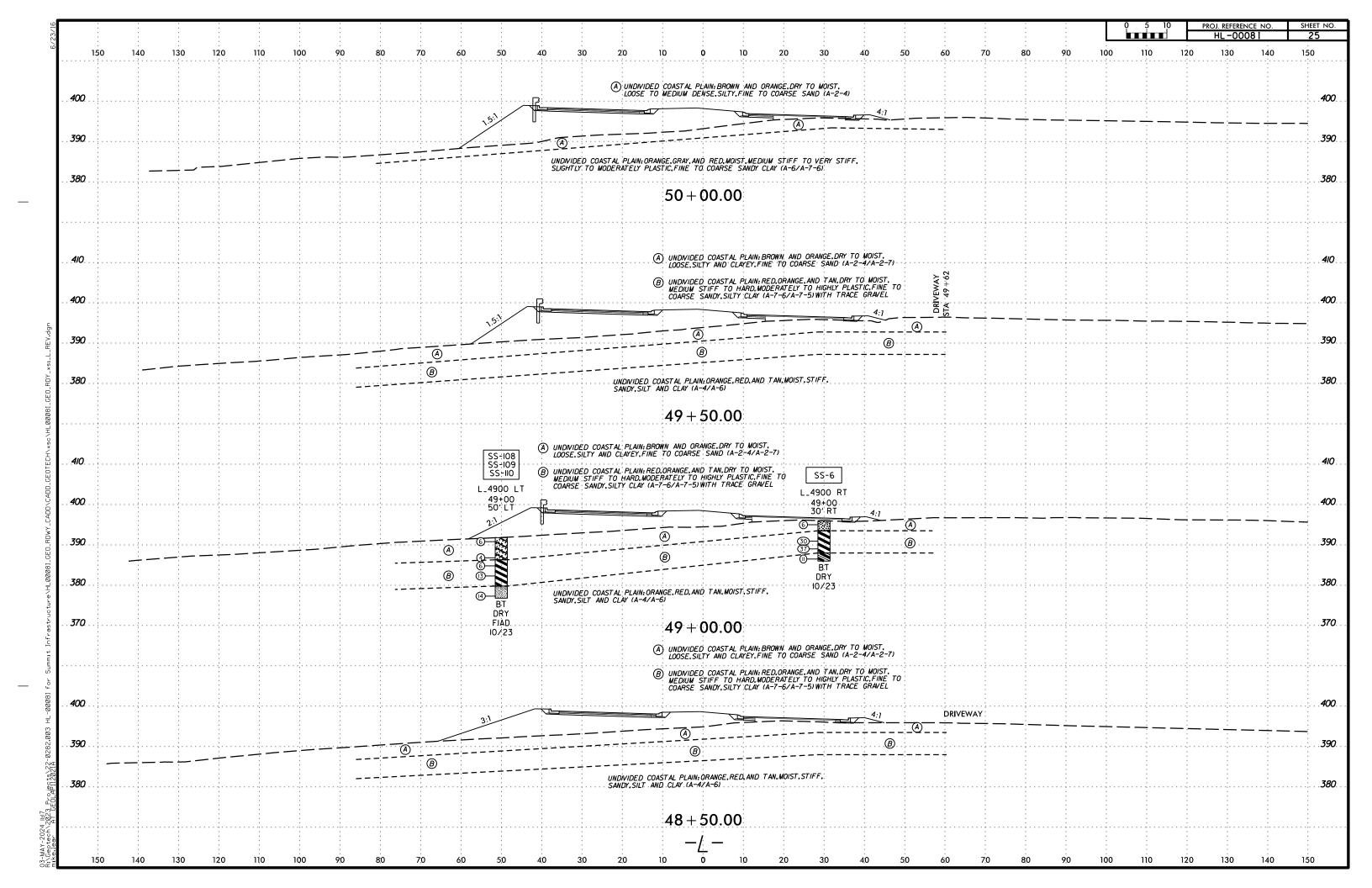


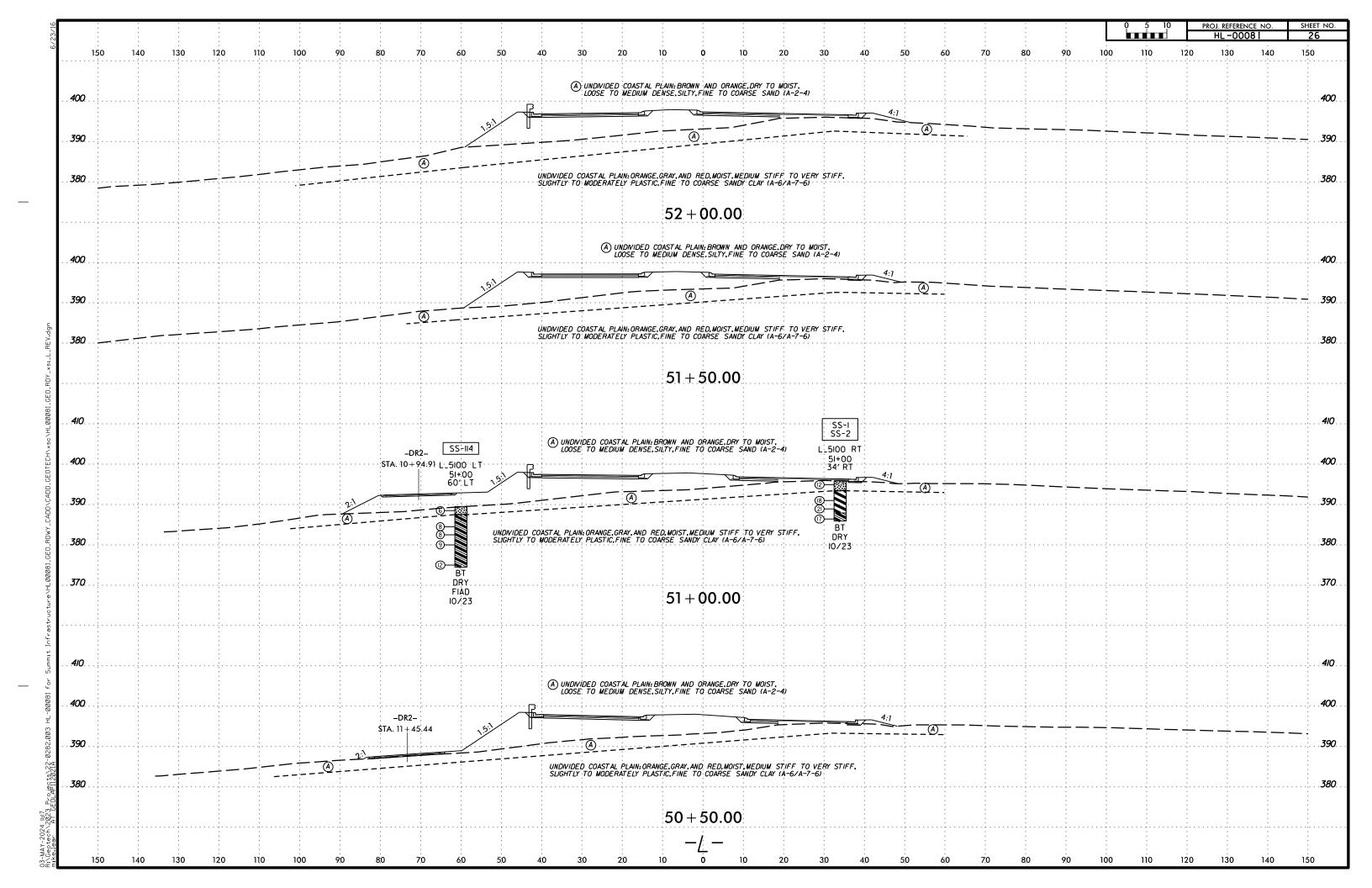


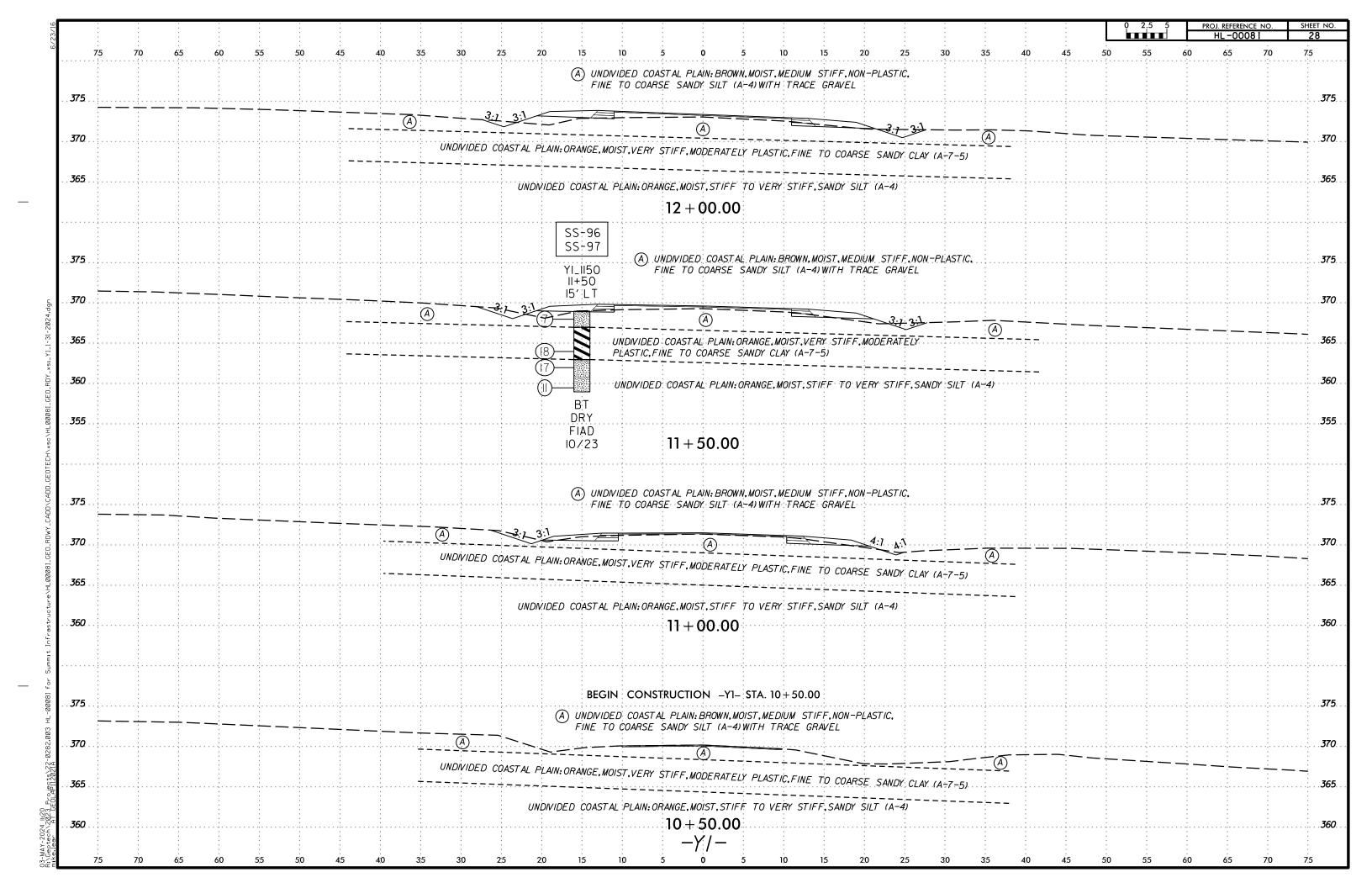


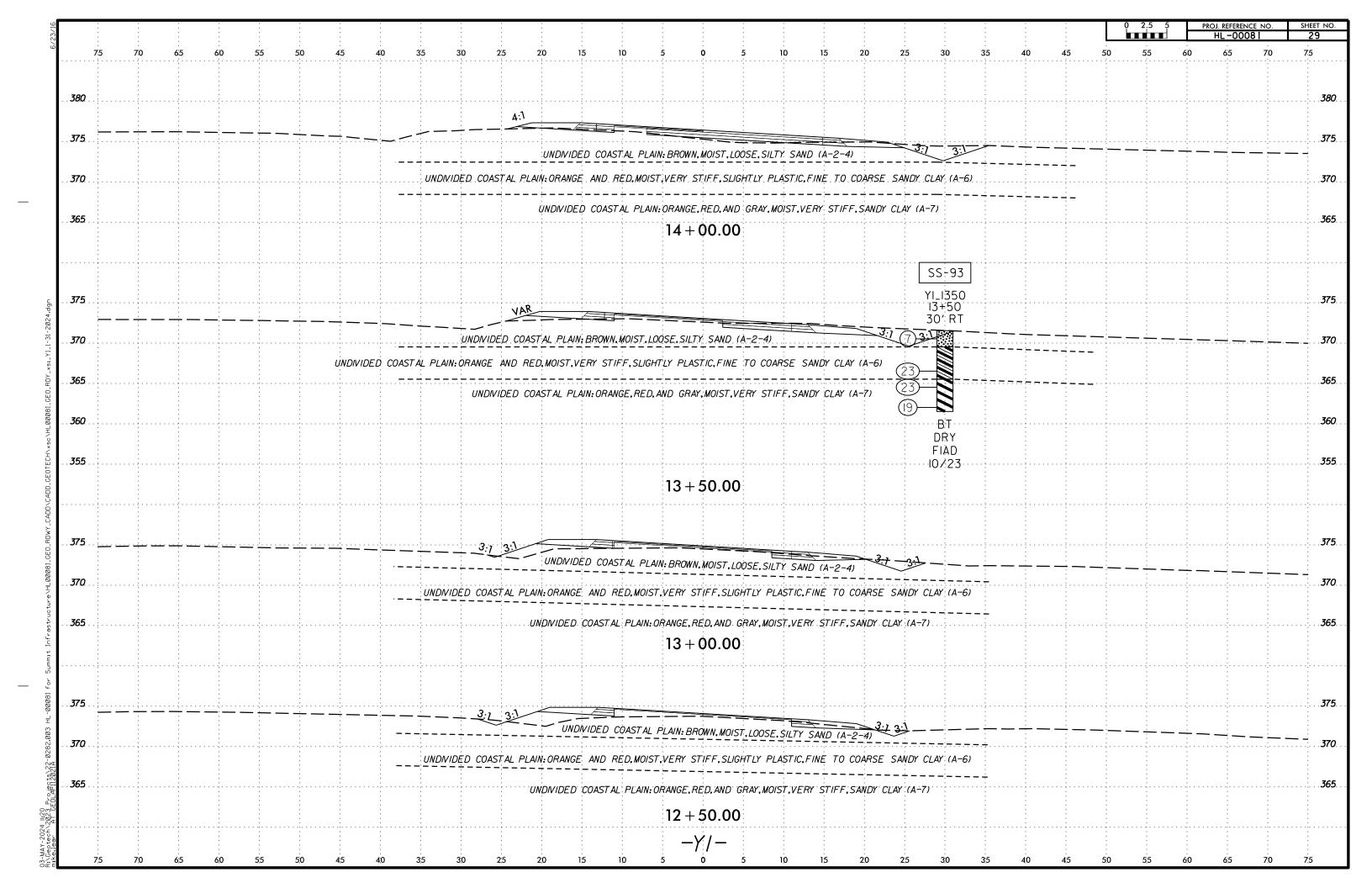


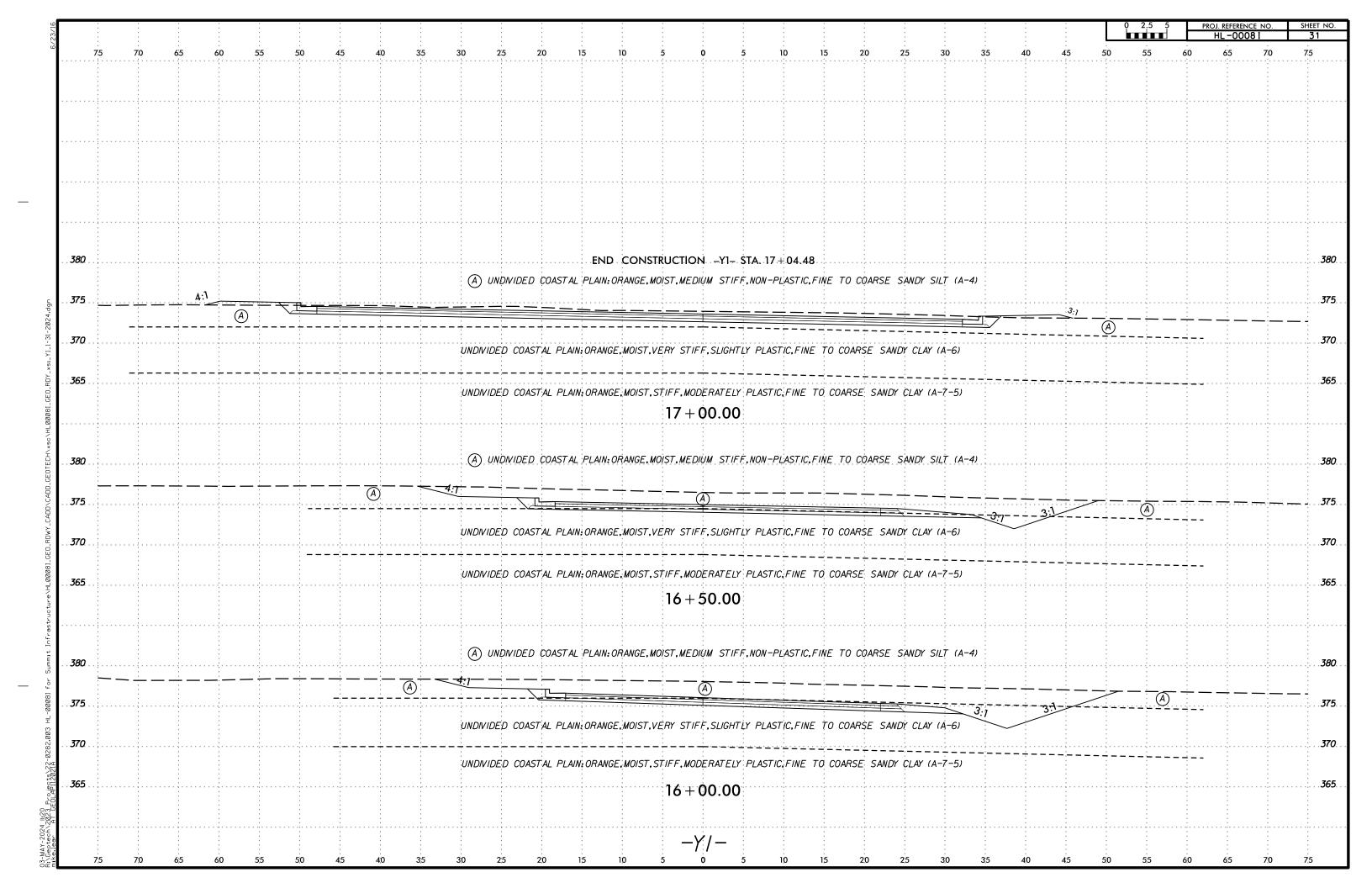


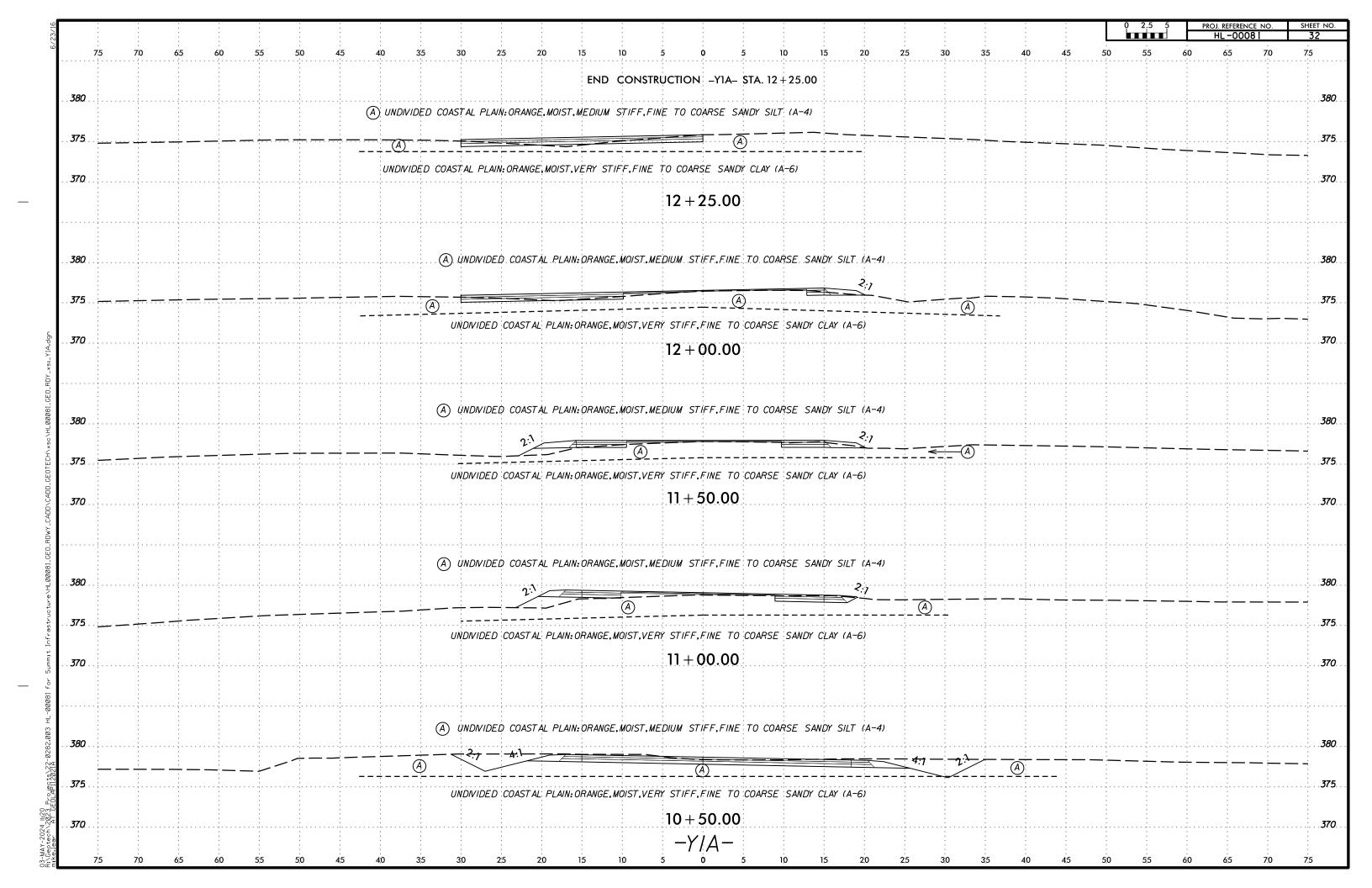


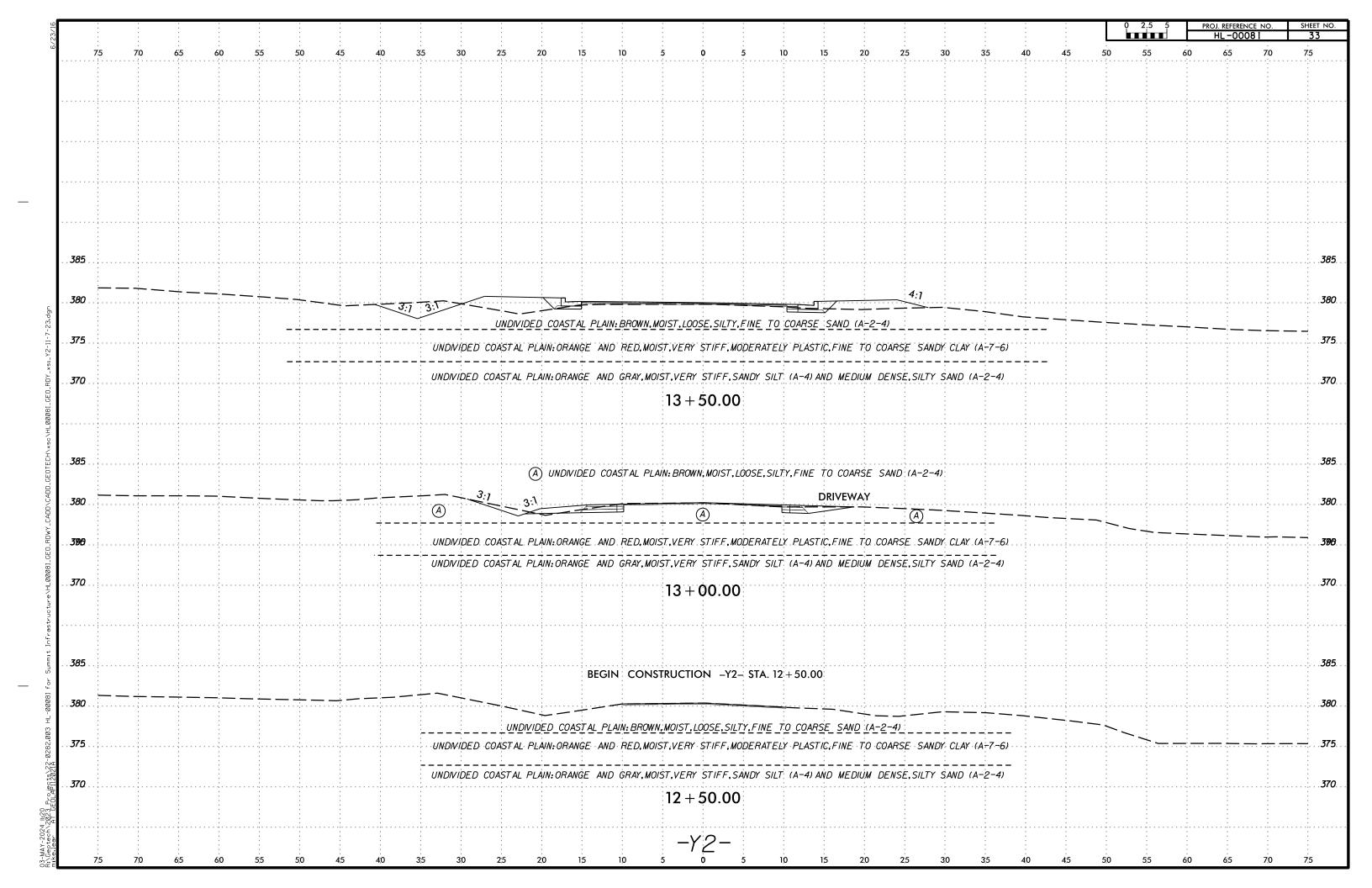


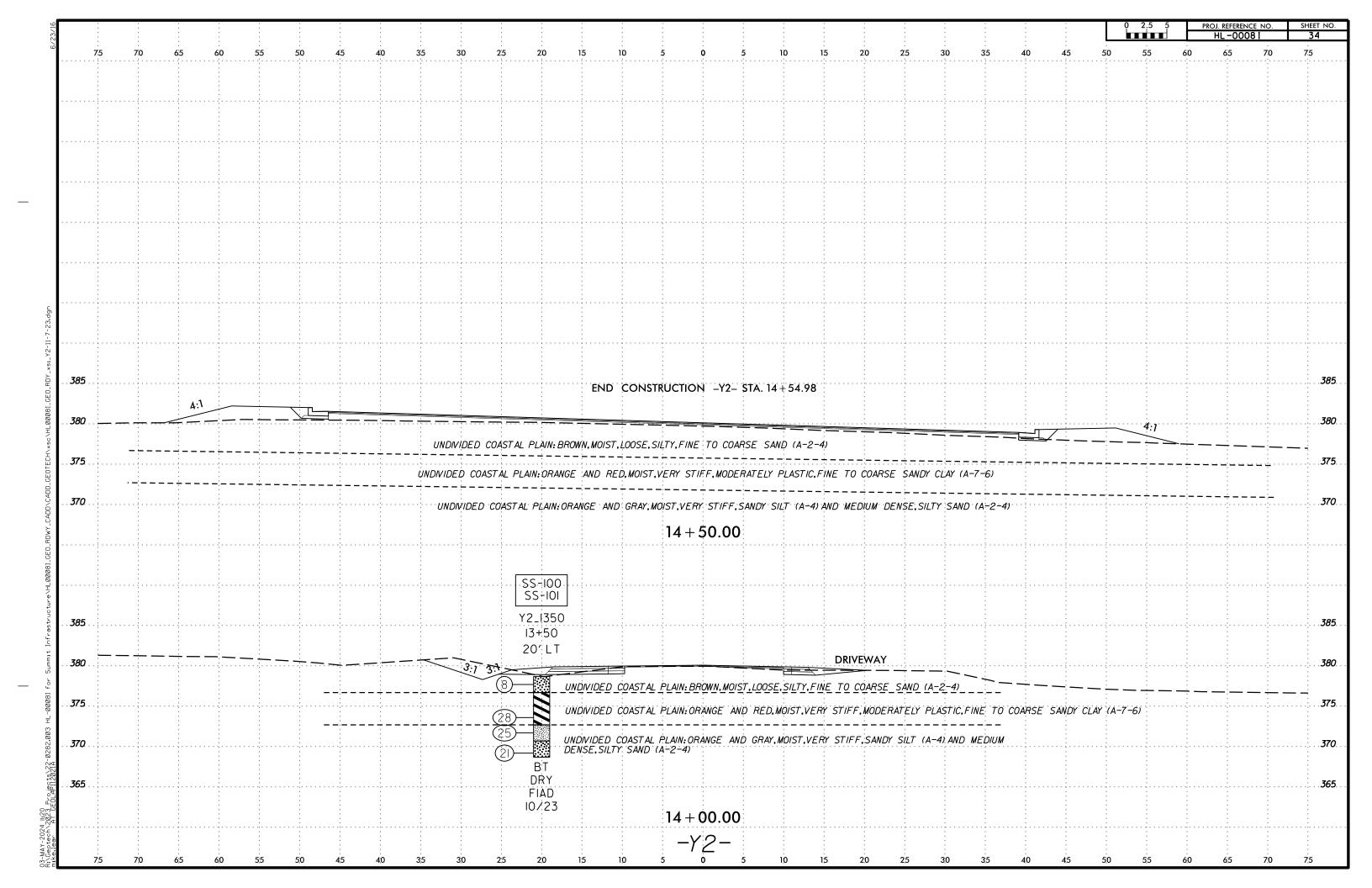


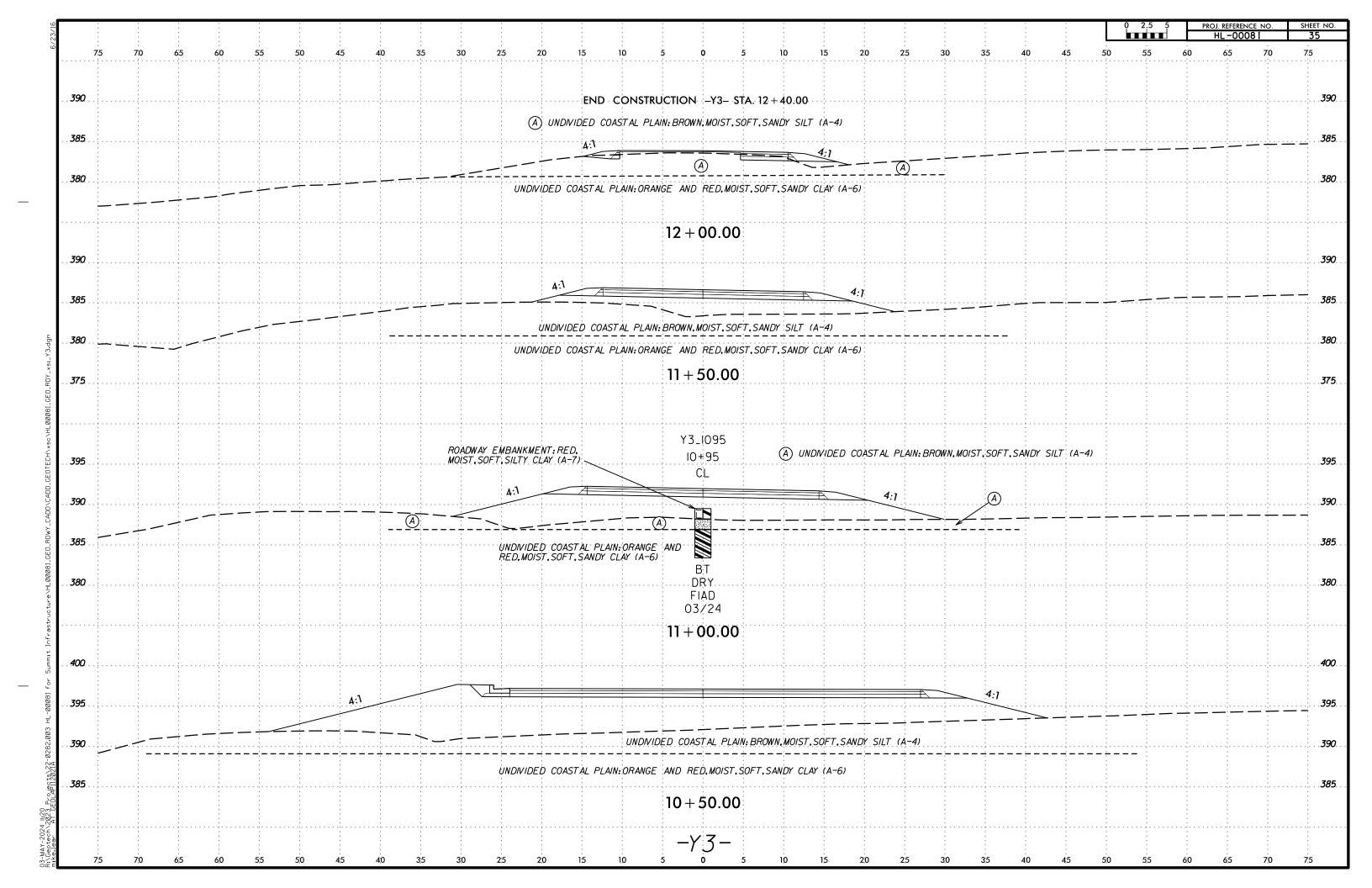


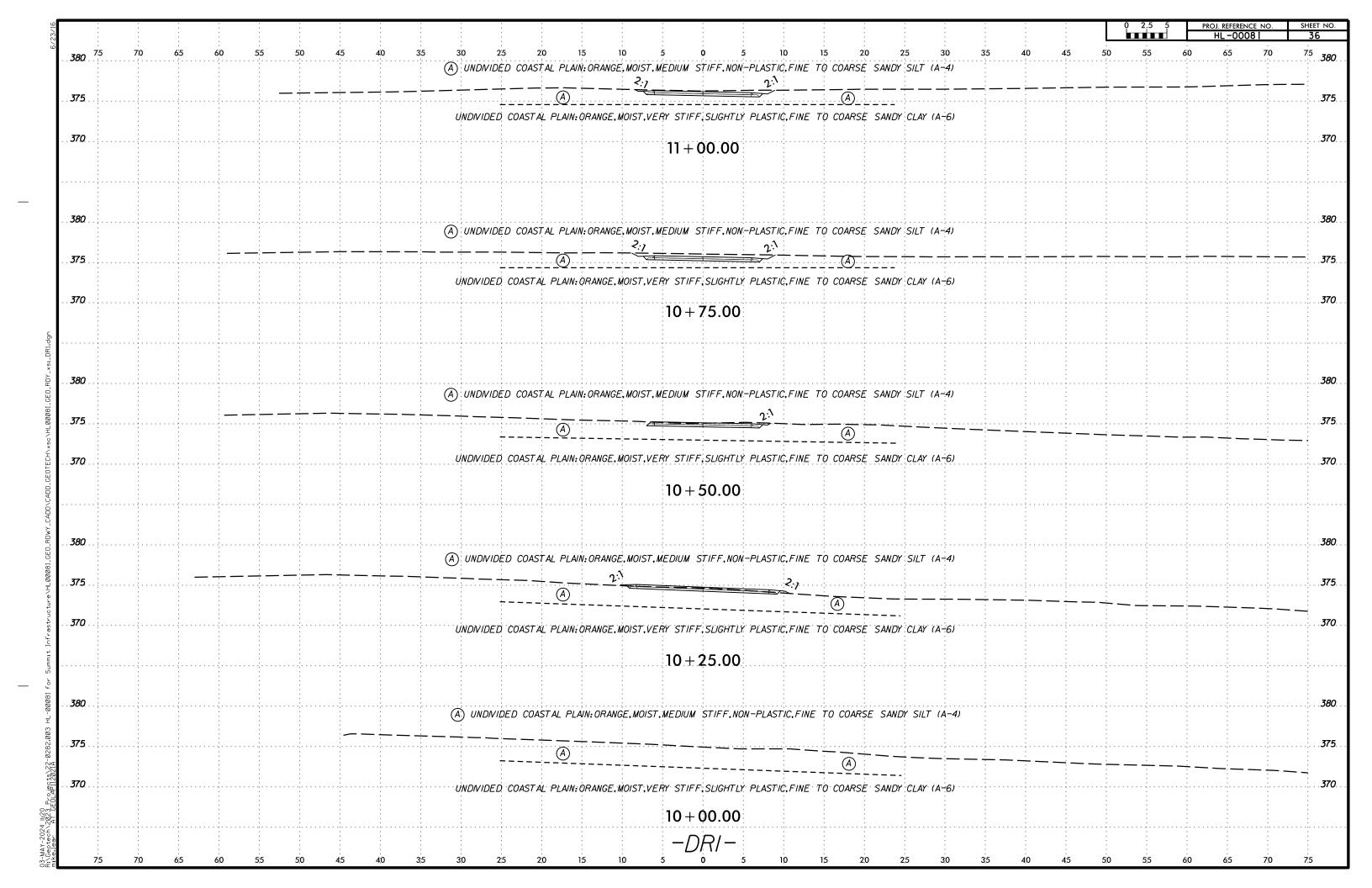












NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION APPENDIX A LABORATORY TEST RESULTS REFERENCE:

49367

PROJECT REFERENCE NO.

HL-00081

38

Prepared in the Office of:



SUMMARY OF LABORATORY DATA

WBS Number: 49367.1.9 TIP Number: HL-0008I County: WAKE

Description: Widening of SR 1006 (Old Stage Road) From SR 2736 (Rock Station Service Road) to SR 3884 (Rolling Meadows Drive)



								SOIL	TEST R	ESULTS	5								
	BORING	NORTH	EAST	ALIGNMENT	STATION	T	DEPTH INTERVAL	AASHTO CLASS.	T	T	% BY WEIGHT				% PASSING SIEVES			%	%
SAMPLE NO.						OFFSET	(ft)		L.L.	P.I.	C. SAND	F. SAND	SILT	CLAY	10	40	200	MOISTURE	
SS-76	L_1150	685224	2097999	-L-	11+50	30' LT	0.0-1.5	A-2-4(0)	16	2	41.8	30.1	9.4	18.7	99	75	30	11.9	T -
SS-77	L_1150	685224	2097999	-L-	11+50	30' LT	4.0-5.5	A-7-5(15)	50	16	9.4	14.8	20.5	55.3	97	90	79	25.2	-
SS-81	L_1350	685401	2097909	-L-	13+50	35' LT	4.0-5.5	A-2-4(0)	23	0	42.7	34.0	4.7	18.6	100	80	26	16.1	-
SS-83	L_1350	685401	2097909	-L-	13+50	35' LT	8.5-10.0	A-7-5(9)	48	15	20.6	21.3	9.3	48.8	100	89	64	23.0	-
SS-86	L_1550	685581	2097818	-L-	15+50	40' LT	6.0-7.5	A-6(4)	33	15	25.2	29.7	10.7	34.4	100	85	52	14.4	-
SS-73	L_1750	685796	2097809	-L-	17+50	40' RT	3.7-5.2	A-2-4(0)	16	1	50.4	36.0	5.5	8.1	99	70	19	17.3	-
SS-69	L_1900	685930	2097760	-L-	19+00	40' RT	4.0-5.5	A-7-5(35)	72	39	9.4	16.7	19.4	54.5	97	90	80	23.7	-
SS-63	L_2100	686119	2097718	-L-	21+00	17' RT	0.0-1.5	A-7-6(7)	45	21	31.7	18.4	7.4	42.5	95	75	51	18.6	-
SS-59	L_2300	686318	2097726	-L-	23+00	20' RT	0.0-1.5	A-2-4(0)	15	0	47.0	38.2	5.0	9.8	98	72	20	5.3	-
SS-56	L_2450	686469	2097720	-L-	24+50	9' RT	4.0-5.5	A-2-4(0)	14	0	56.1	33.0	3.2	7.7	94	64	13	15.8	-
SS-51	L_2650	686668	2097742	-L-	26+50	25' RT	4.0-5.5	A-7-6(7)	53	28	41.6	15.2	7.9	35.3	95	75	43	16.4	-
SS-46	L_2850	686867	2097778	-L-	28+50	56' RT	4.1-5.6	A-2-6(1)	37	16	52.1	16.0	4.1	27.8	99	74	33	11.6	-
SS-42	L_3050	687068	2097759	-L-	30+50	30' RT	3.9-5.4	A-7-6(9)	49	21	27.6	19.6	4.0	48.8	98	83	55	18.2	-
SS-37	L_3350	687357	2097780	-L-	33+40	40' RT	0.0-1.5	A-2-4(0)	13	0	39.9	39.4	6.9	13.8	99	80	26	5.2	-
SS-38	L_3350	687357	2097780	-L-	33+40	40' RT	4.0-5.5	A-7-6(5)	41	19	34.7	23.5	3.1	38.7	100	80	45	14.1	-
SS-32	L_3550	687566	2097799	-L-	35+50	51' RT	0.0-1.5	A-6(2)	29	14	33.7	27.5	6.2	32.6	98	79	42	10.5	-
SS-33	L_3550	687566	2097799	-L-	35+50	51' RT	4.0-5.5	A-6(4)	40	20	39.0	22.4	4.0	34.6	99	77	41	16.7	-
SS-24	L_3950	687967	2097794	-L-	39+50	30' RT	0.0-1.5	A-2-4(0)	15	3	35.7	34.3	9.8	20.2	97	80	34	9.1	-
SS-25	L_3950	687967	2097794	-L-	39+50	30' RT	4.1-5.6	A-7-6(8)	47	22	29.3	22.1	6.7	41.9	98	85	51	19.3	-
SS-17	L_4350	688342	2097808	-L-	43+25	30' RT	0.0-1.5	A-2-4(0)	14	0	46.4	28.3	5.9	19.4	99	72	29	6.5	-
SS-18	L_4350	688342	2097808	-L-	43+25	30' RT	3.9-5.4	A-7-6(11)	48	22	24.9	19.2	7.4	48.5	98	85	58	18.7	-
SS-104	L_4700 LT	688723	2097751	-L-	47+00	50' LT	0.0-1.5	A-2-6(2)	35	19	35.4	29.6	1.1	33.9	91	75	35	16.8	-
SS-106	L_4700 LT	688723	2097751	-L-	47+00	50' LT	6.0-7.5	A-6(2)	39	18	45.1	19.1	3.9	31.9	99	65	37	14.8	-
SS-10	L_4700 RT	688693	2097836	-L-	46+80	38' RT	4.0-5.5	A-7-6(9)	42	15	15.5	28.1	9.9	46.5	94	84	66	18.2	-
SS-11	L_4700 RT	688693	2097836	-L-	46+80	38' RT	6.0-7.5	A-4(0)	25	4	9.3	63.7	7.9	19.1	100	99	46	15.2	-
SS-108	L_4900 LT	688924	2097784	-L-	49+00	50' LT	0.0-1.5	A-2-7(4)	51	29	35.4	27.7	ND	ND	88	74	35	16.8	-
SS-109	L_4900 LT	688924	2097784	-L-	49+00	50' LT	6.0-7.5	A-7-5(19)	62	32	22.9	16.9	8.4	51.8	93	79	62	17.3	-
SS-110	L_4900 LT	688924	2097784	-L-	49+00	50' LT	8.5-10.0	A-7-6(15)	47	24	22.2	26.7	15.0	36.1	97	82	66	20.4	-
SS-6	L_4900 RT	688908	2097862	-L-	49+00	30' RT	4.1-5.6	A-7-6(6)	45	22	33.4	20.2	9.0	37.4	93	74	46	19.7	-
SS-114	L_5100 LT	689124	2097825	-L-	51+00	60' LT	6.0-7.5	A-6(9)	38	12	10.2	41.8	12.4	35.6	99	91	78	16.7	-
SS-1	L_5100 RT	689099	2097915	-L-	51+00	34' RT	0.0-1.5	A-2-4(0)	13	0	36.1	42.2	10.0	11.7	97	79	29	7.0	-
SS-2	L_5100 RT	689099	2097915	-L-	51+00	34' RT	3.9-5.4	A-7-6(5)	42	17	31.0	24.3	4.7	40.0	97	80	48	17.6	-
SS-96	Y1_1150	685631	2097208	-Y1-	11+50	15' LT	0.0-1.5	A-4(0)	20	5	36.6	28.1	7.5	27.8	95	73	38	10.8	-
SS-97	Y1_1150	685631	2097208	-Y1-	11+50	15' LT	4.0-5.5	A-7-5(22)	77	24	15.2	17.7	6.4	60.7	98	89	72	26.7	-
SS-93	Y1_1350	685772	2097388	-Y1-	13+50	30' RT	4.0-5.5	A-6(5)	33	14	21.5	32.9	13.6	32.0	99	86	54	12.3	-
SS-88	Y1_1550	685834	2097551	-Y1-	15+50	CL	0.0-1.5	A-4(0)	16	4	39.0	25.3	7.9	27.8	95	74	38	19.3	-
SS-89	Y1_1550	685834	2097551	-Y1-	15+50	CL	3.9-5.4	A-6(4)	35	14	27.2	29.9	9.0	33.9	98	81	48	14.6	-
SS-91	Y1_1550	685834	2097551	-Y1-	15+50	CL	8.5-10.0	A-7-5(15)	58	23	21.3	16.1	9.6	53.0	100	88	65	26.9	-

SUMMARY OF LABORATORY DATA

WBS Number: 49367.1.9 TIP Number: HL-0008I

County: WAKE

Description: Widening of SR 1006 (Old Stage Road) From SR 2736 (Rock Station Service Road) to SR 3884 (Rolling Meadows Drive)



								SOIL	TEST R	ESULT	S								
SAMPLE NO.	BORING	NORTH	EAST	ALIGNMENT	STATION	OFFSET	DEPTH INTERVAL	AASHTO		P.I.	% BY WEIGHT			% PASSING SIEVES			%	%	
SAIVIPLE NO.	BOKING	NONTH	EAST	ALIGINIVIENT	STATION	OFFSET	(ft)	CLASS.	L.L.		C. SAND	F. SAND	SILT	CLAY	10	40	200	MOISTURE	ORGANIC
SS-100	Y2_1350	686900	2097585	-Y2-	13+50	20' LT	0.0-1.5	A-2-4(0)	14	0	43.6	36.6	11.3	8.5	99	76	25	7.9	-
SS-101	Y2_1350	686900	2097585	-Y2-	13+50	20' LT	4.1-5.6	A-7-6(5)	46	21	48.5	11.0	5.7	34.8	99	64	42	14.0	-

ND = NOT DETERMINED

Jonathan Pope	120-08-0107	Julin Dope
Technician Name	NCDOT Cert. Number	Signature