Note: Invert Elevations i	indicated	are for	Information	Purposes	only and	should	be ve
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											$\mathbb{N}$	RM				], ](	NA		FPA	RI	ז <b>™</b> ז	FN.	$\square$			$\mathbb{R}$ A		SP	$\bigcirc \mathbb{R}$			$\mathbb{T}$	N						L	I <i>-40</i> 15A		31	)-2
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	ь I	STRUC	ATION	VATION	VATION	IRED S													OR STD. 838.11		* TOT QUANT	. <b>A</b> .	STANDARE 840.03	CONCE		9 4	8 ES STE	ES STE ATES. S	0.840.3		.37					ш	). 840.7	40.72		N.D		NARROW DI INLET DROP INLI	
	OFFSE		, EL EV,	AT ELE	RT ELE	I REQU													(UNLESS NOTED						5 840.16	R 840.2 R 840.2	R 840.2 F GRAT	D GRAT	-T. ST[ 840.13		TD. 840 . 840.5					). & SIZ	.Y. STI	STD. 8		D.I G.D G.D.I.(I	.I. G	RATED DROF (NARROW S	INLET
SIZE			10 1	INVE	INVEF	NNINI 12	2" 15" 18" 24" 30"	" 36" 42" 48	в"	, d	12" 15" 18"	24" 30"	36" 42" 48	3" 12'' 15	" 18" 24" 30"	36'' 42''	48''		OTHERWISE) CU. YARDS		LIN. FT.	D. 840.			D. 840.1 E STD.	40.17 O 40.18 O	40.19 O	TH TWO	IT LIN. I B STD.	0.32	AME S			z		OWS NC	rng, c	B" C.Y.		J.E M.H		JUNCTION E MANHOL	BOX
	ŀ		$\neg$			M %			E CSP	E CAAF E CAAF IDPE, F C										HRU 5.				1	OR STD. ) GRATE	STD. 8. STD. 84	STD. 8. TTH TW	VITH T	DP INLET I CH SLAB	I OR 84 34 1 35	AND FR D COVI		HM	H DRA	L (CY)	)E ELB(	PIPE P	S CL.	LIN. FT	T.B.[		TRAFFIC BEA DROP INLI	RING ET
THICKNESS OR GAUGE		FROM	2						NOT USE		064 064 064	064 079	109	60					S P	CH (0' TI	U 10.0'	. 840.01	TYPE OF GRATE	LET BASIN	840.14 <u>ME AN</u> E	PE "A" PE "B"	PE "D" AME W	S.) FR/ S.) FR/	AY DRC	. 840.31 D. 840.3 TD 840.3	RATE /	MH CB	DI TO JBI	3 TO JE TRENC	ILE FIL	AGE PIF	BRICK	OLLAR	AOVAL	T.B.J	J.B.	TRAFFIC BEA JUNCTION E	RING
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SHEET 5																					· 2	- U				9 9 0					<u> </u>	<b>A A</b>				_	<u> </u>						
- L- 21+43.50	LT	501	502	809.7	809.5 C	0.5%	24			×																															HW/D = 1.02,	HW = 811.23	
- L- 21+50.00 - L- 21+50.00	-32 LT	502 502	812.8 503	809.0	804.1 C	).7%									176					1		1																					
- L- 23+25.00 - L- 23+25.00	-32 LT	503	807.9		802.8 C	) 7%									148					1		1	,																				
- L- 24+75.60	-32 LT	503	806.6																	1	0.2	1	1																				
- L- 24+75.60 - L- 25+25.00	-32 LT	504 505	509 806.7		798.3 2	2.1%	32	2												1		1	1																				
- L- 25+25.00 - L- 21+50.00	32 RT	505 506	504 812.8	803.7	803.6 0	).5%									18					1		1	1																				
- L- 21+50.00 - L- 23+25.00	RT 32 RT	506 507	507 807.9	809.8	804.9 C	).8%								17	76					1		1	1																				
- L- 23+25.00 - L- 24+75.60	RT	507 508	508 806.6	804.6	803.3 C	0.6%									148					1		1	1																				
- L- 24+75.60	RT	508	504	802.8	802.6	).4%									60																												
-Y1- 11+56.46 -Y1- 11+56.09	20 RT -20 LT	510 511	818.7 818.8	-																												1											
- L- 26+05.00 - L- 26+05.00	33 RT RT	512 512	807.5 513	804.5	804.4 C	).8%									36					1		1																					
- L- 26+42.50 - L- 26+42.50	39 RT RT	513 513	808.4 514	1 1	804.3 1	.9%	36		+	×										1		1																					
- L- 26+42.50 - L- 26+42.50	-32 LT LT	515 515	808.2 516	_	804.9 C	).4%								1(	00					1		1	1																				
- L- 27+45.00 - L- 27+45.00	-32 LT	516	810.8	804.9		5%	24			×										1	0.9	1	1																				
- L- 28+60.54	-32 LT	518	814.5																	1		1	1																				
- L- 28+60.54 - Y1- 10+50.00	48 RT	518 520	516 816.5			0.5%								1						1	1.0	1																					
- Y1- 10+50.00 - L- 29+45.00	RT RT	520 521	519 520	810.5 816.7	809.5 1 813.3 (	0% 0.01									80																										HW/D = 1.25,	HW = 818.65	
- L- 31+00.00 - L- 31+00.00	-32 LT	522 522	822.6 518	817.7	811.5	0								23	32					1		1	1																				
- L- 31+00.00 - L- 31+00.00	-55 LT	523 523	820.0 522			0	24			×										1					1 1																		
- L- 30+32.00		523 EX0525	524	820.9	820.0 1	.7%	40			×									<b> </b>																								
- L- 30+65.60 - L- 31+00.00	RT E	EX0526 EX03 527 EX03		821.1 824.0	820.9 821.1 C	0 ).4%									40																												
- L- 20+18.05	52 RT																																						24.7		12" F	RCP	
- L- 23+53.29 - L- 27+64.37	-22 LT -28 IT																			$\left[ \right]$																			48.2		15" F 15" F	RCP	
- L- 32+88.66	40 RT																		<u> </u>																				24.2		13 F 12" F 15" F	RCP	
- Y1- 10+52.40																																							128.9		10"	<b>\</b> υΓ	
SHEET TOTALS							0 84 64 0 32	2 0 0	0		0 0 0	0 0	0 0	0 0 70	04 424 384 0	0 0	0 0 0 0	0 0	0 0 0	) 15	2.112	0 14	2 7	5 0	0 1 1	0 0	0 0	0 0 0	0 0 0	0 0	0 0 0	0 2	0 0 0	) 0 0	0 0		0		0 264	.2			



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