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SEE SHEET 3 FOR PLAN SHEET LAYOUT  
AT TIME OF INVESTIGATION

STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5751	1	90

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DATE FEBRUARY 2021

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SIGNATURE DATE

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ROADWAY  
SUBSURFACE INVESTIGATION

COUNTY ROBESON

PROJECT DESCRIPTION UPGRADE OF AT-GRADE  
INTERSECTIONS AT US 74 /NC 72 AND US 74 /NC  
130 TO INTERCHANGE

INVENTORY






REFERENCE: R-5751

PROJECT: 53087

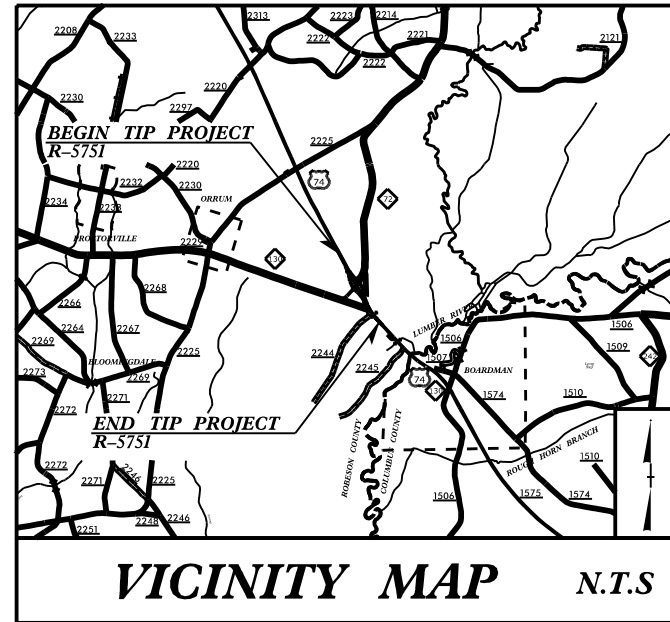
# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT

## SUBSURFACE INVESTIGATION

### SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION	GRADATION	ROCK DESCRIPTION	TERMS AND DEFINITIONS
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i>	WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.	HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:  WEATHERED ROCK (WR)  NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.  CRYSTALLINE ROCK (CR)  FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.  NON-CRYSTALLINE ROCK (NCR)  FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.  COASTAL PLAIN SEDIMENTARY ROCK (CPS)  COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.	ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SCREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
<b>SOIL LEGEND AND AASHTO CLASSIFICATION</b>	<b>ANGULARITY OF GRAINS</b> THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.	<b>WEATHERING</b>	
<b>MINERALOGICAL COMPOSITION</b> MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.	<b>COMPRESSIONIBILITY</b> SLIGHTLY COMPRESSIBLE LL < 31 MODERATELY COMPRESSIBLE LL = 31 - 50 HIGHLY COMPRESSIBLE LL > 50	<b>FRESH</b> ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.  <b>VERY SLIGHT (V SLI.)</b> ROCK GENERALLY FRESH, JOINTS STAINED. SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.  <b>SLIGHT (SLI.)</b> ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.  <b>MODERATE (MOD.)</b> SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED. SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.  <b>MODERATELY SEVERE (MOD. SEV.)</b> ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. <i>IF TESTED, WOULD YIELD SPT REFUSAL</i>  <b>SEVERE (SEV.)</b> ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &gt; 100 BPF</i>  <b>VERY SEVERE (V SEV.)</b> ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &lt; 100 BPF</i>  <b>COMPLETE</b> ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.	
<b>PERCENTAGE OF MATERIAL</b>	<b>GROUND WATER</b>		
ORGANIC MATERIAL TRACE OF ORGANIC MATTER 2 - 3% LITTLE ORGANIC MATTER 3 - 5% MODERATELY ORGANIC 5 - 10% HIGHLY ORGANIC > 10%	GRANULAR SOILS SILT - CLAY SOILS OTHER MATERIAL TRACE 1 - 10% LITTLE 10 - 20% SOME 20 - 35% HIGHLY 35% AND ABOVE		
<b>MISCELLANEOUS SYMBOLS</b>	<b>RECOMMENDATION SYMBOLS</b>	<b>ROCK HARDNESS</b>	
ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION SOIL SYMBOL ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT INFERRED SOIL BOUNDARY INFERRED ROCK LINE ALLUVIAL SOIL BOUNDARY	UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK  AR - AUGER REFUSAL BT - BORING TERMINATED CL - CLAY CPT - CONE PENETRATION TEST CSE - COARSE DMT - DILATOMETER TEST DPT - DYNAMIC PENETRATION TEST e - VOID RATIO F - FINE FOSS. - FOSSILIFEROUS FRAC. - FRACTURED, FRACTURES FRAG. - FRAGMENTS HI. - HIGHLY	VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.  HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.  MODERATELY HARD CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.  MEDIUM HARD CAN BE GROUDED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.  SOFT CAN BE GROUDED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.  VERY SOFT CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.	
<b>CONSISTENCY OR DENSENESS</b>	<b>ABBREVIATIONS</b>	<b>FRACTURE SPACING</b>	<b>BEDDING</b>
PRIMARY SOIL TYPE GENERALLY GRANULAR MATERIAL (NON-COHESIVE) GENERALLY SILT-CLAY MATERIAL (COHESIVE)	RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE) RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> )	TERM SPACING VERY WIDE MORE THAN 10 FEET WIDE 3 TO 10 FEET MODERATELY CLOSE 1 TO 3 FEET CLOSE 0.16 TO 1 FOOT VERY CLOSE LESS THAN 0.16 FEET	TERM THICKNESS VERY THICKLY BEDDED 4 FEET THICKLY BEDDED 1.5 - 4 FEET THINLY BEDDED 0.16 - 1.5 FEET VERY THINLY BEDDED 0.03 - 0.16 FEET THICKLY LAMINATED 0.008 - 0.03 FEET THINLY LAMINATED < 0.008 FEET
VERY LOOSE < 4 LOOSE 4 TO 10 MEDIUM DENSE 10 TO 30 DENSE 30 TO 50 VERY DENSE > 50	< 0.25 0.25 TO 0.5 0.5 TO 1.0 1 TO 2 2 TO 4 > 4		
VERY SOFT < 2 SOFT 2 TO 4 MEDIUM STIFF 4 TO 8 STIFF 8 TO 15 VERY STIFF 15 TO 30 HARD > 30			
<b>TEXTURE OR GRAIN SIZE</b>	<b>EQUIPMENT USED ON SUBJECT PROJECT</b>		
U.S. STD. SIEVE SIZE OPENING (MM) BOULDER (BLDR.) COBBLE (COB.) GRAVEL (GR.) COARSE SAND (CS. SD.) FINE SAND (F SD.) SILT (SL.) CLAY (CL.)	DRILL UNITS: CME-45C CME-55 CME-550 VANE SHEAR TEST PORTABLE HOIST DIEDRICH D-50	VERY HARD HARD MODERATELY HARD MEDIUM HARD SOFT VERY SOFT	
GRAIN SIZE MM 305 IN 12 75 3 2.0 0.25 0.05 0.005	ADVANCING TOOLS: CLAY BITS 6" CONTINUOUS FLIGHT AUGER 8" HOLLOW AUGERS HARD FACED FINGER BITS TUNG-CARBIDE INSERTS CASING w/ ADVANCER TRICONE *STEEL TEETH TRICONE 2-15/16" TUNG-CARB. CORE BIT		
<b>SOIL MOISTURE - CORRELATION OF TERMS</b>			
SOIL MOISTURE SCALE (ATTERBERG LIMITS) FIELD MOISTURE DESCRIPTION GUIDE FOR FIELD MOISTURE DESCRIPTION			
LL - LIQUID LIMIT PL - PLASTIC LIMIT OM - OPTIMUM MOISTURE SHRINKAGE LIMIT	- SATURATED - (SAT.) - WET - (W) - MOIST - (M) - DRY - (D)		
	USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE SOLID; AT OR NEAR OPTIMUM MOISTURE REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE		
<b>PLASTICITY</b>			
NON PLASTIC SLIGHTLY PLASTIC MODERATELY PLASTIC HIGHLY PLASTIC	PLASTICITY INDEX (PI) 0-5 6-15 16-25 26 OR MORE		
	DRY STRENGTH VERY LOW SLIGHT MEDIUM HIGH		
<b>COLOR</b>			
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.			
		<b>INDURATION</b> FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.  FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.  MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.  INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.  EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.	<b>NOTES:</b> FIAD - FILLED IMMEDIATELY AFTER DRILLING   PAVEMENT DESIGN INVESTIGATION TEST LOCATION AND CORE
			BENCH MARK: TOP OF BORING ELEVATIONS ESTIMATED USING PROVIDED PROJECT TINE FILE: (R5751_Is_tin.tin) DATED: 08/30/2018 ELEVATION: N/A FEET

**TIP PROJECT: R-5751**



25% APPROVED PLANS

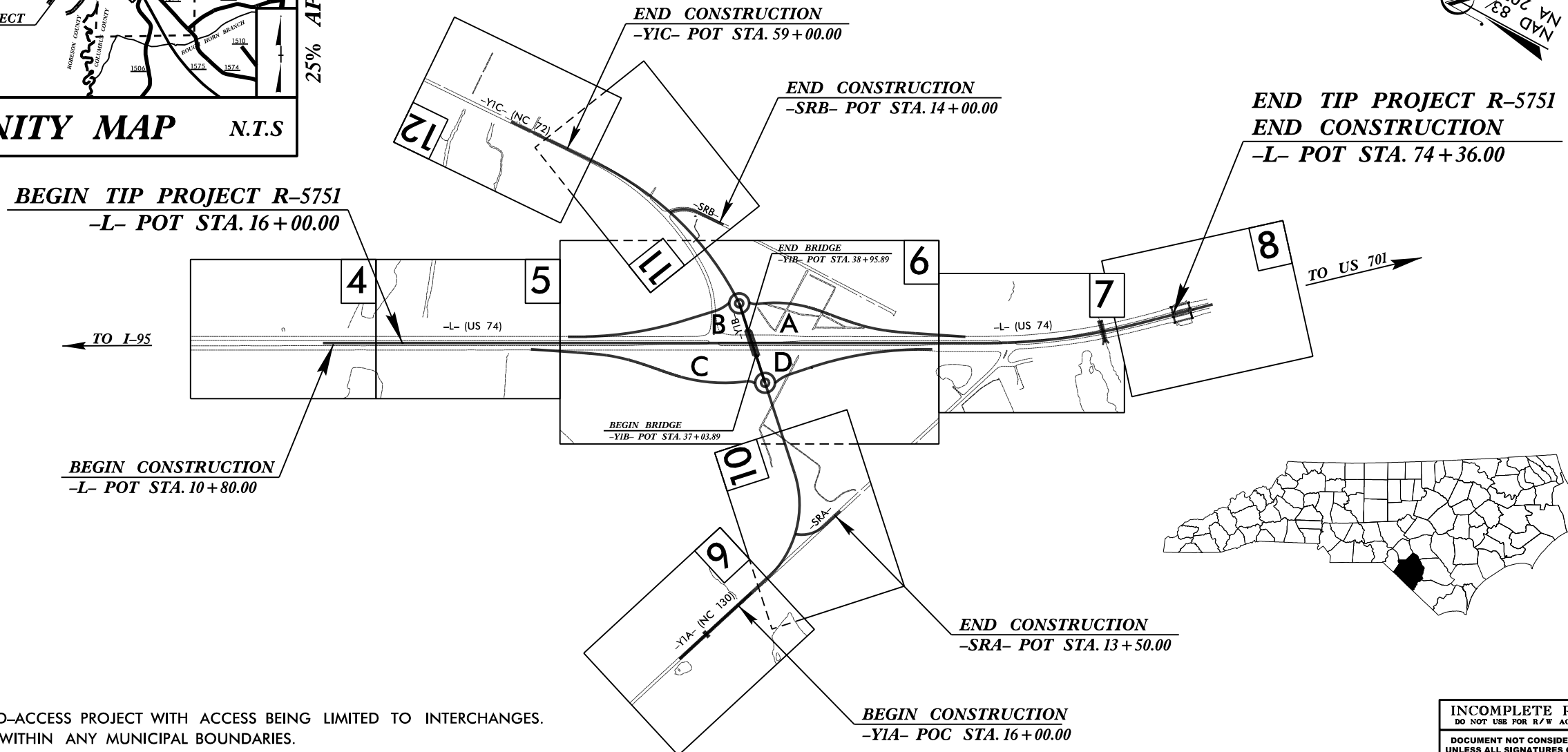
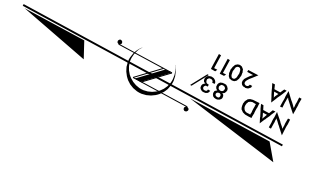
STATE OF NORTH CAROLINA  
DIVISION OF HIGHWAYS

**ROBESON COUNTY**

LOCATION: US 74 AT NC 72 / NC 130  
CONVERT INTERSECTION TO INTERCHANGE

TYPE OF WORK: GRADING, PAVING, DRAINAGE, AND STRUCTURE

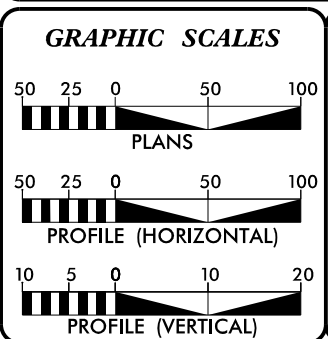
STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5751	3	90
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
53087.1.1	NHP-0074(203)	PE	



THIS IS A CONTROLLED-ACCESS PROJECT WITH ACCESS BEING LIMITED TO INTERCHANGES.  
THIS PROJECT IS NOT WITHIN ANY MUNICIPAL BOUNDARIES.  
CLEARING ON THIS PROJECT SHALL BE PERFORMED TO THE LIMITS ESTABLISHED BY METHOD II.

**INCOMPLETE PLANS**  
DO NOT USE FOR R/W ACQUISITION  
DOCUMENT NOT CONSIDERED FINAL  
UNLESS ALL SIGNATURES COMPLETED

**CONTRACT:**



**DESIGN DATA**

ADT 2022 =	20,300
ADT 2042 =	30,000
K =	8 %
D =	55 %
T =	19 % *
V =	75 MPH
*(TTST=12% + DUAL=7%)	
FUNC CLASS =	FUTURE INTERSTATE STATEWIDE TIER

**PROJECT LENGTH**

LENGTH ROADWAY TIP PROJECT R-5751	=	1.105 MILES
TOTAL LENGTH TIP PROJECT R-5751	=	1.105 MILES

PREPARED IN THE OFFICE OF:  
**RS&H**  
8521 SIX FORKS ROAD, SUITE 400  
RALEIGH, NC 27615  
NC FIRM LICENSE No: F-0493

2018 STANDARD SPECIFICATIONS

**RIGHT OF WAY DATE:**  
JANUARY 24, 2020

**LETTING DATE:**  
JANUARY 18, 2022

PREPARED FOR:  
**DIVISION OF HIGHWAYS**  
DIVISION 6  
558 Gillespie St.  
Fayetteville, NC 28301  
910-364-0603

**JARED BOND, PE**  
PROJECT ENGINEER

**SEAN KANE, EI**  
PROJECT DESIGN ENGINEER

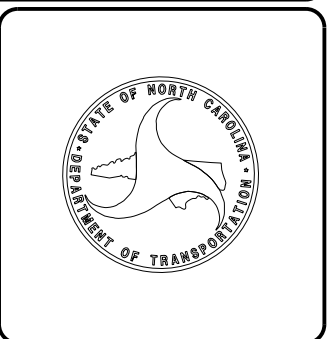
**ALEX HENDERSON**  
NCDOT CONTACT

**HYDRAULICS ENGINEER**

SIGNATURE: \_\_\_\_\_ P.E.

**ROADWAY DESIGN ENGINEER**

SIGNATURE: \_\_\_\_\_ P.E.



Date: January 29, 2021  
 WBS Number: 53087.1.1  
 TIP Number: R-5751  
 County: Robeson  
 Description: Upgrade of at-grade intersections at US 74/NC 72 and US 74/NC 130 to interchange

-Y1PRD- 10+00 to 22+30  
 -SRA- 10+00 to 14+02  
 -SRB- 10+00 to 14+34

**Subject: Roadway Geotechnical Report - Inventory**

**Project Description**

The project is located near the Town of Orrum in Robeson County, North Carolina and consists of the addition of two roundabouts, four ramps, and a bridge over US 74 (-L-). The project reroutes NC 72 (-Y1C-) and NC 130 (-Y1A-) and combines them into a single interchange for access to US 74 (-L-).

The length of the project is about 1.1 miles along -L-, 1.1 miles combined along -Y1A-, -Y1B-, and -Y1C-, and 1.1 miles combined along the ramp alignments (-Y1RPA-, -Y1RPB-, -Y1RPC-, and -Y1RPD-). There are two roundabouts (-RAB-, -RCD-) located along the overpass combined alignment (-Y1A-, -Y1B, and -Y1C-) on either side of US 74. Realignment of two services roads (-SRA-, -SRB-) less than 0.1 miles long will be included in the project. The project corridor is in a rural setting with mostly vegetation and farm land along each alignment, with some areas of delineated wetlands.

The geotechnical subsurface investigation was performed in June and July of 2019 and supplemental hand augers performed in January 2021. The site was investigated with 42 standard penetration test (SPT) borings that were advanced using a Diedrich D-50 track mounted rotary drill rig equipped with a calibrated automatic hammer. The SPT borings were advanced with hollow stem augers to depths of 10 to 12 feet beneath the ground surface and with mud rotary to depths of 19 to 84 feet beneath the ground surface. Representative soil samples were collected in the field for visual classification and selected samples were submitted for laboratory analysis by Terracon's soil testing laboratory. Laboratory testing was performed in accordance with the NCDOT laboratory testing standards. The hand augers were performed to identify groundwater depths in the wet season and included 14 hand augers at previous boring locations and 11 hand augers at new locations. The hand augers ranged in depth from 2 to 6 feet.

The following alignments were investigated by soil testing and visual reconnaissance:

<u>Alignment</u>	<u>Stations (±)</u>
-L-	10+80 to 74+36
-RAB-	10+00 to 14+71
-RCD-	10+00 to 14+71
-Y1A-	10+00 to 34+84
-Y1B-	34+84 to 41+15
-Y1C-	41+15 to 59+00
-Y1RPA-	10+00 to 26+68
-Y1RPB-	10+00 to 22+58
-Y1RPC-	10+00 to 27+26

**Physiography and Geography**

The site is located in the Lumber River basin and primarily consists of Duplin Formation soils with recent alluvial soils in the low lying swampy areas as discussed below. The existing elevations along the investigated corridor range from approximately 76 feet to 86 feet. The western portion of the project is located in the White Oak Swamp. Based on the presence of several rivers and creeks and the surrounding very flat terrain, the site appears to be located in a flood prone and swampy area.

**Soil Properties**

Soils encountered during this investigation are separated into four categories based on their origin. The soils encountered consist of roadway embankment, artificial fill, alluvial deposit and coastal plain soils. We anticipate that roadway embankments were constructed to elevate roads through low-lying swampy areas and areas prone to flooding. Artificial fill was encountered in isolated areas outside the roadway embankments to raise those locations above the surrounding swampy areas. Alluvial deposits were identified within the limits of the delineated wetlands area. Coastal plain soils are found at the surface in some areas and below the surficial roadway embankment, artificial fill and alluvial soil across the entire.

In general, the roadway embankment soils generally consist of very loose to medium dense silty sand and clayey sand to fine sands (A-2-4, A-2-6, A-3) and stiff sandy silt and sandy clay (A-4, A-6), and the artificial fill soils consist of medium dense silty sand and sand with clay (A-2-4, A-2-6). Alluvial deposits consist of very loose to loose, clayey sand, silty sand, and sand with clay (A-1-b, A-2-4, A-2-5, A-2-6), very soft silty and sandy clay and sandy silt (A-6, A-7, A-4) and very soft silty clay with trace organics to highly organic (ORG1, ORG2, A-6). Coastal plain (Duplin Formation) soils encountered consist of very soft to hard sandy silts and sandy to silty clays and clay with sand (A-4, A-6, A-7), very loose to very dense fine to coarse sands (A-1, A-3), and very loose to dense silty to clayey sands (A-2-4, A-2-6).

**Groundwater Properties**

The Lumber River passes near the site to the east, running approximately perpendicular to -L-. Tributary creeks can also be found east of the site, one crossing -L- through a culvert, and tie into the Lumber River. The majority of the west portion and some of the east portion of the project are within the limits of White Oak Swamp. Groundwater was encountered during our explorations from depths of 1 to 6 feet beneath the ground surface. Surface water was observed at several boring locations within the delineated wetlands, in ditches and in other low areas at the time of our investigation.

The depth of groundwater, beneath the ground surface, will fluctuate with seasonal precipitation and may occur at higher levels at other times of the year above less permeable clayey soils.



**Areas of Special Geotechnical Interest**

1) Very soft to soft and wet soils were encountered at the following approximate locations:

<u>Alignment</u>	<u>Stations (±)</u>
-L-	32+00 to 33+00, 36+50 to 37+00
-Y1A-	19+00 to 29+00, 30+50 to 31+50, 32+50 to 33+50
-Y1C-	47+50 to 48+50
-Y1PRB-	17+50 to 18+50, 19+50 to 21+00
-Y1PRC-	15+80 to 16+80, 18+75 to 19+75, 23+75 to 24+75
-Y1RPD-	19+50 TO 20+50

2) Near surface soils with little to moderate organics requiring remediation were encountered at the following approximate locations:

<u>Alignment</u>	<u>Stations (±)</u>
-Y1A-	19+00 to 24+50

3) Groundwater was encountered within 6 feet of proposed pavement subgrade at the following approximate locations:

<u>Alignment</u>	<u>Stations (±)</u>
-Y1RPA-	15+00 TO 18+00
-Y1A-	19+00 TO 25+50
-Y1RPC-	10+00 TO 18+50
-Y1RPB-	10+00 TO 14+50

**BULK SAMPLES**

The following bulk samples were taken for tests to determine the engineering properties of the soil.

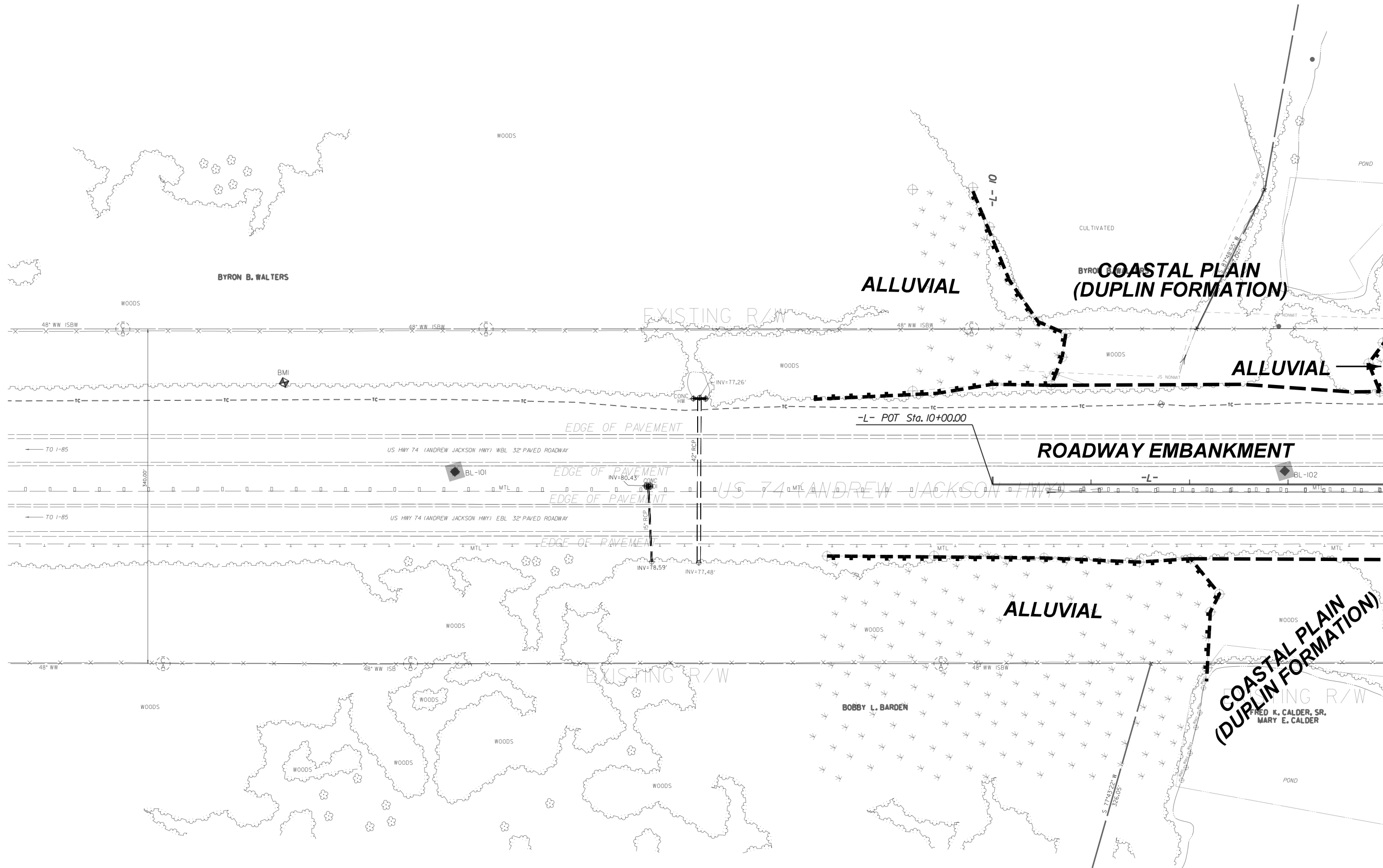
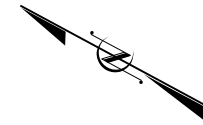
<u>Sample No.</u>	<u>Location</u>	<u>Depth (ft.)</u>	<u>Test</u>
CBR-1	12+00 -Y1RPD-, 70' RT	0.5 – 1.5	Proctor and CBR
CBR-2	13+00 -Y1RPA-, 68' LT	0.5 – 1.5	Proctor and CBR
CBR-4	16+20 -Y1RPC-, CL	0.5 – 1.5	Proctor and CBR

**Closing**

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report, or if we may be of further service, please contact us at your convenience.

**Sincerely,**  
**Terracon Consultants, Inc.**

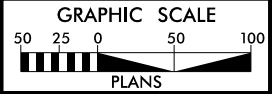
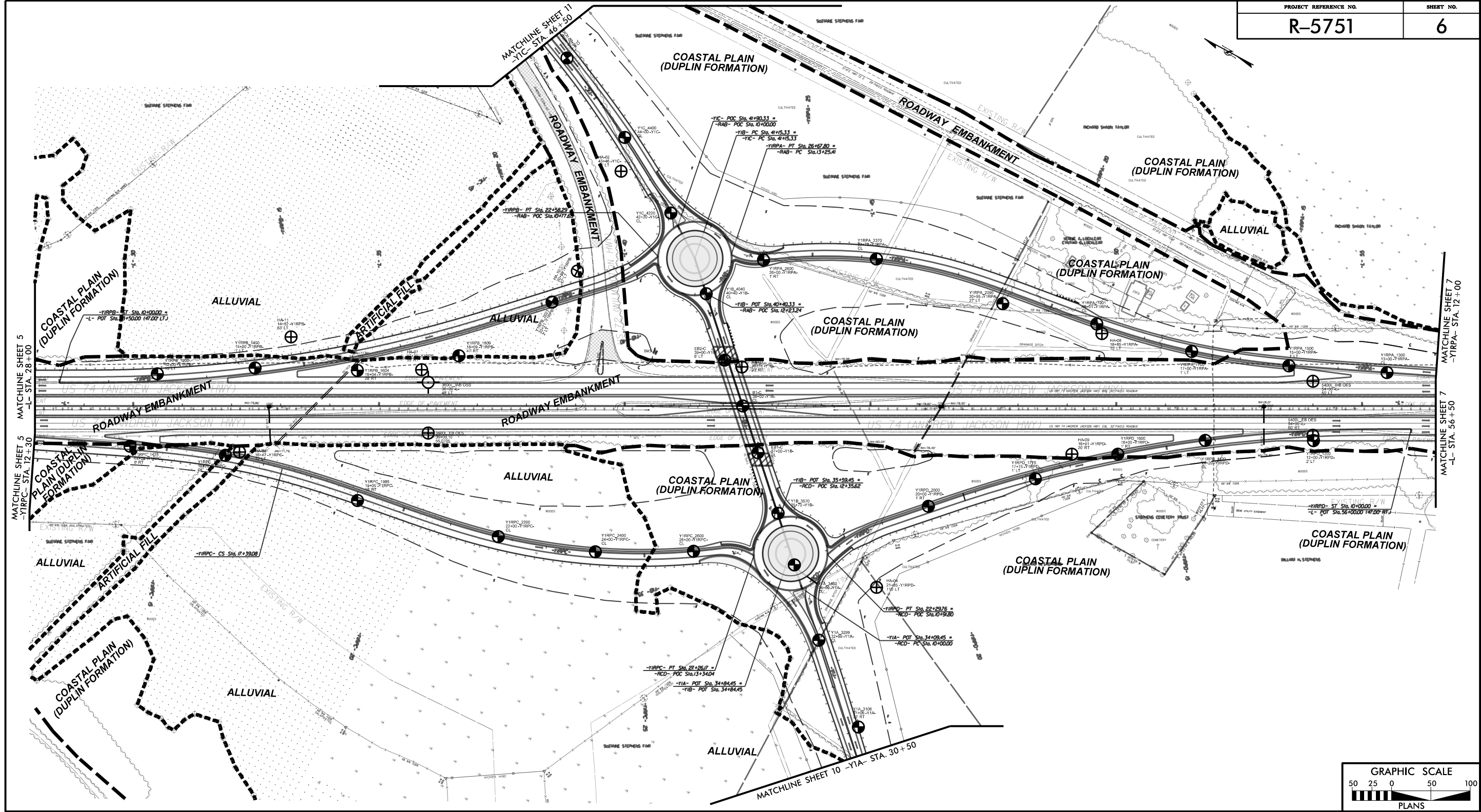
Jonathan P. Manke, PE  
Senior Geotechnical Engineer



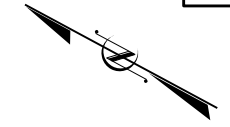
MATCHLINE SHEET 5 -L- STA. 14+00







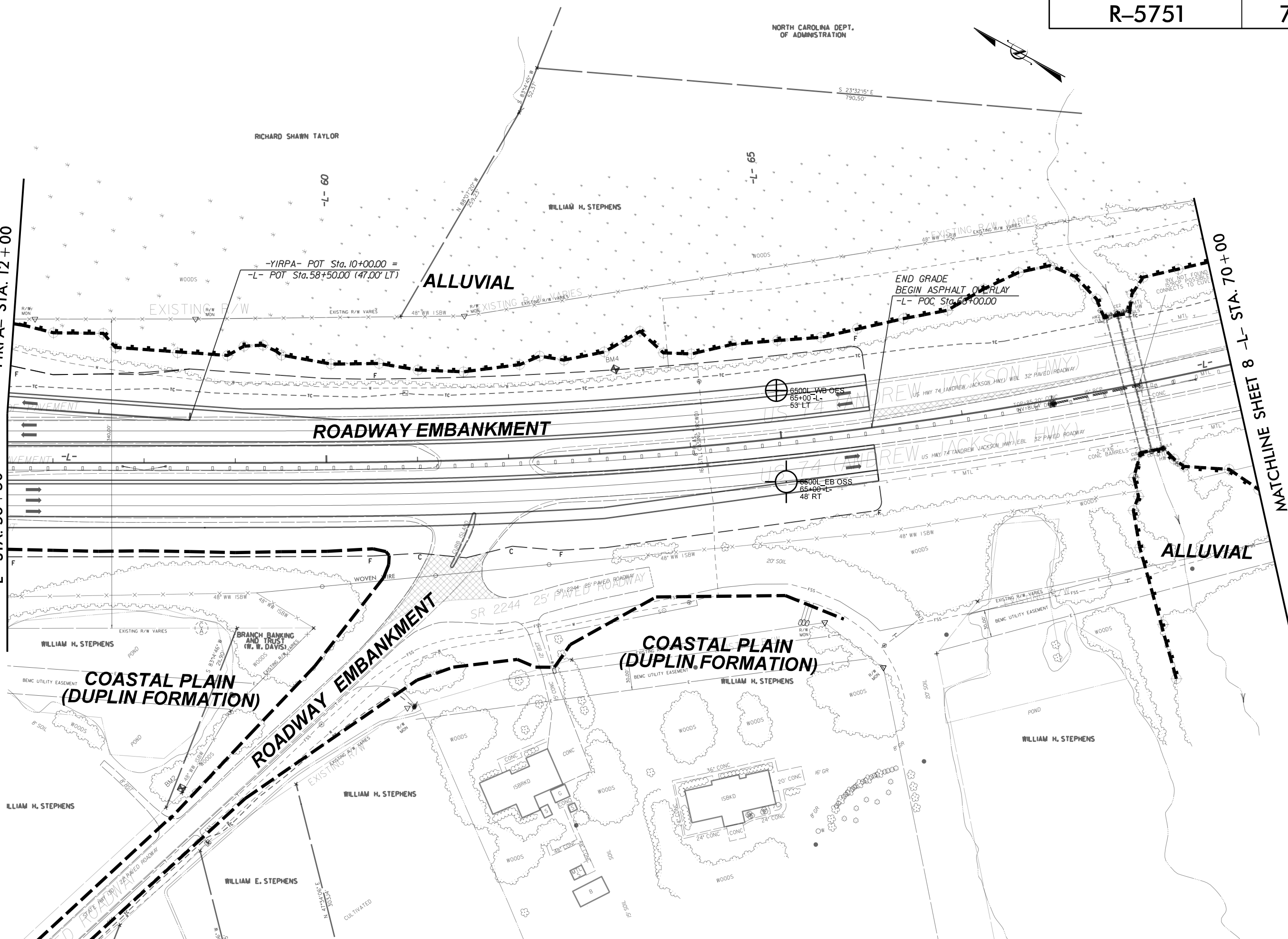
NORTH CAROLINA DEPT. OF ADMINISTRATION



MATCHLINE SHEET 6  
-YIRPA- STA. 12+00

MATCHLINE SHEET 6  
-L- STA. 56+50

MATCHLINE SHEET 8 -L- STA. 70+00



-YIRPA- POT Sta. 10+00.00 =  
-L- POT Sta. 58+50.00 (47.00' LT)

ALLUVIAL

END GRADE  
BEGIN ASPHALT OVERLAY  
-L- POC Sta. 66+00.00

ROADWAY EMBANKMENT

COASTAL PLAIN  
(DUPLIN FORMATION)

ROADWAY EMBANKMENT

ALLUVIAL

COASTAL PLAIN  
(DUPLIN FORMATION)

WILLIAM H. STEPHENS

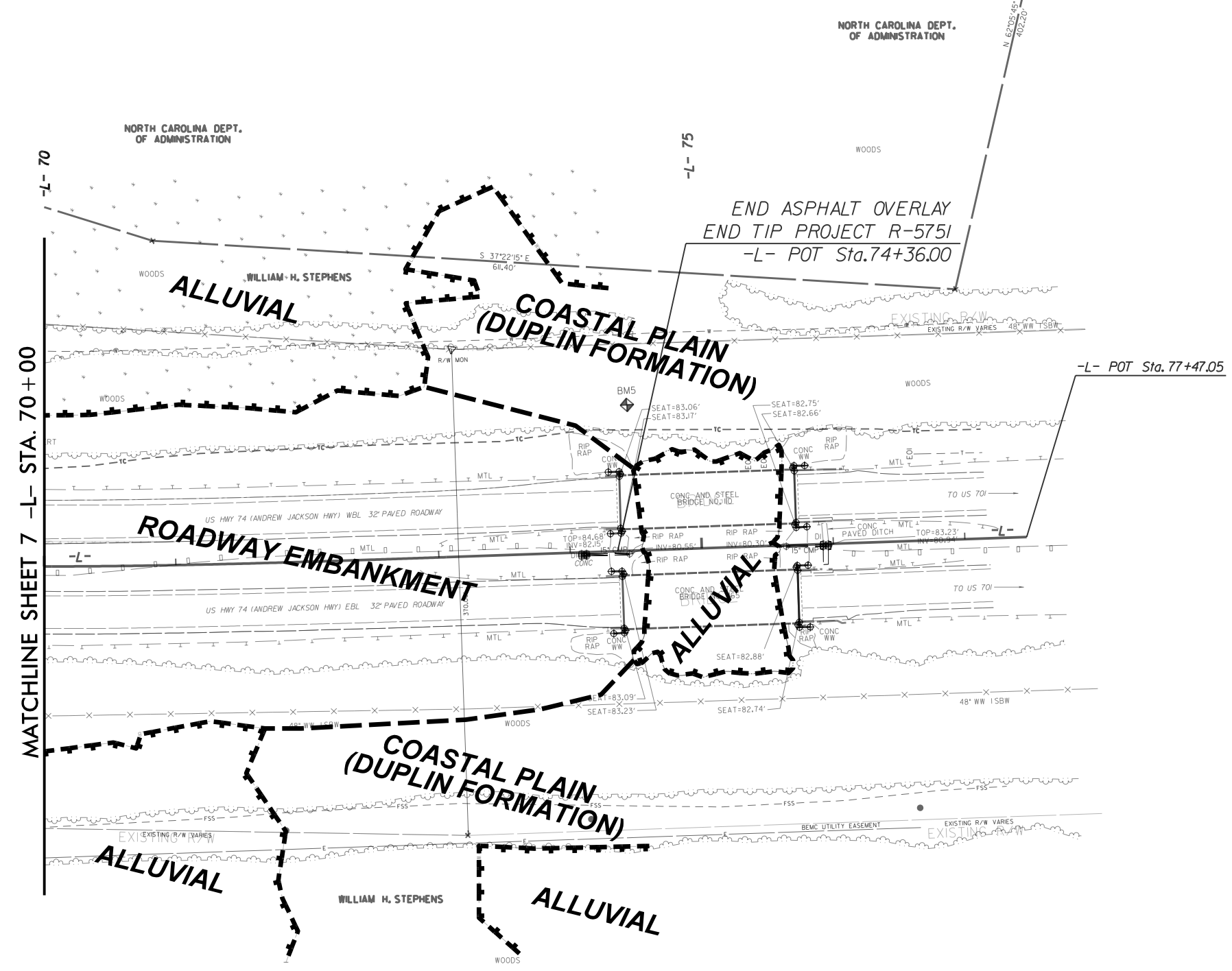
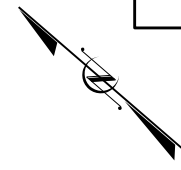
WILLIAM H. STEPHENS

WILLIAM H. STEPHENS

WILLIAM H. STEPHENS

WILLIAM E. STEPHENS

CULTIVATED



SUZANNE STEPHENS FAIR

WILLIAM H. STEPHENS

JULIA F. SMITH  
ANNE F. RICH

JULIA F. SMITH  
ANNE F. RICH

ALLUVIAL

-YIA- POT Sta. 10+00.00

BEGIN CONSTRUCTION  
-YIA- POC Sta. 16+00.00

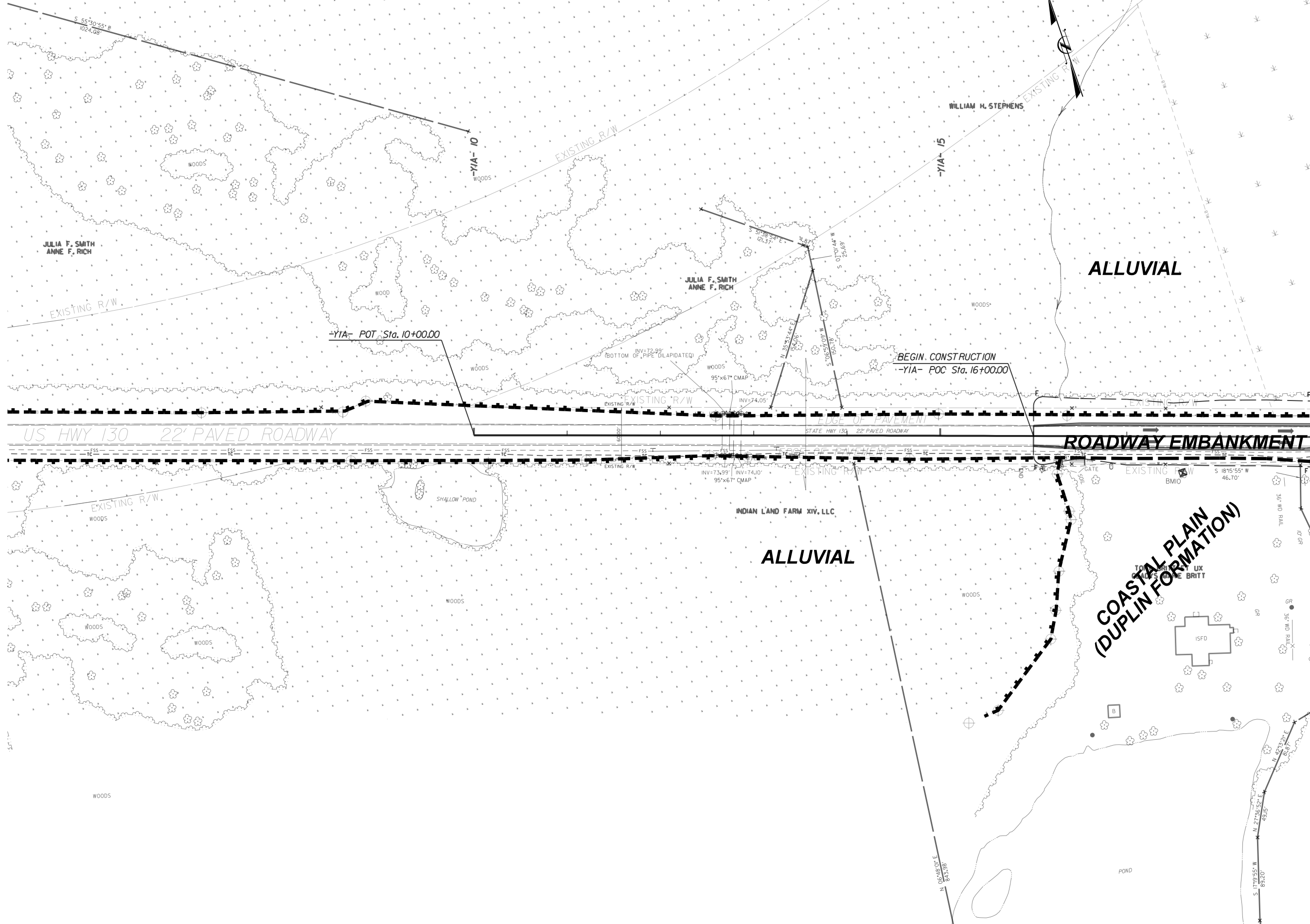
US HWY 130 22' PAVED ROADWAY

ROADWAY EMBANKMENT

INDIAN LAND FARM XIV, LLC

ALLUVIAL

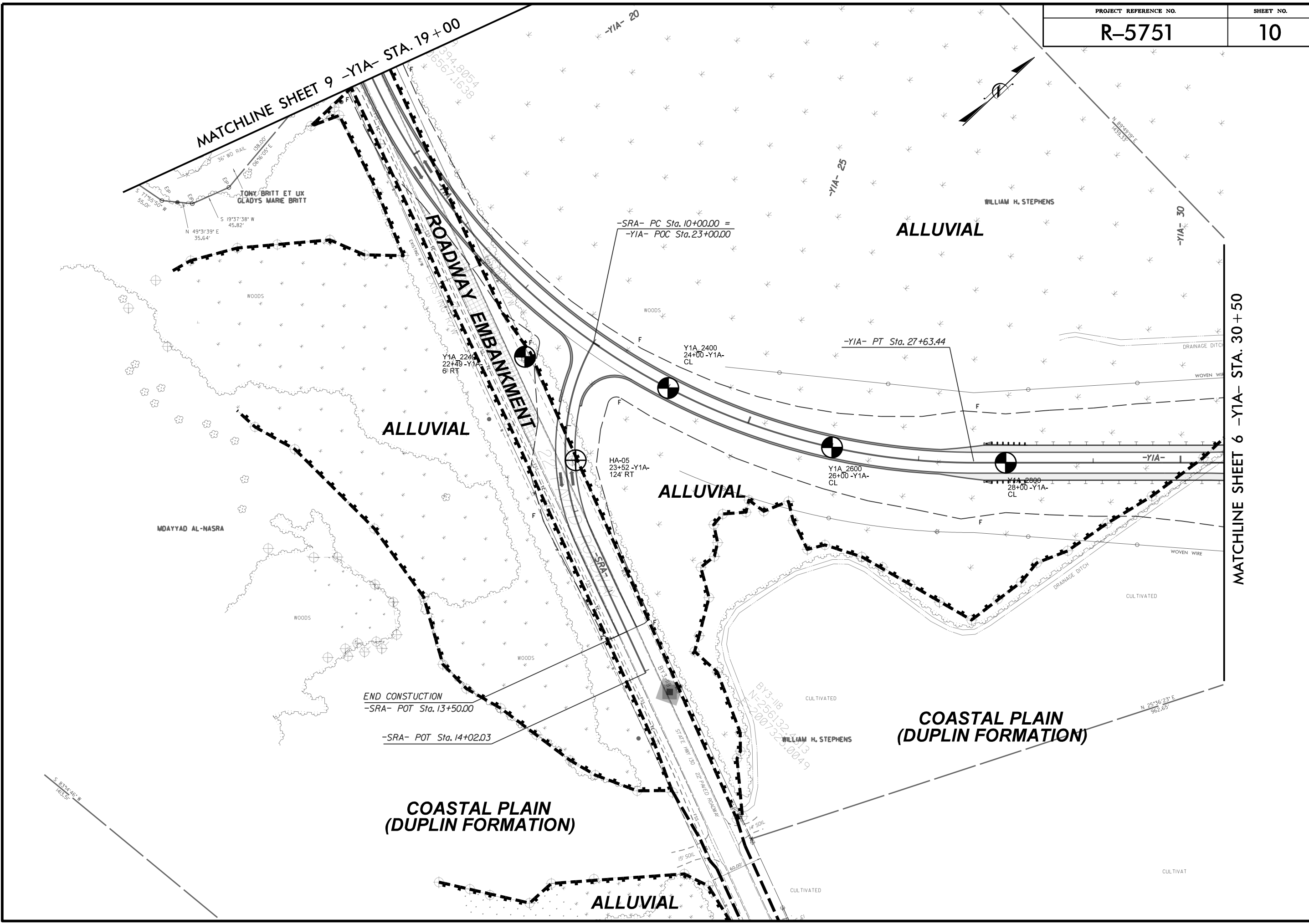
COASTAL PLAIN  
(DUPLIN FORMATION)



MATCHLINE SHEET 10 -YIA- STA. 19+00

MATCHLINE SHEET 9 -Y1A- STA. 19+00

MATCHLINE SHEET 6 -Y1A- STA. 30+50



END CONSTRUCTION  
-SRA- POT Sta. 13+50.00

-SRA- POT Sta. 14+02.03

-SRA- PC Sta. 10+00.00 =  
-Y1A- POC Sta. 23+00.00

-Y1A- PT Sta. 27+63.44

HA-05  
23+52 -Y1A-  
124' RT

Y1A 2400  
24+00 -Y1A-  
CL

Y1A 2600  
26+00 -Y1A-  
CL

Y1A 2800  
28+00 -Y1A-  
CL

COASTAL PLAIN  
(DUPLIN FORMATION)

COASTAL PLAIN  
(DUPLIN FORMATION)

ALLUVIAL

ALLUVIAL

ALLUVIAL

ALLUVIAL

WOODS

WOODS

WOODS

WOODS

CULTIVATED

WILLIAM H. STEPHENS

CULTIVATED

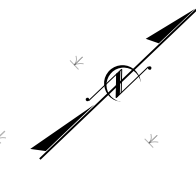
CULTIVATED

CULTIVATED

S 83°46' W  
103.51'

N 25°36' 23" E  
962.65'

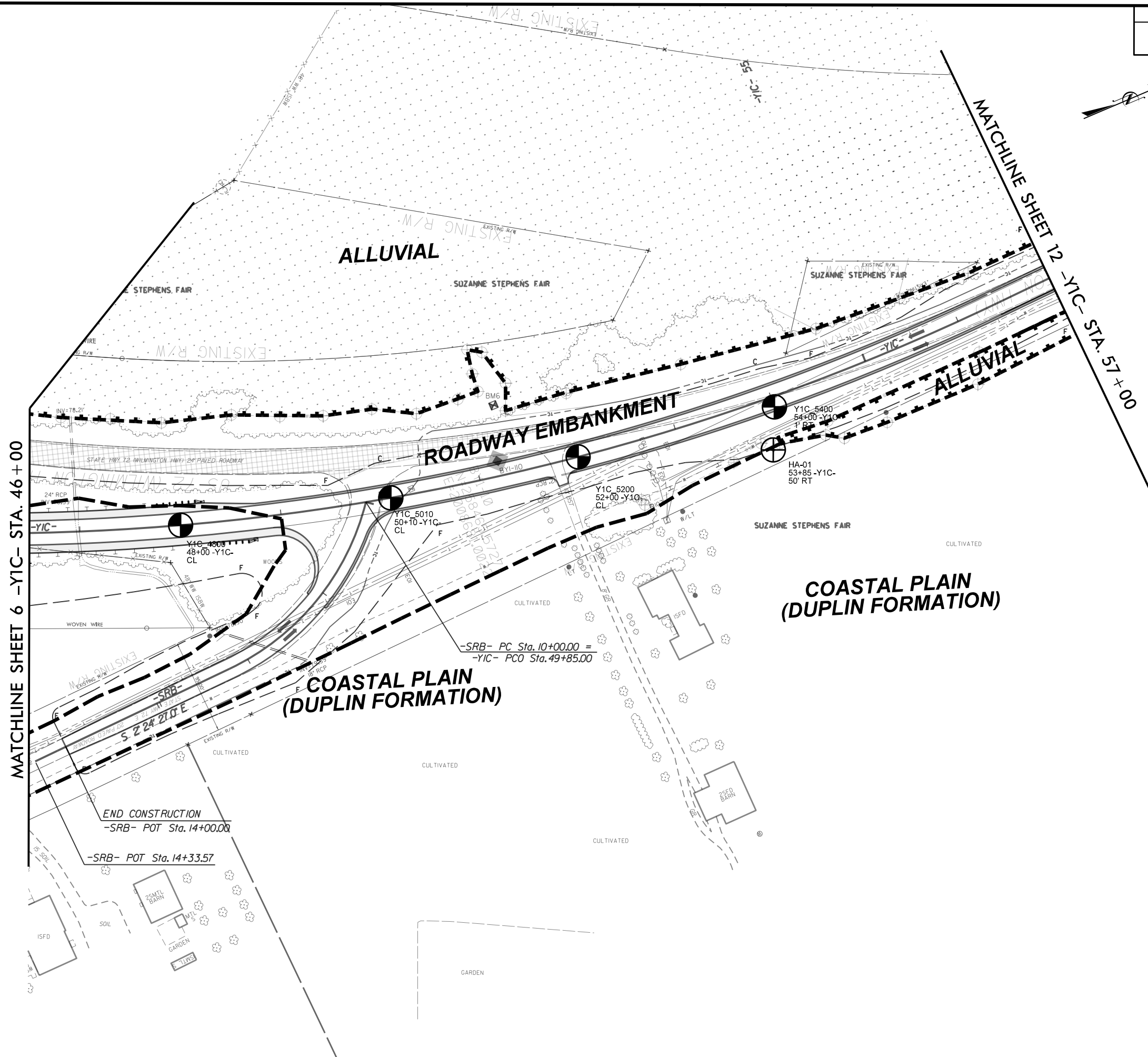
BY3-118  
N-2559132-4113  
20073210049





MATCHLINE SHEET 6 -Y1C- STA. 46+00

MATCHLINE SHEET 12 -Y1C- STA. 57+00



ALLUVIAL

STEPHENS FAIR

SUZANNE STEPHENS FAIR

SUZANNE STEPHENS FAIR

ROADWAY EMBANKMENT

ALLUVIAL

COASTAL PLAIN (DUPLIN FORMATION)

COASTAL PLAIN (DUPLIN FORMATION)

-SRB- PC Sta. 10+00.00 = -Y1C- PCO Sta. 49+85.00

END CONSTRUCTION -SRB- POT Sta. 14+00.00

-SRB- POT Sta. 14+33.57

ISFD

SMITH BARN

GARDEN

GARDEN

HA-01 53+85 -Y1C- 50' RT

Y1C 5200 52+00 -Y1C- CL

Y1C 5010 50+10 -Y1C- CL

Y1C 4800 48+00 -Y1C- CL

-Y1C-

24' RCP

STATE HWY. 72 (WILMINGTON HWY) 24' PAVED ROADWAY

INV. 78.2'

WIRE

EXISTING R/W

EXISTING R/W

EXISTING R/W

EXISTING R/W

EXISTING R/W

EXISTING R/W

EXISTING R/W

EXISTING R/W

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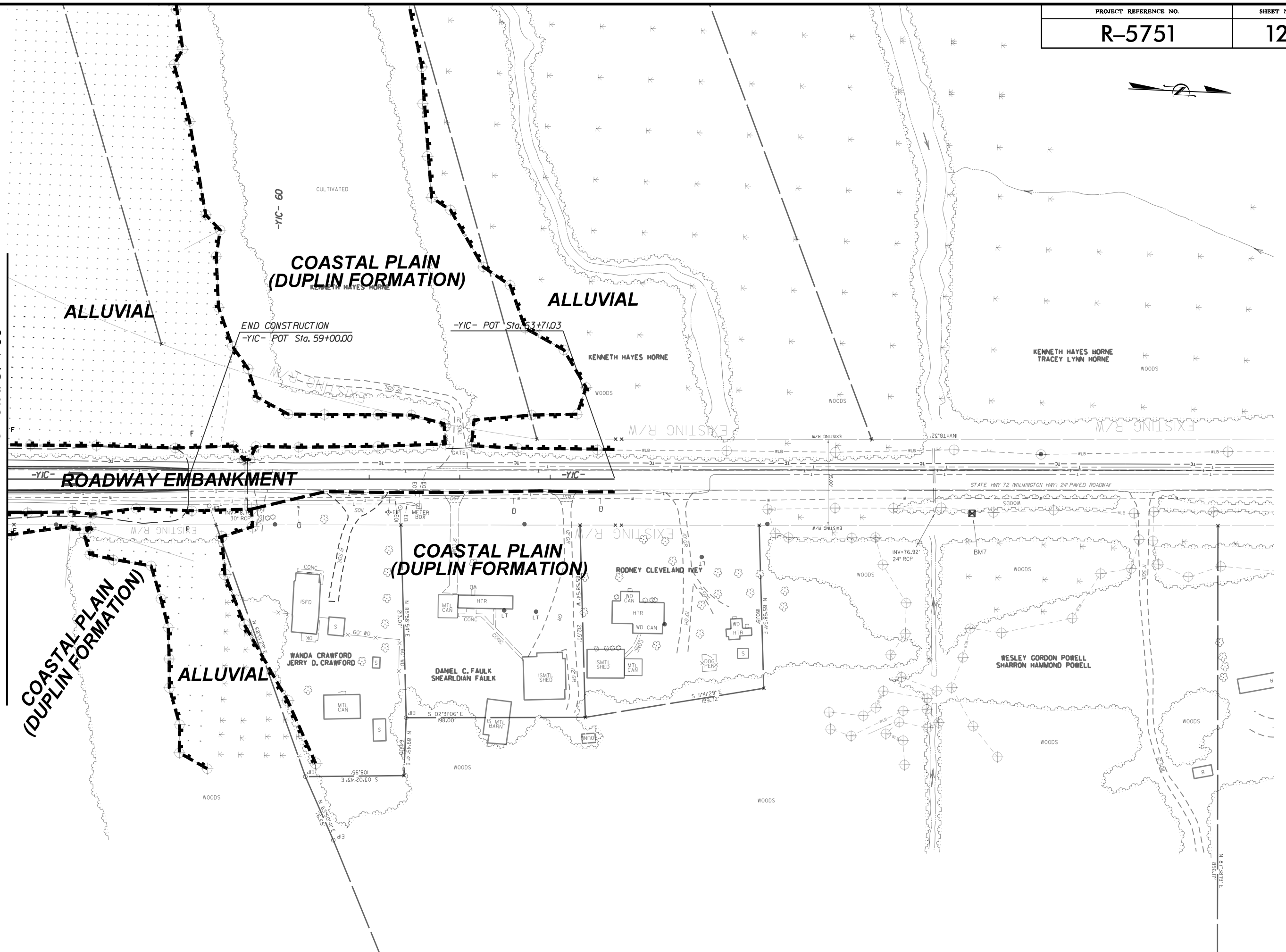
EXISTING R/W

EXISTING R/W

EXISTING R/W



MATCHLINE SHEET 11 -YIC- STA. 57+00



**COASTAL PLAIN  
(DUPLIN FORMATION)**

**ALLUVIAL**

**ALLUVIAL**

END CONSTRUCTION  
-YIC- POT Sta. 59+00.00

-YIC- POT Sta. 63+71.03

**ROADWAY EMBANKMENT**

**COASTAL PLAIN  
(DUPLIN FORMATION)**

**ALLUVIAL**

**COASTAL PLAIN  
(DUPLIN FORMATION)**

WANDA CRAWFORD  
JERRY D. CRAWFORD

DANIEL C. FAULK  
SHEARLIAN FAULK

ROONEY CLEVELAND IVEY

WESLEY GORDON POWELL  
SHARRON HAMMOND POWELL

WOODS

WOODS

WOODS

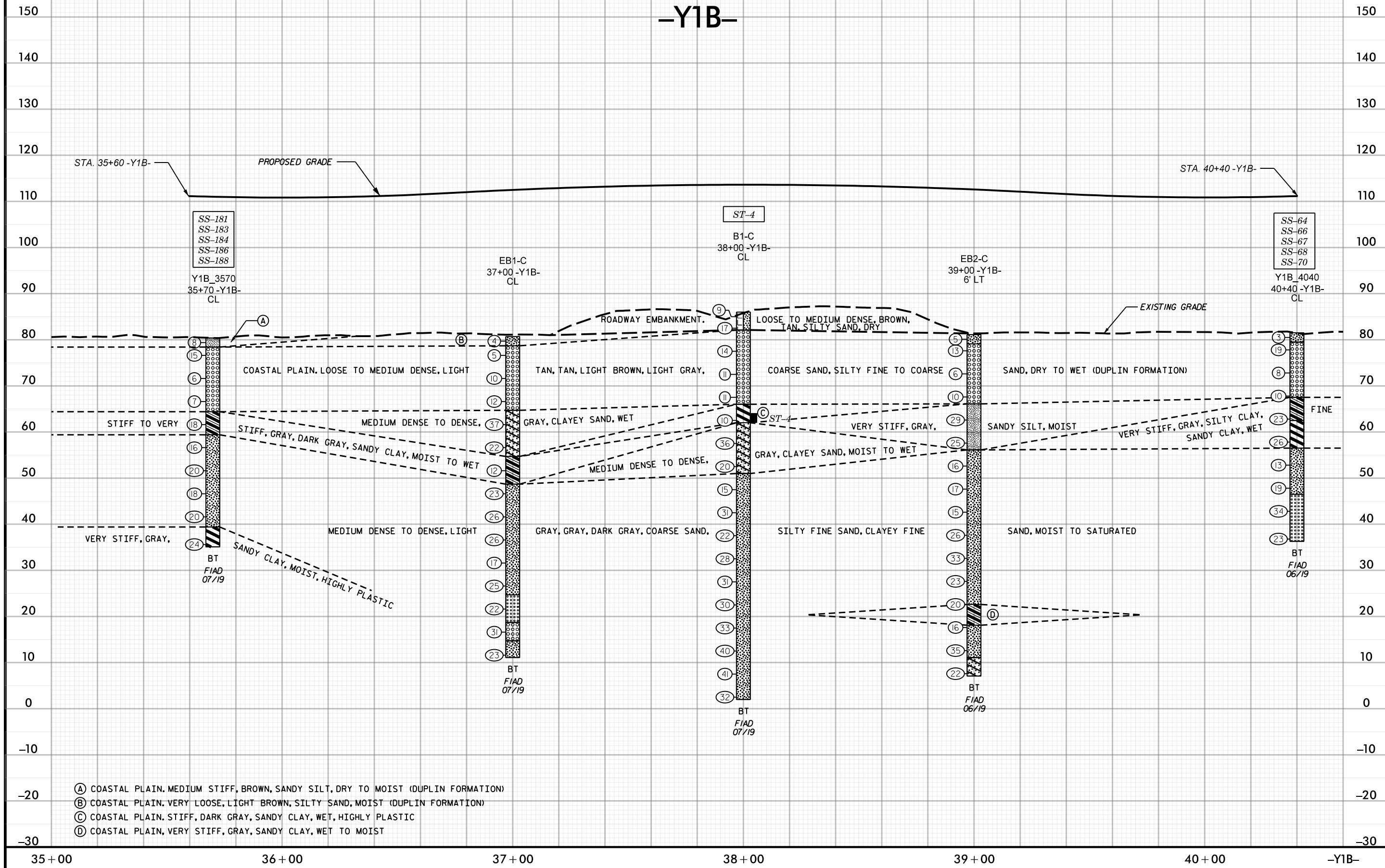
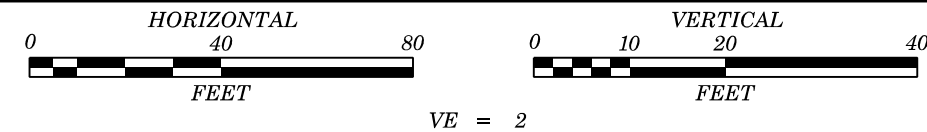
WOODS

WOODS

WOODS

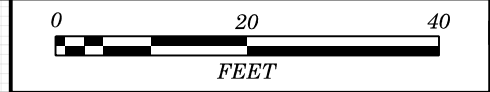
WOODS

N 87°39'07" E  
856.17'

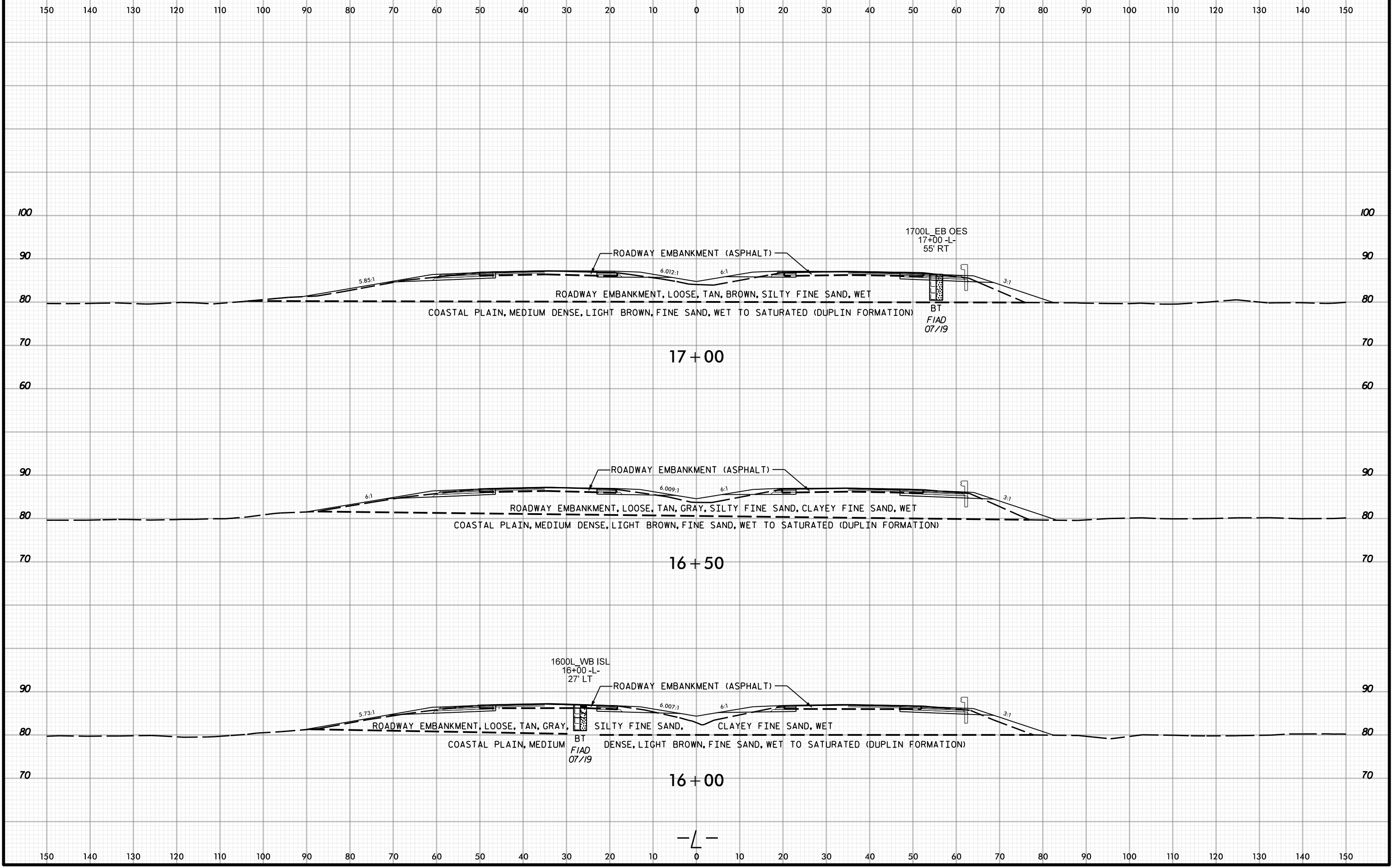


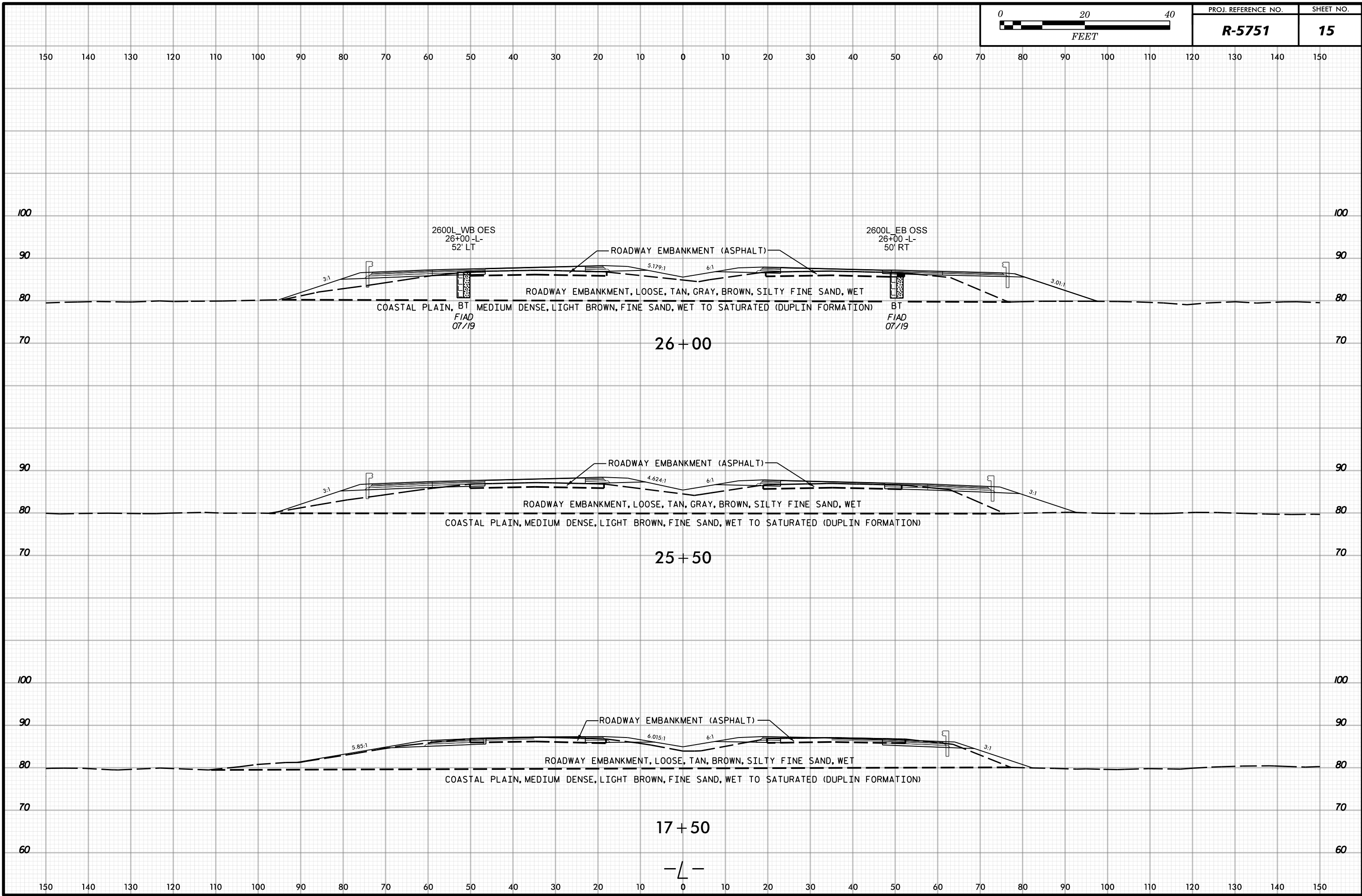
- (A) COASTAL PLAIN. MEDIUM STIFF, BROWN, SANDY SILT, DRY TO MOIST (DUPLIN FORMATION)
- (B) COASTAL PLAIN. VERY LOOSE, LIGHT BROWN, SILTY SAND, MOIST (DUPLIN FORMATION)
- (C) COASTAL PLAIN. STIFF, DARK GRAY, SANDY CLAY, WET, HIGHLY PLASTIC
- (D) COASTAL PLAIN, VERY STIFF, GRAY, SANDY CLAY, WET TO MOIST

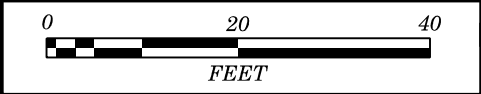




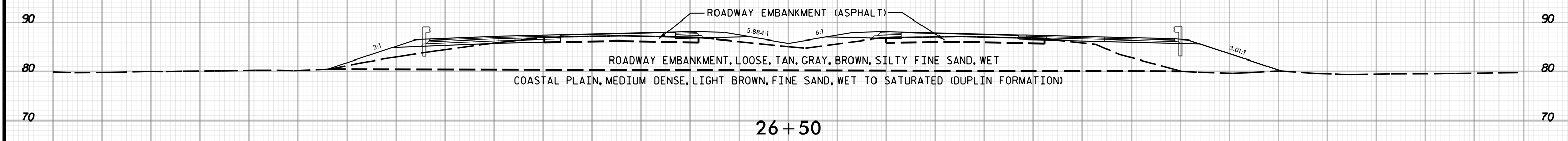
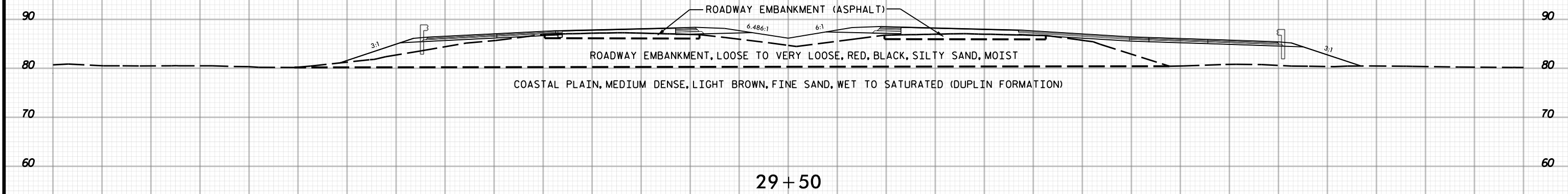
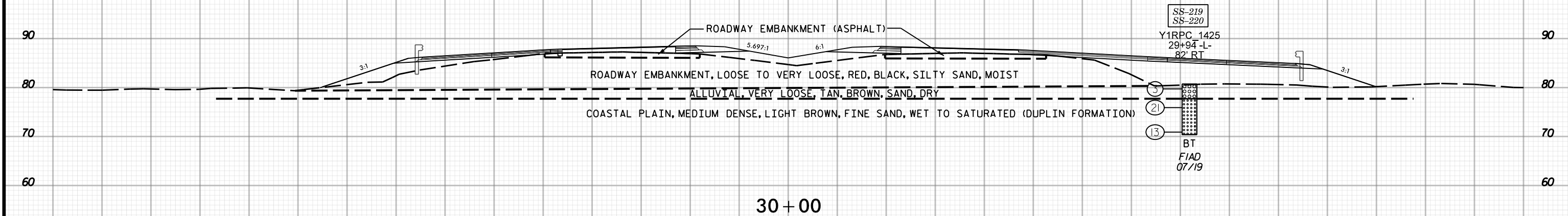
PROJ. REFERENCE NO.	SHEET NO.
<b>R-5751</b>	<b>14</b>



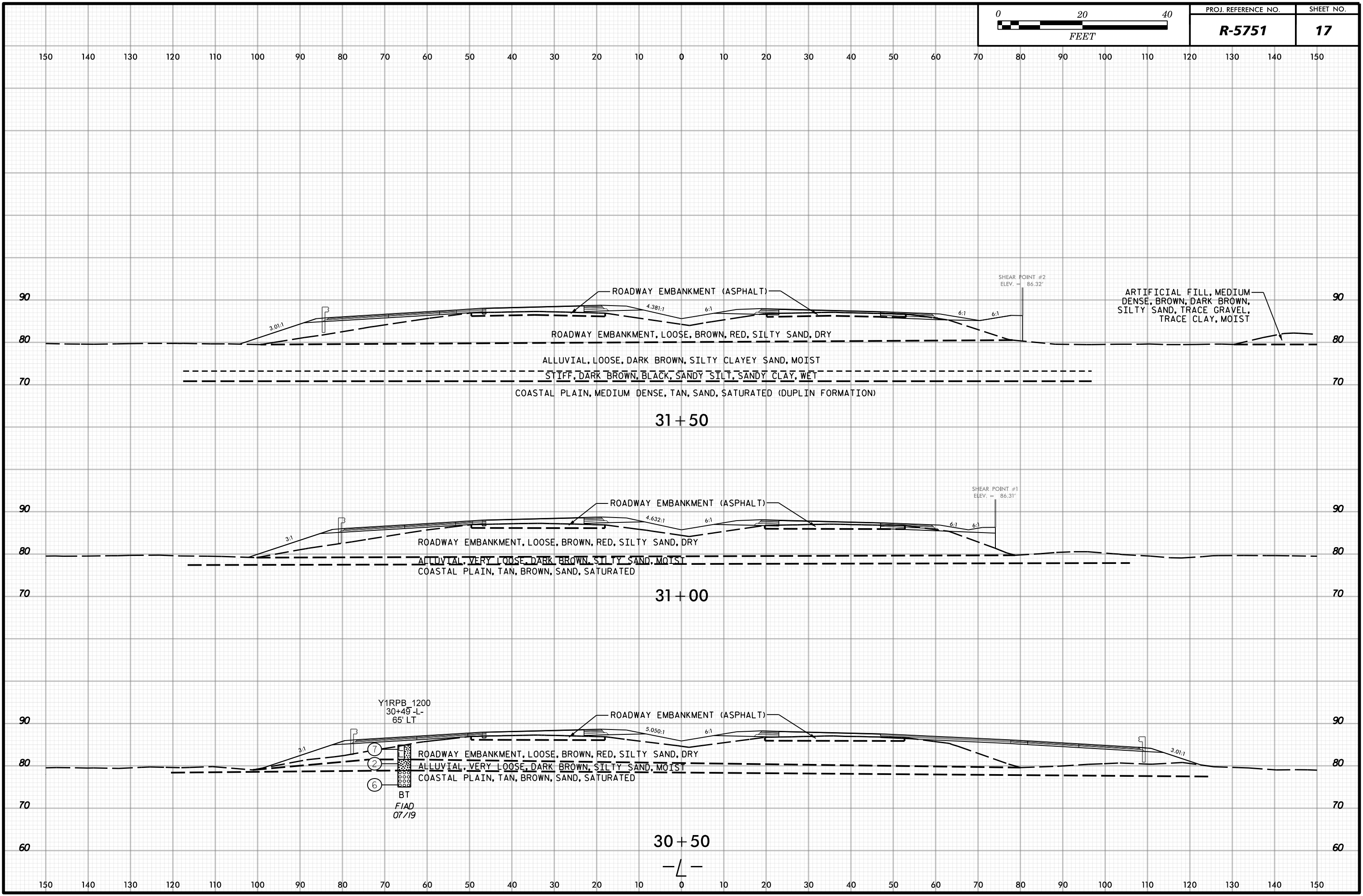
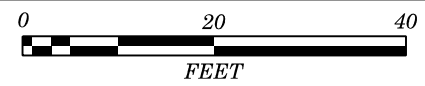




150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



31 + 50

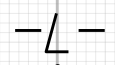
31 + 00

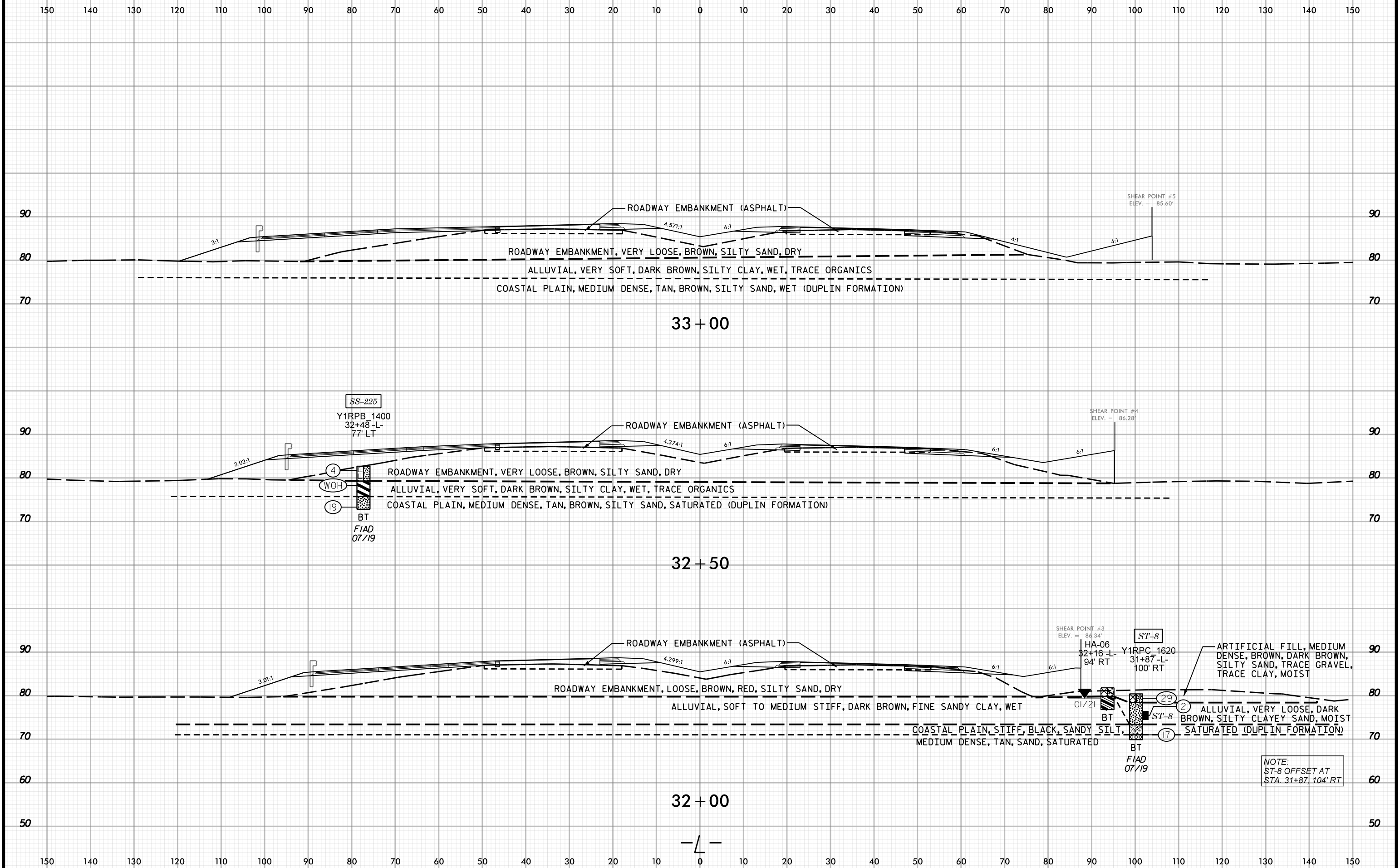
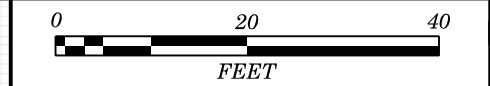
30 + 50

Y1RPB 1200  
30+49-L-  
65' LT

⑦  
②  
⑥

BT  
FIAD  
07/19





SS-225  
Y1RPB 1400  
32+48-L-  
77' LT

4  
WOH  
19

BT  
FIAD  
07/19

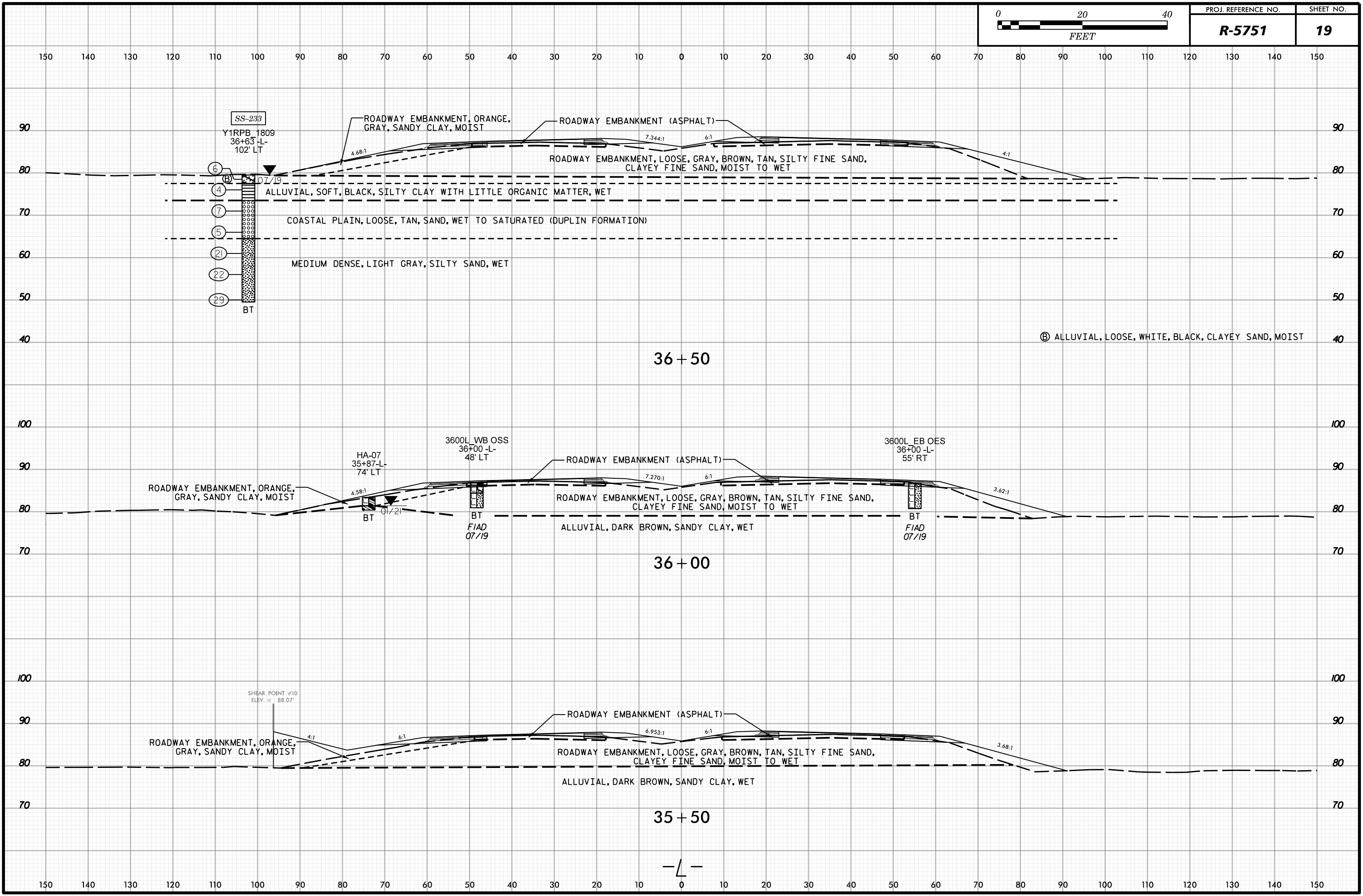
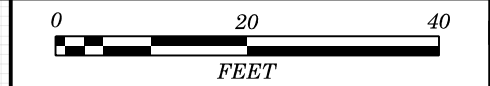
SHEAR POINT #3  
ELEV. = 86.34'

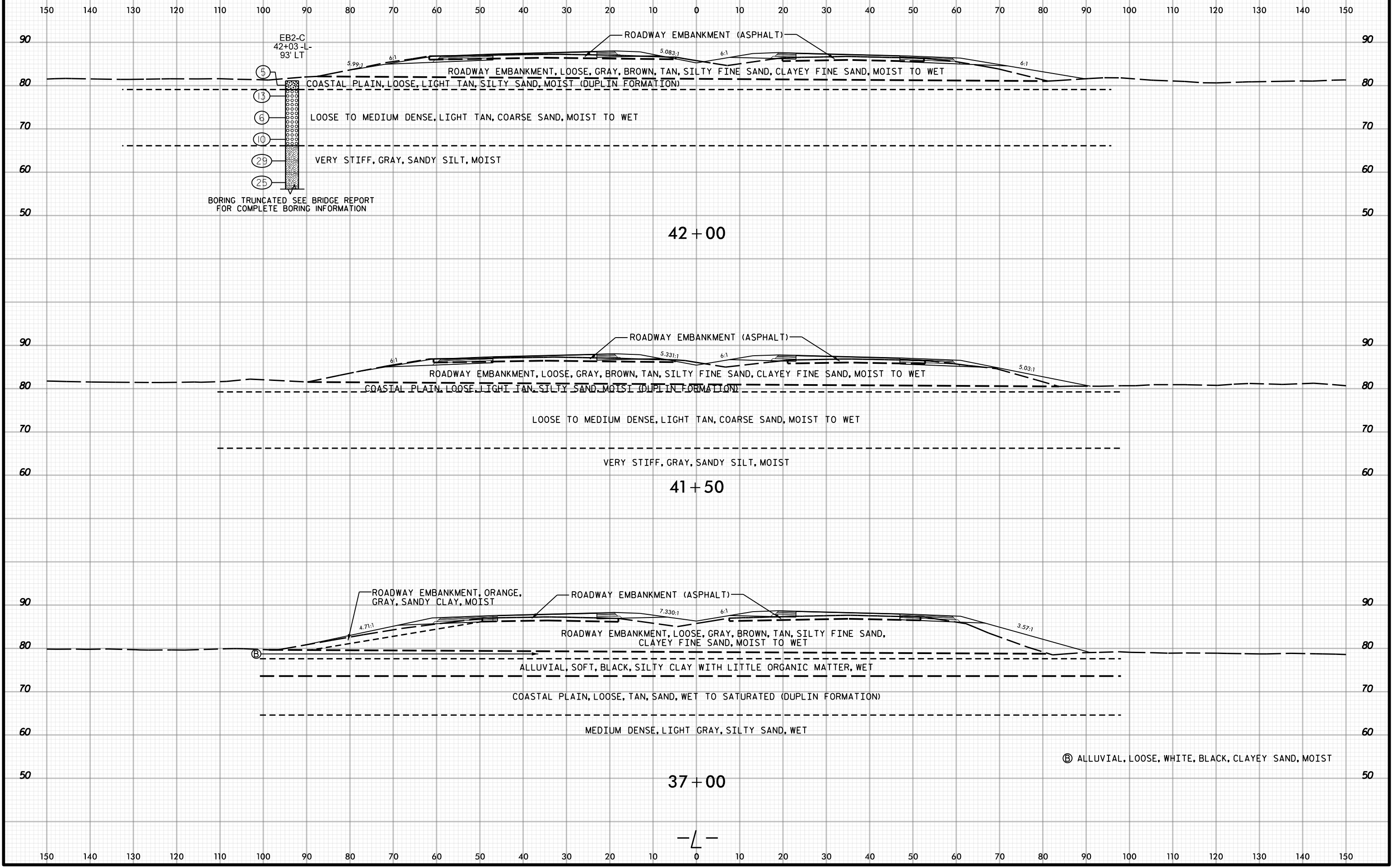
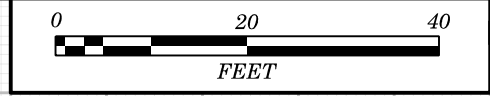
HA-06  
32+16-L-  
94' RT

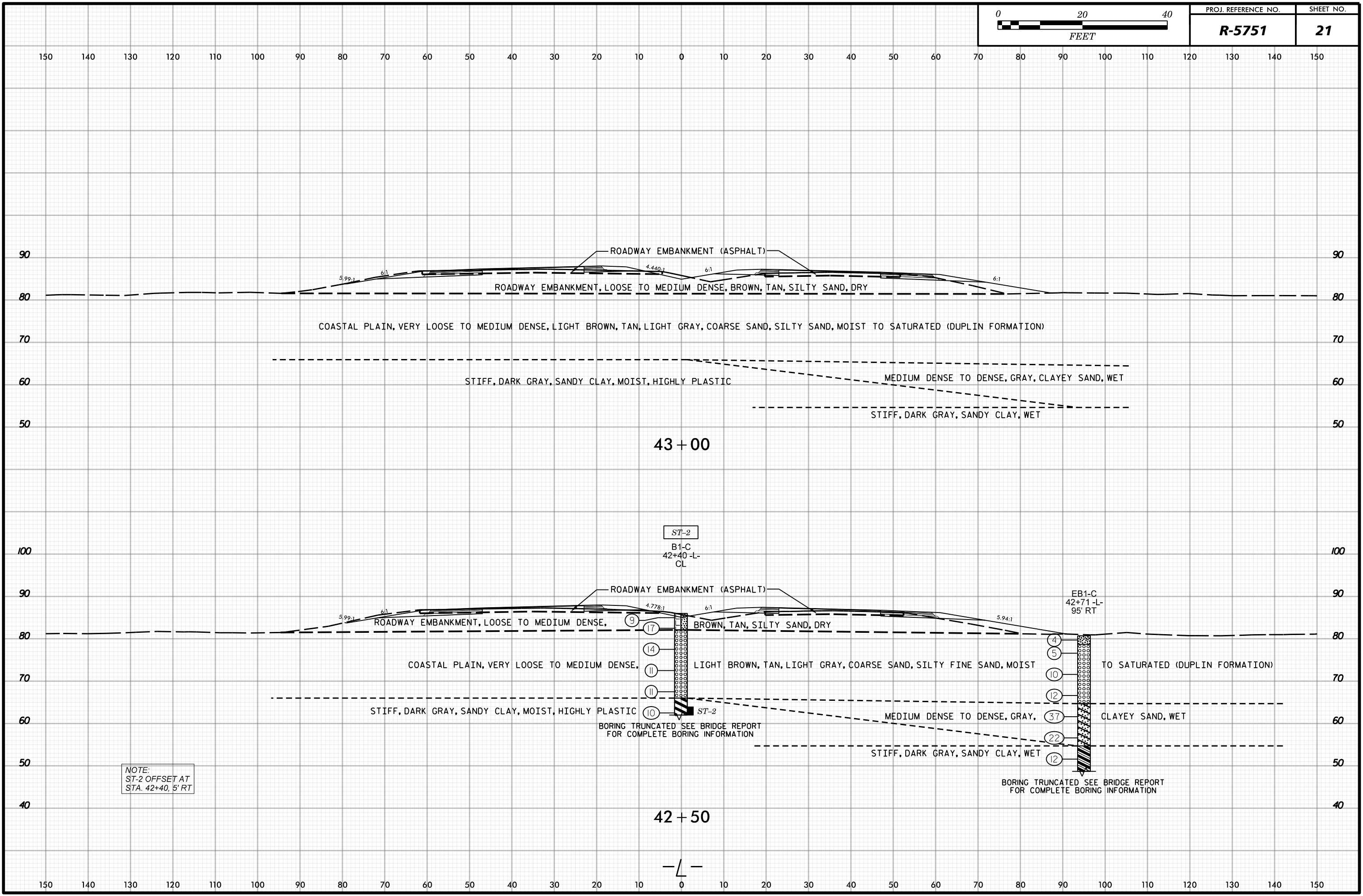
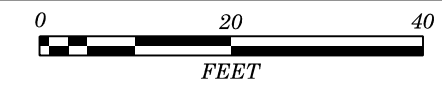
ST-8  
Y1RPC 1620  
31+87-L-  
100' RT

BT  
FIAD  
07/19

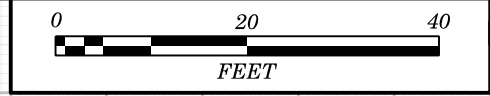
NOTE:  
ST-8 OFFSET AT  
STA. 31+87, 104' RT



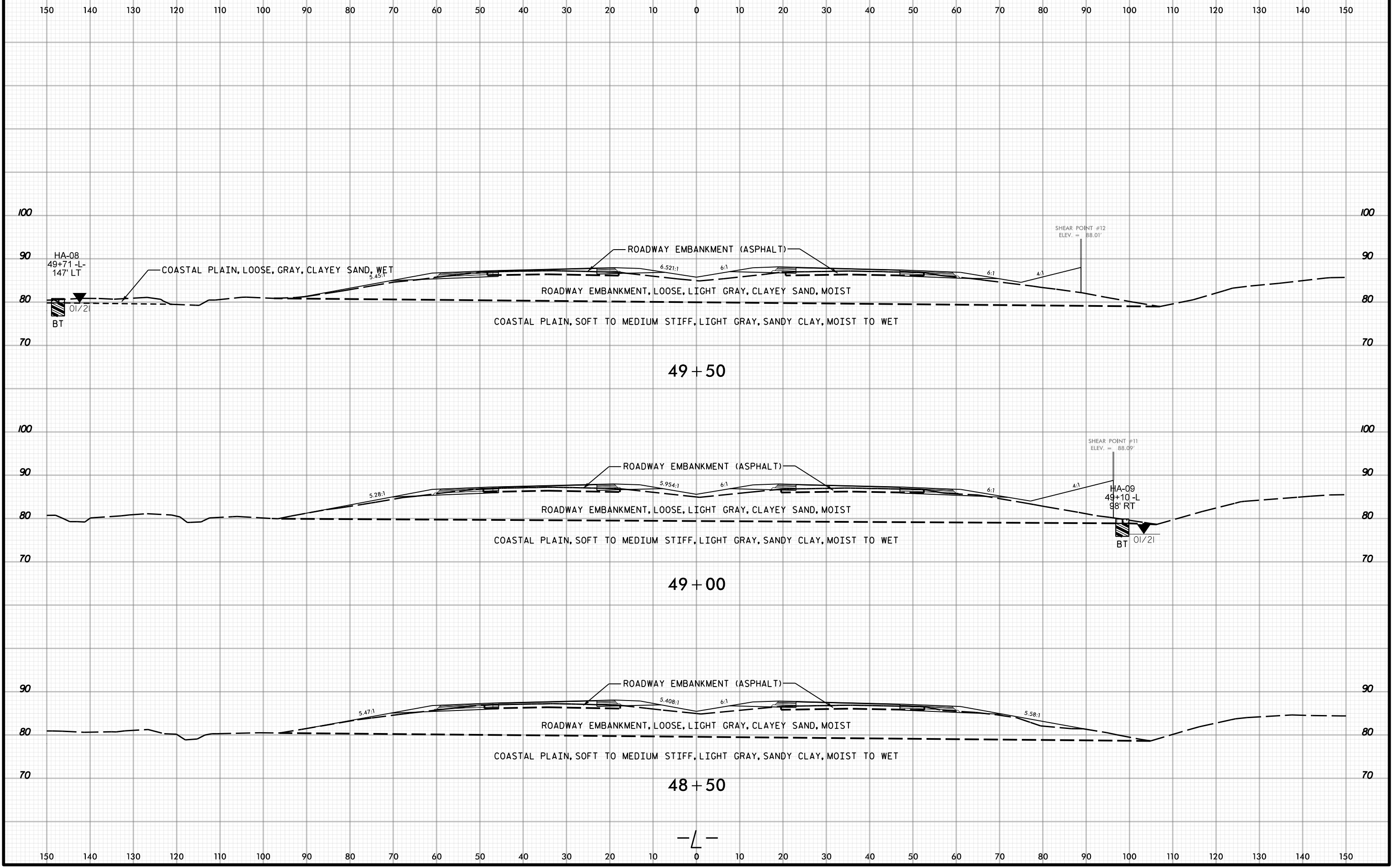








PROJ. REFERENCE NO.	SHEET NO.
<b>R-5751</b>	<b>22</b>



150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

100  
90  
80  
70

HA-08  
49+71 -L-  
147' LT

COASTAL PLAIN, LOOSE, GRAY, CLAYEY SAND, WET

ROADWAY EMBANKMENT (ASPHALT)

ROADWAY EMBANKMENT, LOOSE, LIGHT GRAY, CLAYEY SAND, MOIST

COASTAL PLAIN, SOFT TO MEDIUM STIFF, LIGHT GRAY, SANDY CLAY, MOIST TO WET

5.45:1 6.52:1 6:1 6:1 4:1

SHEAR POINT #12  
ELEV. = 88.01'

BT 01/21

49+50

100  
90  
80  
70

ROADWAY EMBANKMENT (ASPHALT)

ROADWAY EMBANKMENT, LOOSE, LIGHT GRAY, CLAYEY SAND, MOIST

COASTAL PLAIN, SOFT TO MEDIUM STIFF, LIGHT GRAY, SANDY CLAY, MOIST TO WET

5.28:1 5.954:1 6:1 6:1 4:1

SHEAR POINT #11  
ELEV. = 88.09'

HA-09  
49+10 -L-  
98' RT

BT 01/21

49+00

90  
80  
70

ROADWAY EMBANKMENT (ASPHALT)

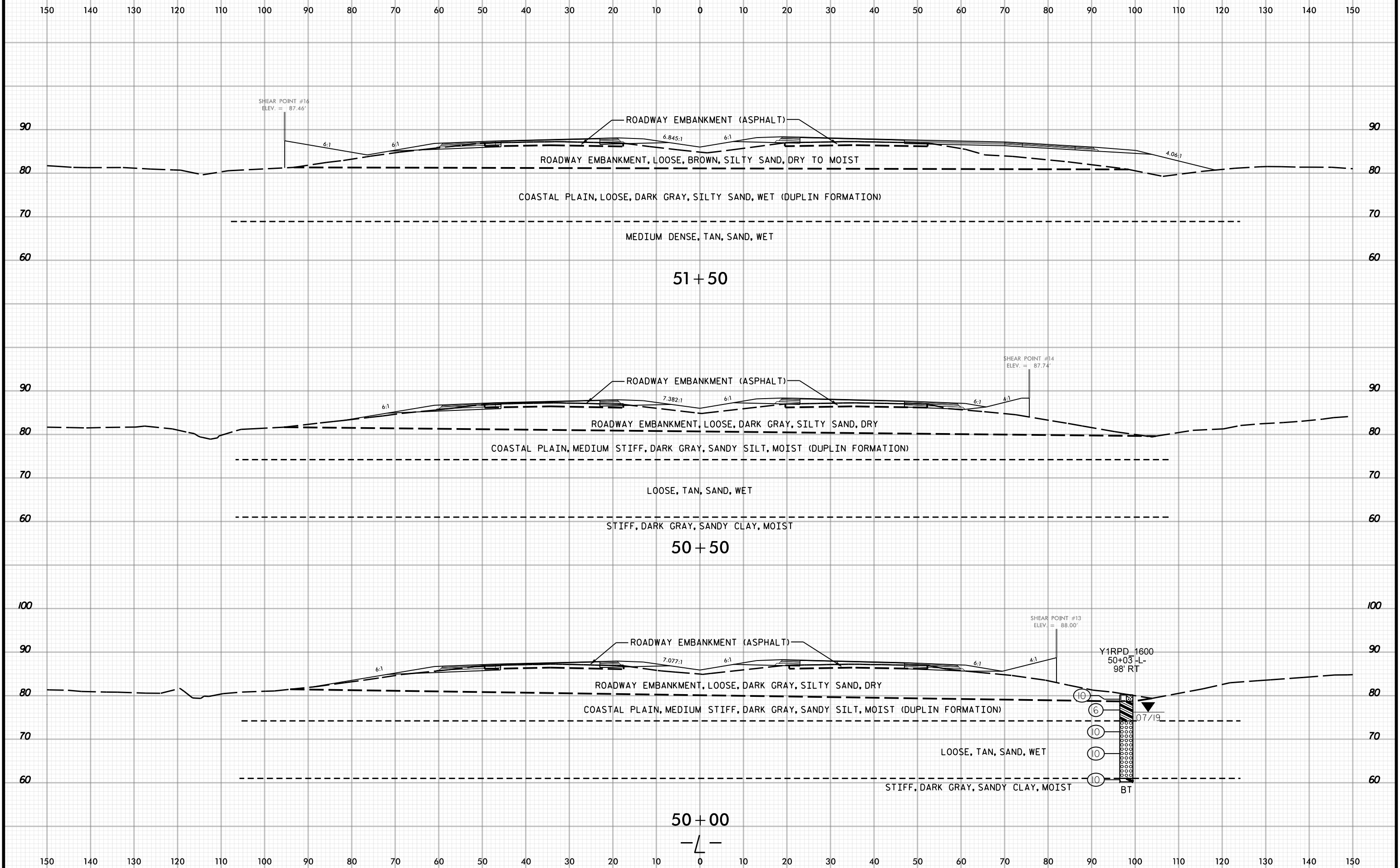
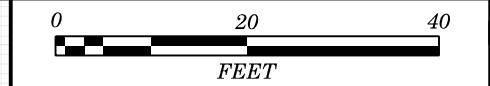
ROADWAY EMBANKMENT, LOOSE, LIGHT GRAY, CLAYEY SAND, MOIST

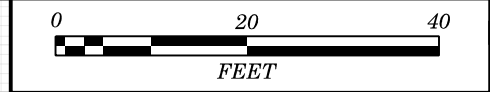
COASTAL PLAIN, SOFT TO MEDIUM STIFF, LIGHT GRAY, SANDY CLAY, MOIST TO WET

5.47:1 5.408:1 6:1 5.58:1

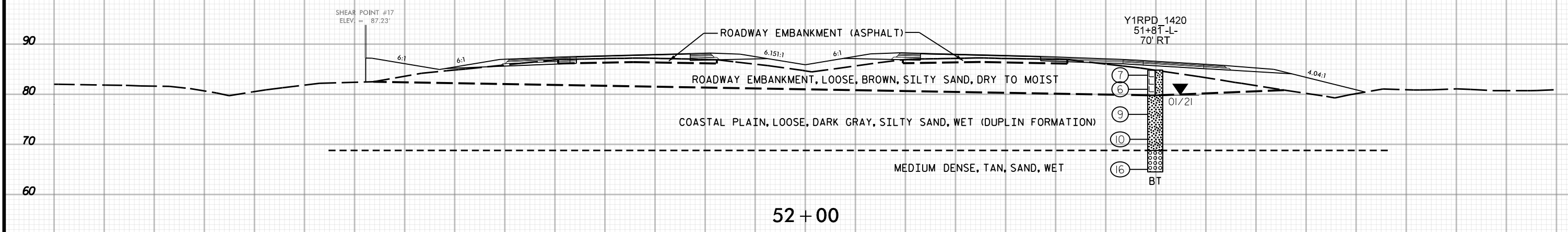
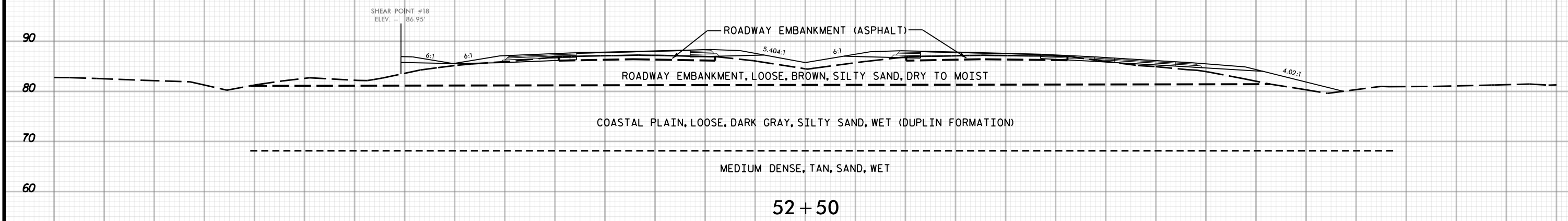
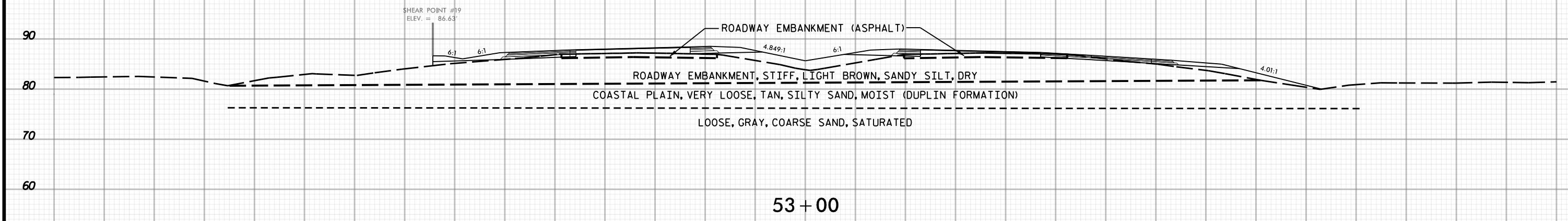
48+50

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

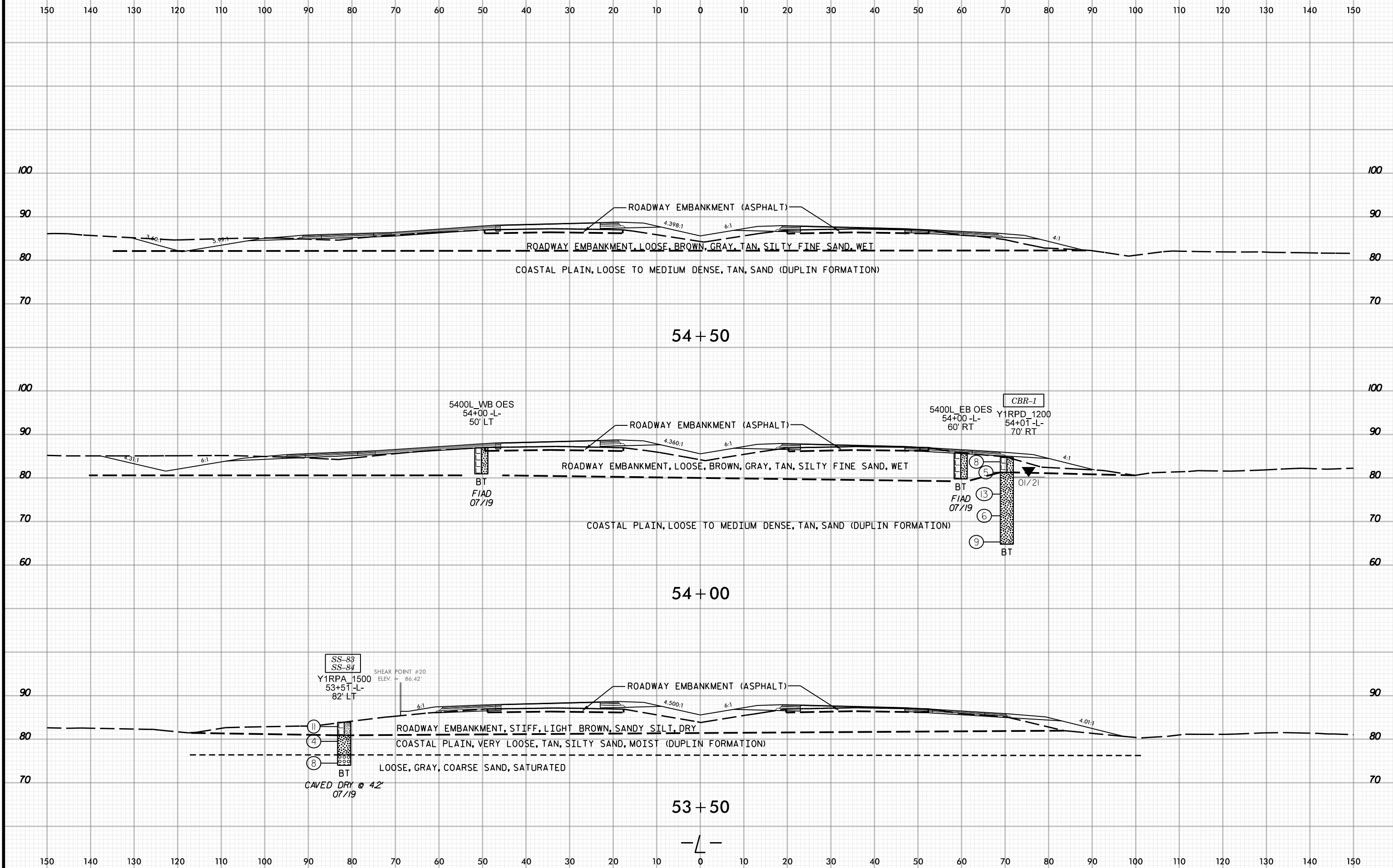
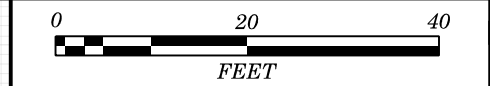




150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



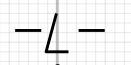
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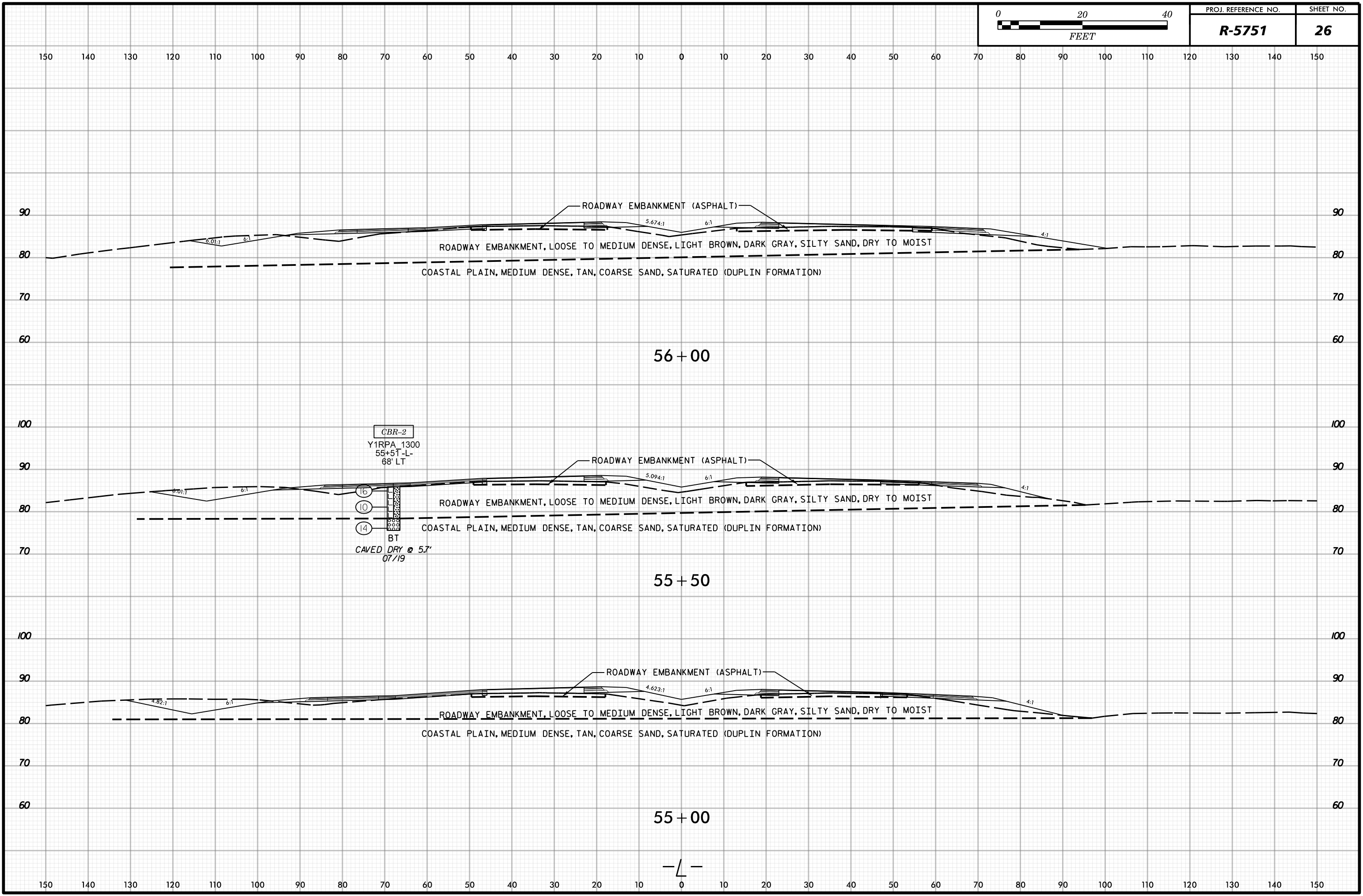
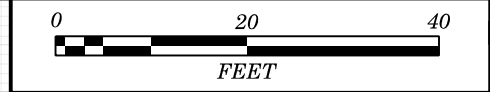


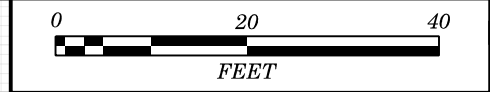
54 + 50

54 + 00

53 + 50

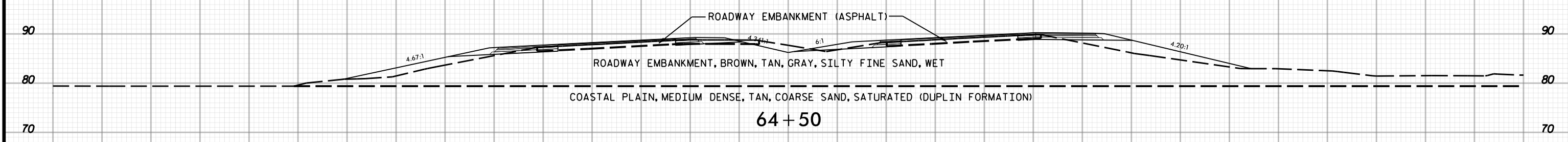
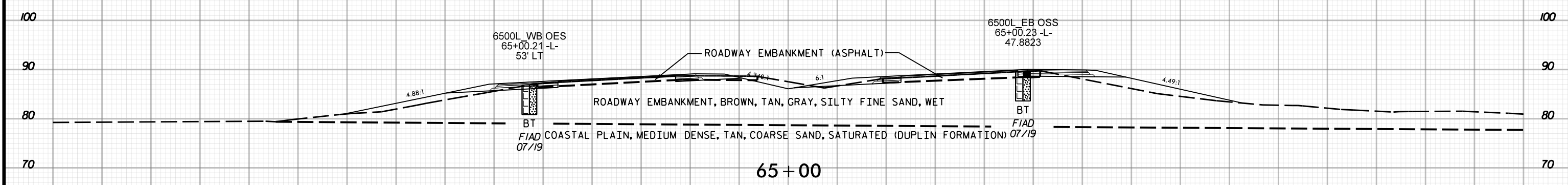
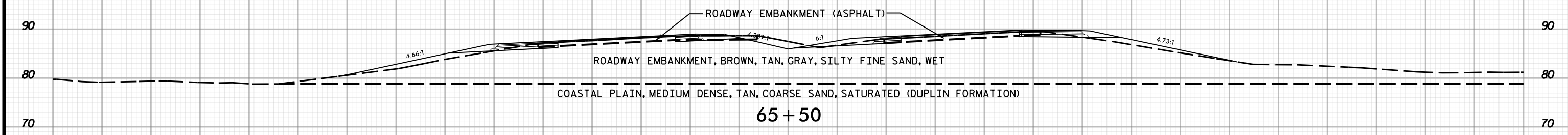




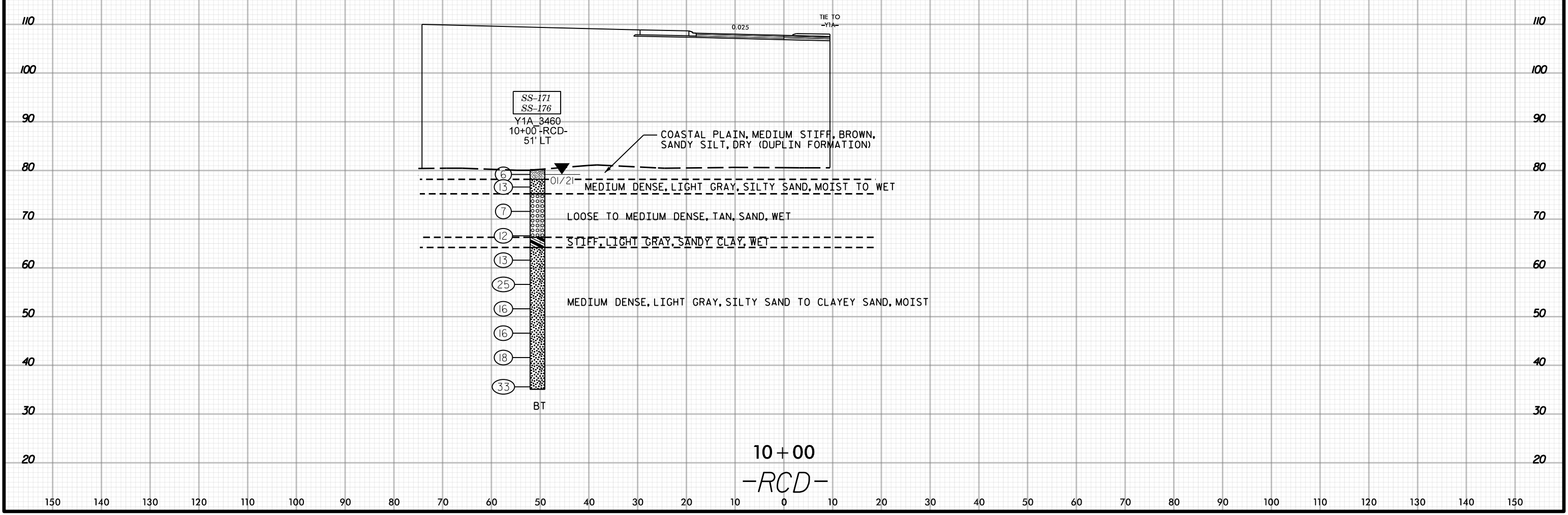
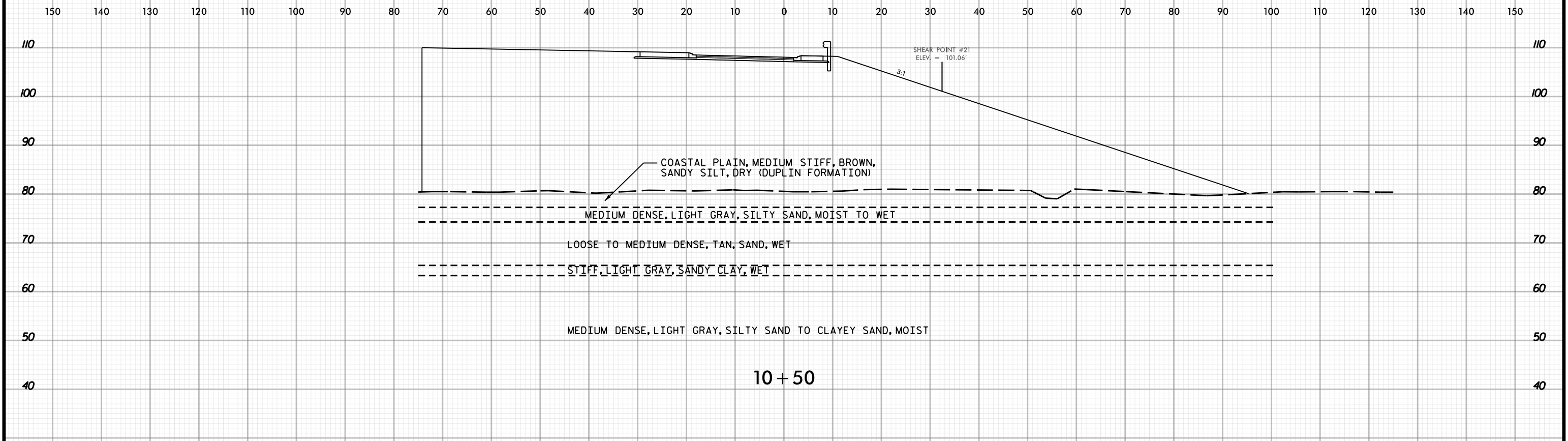
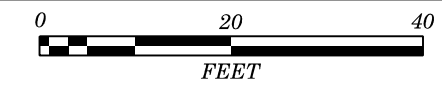


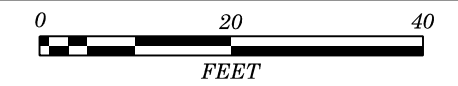
PROJ. REFERENCE NO.	SHEET NO.
R-5751	27

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

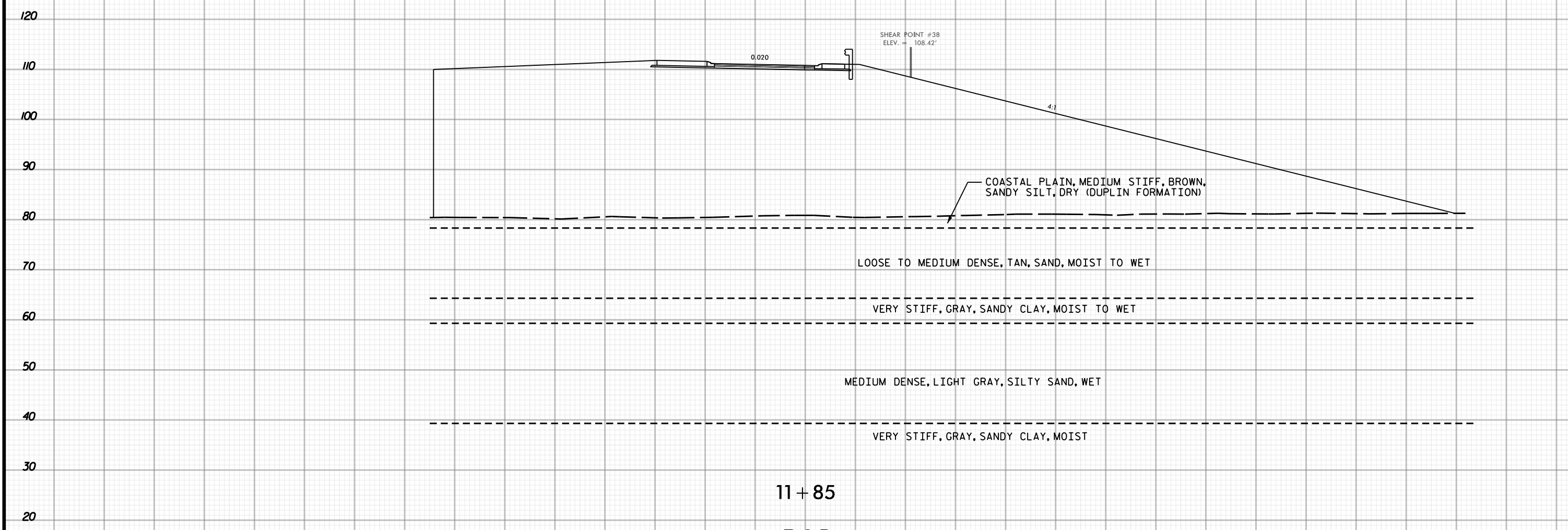


150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150





150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



SHEAR POINT #38  
ELEV. = 108.42'

0.020

4:1

COASTAL PLAIN, MEDIUM STIFF, BROWN,  
SANDY SILT, DRY (DUPLIN FORMATION)

LOOSE TO MEDIUM DENSE, TAN, SAND, MOIST TO WET

VERY STIFF, GRAY, SANDY CLAY, MOIST TO WET

MEDIUM DENSE, LIGHT GRAY, SILTY SAND, WET

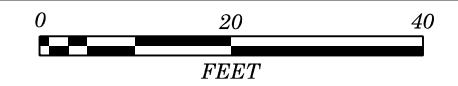
VERY STIFF, GRAY, SANDY CLAY, MOIST

11 + 85

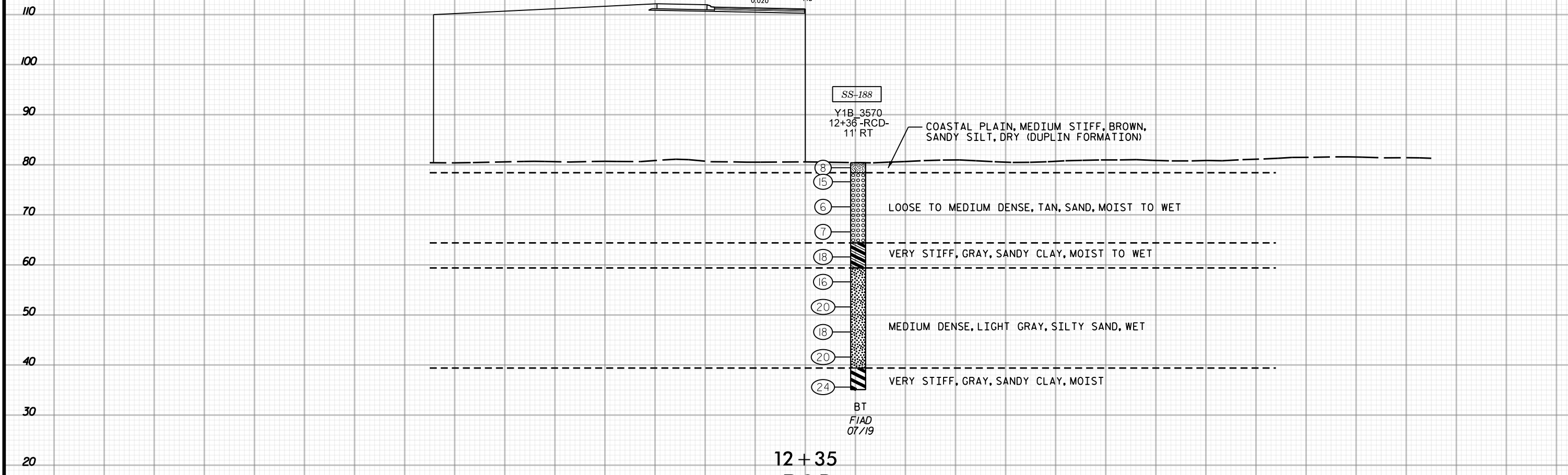
-RCD-

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



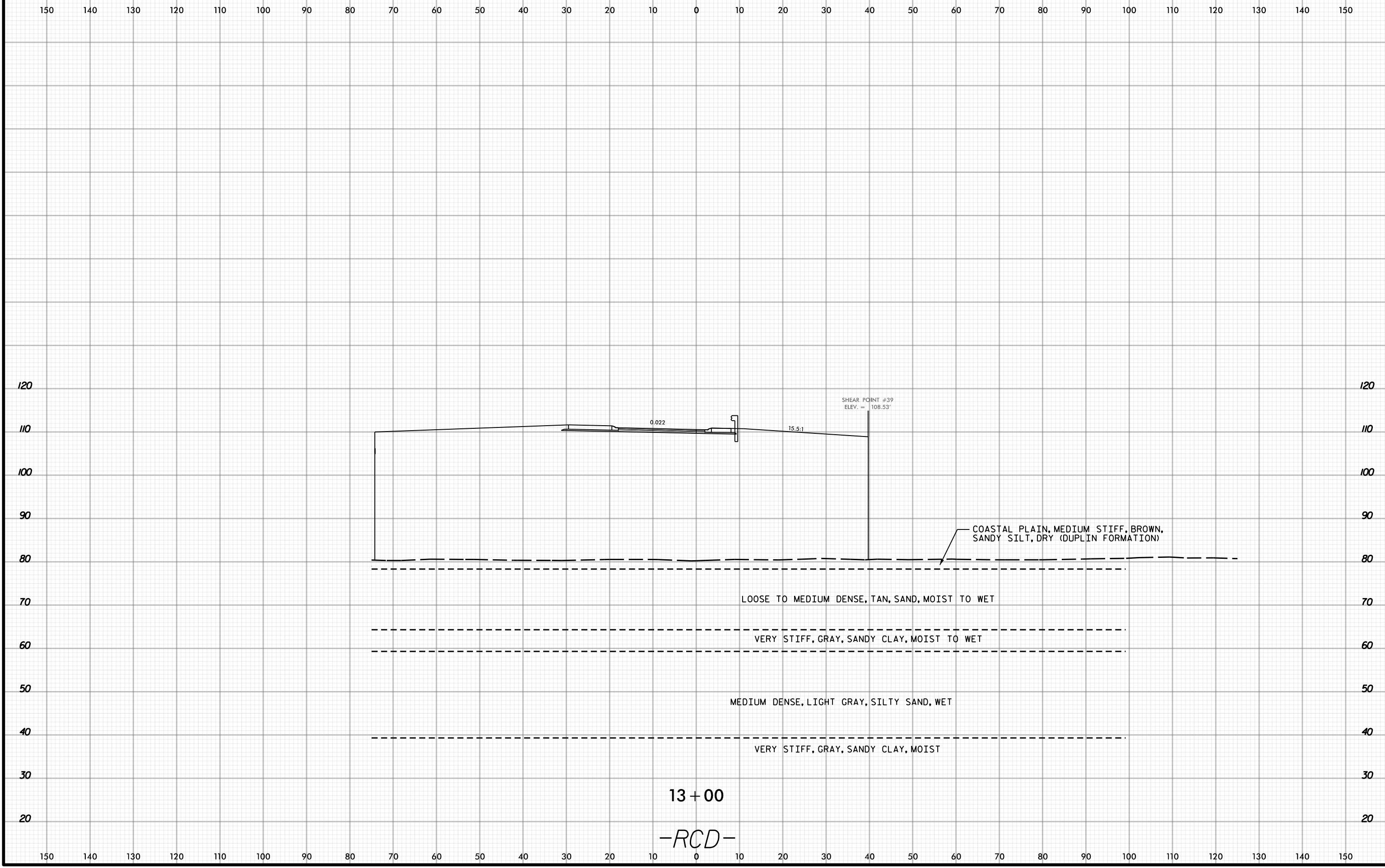
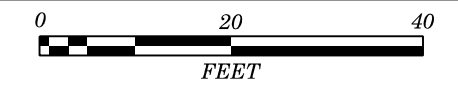


150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

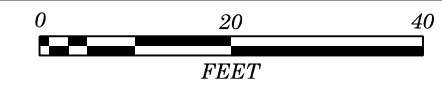


12 + 35  
-RCD-

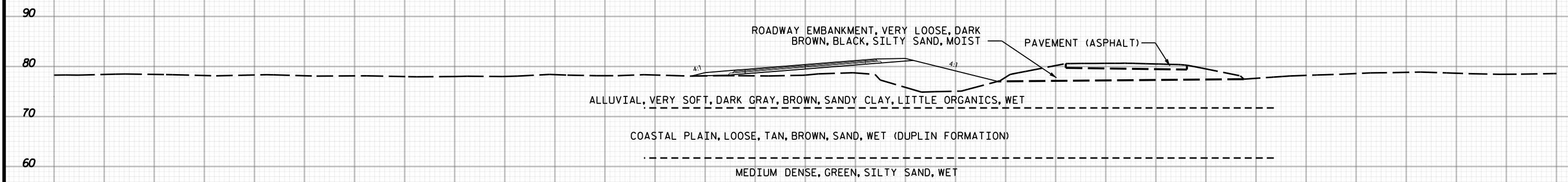
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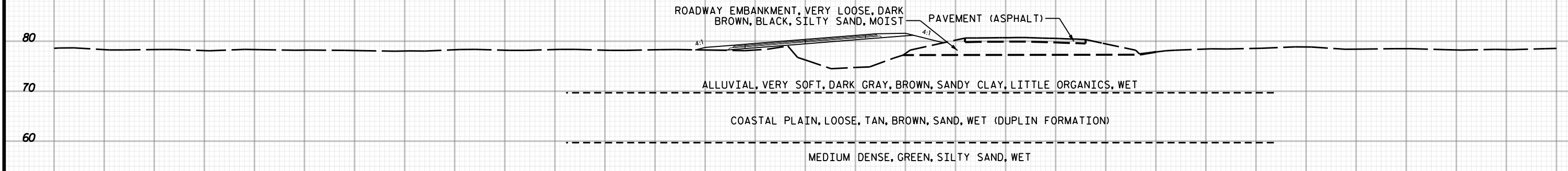
13+00  
-RCD-



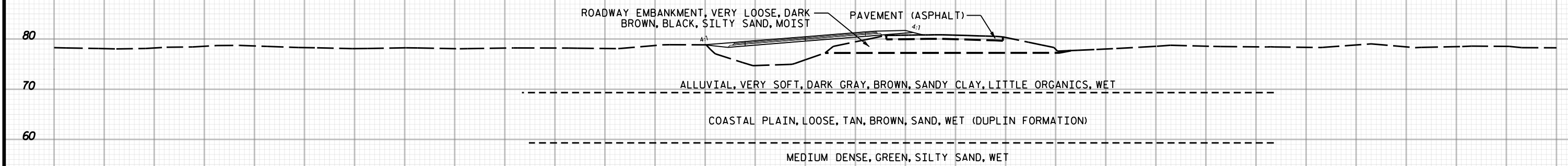
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22+00



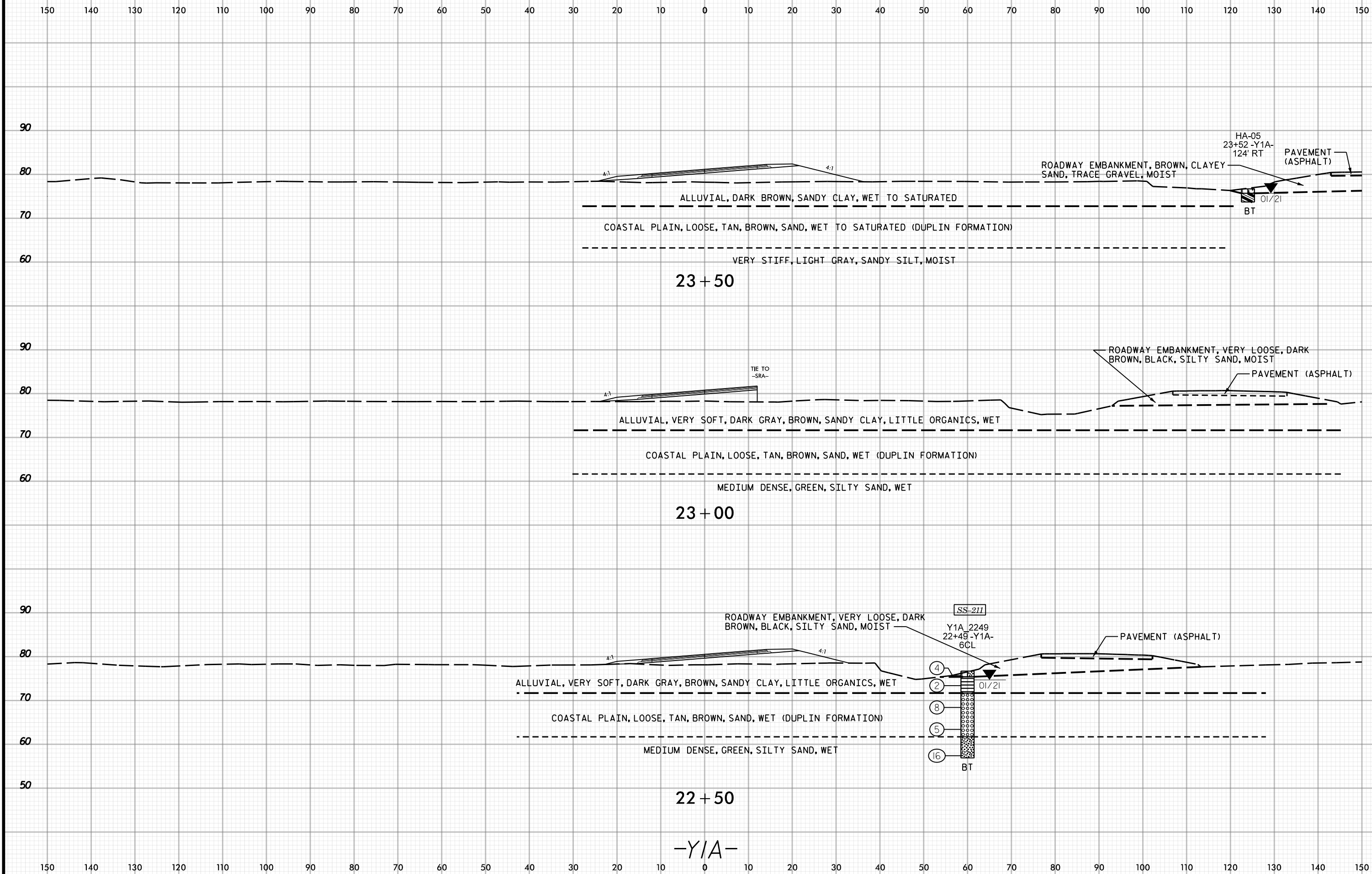
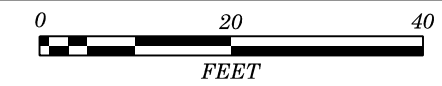
21+50



21+00

-Y/A-

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

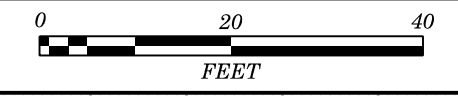


**23 + 50**

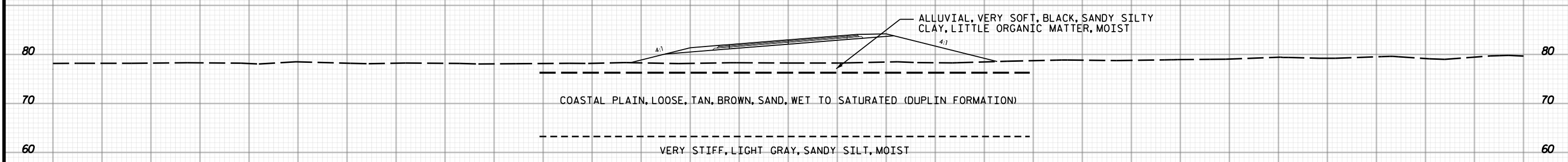
**23 + 00**

**22 + 50**

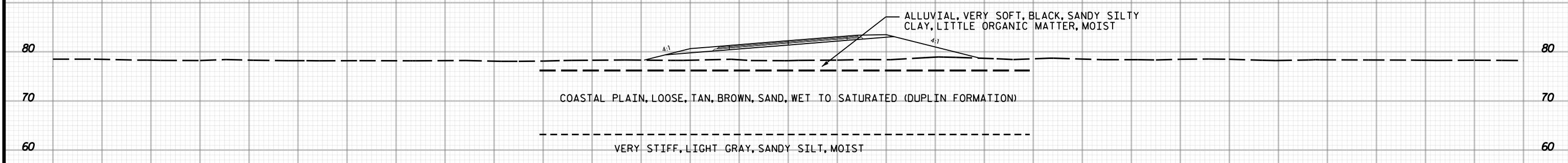
**-Y/A-**



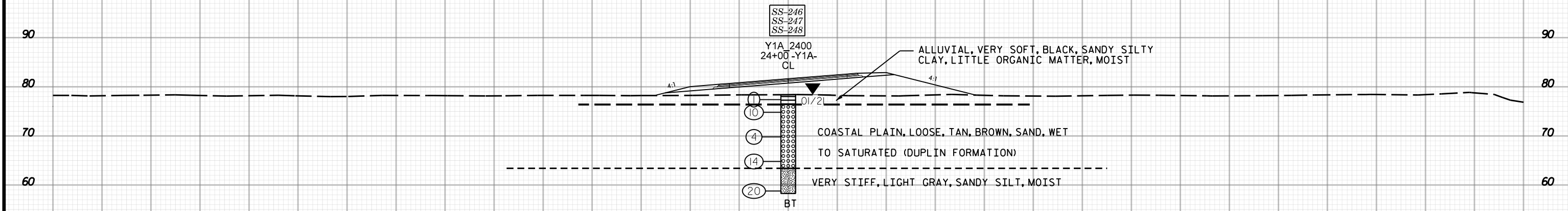
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**25 + 00**



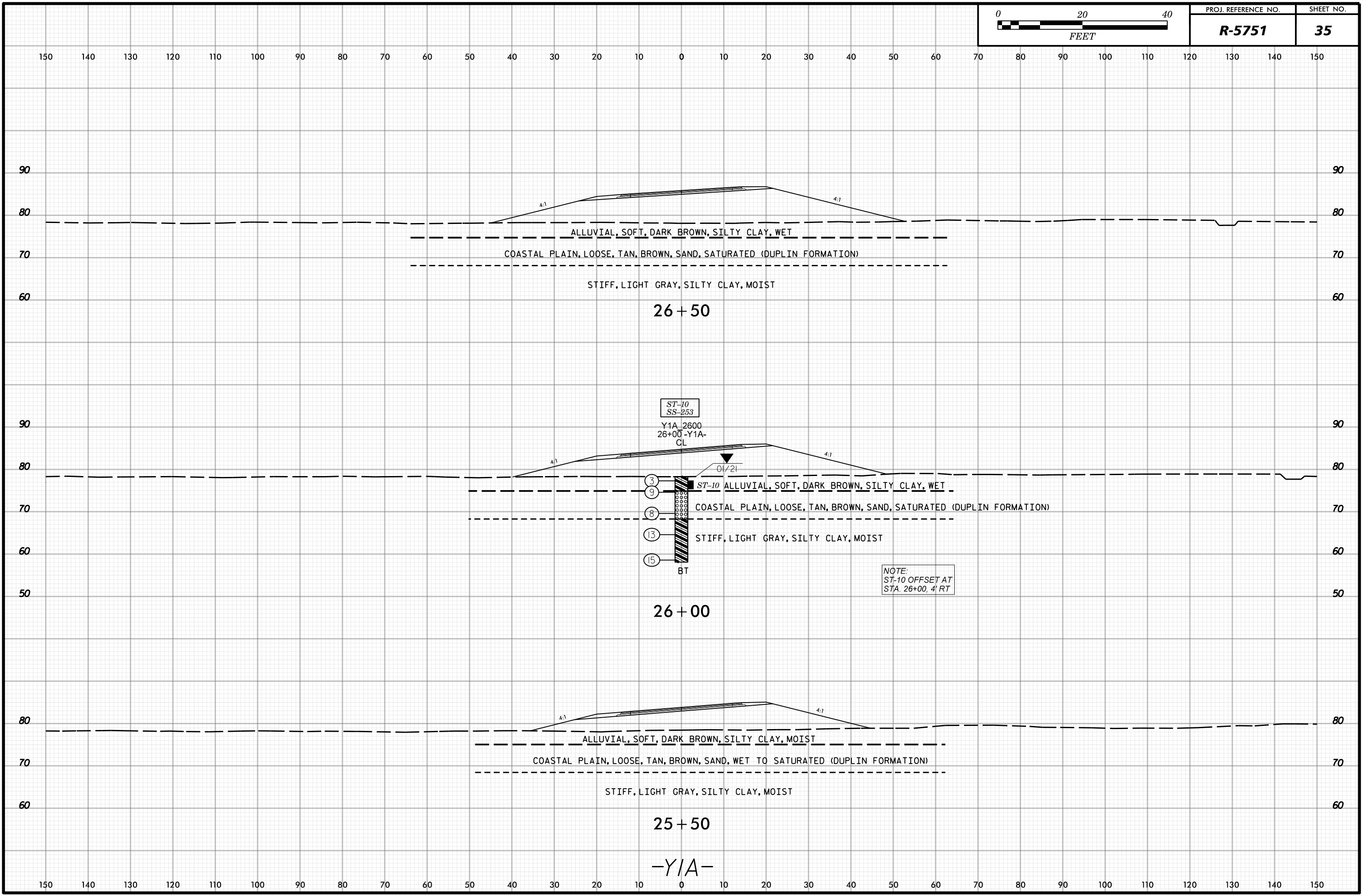
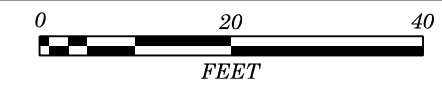
**24 + 50**

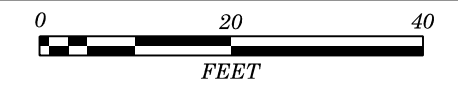


**24 + 00**

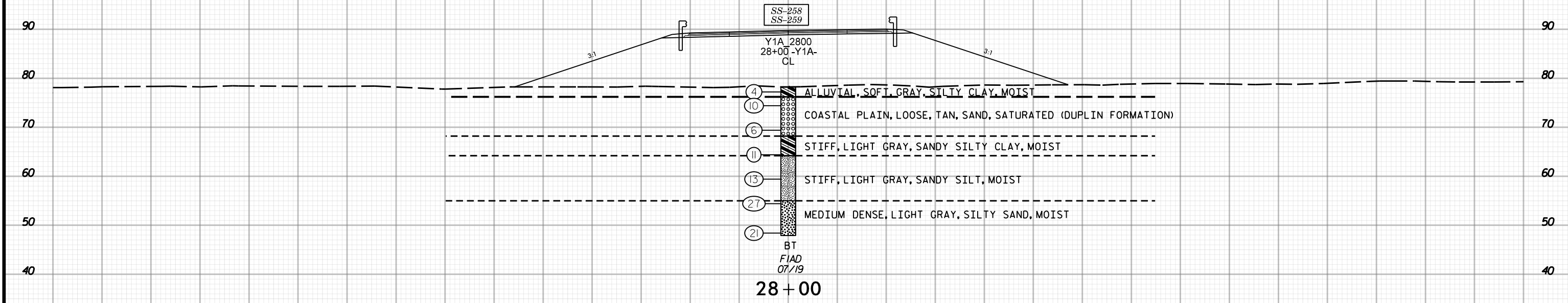
**-Y1A-**

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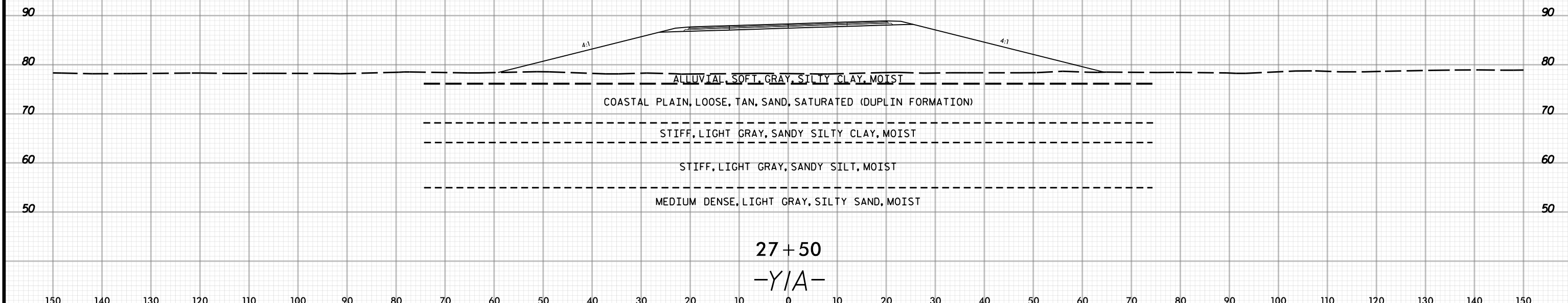




150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



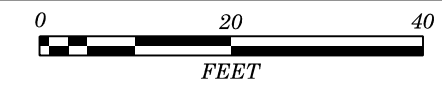
**28 + 00**



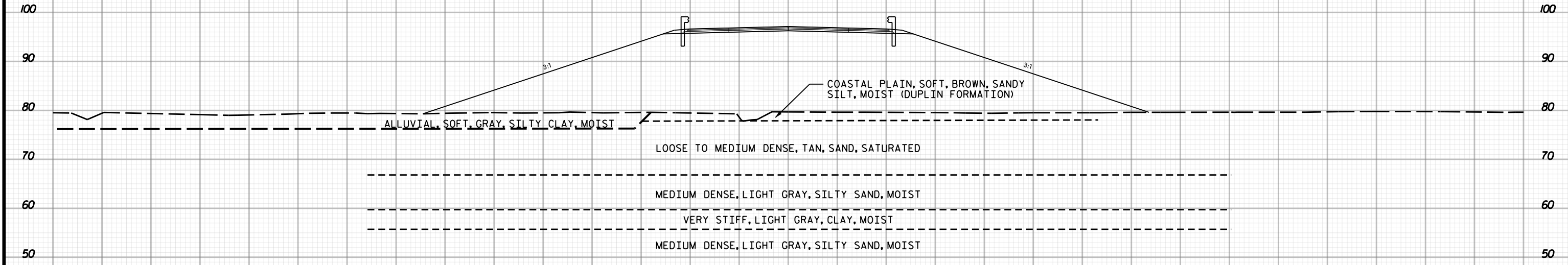
**27 + 50**

**-Y/A-**

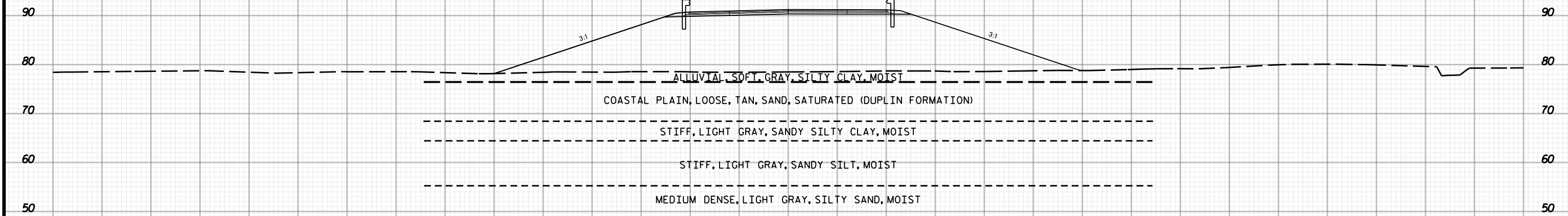
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150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



**30 + 50**

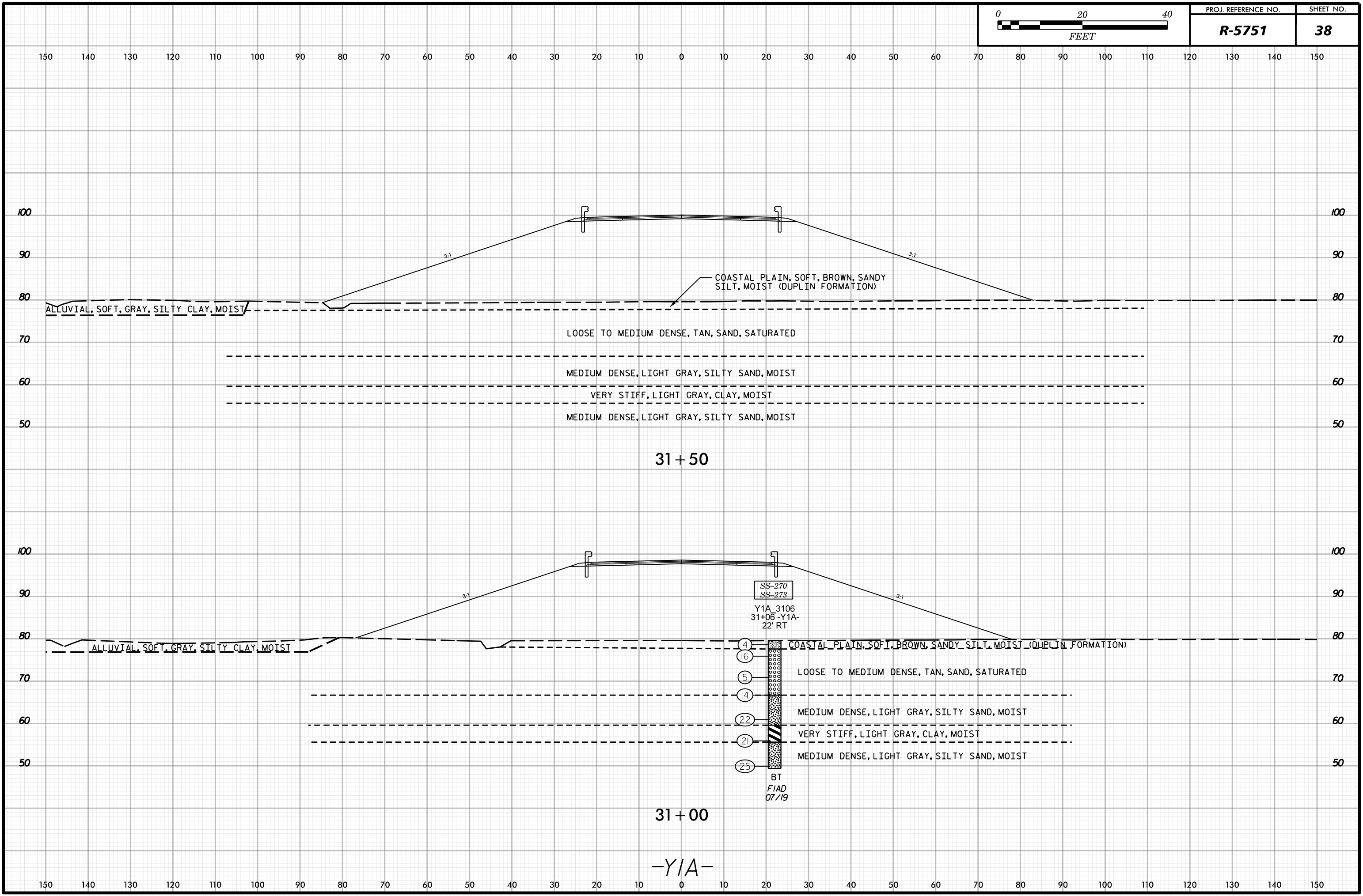
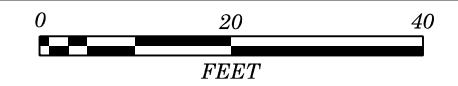


**28 + 50**

-Y/A-

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

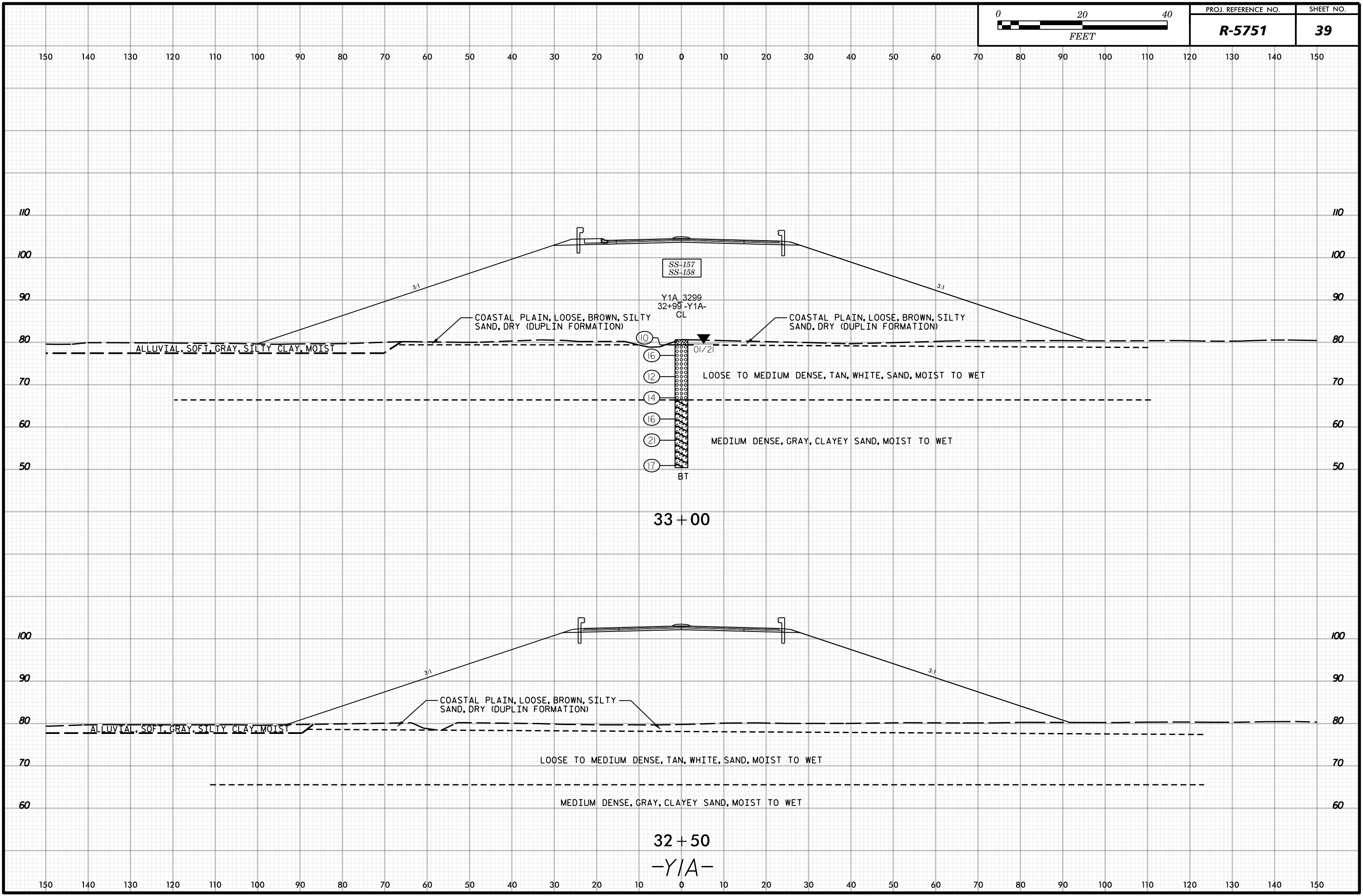
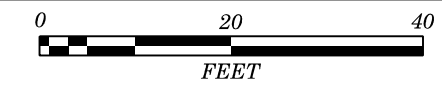




31+50

31+00

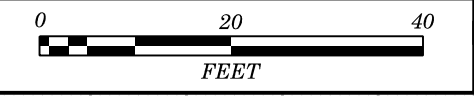
-Y/A-



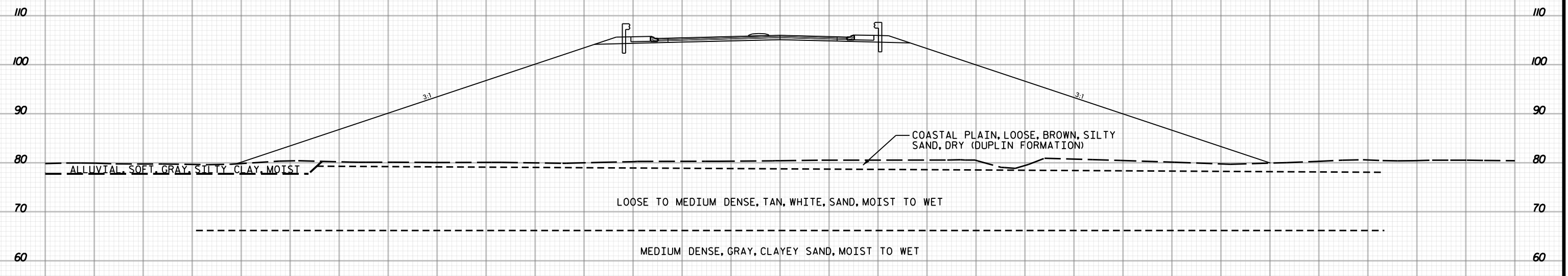
33 + 00

32 + 50

-Y/A-



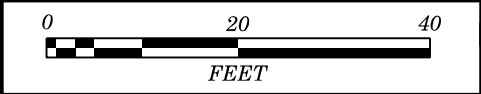
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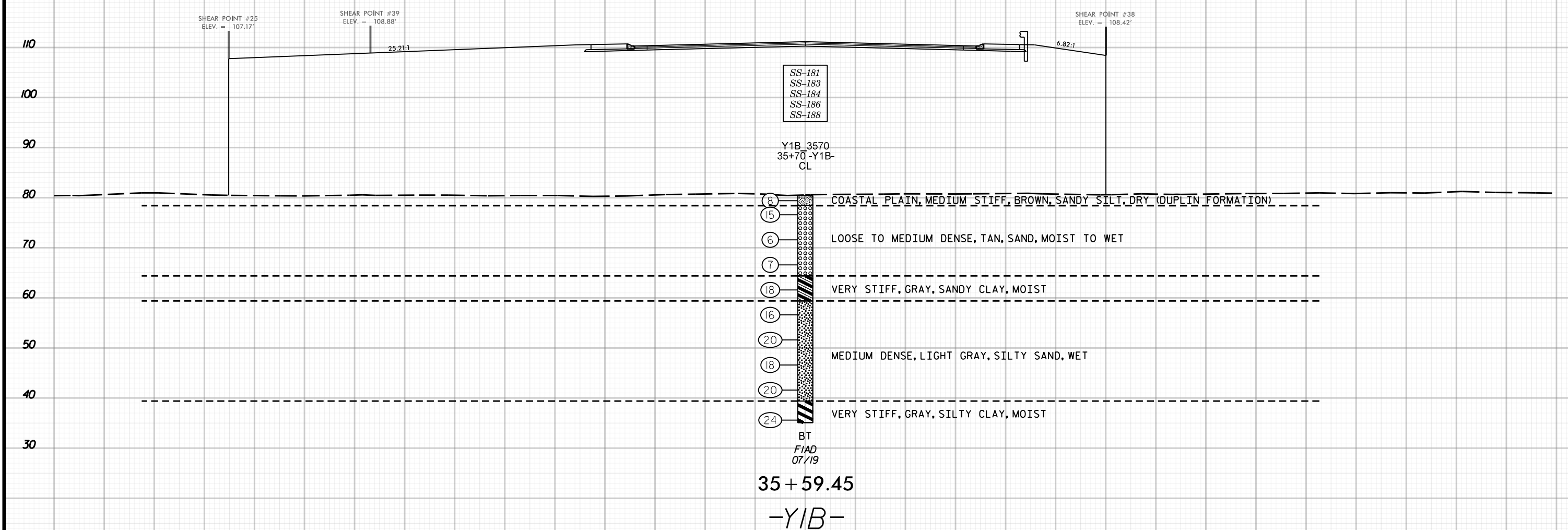
33 + 50

-Y/A-

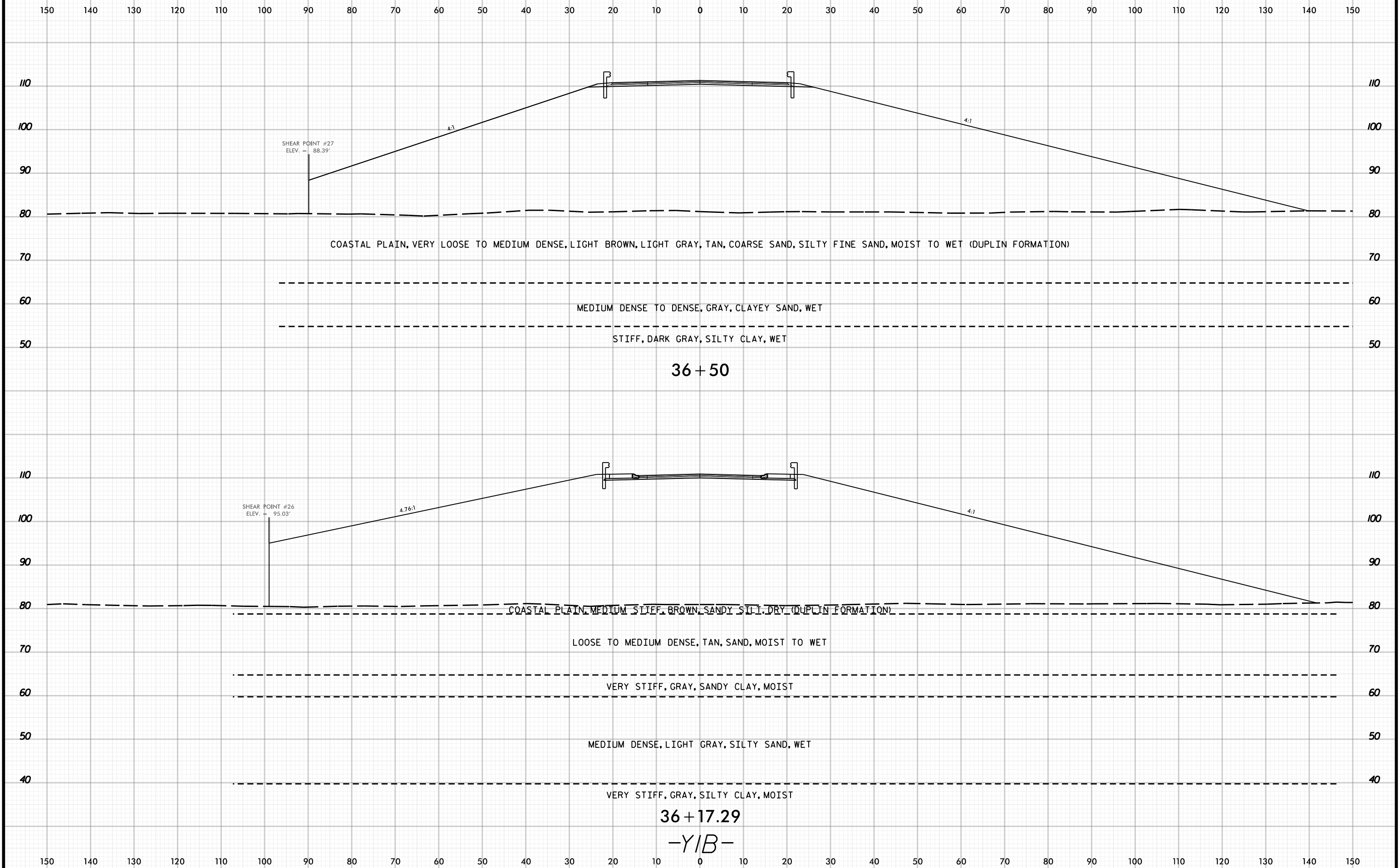
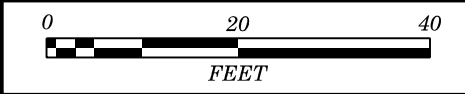
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150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



SHEAR POINT #27  
ELEV. = 88.39'

SHEAR POINT #26  
ELEV. = 95.03'

COASTAL PLAIN, VERY LOOSE TO MEDIUM DENSE, LIGHT BROWN, LIGHT GRAY, TAN, COARSE SAND, SILTY FINE SAND, MOIST TO WET (DUPLIN FORMATION)

MEDIUM DENSE TO DENSE, GRAY, CLAYEY SAND, WET

STIFF, DARK GRAY, SILTY CLAY, WET

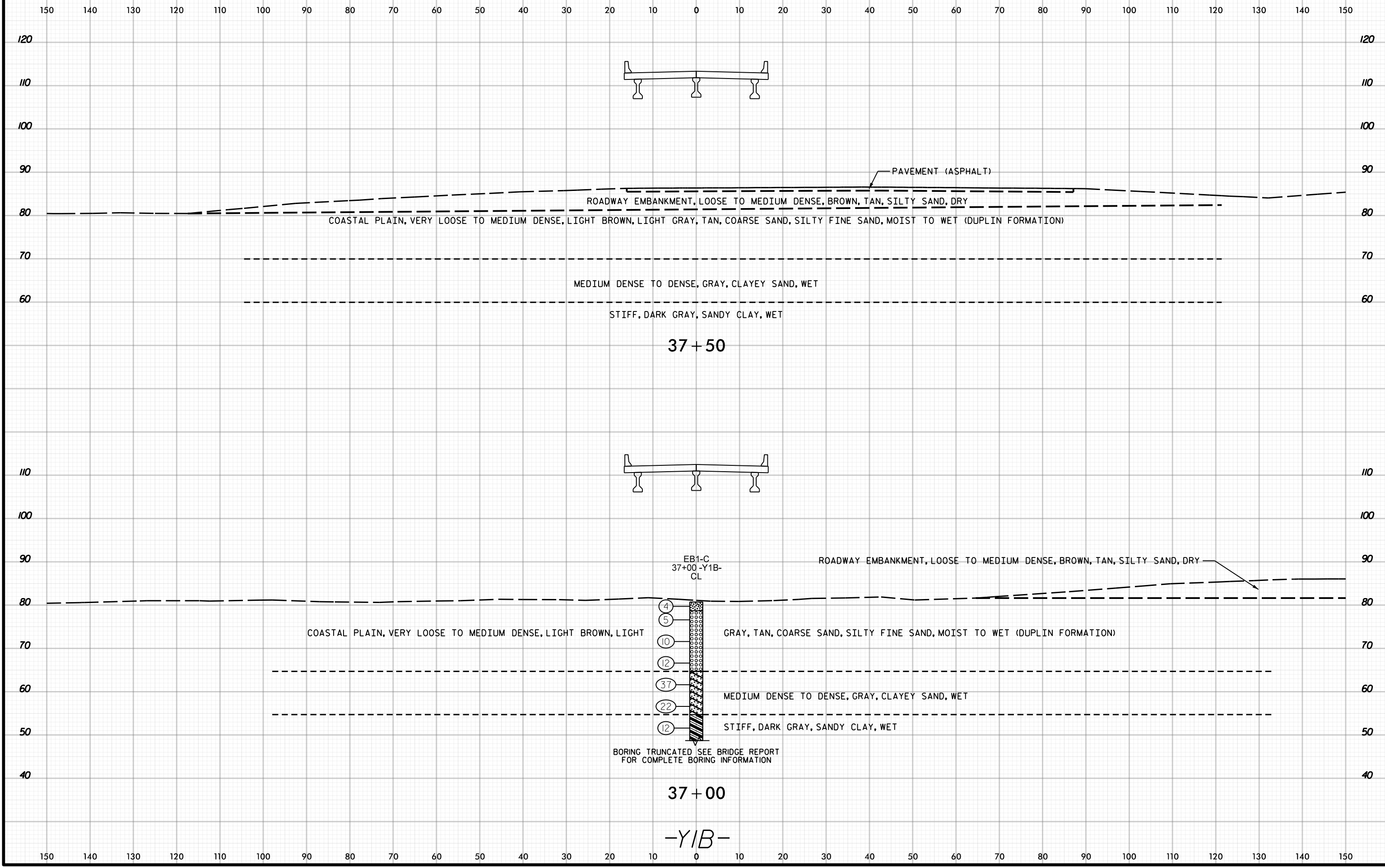
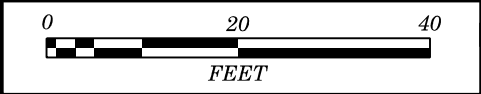
COASTAL PLAIN, MEDIUM STIFF, BROWN, SANDY SILT, DRY (DUPLIN FORMATION)

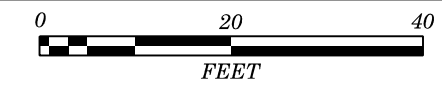
LOOSE TO MEDIUM DENSE, TAN, SAND, MOIST TO WET

VERY STIFF, GRAY, SANDY CLAY, MOIST

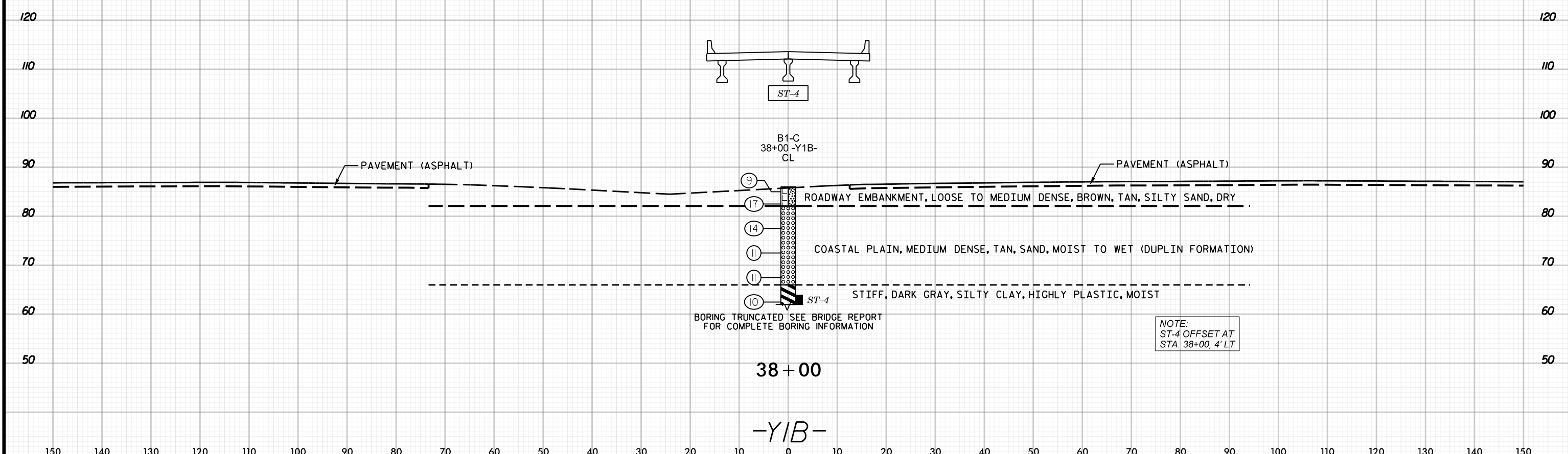
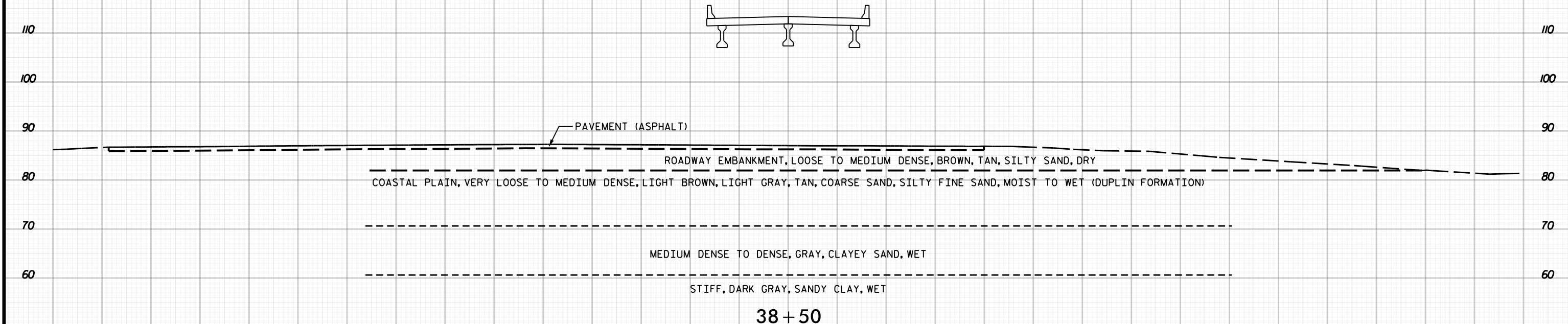
MEDIUM DENSE, LIGHT GRAY, SILTY SAND, WET

VERY STIFF, GRAY, SILTY CLAY, MOIST

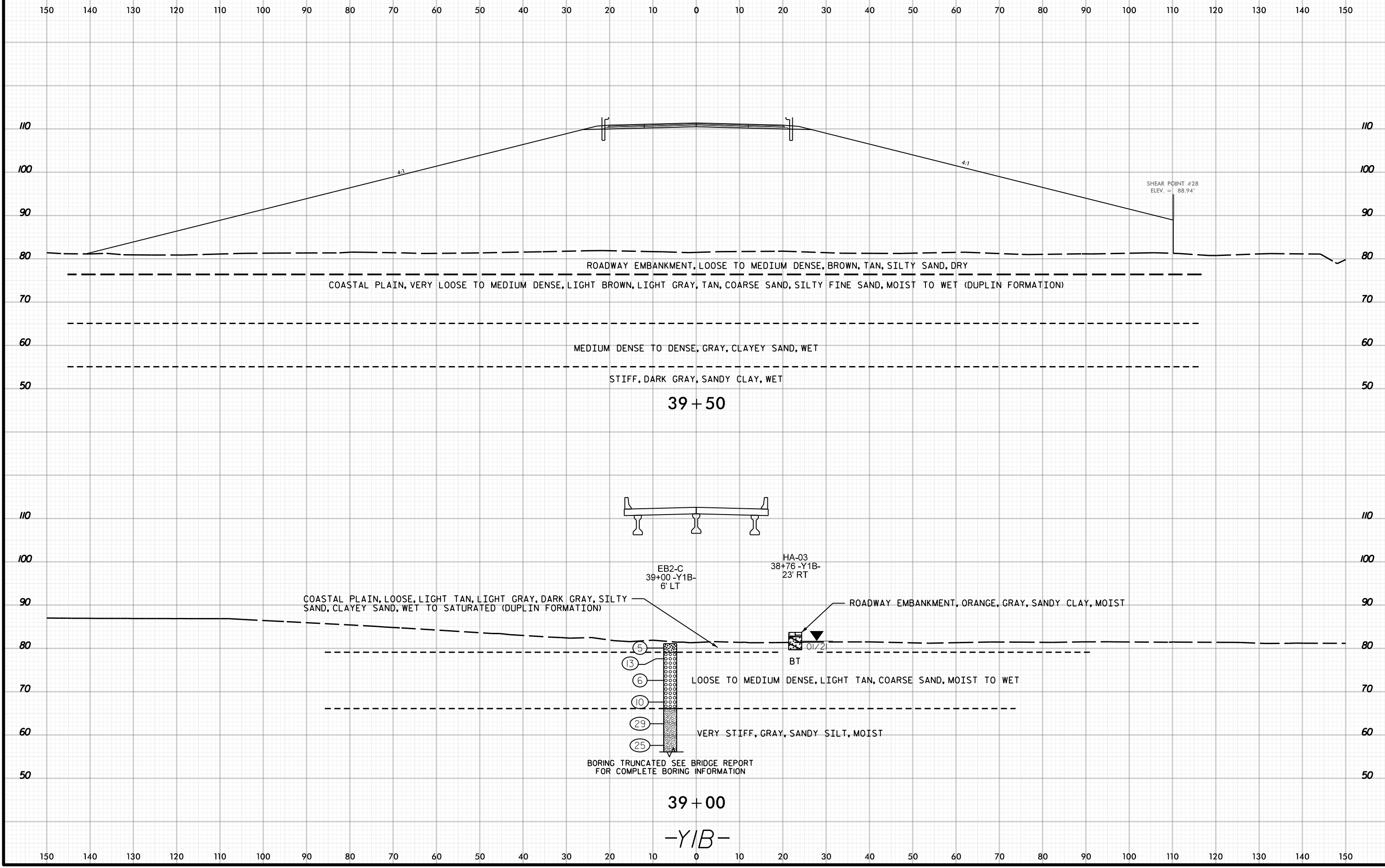
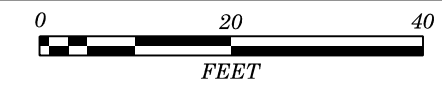




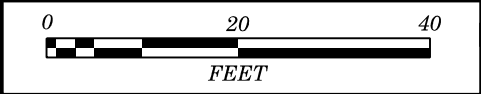
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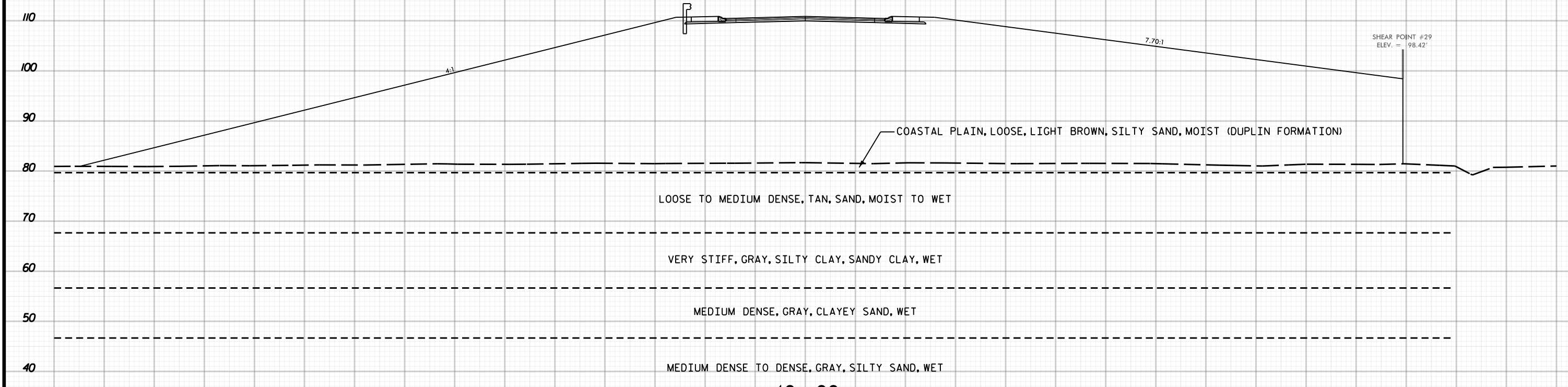
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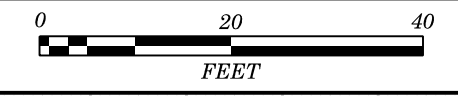


150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

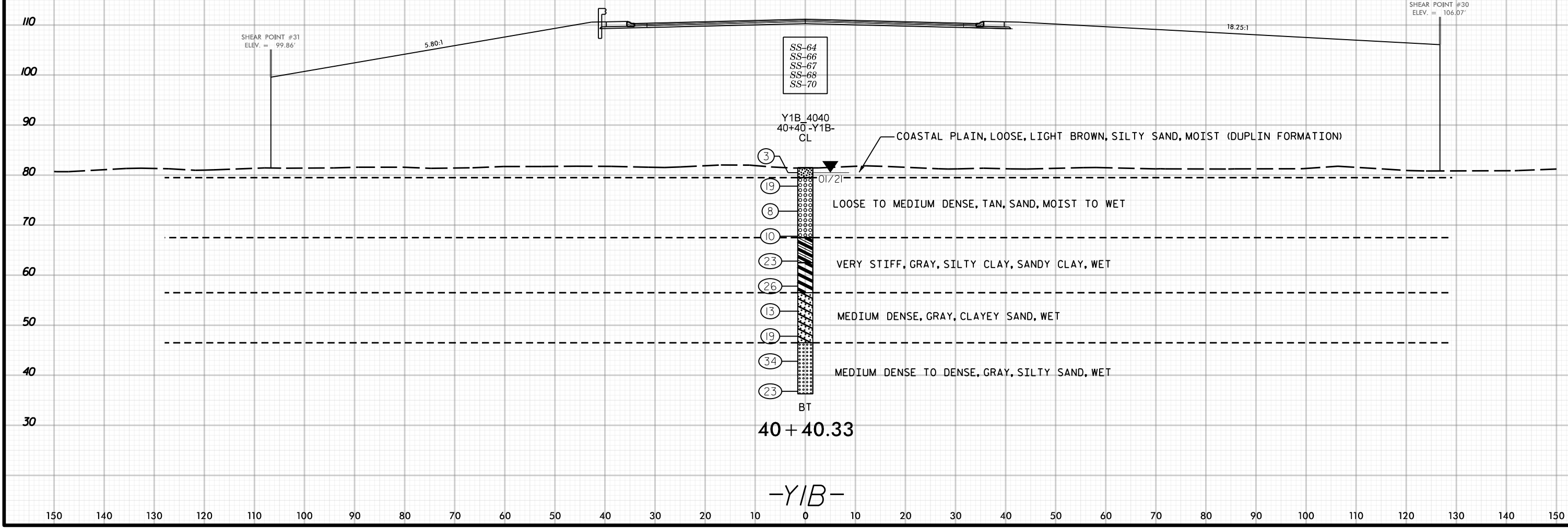


40 + 00  
-YIB-

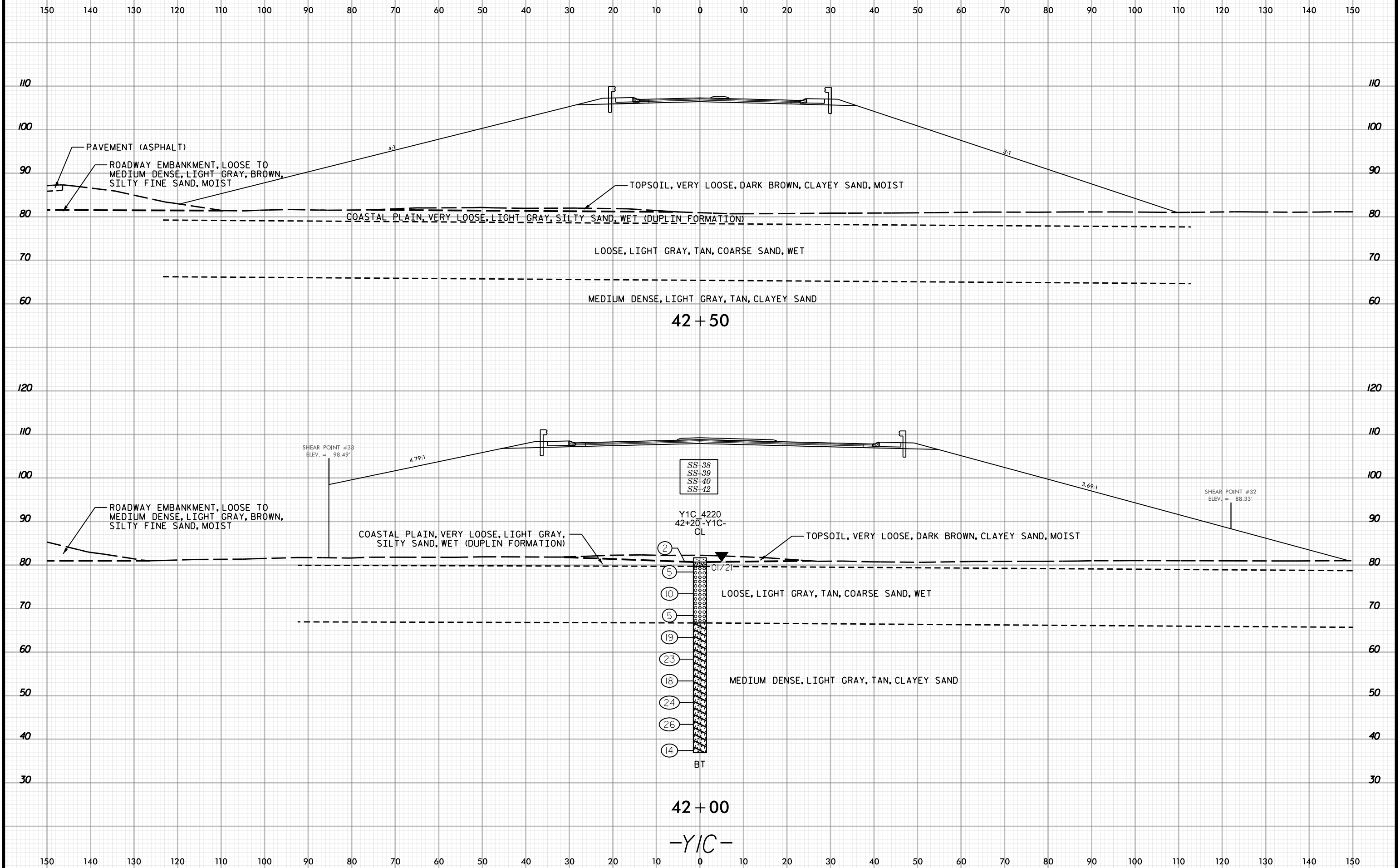
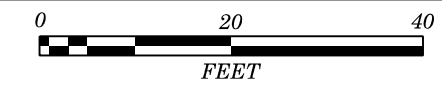
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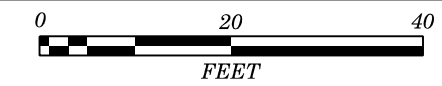


150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

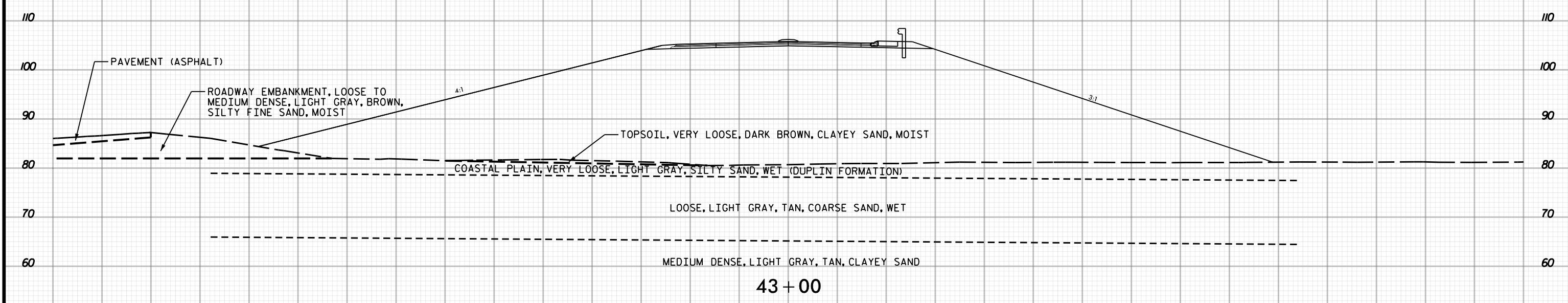
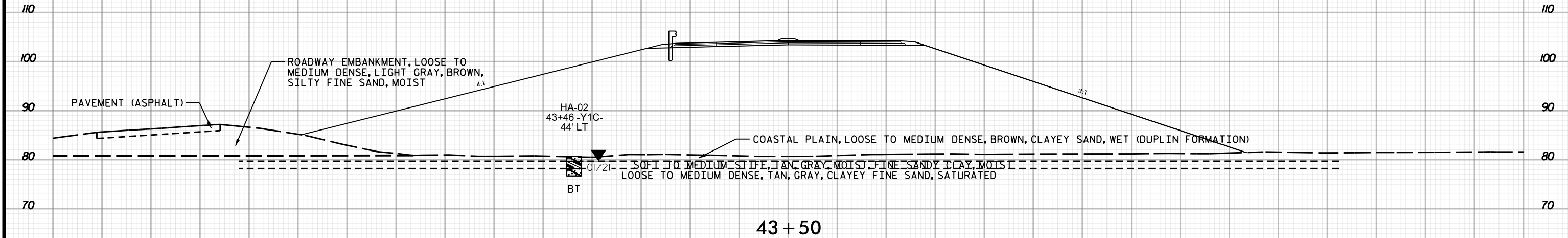


150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



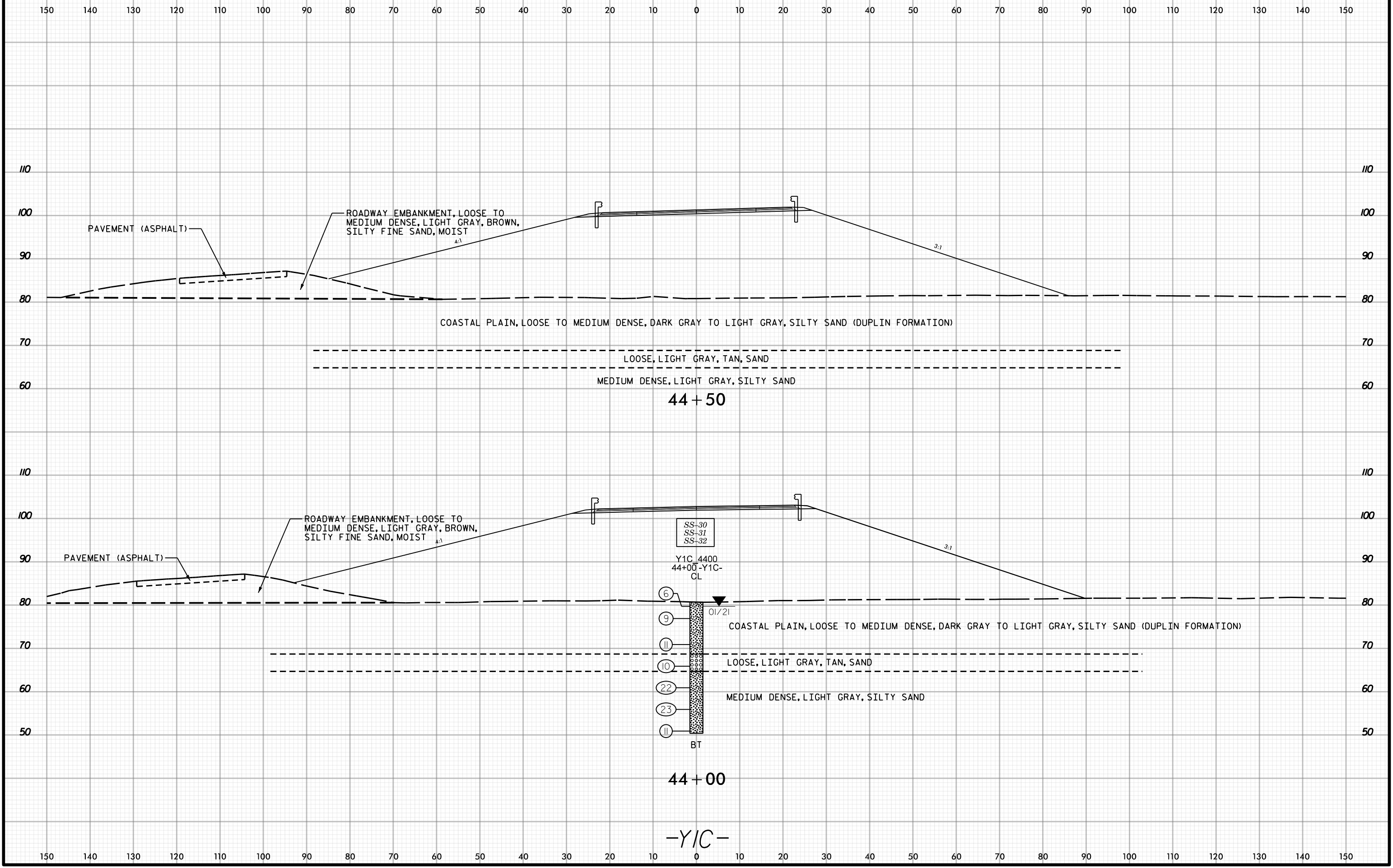
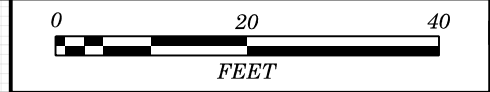


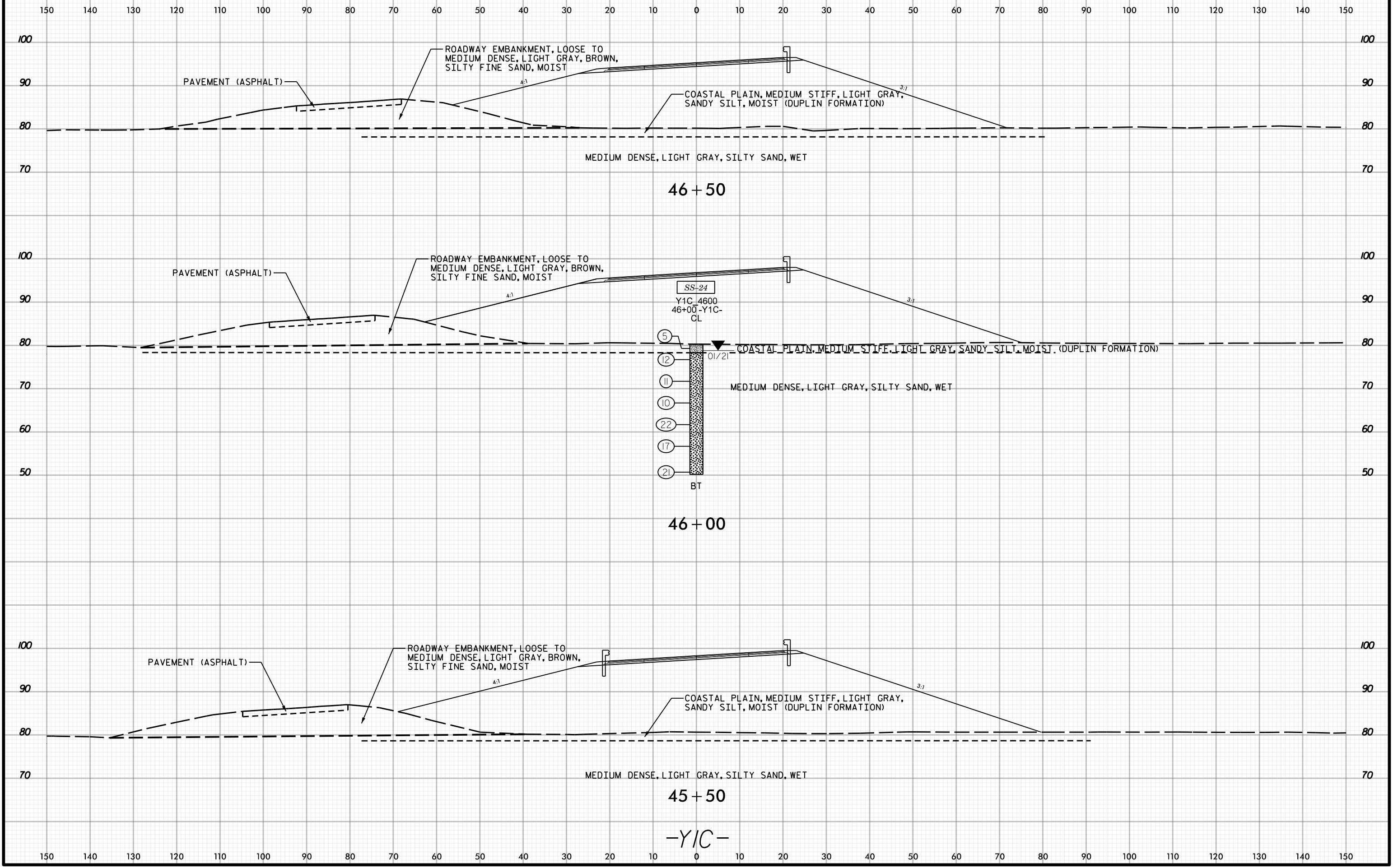
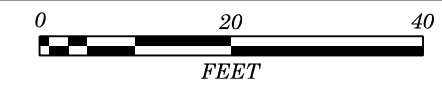
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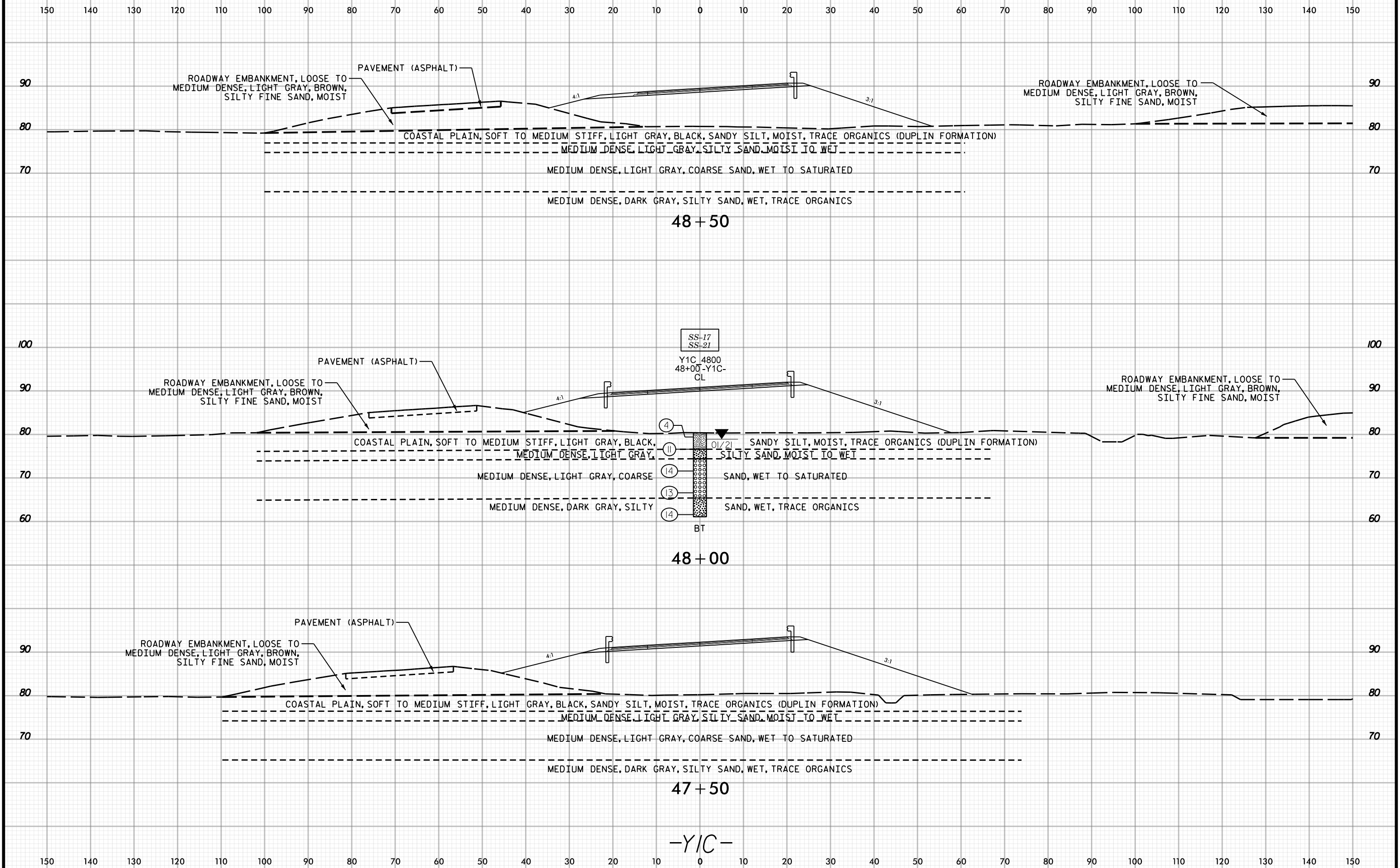
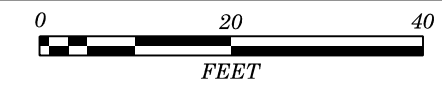


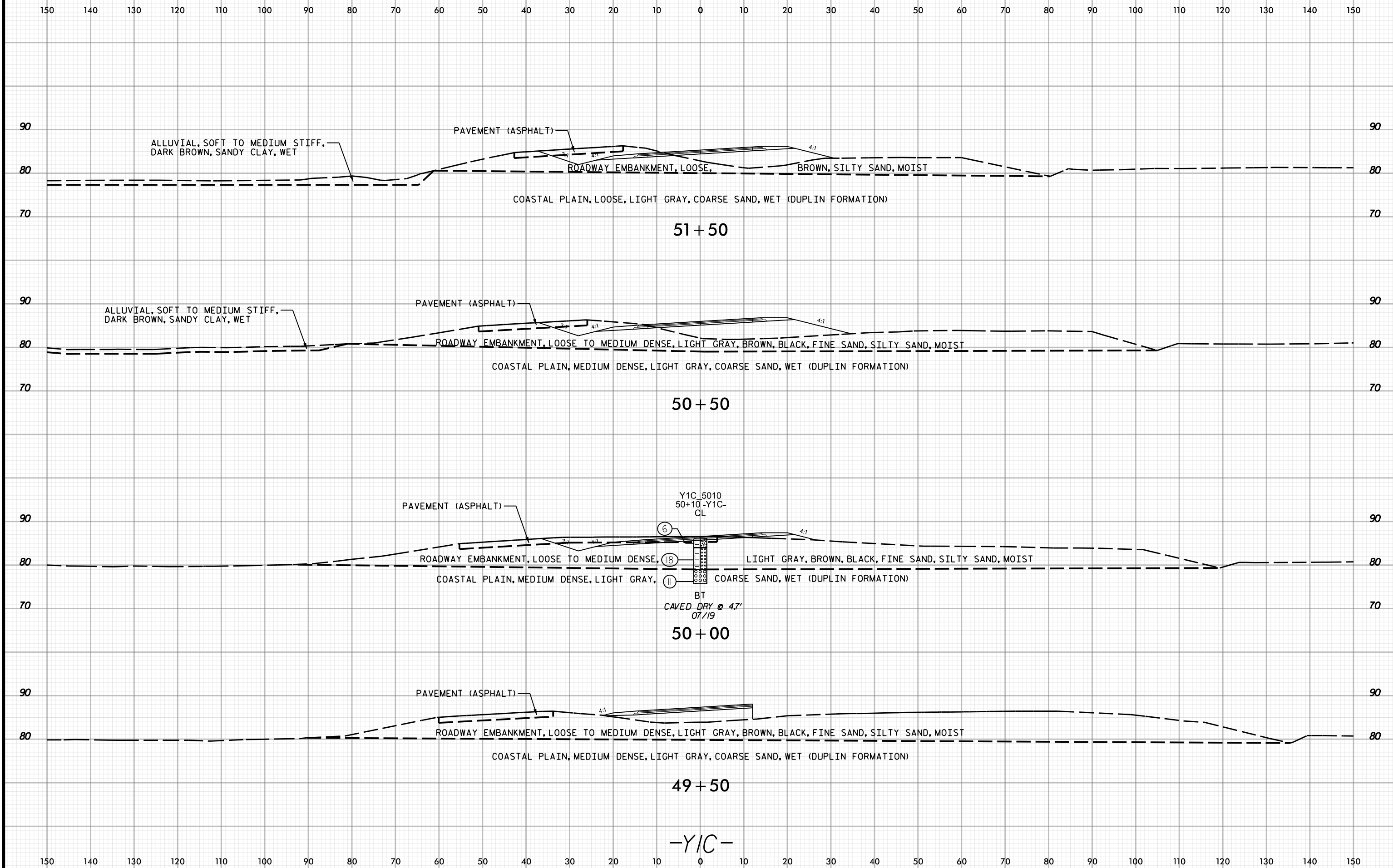
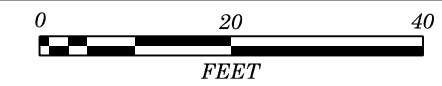
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-Y1C-

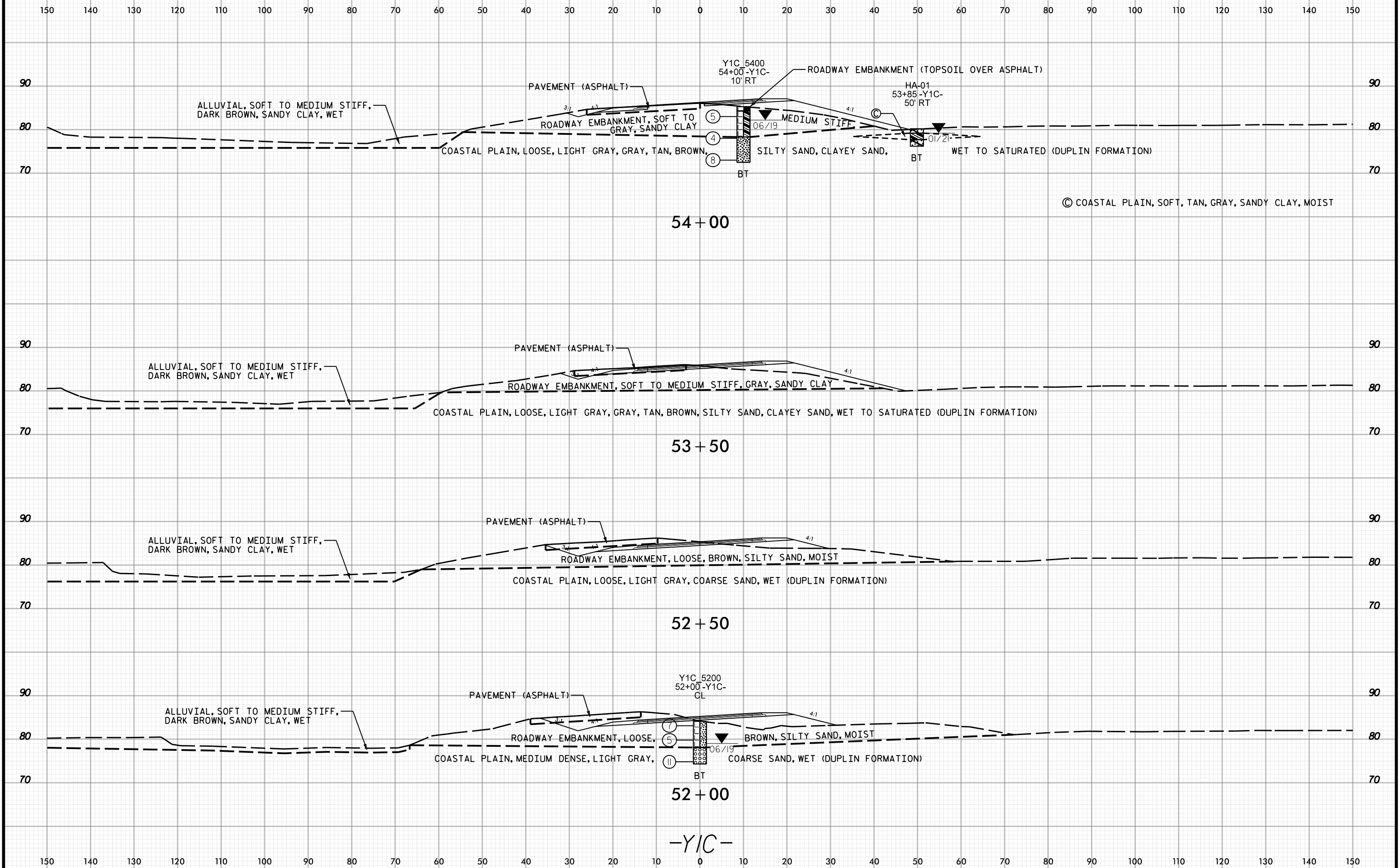
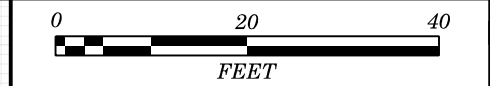






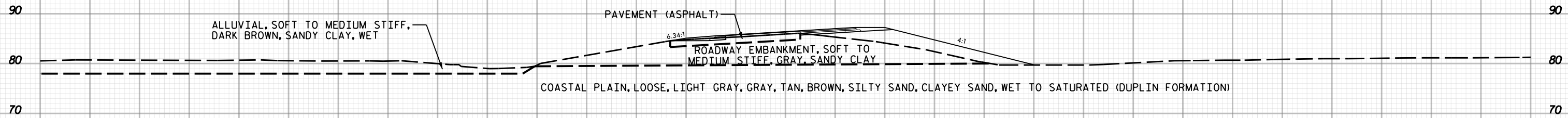






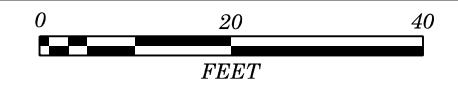


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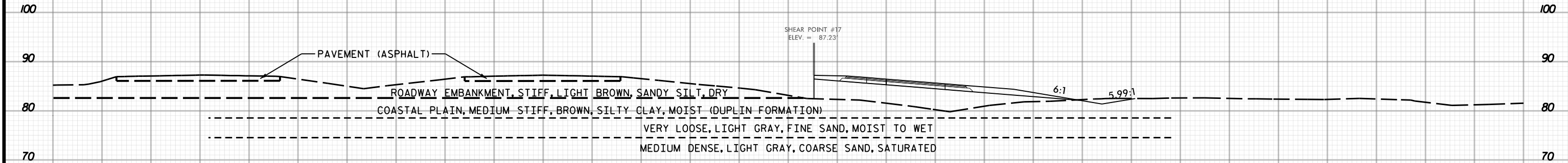


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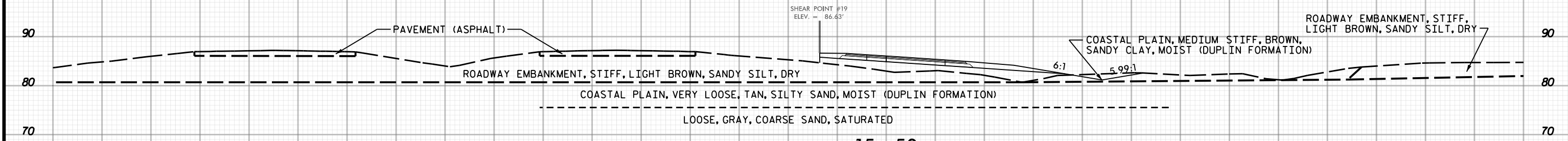
54+50  
-YIC-



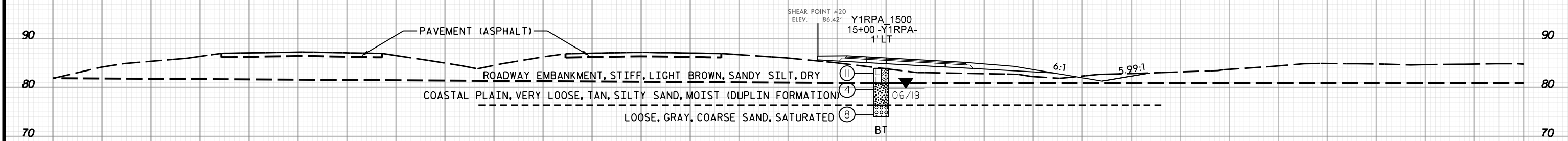
170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130



16+50



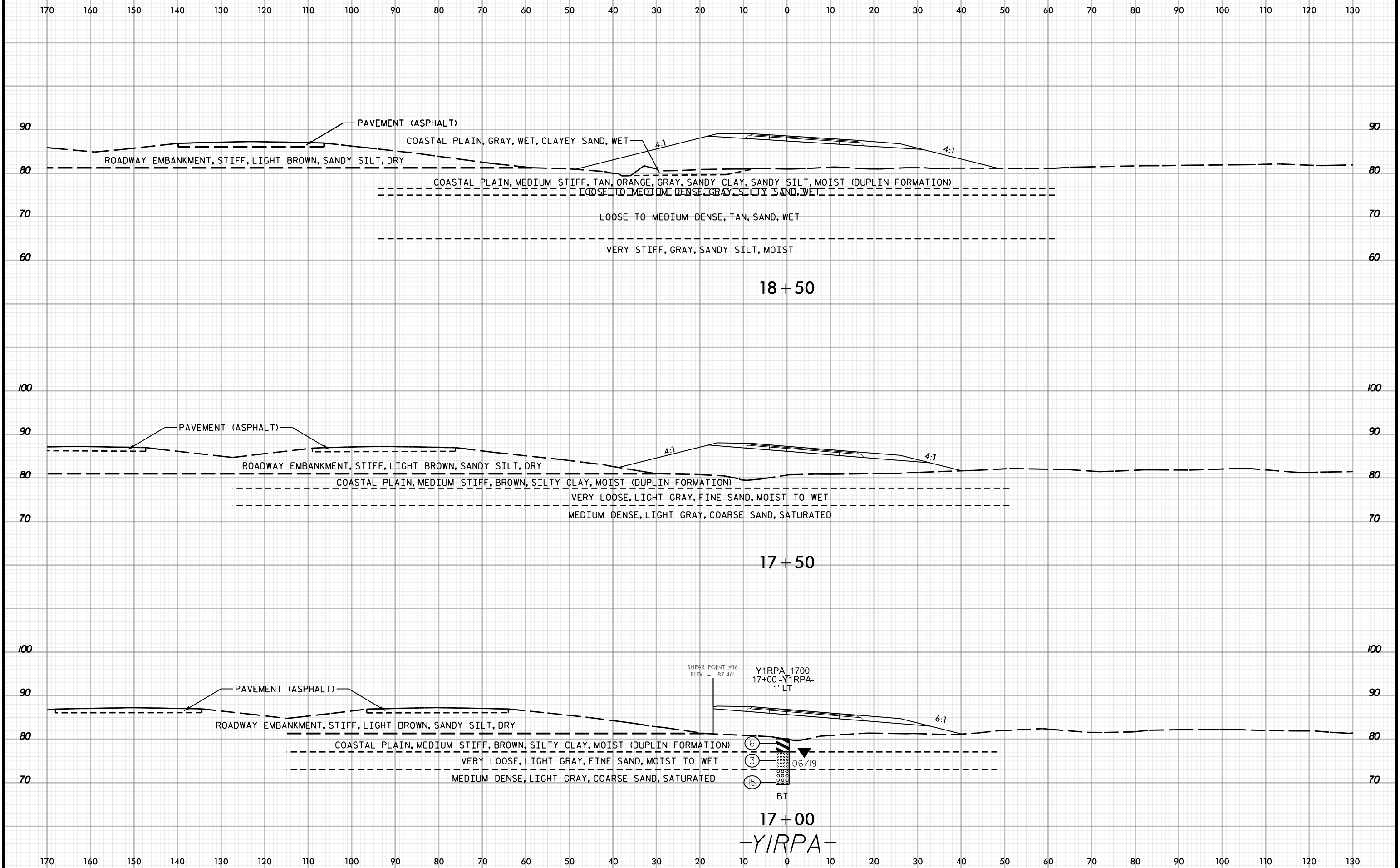
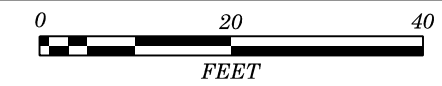
15+50

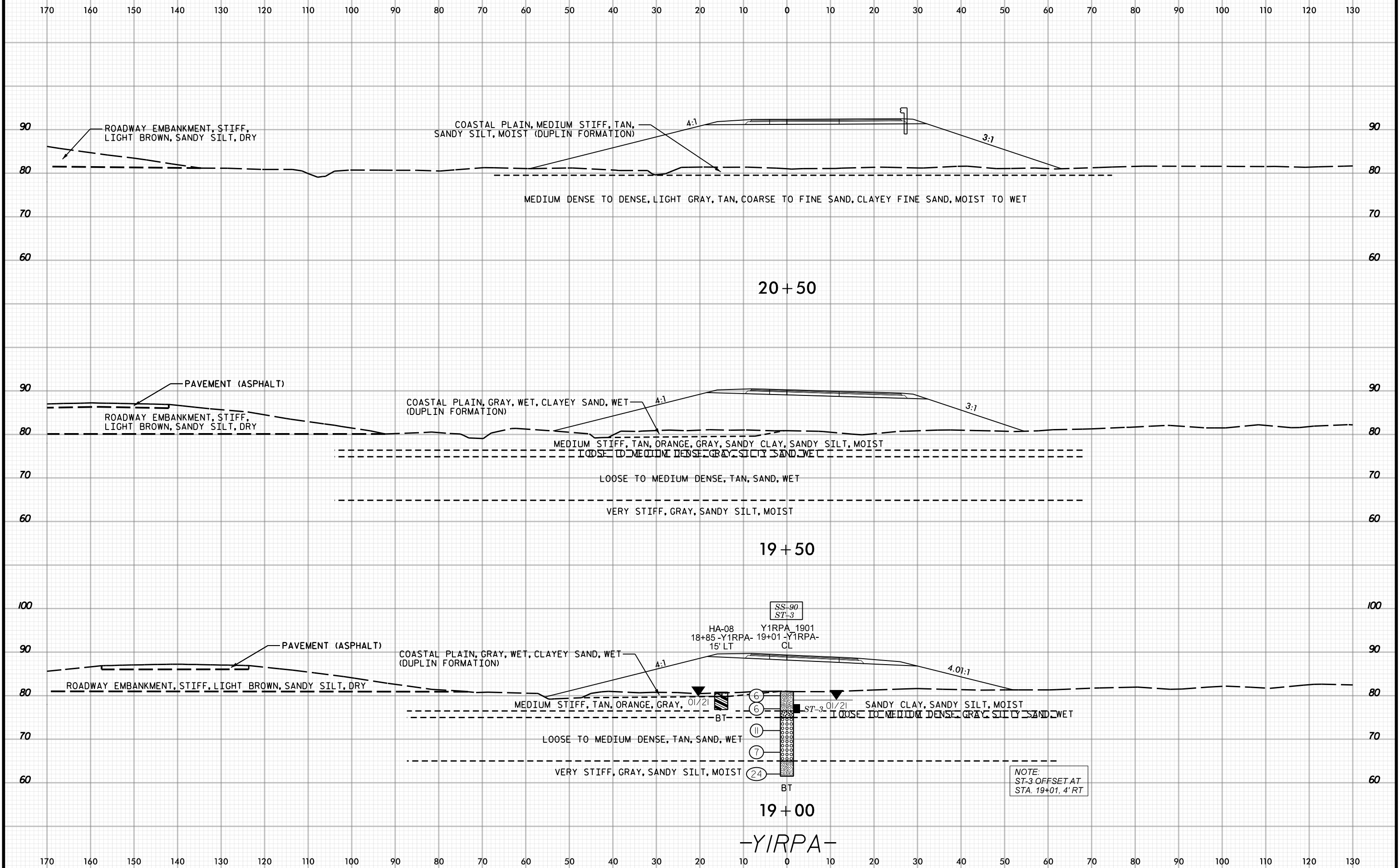
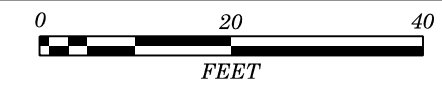


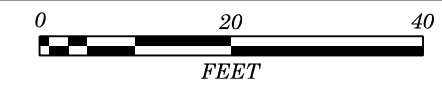
15+00

-Y1RPA-

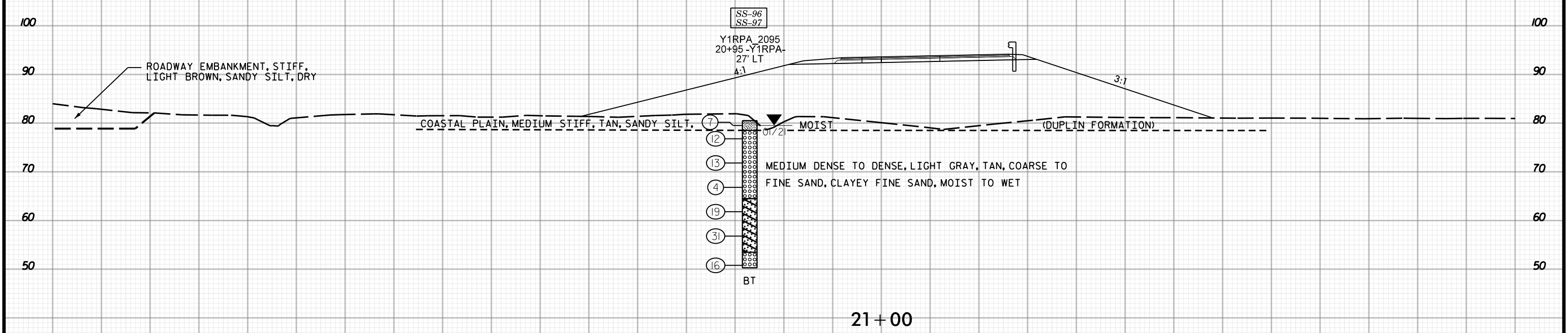
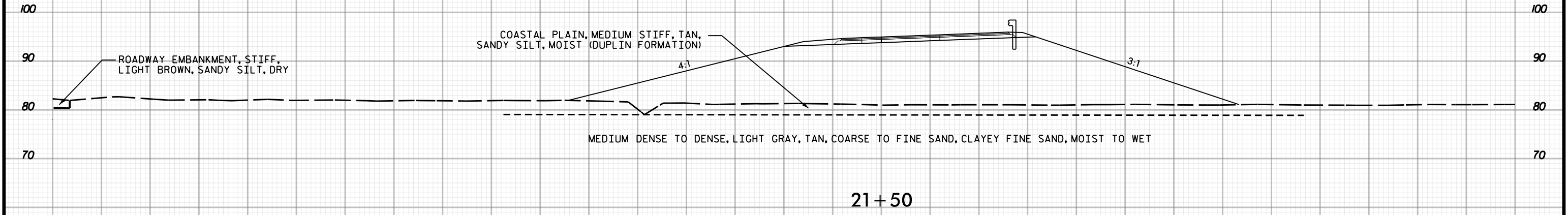
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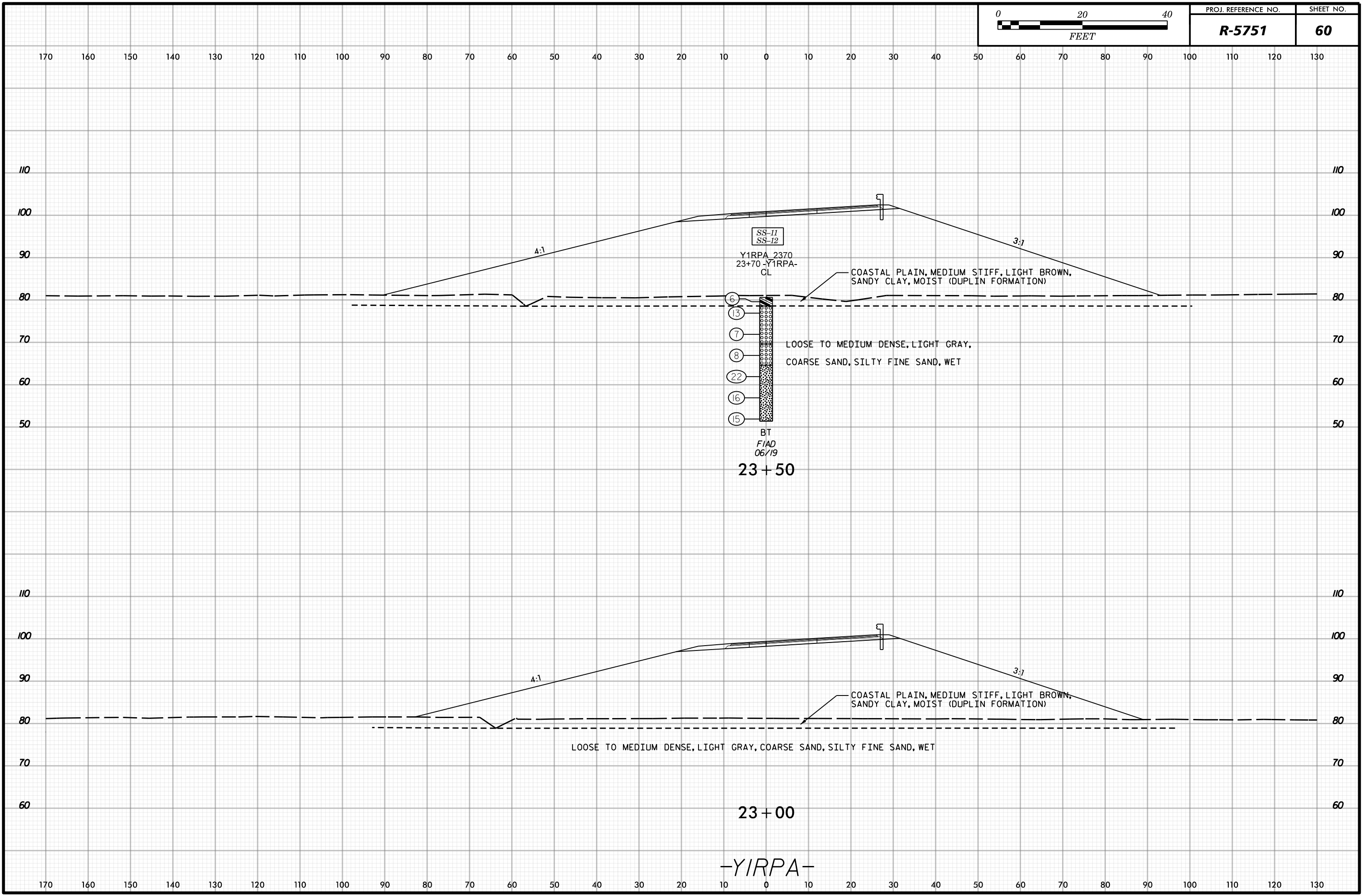
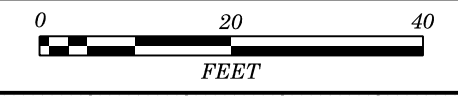


170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130



170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130

-Y1RPA-



SS-11  
SS-12

Y1RPA 2370  
23+70 -Y1RPA-  
CL

COASTAL PLAIN, MEDIUM STIFF, LIGHT BROWN,  
SANDY CLAY, MOIST (DUPLIN FORMATION)

- 6
- 13
- 7
- 8
- 22
- 16
- 15

LOOSE TO MEDIUM DENSE, LIGHT GRAY,  
COARSE SAND, SILTY FINE SAND, WET

BT  
FIAD  
06/19

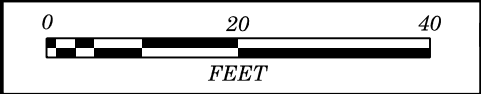
23+50

COASTAL PLAIN, MEDIUM STIFF, LIGHT BROWN,  
SANDY CLAY, MOIST (DUPLIN FORMATION)

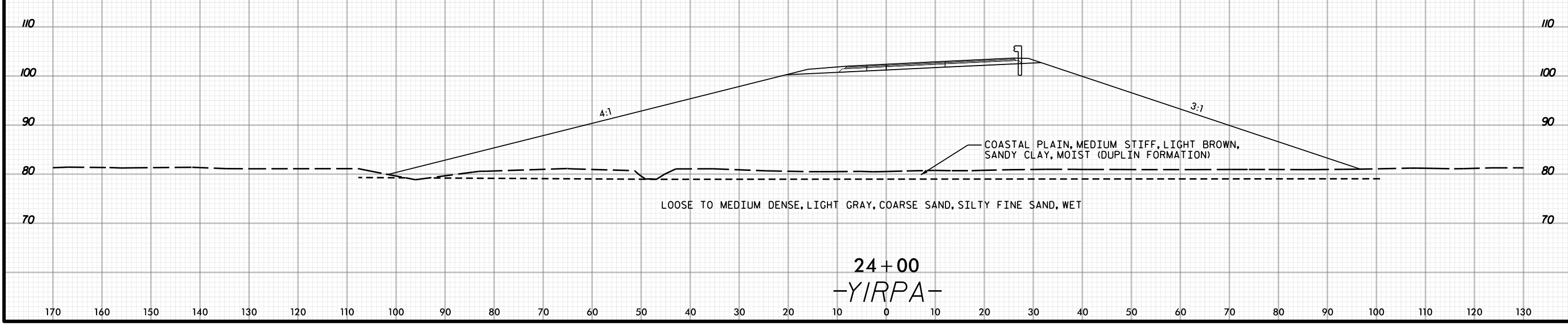
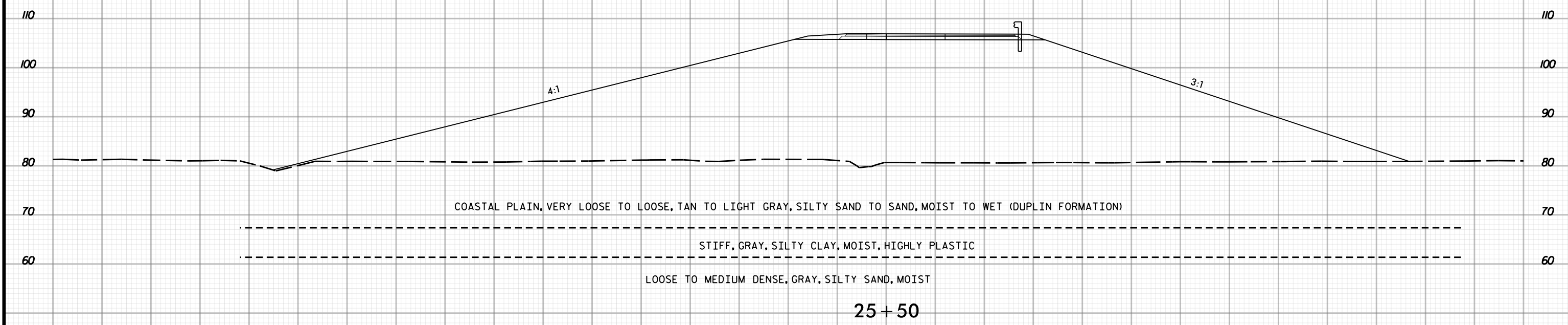
LOOSE TO MEDIUM DENSE, LIGHT GRAY, COARSE SAND, SILTY FINE SAND, WET

23+00

-Y1RPA-

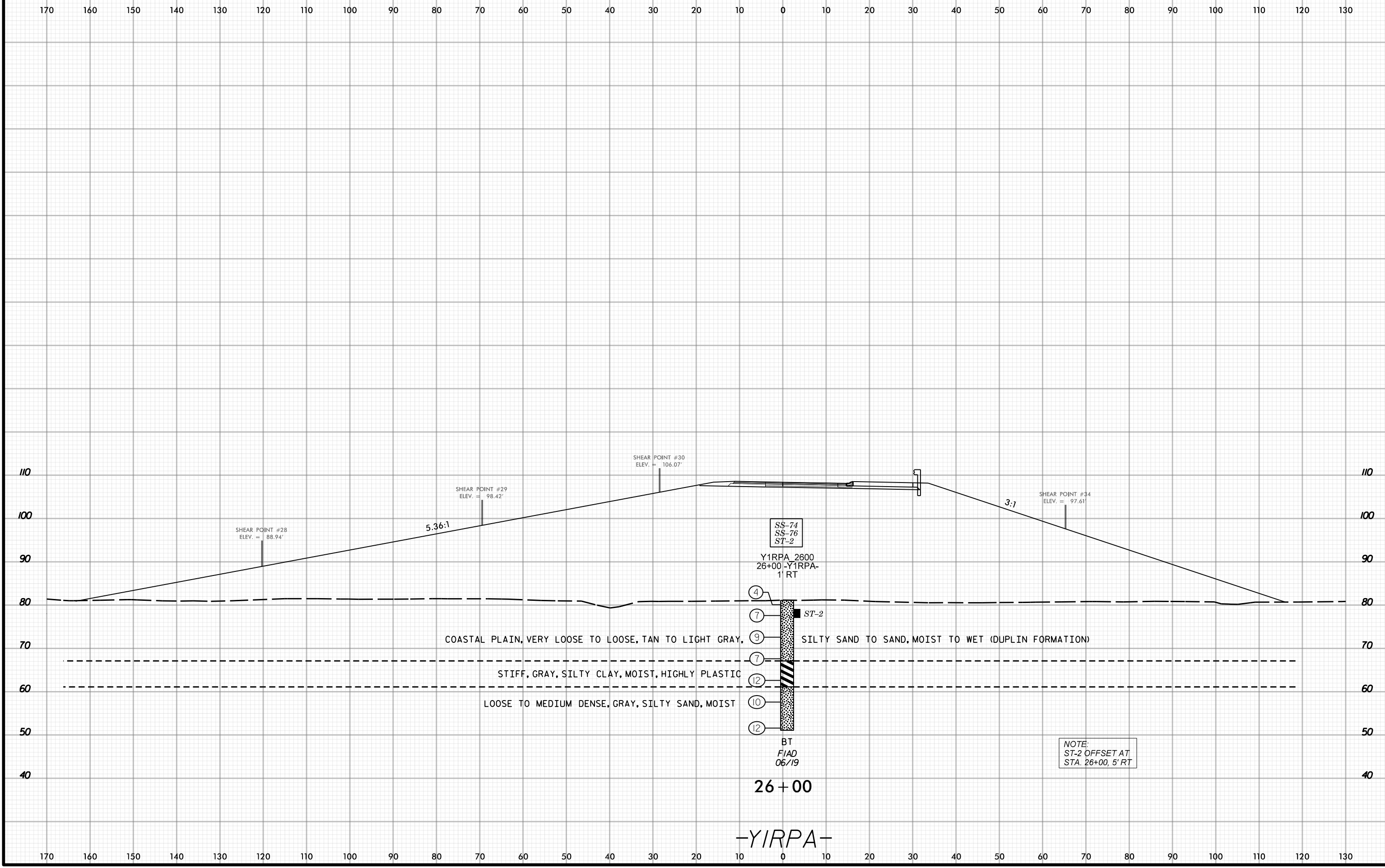
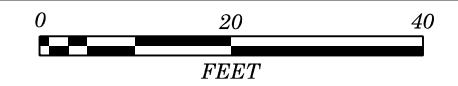


170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130



170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130





SHEAR POINT #28  
ELEV. = 88.94'

SHEAR POINT #29  
ELEV. = 98.42'

SHEAR POINT #30  
ELEV. = 106.07'

SHEAR POINT #34  
ELEV. = 97.61'

5.36:1

3:1

SS-74  
SS-76  
ST-2

Y1RPA 2600  
26+00 -Y1RPA-  
1' RT

- (4)
- (7)
- (9)
- (7)
- (12)
- (10)
- (12)

ST-2

COASTAL PLAIN, VERY LOOSE TO LOOSE, TAN TO LIGHT GRAY,

SILTY SAND TO SAND, MOIST TO WET (DUPLIN FORMATION)

STIFF, GRAY, SILTY CLAY, MOIST, HIGHLY PLASTIC

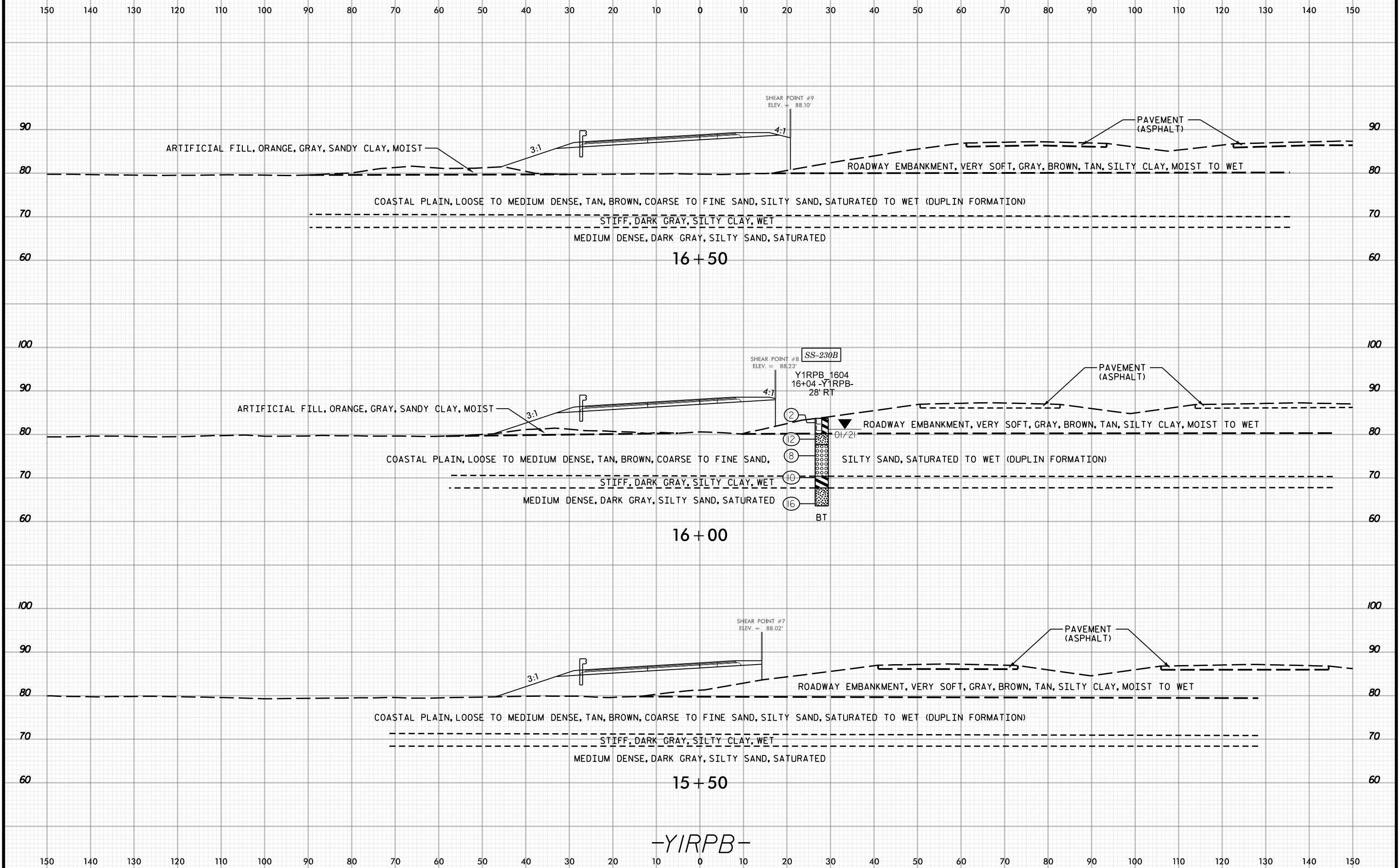
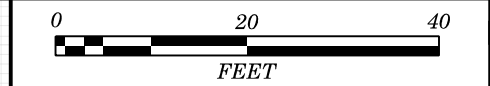
LOOSE TO MEDIUM DENSE, GRAY, SILTY SAND, MOIST

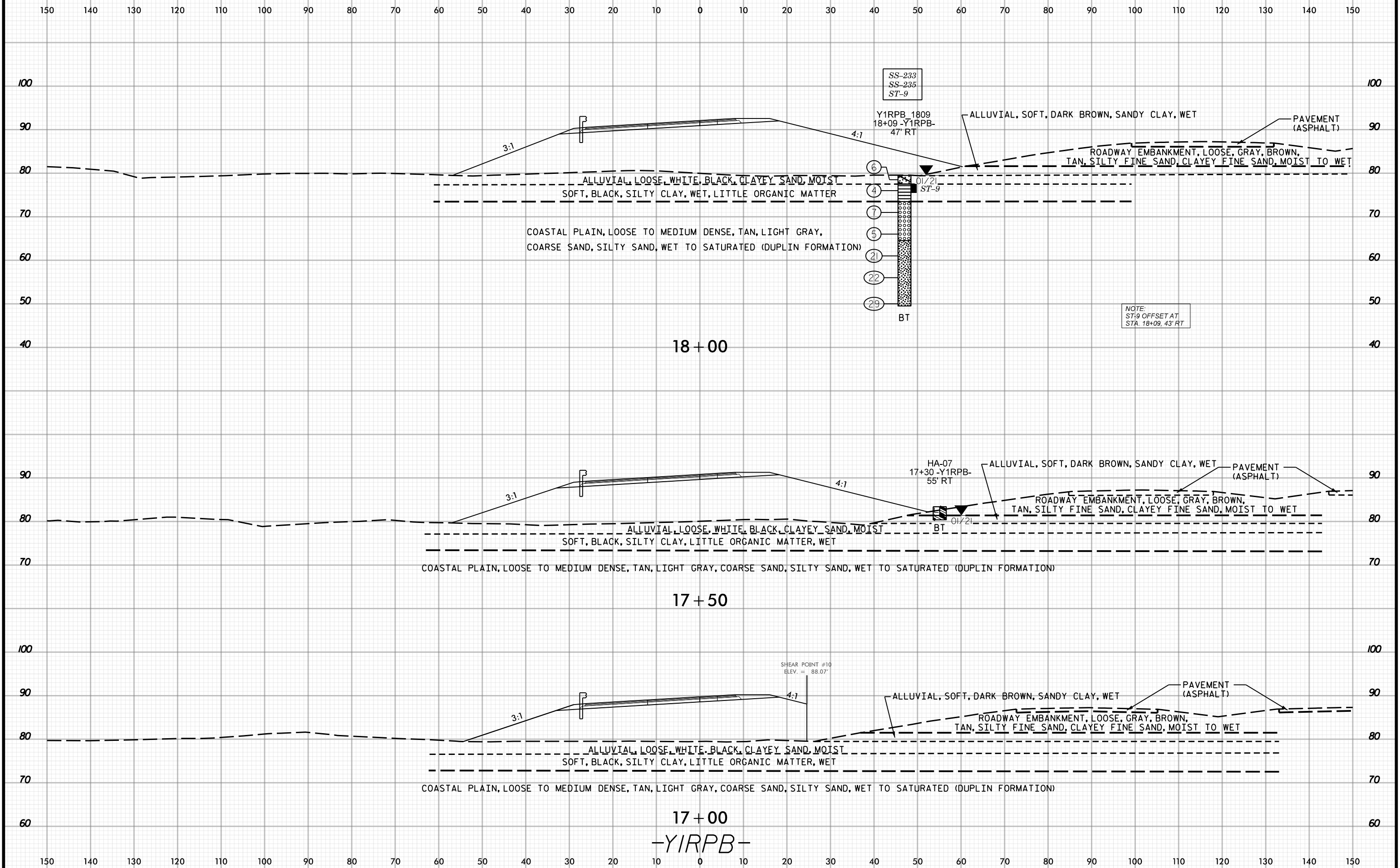
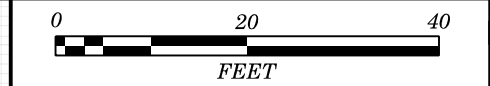
BT  
FIAD  
06/19

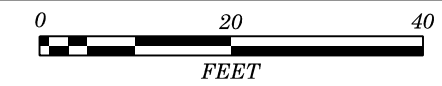
NOTE:  
ST-2 OFFSET AT  
STA. 26+00, 5' RT

26 + 00

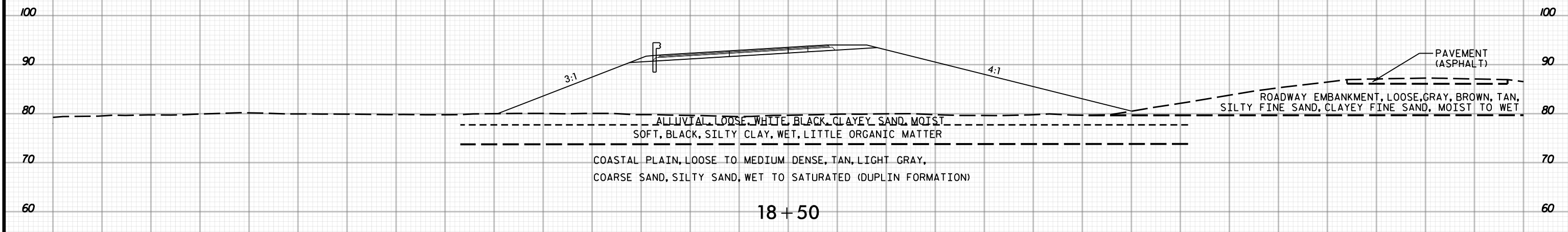
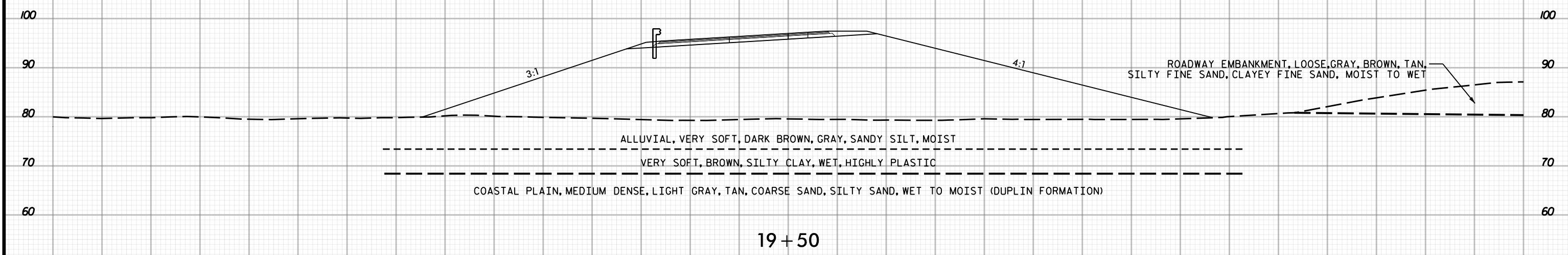
-Y1RPA-





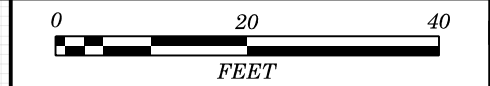


150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

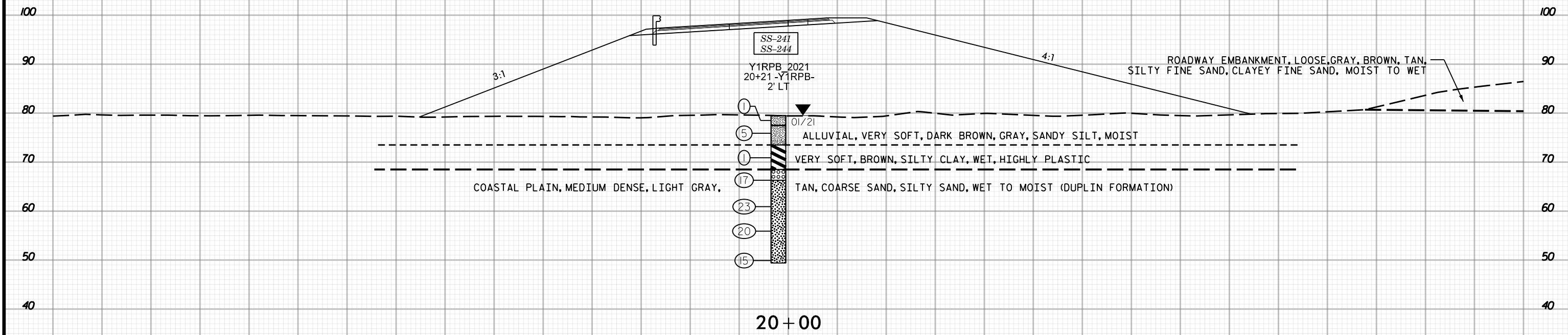
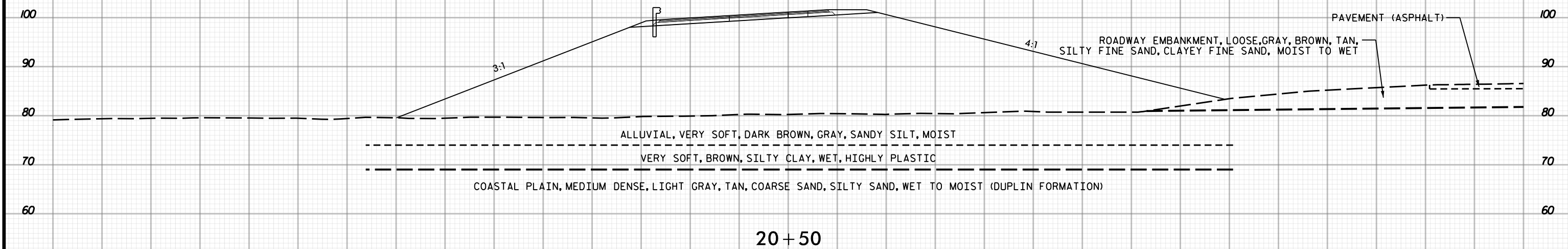


-YIRPB-

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

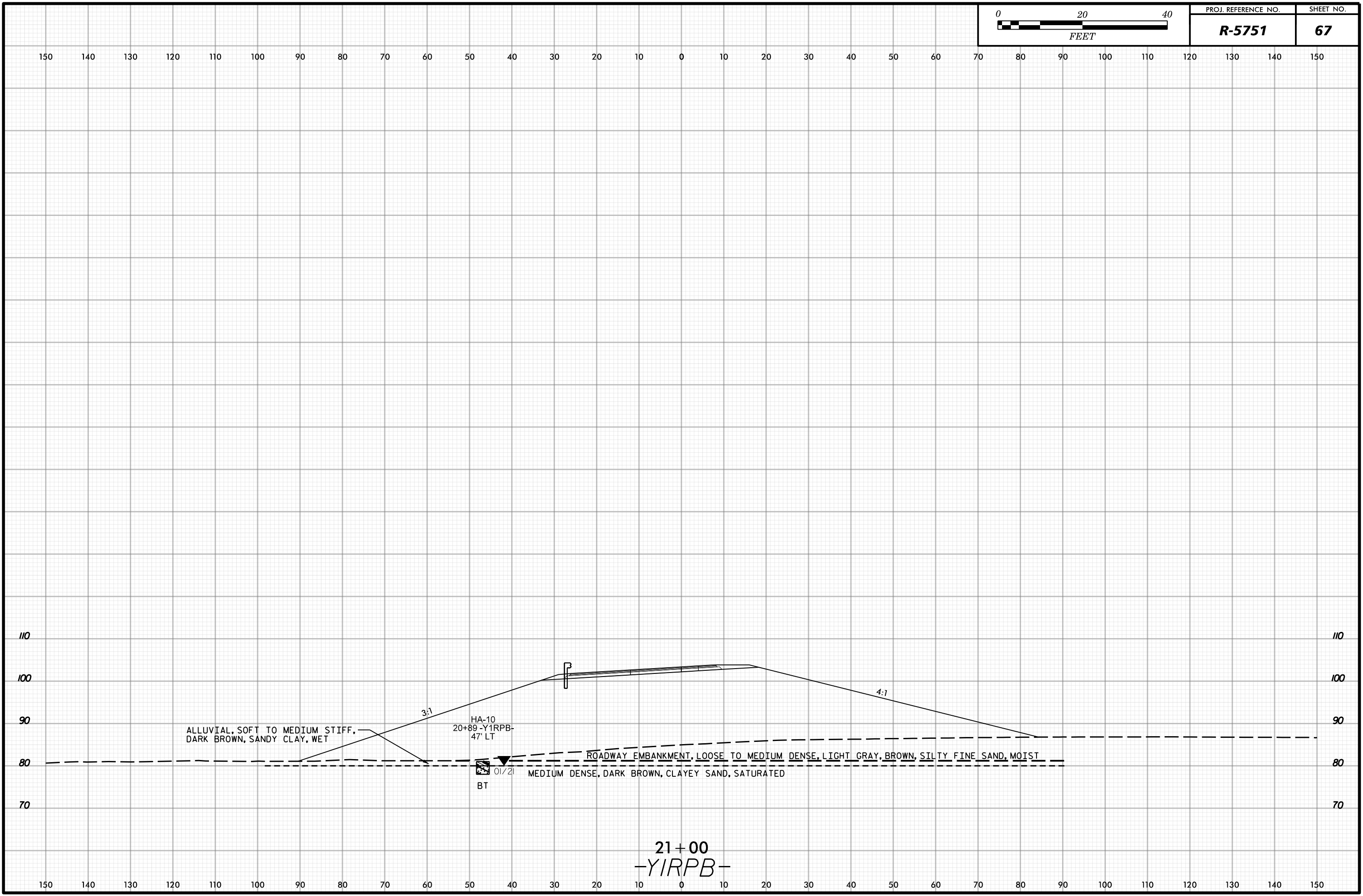
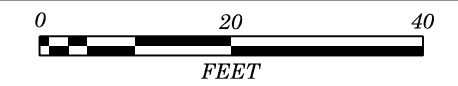


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-Y1RPB-

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



ALLUVIAL, SOFT TO MEDIUM STIFF,  
DARK BROWN, SANDY CLAY, WET

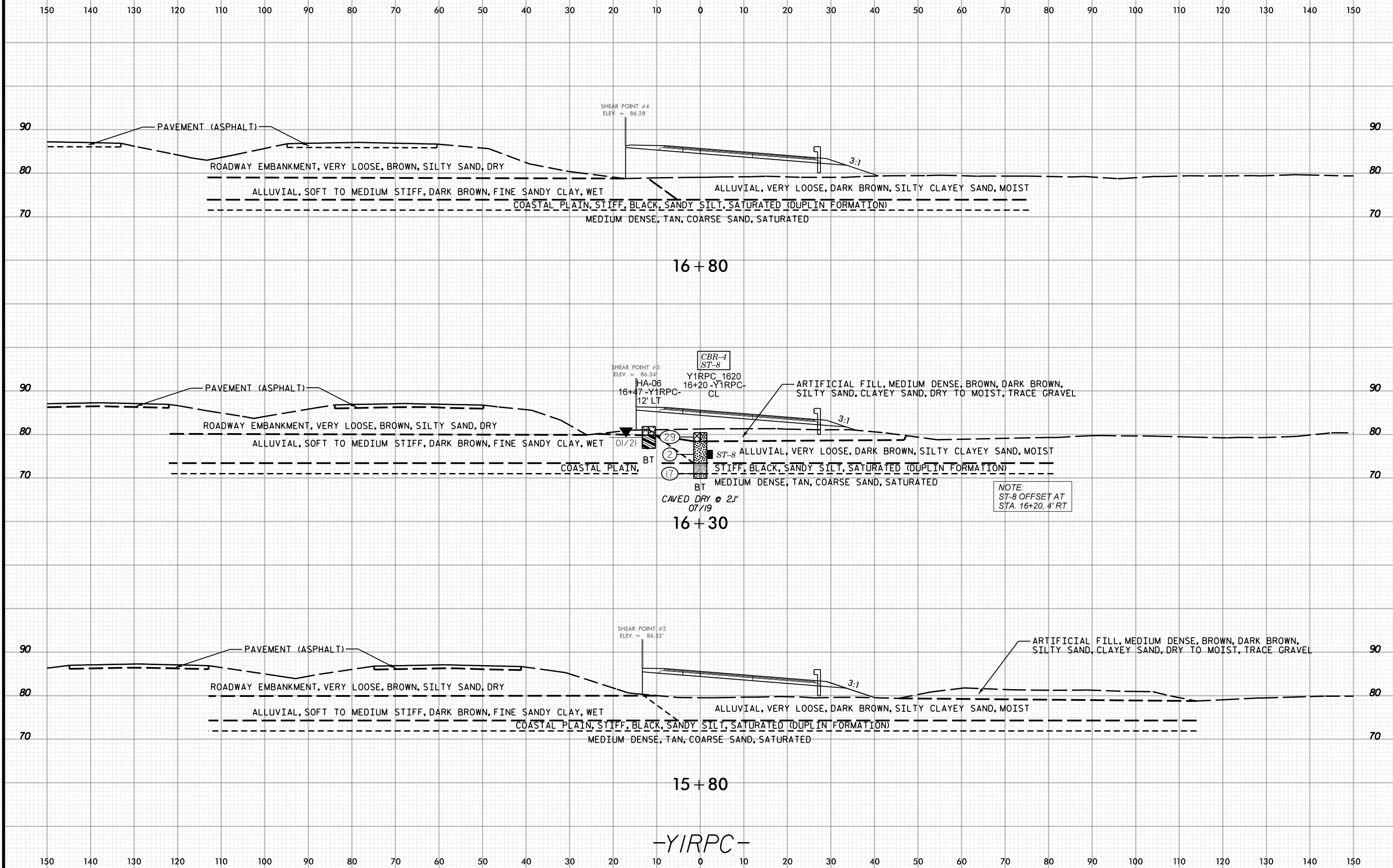
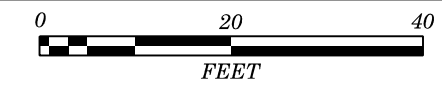
HA-10  
20+89-Y1RPB-  
47' LT

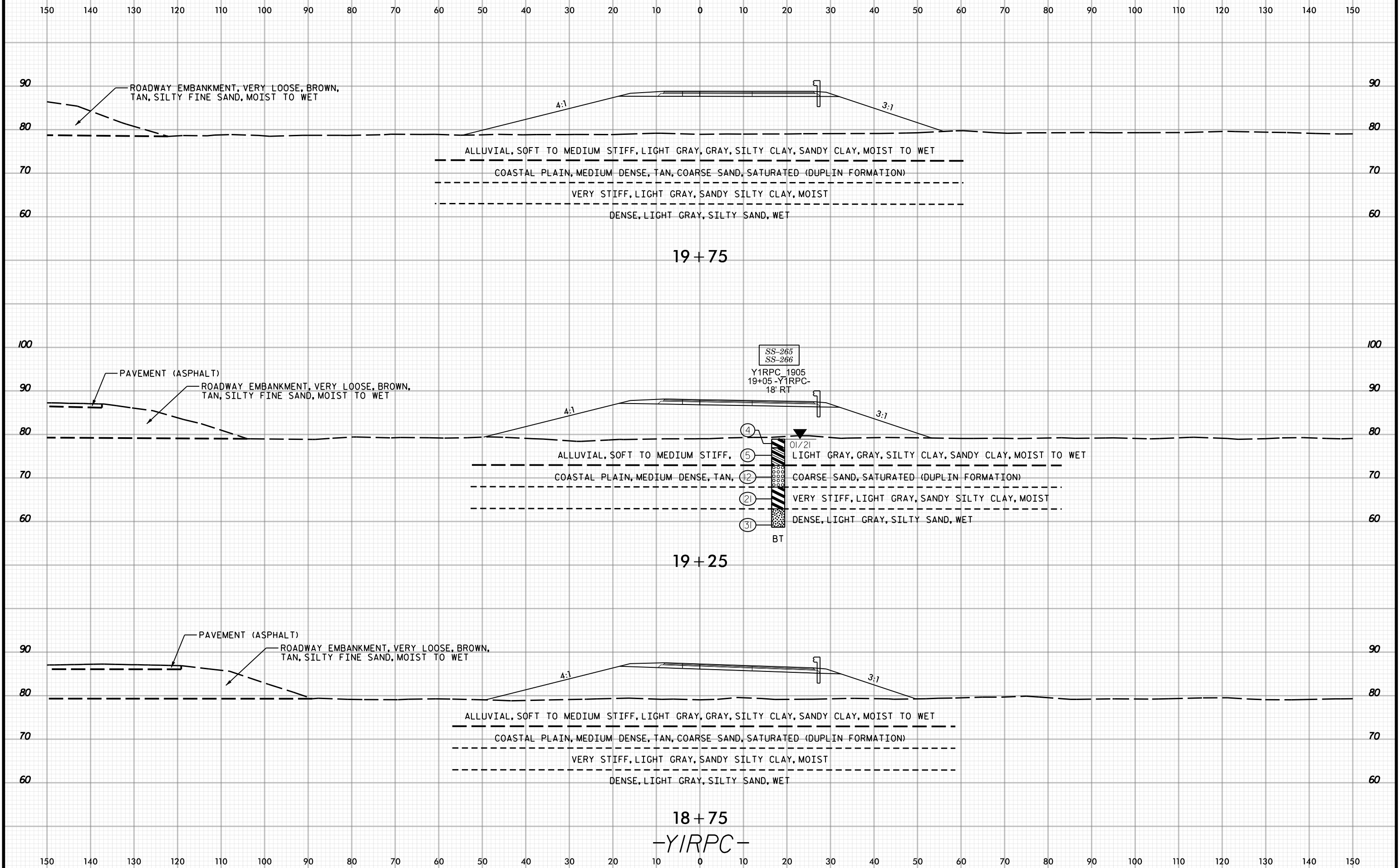
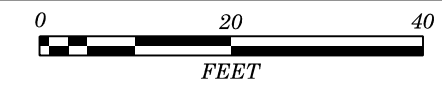
ROADWAY EMBANKMENT, LOOSE TO MEDIUM DENSE, LIGHT GRAY, BROWN, SILTY FINE SAND, MOIST

MEDIUM DENSE, DARK BROWN, CLAYEY SAND, SATURATED

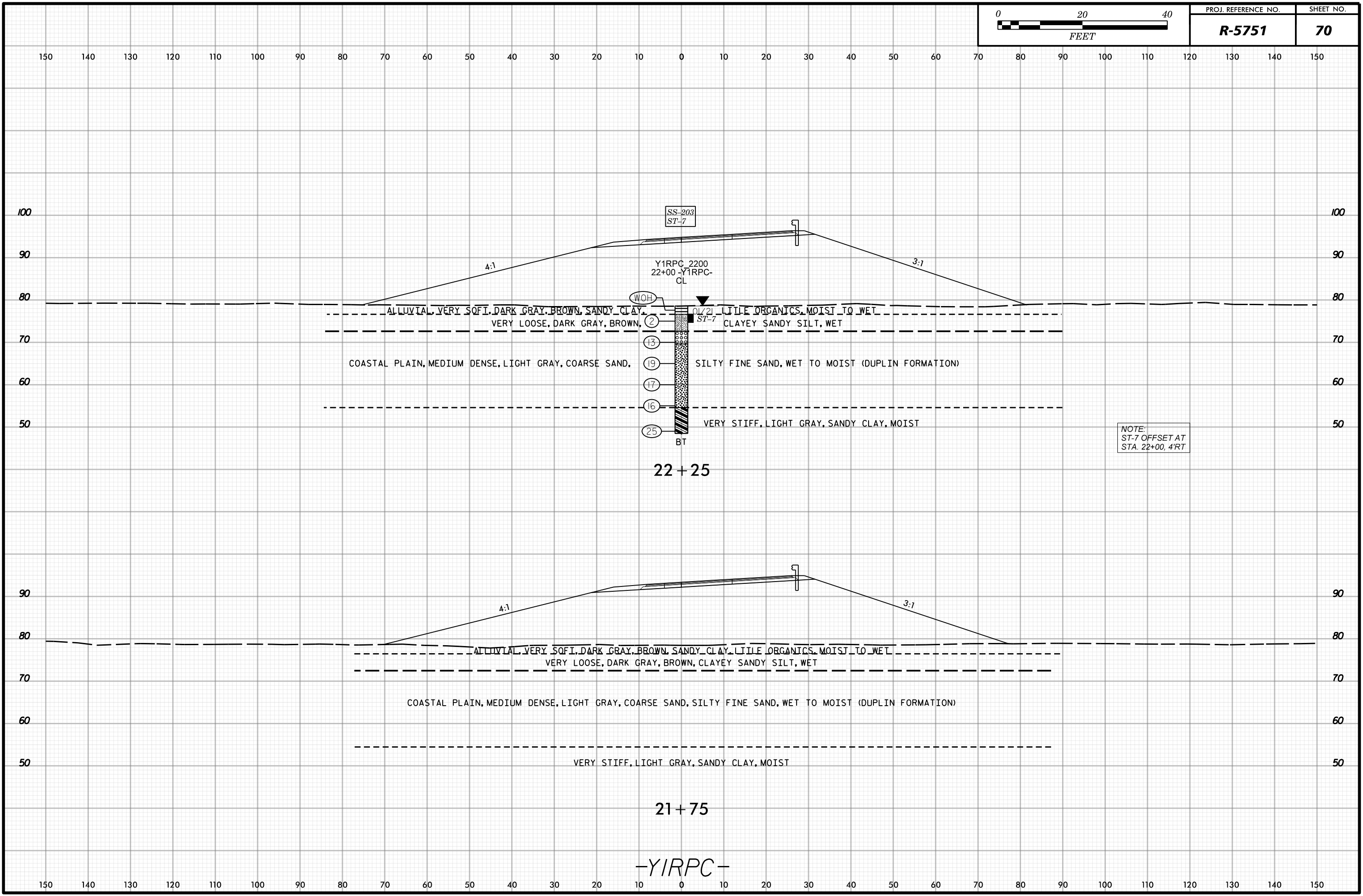
BT

21+00  
-Y1RPB-

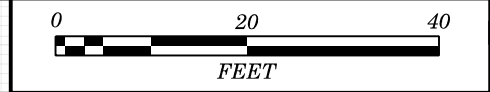




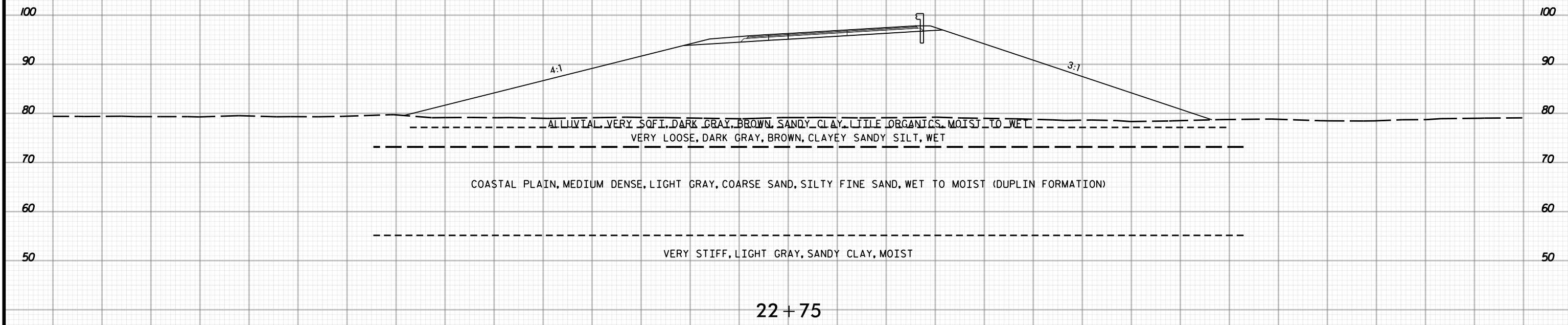
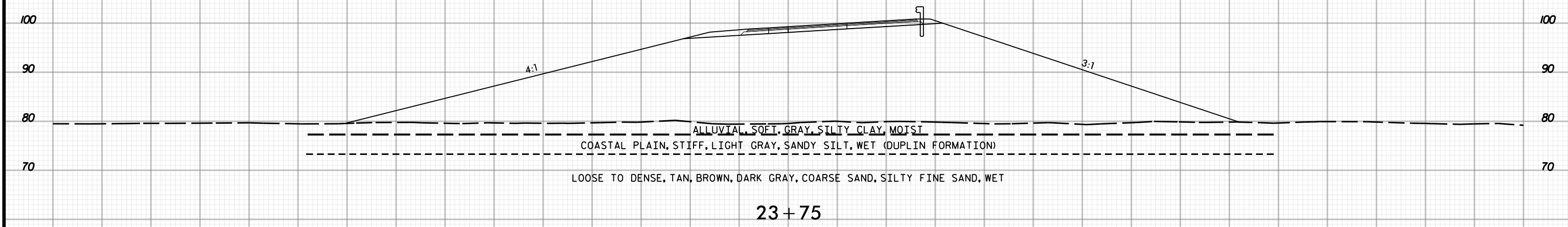




-Y1RPC-

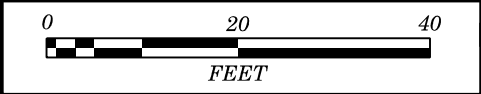


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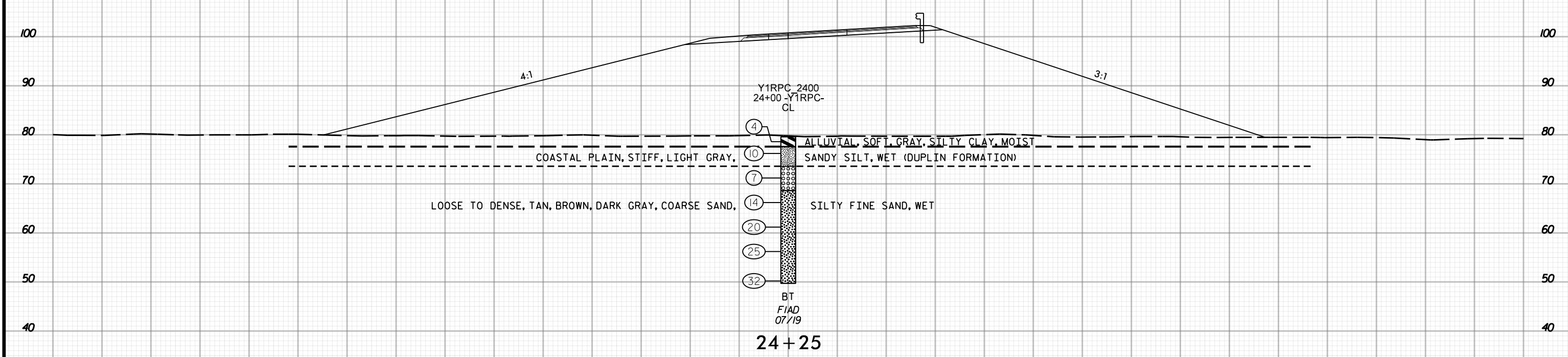


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-YIRPC-

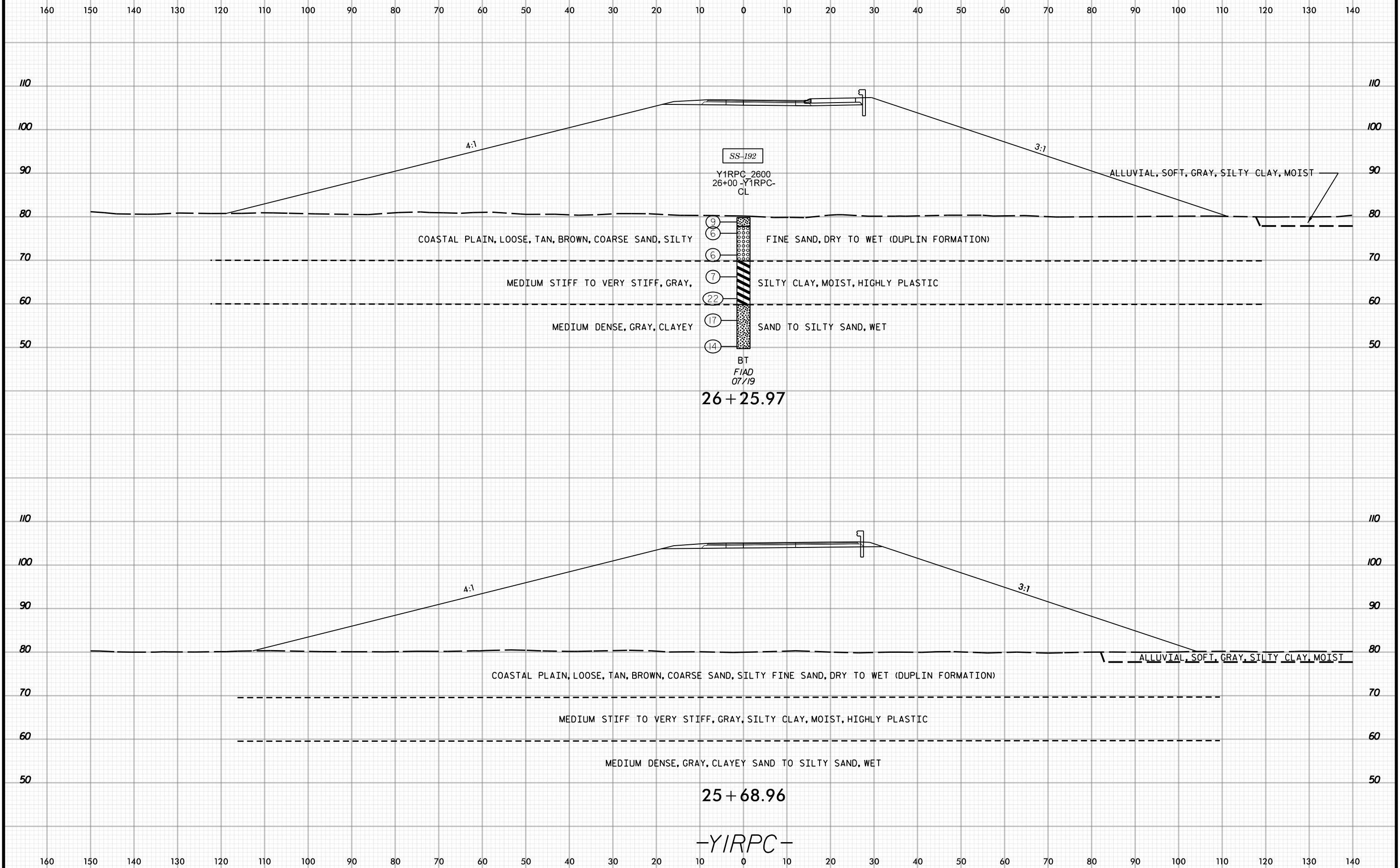
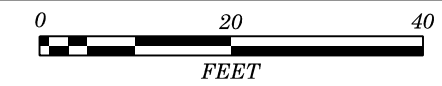


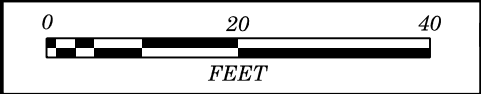
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150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

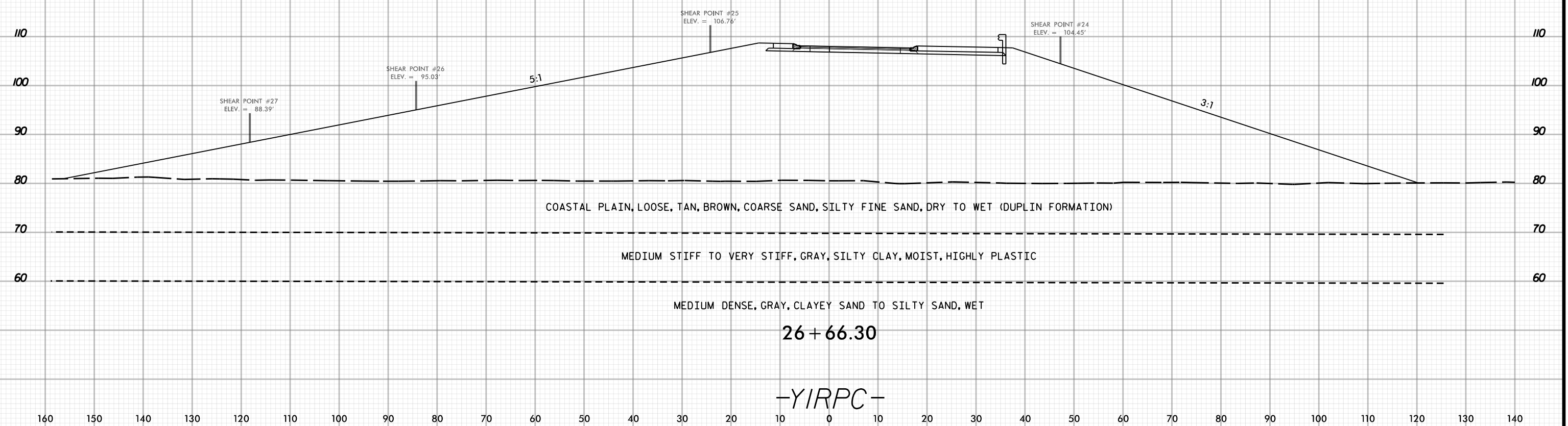
-Y1RPC-



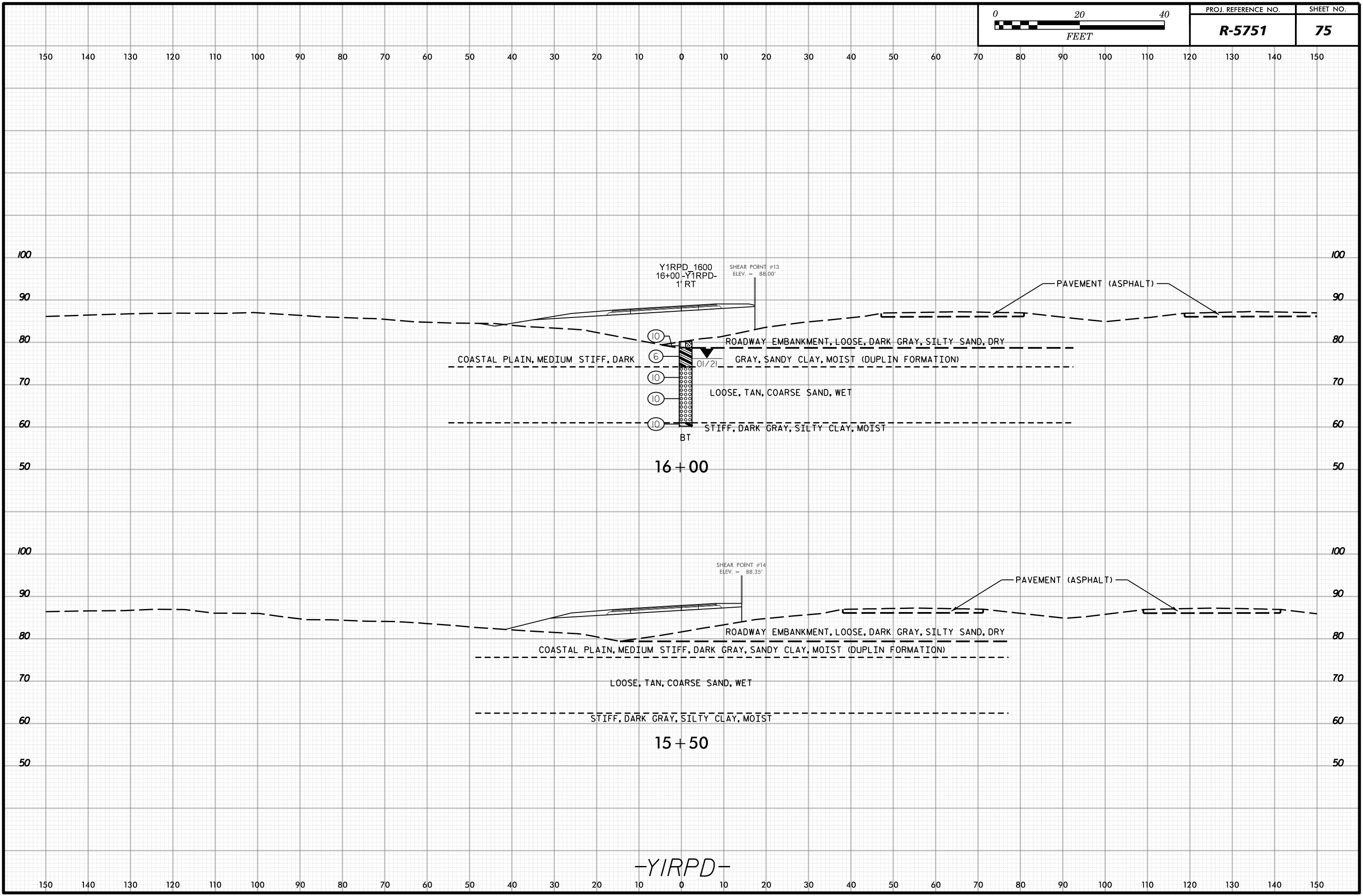


PROJ. REFERENCE NO.	SHEET NO.
<b>R-5751</b>	<b>74</b>

160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140

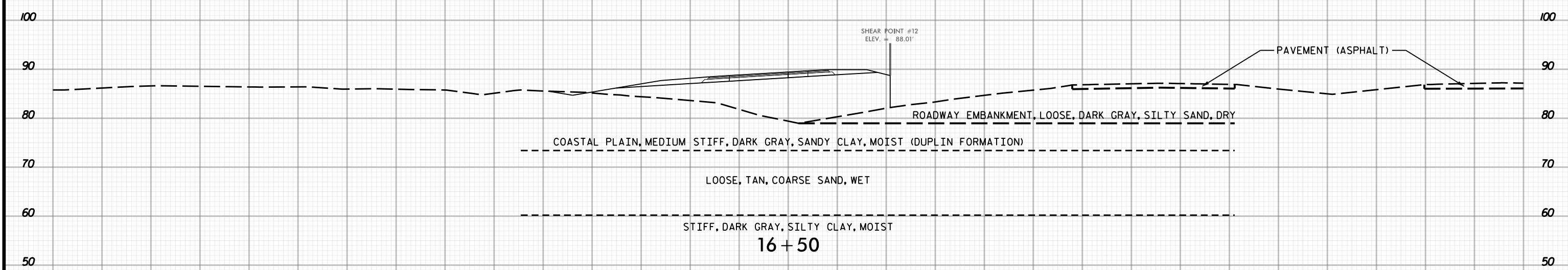
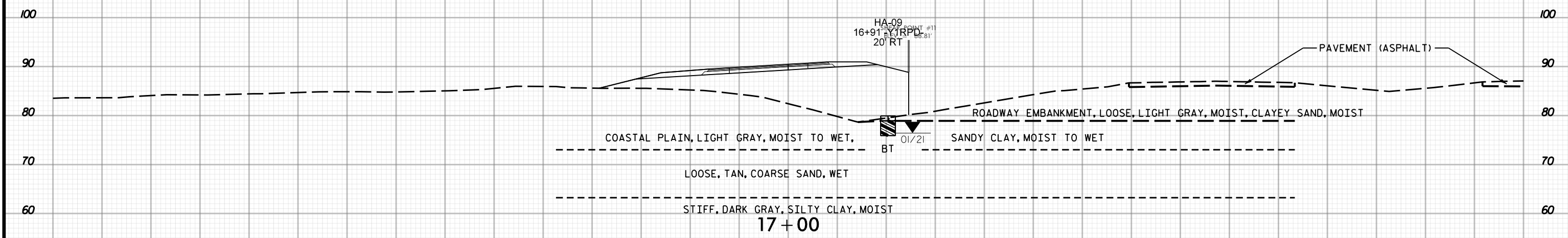


160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140





150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

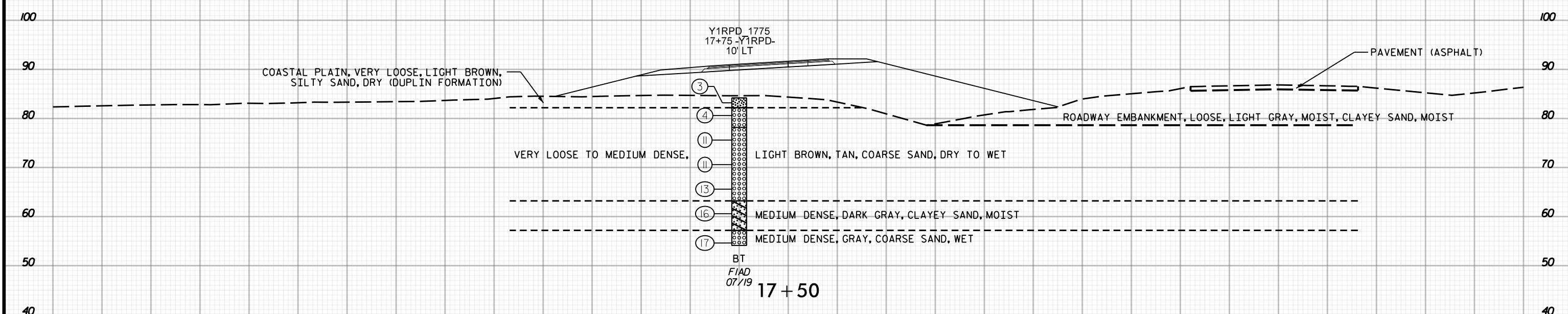
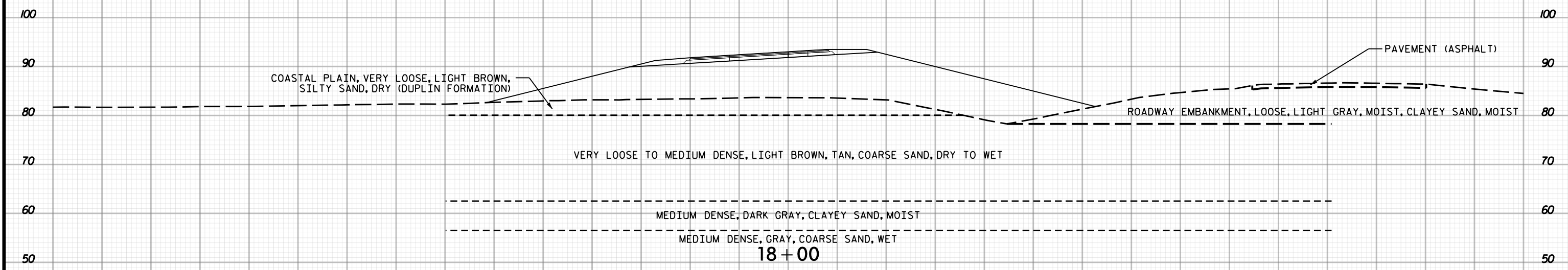


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-YIRPD-



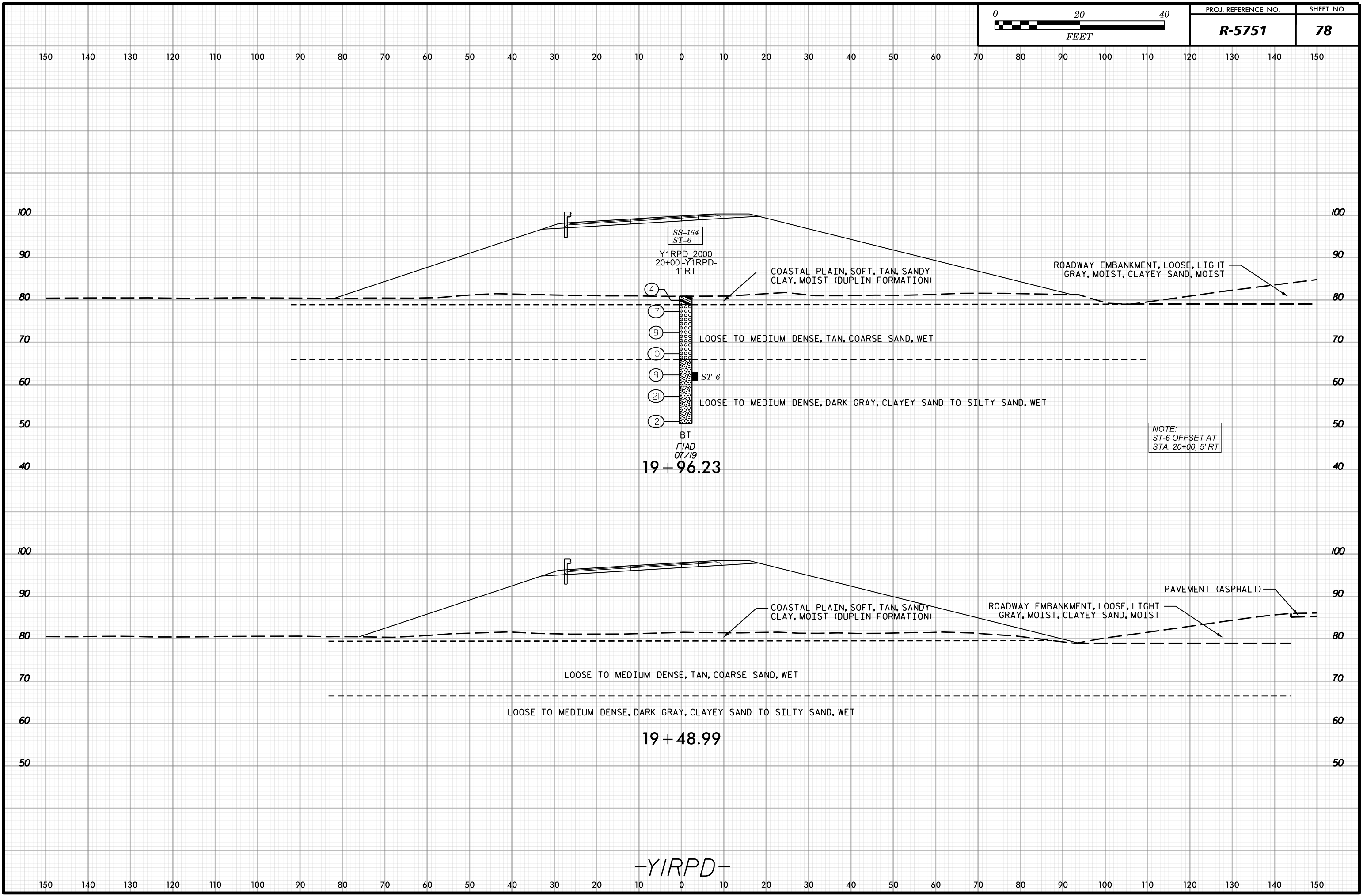
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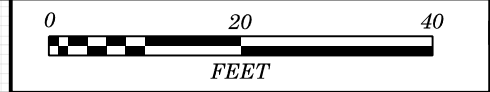
-YIRPD-

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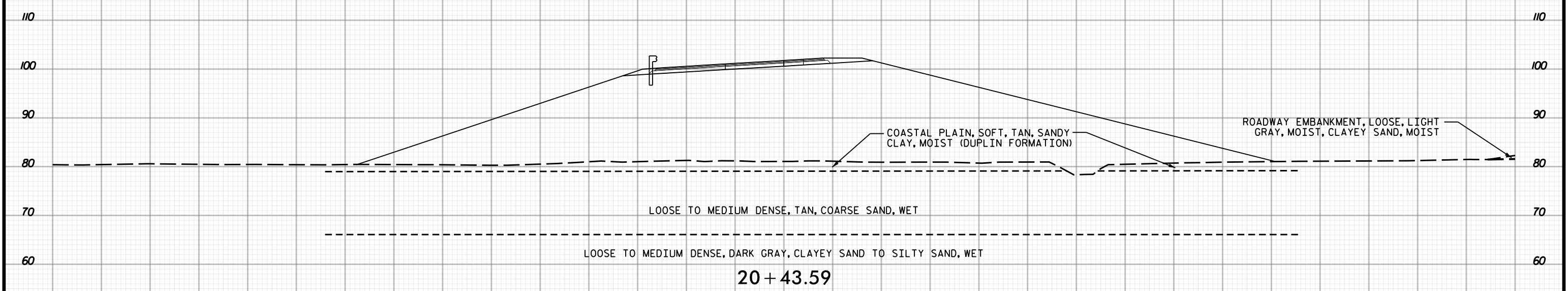
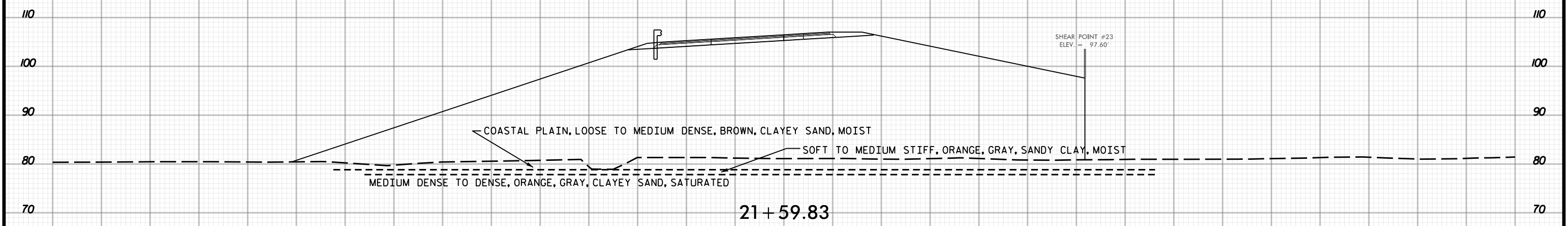


-Y1RPD-



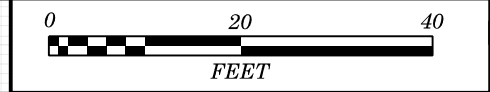
PROJ. REFERENCE NO.	SHEET NO.
<b>R-5751</b>	<b>79</b>

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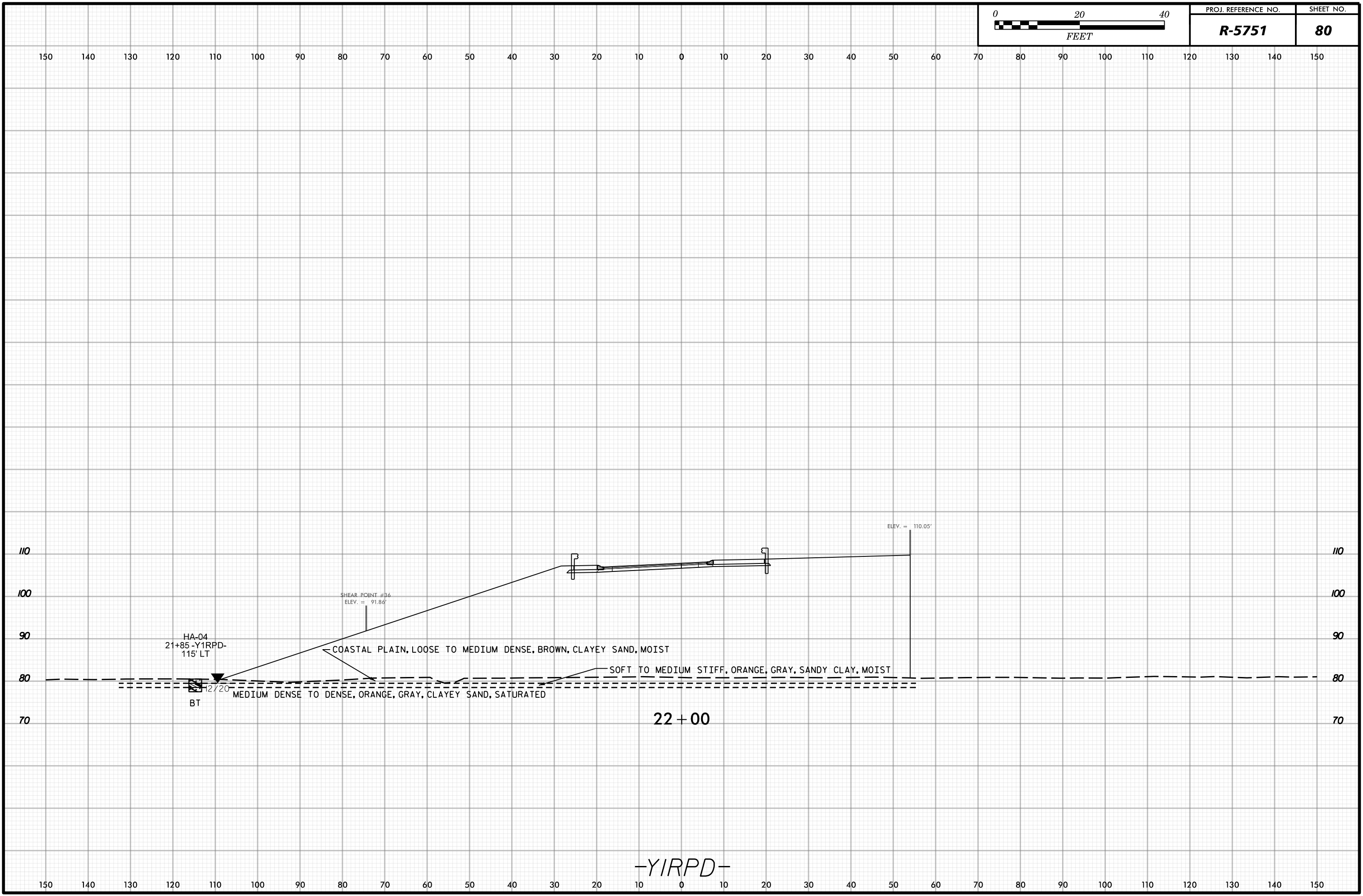


-YIRPD-

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



PROJ. REFERENCE NO.	SHEET NO.
<b>R-5751</b>	<b>80</b>



HA-04  
21+85-YIRPD-  
115' LT

SHEAR POINT #36  
ELEV. = 91.86'

COASTAL PLAIN, LOOSE TO MEDIUM DENSE, BROWN, CLAYEY SAND, MOIST

SOFT TO MEDIUM STIFF, ORANGE, GRAY, SANDY CLAY, MOIST

MEDIUM DENSE TO DENSE, ORANGE, GRAY, CLAYEY SAND, SATURATED

22 + 00

-YIRPD-

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT  
SUBSURFACE INVESTIGATION

APPENDIX A

LABORATORY TESTING SUMMARY  
CONSOLIDATION TEST RESULTS  
CBR - PROCTOR TEST RESULTS

REFERENCE: R-5751

PROJECT: 53087.1.1

Prepared in the Office of:

**Terracon**  
Consulting Engineers and Scientists

2701 WESTPORT ROAD 28208  
CHARLOTTE, NORTH CAROLINA  
NC REGISTERED ENGINEERING FIRM: F-0869  
NC REGISTERED GEOLOGIC FIRM: C-367

**NCDOT LABORATORY TESTING SUMMARY**

PROJECT NUMBER: 53087.1.1

TIP: R-5751

COUNTY: Robeson

DESCRIPTION: US 74 from NC 72/NC 130 Upgrade At-Grade Intersection to Interchange

Sample No.	Alignment	Station	Offset (feet)	Depth Interval (feet)	AASHTO Class.	L.L.	P.I.	% by Weight				% Retained #4 Sieve	% Passing (sieves)			% Moisture	% Organic
								Coarse Sand	Fine Sand	Silt	Clay		#10	#40	#200		
SS-11	-Y1RPA-	23+70	CL	2.7-4.2	-	-	-	-	-	-	-	-	-	-	-	18.5	-
SS-12	-Y1RPA-	23+70	CL	7.7-9.2	-	-	-	-	-	-	-	-	-	-	-	20.6	-
SS-17	-Y1C-	48+00	CL	0.0-1.5	A-4(1)	23	8	20.3	40.5	18.9	20.3	0	100	89	45	20.3	2.8
SS-21	-Y1C-	48+00	CL	17.8-19.3	A-2-4(0)	NP	NP	76.8	12.5	6.4	4.3	7	95	55	11	24.7	1.3
SS-24	-Y1C-	46+00	CL	7.6-9.1	-	-	-	-	-	-	-	-	-	-	-	17.9	-
SS-30	-Y1C-	44+00	CL	2.8-4.3	-	-	-	-	-	-	-	-	-	-	-	19.6	-
SS-31	-Y1C-	44+00	CL	8.8-10.3	-	-	-	-	-	-	-	-	-	-	-	20.1	-
SS-32	-Y1C-	44+00	CL	13.8-15.3	A-1-b(0)	NP	NP	83.5	14.0	2.0	0.5	3	91	35	3	19.8	-
SS-38	-Y1C-	42+20	CL	7.3-8.8	-	-	-	-	-	-	-	-	-	-	-	17.4	-
SS-39	-Y1C-	42+20	CL	12.3-13.8	A-1-b(0)	NP	NP	93.0	5.5	1.4	0.5	1	99	42	2	22.8	-
SS-40	-Y1C-	42+20	CL	17.3-18.8	-	-	-	-	-	-	-	-	-	-	-	20.3	-
SS-42	-Y1C-	42+20	CL	27.3-28.8	A-2-6(0)	4	26	57.1	19.3	19.3	9.6	14	1	99	24	20.4	-
SS-64	-Y1B-	40+40	CL	7.7-9.2	A-1-b(0)	NP	NP	83.1	11.4	3.5	2.0	1	95	35	6	20.1	-
SS-66	-Y1B-	40+40	CL	17.7-19.2	A-6(11)	40	23	22.3	22.2	32.6	22.9	0	100	87	59	22.5	-
SS-67	-Y1B-	40+40	CL	22.7-24.2	A-7-6(4)	41	24	40.6	25.7	27.4	6.3	2	97	72	37	20.9	-
SS-68	-Y1B-	40+40	CL	27.7-29.2	A-2-4(0)	NP	NP	51.0	31.0	7.0	11.0	0	99	83	19	28.4	-
SS-70	-Y1B-	40+40	CL	37.7-29.2	A-3(0)	NP	NP	67.0	24.0	5.4	4.0	1	93	93	10	22.3	-
SS-74	-Y1RPA-	26+00	1 RT	7.5-9.0	-	-	-	-	-	-	-	-	-	-	-	16.7	-
SS-76	-Y1RPA-	26+00	1 RT	17.5-19.0	A-7-6(28)	54	37	3.9	23.6	24.9	47.6	0	97	96	76	49.0	-
SS-83	-Y1RPA-	15+00	1 LT	3.4-4.9	-	-	-	-	-	-	-	-	-	-	-	10.6	-
SS-84	-Y1RPA-	15+00	1 LT	8.4-9.9	-	-	-	-	-	-	-	-	-	-	-	19.1	-
SS-90	-Y1RPA-	19+01	CL	8-9.5	-	-	-	-	-	-	-	-	-	-	-	24.9	-
SS-96	-Y1RPA-	20+95	27 LT	12.7-14.2	-	-	-	-	-	-	-	-	-	-	-	25.3	-
SS-97	-Y1RPA-	20+95	27 LT	17.7-19.2	-	-	-	-	-	-	-	-	-	-	-	20.5	-
SS-157	-Y1A-	32+99	CL	7.7-9.2	-	-	-	-	-	-	-	-	-	-	-	23.9	-
SS-158	-Y1A-	32+99	CL	12.7-14.2	A-1-b(0)	NP	NP	90.2	8.0	1.0	0.8	0	98	29	2	21.8	-
SS-164	-Y1RPD-	20+00	1 RT	7.6-9.1	A-1-b(0)	NP	NP	82.0	15.7	1.6	0.7	0	90	32	2	18.4	-
SS-171	-RCD-	10+00	51 LT	7.6-9.1	A-1-b(0)	NP	NP	83.9	11.6	2.7	1.8	1	94	38	5	20.2	-
SS-176	-RCD-	10+00	51 LT	32.6-34.1	A-2-4(0)	28	8	34.3	43.5	8.2	14.0	0	96	71	26	21.7	-
SS-181	-Y1B-	35+70	CL	7.8-9.3	A-1-b(0)	NP	NP	88.3	11.4	0.3	0.0	0	95	36	1	21.1	-
SS-183	-Y1B-	35+70	CL	17.8-19.3	A-6(5)	36	23	35.1	24.2	16.4	24.3	0	95	78	41	22.6	-
SS-184	-Y1B-	35+70	CL	22.8-24.3	A-2-4(0)	25	5	9.6	66.2	12.2	12.0	0	100	97	27	25.1	-
SS-186	-Y1B-	35+70	CL	32.8-34.3	A-6(5)	33	15	8.5	44.0	26.3	21.2	0	99	96	54	34.4	-
SS-188	-Y1B-	35+70	CL	43.8-45.3	A-7-6(15)	48	32	21.7	24.1	19.4	34.8	0	99	89	59	15.1	-
SS-192	-Y1RPC-	26+00	CL	17.6-19.1	A-7-6(21)	57	34	16.9	15.0	32.2	35.9	0	88	78	66	38.8	-
SS-203	-Y1RPC-	22+00	CL	0.0-1.5	A-6(3)	30	13	32.0	22.1	27.2	18.7	1	96	78	47	39.9	5.9
SS-211	-Y1A-	22+49	60 RT	2.3-3.8	A-6(3)	34	12	24.0	32.8	25.3	17.9	0	100	89	47	45.0	5.8
SS-219	-Y1RPC-	14+25	5 RT	3.8-5.3	-	-	-	-	-	-	-	-	-	-	-	17.6	-
SS-220	-Y1RPC-	14+25	5 RT	8.8-10.3	-	-	-	-	-	-	-	-	-	-	-	18.8	-
SS-225	-L-	32+48	77 LT	3.4-4.9	A-7-6(7)	46	17	33.3	14.0	23.9	28.8	0	100	84	54	50.8	-

NP - NON-PLASTIC

Certified Lab Technician Signature

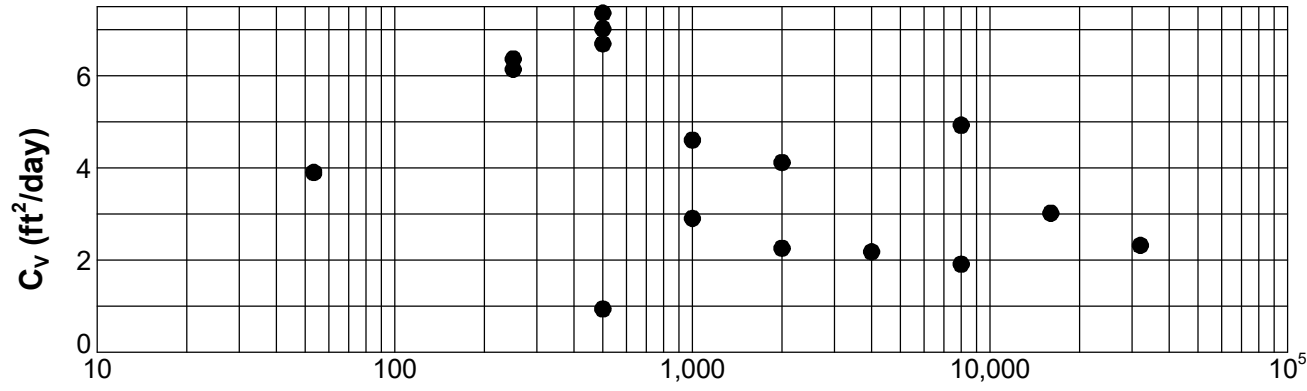
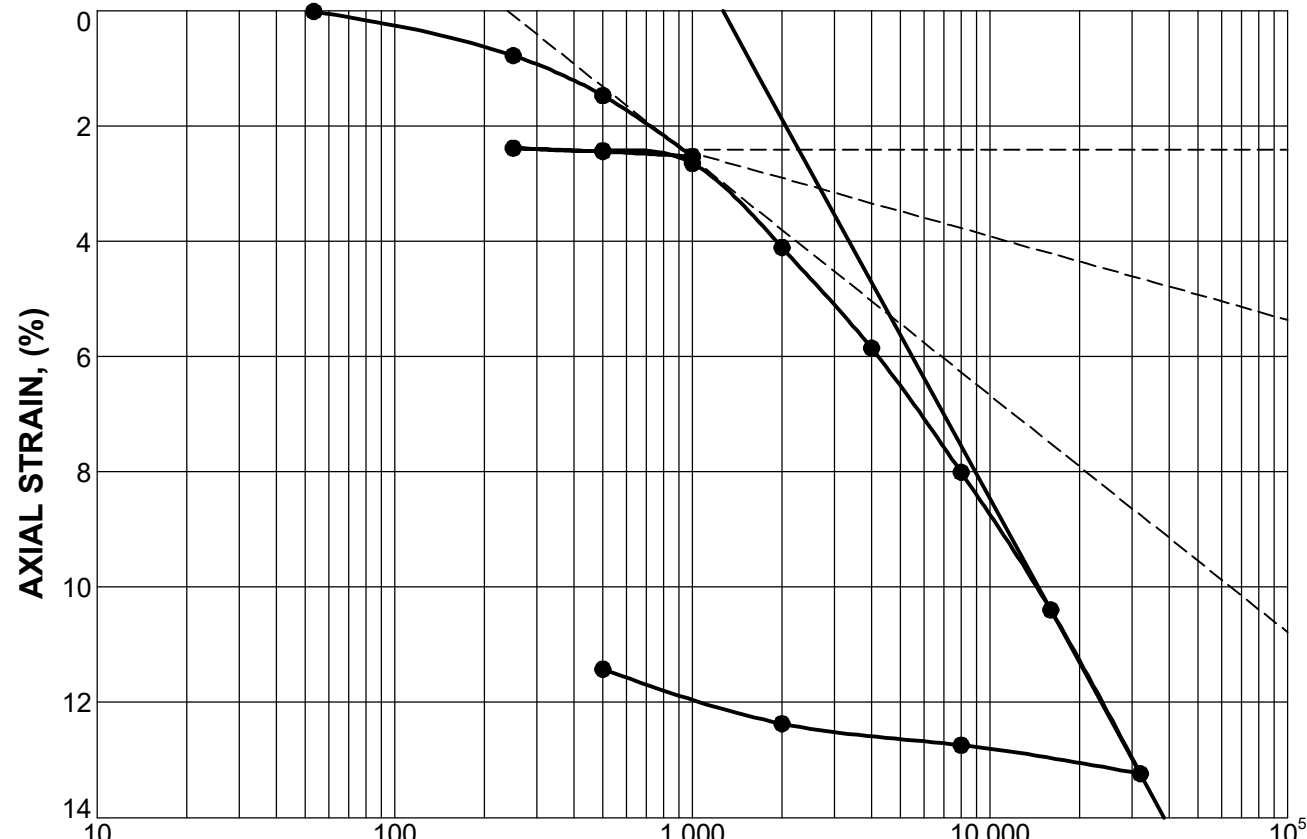
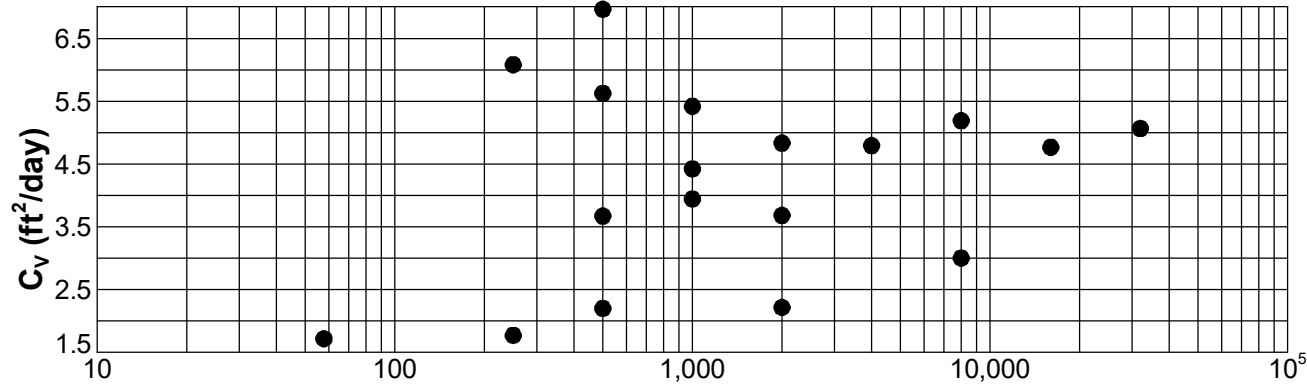
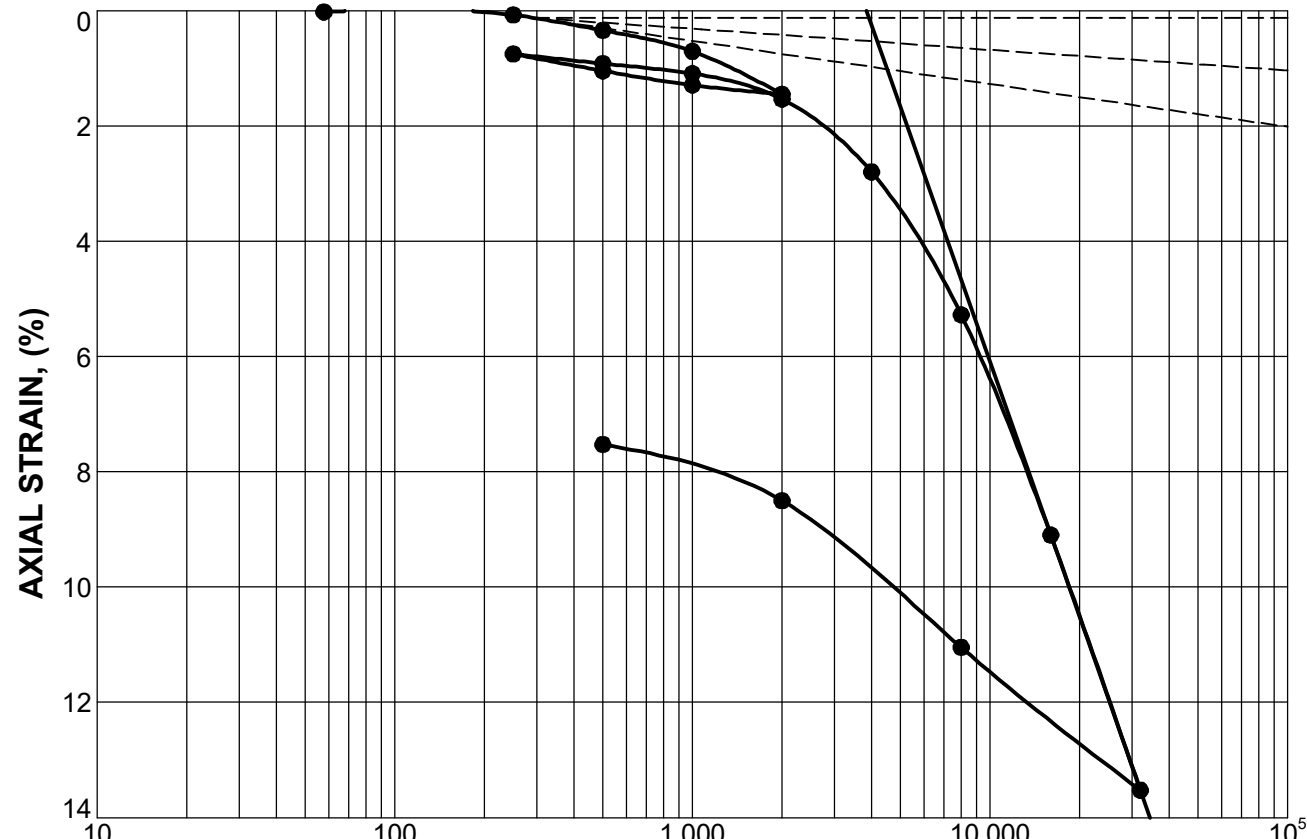
126-01-0910

Certification Number



LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CONS\_LOAD\_DEF\_PROP\_STRESS-STRAIN\_CV\_R5751\_GEO\_TERRACONLIBRARY.GPJ TERRACON\_DATATEMPLATE.GDT\_4/13/20

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CONS\_LOAD\_DEF\_PROP\_STRESS-STRAIN\_CV\_R5751\_GEO\_TERRACONLIBRARY.GPJ TERRACON\_DATATEMPLATE.GDT\_4/13/20



Natural		Initial Dry Density (pcf)	LL	PI	Sp. Gr.	Overburden (psf)	P <sub>c</sub> (psf)	C <sub>c</sub> (%/log stress)	C <sub>r</sub> (%/log stress)	Initial Void Ratio
Saturation	Moisture									
90.1 %	44.9 %	72.1	60	42	2.72			14.713	0.779	1.358

MATERIAL DESCRIPTION								USCS	AASHTO
Gray fat CLAY								CH	A-7-6

NOTES: Percent Passing #200 Sieve= 89.3%

Borehole: B1-C Depth: 22 ft Specimen #: 4

PROJECT: ORRUM	 2701 Westport Rd Charlotte, NC	PROJECT NUMBER: 71195028
SITE: Robeson County Orrum, NC		CLIENT: NCDOT Charlotte, NC
		EXHIBIT: B-1

Natural		Initial Dry Density (pcf)	LL	PI	Sp. Gr.	Overburden (psf)	P <sub>c</sub> (psf)	C <sub>c</sub> (%/log stress)	C <sub>r</sub> (%/log stress)	Initial Void Ratio
Saturation	Moisture									
92.8 %	29.3 %	91.6	26	11	2.74			9.444	0.240	0.865

MATERIAL DESCRIPTION								USCS	AASHTO
SANDY LEAN CLAY								CL	A-6

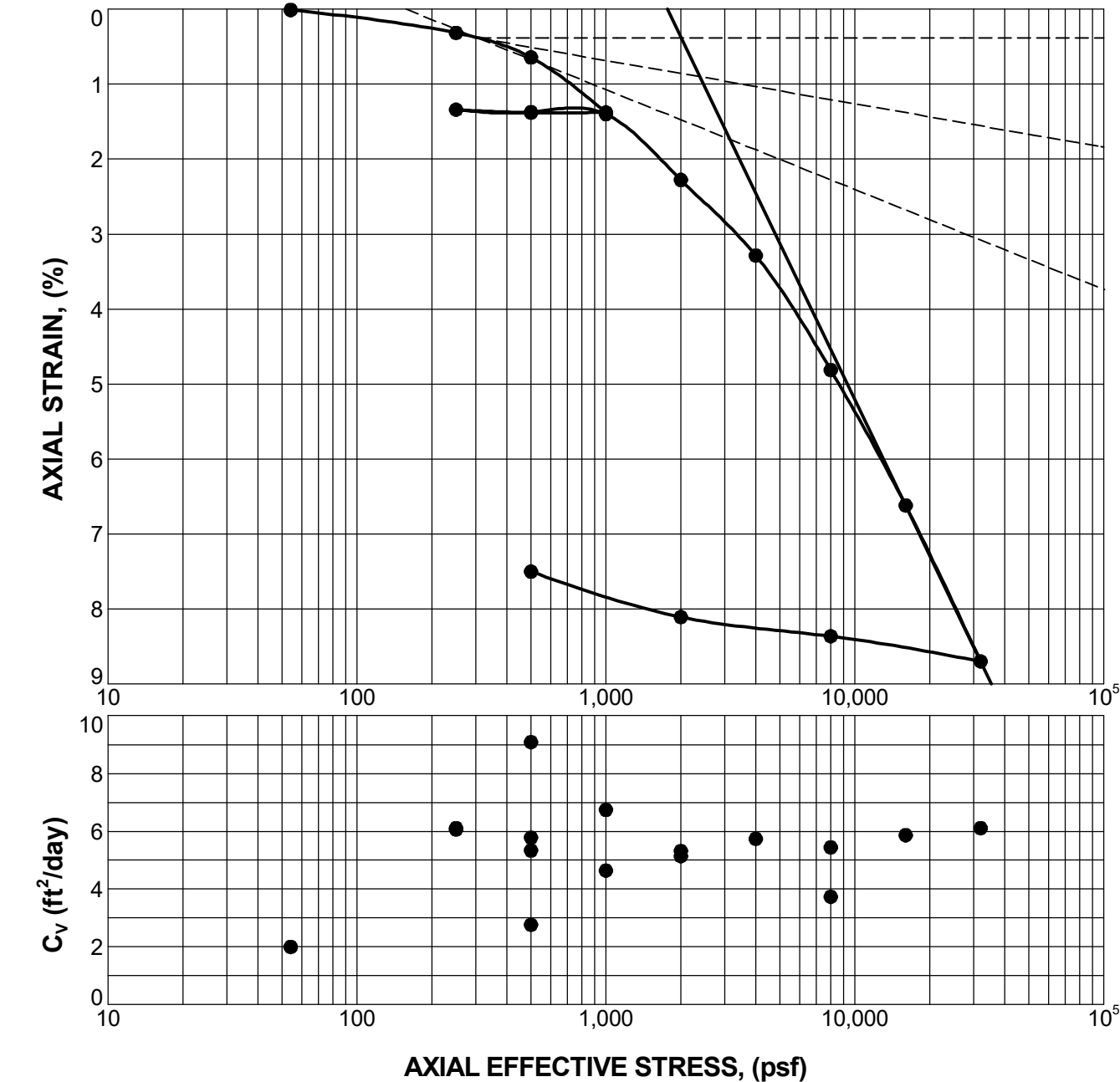
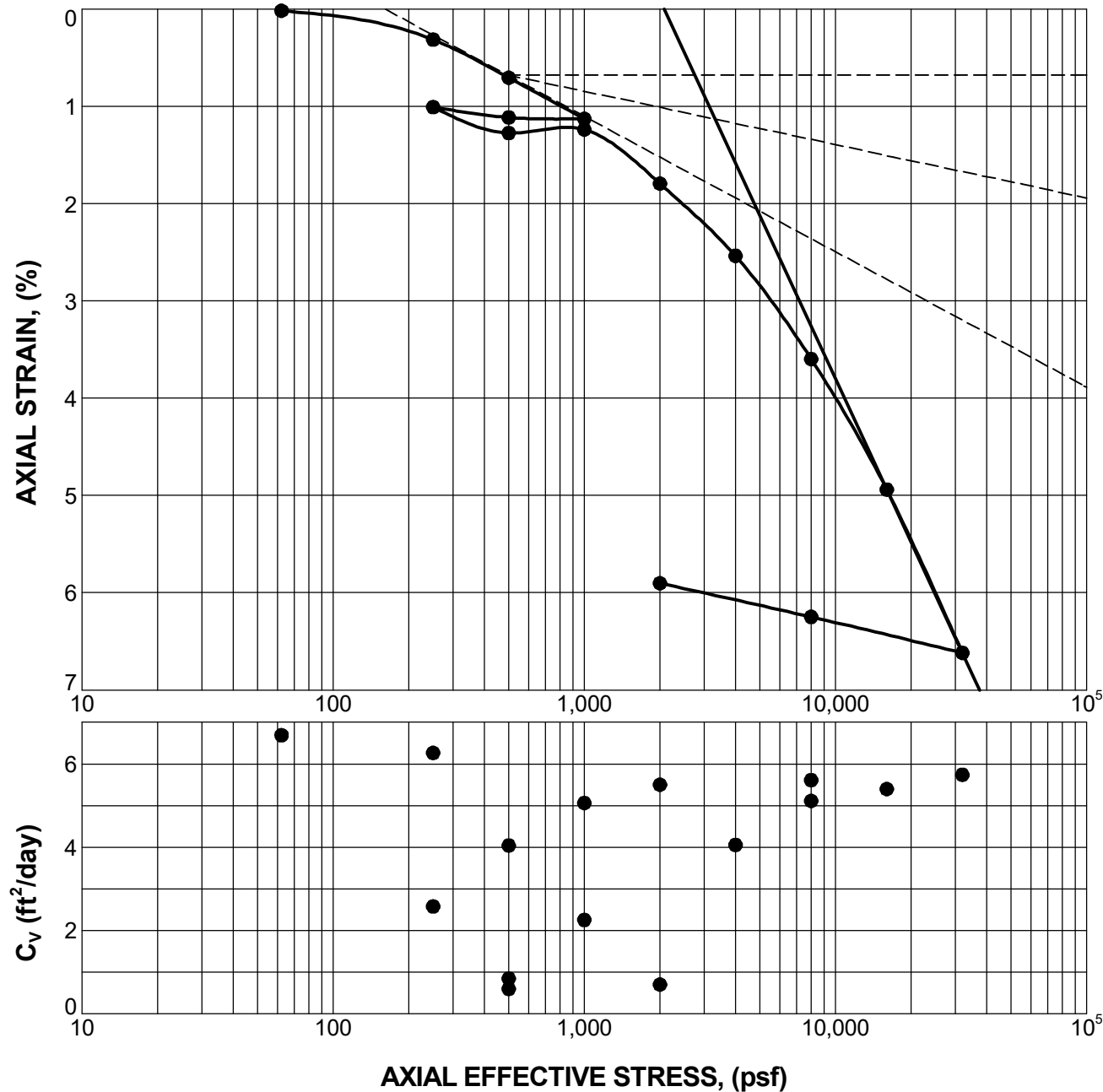
NOTES:

Borehole: Y1A\_2600 Depth: 1 ft Specimen #: 10

PROJECT: ORRUM	 2701 Westport Rd Charlotte, NC	PROJECT NUMBER: 71195028
SITE: Robeson County Orrum, NC		CLIENT: NCDOT Charlotte, NC
		EXHIBIT: B-2

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CONS\_LOAD\_DEF\_PROP\_STRESS-STRAIN\_CV\_R5751\_GEO\_TERRACONLIBRARY.GPJ\_TERRACON\_DATATEMPLATE.GDT\_4/13/20

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CONS\_LOAD\_DEF\_PROP\_STRESS-STRAIN\_CV\_R5751\_GEO\_TERRACONLIBRARY.GPJ\_TERRACON\_DATATEMPLATE.GDT\_4/13/20



Natural		Initial Dry Density (pcf)	LL	PI	Sp. Gr.	Overburden (psf)	P <sub>c</sub> (psf)	C <sub>c</sub> (%/log stress)	C <sub>r</sub> (%/log stress)	Initial Void Ratio
Saturation	Moisture									
81.0 %	19.8 %	100.8	NP	NP	2.67			5.578	0.201	0.654

MATERIAL DESCRIPTION								USCS	AASHTO
SILTY SAND								SM	A-2-4

NOTES:

**Borehole: Y1RPA\_1901 Depth: 3 ft Specimen #: 3**

PROJECT: ORRUM	 2701 Westport Rd Charlotte, NC	PROJECT NUMBER: 71195028
SITE: Robeson County Orrum, NC		CLIENT: NCDOT Charlotte, NC
		EXHIBIT: B-3

Natural		Initial Dry Density (pcf)	LL	PI	Sp. Gr.	Overburden (psf)	P <sub>c</sub> (psf)	C <sub>c</sub> (%/log stress)	C <sub>r</sub> (%/log stress)	Initial Void Ratio
Saturation	Moisture									
80.8 %	13.3 %	114.9	20	8	2.64			6.914	0.059	0.435

MATERIAL DESCRIPTION								USCS	AASHTO
CLAYEY SAND								SC	A-2-4

NOTES:

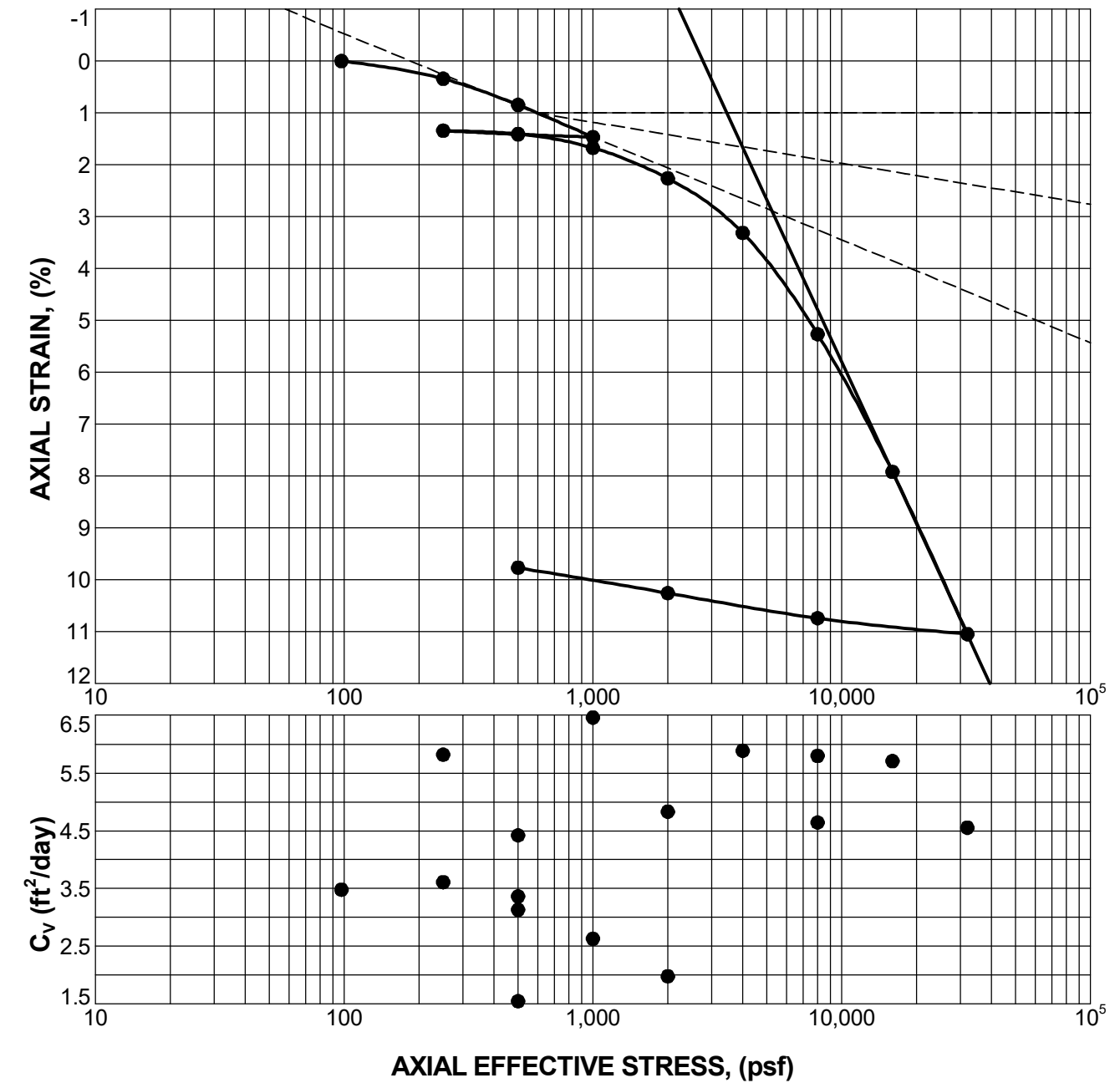
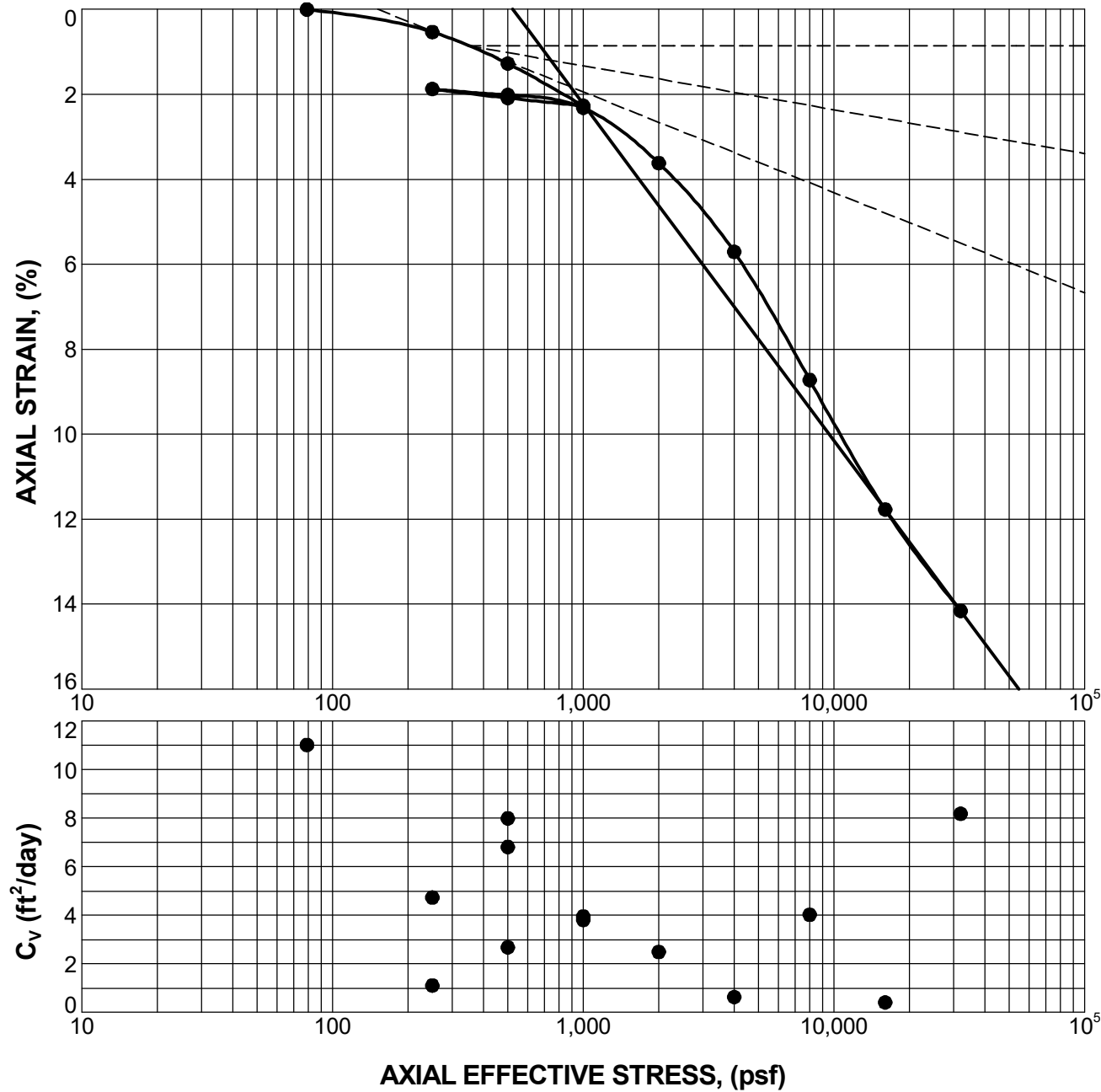
**Borehole: Y1RPA\_2600 Depth: 2 ft Specimen #: 2**

PROJECT: ORRUM	 2701 Westport Rd Charlotte, NC	PROJECT NUMBER: 71195028
SITE: Robeson County Orrum, NC		CLIENT: NCDOT Charlotte, NC
		EXHIBIT: B-4



LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CONS\_LOAD\_DEF\_PROP\_STRESS-STRAIN\_CV\_R5751\_GEO\_TERRACONLIBRARY.GPJ\_TERRACON\_DATATEMPLATE.GDT\_4/13/20

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CONS\_LOAD\_DEF\_PROP\_STRESS-STRAIN\_CV\_R5751\_GEO\_TERRACONLIBRARY.GPJ\_TERRACON\_DATATEMPLATE.GDT\_4/13/20



Natural		Initial Dry Density (pcf)	LL	PI	Sp. Gr.	Overburden (psf)	P <sub>c</sub> (psf)	C <sub>c</sub> (%/log stress)	C <sub>r</sub> (%/log stress)	Initial Void Ratio
Saturation	Moisture									
93.4 %	32.3 %	85.8	38	19	2.62			7.929	0.656	0.904

MATERIAL DESCRIPTION								USCS	AASHTO
SANDY LEAN CLAY								CL	A-6

NOTES:

**Borehole: Y1RPB\_1809 Depth: 2 ft Specimen #: 9**

PROJECT: ORRUM	 2701 Westport Rd Charlotte, NC	PROJECT NUMBER: 71195028
SITE: Robeson County Orrum, NC		CLIENT: NCDOT Charlotte, NC
		EXHIBIT: B-5

Natural		Initial Dry Density (pcf)	LL	PI	Sp. Gr.	Overburden (psf)	P <sub>c</sub> (psf)	C <sub>c</sub> (%/log stress)	C <sub>r</sub> (%/log stress)	Initial Void Ratio
Saturation	Moisture									
92.2 %	25.9 %	92.8	24	6	2.55			10.397	0.205	0.716

MATERIAL DESCRIPTION								USCS	AASHTO
SILTY, CLAYEY SAND								SC-SM	A-2-4

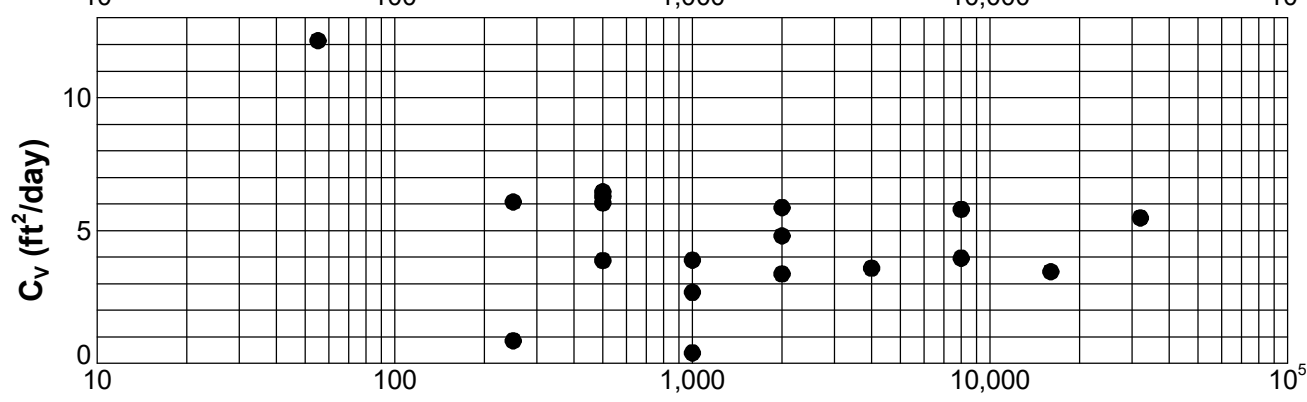
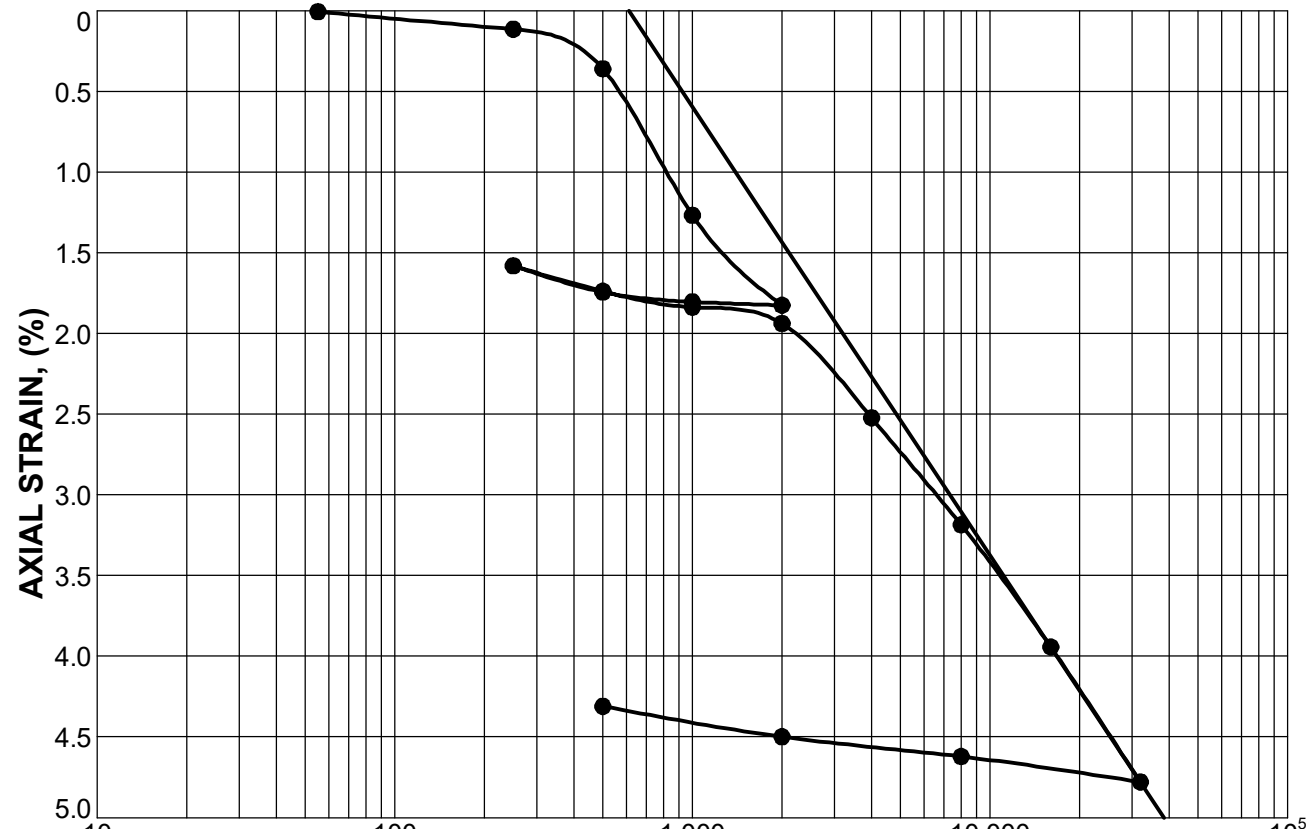
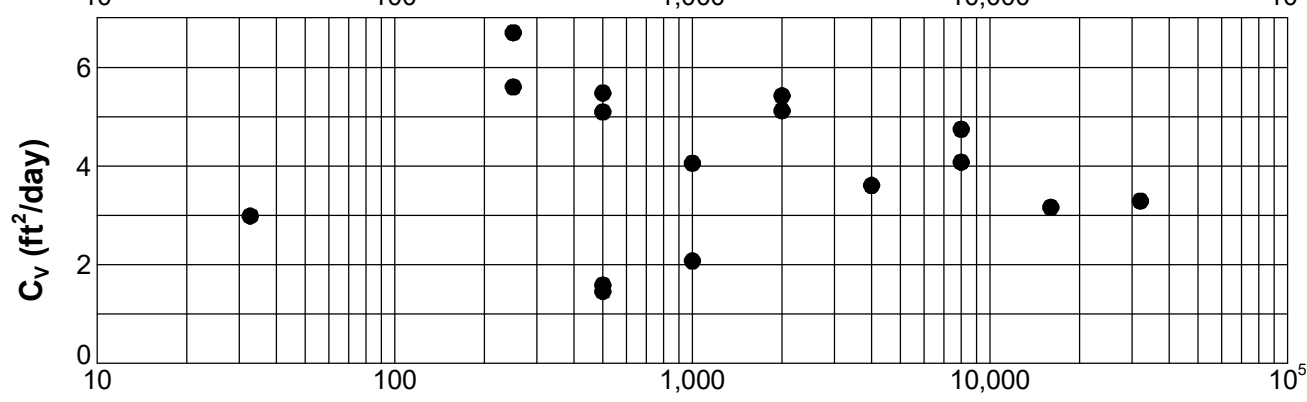
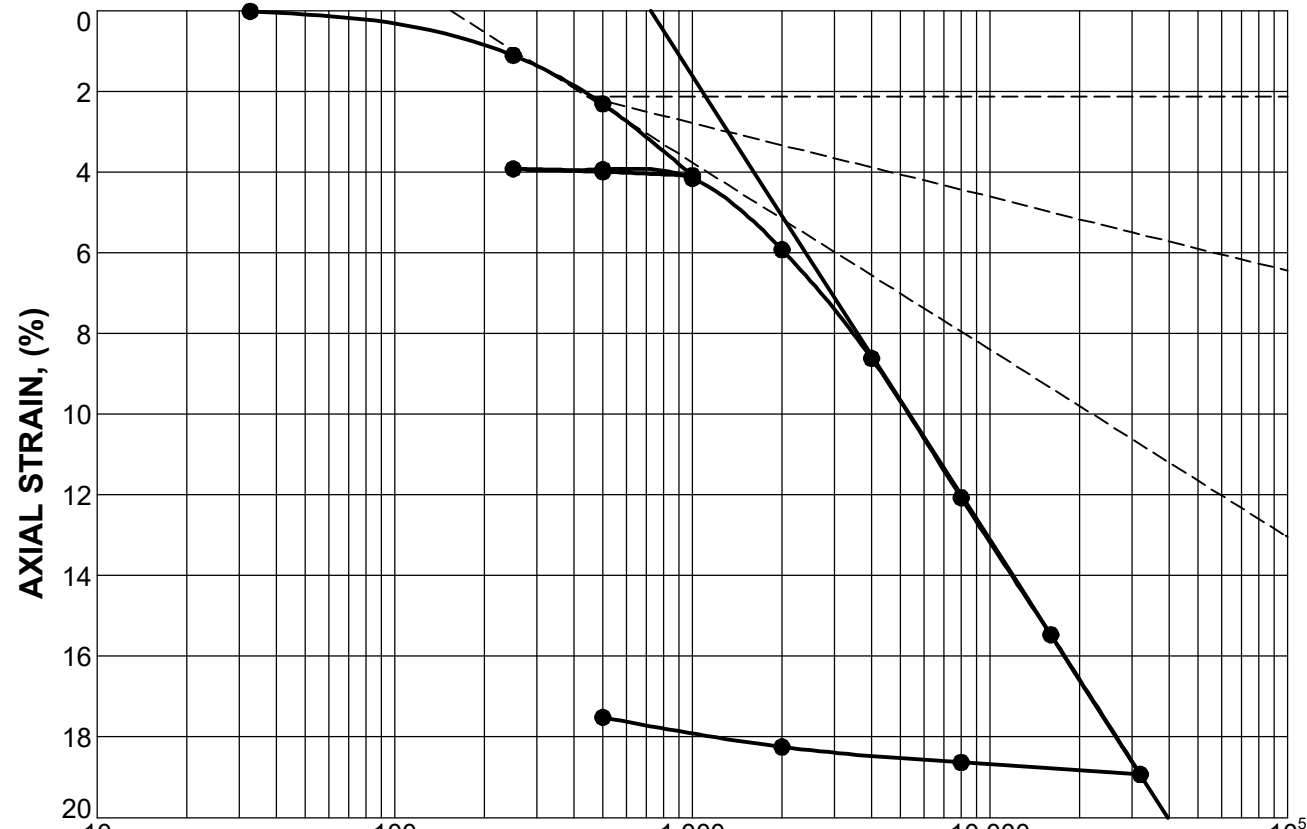
NOTES:

**Borehole: Y1RPC\_1620 Depth: 4 ft Specimen #: 8**

PROJECT: ORRUM	 2701 Westport Rd Charlotte, NC	PROJECT NUMBER: 71195028
SITE: Robeson County Orrum, NC		CLIENT: NCDOT Charlotte, NC
		EXHIBIT: B-6

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CONS\_LOAD\_DEF\_PROP\_STRESS-STRAIN\_CV\_R5751\_GEO\_TERRACONLIBRARY.GPJ\_TERRACON\_DATATEMPLATE.GDT\_4/13/20

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CONS\_LOAD\_DEF\_PROP\_STRESS-STRAIN\_CV\_R5751\_GEO\_TERRACONLIBRARY.GPJ\_TERRACON\_DATATEMPLATE.GDT\_4/13/20



Natural		Initial Dry Density (pcf)	LL	PI	Sp. Gr.	Overburden (psf)	P <sub>c</sub> (psf)	C <sub>c</sub> (%/log stress)	C <sub>r</sub> (%/log stress)	Initial Void Ratio
Saturation	Moisture									
82.4 %	27.6 %	86.8	25	7	2.60			11.513	0.278	0.870

MATERIAL DESCRIPTION								USCS	AASHTO
SILTY, CLAYEY SAND								SC-SM	A-4

NOTES:

**Borehole: Y1RPC-2200 Depth: 2 ft Specimen #:7**

PROJECT: ORRUM	 2701 Westport Rd Charlotte, NC	PROJECT NUMBER: 71195028
SITE: Robeson County Orrum, NC		CLIENT: NCDOT Charlotte, NC
		EXHIBIT: B-7

Natural		Initial Dry Density (pcf)	LL	PI	Sp. Gr.	Overburden (psf)	P <sub>c</sub> (psf)	C <sub>c</sub> (%/log stress)	C <sub>r</sub> (%/log stress)	Initial Void Ratio
Saturation	Moisture									
89.3 %	22.7 %	98.8	NP	NP	2.65			2.781	0.264	0.673

MATERIAL DESCRIPTION								USCS	AASHTO
SILTY SAND								SM	A-2-4

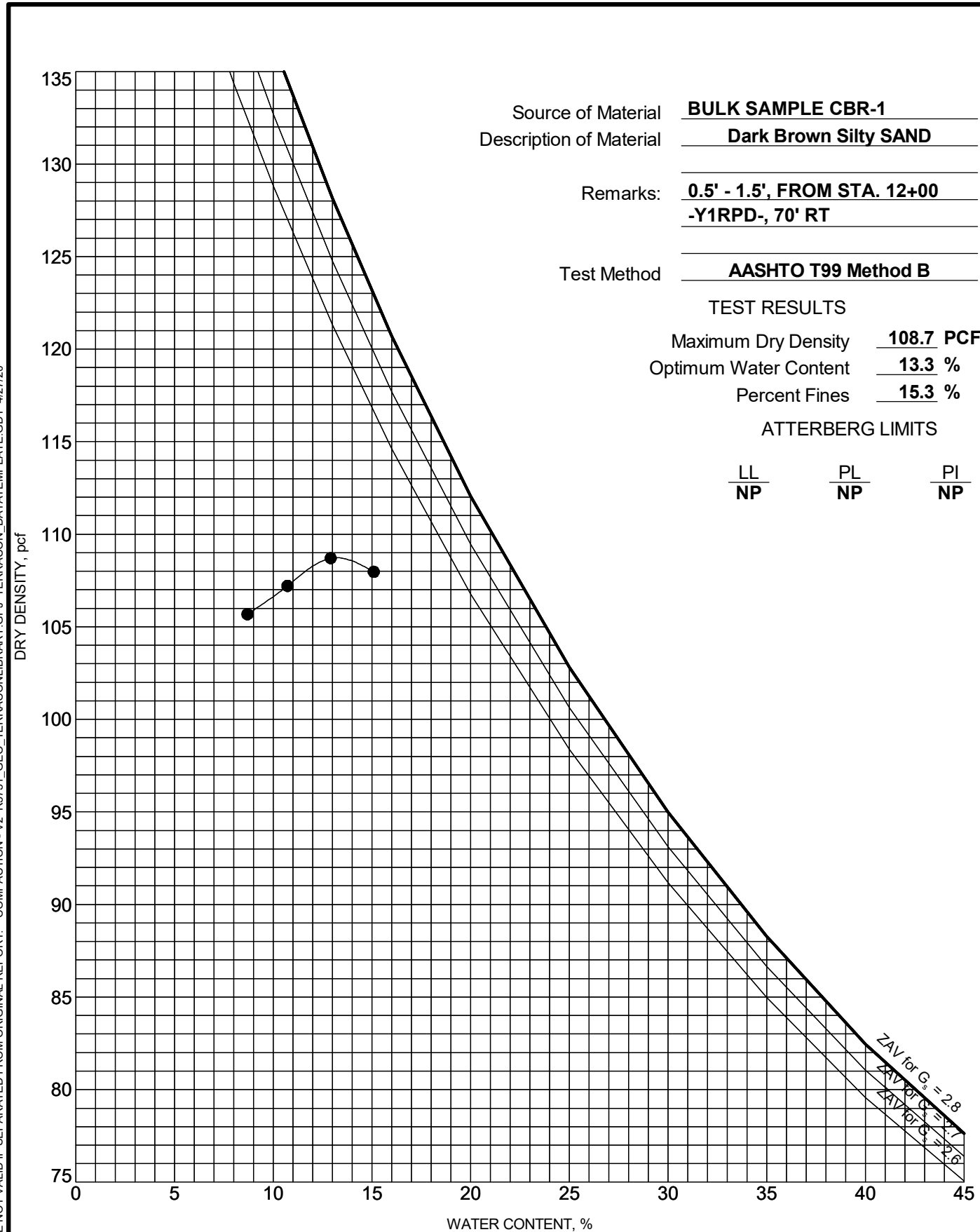
NOTES:

**Borehole: Y1RPD\_2000 Depth: 18 ft Specimen #: 6**

PROJECT: ORRUM	 2701 Westport Rd Charlotte, NC	PROJECT NUMBER: 71195028
SITE: Robeson County Orrum, NC		CLIENT: NCDOT Charlotte, NC
		EXHIBIT: B-8

# MOISTURE-DENSITY RELATIONSHIP

ASTM D698/D1557



Source of Material **BULK SAMPLE CBR-1**  
 Description of Material **Dark Brown Silty SAND**  
 Remarks: **0.5' - 1.5', FROM STA. 12+00 -Y1RPD-, 70' RT**  
 Test Method **AASHTO T99 Method B**

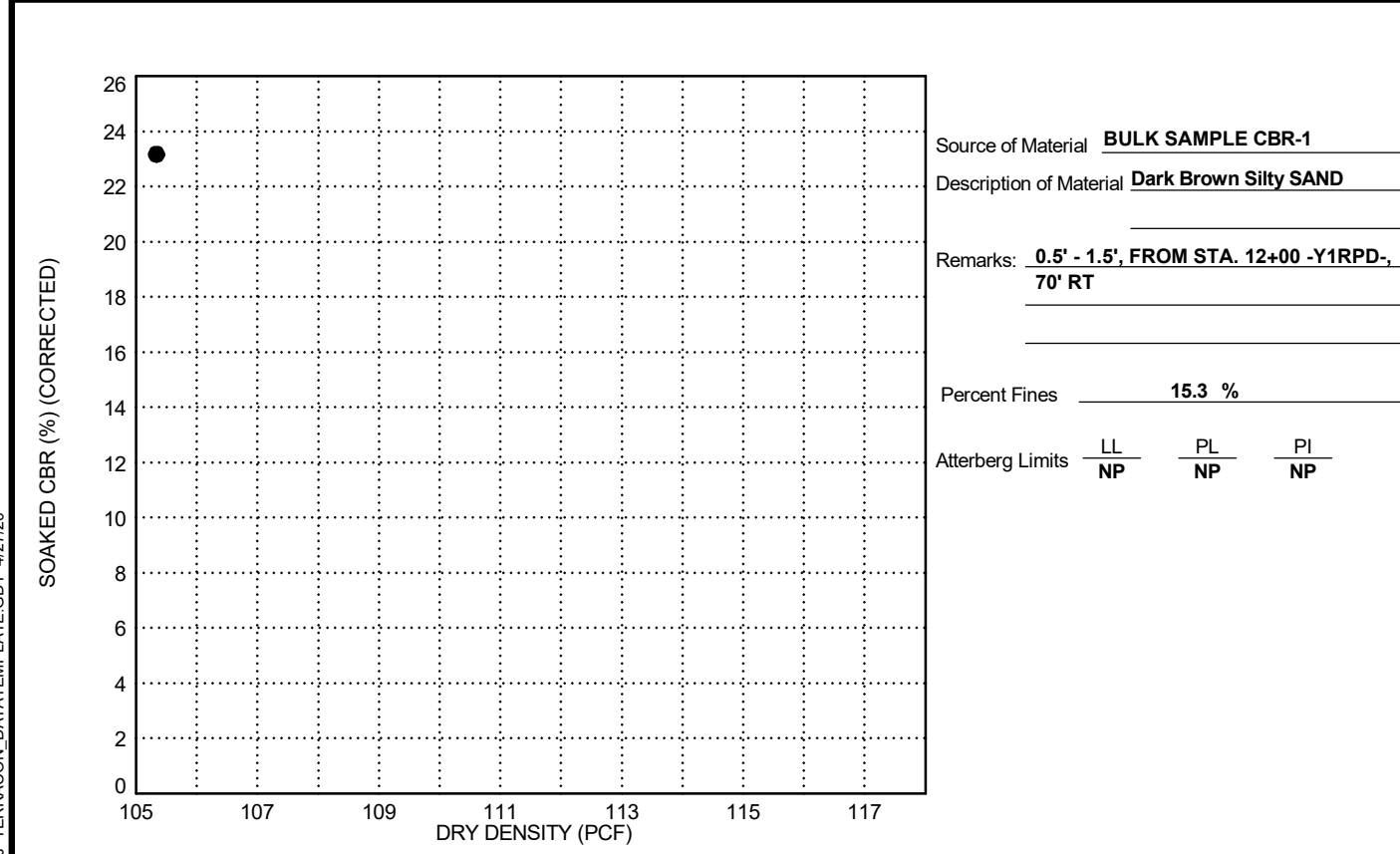
**TEST RESULTS**  
 Maximum Dry Density **108.7 PCF**  
 Optimum Water Content **13.3 %**  
 Percent Fines **15.3 %**

**ATTERBERG LIMITS**

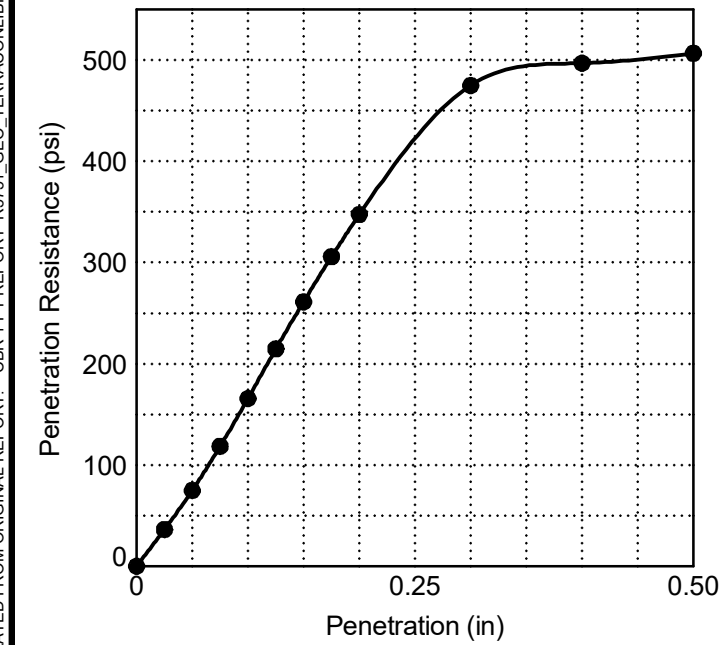
LL	PL	PI
NP	NP	NP

# CALIFORNIA BEARING RATIO

ASTM D1883-07<sup>2</sup>



Source of Material **BULK SAMPLE CBR-1**  
 Description of Material **Dark Brown Silty SAND**  
 Remarks: **0.5' - 1.5', FROM STA. 12+00 -Y1RPD-, 70' RT**  
 Percent Fines **15.3 %**  
 Atterberg Limits **LL NP, PL NP, PI NP**



Sample No.	1
Sample Condition	Soaked
Compaction Method	AASHTO T99B
Maximum Dry Density, (pcf)	108.7
Optimum Moisture Content, (%)	13.3
Dry Density before Soaking, (pcf)	105.34
Moisture Content, (%)	
After Compaction	12.7
Top 1" After Soaking	15.5
Surcharge, (lbs)	10.00
Swell, (%)	0.44
Bearing Ratio, (%)	23.2

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. COMPACTON - V2, R5751, GEO\_TERRACONLIBRARY.GPJ, TERRACON\_DATATEMPLATE.GDT, 4/27/20

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CBR, 1, PT REPORT, R5751, GEO\_TERRACONLIBRARY.GPJ, TERRACON\_DATATEMPLATE.GDT, 4/27/20

PROJECT: ORRUM  
 SITE: Robeson County  
 Orrum, NC



PROJECT NUMBER: 71195028  
 CLIENT: NCDOT  
 Charlotte, NC  
 EXHIBIT: B-1

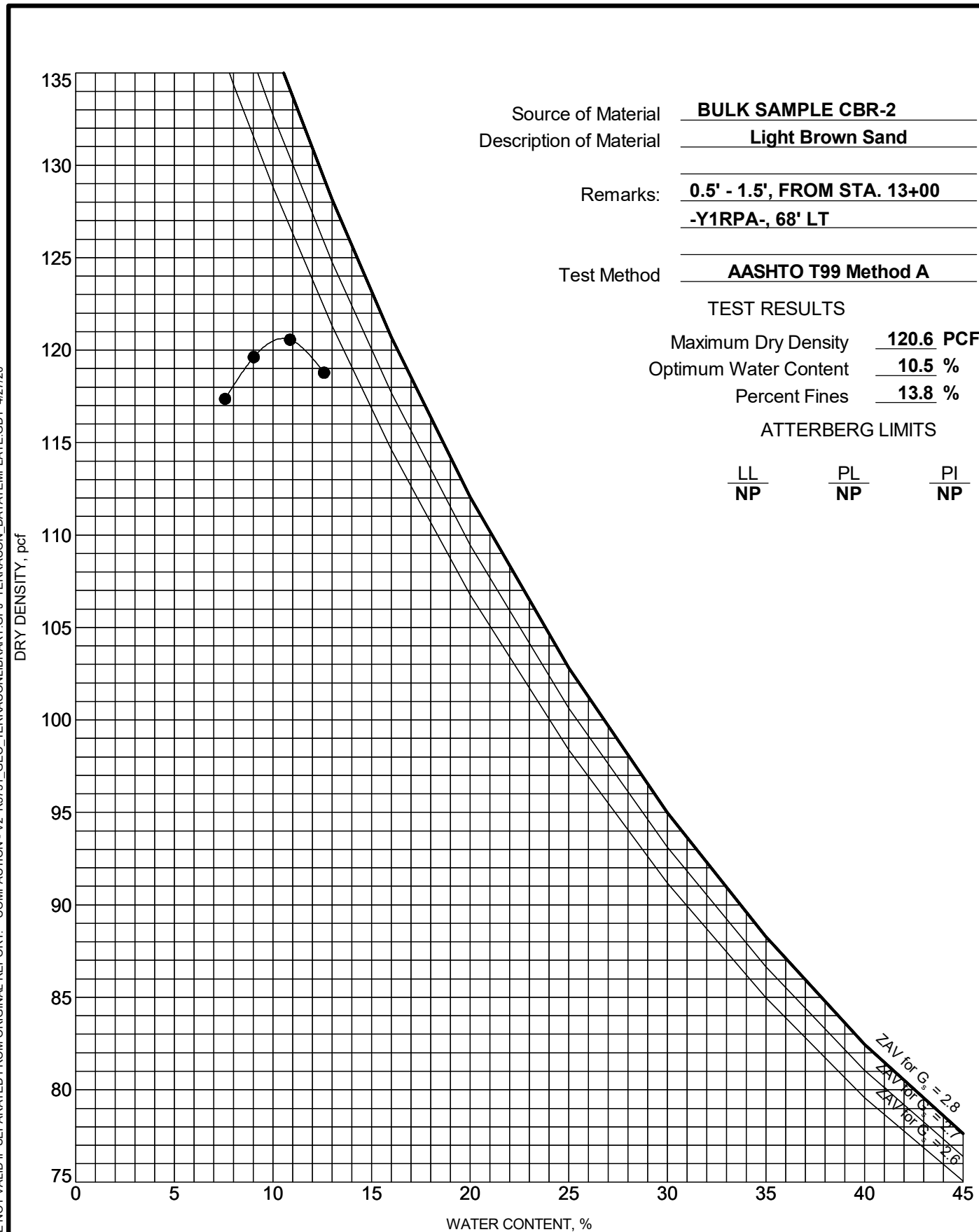
PROJECT: ORRUM  
 SITE: Robeson County  
 Orrum, NC



PROJECT NUMBER: 71195028  
 CLIENT: NCDOT  
 Charlotte, NC  
 EXHIBIT: B-1

# MOISTURE-DENSITY RELATIONSHIP

ASTM D698/D1557

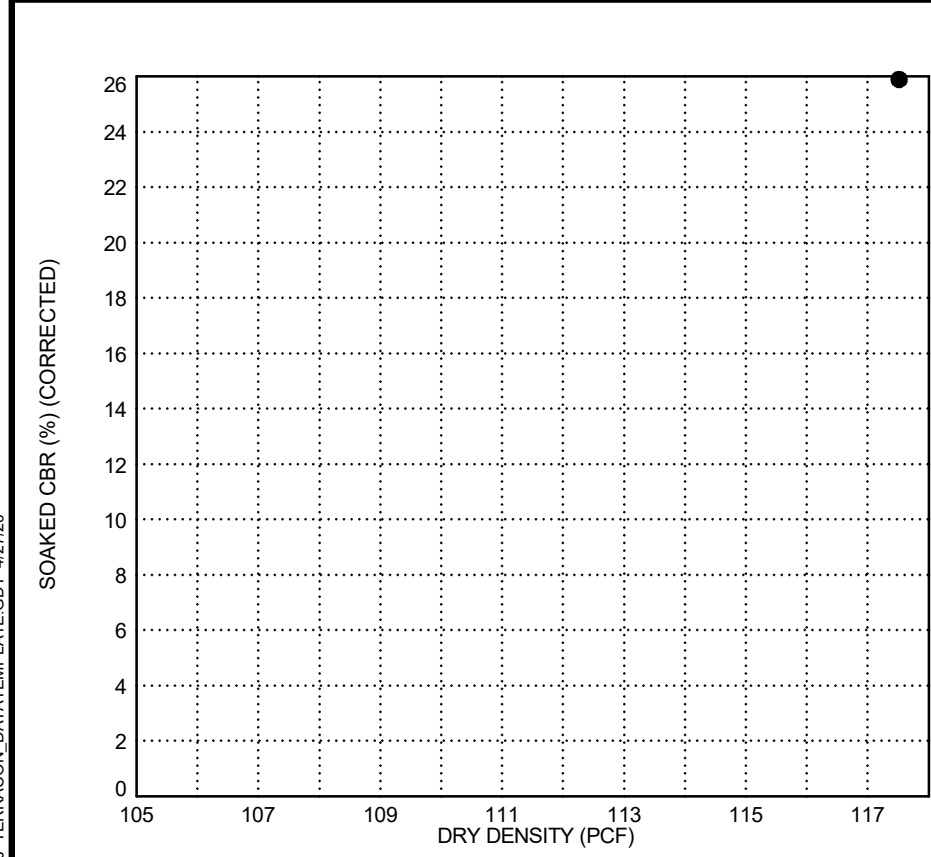


Source of Material **BULK SAMPLE CBR-2**  
 Description of Material **Light Brown Sand**  
 Remarks: **0.5' - 1.5', FROM STA. 13+00 -Y1RPA-, 68' LT**  
 Test Method **AASHTO T99 Method A**

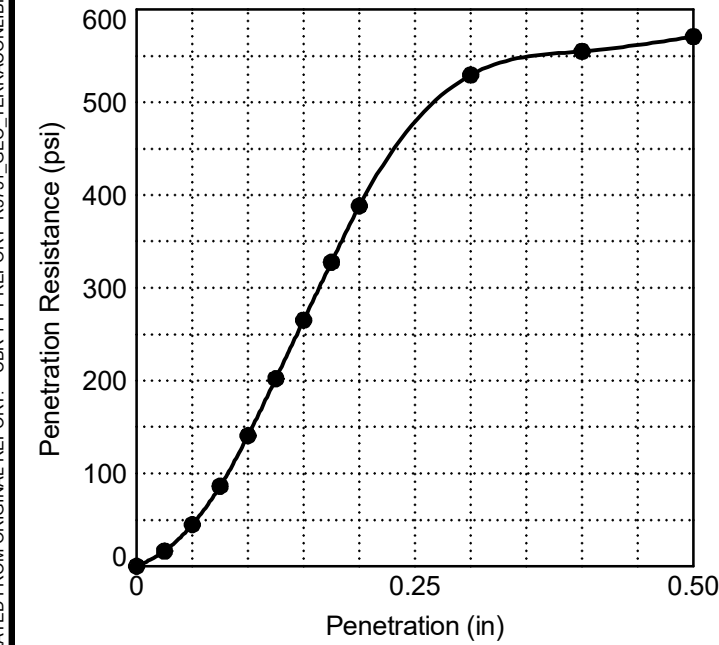
**TEST RESULTS**  
 Maximum Dry Density **120.6 PCF**  
 Optimum Water Content **10.5 %**  
 Percent Fines **13.8 %**  
**ATTERBERG LIMITS**  
 LL **NP** PL **NP** PI **NP**

# CALIFORNIA BEARING RATIO

ASTM D1883-07<sup>2</sup>



Source of Material **BULK SAMPLE CBR-2**  
 Description of Material **Light Brown Sand**  
 Remarks: **0.5' - 1.5', FROM STA. 13+00 -Y1RPA-, 68' LT**  
 Percent Fines **13.8 %**  
 Atterberg Limits **LL NP PL NP PI NP**



Sample No.	1
Sample Condition	Soaked
Compaction Method	AASHTO T99A
Maximum Dry Density, (pcf)	120.6
Optimum Moisture Content, (%)	10.5
Dry Density before Soaking, (pcf)	117.52
Moisture Content, (%)	
After Compaction	10.2
Top 1" After Soaking	12.1
Surcharge, (lbs)	10.00
Swell, (%)	0.04
Bearing Ratio, (%)	25.9

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. COMPACTON - V2, R5751\_GEO\_TERRACONLIBRARY.GPJ TERRACON\_DATATEMPLATE.GDT 4/27/20

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CBR 1 PT REPORT R5751\_GEO\_TERRACONLIBRARY.GPJ TERRACON\_DATATEMPLATE.GDT 4/27/20

PROJECT: ORRUM  
 SITE: Robeson County  
 Orrum, NC



PROJECT NUMBER: 71195028  
 CLIENT: NCDOT  
 Charlotte, NC  
 EXHIBIT: B-2

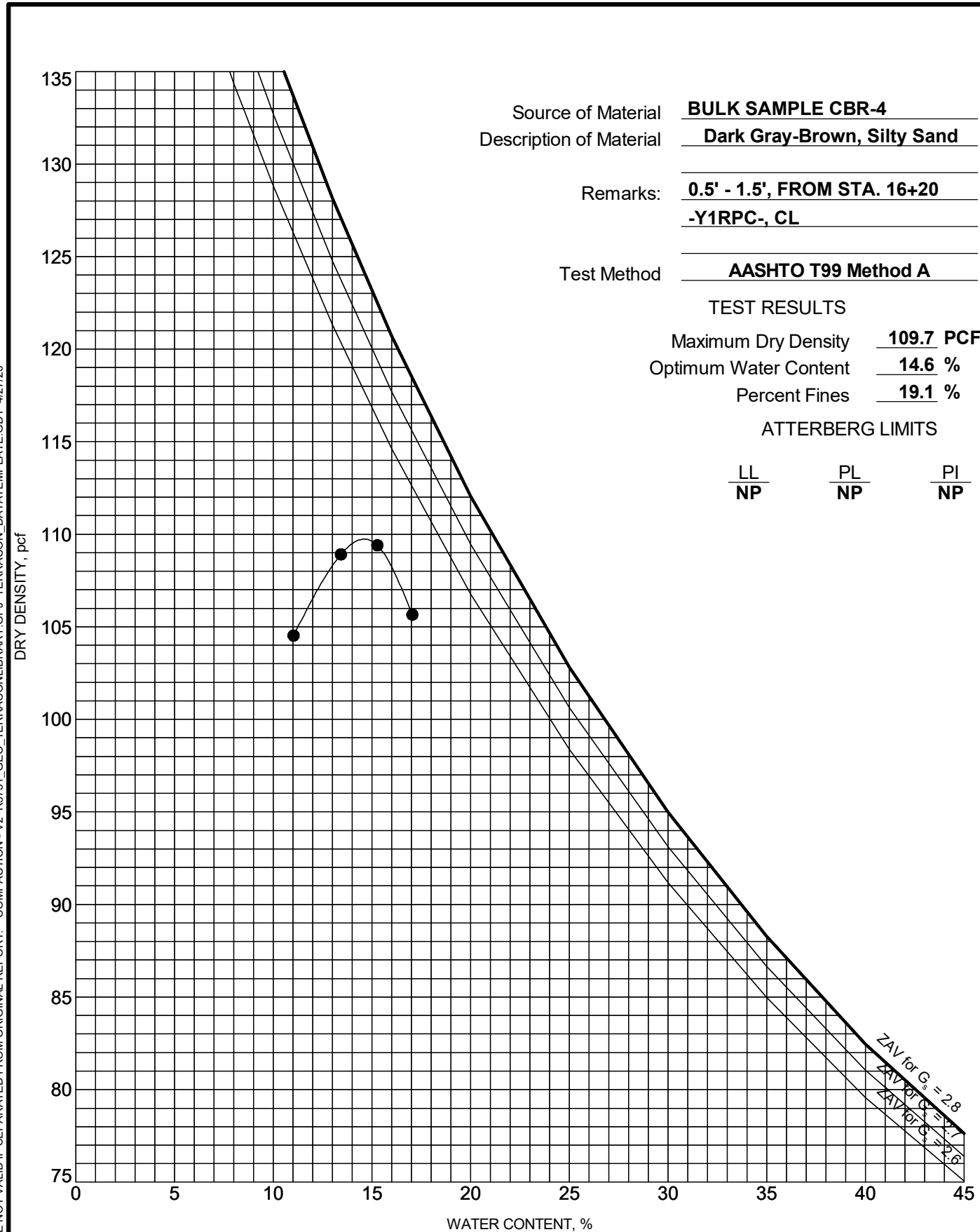
PROJECT: ORRUM  
 SITE: Robeson County  
 Orrum, NC



PROJECT NUMBER: 71195028  
 CLIENT: NCDOT  
 Charlotte, NC  
 EXHIBIT: B-2

# MOISTURE-DENSITY RELATIONSHIP

ASTM D698/D1557



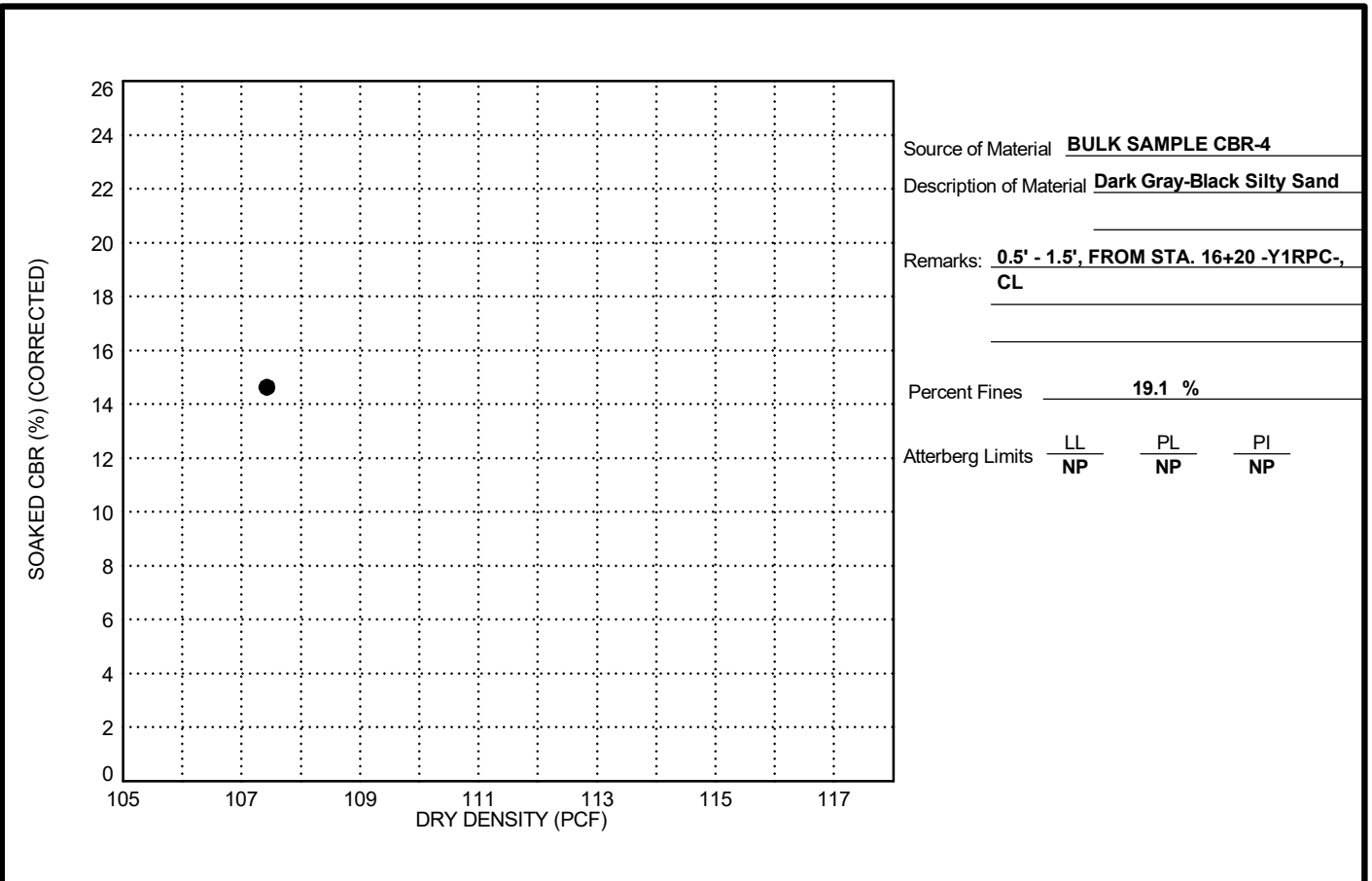
Source of Material **BULK SAMPLE CBR-4**  
 Description of Material **Dark Gray-Brown, Silty Sand**  
 Remarks: **0.5' - 1.5', FROM STA. 16+20 -Y1RPC-, CL**  
 Test Method **AASHTO T99 Method A**

**TEST RESULTS**  
 Maximum Dry Density **109.7 PCF**  
 Optimum Water Content **14.6 %**  
 Percent Fines **19.1 %**  
**ATTERBERG LIMITS**

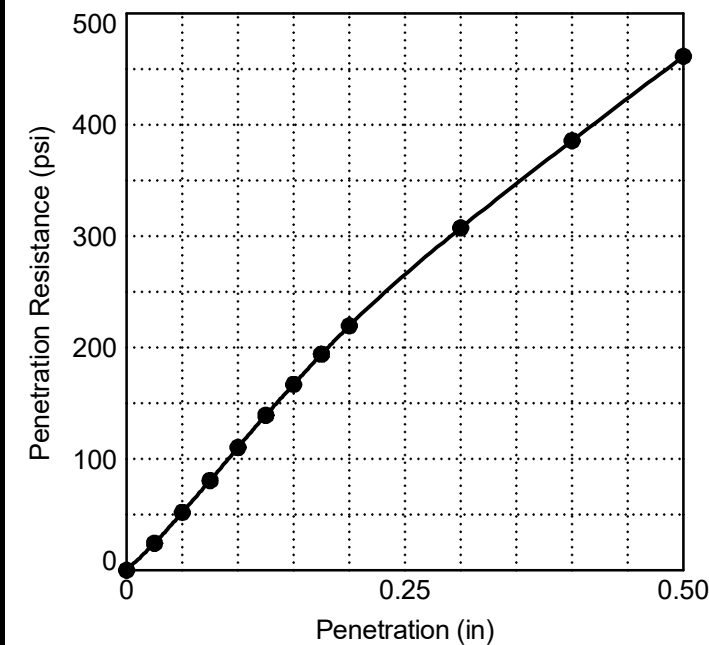
LL	PL	PI
NP	NP	NP

# CALIFORNIA BEARING RATIO

ASTM D1883-07<sup>2</sup>



Source of Material **BULK SAMPLE CBR-4**  
 Description of Material **Dark Gray-Black Silty Sand**  
 Remarks: **0.5' - 1.5', FROM STA. 16+20 -Y1RPC-, CL**  
 Percent Fines **19.1 %**  
 Atterberg Limits **LL NP, PL NP, PI NP**



Sample No.	1
Sample Condition	Soaked
Compaction Method	AASHTO T99A
Maximum Dry Density, (pcf)	109.7
Optimum Moisture Content, (%)	14.6
Dry Density before Soaking, (pcf)	107.43
Moisture Content, (%)	
After Compaction	14.4
Top 1" After Soaking	16.4
Surcharge, (lbs)	10.00
Swell, (%)	0.26
Bearing Ratio, (%)	14.6

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. COMPACTON - V2, R5751\_GEO\_TERRACONLIBRARY.GPJ TERRACON\_DATATEMPLATE.GDT 4/27/20

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CBR 1 PT REPORT R5751\_GEO\_TERRACONLIBRARY.GPJ TERRACON\_DATATEMPLATE.GDT 4/27/20

PROJECT: ORRUM

SITE: Robeson County  
Orrum, NC



PROJECT NUMBER: 71195028

CLIENT: NCDOT  
Charlotte, NC

EXHIBIT: B-3

PROJECT: ORRUM

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