## STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS** GEOTECHNICAL ENGINEERING UNIT

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# **ROADWAY** SUBSURFACE INVESTIGATION

COUNTY CLEVELAND

PROJECT DESCRIPTION US 74 (SHELBY BYPASS) FROM EAST OF NC 180 TO WEST OF SR 2238 (LONG BRANCH ROAD)

PAVEMENT AND SUBGRADE INVESTIGATION

|  | STATE | STATE PROJECT REFERENCE NO. | SHEET<br>NO. | TOTAL<br>SHEETS |
|--|-------|-----------------------------|--------------|-----------------|
|  | N.C.  | R-2707D                     | 1            | 14              |

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# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

|                         |                            |                                | SOIL D                     | ESCR          | PTION                |                         |                                 |                       | Т  |              | GRADATION  |                         |                                    |  |                           |             | ROCK DE                                 | SCRIPTION  |  |  |
|-------------------------|----------------------------|--------------------------------|----------------------------|---------------|----------------------|-------------------------|---------------------------------|-----------------------|--|--------------|--|-------------------------|------------------------------------|--|---------------------------|-------------|---|--|--|--|
| SOIL IS                 |                            |                                | D, SEMI-CON                |               | D, OR WE             | ATHERED E               | ARTH MATERIAL                   | 5 THAT CAN            | WELL GRADED - INDICA   | TES A GOOD   | REPRESENTATION OF PARTI                                | CLE SIZES FROM          | FINE TO COARSE.                    | HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TEST<br>ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIEL |                           |             |   |  |  |  |
| ACCORD                  | ING TO THE                 | STANDARD PENE                  | TRATION TES                | ST (AASH      | .R AND Y<br>TO T 206 | IELD LESS<br>5. ASTM DI | 586). SOIL CLA                  | SIFICATION            | UNIFORMLY GRADED - IN<br>GAP-GRADED - INDICATE                         | NDICATES TH  | HAT SOIL PARTICLES ARE AU<br>RE OF UNIFORM PARTICLE SI | LL APPROXIMATEL         | Y THE SAME SIZE.                   | SPT REFUSAL  | IS PENETRA                | ATION BY    | A SPLIT SPOON S                         | AMPLER EQUAL TO OR LESS THAN 0.1   |  |  |
|                         | BASED ON TH<br>ENCY.COLOR. | HE AASHTO SYS<br>TEXTURE.MOIST | EM. BASIC D<br>URE. AASHTO | ESCRIPT       | IONS GEN             | ERALLY IN<br>AND OTHE   | CLUDE THE FOL<br>R PERTINENT FA | LOWING:<br>CTORS SUCH |  |              |  | NS                      |                                    | REPRESENTED  | I-COASTAL I<br>BY A ZONE  | PLAIN MA    | ATERIAL, THE TRA<br>HERED ROCK.         | NSITION BETWEEN SOIL AND ROCK  |  |  |
| A                       | S MINERALO                 | GICAL COMPOSIT                 | ION, ANGULAR               | ITY, STR      | UCTURE, F            | LASTICITY               | ETC. FOR EXA                    | IPLE,                 | THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: |              |  |                         |                                    | ROCK MATERIA   | LS ARE TYP                | PICALLY C   | DIVIDED AS FOLLOW                       | /S:  |  |  |
|                         | VERT STIFF.G               |                                |                            | AASH1         | O CL                 | ND LATERS,              | ΔTION                           | 7-6                   | ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.                           |              |  |                         |                                    | WEATHERED  |                           |             | NON-COASTAL PLA                         | IN MATERIAL THAT WOULD YIELD SPT   |  |  |
| GENERAL                 | 3                          |                                |                            | SILT          | -CLAY MAT            |                         | JHITUN                          |                       | MINERALOGICAL COMPOSITION  |              |  |                         |                                    |  | - 5                       |             | FINE TO COARSE I                        | GRAIN IGNEOUS AND METAMORPHIC RO   |  |  |
| CLASS.                  | (                          | $\leq$ 35% passing *2          | 30)                        | (>3           | 5% Passing           | 5 =200)                 | ORGANIC I                       | ATERIALS              | MINERAL NAM  | MES SUCH A   | S QUARTZ, FELDSPAR, MICA,                              | TALC, KAOLIN, ETC       |                                    | CRYSTALLINE<br>ROCK (CR)   |                           |             | WOULD YIELD SPT                         | REFUSAL IF TESTED. ROCK TYPE IN  |  |  |
| GROUP                   | A-1                        | A-3                            | A-2                        | A-4           | A-5 A-               | 6 A-7                   | A-1, A-2 A-4,                   | A-5                   | ARE USED IN  |              | COMPRESSION THEY ARE CONSIL                            | DERED OF SIGNIF         | ICANCE.                            |  |                           |             | FINE TO COARSE                          | GRAIN METAMORPHIC AND NON-COASTA   |  |  |
| LLASS.                  | A-1-a A-1-b                | A-2-4 A-2                      | 5 A-2-6 A-2-               | 7<br>N (2002) |                      | A-7-6                   | A-3 A-6,                        | H-7                   | SI IG  |              |  | 11 ( 31                 |                                    | ROCK (NCR)   |                           |             | SEDIMENTARY ROC<br>ROCK TYPE INCLU      | <pre>&lt; THAT WOULD YEILD SPT REFUSAL DES PHYLLITE.SLATE.SANDSTONE.ET()</pre> |  |  |
| SYMBOL                  |                            |                                |                            | 2             | 1.7.1                |                         |                                 |                       | MODE   | RATELY COM   | MPRESSIBLE   | LL = 31 - 50            | 1                                  | COASTAL PLAI   | N                         |             | COASTAL PLAIN SI                        | DIMENTS CEMENTED INTO ROCK. BUT  |  |  |
| % PASSING               | 50.14                      |                                |                            |               |                      |                         | SII SI                          | T- MUCK               | HIGHL  |              | STRLE  |                         |                                    | (CP)   |                           |             | SHELL BEDS, ETC.                        | K TYPE INCLUDES LIMESTUNE, SANDS   |  |  |
| =10<br>=40              | 30 MX<br>30 MX 50 MX       | 51 MN                          |                            |               |                      |                         | SOILS CL                        | PEAT                  |  |              |  |                         |                                    | <b></b>  |                           |             | WEAT                                    | HERING   |  |  |
| *200                    | 15 MX 25 MX                | 10 MX 35 MX 35                 | 1X 35 MX 35 M              | IX 36 MN      | 36 MN 36             | MN 36 MN                |                                 |                       | ORGANIC MATERIAL   | -            | SOILS SOILS  | OTHER M                 | ATERIAL                            | FRESH  | ROCK FRESH,               | I. CRYSTALS | S BRIGHT, FEW JOIN                      | TS MAY SHOW SLIGHT STAINING. ROCK  |  |  |
| MATERIAL<br>PASSING #40 |                            |                                |                            |               |                      |                         |                                 |                       | LITTLE ORGANIC MAT   | TER 2        | 2 - 3% 3 - 5%<br>3 - 5% 5 - 12%                        | LITTLE                  | 10 - 20%                           |  | HAMMER IF U               | CRYSTALLI   | INE.                                    | COME TOTALS MAY SHOW THIN SLAV ST  |  |  |
| LL                      | -                          | - 40 MX 41 M                   | IN 40 MX 41 M              | N 40 MX       | 41 MN 40             | MX 41 MN                | SOILS WITH                      |                       | MODERATELY ORGANIC   | ; 5          | 5 - 10% 12 - 20%                                       | SOME                    | 20 - 35%                           | (V SLI.)   | CRYSTALS O                | IN A BROKE  | EN SPECIMEN FACE                        | SHINE BRIGHTLY. ROCK RINGS UNDER H   |  |  |
| PI                      | 6 MX                       | NP 10 MX 10 1                  | 1X 11 MN 11 M              | N 10 MX       | 10 MX 11             | 4N 11 MN                | MODERATE                        | HIGHLY                | HIGHLY URGANIC   |              |  | HIGHL 1                 | 35% AND ABUVE                      | 1  | OF A CRYSTA               | ALLINE NA   | ATURE.                                  |  |  |  |
| GROUP INDEX             | 0                          | 0 0                            | 4 MX                       | 8 MX          | 12 MX 16             | MX NO MX                | AMOUNTS OF<br>ORGANIC           | SOILS                 |  |              | GROUND WHIER   |                         |                                    | . SLIGHT   | ROCK GENER                | ALLY FRES   | SH. JOINTS STAINED                      | AND DISCOLORATION EXTENDS INTO RO  |  |  |
| USUAL TYPES             | STONE FRAGS.               | FINE SILTY                     | OR CLAYEY                  | SIL           | TY                   | CLAYEY                  | MATTER                          |                       |  | WATER LI     | EVEL IN BORE HOLE IMMEDI                               | ATELY AFTER DR          | ILLING                             | (SEII)   | CRYSTALS AF               | RE DULL /   | AND DISCOLORED. CF                      | RYSTALLINE ROCKS RING UNDER HAMMER   |  |  |
| MATERIALS               | SAND                       | SAND GRAVE                     | . AND SAND                 | S01           | S                    | SOILS                   |                                 |                       |  | STATIC W     | WATER LEVEL AFTER 24                                   | HOURS                   |                                    | MODERATE   | SIGNIFICANT               | PORTIONS    | S OF ROCK SHOW DI                       | SCOLORATION AND WEATHERING EFFECTS   |  |  |
| GEN. RATING             |                            | EXCELLENT TO GOD               | n                          |               | FAIR TO PO           | INR                     | FAIR TO PO                      |                       |  | PERCHED      | WATER, SATURATED ZONE, OF                              | R WATER BEARING         | G STRATA                           | (MOD.)   | GRANITOID R               | ROCKS, MOS  | T FELDSPARS ARE I<br>AMMER BLOWS AND 1  | DULL AND DISCOLORED, SOME SHOW CLA   |  |  |
| AS SUBGRADE             |                            |                                | 0                          |               |                      |                         | POOR                            |                       |  | SPRING (     | DR SEEP  |                         |                                    |  | WITH FRESH                | ROCK.       |   |  |  |  |
|                         |                            | PI OF A-7-5 SUBGR              | DUP IS ≤ LL                | · 30 ; PI 0   | F A-7-6 SL           | BGROUP IS :             | • LL - 30                       |                       |  |              |  | 01.0                    |                                    | MODERATELY   | ALL ROCK E                | XCEPT OUP   | ARTZ DISCOLORED O                       | R STAINED. IN GRANITOID ROCKS.ALL F  |  |  |
|                         |                            |                                | 515 LENC                   |               |                      | INE 55                  | DANCE OF                        |                       |  | N15          | DUELLANEUUS STMB                                       | ULS                     |                                    | (MOD, SEV.)  | AND DISCULU<br>AND CAN BE | EXCAVATE    | A MAJURITY SHUW<br>ED WITH A GEOLOGI    | KAULINIZATION. RUCK SHOWS SEVERE L<br>ST'S PICK. ROCK GIVES "CLUNK" SOUND '    |  |  |
| PRIMARY S               | SOIL TYPE                  |                                | ESS OR                     | PENETR        | ATION RE             | SISTENCE                | COMPRESSI                       | E STRENGTH            | ROADWAY EMB  | 3ANKMENT (P  | RE) 25/025 DIP & DIP DIF                               | RECTION                 |                                    |  | <u>IF TESTED, I</u>       | WOULD YIE   | LD SPT REFUSAL                          |  |  |  |
|                         |                            | 00013131                       |                            |               | (N-VALUE             | )                       | (TON                            | 5/FT²)                |  | SCRIPTION    | OF ROCK STRU   | UCTURES                 |                                    | SEVERE   | ALL ROCK E)               | XCEPT OUP   | ARTZ DISCOLORED O                       | R STAINED, ROCK FABRIC CLEAR AND E   |  |  |
| GENERAL                 | LLY                        | VERY L                         | DOSE<br>F                  |               | < 4<br>4 TO 1        | a                       |                                 |                       | SOIL SYMBOL  |              |  |                         | SLOPE INDICATOR                    | (SEV.)   | TO SOME EX                | TENT. SOM   | 4E FRAGMENTS OF S                       | TRONG ROCK USUALLY REMAIN.   |  |  |
| GRANUL                  | AR<br>AL                   | MEDIUM                         | DENSE                      |               | 10 TO 3              | 0                       |                                 | /A                    |  | ILL (AF) OTH |  |                         | CONE PENETROMETER                  |  | <u>IF TESTED, P</u>       | WOULD YIE   | LD SPT N VALUES                         | > 100 BPF  |  |  |
| (NON-CO                 | HESIVE)                    | DENS<br>VERY D                 | E<br>ENSE                  |               | 30 TO 5              | 60                      |                                 |                       | THAN ROADWA  | Y EMBANKM    |  | , <b>D</b>              | TEST                               | VERY   | ALL ROCK E                | XCEPT QUA   | ARTZ DISCOLORED O                       | R STAINED. ROCK FABRIC ELEMENTS AR   |  |  |
|                         |                            | VERY S                         | OFT                        |               | < 2                  |                         | <                               | <b>7.</b> 25          | INFERRED SO!   | IL BOUNDAR'  |  | •                       | SOUNDING ROD                       | (V SEV.)   | REMAINING.                | SAPROLITE   | IS AN EXAMPLE O                         | ROCK WEATHERED TO A DEGREE THAT  |  |  |
| GENERAL                 | LLY                        | SOF                            | Г                          |               | 2 TO 4               |                         | 0.25                            | TO Ø.5                |  |              | MW   | -                       | TEST BORING                        |  | VESTIGES OF               | F ORIGINAL  | L ROCK FABRIC REM                       | AIN. <u>IF TESTED, WOULD YIELD SPT N V</u>                                     |  |  |
| SILT-CL<br>MATERIA      | AY<br>AL                   | MEDIUM                         | STIFF<br>F                 |               | 4 TO 8<br>8 TO 1     | 5                       | 0.5                             | TO 1.0<br>TO 2        | INFERRED ROC   | JK LINE      | O MONITORING W   |                         | WITH CORE                          | COMPLETE   | ROCK REDUCE               | ED TO SOI   | IL. ROCK FABRIC NO<br>ATIONS, DUARTZ MA | T DISCERNIBLE, OR DISCERNIBLE ONLY<br>( BE PRESENT AS DIKES OR STRINGERS       |  |  |
| (COHESI                 | VE)                        | VERY S                         | TIFF                       |               | 15 TO 3              | Ø                       | 2                               | TO 4                  | +++++ ALLUVIAL SOI   | IL BOUNDAR   | Y A PIEZOMETER   | $\bigcirc$              | SPT N-VALUE                        |  | ALSO AN EX                | AMPLE.      |   |  |  |  |
|                         |                            |                                |                            |               |                      | 175                     |                                 | 4                     | +  |              |  |                         |                                    |  |                           |             | ROCK H                                  | ARDNESS  |  |  |
|                         |                            |                                | ATURE                      | UN UF         | MIN 3                |                         |                                 |                       |  |              |  |                         |                                    | VERY HARD  | CANNOT BE !               | SCRATCHE    | D BY KNIFE OR SHA                       | RP PICK. BREAKING OF HAND SPECIMENS  |  |  |
| U.S. STD. SIE           | EVE SIZE<br>M)             | 4                              | 4 10<br>76 2.00            | 40<br>0.42    | 60<br>0.25           | 200<br>0.075            | 270<br>0.053                    |                       |  |              | ABLE WASTE   | ACCEPTABL               | E, BUT NOT TO BE                   |  | SEVERAL HAP               | RD BLOWS    | OF THE GEOLOGIST                        | 'S PICK.   |  |  |
| 0. 2.11.10              |                            |                                |                            | COARS         | E                    | FINE                    |                                 |                       |  |              | SSIFIED EXCAVATION -                                   | USED IN TI<br>EMBANKMEN | HE TOP 3 FEET OF<br>NT OR BACKFILL | HARD   | TO DETACH !               | HAND SPEC   | Y KNIFE UR PILK UN<br>CIMEN.            | NLY WITH DIFFICULTY. HARD HAMMER BI  |  |  |
| (BLDR.)                 |                            | BBLE GR                        | AVEL                       | SAN           |                      | SAND                    | (SL.)                           | CLAY<br>(CL.)         |  |              |  |                         |                                    | MODERATELY   | CAN BE SCR                | ATCHED B    | Y KNIFE OR PICK. G                      | OUGES OR GROOVES TO 0.25 INCHES DE   |  |  |
|                         |                            |                                |                            | (CSE. S       | 0.)                  | (F SD.                  |                                 |                       |  |              | ABBREVIATIONS  |                         |                                    | HARD   | EXCAVATED E               | BY HARD E   | BLOW OF A GEOLOG                        | ST'S PICK. HAND SPECIMENS CAN BE DI  |  |  |
| GRAIN MM<br>SIZE IN     | 1 305                      | 75<br>3                        | 2.0                        |               | 0.25                 | 0                       | 0.05                            | .005                  | BT - BORING TERMINATE  | .D           | MED MEDIUM<br>MICA MICACEOUS                           | VSI - VA<br>WEA WE      | ANE SHEAR TEST                     | MEDIUM   | CAN BE GRO                | DOVED OR (  | GOUGED 0.05 INCHES                      | DEEP BY FIRM PRESSURE OF KNIEF O   |  |  |
|                         |                            |                                |                            |               |                      |                         | TEDMC                           |                       | CL CLAY  |              | MOD MODERATELY   | 2 - UNΙ                 | T WEIGHT                           | HARD   | CAN BE EXC                | AVATED IN   | N SMALL CHIPS TO                        | PEICES 1 INCH MAXIMUM SIZE BY HARD   |  |  |
| SOTI                    | MOISTURE                   |                                |                            |               |                      |                         |                                 |                       | CPT - CONE PENETRATION     CSE COARSE                                  | N TEST       | NP - NON PLASTIC<br>ORG ORGANIC                        | '∕d- DRY                | UNIT WEIGHT                        | COLT   | POINT OF A                | GEOLOGIS    | T'S PICK.                               |  |  |  |
| (ATT                    | ERBERG LI                  | MITS)                          | DESCRI                     | PTION         | GUI                  | DE FOR F                | IELD MOISTURE                   | DESCRIPTION           | DMT - DILATOMETER TES  | 3T           | PMT - PRESSUREMETER T                                  | EST <u>SAMPL</u>        | E ABBREVIATIONS                    | SUFT   | FROM CHIPS                | TO SEVEF ن  | RAL INCHES IN SIZE                      | BY MODERATE BLOWS OF A PICK POIN   |  |  |
|                         |                            | ·                              | - SATURA                   | TED -         | USI                  |                         | UID: VERY WET.                  |                       | DPT - DYNAMIC PENETRA  | TION TEST    | SAP SAPROLITIC   | S - BULK                |                                    |  | PIECES CAN                | BE BROKE    | N BY FINGER PRESS                       | SURE.  |  |  |
|                         |                            |                                | (SAT.)                     |               | FRO                  | M BELOW                 | THE GROUND                      | ATER TABLE            | F - FINE   |              | SL SILT, SILTY   | ST - SHE                | LBY TUBE                           | VERY   | CAN BE CAR                | VED WITH    | KNIFE. CAN BE EXC                       | AVATED READILY WITH POINT OF PICK.   |  |  |
|                         |                            |                                |                            |               |                      |                         |                                 |                       | - FOSS FOSSILIFEROUS   | CTUDEC       | SLI SLIGHTLY   | RS - ROC                |                                    | 3011   | FINGERNAIL.               |             | S CHILDE BROKEN                         |  |  |  |
| RANGE <                 |                            |                                | - WET -                    | (W)           | SEN                  | 1ISOLID;R<br>AIN OPTI   | EQUIRES DRYIN<br>MUM MOISTURE   | 5 ТО                  | FRAGS FRAGMENTS  | , TURES      | w - MOISTURE CONTENT                                   | CBR - CA                | LIFORNIA BEARING                   | F  | RACTURE                   | E SPAC      | CING                                    | BEDDING  |  |  |
| (PI) PL L               |                            | C LIMIT _                      |                            |               |                      |                         |                                 |                       | HI HIGHLY  |              | V - VERY   | RA                      | TIO                                | TERM   |                           | ç           | SPACING                                 | TERM   |  |  |
|                         |                            |                                | - MOIST                    | - (M)         | SOL                  | ID: AT OR               | NEAR OPTIMU                     | MOISTURE              | EO   | UIPMENT      | USED ON SUBJEC   | T PROJECT               |                                    | VERY WIDE  |                           | MORE T      | THAN 10 FEET                            | VERY THICKLY BEDDED  |  |  |
| UM<br>SL                |                            | M MUISTURE                     |                            |               |                      | •                       |                                 |                       | DRILL UNITS:   | ADVANCIN     | NG TOOLS:  | HAMMER TYPE             | E:                                 | MODERATEL  | Y CLOSE                   | 1 T         | O 3 FEET                                | THINLY BEDDED 0.1  |  |  |
|                         | T                          |                                |                            | _             | REC                  | UIRES AD                | DITIONAL WATE                   | R TO                  | CME-45C  |              | AY BITS  |                         | ATIC MANUAL                        | CLOSE<br>VERY CLOS   | F                         | 0.16        | TO 1 FOOT                               | VERY THINLY BEDDED 0.0   |  |  |
|                         |                            |                                | - DRY -                    | (U)           | AT                   | AIN OPTI                | MUM MOISTURE                    |                       | CME-55   | 6. C         | CONTINUOUS FLIGHT AUGER                                | CORE SIZE:              |                                    |  | -                         | 2200 11     |   | THINLY LAMINATED <   |  |  |
|                         | 1                          |                                | PLA                        | STICI         | TY                   |                         |                                 |                       | 1  | 8. H         | HOLLOW AUGERS  | в                       |                                    |  |                           |             | INDUF                                   | RATION   |  |  |
|                         |                            |                                | PLASTI                     | CITY IN       | DEX (PI)             |                         | DRY ST                          | RENGTH                | CME-550  | HAP          | RD FACED FINGER BITS                                   | <u> </u>                |                                    | FOR SEDIMENT   | ARY ROCKS.                | , INDURATI  | ION IS THE HARDEN                       | NING OF MATERIAL BY CEMENTING, HE  |  |  |
| NON                     | PLASTIC                    |                                |                            | 0-5           |                      |                         | VERY                            | LOW                   |  |              | NGCARBIDE INSERTS                                      |                         | _                                  | FRIABL   | Ξ                         |             | RUBBING WITH                            | FINGER FREES NUMEROUS GRAINS;  |  |  |
| SL10<br>MOD             | GHTLY PLAS                 | STIC<br>LASTIC                 |                            | 6-15<br>16-25 |                      |                         | SLI                             | HT<br>UM              | VANE SHEAR TEST  |              | SING W/ ADVANCER                                       | HAND TOOLS:             |                                    |  |                           |             | GENILE BLOW                             | DI NHMMER DISINIEGRAIES SAMPLE.  |  |  |
| HIG                     | HLY PLASTI                 | C                              | 2                          | S OR MC       | RE                   |                         | HI                              | iΗ                    | PORTABLE HOIST   |              | ICONE 'STEEL TEETH                                     |                         | IULE DIGGER                        | MODERA   | TELY INDUR                | RATED       | GRAINS CAN B                            | E SEPARATED FROM SAMPLE WITH ST<br>Y WHEN HIT WITH HAMMER.                     |  |  |
|                         |                            |                                | (                          | OLOR          |                      |                         |                                 |                       | 1  |              |  |                         |                                    |  |                           |             | GRAINS ARE D                            | IFFICULT TO SEPARATE WITH STEEL  |  |  |
|                         |                            |                                | 00 601 00                  |               |                      |                         |                                 |                       | X <u>CME-450</u>   |              | NCH THIN WALL CODE DIT                                 |                         | NG ROD                             | INDURA   | ED                        |             | DIFFICULT TO                            | BREAK WITH HAMMER.   |  |  |
| DESCRIPT                | DIFIERS SI                 | INCLUDE COLOF                  | OR COLOR                   | COMBINA       | ARE US               | ED TO DE                | YELLOW-BROWN,<br>SCRIBE APPF∆®  | BLUE-GRAY).<br>ANCE.  |  |              | NCH IMIN WHEL LUKE BIT                                 |                         | HEAR TEST                          | EVTDEN   |                           | ΔΤΕΠ        | SHARP HAMMER                            | BLOWS REQUIRED TO BREAK SAMPLE   |  |  |
|                         |                            |                                |                            |               |                      |                         |                                 |                       |  | X 2.         | 25 SOLID-STEM AUGERS                                   | I X KESSI               | LEK DUP                            | LAIREM   | LEI INDORA                |             | SAMPLE BREAK                            | S ACROSS GRAINS.   |  |  |

#### PROJECT REFERENCE NO.



2

| D. AN INFERRED                |  |
|-------------------------------|--|
| SPT REFUSAL.                  | ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.   |
| IS OFTEN                      | AUDIFER - A WAIER BEARING FURMAIIUN UK SIRAIA.   |
|                               | ARCHILLACEOUS - APPLIED TO ALL ROCKS OR SHIRETANCES COMPOSED OF CLAY MINERALS OR HAVING  |
| N VALUES >                    | A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.  |
|                               | ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT   |
| CK THAT                       | WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.   |
|                               | CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.  |
| IF TESTED.                    | COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM  |
| MAY NOT YIELD                 | OF SLOPE.  |
| TONE, CEMENTED                | CURE RECOVERED IN THE CORE RUN AND EXPRESSED AS A PERCENTAGE.  |
|                               | DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT   |
| RINGS UNDER                   | ROCKS OR CUIS MASSIVE ROCK.<br>DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE   |
| DATINGS IE OPEN               | HORIZONTAL.  |
| AMMER BLOWS IF                | <u>DIP DIRECTION (DIP AZIMUTH)</u> - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.   |
| CK UP TO<br>L FELDSPAR        | <u>FAULT</u> - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE<br>SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.   |
| BLOWS.                        | FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.  |
| S. IN<br>Y. ROCK HAS          | FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM<br>PARENT MATERIAL.  |
| AS COMPARED                   | FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.  |
| ELDSPARS DULL                 | FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE  |
| OSS OF STRENGTH               |  |
| WHEN STRUCK.                  | JUINT - FRACTORE IN ROLK ALONG WHICH NO AFFRECIABLE MOVEMENT HAS OCCORRED.   |
| VIDENT BUT                    | ITS LATERAL EXTENT.  |
| RE KAOLINIZED                 | LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.  |
|                               | MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTTLING IN SOILS  |
| E DISCERNIBLE                 | PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE   |
| ONLY MINOR                    | OF AN INTERVENING IMPERVIOUS STRATUM.  |
| ALUES ( 100 BPF               | RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.   |
| SAPROLITE IS                  | ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF<br>ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE<br>RUN AND EXPRESSED AS A PERCENTAGE.   |
|                               | SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT  |
| 5 REQUIRES                    | ROCK.  |
| OWS REQUIRED                  | <u>SILL</u> - AN INTRUSIVE BODY OF IONEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND<br>RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT. THAT HAS BEEN EMPLACED PARALLEL TO<br>THE BEDDING OR SCHISTOSITY OF THE INTRUGED ROCKS.  |
| EP CAN BE                     | SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT   |
| ETACHED                       | OR SLIP PLANE.   |
| R PICK POINT.<br>BLOWS OF THE | STANDARD FENETRATION TEST TRENETRATION RESISTANCE (SPT) - NUMBER OF BLOWS IN OR BPF) OF<br>A 140 LB.HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF I FOOT INTO SOIL<br>WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL<br>TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. |
|                               | STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY  |
| PIECES 1 INCH                 | STRATA ROCK DUALITY DESIGNATION (SROD) - A MEASUME OF ROCK DUALITY DESCRIBED BY TOTAL<br>LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO DR GREATER THAN 4 INCHES DIVIDED BY   |
| ED READILY BY                 | TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.   |
|                               | BENCH MARK.  |
| THICKNESS                     |  |
| 4 FEET                        | ELEVATION: FEET  |
| 6 - 1.5 FEET                  | NOTES:   |
| 18 - 0.03 FEET                | EB = EASTBOUND   |
| 0.008 FEET                    | WB = WESTBOUND   |
| AT, PRESSURE, ETC.            |  |
|                               |  |
| EEL PROBE;                    | OSS = OUTSIDE SHOULDER   |
| ·                             | OSL = OUTSIDE LANE   |
| PROBE:                        | ISL = INSIDE LANE  |
| :                             |  |
|                               | DATE: 8-15-14  |
|                               |  |





## **PAVEMENT INVESTIGATION DATA SHEET**

| Project: | 34497.1.2 |
|----------|-----------|
| TIP:     | R-2707D   |

Route: US-74 Cleveland County:

| Width (ft.)                 |                                      |                                  |                    |   |                                 |                         | Th      | ickness (ir | ı.)                           |          | Subgrade  |                          |               |                   |   | GPS Coo  | rdinates  |
|-----------------------------|--------------------------------------|----------------------------------|--------------------|---|---------------------------------|-------------------------|---------|-------------|-------------------------------|----------|---|--------------------------|---------------|-------------------|---|----------|-----------|
| Position (Sta.,Lane,Shldr.) | Cut/Fill (Est. of<br>Amount in feet) | Lane(s)                          | Shoulder           | Offset Distance<br>from White Line<br>(ft.) | Crown "C" or<br>Super "S" (in.) | Gross to Top of<br>Soil | Asphalt | ABC         | Stabilizaed<br>Subgradae Soil | Concrete | Description   | AASHTO<br>Classification | Soil Moisture | Probe Depth (ft.) | Asphalt Notes   | Northing | Easting   |
|                             |                                      |                                  | •                  | •   |                                 |                         |         |             |                               |          |   |                          |               |                   |   |          |           |
| (-Y5_EBL-) 35+50 - ISS      | Fill<br>2                            | ISL = 12<br>OSL = 12             | ISS = 3<br>OSS = 4 | 26  | C - 4                           | 18                      | 12      | 6           | N/A                           | N/A      | (1.5'-5.0') RES: brown, slightly plastic, sandy CLAY with some<br>mica<br>Sample No. S-80 (2.4 - 5.0 feet)  | A-6                      | 16%           | 5                 | Asphalt in good condition, no signs of distress observed.                       | 559,565  | 1,263,652 |
| (-Y5_EBL-) 35+50 - ISL      | Fill<br>2                            | ISL = 12<br>OSL = 12             | ISS = 3<br>OSS = 4 | 22  | C - 4                           | 22                      | 12      | 10          | N/A                           | N/A      | (1.8'-5.0') RES: brown, slightly plastic, sandy CLAY with some mica   | A-6                      | М             | 5                 | Asphalt in good condition, no signs of distress observed.                       | 559,562  | 1,263,651 |
| (-Y5_EBL-) 35+50 - OSS      | Fill<br>2                            | ISL = 12<br>OSL = 12             | ISS = 3<br>OSS = 4 | 2   | C - 4                           | 18.5                    | 8.5     | 10          | N/A                           | N/A      | (1.5'-5.0') RES: red, moderately plastic, clayey SAND with some<br>mica<br>Sample No. S-82 (2.2 - 5.0 feet)   | A-2-7                    | 22%           | 5                 | Low severity transverse cracking observed.                                      | 559,539  | 1,263,642 |
| (-Y5_WBL-) 39+50 - RTL      | Fill<br>3                            | ISL = 12<br>OSL = 12<br>RTL = 12 | ISS = 3<br>OSS = 2 | 3   | C - 4                           | 14                      | 10      | 4           | N/A                           | N/A      | (1.2'-3.0') RE: brown, slightly plastic, highly sandy, silty CLAY<br>(3.0'-5.0') RES: brown, slightly plastic, highly sandy, silty CLAY<br>Sample No. S-78 (2.0 - 5.0 feet) | A-7-5                    | 23%           | 5                 | Low severity fatigue cracking observed near the inside edge of right turn lane. | 559,761  | 1,263,298 |
| (-RAMP_A-) 46+00 - WB ISS   | Fill<br>5                            | ISL = 12<br>OSL = 12             | ISS = 2<br>OSS = 3 | 26  | S-LT                            | 21.5                    | 11.5    | 10          | N/A                           | N/A      | (1.7'-5.0') RE: brown, slightly plastic, sandy CLAY with some<br>mica<br>Sample No. S-79 (2.3- 5.0 feet)  | A-6                      | 21%           | 5                 | Low severity edge cracking observed on ISS.                                     | 559,387  | 1,264,198 |
| (-RAMP_A-) 46+00 - WB OSL   | Fill<br>5                            | ISL = 12<br>OSL = 12             | ISS = 2<br>OSS = 3 | 2   | S-LT                            | 21                      | 13      | 8           | N/A                           | N/A      | (1.7'-5.0') RE: brown, slightly plastic, clayey SAND with some mica   | A-2-7                    | М             | 5                 | Asphalt in good condition, no signs of distress observed.                       | 559,410  | 1,264,205 |
| (-RAMP_A-) 46+00 - WB OSS   | Fill<br>5                            | ISL = 12<br>OSL = 12             | ISS = 2<br>OSS = 3 | 1   | S-LT                            | 22.5                    | 10.5    | 12          | N/A                           | N/A      | (1.8'-5.0') RE: brown, slightly plastic, clayey SAND with some<br>mica<br>Sample No. S-76 (2.3- 5.0 feet)   | A-2-7                    | 19%           | 5                 | Asphalt in good condition, no signs of distress observed.                       | 559,413  | 1,264,206 |
|                             |                                      |                                  |                    |   |                                 |                         |         |             |                               |          |   |                          |               |                   |   |          |           |
|                             |                                      |                                  |                    |   |                                 |                         |         |             |                               |          |   |                          |               | T                 |   |          |           |
|                             |                                      |                                  |                    |   |                                 |                         |         |             |                               |          |   |                          |               |                   |   |          |           |
|                             |                                      | _                                |                    |   |                                 |                         |         |             |                               |          |   |                          |               | T                 |   |          |           |
|                             |                                      |                                  |                    |   |                                 |                         |         |             |                               |          |   |                          |               |                   |   |          |           |
|                             |                                      |                                  |                    |   |                                 |                         |         |             |                               |          |   |                          |               |                   |   |          |           |
|                             |                                      |                                  |                    |   |                                 |                         |         |             |                               |          |   |                          |               |                   |   |          |           |
|                             |                                      |                                  |                    |   |                                 |                         |         |             |                               |          |   |                          |               |                   |   |          |           |
|                             |                                      |                                  |                    |   |                                 |                         |         |             |                               |          |   |                          |               |                   |   |          |           |

<u>Notes:</u> OSL = Outside Lane ISL = Inside Lane RTL = Right Turn Lane

CTL = Center Turn Lane LTL = Left Turn Lane PS = Paved Shoulder

OSS = Outside Shoulder ISS = Inside Shoulder ACC = Acceleration Lane N/M = not measured

DL = Deceleration Lane HA = Hand Auger WB = Westbound EB = Eastbound

| Date:     | 1/8/19 - 1/9/19 |
|-----------|-----------------|
| Notes By: | Brett Smith, PG |

|                            |                      |                            | PROJECT NUMBER  |             | PROJECT I.D.        |            | ROUTE              |               |          |  |  |  |  |
|----------------------------|----------------------|----------------------------|-----------------|-------------|---------------------|------------|--------------------|---------------|----------|--|--|--|--|
|                            | CONE PENE            | TROMETER                   | 34497 1 2       |             | R-2707D             |            | US-74              |               |          |  |  |  |  |
|                            |                      |                            |                 |             |                     |            |                    |               |          |  |  |  |  |
|                            | DATACOD              | E SHEET                    |                 |             | GEOLOGIST           |            | Miles 6            | ECHNICIANS    |          |  |  |  |  |
| o:                         |                      |                            | Cleveland       | <u> </u>    | Brett Smith, PG     |            | IVIIKE 8           | * Jonnathon M | oseley   |  |  |  |  |
| Station                    | (location) informati | on                         | Date run        | Station (lo | cation) information |            |                    | Date          | run      |  |  |  |  |
| (-Y5_EE                    | 3L-) 35+50 - ISS     | N 1 1 1 1                  | 1/8/19 - 1/9/19 | (-Y5_EBL-   | -) 35+50 - ISL      | N.1. 11.1  |                    | 1/8/19 -      | . 1/9/19 |  |  |  |  |
| Datum                      | cut or fill          | Northing                   | Easting         | Datum       | cut or fill         | Northing   |                    | Easting       | 00.054   |  |  |  |  |
| ABC                        | Fill - 2'            | 559,565                    | 1,263,652       | ABC         | Fill - 2'           | 5          | 559,562            | 1,20          | 63,651   |  |  |  |  |
|                            | Cum                  | ulative Penetration in Cer | ntimeters       |             | Cumul               | ative Pene | etration in Centil | meters        |          |  |  |  |  |
| 0.9                        | 87.9                 |                            |                 | 0.8         | 41.8                |            |                    |               |          |  |  |  |  |
| 1.6                        | 89.5                 |                            |                 | 1.5         | 42.9                |            |                    |               |          |  |  |  |  |
| 2.2                        | 91.1                 |                            |                 | 1.8         | 44.1                |            |                    |               |          |  |  |  |  |
| 2.7                        | 92.0                 |                            |                 | 2.2         | 45.2                |            |                    |               |          |  |  |  |  |
| 3.3                        | 92.6                 |                            |                 | 2.6         | 46.1                |            |                    |               |          |  |  |  |  |
| 3.9                        |                      |                            |                 | 3.0         | 47.2                |            |                    |               |          |  |  |  |  |
| 4.6                        |                      |                            |                 | 3.4         | 48.1                | _          |                    |               |          |  |  |  |  |
| 5.4                        |                      |                            |                 | 3.8         | 49.1                | _          |                    |               |          |  |  |  |  |
| 6.3                        |                      |                            |                 | 4.3         | 49.8                |            |                    |               |          |  |  |  |  |
| 1.1                        |                      |                            |                 | 4./         | 50.6                |            |                    |               |          |  |  |  |  |
| 8.1                        |                      |                            |                 | 5.0         | 51.4                |            |                    |               |          |  |  |  |  |
| 9.1                        |                      |                            |                 | 5.3         | 52.2                | _          |                    |               |          |  |  |  |  |
| 10.3                       |                      |                            |                 | 5.8         | 53.0                | _          |                    |               |          |  |  |  |  |
| 11.8                       |                      |                            |                 | 6.0         | 54.2                | _          | _                  |               |          |  |  |  |  |
| 14.5                       |                      |                            |                 | 6.3         | 55.6                | _          | _                  |               |          |  |  |  |  |
| 19.4                       |                      |                            |                 | 6.6         | 56.8                | _          | _                  |               |          |  |  |  |  |
| 22.3                       |                      |                            |                 | 7.0         | 58.1                | _          | _                  |               |          |  |  |  |  |
| 23.6                       |                      |                            |                 | 7.2         | 59.5                | _          | _                  |               |          |  |  |  |  |
| 25.0                       |                      |                            |                 | 7.6         | 60.9                | _          |                    |               |          |  |  |  |  |
| 26.3                       |                      |                            |                 | 8.0         | 62.4                | _          | _                  |               |          |  |  |  |  |
| 21.1                       |                      |                            |                 | 8.1         | 03.8                | _          |                    |               |          |  |  |  |  |
| 29.3                       |                      |                            |                 | 8.5         | 65.4                | _          |                    |               |          |  |  |  |  |
| 30.9                       |                      |                            |                 | 9.0         | 69.2                | _          | _                  |               |          |  |  |  |  |
| 32.0                       |                      |                            |                 | 9.2         | 60.6                | _          | _                  |               |          |  |  |  |  |
| 25.0                       |                      |                            |                 | 9.0         | 70.9                | -          |                    |               |          |  |  |  |  |
| 27.0                       |                      |                            |                 | 9.0         | 70.0                | -          |                    |               |          |  |  |  |  |
| <u>37.9</u><br><u>40.1</u> |                      |                            |                 | 10.1        | 73.5                | -          |                    |               |          |  |  |  |  |
| 40.1                       |                      |                            |                 | 10.4        | 74.8                | -          | _                  |               |          |  |  |  |  |
| 42.4                       |                      |                            |                 | 11.0        | 76.1                | -          | _                  |               |          |  |  |  |  |
| 44.5                       |                      |                            |                 | 11.2        | 77.5                | _          |                    |               |          |  |  |  |  |
| 43.3                       |                      |                            |                 | 12.0        | 79.0                | _          |                    |               |          |  |  |  |  |
| 48.4                       |                      |                            |                 | 12.0        | 80.3                | -          |                    |               |          |  |  |  |  |
| 49.8                       |                      |                            |                 | 13.0        | 81.8                | _          |                    |               |          |  |  |  |  |
| 51.4                       |                      |                            |                 | 13.5        | 83.1                | -          |                    |               |          |  |  |  |  |
| 53.1                       |                      |                            |                 | 14.0        | 84.5                | -          |                    |               |          |  |  |  |  |
| 54.7                       |                      |                            |                 | 14.5        | 85.8                | _          |                    |               |          |  |  |  |  |
| 56.8                       |                      |                            |                 | 15.0        | 87.0                | _          |                    |               |          |  |  |  |  |
| 59.4                       |                      |                            |                 | 15.5        | 88.4                | _          |                    |               |          |  |  |  |  |
| 61.6                       |                      |                            |                 | 16.2        | 89.6                | _          |                    |               |          |  |  |  |  |
| 63.7                       |                      |                            |                 | 17.3        | 90.8                | _          |                    |               |          |  |  |  |  |
| 65.8                       |                      |                            |                 | 18.4        | 91.9                | _          |                    |               |          |  |  |  |  |
| 67.3                       |                      |                            |                 | 19.7        | 92.4                |            |                    |               |          |  |  |  |  |
| 68.8                       |                      |                            |                 | 21.7        |                     |            |                    |               |          |  |  |  |  |
| 70.6                       |                      |                            |                 | 24.5        |                     |            |                    |               |          |  |  |  |  |
| 72.5                       |                      |                            |                 | 28.1        |                     |            |                    |               |          |  |  |  |  |
| 74.6                       |                      |                            |                 | 30.7        |                     |            |                    |               |          |  |  |  |  |
| 76.6                       |                      |                            |                 | 33.0        |                     |            |                    |               |          |  |  |  |  |
| 78.5                       |                      |                            |                 | 35.1        |                     |            |                    |               |          |  |  |  |  |
| 80.6                       |                      |                            |                 | 36.8        |                     |            |                    |               |          |  |  |  |  |
| 82.6                       |                      |                            |                 | 38.1        |                     |            |                    |               |          |  |  |  |  |
| 84.5                       |                      |                            |                 | 39.4        |                     |            |                    |               |          |  |  |  |  |
| 86.2                       |                      |                            |                 | 40.6        |                     |            |                    |               |          |  |  |  |  |

|            |                     |                           | PROJECT NUMBER  |              | PROJECT I.D.       |            | ROUTE<br>US-74   |               |          |  |  |  |
|------------|---------------------|---------------------------|-----------------|--------------|--------------------|------------|------------------|---------------|----------|--|--|--|
|            | CONE PENE           | TROMETER                  | 34497.1.2       | 1            | R-2707D            |            |                  |               |          |  |  |  |
|            |                     |                           | COUNTY          |              | CEOLOGIST          |            | TECHNICIANS      |               |          |  |  |  |
|            | DATA COL            |                           | Cleveland       |              | Brett Smith PG     |            | Mike             | & Johnathon I | loselev  |  |  |  |
| Station    | (location) informat | ion                       | Dete rup        | Station (loo | blett Siffitti, FG |            | Data run         |               |          |  |  |  |
|            |                     | 1011                      | 1/8/10 1/0/10   |              |                    |            |                  |               |          |  |  |  |
| Catum      | BL-) 35+50 - 035    | Northing                  | 1/8/19 - 1/9/19 | C-T5_WBL-    | out or fill        | Northing   |                  | Facting       | - 1/9/19 |  |  |  |
|            | Eill 2'             | 550 530                   | 1 263 642       |              |                    |            | 550 761          |               | 263 208  |  |  |  |
| ABC        |                     | ulative Penetration in Co | 1,200,042       | ABC          | TIII-5             | ativo Pono | otration in Cont | imotors       | 200,290  |  |  |  |
| 0.0        | 12 7                |                           |                 | 0.6          |                    |            |                  |               |          |  |  |  |
| 0.9        | 12.7                | 72.3                      |                 | 1.2          | 67.9               | -          |                  |               |          |  |  |  |
| 1.4        | 13.2                | 73.6                      |                 | 1.2          | 69.4               | -          |                  |               |          |  |  |  |
| 1.0        | 13.4                | 75.0                      |                 | 1.0          | 70.8               | -          |                  |               |          |  |  |  |
| 2.0        | 13.7                | 76.1                      |                 | 2.4          | 72.1               | -          |                  |               |          |  |  |  |
| 2.3        | 14.0                | 77.3                      |                 | 2.8          | 73.4               | _          |                  |               |          |  |  |  |
| 2.5        | 14.4                | 78.5                      |                 | 3.2          | 75.0               | _          |                  |               |          |  |  |  |
| 2.6        | 14.6                | 79.7                      |                 | 3.5          | 76.1               |            |                  |               |          |  |  |  |
| 3.1        | 14.9                | 80.9                      |                 | 3.9          | 77.4               |            |                  |               |          |  |  |  |
| 3.2        | 15.3                | 82.0                      |                 | 4.3          | 78.6               |            |                  |               |          |  |  |  |
| 3.4        | 15.7                | 83.2                      |                 | 4.5          | 79.9               |            |                  |               |          |  |  |  |
| 3.6        | 16.0                | 84.2                      |                 | 5.1          | 81.0               |            |                  |               |          |  |  |  |
| 3.7        | 16.4                | 85.4                      |                 | 5.7          | 82.1               |            |                  |               |          |  |  |  |
| 4.0        | 16.7                | 86.7                      |                 | 6.1          | 83.3               |            |                  |               |          |  |  |  |
| 4.2        | 17.3                | 87.9                      |                 | 6.5          | 84.5               |            |                  |               |          |  |  |  |
| 4.4        | 17.6                | 89.2                      |                 | 6.9          | 85.8               |            |                  |               |          |  |  |  |
| 4.6        | 18.0                | 90.0                      |                 | 7.5          | 87.0               |            |                  |               |          |  |  |  |
| 4.9        | 18.4                | 91.1                      |                 | 8.4          | 87.9               |            |                  |               |          |  |  |  |
| 5.2        | 18.8                | 91.7                      |                 | 9.8          | 88.6               | _          |                  |               |          |  |  |  |
| 5.4        | 19.3                | 92.0                      |                 | 11.5         |                    | _          |                  | _             | -        |  |  |  |
| 5.6        | 19.9                | 92.4                      |                 | 14.5         |                    | _          |                  | _             |          |  |  |  |
| 5.7        | 20.4                |                           |                 | 17.3         |                    | _          | _                | _             |          |  |  |  |
| 6.3        | 21.0                |                           |                 | 21.5         |                    | _          |                  |               |          |  |  |  |
| 6.4        | 22.0                |                           |                 | 23.1         |                    | -          |                  |               |          |  |  |  |
| 6.6        | 23.0                |                           |                 | 24.7         |                    | -          |                  |               |          |  |  |  |
| 6.7        | 24.0                |                           |                 | 26.3         |                    | _          |                  |               |          |  |  |  |
| 7.0        | 25.2                |                           |                 | 28.0         |                    |            |                  |               |          |  |  |  |
| 7.1        | 26.9                |                           |                 | 29.7         |                    |            |                  |               |          |  |  |  |
| 7.2        | 29.9                |                           |                 | 31.2         |                    |            |                  |               |          |  |  |  |
| 7.5        | 32.0                |                           |                 | 32.8         |                    |            |                  |               |          |  |  |  |
| 7.6        | 33.9                |                           |                 | 34.3         |                    |            |                  |               |          |  |  |  |
| 7.8        | 35.5                |                           |                 | 35.8         |                    |            |                  |               |          |  |  |  |
| 8.1        | 37.3                |                           |                 | 37.3         |                    | _          |                  |               |          |  |  |  |
| 8.2        | 38.9                |                           |                 | 38.8         |                    | _          |                  |               |          |  |  |  |
| 0.3        | 40.7                |                           |                 | 40.2         |                    |            |                  |               |          |  |  |  |
| 0.4<br>8 7 | 42.0                |                           |                 | 43.3         |                    |            |                  |               |          |  |  |  |
| 8.9        | 47.1                |                           |                 | 44.8         |                    |            |                  |               |          |  |  |  |
| 9.2        | 49.5                |                           |                 | 46.3         |                    |            |                  |               |          |  |  |  |
| 9.4        | 51.8                |                           |                 | 47.7         |                    |            |                  |               |          |  |  |  |
| 9.6        | 53.7                |                           |                 | 49.2         |                    |            |                  |               |          |  |  |  |
| 9.8        | 55.1                |                           |                 | 50.6         |                    |            |                  |               |          |  |  |  |
| 9.9        | 56.4                |                           |                 | 52.1         |                    |            |                  |               |          |  |  |  |
| 10.1       | 57.9                |                           |                 | 53.4         |                    |            |                  |               |          |  |  |  |
| 10.4       | 59.4                |                           |                 | 54.9         |                    |            |                  |               |          |  |  |  |
| 10.9       | 60.8                |                           |                 | 56.4         |                    |            |                  |               |          |  |  |  |
| 11.1       | 62.3                |                           |                 | 57.7         |                    |            |                  |               |          |  |  |  |
| 11.5       | 63.6                |                           |                 | 59.1         |                    |            |                  |               | _        |  |  |  |
| 11.7       | 65.0                |                           |                 | 60.6         |                    | _          |                  |               |          |  |  |  |
| 11.9       | 00.0                |                           |                 | 02.0         |                    |            |                  |               |          |  |  |  |
| 12.2       | 60.4                |                           |                 | 65.0         |                    |            |                  |               |          |  |  |  |
| 12.4       | 09.4                |                           |                 | 00.0         |                    |            |                  |               |          |  |  |  |

## SHEET 6

|           |                       |                           | PROJECT NUMBER  |             | PROJECT I.D.        |             | ROUTE                    |                |        |  |  |  |  |
|-----------|-----------------------|---------------------------|-----------------|-------------|---------------------|-------------|--------------------------|----------------|--------|--|--|--|--|
|           | CONE PENET            | ROMETER                   | 34497.1.2       |             | R-2707D             |             |                          | US-74          |        |  |  |  |  |
|           |                       |                           |                 |             |                     |             | TECHNICIANS              |                |        |  |  |  |  |
|           | DATACODI              |                           | Cloveland       |             | Brott Smith DC      |             | Mike & Johnsthon Moseley |                |        |  |  |  |  |
| Ctation ( | ( +:                  |                           | Clevelarid      |             | Breu Smith, PG      |             | IVIIKE 6                 | a Johnathon Mc | oseley |  |  |  |  |
| Station ( | (location) Informatio | on<br>No                  |                 | Station (lo | cation) Information | 1           | Daté run                 |                |        |  |  |  |  |
| (-RAMP    | _A-) 46+00 - WB IS    | 55                        | 1/8/19 - 1/9/19 | (-RAMP_A    | -) 46+00 - WB OS    | N           |                          | 1/8/19 -       | 1/9/19 |  |  |  |  |
| Datum     |                       |                           | Easting         | Datum       |                     | Northing    | 550 440                  | Easting        | 4.005  |  |  |  |  |
| АВС       | FIII - 5              | 559,387                   | 1,264,198       | ABC         | FIII - 5            |             | 559,410                  | 1,20           | 4,205  |  |  |  |  |
|           | Cumu                  | lative Penetration in Cel | ntimeters       |             | Cumu                | lative Pene | etration in Centil       | neters         |        |  |  |  |  |
| 1.1       | 54.4                  |                           |                 | 1.0         | 56.0                |             |                          |                |        |  |  |  |  |
| 1.8       | 56.5                  |                           |                 | 1.5         | 57.6                |             |                          |                |        |  |  |  |  |
| 2.5       | 58.5                  |                           |                 | 1.9         | 59.2                |             |                          |                |        |  |  |  |  |
| 3.0       | 60.5                  |                           |                 | 2.4         | 60.9                |             | _                        |                |        |  |  |  |  |
| 3.5       | 62.4                  |                           |                 | 2.8         | 62.4                |             | _                        |                |        |  |  |  |  |
| 4.1       | 64.4                  |                           |                 | 3.2         | 63.9                |             | _                        |                |        |  |  |  |  |
| 4.7       | 66.4                  |                           |                 | 3.5         | 65.5                |             |                          |                |        |  |  |  |  |
| 5.1       | 08.4                  |                           |                 | 3.9         | 00.9                |             |                          |                |        |  |  |  |  |
| 5.5       | 70.4                  |                           |                 | 4.2         | 60.9                |             |                          |                |        |  |  |  |  |
| U.O       | 74.9                  |                           |                 | 4.0         | 71.2                |             |                          |                |        |  |  |  |  |
| 0.1       | 77.1                  |                           |                 | 4.9         | 70.7                |             |                          |                |        |  |  |  |  |
| 6.9       | 70.4                  |                           |                 | 5.3         | 74.1                |             |                          |                |        |  |  |  |  |
| 7.1       | 9.4                   |                           |                 | 5.7         | 75.2                |             |                          |                |        |  |  |  |  |
| 7.1       | 01.7                  |                           |                 | 6.0         | 76.6                |             | _                        | _              |        |  |  |  |  |
| 7.5       | 04.0                  |                           |                 | 6.0         | 78.0                |             | _                        | _              |        |  |  |  |  |
| 7.9       | 00.2                  |                           |                 | 0.9         | 70.0                |             | _                        | _              |        |  |  |  |  |
| 0.0       | 00.0                  |                           |                 | 7.4         | 79.3                |             |                          |                |        |  |  |  |  |
| 0.0       | 90.4                  |                           |                 | 7.0         | 00.0                |             | _                        |                |        |  |  |  |  |
| 9.3       | 91.0                  |                           |                 | 0.3         | 01.9                |             | _                        |                |        |  |  |  |  |
| 9.7       | 92.0                  |                           |                 | 0.0         | 03.1                |             | _                        |                |        |  |  |  |  |
| 10.0      | 93.1                  |                           |                 | 9.4         | 85.6                |             | _                        |                |        |  |  |  |  |
| 10.4      |                       |                           |                 | 10.0        | 86.8                |             |                          |                |        |  |  |  |  |
| 11.3      |                       |                           |                 | 10.4        | 88.1                |             |                          |                |        |  |  |  |  |
| 11.0      |                       |                           |                 | 11.6        | 89.3                |             |                          |                |        |  |  |  |  |
| 12.4      |                       |                           |                 | 12.2        | 90.5                |             | _                        |                |        |  |  |  |  |
| 12.1      |                       |                           |                 | 12.8        | 91.6                |             |                          |                |        |  |  |  |  |
| 13.3      |                       |                           |                 | 13.7        | 92.5                |             |                          |                |        |  |  |  |  |
| 13.7      |                       |                           |                 | 14.5        | 93.0                |             |                          |                |        |  |  |  |  |
| 14.2      |                       |                           |                 | 15.9        | 0010                |             |                          |                |        |  |  |  |  |
| 14.7      |                       |                           |                 | 17.5        |                     |             |                          |                |        |  |  |  |  |
| 15.2      |                       |                           |                 | 19.7        |                     |             |                          |                |        |  |  |  |  |
| 15.8      |                       |                           |                 | 21.6        |                     |             |                          |                |        |  |  |  |  |
| 16.3      |                       |                           |                 | 23.4        |                     |             |                          |                |        |  |  |  |  |
| 17.0      |                       |                           |                 | 24.9        |                     |             |                          |                |        |  |  |  |  |
| 17.6      |                       |                           |                 | 26.7        |                     |             |                          |                |        |  |  |  |  |
| 18.2      |                       |                           |                 | 28.3        |                     |             |                          |                |        |  |  |  |  |
| 19.2      |                       |                           |                 | 29.7        |                     |             |                          |                |        |  |  |  |  |
| 20.5      |                       |                           |                 | 31.8        |                     |             |                          |                |        |  |  |  |  |
| 22.0      |                       |                           |                 | 33.6        |                     |             |                          |                |        |  |  |  |  |
| 24.6      |                       |                           |                 | 35.3        |                     |             |                          |                |        |  |  |  |  |
| 27.1      |                       |                           |                 | 36.8        |                     |             |                          |                |        |  |  |  |  |
| 29.5      |                       |                           |                 | 38.4        |                     |             |                          |                |        |  |  |  |  |
| 32.0      |                       |                           |                 | 40.1        |                     |             |                          |                |        |  |  |  |  |
| 34.2      |                       |                           |                 | 41.7        |                     |             |                          |                |        |  |  |  |  |
| 36.6      |                       |                           |                 | 43.3        |                     |             |                          |                |        |  |  |  |  |
| 38.9      |                       |                           |                 | 45.0        |                     |             |                          |                |        |  |  |  |  |
| 41.4      |                       |                           |                 | 46.4        |                     |             |                          |                |        |  |  |  |  |
| 43.9      |                       |                           |                 | 47.8        |                     |             |                          |                |        |  |  |  |  |
| 46.1      |                       |                           |                 | 49.4        |                     |             |                          |                |        |  |  |  |  |
| 48.3      |                       |                           |                 | 51.1        |                     |             |                          |                |        |  |  |  |  |
| 50.3      |                       |                           |                 | 52.8        |                     |             |                          |                |        |  |  |  |  |
| 52.4      |                       |                           |                 | 54.5        |                     |             |                          |                |        |  |  |  |  |

|          |                        |                          | PROJECT        |             | PROJECT I.D.                   |    |         |           |        |          | ROUTE                         |              |          |   |          |  |  |
|----------|------------------------|--------------------------|----------------|-------------|--------------------------------|----|---------|-----------|--------|----------|-------------------------------|--------------|----------|---|----------|--|--|
|          | CONE PENE              | TROMETER                 | 34497          | 12          |                                |    | R-2707  | D         |        |          | US-74                         |              |          |   |          |  |  |
|          |                        |                          | 0011           |             |                                | (  |         | ICT       |        |          |                               | TI           |          |   |          |  |  |
|          | DATACOL                |                          | COUN           | and .       |                                |    | JEULUG  |           |        |          |                               | 11<br>Aika 9 |          |   | a a la v |  |  |
| 01.1     |                        |                          | Cievei         | anu         | 01.1                           | DI | eu Smin | I, PG     |        | _        | Ivince & Jorination Ivioseley |              |          |   |          |  |  |
| Station  | (location) information |                          | Date           | - <u>un</u> | Station (location) information |    |         |           |        |          |                               |              | Date run |   |          |  |  |
| (-RAIVIP | A-) 40+00 - WB         | USS Northing             | 1/6/19 -       | 1/9/19      | True a state of GU Manthaire a |    |         |           |        |          |                               |              | Fastin   | ~ |          |  |  |
| Datum    |                        | 550 /13                  | Lasung<br>1.26 | 1 206       | Type Cut or fill Northing      |    |         |           |        |          |                               |              | Easuii   | y |          |  |  |
| ABC      |                        | Ulativo Depotration in C | 1,204          |             |                                |    | Cumu    | lativo Do | notrat | ion in ( | Contim                        | otoro        |          |   |          |  |  |
| 0.9      | 21.0                   |                          | enumeters      | _           | -                              | _  | _       | Cuntu     |        | lietiat  |                               | Jenum        |          |   |          |  |  |
| 0.0      | 21.0                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 1.4      | 22.0                   |                          |                |             |                                |    | -       |           |        |          | -                             |              |          |   |          |  |  |
| 2.2      | 22.0                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 2.2      | 23.3                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 27       | 24.0                   |                          |                |             |                                |    | -       |           |        |          |                               |              |          |   |          |  |  |
| 3.1      | 24.9                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 3.4      | 25.5                   |                          |                |             |                                |    | -       |           |        |          |                               |              |          |   |          |  |  |
| 3.8      | 26.4                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 4.1      | 27.5                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 4.4      | 28.5                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 4.7      | 30.3                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 5.1      | 32.3                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 5.4      | 35.0                   |                          |                |             |                                |    |         |           |        |          |                               | _            |          |   |          |  |  |
| 5.9      | 30.0                   |                          |                |             |                                |    |         |           | _      |          |                               |              |          |   |          |  |  |
| 6.8      | 40.7                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 7.2      | 40.7                   |                          |                |             |                                |    | -       |           |        |          |                               |              |          |   |          |  |  |
| 7.5      | 44.8                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 8.0      | 46.8                   |                          |                |             |                                |    | -       |           |        |          |                               |              |          |   |          |  |  |
| 8.3      | 48.9                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 8.9      | 51.2                   |                          |                |             |                                |    | -       |           |        |          |                               |              |          |   |          |  |  |
| 9.4      | 53.7                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 9.8      | 56.2                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 10.1     | 58.0                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 10.7     | 59.7                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 11.1     | 62.0                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 11.5     | 66.0                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 12.0     | 69.3                   |                          | _              |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 12.4     | 71.6                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 13.0     | 74.0                   |                          |                |             |                                |    | -       |           |        |          |                               |              |          |   |          |  |  |
| 13.4     | 76.1                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 13.7     | 78.3                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 14.0     | 80.6                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 14.2     | 82.9                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 14.4     | 85.0                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 14.8     | 86.8                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 15.0     | 88.8                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 15.4     | 90.5                   |                          |                |             |                                |    |         |           |        |          |                               | _            |          |   |          |  |  |
| 15.7     | 91.0                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 16.0     | 92.3                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 16.7     | 00.2                   |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 17.1     |                        |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 17.5     |                        |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 17.9     |                        |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 18.3     |                        |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 18.8     |                        |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 19.1     |                        |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 19.6     |                        |                          |                |             | <u> </u>                       |    |         |           |        |          |                               |              |          |   |          |  |  |
| 20.1     |                        |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |
| 20.5     |                        |                          |                |             |                                |    |         |           |        |          |                               |              |          |   |          |  |  |

## SHEET 7

### North Carolina Department of Transportation Geotechnical Unit

Asphalt Core Photo



<u>Notes:</u> EB = Eastbound WB = Westbound ISS/OSS = Inside Shoulder/Outside Shoulder ISL/OSL = Inside Lane/Outside Lane



|                             | North Carolina Dep        |
|-----------------------------|---------------------------|
|                             | Geote                     |
| Project No: 34497.1.2       | <i>I.D. No.</i> : R-2707D |
| Site Description: US-74 (Sh | elby Bypass) from East of |
| Driller: Mike Moseley       | Core Size: 4-             |
| Geologist / Engineer: Brett | Smith, PG                 |
| Inches                      |                           |
| 0                           | 6"                        |
|                             |                           |
| Inches                      |                           |
| 0                           | 6"                        |
|                             |                           |
|                             |                           |

<u>Notes:</u> EB = Eastbound WB = Westbound ISS/OSS = Inside Shoulder/Outside Shoulder ISL/OSL = Inside Lane/Outside Lane





#### NORTH CAROLINA DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAY MATERIALS & TESTS UNIT** SOILS LABORATORY

#### T. I. P. No. R-2707D

#### **REPORT ON SAMPLES OF** PDI - US 74 Shelby Bypass

| Project       | 34497.1.1           | County     | Cleveland |    | Owner    | Geotech                 |
|---------------|---------------------|------------|-----------|----|----------|-------------------------|
| Date: Sampled | January 2019        | Received   | 1/9/19    |    | Reported | 2/25/19                 |
| Sampled from  | Pavement Design Inv | estigation |           | By | Geotech  |                         |
| Submitted by  | B. Smith            |            |           |    | 2008     | Standard Specifications |

2/25/19

#### **TEST RESULTS**

| Proj. Sample No.     | S-76   | <b>S-78</b> | S-79   | S-80 | S-82 |  |
|----------------------|--------|-------------|--------|------|------|--|
| Boring No.           | WB_OSS | RTL         | WB_ISS | ISS  | OSS  |  |
| Retained #4 Sieve %  | 2      | 3           | 3      | 1    | 1    |  |
| Passing #10 Sieve %  | 95     | 94          | 93     | 94   | 90   |  |
| Passing #40 Sieve %  | 32     | 78          | 74     | 73   | 36   |  |
| Passing #200 Sieve % | 21     | 57          | 57     | 51   | 29   |  |

|                       |   | MINUS | NO. 10 FR. | ACTION |      |      |  |
|-----------------------|---|-------|------------|--------|------|------|--|
| SOIL MORTAR - 100%    |   |       |            |        |      |      |  |
| Coarse Sand Ret - #60 | % | 75.2  | 24.3       | 27.7   | 31.1 | 63.5 |  |
| Fine Sand Ret - #270  | % | 3.9   | 20.9       | 16.4   | 20.6 | 7.7  |  |
| Silt 0.05 - 0.005 mm  | % | 4.8   | 22.0       | 20.4   | 15.0 | 4.1  |  |
| Clay < 0.005 mm       | % | 16.2  | 32.8       | 35.4   | 33.3 | 24.6 |  |
| Passing #40 Sieve     | % | 34.2  | 83.3       | 79.6   | 77.4 | 39.7 |  |
| Passing #200 Sieve    | % | 22.1  | 60.9       | 60.8   | 54.0 | 32.2 |  |

| L. L.                 | 42      | 43       | 35       | 39       | 43       |  |
|-----------------------|---------|----------|----------|----------|----------|--|
| P. I.                 | 15      | 12       | 11       | 14       | 18       |  |
| AASHTO Classification | A-2-7   | A-7-5    | A-6      | A-6      | A-2-7    |  |
| Group Index           | 0       | 6        | 4        | 4        | 1        |  |
| pH                    | N/A     | N/A      | N/A      | N/A      | N/A      |  |
| Station               | 46+00   | 39+50    | 46+00    | 35+50    | 35+50    |  |
| OFFSET                | N/A     | N/A      | N/A      | N/A      | N/A      |  |
| ALIGNMENT             | -RAMP_A | -Y5_WBL- | -RAMP_A- | -Y5_EBL- | -Y5_EBL- |  |
| Depth (Ft)            | 2.3     | 2.0      | 2.3      | 2.4      | 2.2      |  |
| to                    | 5.0     | 5.0      | 5.0      | 5.0      | 5.0      |  |
| Natural Moisture %    | 18.5    | 23.1     | 20.6     | 16.0     | 22.1     |  |

#### NORTH CAROLINA DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAY MATERIALS & TESTS UNIT** SOILS LABORATORY

T. I. P. No. R-2707D

#### **REPORT ON SAMPLES OF** PDI - US 74 Shelby Bypass Project 34497.1.1 County Clevela **Received** 1/9/19 **Date: Sampled** January 2019 Sampled from Pavement Design Investigation Submitted by B. Smith

#### 3/6/19

#### **TEST RESULTS** Proj. Sample No. S-5 **S-6** Boring No. N/A N/A Retained #4 Sieve 19 1 % 97 Passing #10 Sieve 73 % Passing #40 Sieve 42 54 % Passing #200 Sieve 22 26 %

#### MINUS NO. 10 FRACTION

| SOIL MORTAR - 100%    |   |      |      |      |  |  |
|-----------------------|---|------|------|------|--|--|
| Coarse Sand Ret - #60 | % | 51.7 | 62.1 | 44.1 |  |  |
| Fine Sand Ret - #270  | % | 16.8 | 19.9 | 20.4 |  |  |
| Silt 0.05 - 0.005 mm  | % | 18.0 | 12.5 | 35.1 |  |  |
| Clay < 0.005 mm       | % | 13.6 | 5.5  | 0.4  |  |  |
| Passing #40 Sieve     | % | 58.1 | 55.7 | 68.6 |  |  |
| Passing #200 Sieve    | % | 35.2 | 22.8 | 39.4 |  |  |

| L. L.                 | 50     | 36      | 41       |  |  |
|-----------------------|--------|---------|----------|--|--|
| P. I.                 | 6      | 2       | 5        |  |  |
| AASHTO Classification | A-2-5  | A-2-4   | A-5      |  |  |
| Group Index           | 0      | 0       | 0        |  |  |
| pН                    | N/A    | N/A     | N/A      |  |  |
| Station               | 845+00 | 20+00   | 43+00    |  |  |
| OFFSET                | 80' RT | 16' LT  | CL       |  |  |
| ALIGNMENT             | -L-    | -RAMP_D | -RAMP_A- |  |  |
| Depth (Ft)            | 0.5    | 0.5     | 0.5      |  |  |
| to                    | 3.5    | 3.5     | 3.5      |  |  |
| Natural Moisture %    | N/A    | N/A     | N/A      |  |  |

Aaron Hackett

Soils Engineer

M & T Form 503

| ind |    | Owner    | Geotech                 |
|-----|----|----------|-------------------------|
|     |    | Reported | 2/25/19                 |
|     | By | Geotech  |                         |
|     |    | 2008     | Standard Specifications |
|     |    |          |                         |

| S-7 |  |  |
|-----|--|--|
| N/A |  |  |
| 2   |  |  |
| 93  |  |  |
| 64  |  |  |
| 37  |  |  |

Aaron Hackett

Soils Engineer



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## **Standard Moisture-Density Relationship Report**

ASTM D698

Project Number 18-0173.146 Project Name R-2707D Client NCDOT Date 2/26/2019 Sample Number 5-5

Sample Description A-2-5 Sample Location -L- 845+00 80' RT Maximum Dry Density **89.2** Optimum Moisture **25.3%** 



| Natural Moisture: | N/A            |
|-------------------|----------------|
| Specific Gravity: | 2.60 (Assumed) |
| Liquid Limit:     | 50             |
| Plasticity Index: | 6              |
| % Fines:          | 26.0%          |
| % Sand:           | 55.0%          |
| % Gravel:         | 19.0%          |

| Rammer Type:         | Manual       |
|----------------------|--------------|
| Preparation Method:  | Dry          |
| Method:              | Α            |
| Oversize Correction: | Not Required |



Project Number 18-0173.146

## Standard Moisture-Density Relationship Report

ASTM D698

| n A-2-4<br>-RAMP_D- 20+00 16' LT<br>Moisture-Dens |
|---|
| Moisture-Dens                                     |
|   |
|   |
|   |
|   |
|   |
|   |
| • • • • • • • • • • • • • • • • • • •             |
|   |
|   |
|   |
|   |
| 12.5% 15.0% 17.5%                                 |
|   |

| Natural Moisture: | N/A            |
|-------------------|----------------|
| Specific Gravity: | 2.60 (Assumed) |
| Liquid Limit:     | 36             |
| Plasticity Index: | 2              |
| % Fines:          | 22.0%          |
| % Sand:           | 77.0%          |
| % Gravel:         | 1.0%           |
|                   |                |

Aaron Hackett, El

Lab Manager

Aaron Hackett, El

Lab Manager

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Date 3/6/2019 Sample Number S-6

Maximum Dry Density **94.0** Optimum Moisture **18.5%** 



Rammer Type:ManualPreparation Method:DryMethod:AOversize Correction:Not Required



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## **Standard Moisture-Density Relationship Report**

ASTM D698

| Project Number | 18-0173.146 |
|----------------|-------------|
| Project Name   | R-2707D     |
| Client         | NCDOT       |

Date 3/6/2019 Sample Number **S-7** 

Sample Description A-5 Sample Location -RAMP\_A- 43+00 CL Maximum Dry Density **109.1** Optimum Moisture 15.9%



| Natural Moisture: | N/A            |
|-------------------|----------------|
| Specific Gravity: | 2.60 (Assumed) |
| Liquid Limit:     | 41             |
| Plasticity Index: | 5              |
| % Fines:          | 37.0%          |
| % Sand:           | 61.0%          |
| % Gravel:         | 2.0%           |
|                   |                |

| Rammer Type:         | Manual       |
|----------------------|--------------|
| Preparation Method:  | Dry          |
| Method:              | Α            |
| Oversize Correction: | Not Required |



## Report on California Bearing Ratio (ASTM D 1883/AASHTO T 193)

| Date            | 3/6/2019          |
|-----------------|-------------------|
| Sample No.      | S-5, Run #1       |
| Sample Location | -L- 845+00 80' RT |

| Proctor and Classification Data |       |  |
|---------------------------------|-------|--|
| Sample Description              | N/A   |  |
| Classification                  | A-2-5 |  |
| Max. Dry Density                | 89.2  |  |
| Optimum Moisture                | 25.3% |  |

| Compaction Moisture Content | 27.4% |
|-----------------------------|-------|
| Moisture Content of Top 1"  |       |
| After Soaking               | 31.7% |
|                             |       |
| Swell                       | 0.6%  |



Remarks:

Aaron Hackett Lab Manager

Aaron Hackett, El

Lab Manager

CMT & SI Department Manager

Jeff Elliott, PE



| Project Name | R-2707D     |
|--------------|-------------|
| Project No.  | 18-0173.I46 |
| Client       | NCDOT       |

| <b>CBR Preparation Data</b>  |                    |  |  |
|------------------------------|--------------------|--|--|
| Rammer Used 5.5 lb, 12" drop |                    |  |  |
| Compaction Method            | 3 Layers, 56 Blows |  |  |
| Surcharge Amount             | 10 lbs             |  |  |
| Soaked/Unsoaked              | Soaked             |  |  |
|                              |                    |  |  |

### **CBR Results**

| Dry unit weight (lbs/cu.ft) | 89.7   |
|-----------------------------|--------|
| Percent of Max. Dry Density | 100.6% |

| CBR Values       |      |       |
|------------------|------|-------|
| Penetration (in) | 0.1  | 0.2   |
| Stress (psi)     | 9.30 | 18.40 |
| CBR              | 0.9  | 1.2   |

Zero-point correction applied. All material passed the 3/4" sieve.



## Report on California Bearing Ratio (ASTM D 1883/AASHTO T 193)

| Date            | 3/6/2019          | Project Name | R-2707D     |
|-----------------|-------------------|--------------|-------------|
| Sample No.      | S-5, Run #2       | Project No.  | 18-0173.146 |
| Sample Location | -L- 845+00 80' RT | Client       | NCDOT       |

#### **Proctor and Classification Data**

| Sample Description | N/A   |
|--------------------|-------|
| Classification     | A-2-5 |
| Max. Dry Density   | 89.2  |
| Optimum Moisture   | 25.3% |

| <b>CBR Preparation Data</b> |                    |
|-----------------------------|--------------------|
| Rammer Used                 | 5.5 lb, 12" drop   |
| Compaction Method           | 3 Layers, 56 Blows |
| Surcharge Amount            | 10 lbs             |
| Soaked/Unsoaked             | Soaked             |

## **CBR Results**

| Compaction Moisture Content | 29.1% | Dry unit weight (lbs/ | cu.ft) | 88.1  |
|-----------------------------|-------|-----------------------|--------|-------|
| Moisture Content of Top 1"  |       | Percent of Max. Dry D | ensity | 98.8% |
| After Soaking               | 28.4% |                       | -      |       |
| -                           |       | CBR Val               | ues    |       |
| Swell                       | 0.2%  | Penetration (in)      | 0.1    | 0.2   |
| -                           |       | Stress (psi)          | 9.30   | 16.10 |
|                             |       | CBR                   | 0.9    | 1.1   |





Zero-point correction applied. All material passed the 3/4" sieve.

Aaron Hackett Lab Manager

Jeff Elliott, P.E. CMT & SI Dept. Manager



## Report on California Bearing Ratio (ASTM D 1883/AASHTO T 193)

| Date            | 3/6/2019             |
|-----------------|----------------------|
| Sample No.      | S-6, Run #1          |
| Sample Location | RAMP_D- 20+00 16' L' |

# **Proctor and Classification Data**

| Sample Description | N/A   |
|--------------------|-------|
| Classification     | A-2-4 |
| Max. Dry Density   | 94.0  |
| Optimum Moisture   | 18.5% |
| -                  |       |

| <b>Compaction Moisture Content</b> | 10.0% |
|------------------------------------|-------|
| Moisture Content of Top 1"         |       |
| After Soaking                      | 30.0% |
|                                    |       |
| Swell                              | N/A   |

Remarks:



| Project Name | R-2707D     |
|--------------|-------------|
| Project No.  | 18-0173.I46 |
| Client       | NCDOT       |

| <b>CBR Preparation Data</b> |                    |  |
|-----------------------------|--------------------|--|
| Rammer Used                 | 5.5 lb, 12" drop   |  |
| Compaction Method           | 3 Layers, 56 Blows |  |
| Surcharge Amount            | 10 lbs             |  |
| Soaked/Unsoaked             | Soaked             |  |
| -                           |                    |  |

### **CBR Results**

| Dry unit weight (lbs/cu.ft) | 89.7  |
|-----------------------------|-------|
| Percent of Max. Dry Density | 95.4% |

| CBR Values       |       |       |
|------------------|-------|-------|
| Penetration (in) | 0.1   | 0.2   |
| Stress (psi)     | 38.00 | 72.50 |
| CBR              | 3.8   | 4.8   |



Zero-point correction applied. All material passed the 3/4" sieve.

Jeff Elliott, P.E. CMT & SI Dept. Manager



## Report on California Bearing Ratio (ASTM D 1883/AASHTO T 193)

| Date            | 3/6/2019             | Project Name | R-2707D     |
|-----------------|----------------------|--------------|-------------|
| Sample No.      | S-6, Run #2          | Project No.  | 18-0173.146 |
| Sample Location | RAMP_D- 20+00 16' L' | Client       | NCDOT       |

### **Proctor and Classification Data**

| Sample Description | N/A   |
|--------------------|-------|
| Classification     | A-2-4 |
| Max. Dry Density   | 94.0  |
| Optimum Moisture   | 18.5% |

| <b>CBR Preparation Data</b> |                    |  |
|-----------------------------|--------------------|--|
| Rammer Used                 | 5.5 lb, 12" drop   |  |
| <b>Compaction Method</b>    | 3 Layers, 56 Blows |  |
| Surcharge Amount            | 10 lbs             |  |
| Soaked/Unsoaked             | Soaked             |  |

## **CBR Results**

| <b>Compaction Moisture Content</b> | 9.8%  | Dry unit weight (lbs/cu.ft) | 87.3  |
|------------------------------------|-------|-----------------------------|-------|
| Moisture Content of Top 1"         |       | Percent of Max. Dry Density | 92.9% |
| After Soaking                      | 32.0% |                             |       |
|                                    |       | CBR Values                  |       |
| Swell                              | 1.1%  | Penetration (in) 0.1        | 0.2   |
|                                    |       | Stress (psi) 36.00          | 60.40 |
|                                    |       | CBR <b>3.6</b>              | 4.0   |





Zero-point correction applied. All material passed the 3/4" sieve.

Aaron Hackett Lab Manager

| Jeff    | Elliott, P.E.   |
|---------|-----------------|
| CMT & S | I Dept. Manager |



## Report on California Bearing Ratio (ASTM D 1883/AASHTO T 193)

| Date            | 3/6/2019          |
|-----------------|-------------------|
| Sample No.      | S-7, Run #1       |
| Sample Location | -RAMP_A- 43+00 CL |

#### **Proctor and Classification Data** . . . . . . . . . . **NI / A**

| Sample Description | N/A   |
|--------------------|-------|
| Classification     | A-5   |
| Max. Dry Density   | 109.1 |
| Optimum Moisture   | 15.9% |
|                    |       |

| Compaction Moisture Content | 12.3% |
|-----------------------------|-------|
| Moisture Content of Top 1"  |       |
| After Soaking               | 23.0% |
|                             |       |
| Swell                       | 1.3%  |



Remarks:



| Project Name | R-2707D     |  |
|--------------|-------------|--|
| Project No.  | 18-0173.I46 |  |
| Client       | NCDOT       |  |

| <b>CBR Preparation Data</b>         |        |  |  |
|-------------------------------------|--------|--|--|
| Rammer Used 5.5 lb, 12" drop        |        |  |  |
| Compaction Method 3 Layers, 56 Blow |        |  |  |
| Surcharge Amount                    | 10 lbs |  |  |
| Soaked/Unsoaked Soaked              |        |  |  |
|                                     |        |  |  |

### **CBR Results**

| Dry unit weight (lbs/cu.ft) | 109.9  |
|-----------------------------|--------|
| Percent of Max. Dry Density | 100.7% |

| CBR Values       |       |       |
|------------------|-------|-------|
| Penetration (in) | 0.1   | 0.2   |
| Stress (psi)     | 43.00 | 77.00 |
| CBR              | 4.3   | 5.1   |

Zero-point correction applied. All material passed the 3/4" sieve.





## Report on California Bearing Ratio (ASTM D 1883/AASHTO T 193)

| Date            | 3/6/2019          | Project Name | R-2707D     |  |
|-----------------|-------------------|--------------|-------------|--|
| Sample No.      | S-7, Run #2       | Project No.  | 18-0173.I46 |  |
| Sample Location | -RAMP_A- 43+00 CL | Client       | NCDOT       |  |

| Proctor and C      | <b>Classification Data</b> | CBR P             | reparation Data    |
|--------------------|----------------------------|-------------------|--------------------|
| Sample Description | N/A                        | Rammer Used       | 5.5 lb, 12" drop   |
| Classification     | A-5                        | Compaction Method | 3 Layers, 56 Blows |
| Max. Dry Density   | 109.1                      | Surcharge Amount  | 10 lbs             |
| Optimum Moisture   | 15.9%                      | Soaked/Unsoaked   | Soaked             |

|                             |       | CBR Results                       |
|-----------------------------|-------|-----------------------------------|
| Compaction Moisture Content | 12.3% | Dry unit weight (lbs/cu.ft) 108.9 |
| Moisture Content of Top 1"  |       | Percent of Max. Dry Density 99.9% |
| After Soaking               | 22.1% |                                   |
|                             |       | CBR Values                        |
| Swell                       | 1.3%  | Penetration (in) 0.1 0.2          |
|                             |       | Stress (psi) 49.03 91.13          |
|                             |       | CBR <b>4.9 6.1</b>                |



Remarks:

No zero-point correction. All material passed the 3/4" sieve.

Aaron Hackett Lab Manager Jeff Elliott, P.E. CMT & SI Dept. Manager

## SHEET 14