



STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION

ROY COOPER  
GOVERNOR

J. ERIC BOYETTE  
SECRETARY

July 1, 2020

MEMORANDUM TO: Brenda L. Moore, P.E., CPM  
State Roadway Design Engineer

ATTENTION: David Stutts, PE  
Project Engineer – PEF/Program Mgt.

FROM:   John L. Pilipchuk, L.G., P.E.  
State Geotechnical Engineer

DocuSigned by:  
*John L. Pilipchuk*  
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STATE PROJECT: 45693.1.1 (B-5737)  
COUNTY: Rockingham

DESCRIPTION: Replace Bridge No. 108 on US 311 & NC 700 over US 311, NC  
14, NC 87 and NC 770

SUBJECT: Geotechnical Recommendations

The Geotechnical Engineering Unit has reviewed and presents the subsurface investigation and foundation recommendations prepared by Kleinfelder Inc. for the above referenced project.

- Roadway Subsurface Investigation (18) pages
- Geotechnical Report - Recommendations (3) pages
- Click here to enter text. (# Of Pages) pages

Please call John McCray at (919) 707-6890 or David Teague, PE at (919) 707-6877 if there are any questions concerning this memorandum.

Attachment

Roadway Subsurface Investigation  
Geotechnical Report – Recommendations

Cc:

Jacquelyn K. Bowles. PE – PEF Coordination

REFERENCE: B-5737

PROJECT: 36637

SEE SHEET 3 FOR PLAN SHEET LAYOUT  
AT TIME OF INVESTIGATION

**STATE OF NORTH CAROLINA**  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	B-5737	1	15

**CAUTION NOTICE**

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

- NOTES:
1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
  2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

**ROADWAY**  
**SUBSURFACE INVESTIGATION**

COUNTY ROCKINGHAM

PROJECT DESCRIPTION REPLACE BRIDGE NO. 108 ON  
US 311 & NC 700 OVER US 311, NC 14, NC 87  
AND NC 770

**INVENTORY**

**CONTENTS**

LINE	STATION	PLAN	PROFILE
-L-	17+00.00 - 25+00.00	4	N/A
-RPA-	10+00.00 - 12+54.82	4	N/A
-DET-	17+67.80 - 24+17.64	4	N/A

**CROSS SECTIONS**

LINE	STATION	SHEETS
-L-	18+00.00 - 23+50.00	5-8
-RPA-	10+50.00 - 12+00.00	9-10
-DET-	18+00.00 - 24+00.00	11-13

**APPENDICES**

APPENDIX	TITLE	SHEETS
A	LABORATORY RESULTS	14-15

PERSONNEL

C. DRISCOLL

TRIGON EXPLORATION

INVESTIGATED BY C. DRISCOLL

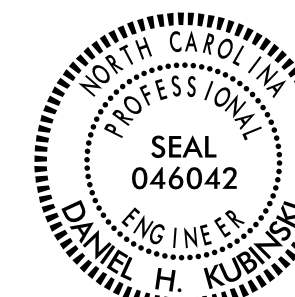
DRAWN BY C. DRISCOLL

CHECKED BY D. KUBINSKI

SUBMITTED BY KLEINFELDER, INC

DATE MAY 2020

Prepared in the Office of:







DocuSigned by:

Daniel Kubinski

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**DOCUMENT NOT CONSIDERED FINAL  
UNLESS ALL SIGNATURES COMPLETED**

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT  
**SUBSURFACE INVESTIGATION**  
SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION										GRADATION										ROCK DESCRIPTION										TERMS AND DEFINITIONS																			
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 208, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i>										<b>WELL GRADED</b> - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. <b>UNIFORMLY GRADED</b> - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. <b>GAP-GRADED</b> - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.										<b>HARD ROCK</b> IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:										<b>ALLUVIUM (ALLUV.)</b> - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. <b>AQUIFER</b> - A WATER BEARING FORMATION OR STRATA. <b>ARENACEOUS</b> - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. <b>ARGILLACEOUS</b> - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. <b>ARTESIAN</b> - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. <b>CALCAREOUS (CALC.)</b> - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. <b>COLLUVIUM</b> - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. <b>CORE RECOVERY (REC.)</b> - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. <b>DIKE</b> - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. <b>DIP</b> - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. <b>DIP DIRECTION (DIP AZIMUTH)</b> - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. <b>FAULT</b> - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. <b>FISSILE</b> - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. <b>FLOAT</b> - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOADED FROM PARENT MATERIAL. <b>FLOOD PLAIN (FP)</b> - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. <b>FORMATION (FM)</b> - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. <b>JOINT</b> - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. <b>LEDGE</b> - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. <b>LENS</b> - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. <b>MOTTLED (MOT.)</b> - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. <b>PERCHED WATER</b> - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. <b>RESIDUAL (RES.) SOIL</b> - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. <b>ROCK QUALITY DESIGNATION (RQD)</b> - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. <b>SAPROLITE (SAP.)</b> - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. <b>SILL</b> - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. <b>SLICKENSIDE</b> - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. <b>STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT)</b> - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. <b>STRATA CORE RECOVERY (SREC.)</b> - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. <b>STRATA ROCK QUALITY DESIGNATION (SROD)</b> - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. <b>TOPSOIL (TS.)</b> - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.																			
<b>SOIL LEGEND AND AASHTO CLASSIFICATION</b>										<b>ANGULARITY OF GRAINS</b> THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: <b>ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.</b>										<b>WEATHERED ROCK (WR)</b>  NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.										<b>CRYSTALLINE ROCK (CR)</b>  FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.																			
<b>MINERALOGICAL COMPOSITION</b> MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.										<b>COMPRESSION</b> SLIGHTLY COMPRESSIBLE LL < 31 MODERATELY COMPRESSIBLE LL = 31 - 50 HIGHLY COMPRESSIBLE LL > 50										<b>NON-CRYSTALLINE ROCK (NCR)</b>  FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.										<b>COASTAL PLAIN SEDIMENTARY ROCK (CP)</b>  COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.																			
<b>PERCENTAGE OF MATERIAL</b>										<b>GROUND WATER</b>										<b>WEATHERING</b>										<b>PERCHED WATER</b> - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.																			
<b>TEXTURE OR GRAIN SIZE</b>										<b>MISCELLANEOUS SYMBOLS</b>										<b>ROCK HARDNESS</b>										<b>RECOMMENDATION SYMBOLS</b>																			
U.S. STD. SIEVE SIZE OPENING (MM): 4, 10, 40, 60, 200, 270 4.75, 2.00, 0.42, 0.25, 0.075, 0.053										ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION SOIL SYMBOL ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT INFERRED SOIL BOUNDARY INFERRED ROCK LINE ALLUVIAL SOIL BOUNDARY										ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. IF TESTED, WOULD YIELD SPT REFUSAL ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. FABRIC MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.										UNDERCUT SHALLOW UNDERCUT UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL																			
<b>SOIL MOISTURE - CORRELATION OF TERMS</b>										<b>ABBREVIATIONS</b>										<b>SOIL MOISTURE SCALE (ATTERBERG LIMITS)</b>										<b>EQUIPMENT USED ON SUBJECT PROJECT</b>																			
SOIL MOISTURE SCALE (ATTERBERG LIMITS) FIELD MOISTURE DESCRIPTION GUIDE FOR FIELD MOISTURE DESCRIPTION										AR - AUGER REFUSAL BT - BORING TERMINATED CL - CLAY CPT - COARSE PENETRATION TEST CSE - COARSE DMT - DILATOMETER TEST DPT - DYNAMIC PENETRATION TEST e - VOID RATIO F - FINE FOSS. - FOSSILIFEROUS FRAC. - FRACTURED, FRACTURES FRAGS. - FRAGMENTS HI. - HIGHLY										LL - LIQUID LIMIT PL - PLASTIC LIMIT OM - OPTIMUM MOISTURE SHRINKAGE LIMIT										MED. - MEDIUM MICA - MICACEOUS MOD. - MODERATELY NP - NON PLASTIC ORG. - ORGANIC PMT - PRESSUREMETER TEST SAP. - SAPROLITIC SD. - SAND, SANDY SL. - SILTY, SILTY SLI. - SLIGHTLY TCR - TRICONE REFUSAL w - MOISTURE CONTENT V - VERY										VST - VANE SHEAR TEST WEA. - WEATHERED UG - UNIT WEIGHT UG - DRY UNIT WEIGHT SAMPLE ABBREVIATIONS S - BULK SS - SPLIT SPOON ST - SHELBY TUBE RS - ROCK RT - RECOMPACTED TRIAXIAL CBR - CALIFORNIA BEARING RATIO									
<b>PLASTICITY</b>										<b>FRACATURE SPACING</b>										<b>BEDDING</b>										<b>INDURATION</b>																			
NON PLASTIC SLIGHTLY PLASTIC MODERATELY PLASTIC HIGHLY PLASTIC										VERY WIDE MORE THAN 10 FEET WIDE 3 TO 10 FEET MODERATELY CLOSE 1 TO 3 FEET CLOSE 0.16 TO 1 FOOT VERY CLOSE LESS THAN 0.16 FEET										VERY THICKLY BEDDED 4 FEET THICKLY BEDDED 1.5 - 4 FEET THINLY BEDDED 0.16 - 1.5 FEET VERY THINLY BEDDED 0.03 - 0.16 FEET THICKLY LAMINATED 0.008 - 0.03 FEET THINLY LAMINATED < 0.008 FEET										FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE. MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER. INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER. EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.																			
<b>COLOR</b>										<b>DRILL UNITS:</b>										<b>ADVANCING TOOLS:</b>										<b>HAMMER TYPE:</b>																			
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.										<input type="checkbox"/> CME-45C <input checked="" type="checkbox"/> CME-55 <input type="checkbox"/> CME-550 <input type="checkbox"/> VANE SHEAR TEST <input type="checkbox"/> PORTABLE HOIST										<input type="checkbox"/> CLAY BITS <input type="checkbox"/> 6" CONTINUOUS FLIGHT AUGER <input checked="" type="checkbox"/> 8" HOLLOW AUGERS <input type="checkbox"/> HARD FACED FINGER BITS <input type="checkbox"/> TUNG-CARBIDE INSERTS <input checked="" type="checkbox"/> CASING <input checked="" type="checkbox"/> W/ ADVANCER <input type="checkbox"/> TRICONE *STEEL TEETH <input checked="" type="checkbox"/> TRICONE 2 1/2% *TUNG-CARB. <input type="checkbox"/> CORE BIT										<input checked="" type="checkbox"/> AUTOMATIC <input type="checkbox"/> MANUAL CORE SIZE: <input type="checkbox"/> -B <input type="checkbox"/> -H <input checked="" type="checkbox"/> -N Q2 HAND TOOLS: <input type="checkbox"/> POST HOLE DIGGER <input checked="" type="checkbox"/> HAND AUGER <input type="checkbox"/> SOUNDING ROD <input type="checkbox"/> VANE SHEAR TEST																			
<b>NOTES:</b>										<b>FRACATURE SPACING</b>										<b>BEDDING</b>										<b>INDURATION</b>																			
FIAD - FILLED IMMEDIATELY AFTER DRILLING BRIDGE AND RETAINING WALL BORING ELEVATIONS WERE OBTAINED USING THE BENCH MARK NOTED ABOVE. ROADWAY BORING ELEVATIONS WERE OBTAINED USING THE PROJECT TIN FILE, B5737.LS.TIN.170209 RECEIVED ON APRIL 13, 2020.										BENCH MARK: BL-4 AT STA. 19+93.69 -L- 27' LT (1,004,300.90 N., 1,780,953.48 FT.E) ELEVATION: 659.61 FEET										BENCH MARK: BL-4 AT STA. 19+93.69 -L- 27' LT (1,004,300.90 N., 1,780,953.48 FT.E) ELEVATION: 659.61 FEET										BENCH MARK: BL-4 AT STA. 19+93.69 -L- 27' LT (1,004,300.90 N., 1,780,953.48 FT.E) ELEVATION: 659.61 FEET																			

**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT**

# **SUBSURFACE INVESTIGATION**

**SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES  
FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS**

AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

<p><b>GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000)</b></p> <p>From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.</p> <p><b>STRUCTURE</b></p>	<p><b>SURFACE CONDITIONS</b></p>	<p><b>VERY GOOD</b> Very rough, fresh unweathered surfaces</p>	<p><b>GOOD</b> Rough, slightly weathered, iron stained surfaces</p>	<p><b>FAIR</b> Smooth, moderately weathered and altered surfaces</p>	<p><b>POOR</b> Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments</p>	<p><b>VERY POOR</b> Slickensided, highly weathered surfaces with soft clay coatings or fillings</p>						
<p><b>GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000)</b></p> <p>From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.</p> <p><b>COMPOSITION AND STRUCTURE</b></p>	<p><b>SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes)</b></p>	<p><b>VERY GOOD</b> - Very Rough, fresh unweathered surfaces</p>	<p><b>GOOD</b> - Rough, slightly weathered surfaces</p>	<p><b>FAIR</b> - Smooth, moderately weathered and altered surfaces</p>	<p><b>POOR</b> - Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments</p>	<p><b>VERY POOR</b> - Very smooth, slickensided or highly weathered surfaces with soft clay coatings or fillings</p>						
<p><b>DECREASING INTERLOCKING OF ROCK PIECES</b></p> <div style="display: flex; flex-direction: column; gap: 5px;"> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>INTACT OR MASSIVE</b> - intact rock specimens or massive in situ rock with few widely spaced discontinuities</p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>BLOCKY</b> - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets</p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>VERY BLOCKY</b> - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets</p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>BLOCKY/DISTURBED/SEAMY</b> - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity</p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>DISINTEGRATED</b> - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces</p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>LAMINATED/SHEARED</b> - Lack of blockiness due to close spacing of weak schistosity or shear planes</p> </div> </div> </div>	<p>DECREASING SURFACE QUALITY →</p>	<p>90</p>	<p>80</p>	<p>70</p>	<p>60</p>	<p>50</p>	<p>40</p>	<p>30</p>	<p>20</p>	<p>10</p>	<p>N/A</p>	<p>N/A</p>
<div style="display: flex; flex-direction: column; gap: 5px;"> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>A. Thick bedded, very blocky sandstone</b> The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.</p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>B. Sandstone with thin inter-layers of siltstone</b></p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>C. Sandstone and siltstone in similar amounts</b></p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>D. Siltstone or silty shale with sandstone layers</b></p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>E. Weak siltstone or clayey shale with sandstone layers</b></p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure</b></p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers</b></p> </div> </div> <div style="display: flex; align-items: center;"> <div style="font-size: 0.8em;"> <p><b>H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces.</b></p> </div> </div> </div> <p style="font-size: 0.8em; margin-top: 5px;">→ Means deformation after tectonic disturbance</p>	<p>70</p>	<p>60</p>	<p>50</p>	<p>40</p>	<p>30</p>	<p>20</p>	<p>10</p>	<p>N/A</p>	<p>N/A</p>			

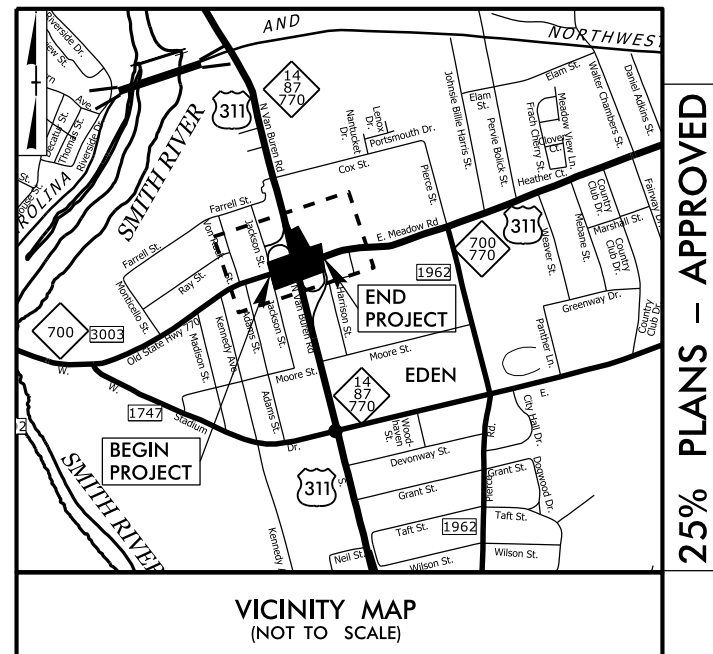
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N.C.	B-5737	3	15
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
45693.1.1	N/A	PE	

STATE OF NORTH CAROLINA  
DIVISION OF HIGHWAYS

# ROCKINGHAM COUNTY

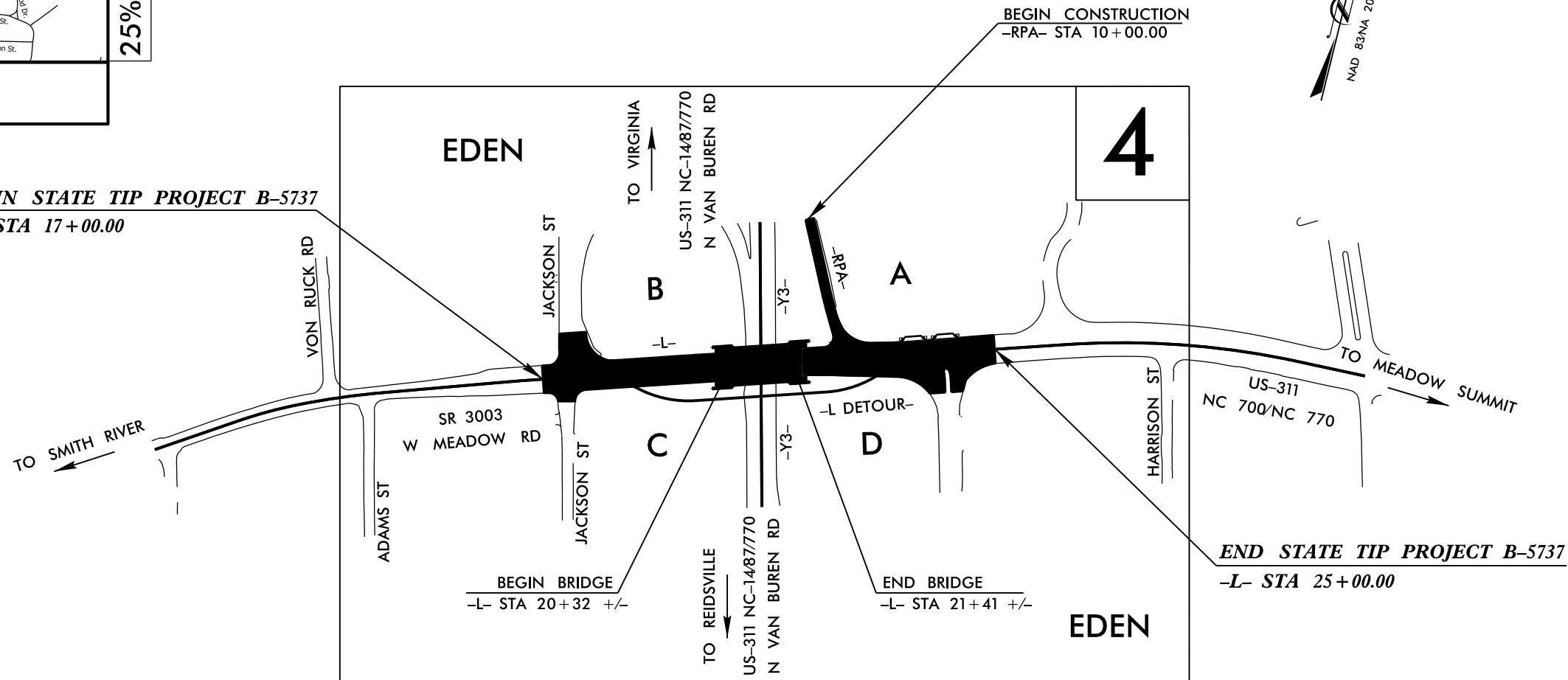
**LOCATION: REPLACE BRIDGE NO. 108 OVER US 311 / NC 14 / NC 87 / NC 770  
ON US 311 / NC 700 / NC 770, SR 3003 (W. MEADOW RD)**

**TYPE OF WORK: GRADING, DRAINAGE, PAVING AND STRUCTURE**



25% PLANS - APPROVED

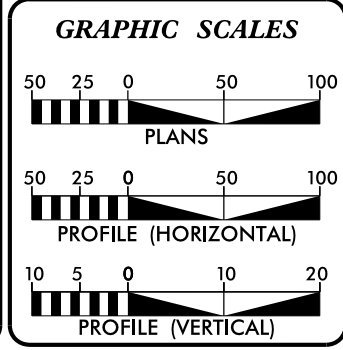
BEGIN STATE TIP PROJECT B-5737  
-L- STA 17+00.00



THERE IS NO CONTROL OF ACCESS ON THIS PROJECT.  
CLEARING ON THIS PROJECT SHALL BE PERFORMED TO THE LIMITS ESTABLISHED BY METHOD \_\_\_\_\_  
THIS PROJECT IS WITHIN THE MUNICIPAL BOUNDARIES OF EDEN

**INCOMPLETE PLANS**  
DO NOT USE FOR R/W ACQUISITION  
DOCUMENT NOT CONSIDERED FINAL  
UNLESS ALL SIGNATURES COMPLETED

**CONTRACT:**



**DESIGN DATA**

ADT 2020 =	11,300
ADT 2040 =	12,100
K =	8 %
D =	55 %
T =	14 % *
V =	40 MPH
* TTST =	12% DUAL = 2%
FUNC CLASS =	MINOR-ARTERIAL REGIONAL TIER

**PROJECT LENGTH**

LENGTH ROADWAY TIP PROJECT B-5753 =	0.131
LENGTH STRUCTURE TIP PROJECT B-5753 =	0.021
TOTAL LENGTH TIP PROJECT B-5753 =	0.152

Prepared for NCDOT In the Office of:

**moftatt & nichol**  
4700 FALLS OF NEUSE ROAD, SUITE 300  
RALEIGH, NORTH CAROLINA 27609  
1919/181-4655 VOICE 1919/181-4869 FAX  
NC License NO.: F-0105

2018 STANDARD SPECIFICATIONS

RIGHT OF WAY DATE: MAY 19, 2020

LETTING DATE: MAY 18, 2021

TIM REID, PE  
PROJECT ENGINEER

TRENT HUFFMAN, PE  
PROJECT DESIGN ENGINEER

DAVID STUTTS, P.E.  
NCDOT CONTACT

HYDRAULICS ENGINEER

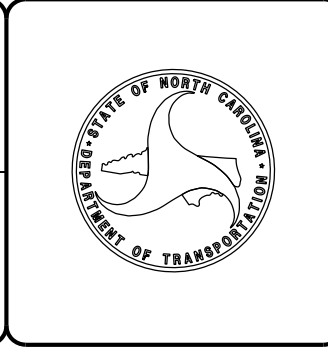
**moftatt & nichol**

SIGNATURE: \_\_\_\_\_ P.E.

ROADWAY DESIGN ENGINEER

**moftatt & nichol**

SIGNATURE: \_\_\_\_\_ P.E.



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May 21, 2020

STATE PROJECT: 45693.1.1 (B-5737)  
 COUNTY: Rockingham  
 DESCRIPTION: Replace Bridge No. 108 on US 311 & NC 700 over US 311, NC 14, NC 87 and NC 770

**SUBJECT: GEOTECHNICAL REPORT - INVENTORY**

**PROJECT DESCRIPTION**

This project consists of a widening of US 311 & NC 700 (-L-) and replacement of Bridge No. 108 over US 311, NC 14, NC 87 and NC 770 (-Y3-). For Bridge No. 108, retaining walls will be constructed at each end bent. This project will also include the widening of ramp A (-RPA-).

The geotechnical investigation was conducted in April 2020. Standard Penetration Test borings were advanced with a CME-55 drill rig with an automatic hammer. Hand Augers were also performed in areas where the use of a drill rig was restricted or underground and overhead utility conflicts were observed. Representative soil samples were collected for visual classification in the field and selected samples were submitted for laboratory analysis by Kleinfelder, Inc.

The following alignments, totaling 0.32 miles, were investigated. Plan sheets and cross sections of these alignments are included in this report.

<u>LINE</u>	<u>STATIONS</u>
-L-	17+00 to 25+00
-RPA-	10+00 to 12+55
-DET-	17+68 to 24+18

**PHYSIOGRAPHY AND GEOLOGY**

The project is located in the Piedmont Physiographic Province. The project corridor is comprised primarily of urban properties. The general topography along the project is flat to gently sloping.

Geologically, the project area is located within the Dan River Triassic Basin. The basin consists of the Dan River Group divided into the Stoneville and Cow Branch Formations filled with sedimentary rocks as streams carried mud, silt, sand, and gravel from adjacent highlands into rift valleys. Triassic sedimentary rocks are mapped as conglomerate, sandstone, and mudstone.

Surface water is drained from the corridor by the existing roadway ditches and stormwater drainage grates with outlet culverts.

**SOIL PROPERTIES**

Soils encountered during this investigation are separated into two categories based on origin. They consist of Artificial Fill and Triassic residual soil.

Artificial Fill soils are present along the existing roadways on the project in landscaping areas. The artificial soils encountered generally consist of moist, loose, non plastic, silty sand (A-2-4). The plasticity index of the Artificial Fill sand tested was 3.

Triassic residual soils are derived from the weathering of underlying Triassic conglomerate, sandstone, and mudstone. The majority of the Triassic residual soils encountered consist of moist, medium stiff, slightly to moderately plastic, sandy silts (A-4) and sandy clays (A-6), wet, loose, non plastic, sands (A-1), and dry to saturated, loose to very dense, non plastic, silty sands (A-2-4) with rock fragments. The plasticity index of the Triassic residual silt and sand tested are 8 and 2, respectively.

**ROCK PROPERTIES**

Weathered rock was encountered along the existing roadways (-L-) at elevations ranging from 640.6 to 655.7 feet (MSL). Non-crystalline bedrock was encountered along the existing roadways (-L-) at elevations ranging from 630.5 to 654.6 feet (MSL). The weathered rock and non-crystalline bedrock consists of Triassic sandstone, and mudstone.

The weathered rock and non-crystalline bedrock of the Triassic Basin is typically considered degradable rock. Degradable rock will deteriorate when exposed to air and water once exposed in cuts or excavations.

**GROUNDWATER**

Groundwater was encountered at elevations ranging from 648.0 to 656.2 feet and typically ranges from 3.5 to 3.7 feet below the existing ground surface. Due to the nature of the soils and time of the groundwater readings, the groundwater encountered may be perched groundwater rather than the static groundwater table.

**AREAS OF SPECIAL GEOTECHNICAL INTEREST**

1) Groundwater: The following areas exhibit a high water table, seasonal high groundwater or the potential for groundwater related construction problems:

<u>LINE</u>	<u>STATIONS</u>	<u>OFFSETS</u>
-L-	17+00 to 19+00	LT, RT
-RPA-	10+00 to 11+25	LT, RT

2) Artificial Fill: Artificial Fill was encountered on the project at the following locations:

<u>LINE</u>	<u>STATIONS</u>	<u>OFFSETS</u>
-L-	19+95 to 20+50	LT
-L-	20+05 to 20+45	RT
-L-	21+30 to 21+80	LT
-L-	21+15 to 22+80	RT
-L-	23+10 to 23+70	RT

3) Weathered Rock and Non-Crystalline Rock: The following areas exhibit shallow non-crystalline rock within 6 feet of the proposed grade (including at or above the proposed grades):

<u>LINE</u>	<u>STATIONS</u>	<u>OFFSETS</u>
-L-	21+41 to 22+75	RT
-RPA-	11+25 to 12+25	LT, RT

Prepared by,  
**KLEINFELDER, INC.**  
NC License No. F-1312



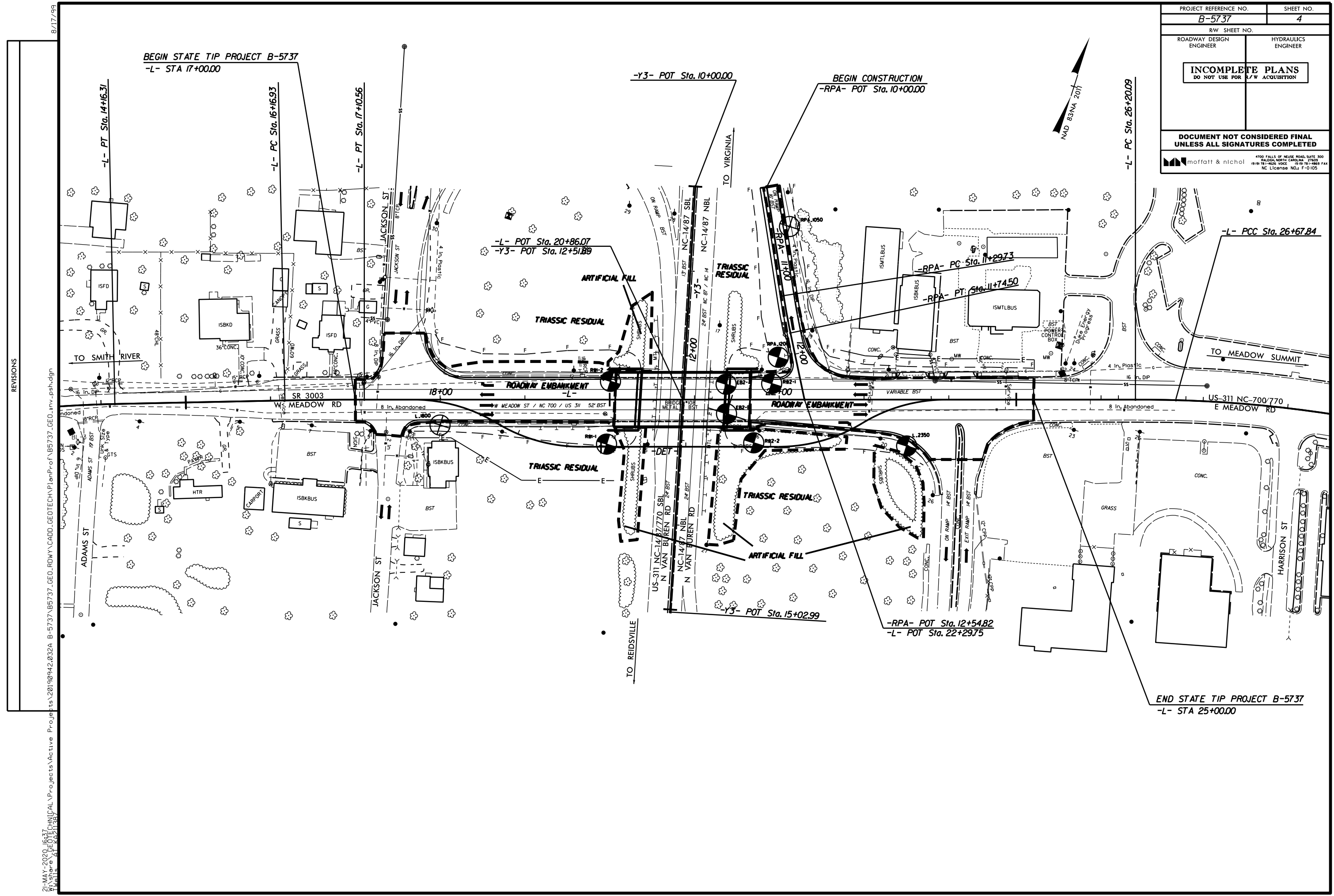
F. Christopher Driscoll, GIT  
Staff Professional

FCD/DHK:asp



Daniel H. Kubinski, PE  
Staff Professional

PROJECT REFERENCE NO. <b>B-5737</b>	SHEET NO. <b>4</b>
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR A/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	
<small>4700 FALLS OF NEUSE ROAD, SUITE 200 RALEIGH, NORTH CAROLINA 27609 919 781-4626 VOICE 919 781-4669 FAX NC License No. F-0105</small>	

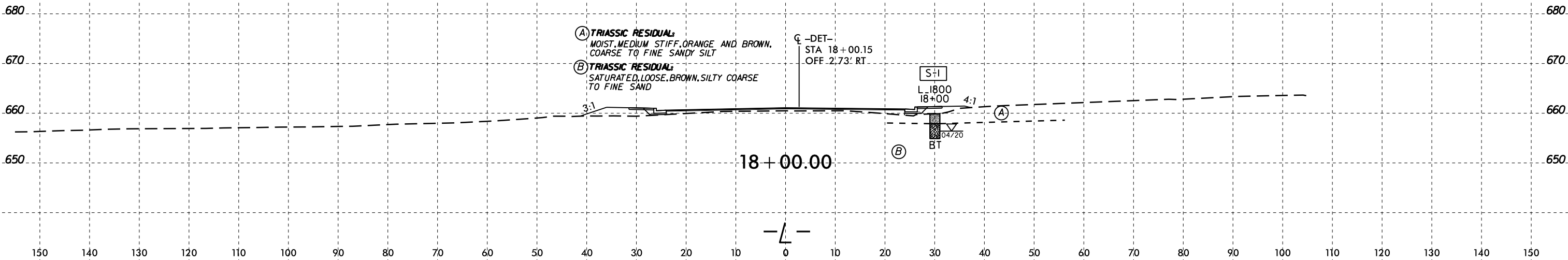


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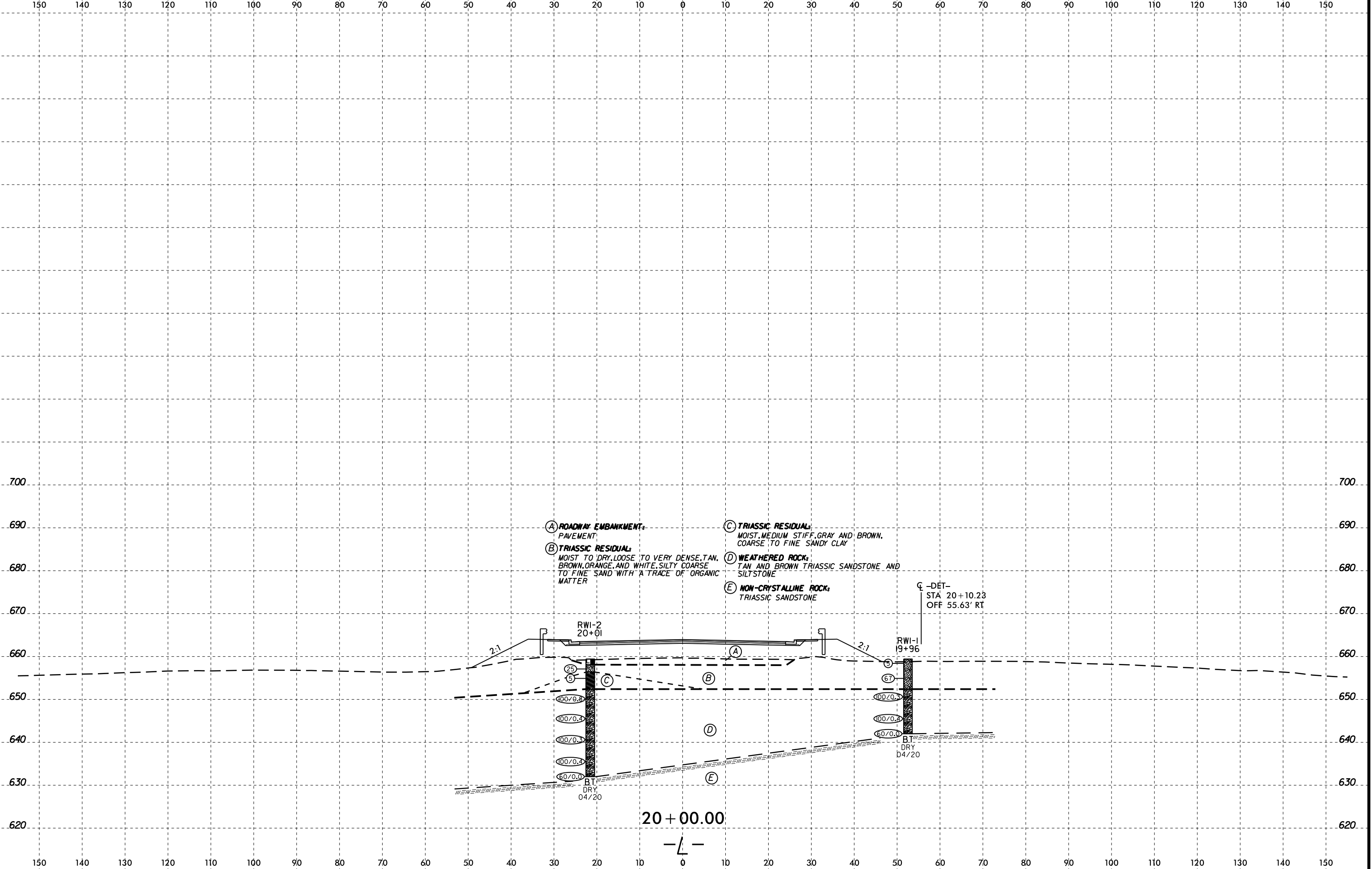




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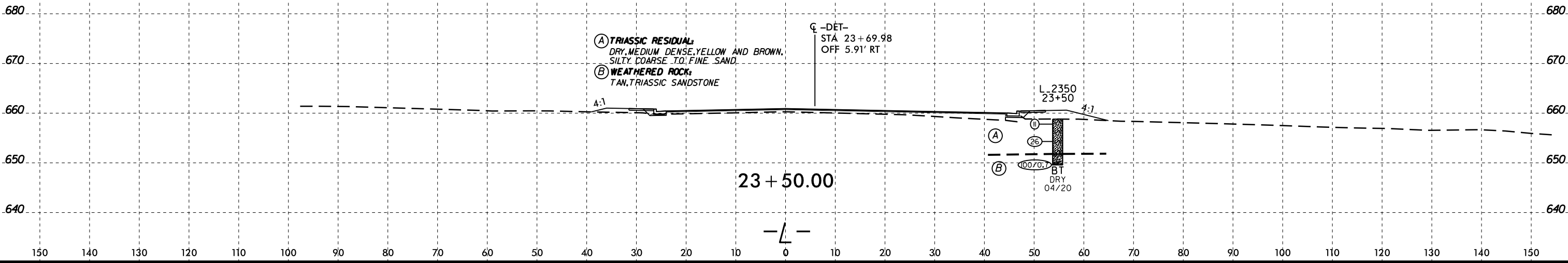
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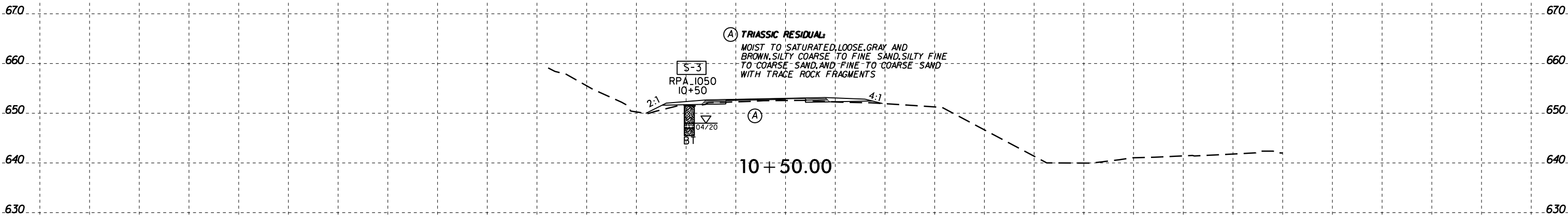
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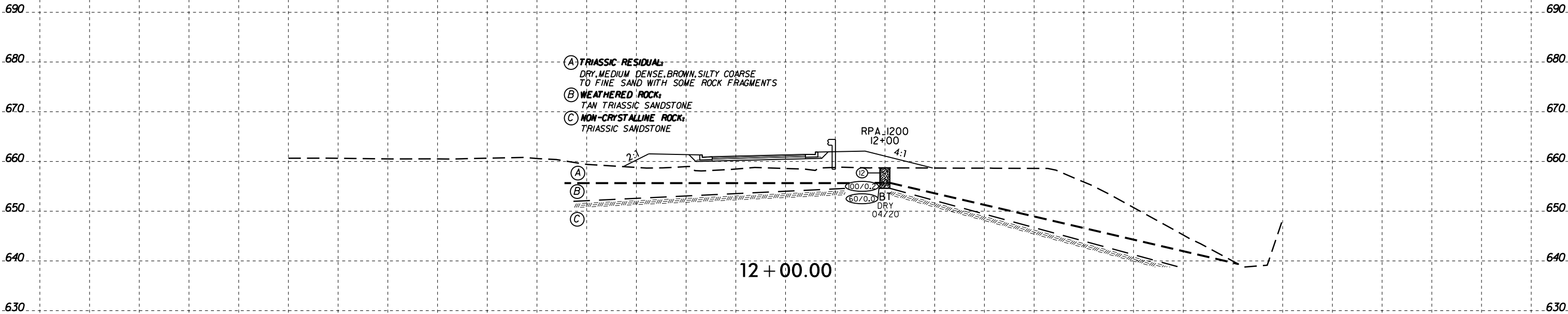


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(A) **TRIASSIC RESIDUAL**  
 MOIST TO SATURATED, LOOSE, GRAY AND  
 BROWN, SILTY COARSE TO FINE SAND, SILTY FINE  
 TO COARSE SAND, AND FINE TO COARSE SAND  
 WITH TRACE ROCK FRAGMENTS

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



- (A) **FRIASSIC RESIDUAL**  
DRY, MEDIUM DENSE, BROWN, SILTY COARSE TO FINE SAND WITH SOME ROCK FRAGMENTS
- (B) **WEATHERED ROCK**  
TAN TRIASSIC SANDSTONE
- (C) **NON-CRYSTALLINE ROCK**  
TRIASSIC SANDSTONE

RPA 1200  
12+00

BT  
04720

12 + 00.00

-RPA-

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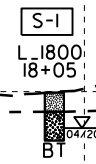


150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

680  
670  
660  
650

680  
670  
660  
650

- (A) TRIASSIC RESIDUALs  
MOIST, MEDIUM STIFF, ORANGE AND BROWN,  
COARSE TO FINE SANDY SILT
- (B) TRIASSIC RESIDUALs  
SATURATED, LOOSE, BROWN, SILTY COARSE  
TO FINE SAND



18+00.00

-DET-

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

700

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630

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

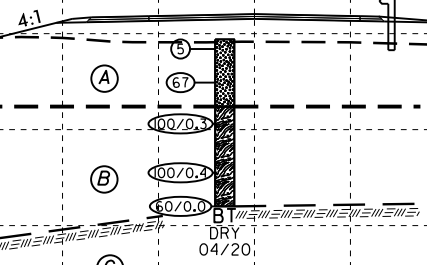
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 Wells - AT KA211387

EXIST EOT

EXIST EOT

- (A) TRIASSIC RESIDUAL  
MOIST TO DRY, LOOSE TO VERY DENSE, TAN, BROWN, ORANGE, AND WHITE, SILTY COARSE TO FINE SAND WITH A TRACE OF ORGANIC MATTER
- (B) WEATHERED ROCK  
BROWN TRIASSIC SANDSTONE
- (C) NON-CRYSTALLINE ROCK  
TRIASSIC SANDSTONE

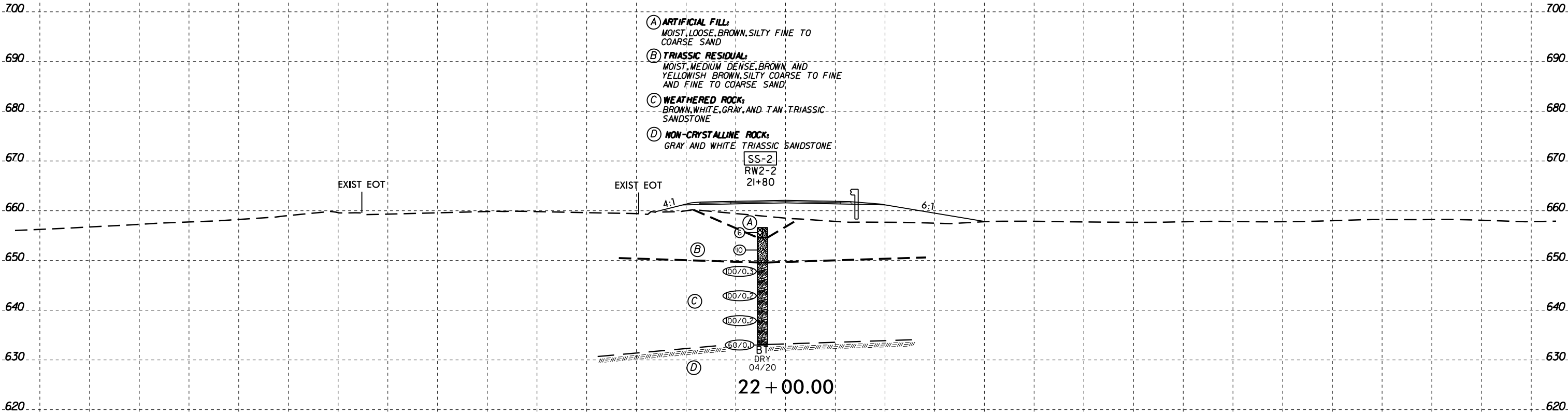
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-DET-

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT  
SUBSURFACE INVESTIGATION  
APPENDIX A  
LABORATORY RESULTS

REFERENCE: B-5737

PROJECT: 36637

Prepared in the Office of:



**LABORATORY SUMMARY SHEET FOR SOIL SAMPLES**

**PROJECT NO.: 45693.1.1 (B-5737)**  
**COUNTY: ROCKINGHAM**  
**REPLACE BRIDGE NO. 108 ON US 311 & NC 700 OVER US 311, NC 14, NC 87 AND NC 770**

Sample No.	Boring Number	Alignment	Station	Offset	Sample Depth (ft.)	Natural Moisture Content (%)	AASHTO Class.	Atterberg Limits			Gradation Results							
								L.L.	P.L.	P.I.	Retained #4 Sieve	Pass #10 Sieve	Pass #40 Sieve	Pass #200 Sieve	Coarse Sand (%)	Fine Sand (%)	Silt (%)	Clay (%)
S-1	L_1800	-L-	18+00	30' RT	0.0 - 2.0	19.5	A-4	27	19	8	0.0	82.0	71.0	52.0	35.0	36.2	11.5	17.3
SS-2	RW2-2	-L-	21+70	51' RT	0.0 - 1.5	--	A-2-4	26	23	3	10.0	54.0	49.0	33.6	55.0	28.9	6.3	9.8
S-3	RPA_1050	-RPA-	10+50	20' LT	0.0 - 3.5	21.5	A-2-4	30	28	2	12.0	54.0	45.0	31.1	58.0	32.8	4.3	4.9



May 11, 2020

MEMORANDUM TO: John Pilipchuk, LG, PE  
 State Geotechnical Engineer

FROM: Thomas R. Wells, PE  
 Kleinfelder, Inc.

STATE PROJECT: 45693.1.1 (B-5737)

COUNTY: Rockingham

DESCRIPTION: Replace Bridge No. 108 on US 311 & 700 over US 311, NC 14, NC 87, and NC 770

**SUBJECT: Geotechnical Report – Design and Construction Recommendations**

Kleinfelder, Inc. has completed the subsurface investigation for this project and submits the following recommendations. Roadway recommendation graphics will not be provided for this project.

**I. SLOPE AND EMBANKMENT STABILITY**

- A. Slope Design  
 Recommend that fill slopes be constructed at a ratio of 2:1 (H:V) or flatter and cut slopes be constructed at a ratio of 3:1 (H:V) or flatter.
- B. Undercut for Embankment Stabilization  
 A quantity of 200 cubic yards of Undercut Excavation is recommended for inclusion in the contract as a contingency item, to be used at the discretion of the Engineer.
- C. Geotextile for Soil Stabilization  
 A quantity of 200 square yards of Geotextile for Soil Stabilization should be included in the project contract as a contingency to be used at the discretion of the Engineer.

**II. SUBGRADE STABILITY**

- A. Subsurface Drainage – Subsurface Drain  
 Recommend 650 linear feet of 6-inch Perforated Subsurface Drain Pipe (Roadway Standard Drawing No. 815.02) to be included in the project contract for use in the following areas:

<u>LINE</u>	<u>STATIONS</u>	<u>OFFSETS</u>
-L-	17+00 to 19+00	LT, RT
-RPA-	10+00 to 11+25	LT, RT

It is recommended that 200 linear feet of 6-inch Perforated Subsurface Drain Pipe be included in the project contract as a contingency item, to be used at the discretion of the Engineer.

- B. Grade Point Undercut  
 Recommend 100 cubic yards of Grade Point Undercut Excavation for inclusion in the contract as a contingency item to be used at the discretion of the Engineer.
- C. Undercut for Subgrade Stability  
 It is recommended that 200 cubic yards of Undercut Excavation be included in the project contract as a contingency item, to be used at the discretion of the Engineer.



D. Aggregate Subgrade Type 1

It is recommended that 100 cubic yards of shallow undercut be included in the project contract as a contingency, to be used at the discretion of the Engineer.

It is recommended that 200 tons of Class IV material be included in the project contract as a contingency, to be used at the discretion of the Engineer.

It is recommended that 200 square yards of geotextile for soil stabilization be included in the project contract, to be used at the discretion of the Engineer.

E. Geotextile for Soil Stabilization

It is recommended that 200 square yards of Geotextile for Soil Stabilization be included in the project contract as a contingency to be used at the discretion of the Engineer. This contingency quantity is for use with Section II C.

**III. BORROW SPECIFICATIONS**

A. Borrow Criteria

Common borrow for embankment construction to subgrade shall meet Piedmont and Western criteria outlined in the Standard Specifications, Article 1018-2(A).

B. Shrinkage Factor

Recommend a 20% shrinkage factor be used for earthwork calculations.

C. Select Granular Material

Select Granular Material for embankment construction on geotextile for soil stabilization shall meet the criteria outlined in Standard Specifications, Article 1016-3 Class II or III. It is recommended that 200 cubic yards of Select Granular Material be included in the project contract as a contingency to be used at the discretion of the Engineer.

**IV. MISCELLANEOUS**

A. Reduction of Unclassified Excavation - Clearing and Grubbing

A loss of 50 cubic yards is estimated on the project due to clearing and grubbing of cut sections.

Prepared by,  
**KLEINFELDER, INC.**  
NC License No. F-1312

F. Christopher Driscoll, GIT  
Staff Professional

FCD/DHK:asp



Daniel H. Kubinski PE  
Staff Professional





**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION**

**GEOTECHNICAL ENGINEERING UNIT**

Summary of Quantities

WBS Number: 45396.1.1

County: Rockingham

Project Engineer: D. Kubinski

TIP Number: B-5737

Field Office: Kleinfelder, Inc.

Project Geologist: \_\_\_\_\_

Description: Replace Bridge No. 108 on US 311 & 700 over US 311, NC 14, NC 87, and NC 770

Pay Item No.	Pay Item/ Quantity Adjustment	Spec Book Section No. or Special Provision (SP) Reference	Report Section	Alignment	Begin Station	End Station	Quantity	Units / %
0036000000-E	Undercut Excavation	225 - Roadway Excavation	I. B	Contingency	N/A	N/A	200	CY
0036000000-E	Undercut Excavation	225 - Roadway Excavation	II. B	Contingency	N/A	N/A	100	CY
0036000000-E	Undercut Excavation	225 - Roadway Excavation	II. C	Contingency	N/A	N/A	200	CY
<b>Total Quantity of Undercut Excavation =</b>							<b>500</b>	<b>CY</b>
0195000000-E	Select Granular Material	265 - Select Granular Material	III. C	Contingency	N/A	N/A	200	CY
<b>Total Quantity of Select Granular Material =</b>							<b>200</b>	<b>CY</b>
0196000000-E	Geotextile for Soil Stabilization	270 - Geotextile for Soil Stabilization	I. C	Contingency	N/A	N/A	200	SY
0196000000-E	Geotextile for Soil Stabilization	270 - Geotextile for Soil Stabilization	II. D	Contingency	N/A	N/A	200	SY
0196000000-E	Geotextile for Soil Stabilization	270 - Geotextile for Soil Stabilization	II. E	Contingency	N/A	N/A	200	SY
<b>Total Quantity of Geotextile for Soil Stabilization =</b>							<b>600</b>	<b>SY</b>
1099500000-E	Shallow Undercut	505 - Aggregate Subgrade	II. D	Contingency	N/A	N/A	100	CY
<b>Total Quantity of Shallow Undercut =</b>							<b>100</b>	<b>CY</b>
1099700000-E	Class IV Subgrade Stabilization	505 - Aggregate Subgrade	II. D	Contingency	N/A	N/A	200	TON
<b>Total Quantity of Class IV Subgrade Stabilization =</b>							<b>200</b>	<b>TON</b>
2044000000-E	6" Perforated Subdrain Pipe	815 - Subsurface Drainage	II. A	Contingency	N/A	N/A	200	LF
2044000000-E	6" Perforated Subdrain Pipe	815 - Subsurface Drainage	II. A	-L-	17+00.00	19+00.00	400	LF
2044000000-E	6" Perforated Subdrain Pipe	815 - Subsurface Drainage	II. A	-RPA-	10+00.00	11+25.00	250	LF
<b>Total Quantity of 6" Perforated Subdrain Pipe =</b>							<b>850</b>	<b>LF</b>

<b>These Items Only Impact Earthwork Totals</b>								
N/A	Loss Due to Clearing & Grubbing	200 - Clearing and Grubbing	IV. A	N/A	N/A	N/A	50	CY
N/A	Shrinkage Factor	235 - Embankments	III. B	N/A	N/A	N/A	20	%