-0048 8 REFERENCE **CONTENTS** 

**DESCRIPTION** 

LEGEND (SOIL & ROCK)

SUPPLEMENTAL LEGEND (GSI)

ROCK LABORATORY RESULTS SITE PHOTOGRAPHS

BORE LOGS, CORE REPORTS & CORE PHOTOGRAPHS

TITLE SHEET

SITE PLAN PROFILE CROSS SECTIONS

SHEET NO.

2A

6-15

3

#### STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS** GEOTECHNICAL ENGINEERING UNIT

# **STRUCTURE** SUBSURFACE INVESTIGATION

| COUNTY              | SUF    | RRY  |      |             |                |      |           |     |            |    |
|---------------------|--------|------|------|-------------|----------------|------|-----------|-----|------------|----|
| PROJEC <sup>-</sup> | r DES  | CRIP | TION | REPL        | <b>ACEM</b>    | ENT  | <b>OF</b> | BI  | RID        | GE |
| <b>NO. 103</b>      | ON     | NC   | 268  | <b>OVER</b> | MITO           | CHEL | LR        | IVI | E <b>R</b> |    |
| <u>US</u> 311       | ! I-40 |      |      |             |                |      |           |     |            |    |
| SITE DE             | SCRIP  | TION | ST   | A. 18 + 7   | ′5 <b>_L</b> _ |      |           |     |            |    |
|                     |        |      |      |             |                |      |           |     |            |    |

STATE PROJECT REFERENCE NO. BR-0048

#### **CAUTION NOTICE**

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (1999) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

CENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (MH-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS NIDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE TRUDE ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISTY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

- NOTES:

  1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N.C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.

  2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

J. STICKNEY C. DRISCOLL C. SMITH TRIGON EXPLORATION INVESTIGATED BY <u>J. STICKNEY</u> DRAWN BY \_S. PAPKE

CHECKED BY <u>E. BEVERLY</u> SUBMITTED BY K. MILLER



**DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED** 

PROJECT REPERENCE NO. SHEET NO.

BR-0048
2

# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT

# SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

| SOIL DESCRIPTION   | GRADATION  | ROCK DESCRIPTION   | TERMS AND DEFINITIONS  |
|--|--|--|--|
| SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT  | WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. | HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL.   | ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.   |
| ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING:  | GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.   | SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN   | AQUIFER - A WATER BEARING FORMATION OR STRATA.   |
| CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH   | ANGULARITY OF GRAINS   | REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:  | ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.   |
| AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE,  VERY STIFF.GRAY.SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6   | THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS:   | SI//AI//A  | ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.   |
| SOIL LEGEND AND AASHTO CLASSIFICATION  | ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.   | WEATHERED VIOLENTIAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.  | ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT   |
| GENERAL GRANULAR MATERIALS SILT-CLAY MATERIALS ORGANIC MATERIALS   | MINERALOGICAL COMPOSITION  | CRYSTALLINE CRYSTA | WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND  |
| LLASS. (\$\(\sigma\) 2000 (\$\(\sigma\) 35% PASSING "2000)   | MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC.  ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.                                       | ROCK (CR) WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.  | SURFACE.   |
| GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5 CLASS. A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5 A-6 A-7   | COMPRESSIBILITY  | NON-CRYSTALLINE FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN   | CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.  COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM   |
| 000000000  | SLIGHTLY COMPRESSIBLE LL < 31  | ROCK (NCR)  SEDIMENTARY ROCK THAT WOULD YEILD SPT REFUSAL IF TESTED.  ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.  | OF SLOPE.  |
| SYMBOL 000000000000000000000000000000000000  | MODERATELY COMPRESSIBLE LL = 31 - 50   | COASTAL PLAIN COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SEDIMENTARY ROCK SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED  | CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED   |
| 7. PASSING   | HIGHLY COMPRESSIBLE LL > 50  PERCENTAGE OF MATERIAL  | SEDIMENTARY ROCK SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.   | BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.   |
| *40 30 MX 50 MX 51 MN CLAY PEAT  |  | - WEATHERING   | DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.   |
| א מון אויי בין אייני איי | GRANULAR SILT - CLAY ORGANIC MATERIAL SOILS SOILS OTHER MATERIAL TRACE OF ORGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10%   | FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER   | DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE  |
| MATERIAL PASSING *40   | LITTLE ORGANIC MATTER 3 - 5% 5 - 12% LITTLE 10 - 20%   | HAMMER IF CRYSTALLINE.   | HORIZONTAL.  |
| LL - 40 MX 41 MN   | MODERATELY ORGANIC 5 - 10% 12 - 20% SOME 20 - 35%  | VERY SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN, (V SLI.) CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF  | DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE  |
| PI 6 MX NP IW MX IW MX II MN II MN IW MX IW MX II MN II MN MODERATE ORGANIC  | HIGHLY ORGANIC > 10% > 20% HIGHLY 35% AND ABOVE  | OF A CRYSTALLINE NATURE.   | LINE OF DIP, MEASURED CLOCKWISE FROM NORTH,  |
| GROUP INDEX W W 4 MX 8 MX 12 MX 16 MX NU MX AMOUNTS OF SOILS   | GROUND WATER   | SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO (SLI.) I INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR   | FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.   |
| USUAL TYPES STUNE HARDS. FINE SILTY OR CLAYEY SILTY CLAYEY MATTER  | WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING  | CRYSTALS ARE DULL AND DISCOLORED, CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.   | FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.  |
| MATERIALS SAND SAND GRAVEL AND SAND SOILS SOILS  | $lacksquare$ static water level after $\underline{24}$ hours   | MODERATE SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN  | FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM  |
| GEN. RATING EXCELLENT TO GOOD FAIR TO POOR POOR POOR UNSUITABLE  | <u> </u>   | (MOD.) GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED  | PARENT MATERIAL.   |
| AS SUBURADE POUR   | SPRING OR SEEP   | WITH FRESH ROCK.   | FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.  |
| PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30  | -  | MODERATELY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL  | FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.   |
| CONSISTENCY OR DENSENESS  RANGE OF STANDARD RANGE OF UNCONFINED  | MISCELLANEOUS SYMBOLS  | SEVERE AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH (MOD. SEV.)  AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK.   | JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.   |
| PRIMARY SOIL TYPE COMPACTNESS OR PENETRATION RESISTENCE COMPRESSIVE STRENGTH   | ROADWAY EMBANKMENT (RE) 25/025 DIP & DIP DIRECTION   | <u>IF TESTED, WOULD YIELD SPT REFUSAL</u>  | LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO  |
| (N-VALUE) (TUNS/FT-)   | WITH SOIL DESCRIPTION OF ROCK STRUCTURES   | SEVERE ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT (SEV.) REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED  | ITS LATERAL EXTENT.  |
| GENERALLY VERY LOOSE 4 TO 10   | SOIL SYMBOL  OPT DMT TEST BORING  SLOPE INDICATOR INSTALLATION   | (SEV.) REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN.   | LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.  |
| MEDIUM DENSE 10 TO 30 N/A  | ARTIFICIAL FILL (AF) OTHER AUGER BORING COME PENETROMETER  | IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF  | MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.   |
| (NON-COHESIVE) DENSE 30 TO 50  VERY DENSE > 50   | ARTIFICIAL FILL (AF) OTHER  THAN ROADWAY EMBANKMENT  AUGER BORING  CONE PENETROMETER TEST  | VERY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE SEVERE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK  | PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE   |
| VERY SOFT < 2 < 0.25   | — INFERRED SOIL BOUNDARY — CORE BORING SOUNDING ROD  | (V SEV.) REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR  | OF AN INTERVENING IMPERVIOUS STRATUM.  |
| GENERALLY SOFT 2 TO 4 0.25 TO 0.5  | TEST BORING  | VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <u>IF TESTED, WOULD YIELD SPT N VALUES &lt; 100 BPF</u>   | RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.   |
| SILT-CLAY         MEDIUM STIFF         4 TO 8         0.5 TO 1.0           MATERIAL         STIFF         8 TO 15         1 TO 2   | MONITORING WELL WITH CORE  | COMPLETE ROCK REDUCED TO SOIL, ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS   | ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF  |
| (COHESIVE) VERY STIFF 15 TO 30 2 TO 4  | →▼▼▼→ ALLUVIAL SOIL BOUNDARY  △ PIEZOMETER INSTALLATION  — SPT N-VALUE   | ALSO AN EXAMPLE.   | ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.   |
| HARD > 30 > 4  TEXTURE OR GRAIN SIZE   | RECOMMENDATION SYMBOLS   | ROCK HARDNESS  | SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT  |
|  |  | VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK, BREAKING OF HAND SPECIMENS REQUIRES  | ROCK.  |
| U.S. STD. SIEVE SIZE 4 10 40 60 200 270 OPENING (MM) 4.76 2.00 0.42 0.25 0.075 0.053   | UNSUITABLE WASTE   | SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.  | SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO   |
| COARSE FINE  | SHALLOW UNCLASSIFIED EXCAVATION - USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL   | HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.   | THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.  |
| BUULDER CUBBLE GRAVEL SAND SAND SILI CLAY  | UNDERCOT LESS ACCEPTABLE DEGRAPABLE NOCK   | MODERATELY CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE   | SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT   |
| (USE, SU.) (F SU.)   | ABBREVIATIONS  | HARD EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.   | OR SLIP PLANE.   |
| GRAIN MM 305 75 2.0 0.25 0.05 0.005<br>SIZE IN. 12 3   | AR - AUGER REFUSAL MED MEDIUM VST - VANE SHEAR TEST BT - BORING TERMINATED MICA MICACEOUS WEA WEATHERED  | MEDIUM CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT.  | STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB, HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL  |
| SOIL MOISTURE - CORRELATION OF TERMS   | CL CLAY MOD MODERATELY 7 - UNIT WEIGHT   | HARD CAN BE EXCAVATED IN SMALL CHIPS TO PEICES I INCH MAXIMUM SIZE BY HARD BLOWS OF THE  | WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL   |
| COL MOISTURE COLE FIELD MOISTURE   | CPT - CONE PENETRATION TEST NP - NON PLASTIC $\gamma_{ m d}$ - DRY UNIT WEIGHT CSE COARSE ORG ORGANIC  | POINT OF A GEOLOGIST'S PICK.   | TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.  STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY  |
| (ATTERBERG LIMITS)  OESCRIPTION  GUIDE FOR FIELD MOISTURE DESCRIPTION  | DMT - DILATOMETER TEST PMT - PRESSUREMETER TEST <u>SAMPLE ABBREVIATIONS</u>  | SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN   | TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.   |
| - SATURATED - USUALLY LIQUID; VERY WET, USUALLY  | DPT - DYNAMIC PENETRATION TEST SAP SAPROLITIC S - BULK e - VOID RATIO SD SAND, SANDY SS - SPLIT SPOON  | PIECES CAN BE BROKEN BY FINGER PRESSURE.   | STRATA ROCK QUALITY DESIGNATION (SRQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY  |
| (SAT.) FROM BELOW THE GROUND WATER TABLE   | F - FINE SL SILT, SILTY ST - SHELBY TUBE   | VERY CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK, PIECES 1 INCH SOFT OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY  | THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.  |
| PLASTIC CONTROL TO CON | FOSS FOSSILIFEROUS SLI SLIGHTLY RS - ROCK FRAC FRACTURED, FRACTURES TCR - TRICONE REFUSAL RT - RECOMPACTED TRIAXIAL  | FINGERNAIL.  | TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.   |
| RANGE - WET - (W) SEMISULIDE REQUIRES DRIVING TO   | FRAGS FRAGMENTS $\omega$ - MOISTURE CONTENT CBR - CALIFORNIA BEARING   | FRACTURE SPACING BEDDING   | BENCH MARK: BL- 6 AT STA. 18+58.91-L- 12' RT   |
| (P) PL PLASTIC LIMIT ATTAIN OPTIMUM MOISTURE   | HI HIGHLY V - VERY RATIO   | TERM SPACING TERM THICKNESS  | (924566 FT.N., 1477946 FT.E.)  |
| OM OPTIMUM MOISTURE - MOIST - (M) SOLID; AT OR NEAR OPTIMUM MOISTURE   | EQUIPMENT USED ON SUBJECT PROJECT  | VERY WIDE MORE THAN 10 FEET VERY THICKLY BEDDED 4 FEET WIDE 3 TO 10 FEET THICKLY BEDDED 1.5 - 4 FEET   | ELEVATION: 892.63 FEET   |
| SL _ SHRINKAGE LIMIT   | DRILL UNITS: ADVANCING TOOLS: HAMMER TYPE:   | MODERATELY CLOSE 1 TO 3 FEET THINLY BEDDED 0.16 - 1.5 FEET   | NOTES:   |
| REQUIRES ADDITIONAL WATER TO   | CME-45C CLAY BITS X AUTOMATIC MANUAL   | CLOSE 0.16 TO 1 FOOT VERY THINLY BEDDED 0.03 - 0.16 FEET VERY CLOSE LESS THAN 0.16 FEET THICKLY LAMINATED 0.008 - 0.03 FEET  | FIAD - FILLED IMMEDIATELY AFTER DRILLING   |
| - DRY - (D) ATTAIN OPTIMUM MOISTURE  | X CME-55  G' CONTINUOUS FLIGHT AUGER  CORE SIZE:   | THINLY LAMINATED < 0.008 FEET  | The state of the s |
| PLASTICITY   | X 8 HULLOW AUGERS   □-B □-H  | INDURATION   |  |
| PLASTICITY INDEX (PI) DRY STRENGTH   | X CME-550X HARD FACED FINGER BITS X-N X  | FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.  |  |
| NON PLASTIC 0-5 VERY LOW   | TUNGCARBIDE INSERTS  | FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.   |  |
| SLIGHTLY PLASTIC 6-15 SLIGHT<br>MODERATELY PLASTIC 16-25 MEDIUM  | VANE SHEAR TEST X CASING X W/ ADVANCER HAND TOOLS:  POST HOLE DIGGER   | CONTROL CAN DE CEDADATED FROM CAMPLE MITH CTEFL DOOR   |  |
| HIGHLY PLASTIC 26 OR MORE HIGH   | PORTABLE HOIST TRICONE STEEL TEETH HAND AUGER  | MODERATELY INDURATED  ORANINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE;  BREAKS EASILY WHEN HIT WITH HAMMER.  |  |
| COLOR  | X TRICONE 1-15/6 TUNGCARB. SOUNDING ROD  | INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE;   |  |
| DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY).  | X CORE BIT SOUNDING NOD  | DIFFICULT TO BREAK WITH HAMMER.  |  |
| MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.   |  | EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE;   | 2275 2 75  |
| •  |  | SAMPLE BREAKS ACROSS GRAINS.   | DATE: 8-15-1   |

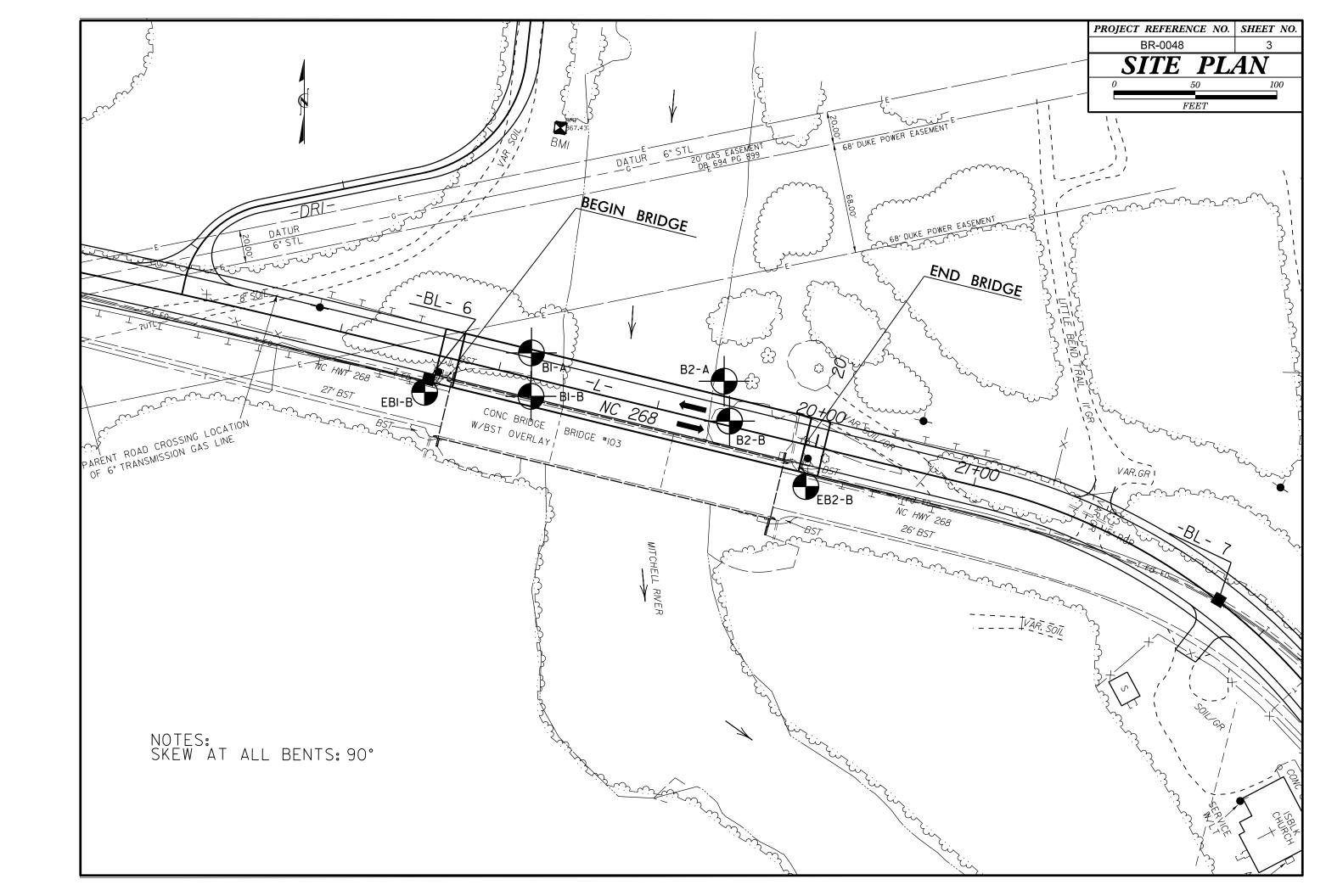
| PROJECT REFERENCE NO. | SHEET NO. |
|-----------------------|-----------|
| 3R-0048               | 2A        |

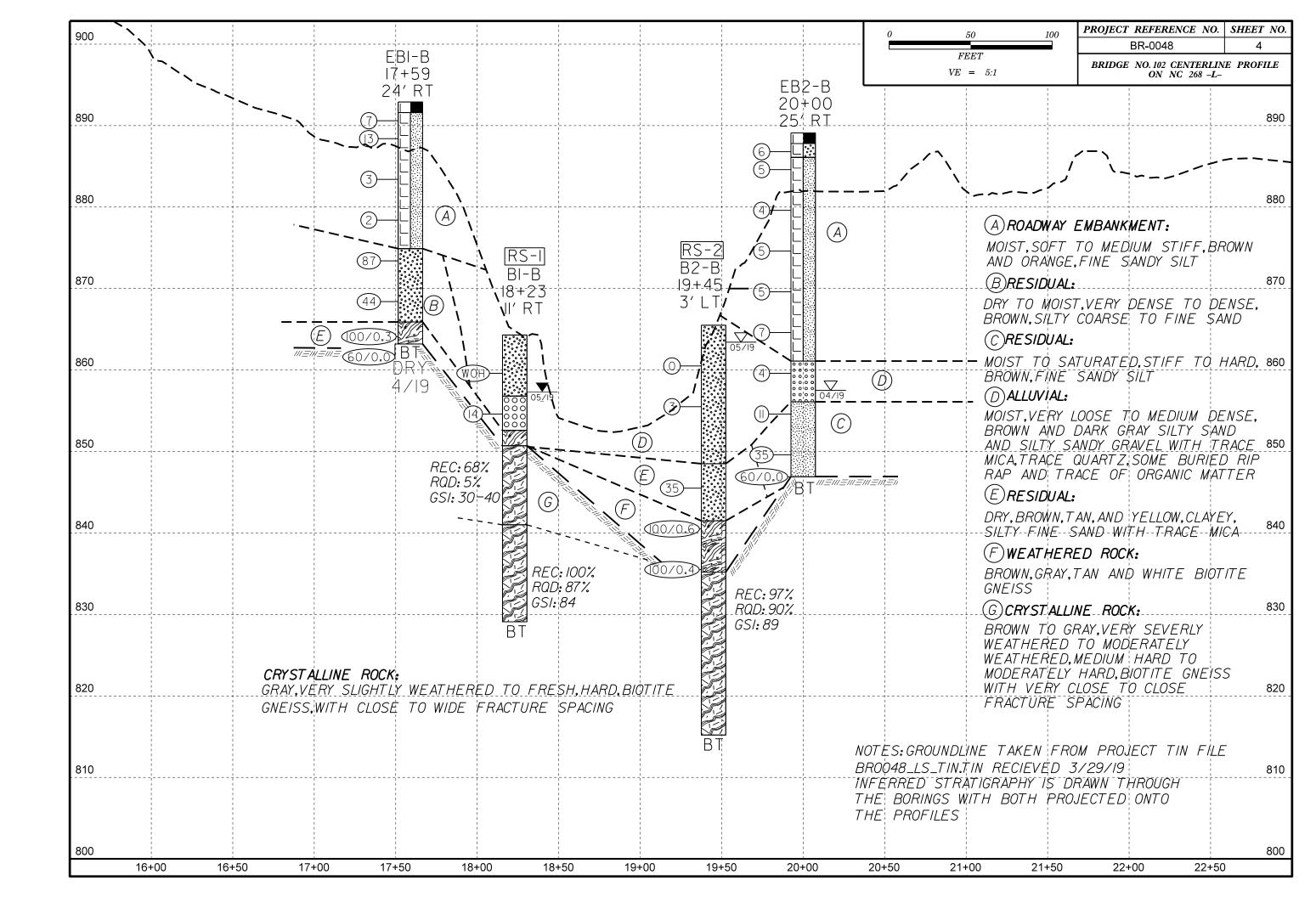
# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT

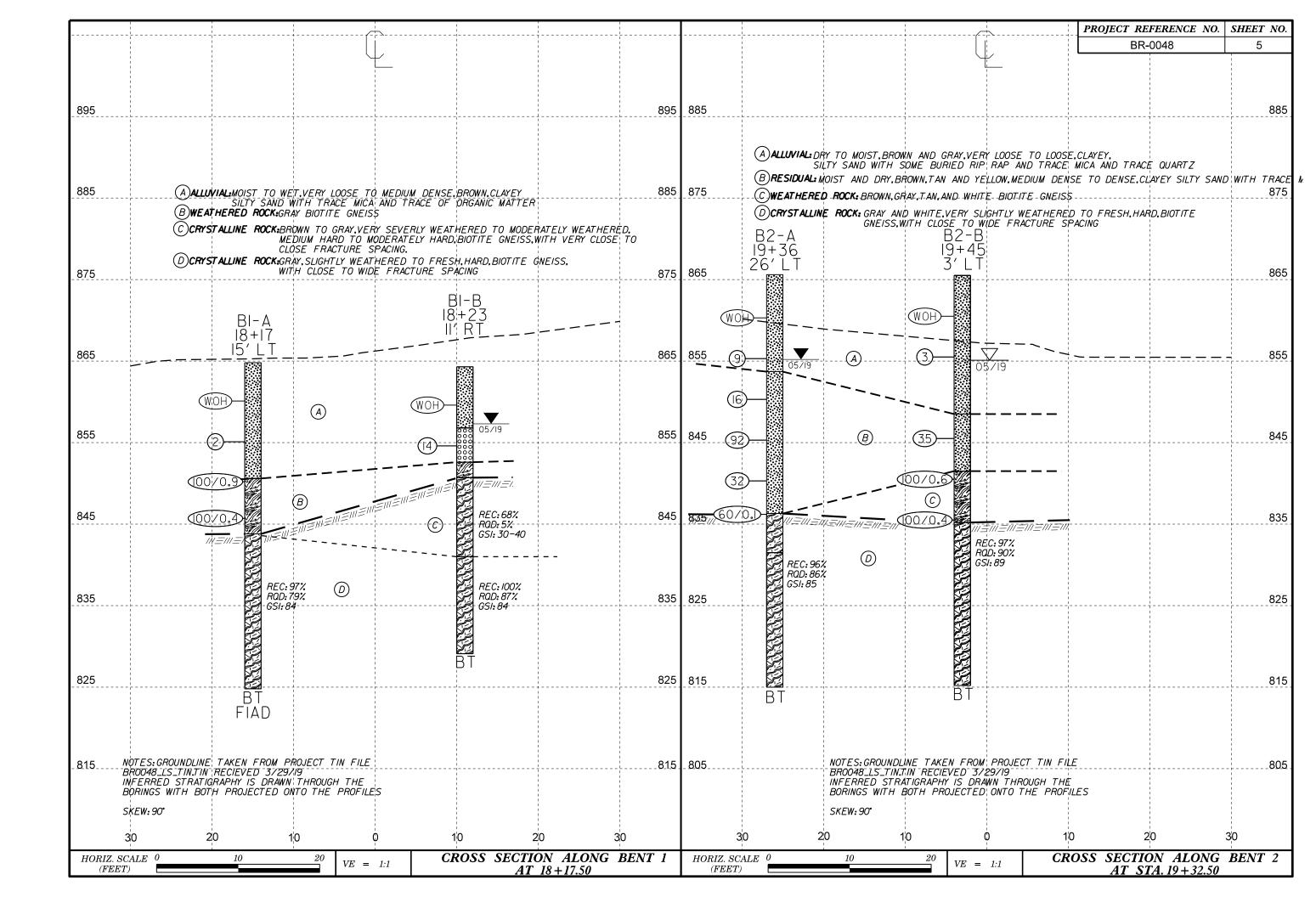
# SUBSURFACE INVESTIGATION

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES

| AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Joint   | ed Rock Mass (Mar   |   |  |  |   | GE DESIGN SPECIFICATIONS  AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)   | <b>1</b> Ø)   |
|--|---|---|--|--|---|---|---|
| GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000)  From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis. | SURFACE CONDITIONS  VERY GOOD  Very rough, fresh unweathered surfaces | GOOD<br>Rough, slightly weathered, iron stained<br>surfaces | FAIR<br>Smooth, moderately weathered and<br>altered surfaces | POOR<br>Slickensided, highly weathered surfaces<br>with compact coatings or fillings<br>or angular fragments | VERY POOR<br>Slickensided, highly weathered surfaces<br>with soft clay coatings or fillings | GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos. P and Hoek E., 2000)  From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass.  The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis. | <pre>VERT roun - Very smooth, slicken-<br/>sided or highly weathered surfaces<br/>with soft clay coatings or fillings</pre> |
| INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities   | 90 80   | CREASING SUF  | NI ACE GO  | N/A  | N/A   | COMPOSITION AND STRUCTURE  A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.   |   |
| BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets  VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks  | OCKING OF ROCK PI   | 70 60 50  |  |  |   | B. Sand- stone with thin inter- layers of siltstone amounts  D. Siltstone or silty shale with sand- stone layers stone layers amounts  B. Weak siltstone or clayey shale with sandstone layers  40  | <del></del>   |
| formed by 4 or more joint sets  BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity   | ASING INTERLOC  |   | 40   | 30   |   | C. D. E. and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H.  F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure   |   |
| DISINTEGRATED - poorly inter-<br>locked, heavily broken rock mass<br>with mixture of angular and<br>rounded rock pieces  | DECRE   |   |  | 20   |   | G. Undisturbed silty or clayey shale with or clayey shale forming a chaotic structure with pockets of clay. Thin sandstone layers of sandstone are transformed into small rock pieces.  |   |
| LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes  | V N/A   | N/A   | //   |  | 10  | ——→ Means deformation after tectonic disturbance  | ATE: 8-19-  |





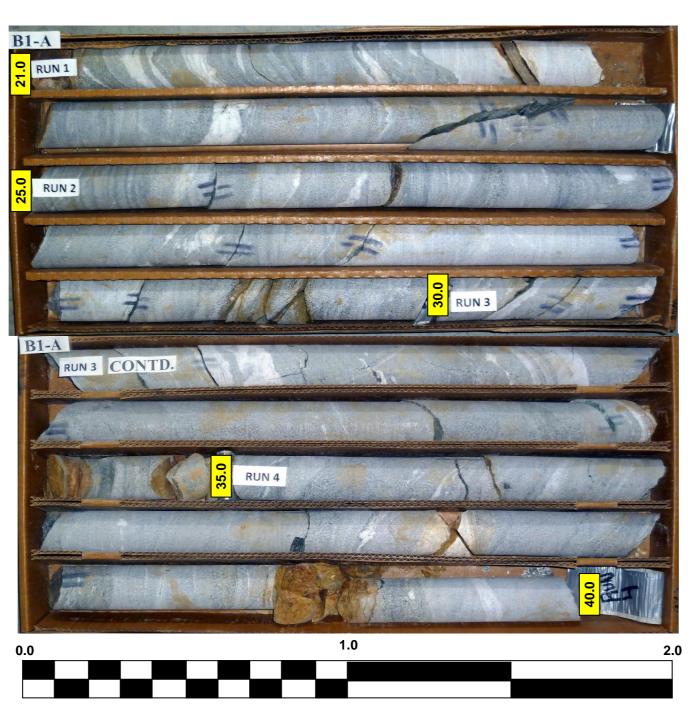


|              |                           |      |              |       |              |                  |                  | В         | <u>ORE L</u> | <u>.OG</u> |       |             |                         |                              |             |          |            |
|--------------|---------------------------|------|--------------|-------|--------------|------------------|------------------|-----------|--------------|------------|-------|-------------|-------------------------|------------------------------|-------------|----------|------------|
| WBS          | 67048.1.1                 |      |              |       | TI           | <b>P</b> BR-0048 | 1                | COUNT     | Y SURRY      |            |       |             | GEOLOGI                 | ST C. Drisc                  | oll         |          |            |
|              |                           |      |              | lacem |              | Bridge 103       |                  | 8 over Mi |              |            |       |             |                         |                              |             |          | ID WTR (ft |
|              | ING NO. EI                |      |              |       |              | TATION 17        |                  |           | OFFSET       |            |       |             | ALIGNMEI                |                              |             | 0 HR.    | Dry        |
| COLL         | LAR ELEV.                 | 892  | 2.9 ft       |       | TO           | OTAL DEPTI       | <b>H</b> 29.7 ft |           | NORTHIN      |            |       |             |                         | 1,477,944                    |             | 24 HR.   | FIA        |
| DRILL        | RIG/HAMME                 | R EF | F./DA        | TE TE | RI0055       | CME-55 87%       | 03/21/2019       |           |              |            |       | D H         | .S. Augers              |                              | HAMME       | R TYPE   | Automatic  |
| DRIL         | LER R. To                 | othn |              |       |              | TART DATE        |                  |           | COMP. DA     |            | 15/19 | <del></del> | SURFACE                 | WATER DE                     | PTH N/A     | ١        |            |
| ELEV<br>(ft) | DRIVE<br>ELEV<br>(ft) DEF |      | BLC<br>0.5ft | 0.5ft | JNT<br>0.5ft | 0 25             | BLOWS P          | PER FOOT  | 75 100       | SAMP.      | MOI   | O<br>G      | ELEV. (ft)              | SOIL AND RO                  | OCK DESC    | RIPTION  | DEPTH (    |
| 895          |                           |      |              |       |              |                  |                  |           |              |            |       | -           | —<br>-<br>892.9         | GPO! IN                      | ID SURFA    | ^E       | (          |
|              | 891.6 + 1.                | .3   | _            |       |              |                  |                  |           |              |            |       |             | - 891.6                 | ROADWAY                      | EMBANK      | MENT     |            |
| 890          | 889.4 3.                  | .5   | 7            | 4     | 3            | 7                | · · · ·          |           |              | -          | М     |             |                         | ABC Stone                    |             | Feet)    |            |
|              | ‡                         |      | 5            | 6     | 7            | 13.              |                  |           |              |            | М     |             | -<br>-                  | Brown and Orai               | nge, Fine S | andy SIL | Т          |
| 885          |                           |      |              |       |              | :/:::            |                  |           |              |            |       |             | -<br>-                  |                              |             |          |            |
| 000          | 884.4 + 8.                | .5   | 2            | 1     | 2            | 1 7              |                  |           |              | 1          | M     |             | -                       |                              |             |          |            |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            | "     |             | -<br>-                  |                              |             |          |            |
| 880          | +<br>879.4 + 13           | 5.5  |              |       |              |                  |                  |           |              | -          |       |             | -<br>                   |                              |             |          |            |
|              | <del></del>               |      | 1            | 1     | 1            | di               |                  |           |              |            | М     | L           | -<br>-                  |                              |             |          |            |
| 875          | ‡                         |      |              |       |              | ::::7            | ·                |           |              |            |       |             | -                       |                              |             |          |            |
| 6/3          | 874.4 18                  | 3.5  | 20           | 17    | 70           |                  |                  |           |              | 1          | D     |             | <u>874.9</u>            |                              | SIDUAL      |          | 18         |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            |       |             | -                       | Brown, Silty C               | oarse to Fi | ne SAND  |            |
| 870          | +<br>869.4 + 23           |      |              |       |              |                  | · · · ·          | /         |              |            |       |             | -<br>-                  |                              |             |          |            |
|              | 009.4 23                  |      | 3            | 17    | 27           |                  |                  |           |              |            | М     |             | -<br>-                  |                              |             |          |            |
| 005          |                           |      |              |       |              |                  | : : : <u> </u>   |           |              |            |       |             | 865.9                   |                              |             |          | 2          |
| 865          | 864.4 28                  |      | 00/0.3       |       |              |                  |                  |           | 100/0.3      | 1          |       |             | <del>-</del><br>- 863.2 |                              | White GNE   |          | 00         |
|              | 863.2 T 29                |      | 60/0.0       |       |              |                  |                  |           | 60/0.0       | H          |       | 34774       | - Е                     | Boring Terminat              | ed WITH S   | TANDAR   | .D         |
|              | 1                         |      |              |       |              |                  |                  |           |              |            |       |             |                         | PENETRATION ation 863.2 ft o | n CRYSTA    |          |            |
|              | 1                         |      |              |       |              |                  |                  |           |              |            |       |             | <u>-</u>                | G                            | SNEISS      |          |            |
|              | 1                         |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | <del>-</del>              |      |              |       |              |                  |                  |           |              |            |       |             | _                       |                              |             |          |            |
|              | Ŧ                         |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | Ŧ                         |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | 1 7                       |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | 1                         |      |              |       |              |                  |                  |           |              |            |       |             | -<br>-                  |                              |             |          |            |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            |       |             | -<br>-                  |                              |             |          |            |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            |       |             | -<br>-                  |                              |             |          |            |
|              |                           |      |              |       |              |                  |                  |           |              |            |       |             | <del>-</del>            |                              |             |          |            |
|              | <u> </u>                  |      |              |       |              |                  |                  |           |              |            |       |             | -<br>-                  |                              |             |          |            |
|              | 1                         |      |              |       |              |                  |                  |           |              |            |       |             | _                       |                              |             |          |            |
|              | <u> </u>                  |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | 1                         |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | <del> </del>              |      |              |       |              |                  |                  |           |              |            |       |             | <u>-</u>                |                              |             |          |            |
|              | <del> </del>              |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            |       |             | <del></del><br>-        |                              |             |          |            |
|              |                           |      |              |       |              |                  |                  |           |              |            |       |             | -<br>-                  |                              |             |          |            |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            |       |             | -<br>                   |                              |             |          |            |
|              | ‡                         |      |              |       |              |                  |                  |           |              |            |       |             | -<br>-                  |                              |             |          |            |
|              | 1 🖠                       |      |              |       |              |                  |                  |           |              |            |       |             | -                       |                              |             |          |            |

SHEET 6

|  | <i>E</i>                                    | BORE LOG         |  |                                   |                                    |  | CORE LOG                |  |
|--|---|------------------|--|-----------------------------------|------------------------------------|--|-------------------------|--|
| <b>WBS</b> 67048.1.1   | TIP BR-0048 COUNT                           | TY SURRY         | GEOLOGIST Stickney, J. K.                            | _                                 | <b>WBS</b> 67048.1.1               | TIP BR-0048 COUN   | TY SURRY                | GEOLOGIST Stickney, J. K.  |
| SITE DESCRIPTION Replaceme                                   | ent of Bridge 103 on NC 268 over Mit        | chell River      | ·  | GROUND WTR (ft)                   | SITE DESCRIPTION Replace           | ement of Bridge 103 on NC 268 over Mi  | tchell River            | GROUND WTR (ft)  |
| BORING NO. B1-A  | STATION 18+17                               |                  | ALIGNMENT -L-  | <b>0 HR.</b> N/A                  | BORING NO. B1-A                    | STATION 18+17  | OFFSET 15 ft LT         | ALIGNMENT -L- 0 HR. N/A  |
| COLLAR ELEV. 864.8 ft  | TOTAL DEPTH 40.0 ft                         |                  | 1  | <b>24 HR.</b> N/A                 | COLLAR ELEV. 864.8 ft              | TOTAL DEPTH 40.0 ft  | <b>NORTHING</b> 924,714 | <b>EASTING</b> 1,478,042 <b>24 HR.</b> N/A                                   |
| DRILL RIG/HAMMER EFF./DATE HF                                |   | DRILL METHOD NW  | Casing W/SPT & Core HAMMI                            | ER TYPE Automatic                 |                                    | HFO0072 CME-550X 92% 08/15/2018  |                         | NW Casing W/SPT & Core HAMMER TYPE Automatic                                 |
| DRILLER Smith, C. L.   | <b>START DATE</b> 05/22/19                  |                  | SURFACE WATER DEPTH N/                               | /A                                | DRILLER Smith, C. L.               | START DATE 05/22/19  | COMP. DATE 05/22/19     | SURFACE WATER DEPTH N/A  |
| ELEV DRIVE DEPTH BLOW COU                                    | JNT BLOWS PER FOC<br>0.5ft 0 25 50          | 7   0            | SOIL AND ROCK DESC                                   | CRIPTION                          | CORE SIZE NX                       | TOTAL RUN 19.0 ft  |                         |  |
| (ft) (ft) (ft) 0.5ft 0.5ft                                   | 0.5ft 0 25 50                               | 75 100 NO. MOI G | ELEV. (ft)   | DEPTH (ft)                        | ELEV RUN DEPTH RUN R. (ft) (ft) (M | RILL   RUN   STRATA     ATE   REC.   RQD   NO.   (ft)   (ft)     Ini/ft)   (ft)   (ft)   (ft)   (ft)   |                         | DESCRIPTION AND REMARKS  |
|  |   |                  |  |                                   | (II)                               |  | <u> </u>                | DEPTH (fi  |
| 865  |   | 1.000.00         | .864.8 GROUND SURF.<br>ALLUVIAL                      |                                   | 843.8 21.0 4.0 NN                  | W/1.0 (3.6) (3.2) (18.4) (15.  | 1) 843.8                | Begin Coring @ 21.0 ft CRYSTALLINE ROCK 21.0                                 |
|  |   | -                | Brown, Clayey Silty SAND wand Trace of Organic Matte | with Trace Mica<br>er (Leaves and | NN 1:4                             | W1.0 (3.6) (3.2) (18.4) (15. W1.0 90% 80% 97% 7994.4/1.0   | 6 Gray, Slightly        | Weathered to Fresh, Hard, Biotite Gneiss with Close to Wide Fracture Spacing |
| 860 861.1 3.7 WOH WOH  | WOH 0                                       | M                | Wood)  | `                                 | 840 839.8 25.0 1.5<br>5.0 1.3      | 0/1.0   (4.9)   (4.3)   (4.10) |                         | GSI: 84  |
|  |   |                  |  |                                   | 1:4                                | 17/1.0   98%   86%   |                         |  |
| 856.1 8.7  | 1   | .                |  |                                   | 835 834.8 30.0 1:4<br>1:4          | 15/1.0<br>1/1/1.0  |                         |  |
| 855 2 1  | '   • 2 · · · · · · · · · · · · · · · · · · |                  |  |                                   | +   5.0   1:5<br>1:4               | 0/1.0   55/8   66/8   60/8   6 |                         |  |
| 851.1 1 13.7   |   |                  |  |                                   | 1.4                                | 12/1.0<br>14/1.0   |                         |  |
| 850 851.1 13.7 2 98/0.4                                      | · · · · · · · · · · · · · · · · · · ·       | 100/0.9   N/J=/1 | WEATHERED RO   | OCK 14.2                          | 629.8 <u>35.0</u> 1:4<br>- 5.0 1:3 | 11/1.0   18/1.0   (5.0)   (3.7)   15/1.0   100%   74%  | 1) 843.8 Gray, Slightly |  |
|  |   |                  | Gray BIOTITE GN                                      | NEISS                             |                                    | 19/1.0   100%   74%  |                         |  |
| 845 1 18.7 100/0.4   |   | 100/0.4          |  |                                   | 825 824.8 40.0 1:4                 | 9/1.0<br>4/1.0   | 824.8<br>Boring Terr    | 40. minated at Elevation 824.8 ft in CRYSTALLINE ROCK:                       |
|  |   |                  | 843.8 CRYSTALLINE R                                  | 21.0                              |                                    |  | -                       | BIOTITE GNEISS   |
|  |   |                  | Gray BIOTITE GN                                      |                                   |                                    |  | <u> </u>                |  |
| 840  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
| 835  |   |                  |  |                                   | +                                  |  | -                       |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
| 830  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
| 825  |   |                  | .824.8   | 40.0                              |                                    |  | -                       |  |
|  |   |                  | Boring Terminated at Eleva<br>CRYSTALLINE ROCK: BIO  | ation 824.8 ft in<br>OTITE GNEISS |                                    |  |                         |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   | ‡                                  |  | -                       |  |
|  |   |                  |  |                                   |                                    |  |                         |  |
|  |   |                  |  |                                   | ‡                                  |  |                         |  |
|  |   |                  |  |                                   |                                    |  | F                       |  |
|  |   |                  |  |                                   |                                    |  | F                       |  |
|  |   |                  |  |                                   |                                    |  | [-                      |  |
|  |   | F                |  |                                   |                                    |  | [                       |  |
| 849<br>  |   |                  |  |                                   |                                    |  |                         |  |
|  |   | [-               |  |                                   |                                    |  |                         |  |
|  |   | [                |  |                                   |                                    |  |                         |  |
|  |   | [                |  |                                   | ‡                                  |  | -                       |  |
| NCDOT BORE DOUBLE BROOM GEO_BROG_GINT.GPU NC_DOT.GDU 6/26/19 |   |                  |  |                                   |                                    |  |                         |  |
|  |   | [                |  |                                   |                                    |  |                         |  |
| žL   |   |                  |  |                                   |                                    |  | 1 -                     |  |

**B1-A**BOX 1 & 2: 21.0 to 40.0 FEET

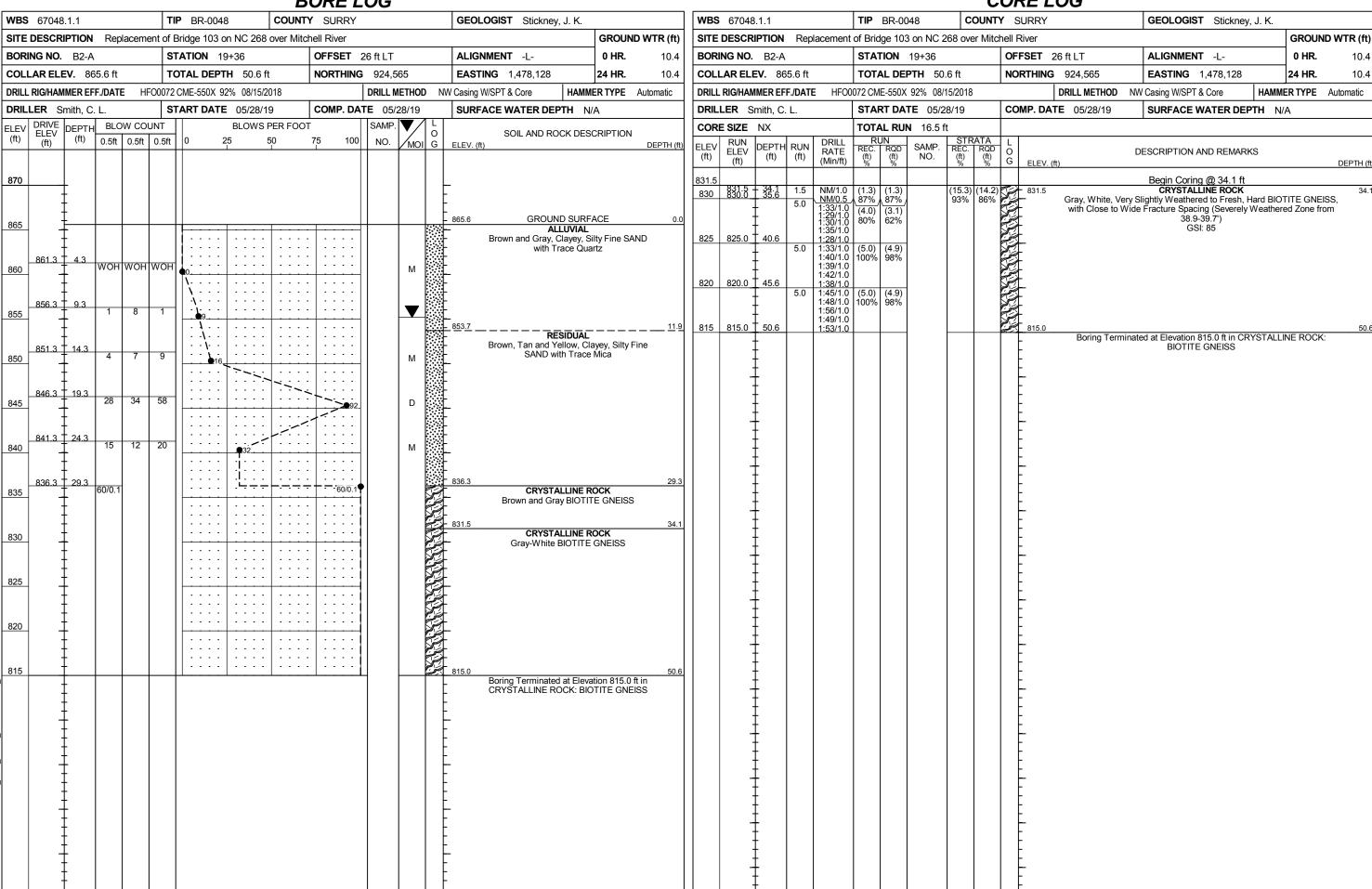


| BORE LOG |               |  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            | C            | ORE            | LOG            |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
|----------|---------------|--|---------|--------|----------|--|----------------|---------|-----------|--------------|----------------|--------|-----------------|--------------------------|--------------------------|--------------------------|------------|--------------|----------------|----------------|---------|----------------------------------|----------------------|-------------------------|----------------|-----------|--------------------------|------------------|-------------------|-----------|--|---------------|------------------|
| WB       | 67048         | 3.1.1  |         |        | TIF      | BR-004   | 8              | С       | OUNTY     | SURRY        | <u> </u>       |        |                 | GEOLOGIST Stick          | ney, J. K.               |                          |            | WBS          | 67048          | 3.1.1          |         |                                  | TIP                  | BR-00                   | 048            | С         | TNUO                     | Y SURR           | Υ                 |           | GEOLOGIST Stickney   | J. K.         |                  |
| SITE     | DESCR         | IPTION   | Rep     | laceme | ent of B | ridge 103 o                                      | on NC 20       | 268 ove | er Mitch  | ell River    |                |        |                 |                          |                          | GROUND                   | WTR (ft)   | SITE         | DESCR          | IPTION         | Repl    | acement                          | t of Bri             | dge 103                 | 3 on NC        | 268 ove   | er Mitcl                 | nell River       |                   |           |  | GR            | OUND WTR (ft)    |
| BOF      | ING NO.       | B1-B   |         |        | ST       | ATION 1  | 8+23           |         |           | OFFSET       | 11 ft R        | Γ      |                 | ALIGNMENT -L-            |                          | 0 HR.                    | 7.0        | BORI         | NG NO.         | B1-B           |         |                                  | STA                  | TION                    | 18+23          |           |                          | OFFSET           | 11 ft RT          |           | ALIGNMENT -L-  | 0 H           | <b>HR.</b> 7.0   |
| COL      | LAR EL        | <b>EV</b> . 86                                   | 34.3 ft |        | то       | TAL DEP  | <b>TH</b> 35.2 | .2 ft   |           | NORTHIN      | <b>IG</b> 924, | 556    |                 | <b>EASTING</b> 1,478,00  | 9                        | 24 HR.                   | 7.0        | COLL         | AR ELI         | <b>EV</b> . 86 | 4.3 ft  |                                  | тот                  | AL DE                   | <b>PTH</b> 35  | 5.2 ft    |                          | NORTHI           | <b>NG</b> 924,556 |           | <b>EASTING</b> 1,478,009                                     | 24 I          | <b>HR.</b> 7.0   |
| DRIL     | _ RIG/HAN     | MER EF   | F./DATE | E HF   | O0072 (  | ME-550X 9  | 2% 08/1        | 15/2018 | 3         |              | DRILL          | METHO  | ) NW C          | Casing W/SPT & Core      | HAMI                     | MER TYPE                 | Automatic  | DRILL        | RIG/HAN        | IMER EF        | F./DATE | HF00                             | 0072 CI              | ME-550X                 | 92% 08         | /15/2018  | 3                        |                  | DRILL METH        | OD N      | NW Casing W/SPT & Core                                       | HAMMER TY     | PE Automatic     |
|          | LER S         |  |         |        |          | ART DATI   | E 05/22        | 2/19    |           | COMP. D      |                |        |                 | SURFACE WATER [          | DEPTH N                  | N/A                      |            | DRILI        | L <b>ER</b> S  | mith, C        | L.      |                                  | STA                  | RT DA                   | <b>TE</b> 05/2 | 22/19     |                          | COMP. [          | DATE 05/22/1      | 9         | SURFACE WATER DEF  | TH N/A        |                  |
| ELEV     | DRIVE<br>ELEV | DEPTH  | BLO     | W CO   |          |  |                |         | R FOOT    |              |                | °.  ▼/ | L               | SOIL AND                 | ROCK DES                 | SCRIPTION                |            | CORE         | SIZE           | NX             |         |                                  | тот                  | AL RU                   | <b>N</b> 21.6  |           |                          |                  |                   |           |  |               |                  |
| (ft)     | (ft)          | (ft)   | 0.5ft   | 0.5ft  | 0.5ft    | 0  | 25<br>         | 50      | 7         | 75 10        | 0 NO.          | MOI    | G E             | LEV. (ft)                |                          |                          | DEPTH (ft) | ELEV         |                | DEPTH          | RUN     | DRILL<br>RATE                    | REC.                 | RUN<br>RQD<br>(ft)<br>% | SAMP.          | REC.      | RATA<br>RQD<br>(ft)<br>% | L                |                   |           | DESCRIPTION AND REMARK                                       | S             |                  |
|          |               |  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            | (ft)         | (ft)           | (ft)           | (ft)    | (Min/ft)                         | (II)<br>%            | (11)                    | NO.            | (II)<br>% | (II)<br>%                | G <sub>ELE</sub> | V. (ft)           |           |  |               | DEPTH (ft)       |
| 865      | _             | <b>∔</b>   |         |        |          |  |                |         |           |              |                |        | -86             |                          | UND SUR                  |                          | 0.0        | 850.7<br>850 | 850.7          | 13.6           | 1.6     | NM/1.0                           | (0.8)                | (0.5)                   |                | (6.6)     | (0.5)                    | 850              | 7                 |           | Begin Coring @ 13.6 ft<br>CRYSTALLINE ROCK                   |               | 13.6             |
|          |               | ‡  |         |        |          |  |                |         |           |              | 1 1            |        |                 | Brown, Clayey,           | ALLUVIAL<br>Silty fine S | L<br>SAND with Tra       | ce         | -            | 850.7<br>849.1 | 15.2           | 5.0     | NM/0.6<br>NM/1.0                 | _ ₹ 50%              | 31%                     | ł              | 68%       | 5%                       | — 850.<br>—      | Brown to          | Gray,     | Very Severly Weathered to Mo<br>loderately Hard, BIOTITE GNE | derately Weat | hered,           |
| 860      | 860.6         | 3.7  | MOLL    | MOLL   | WOLL     |  |                | .       |           |              |                |        |                 | . , , ,                  | Mica                     |                          |            |              | -              | Ŧ              |         | NM/1.0<br>NM/1.0                 | 62%                  | (0.0)                   |                |           |                          |                  | Close Fract       | ure Spa   | acing. (13.6-14.2' is Fresh Whit<br>GSI: 30-40               | e Plagioclase | Feldspar)        |
| 333      | -             | ŧ  | WOH     | WOH    | WOH      | 0  |                |         |           |              |                | M      |                 |                          |                          |                          |            | 845          | 844.1          | 20.2           |         | NM/1.0<br>NM/1.0                 |                      |                         |                |           |                          |                  |                   |           | GSI. 30-40   |               |                  |
|          |               | ‡  |         |        |          | \  |                |         |           |              |                |        | 8               | 56.8<br>Dark Gray, Silty | Sondy CD                 |                          | 7.5        |              | -              | ł              | 5.0     | 1:45/1.0<br>1:53/1.0<br>1:39/1.0 | )   (4.7)<br>)   94% | (1.8)<br>36%            |                |           |                          |                  |                   |           |  |               |                  |
| 855      | 855.6         | + 8.7<br>+                                       | 4       | 6      | 8        | 14   |                |         |           |              | $\perp$        |        |                 | of Organic N             | Matter (Woo              | od) and Trace            | ace        | 840          |                |                |         | 1:50/1.0                         | ) I                  |                         |                | (11.9)    | (10.4)<br>87%            | 841.             | 0<br>Gray, Ver    | y Slightl | ly Weathered to Fresh, Hard, B                               | IOTITE GNEI   | 23.3<br>SS, with |
|          |               | Ŧ  |         |        |          | : :  ; :   |                |         |           |              |                |        | 000 <b>-</b> 8! | 52.6                     | ATHERED F                | BOCK                     | 11.7       | -            | 839.1          | 25.2           | 5.0     | 1:54/1.0<br>1:42/1.0             | )   (5 0)            | (5.0)                   |                | 100%      | 87%                      |                  |                   |           | Close to Wide Fracture Spac<br>GSI: 84                       | ng            |                  |
| 850      |               | Ŧ  |         |        |          |  |                | .       |           |              |                |        | 8               | 50.7 BIC                 | OTITE GNE                | EISS                     | 13.6       |              | -              | <u> </u>       |         | 1:38/1.0<br>1:34/1.0             | ) [                  | 100%                    | RS-1           |           |                          |                  |                   |           |  |               |                  |
|          |               | Ŧ  |         |        |          |  |                |         |           |              |                |        |                 | CRY:<br>Brown to 0       | STALLINE  <br>Gray BIOTI | <b>ROCK</b><br>TE GNEISS |            | 835          | 834.1          | 30.2           |         | 1:40/1.0<br>1:42/1.0             | ) l                  |                         |                | 1         |                          |                  |                   |           |  |               |                  |
|          |               | Ŧ  |         |        |          | : :  : :   |                | .       |           |              |                |        |                 |                          | •                        |                          |            |              |                | ŧ              | 5.0     | 1:47/1.0<br>1:41/1.0<br>1:50/1.0 | )   (5.0)<br>)  100% | (3.6)                   |                |           |                          |                  |                   |           |  |               |                  |
| 845      |               | Ŧ  |         |        |          |  |                |         | · · · · · |              |                |        |                 |                          |                          |                          |            | 830          |                |                |         | 1:46/1.0                         | )                    |                         |                |           |                          | 829.             |                   |           |  |               |                  |
|          |               | Ŧ  |         |        |          |  |                | .       |           |              |                |        | 8               |                          |                          |                          |            | -            | 829.1          | 35.2           |         | 1:51/1.0                         | )                    |                         |                |           | +                        | 829.             | Boring B          | Termina   | ated at Elevation 829.1 ft in CR                             | YSTALLINE F   | OCK: 35.2        |
| 840      |               | Ŧ  |         |        |          |  | 1              | -       |           |              |                |        | 8.<br>L         | 41.0 Gray                | BIOTITE G                | SNEISS                   | 23.3       |              |                | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           | BIOTITE GNEISS   |               |                  |
|          |               | Ŧ  |         |        |          | [  |                |         |           |              |                |        |                 | •                        |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          | -                |                   |           |  |               |                  |
|          |               | ŧ  |         |        |          |  |                | .       |           |              | RS-1           | -      |                 |                          |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
| 835      |               | ╁  |         |        |          | <del>                                     </del> | <del> </del>   |         |           | <del> </del> |                |        |                 |                          |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
|          |               | ŧ  |         |        |          | <br>   |                | .       |           |              |                |        |                 |                          |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          | -                |                   |           |  |               |                  |
| 830      | _             | ŧ  |         |        |          | · · j. ·   |                | -   -   | <br>      |              |                |        |                 |                          |                          |                          |            |              |                | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
|          |               | <del>                                     </del> |         |        |          | !  |                |         |           |              |                |        | 82              | Boring Termina           |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          | -                |                   |           |  |               |                  |
|          |               | ‡  |         |        |          |  |                |         |           |              |                |        |                 | CRYSTALLINE              | ROCK: BI                 | IOTITE GNEIS             | SS         |              | -              | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
|          | -             | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
|          |               | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
|          | -             | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              |                | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
|          |               | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| 19       |               | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              | -              | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
| 6/26/    | -             | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              | _              | ‡              |         |                                  |                      |                         |                |           |                          |                  |                   |           |  |               |                  |
| GDT      |               | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              | -              | Ŧ              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| DOT.     | -             | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              |                | Ŧ              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| S        |               | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              | -              | Ŧ              |         |                                  |                      |                         |                |           |                          | l F              |                   |           |  |               |                  |
| .GPJ     |               | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              |                | Ŧ              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| GINT     | -             | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              | _              | Ŧ              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| SDG      |               | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              | -              | Ŧ              |         |                                  |                      |                         |                |           |                          | l F              |                   |           |  |               |                  |
| O_BR     | -             | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              |                | Ŧ              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| 3 GE     |               | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              | -              | Ŧ              |         |                                  |                      |                         |                |           |                          | l F              |                   |           |  |               |                  |
| R004     | :             | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              | -              | Ŧ              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| LE B     | -             | ‡  |         |        |          |  |                |         |           |              |                |        | -               |                          |                          |                          |            |              | -              | F              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| OUBI     |               | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              | -              | Ŧ              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| RE D     |               | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              |                | Ŧ              |         |                                  |                      |                         |                |           |                          | F                |                   |           |  |               |                  |
| T BO     | :             | ‡  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              | -              | Ŧ              |         |                                  |                      |                         |                |           |                          | l F              |                   |           |  |               |                  |
| NCDC     |               | Ŧ  |         |        |          |  |                |         |           |              |                |        |                 |                          |                          |                          |            |              |                | Í              |         |                                  |                      |                         |                |           |                          | E                |                   |           |  |               |                  |

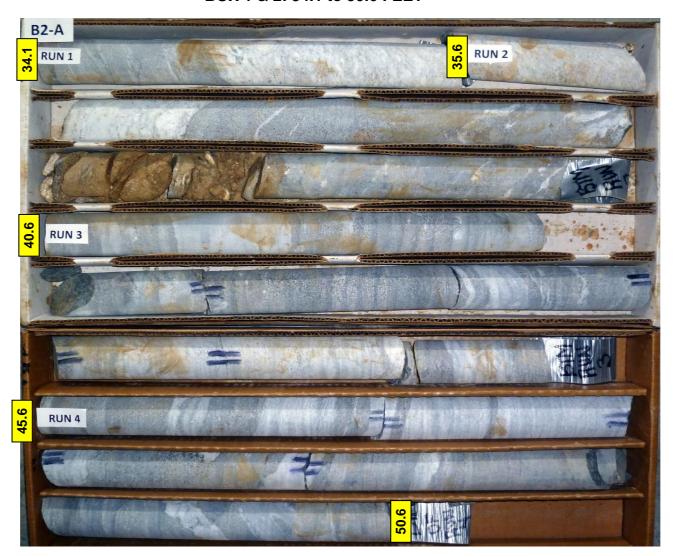
**B1-B**BOX 1: 13.6 to 35.2 FEET





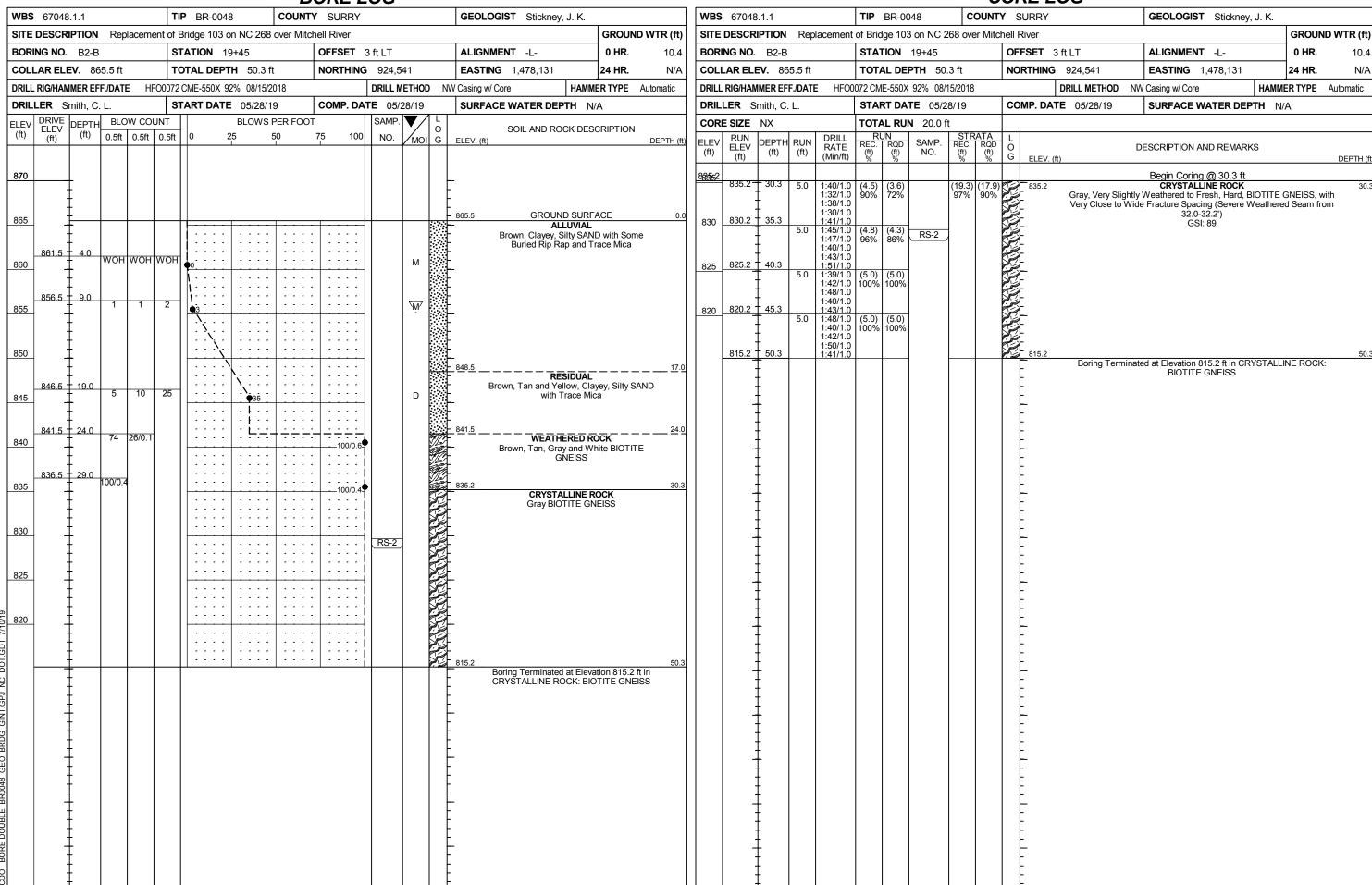


**B2-A**BOX 1 & 2: 34.1 to 50.6 FEET

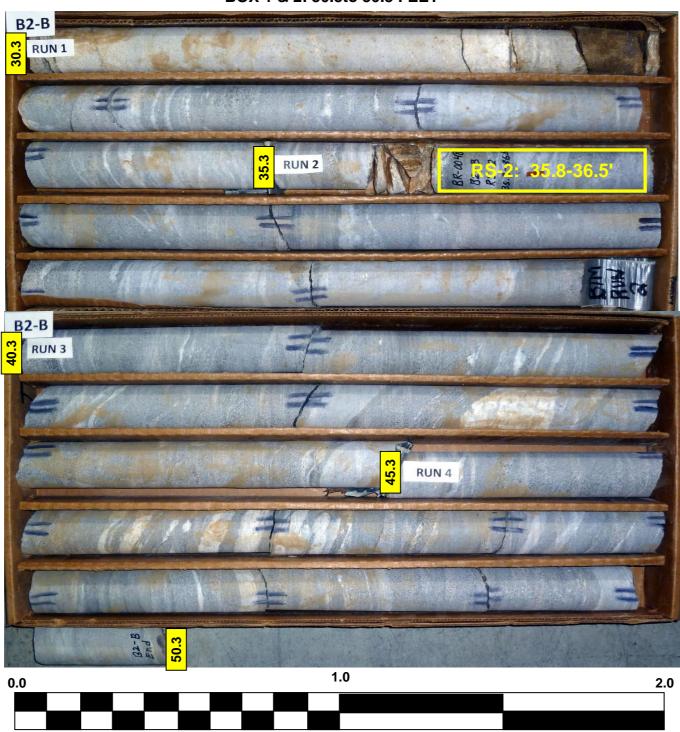




FEET



**B2-B**BOX 1 & 2: 30.3to 50.3 FEET



FEET

|              |                 |               |        |       |          |                                   |  | <u>ORE L</u>   | <u> </u> |        |              |            |                                |                                 |                       |            |
|--------------|-----------------|---------------|--------|-------|----------|-----------------------------------|--|----------------|----------|--------|--------------|------------|--------------------------------|---------------------------------|-----------------------|------------|
| WBS          | 67048           | .1.1          |        |       | TI       | <b>P</b> BR-0048                  | COUNT  | Y SURRY        |          |        |              | GEOLOGI    | ST C. Drisc                    | oll                             |                       |            |
| SITE         | DESCR           | IPTION        | Repl   | aceme | ent of B | Bridge 103 on NC 268              | over Mitch                                       | ell River      |          |        |              |            |                                |                                 | GROUN                 | D WTR (ft) |
| BOR          | ING NO.         | EB2-          | <br>В  |       | S        | <b>TATION</b> 20+00               |  | OFFSET 2       | 25 ft RT |        |              | ALIGNME    | NT -L-                         |                                 | 0 HR.                 | 31.6       |
|              | LAR ELE         |               |        |       | -+       | OTAL DEPTH 42.21                  | ft   | NORTHING       |          | )1     |              | FASTING    | 1,478,178                      |                                 | 24 HR.                | FIAD       |
|              |                 |               |        | E TDI |          | ME-55 87% 03/21/2019              |  | 11011111111    | DRILL M  |        | шс           |            | .,,                            |                                 | RTYPE                 |            |
|              |                 |               |        | L IIV |          |                                   | 10   | COMP. DA       |          |        | 11.0         |            | WATER RE                       |                                 |                       | Automatic  |
|              | LER R.<br>DRIVE |               |        | W CO  |          | TART DATE 04/15/                  |  |                | SAMP.    |        | L            | SURFACE    | WATER DE                       | PIH N/A                         | 4                     |            |
| ELEV<br>(ft) | ELEV<br>(ft)    | DEPTH<br>(ft) | 0.5ft  |       |          | 0 25                              | PER FOOT   | 75 100         | NO.      | '/     | Ö<br>G       | ELEV. (ft) | SOIL AND RO                    | OCK DESC                        | RIPTION               | DEPTH (ft) |
|              |                 |               |        |       |          |                                   |  |                |          |        |              |            |                                |                                 |                       |            |
| 890          |                 |               |        |       |          |                                   |  |                |          |        |              | 889.1      |                                | ID SURFA                        |                       | 0.0        |
|              | 887.8 -         | 1.3           | 5      | 3     | 3        |                                   |  |                |          | l , l  | - <u>-</u>   | 887.8      | ROADWAY<br>Asphalt             | <b>( EMBANK</b><br>(0.0 - 0.5 F |                       | 1.3        |
| 885          | 885.6 -         | 3.5           |        |       |          | •6                                |  |                |          | М      | <u> :</u>    | 886.1      | ABC Stone                      | è (0.5 - 1.3                    | Feet)                 | 3.0        |
| 885          | _               |               | 2      | 2     | 3        | 5                                 | +  | +              |          | М      |              | - ¦ (      | Gray and Brown                 | n, Silty Coa<br>th Trace G      |                       | e          |
|              | _               | -             |        |       |          |                                   |  |                |          | L      |              | · - (      | Orange and Bro                 |                                 |                       | i — 1      |
| 880          | 880.6 -         | 8.5           |        |       |          |                                   |  |                |          | Į      | -#           |            |                                |                                 |                       |            |
| 000          | -               | -             | 2      | 2     | 2        | 4                                 | <del> </del>                                     | <del>   </del> |          | М      |              | -          |                                |                                 |                       |            |
|              | -               | -             |        |       |          |                                   |  |                |          | L      | -84-         |            |                                |                                 |                       |            |
| 875          | 875.6 -         | 13.5          |        |       |          | (                                 |  |                |          | Į      | -            |            |                                |                                 |                       |            |
| 0/5          | -               | -             | 2      | 2     | 3        | 5                                 | <del> </del>                                     | <del>   </del> |          | М      |              | -          |                                |                                 |                       |            |
|              | -               | -             |        |       |          |                                   |  |                |          | L      | -  } -       |            |                                |                                 |                       |            |
| 870          | 870.6 -         | 18.5          |        |       |          |                                   |  |                |          | Ĺ      |              |            |                                |                                 |                       |            |
| 670          | -               | -             | WOH    | 2     | 3        | 5                                 | <del>                                     </del> | <del>   </del> |          | М      | ""           | -          |                                |                                 |                       |            |
|              | -               | -             |        |       |          |                                   |  |                |          | L      | -81          |            |                                |                                 |                       |            |
| 005          | 865.6 -         | 23.5          |        |       |          | 1 : : :   : : : :                 |  |                |          | Ĺ      | -Wt          |            |                                |                                 |                       |            |
| 865          |                 | -             | 2      | 3     | 4        | <del>  •</del> 7                  | +  | +              |          | М      | _   -        | -          |                                |                                 |                       |            |
|              | _               | F             |        |       |          |                                   |  |                |          | L      | - <b>   </b> |            |                                |                                 |                       |            |
|              | -<br>860.6 -    | 28.5          |        |       |          |                                   |  |                |          | إ      |              | 861.1      |                                |                                 |                       | 28.0       |
| 860          | - 000.0         | 20.5          | 2      | 2     | 2        | 4                                 | <del> </del>                                     |                |          | М      |              | _          | <b>Al</b><br>Brown             | LUVIAL<br>, Fine SAN            | 1D                    |            |
|              | -               | -             |        |       |          | 1   1   1   1   1   1   1   1   1 |  |                |          |        |              |            |                                | ,                               |                       |            |
|              | -<br>855.6 -    | 33.5          |        |       |          | :\: : :   : : : :                 |  |                |          |        |              | 856.1      |                                |                                 |                       | 33.0       |
| 855          | - 655.0         | - 55.5        | 2      | 2     | 9        |                                   | <del> </del>                                     | <del> </del>   |          | М      | ▓┢           | -          |                                | SIDUAL ine Sandy                | SILT                  |            |
|              | -               | ļ             |        |       |          | ::::::                            |  |                |          | ****** |              |            | 2.0, .                         |                                 | 0.2.                  |            |
|              | -<br>850.6 -    | -<br>- 38.5   |        |       |          | :::::\.::::                       |  |                |          | 3.500  | 鮲            |            |                                |                                 |                       |            |
| 850          | - 650.6         | 30.5          | 12     | 22    | 13       | 35                                | <del> </del>                                     | <del> </del>   |          | Sat.   | ₩            | -          |                                |                                 |                       |            |
|              | _               | ļ             |        |       |          |                                   |  |                |          | 100000 | **           |            |                                |                                 |                       |            |
|              | 846.9           | 42.2          | 60/0.0 |       |          |                                   |  | 60/0.0         | 4        |        |              | 846.9<br>B | oring Terminat                 | ed WITH                         | STANDAR               | 42.2<br>D  |
|              |                 |               |        |       |          |                                   |  |                |          |        |              | _          | PENETRATIOI<br>Elevation 846.9 | N TEST R                        | EFUSAL a<br>'STALLINE | t          |

SHEET 15

#### LABORATORY SUMMARY SHEET FOR ROCK CORE SAMPLES

SHEET 16

PROJECT NO.: 67048.1.1 (BR-0048)

**COUNTY: SURRY** 

REPLACEMENT OF BRIDGE NO. 103 ON NC 268 OVER MITCHELL RIVER

| Sample No. | Boring No. | Depth (ft) | Rock Type      | Geologic Map<br>Unit | Run RQD<br>(%) | Length (in) | Diameter<br>(in) | Wet Unit<br>Weight<br>(lbf/ft <sup>3</sup> ) | Unconfined<br>Compressive<br>Strength (ksi) | Young's<br>Modulus (psi) | Splitting Tensile<br>Strength (psi) | Remarks |
|------------|------------|------------|----------------|----------------------|----------------|-------------|------------------|--|---|--------------------------|-------------------------------------|---------|
| RS-1       | B1-B       | 27.3-27.8  | Biotite Gneiss | CZmg                 | 100            | 3.70        | 1.86             | 174.7  | 11.68                                       | N/A                      | N/A                                 | GSI 84  |
| RS-2       | B2-B       | 35.8-36.5  | Biotite Gneiss | CZmg                 | 90             | 3.69        | 1.86             | 169.9  | 16.05                                       | N/A                      | N/A                                 | GSI 89  |

# WBS NO.: 67048.1.1 - TIP NO.: BR-0048 REPLACEMENT OF BRIDGE NO. 103 ON NC 268 OVER MITCHELL RIVER SITE PHOTOGRAPHS



View from End Bent 1 Looking East



View from Downstream Side of Bridge