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REFERENCE: R-2530B

PROJECT: 34446

SEE SHEET 3 FOR PLAN SHEET LAYOUT
AT TIME OF INVESTIGATION

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-2530B	1	131

ROADWAY
SUBSURFACE INVESTIGATION

COUNTY STANLY
PROJECT DESCRIPTION NC 24-27 FROM NC 740 IN
ALBEMARLE TO EAST OF THE PEE DEE RIVER

INVENTORY

CONTENTS

<u>LINE</u>	<u>STATION</u>	<u>PLAN</u>	<u>PROFILE</u>
-L-	19+61 - 396+23	4-31	34-47
-Y8-	13+68 - 27+09	33	48
-Y11-	10+00 - 12+75	20	49
-Y12-	10+00 - 16+72	22	50
-Y16-	10+00 - 16+05	28	51
-DRW14-	10+00 - 11+30	24	52
-DRW15-	10+00 - 11+25	26	53

CROSS SECTIONS

<u>LINE</u>	<u>STATION</u>	<u>SHEETS</u>
-L-	98+50 - 101+00	54-59
-L-	111+00	60
-L-	120+00	61
-L-	123+00 - 126+50	62-69
-L-	174+50 - 179+50	70-74
-L-	185+00 - 194+50	75-90
-L-	201+50 - 203+00	91-94
-L-	274+00	95
-L-	278+00	96
-L-	298+50 - 299+50	97-99
-L-	300+50 - 301+00	100-101
-L-	302+00	102
-L-	304+00	103
-L-	355+50 - 359+50	104-112

APPENDICES

<u>APPENDIX</u>	<u>TITLE</u>	<u>SHEETS</u>
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B	LABORATORY RESULTS	119-127

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT 1919 TOTTENHAM. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

NOTES:

1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

PERSONNEL

GOODNIGHT, D. J.

HPC

INVESTIGATED BY DJG

DRAWN BY HUNSBERGER, W. S.

CHECKED BY HAMM, J. R.

SUBMITTED BY FALCON

DATE APRIL 2017



DocuSigned by
W. Scott Hunsberger

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4/25/2017

SIGNATURE

DATE

**DOCUMENT NOT CONSIDERED FINAL
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NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT
SUBSURFACE INVESTIGATION
SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION										GRADATION										ROCK DESCRIPTION										TERMS AND DEFINITIONS																																																																																																																																																																	
<p>SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i></p>										<p>WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.</p>										<p>HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:</p>										<p>ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENISE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (IN OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.</p>																																																																																																																																																																	
<p>SOIL LEGEND AND AASHTO CLASSIFICATION</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>GENERAL CLASS.</th> <th colspan="5">GRANULAR MATERIALS (≤ 35% PASSING #200)</th> <th colspan="5">SILT-CLAY MATERIALS (> 35% PASSING #200)</th> <th colspan="5">ORGANIC MATERIALS</th> </tr> <tr> <th>GROUP CLASS.</th> <th>A-1</th> <th>A-3</th> <th>A-2</th> <th>A-4</th> <th>A-5</th> <th>A-6</th> <th>A-7</th> <th>A-1, A-2</th> <th>A-3</th> <th>A-4, A-5</th> <th>A-6, A-7</th> <th colspan="5"></th> </tr> <tr> <th>SYMBOL</th> <td colspan="5">[Pattern]</td> <td colspan="5">[Pattern]</td> <td colspan="5">[Pattern]</td> </tr> <tr> <th>% PASSING #10 #40 #200</th> <td>50 MX 30 MX 15 MX</td> <td>50 MX 25 MX</td> <td>51 MN 35 MX 35 MX</td> <td>40 MX 41 MN 10 MX 11 MN</td> <td>40 MX 41 MN 11 MN 11 MN</td> <td>40 MX 41 MN 10 MX 11 MN</td> <td>40 MX 41 MN 11 MN 11 MN</td> <td>40 MX 41 MN 10 MX 11 MN</td> <td>40 MX 41 MN 11 MN 11 MN</td> <td>40 MX 41 MN 10 MX 11 MN</td> <td>40 MX 41 MN 11 MN 11 MN</td> <td>GRANULAR SOILS</td> <td>SILT-CLAY SOILS</td> <td colspan="3">MUCK, PEAT</td> </tr> <tr> <th>MATERIAL PASSING #40 LL PI</th> <td colspan="5"></td> <td>40 MX 41 MN NP</td> <td>40 MX 41 MN 10 MX 11 MN</td> <td>40 MX 41 MN 11 MN 11 MN</td> <td>40 MX 41 MN 10 MX 11 MN</td> <td>40 MX 41 MN 11 MN 11 MN</td> <td>40 MX 41 MN 10 MX 11 MN</td> <td colspan="5">SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER</td> </tr> <tr> <th>GROUP INDEX</th> <td colspan="5">0</td> <td>0</td> <td>4 MX</td> <td>8 MX</td> <td>12 MX</td> <td>16 MX</td> <td>NO MX</td> <td colspan="5">HIGHLY ORGANIC SOILS</td> </tr> <tr> <th>USUAL TYPES OF MAJOR MATERIALS</th> <td colspan="2">STONE FRAGS. 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IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.</p> <p>MODERATE (MOD.) - SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.</p> <p>MODERATELY SEVERE (MOD. SEV.) - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. <i>IF TESTED, WOULD YIELD SPT REFUSAL</i></p> <p>SEVERE (SEV.) - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF</i></p> <p>VERY SEVERE (IV SEV.) - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF</i></p> <p>COMPLETE - ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.</p>									
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<p>INDURATION</p> <p>FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.</p> <p>FRIABLE - RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.</p> <p>MODERATELY INDURATED - GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.</p> <p>INDURATED - GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.</p> <p>EXTREMELY INDURATED - SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.</p>										<p>BENCH MARK:</p> <p>BORING ELEVATIONS COLLECTED USING "r-2530b_ls_tin_tin" DATED 9/28/16. ELEVATION: FEET</p> <p>NOTES:</p> <p>FIAD - FILLED IMMEDIATELY AFTER DRILLING</p>																																																																																																																																																																																					

09/08/19

TIP PROJECT: R-2530B/B-4974

CONTRACT: C203751

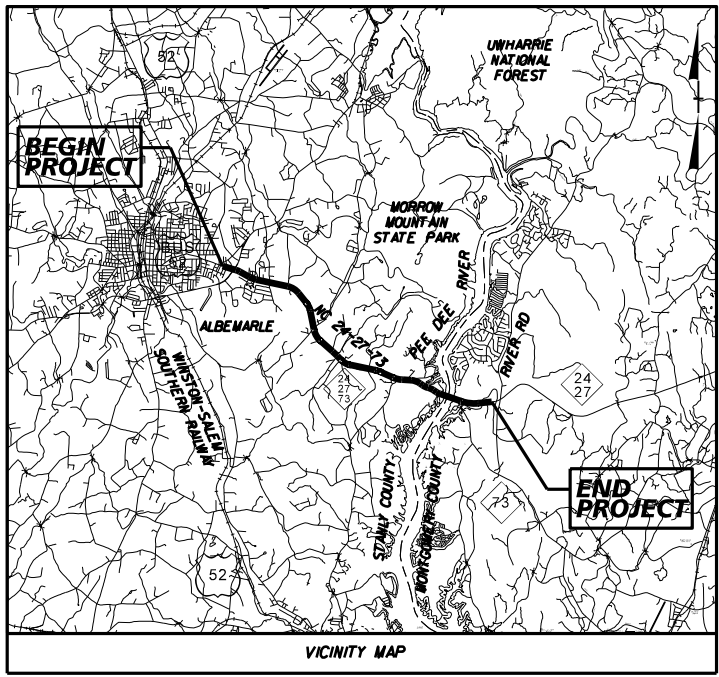
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STATE OF NORTH CAROLINA
DIVISION OF HIGHWAYS

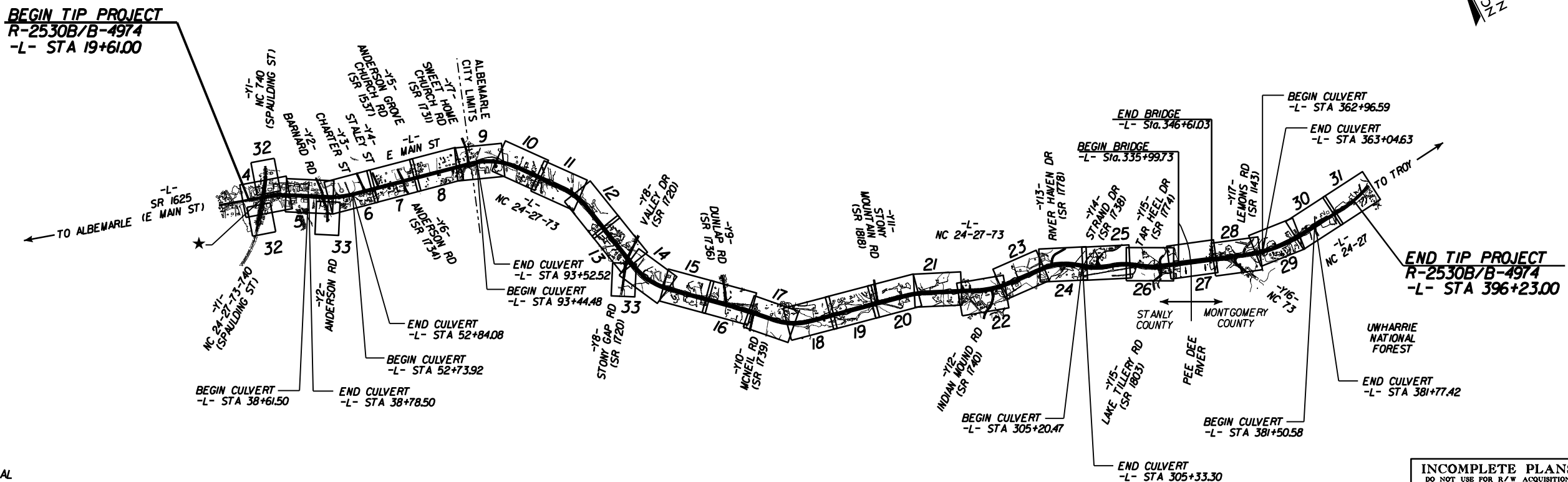
STANLY & MONTGOMERY COUNTIES

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-2530B/B-4974	3	131
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
34446.1.6	BRSTP-0024(33)	P.E.	

APPROVED 25% PLANS

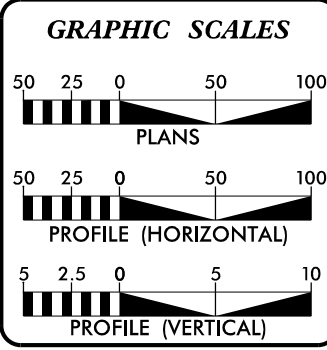


LOCATION: NC 24-27 FROM NC 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER
 TYPE OF WORK: GRADING, DRAINAGE, PAVING, SIGNING, SIGNALS, AND STRUCTURES



★ TRAFFIC SIGNAL
 CLEARING ON THIS PROJECT SHALL BE PERFORMED TO THE LIMITS ESTABLISHED BY METHOD ____
 A PORTION OF THIS PROJECT IS WITHIN THE MUNICIPAL BOUNDARIES OF THE CITY OF ALBEMARLE

INCOMPLETE PLANS
 DO NOT USE FOR R/W ACQUISITION
 DOCUMENT NOT CONSIDERED FINAL
 UNLESS ALL SIGNATURES COMPLETED



DESIGN DATA

AADT 2019 =	16,400
AADT 2039 =	21,500
K =	9%
D =	55%
T =	10%*
V =	50/60 MPH
* (TTST 4% + DUAL 6%)	
FUNCTIONAL CLASSIFICATION: URBAN/RURAL ARTERIAL REGIONAL TIER	

PROJECT LENGTH

LENGTH ROADWAY TIP PROJECT R-2530B /B-4974 =	6.932 MILES
LENGTH STRUCTURE TIP PROJECT R-2530B /B-4974 =	0.201 MILES
TOTAL LENGTH TIP PROJECT R-2530B /B-4974 =	7.133 MILES

PLANS PREPARED FOR THE NCDOT BY:

2012 STANDARD SPECIFICATIONS

RIGHT OF WAY DATE: MAY 19, 2017

LETTING DATE: MARCH 19, 2019

Kimley»Horn

JEFFREY W. MOORE, P.E.
PROJECT ENGINEER

RHODES S. HUNT, EIT
PROJECT DESIGN ENGINEER

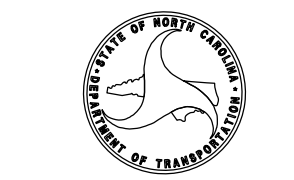
THAD DUNCAN, P.E.
PROJECT DESIGN ENGINEER
NCDOT ROADWAY DESIGN
ENGINEERING COORDINATION SECTION

HYDRAULICS ENGINEER

SIGNATURE: _____ P.E.

ROADWAY DESIGN ENGINEER

SIGNATURE: _____ P.E.





WBS: 34446.1.6
TIP: R-2530B
Project ID: 29226
COUNTY: Stanly
DESCRIPTION: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
SUBJECT: Roadway Subsurface Investigation – Inventory

Roadway Subsurface Investigation Report - Inventory

NC 24-27 From NC 740 in Albemarle to East of the Pee Dee River
Stanly and Montgomery Counties, North Carolina
WBS: 34446.1.6 TIP: R-2530B
Falcon Project No.: G16056.00

Prepared for:
NCDOT Geotechnical Engineering Unit
1589 Mail Service Center
Raleigh, NC 27699-1589

Submitted by:
Falcon Engineering, Inc.
1210 Trinity Road, Suite 110
Raleigh, North Carolina 27607
(919) 871-0800
www.falconengineers.com

April 23, 2017

PROJECT DESCRIPTION

This project consists of 7.1 miles of proposed new roadway, realignment, and widening in Stanly and Montgomery Counties. An additional two lanes of new roadway will be constructed parallel to the existing two lane US 24-27. NC 73 will be realigned at the intersection with NC 24-27 east of the Pee Dee River. Multiple side streets and attached drives will be widened, realigned, or graded at various locations.

Included in this project are three culverts on alignment -L- over small creeks and waterways and a bridge structure along -L- over the Pee Dee River. The culvert structures were investigated as a part of this investigation. The bridge structure was not investigated as a part of this investigation.

The investigation was conducted between October 19, 2016 and February 13, 2017 in general accordance with our Proposal to Provide Geotechnical Engineering Services, dated October 28, 2016. The recommendations provided in this report are based solely on our site reconnaissance, soil test borings and laboratory test data, engineering evaluation of these data, and generally accepted soil and foundation engineering practices and principles.

A total of one hundred and ninety-one (191) Standard Penetration Test (SPT) borings, one hundred (100) auger probe and two (2) hand auger borings were drilled for the proposed roadway alignments. All mechanical borings were drilled using a CME-550X ATV or Diedrich D-50 Track drill rig equipped with 2 ¼-inch inside diameter hollow-stem augers, and SPT testing was performed with an automatic hammer. Representative soil samples, collected with a split-barrel sampler or hand auger, were selected for laboratory testing to verify visual field classifications. In addition, bulk samples were collected for standard Proctor compaction and California Bearing Ratio (CBR) testing.



The following alignments, totaling approximately 7.8 miles were explicitly investigated. Other minor Y-lines and driveways are included on the project but improvements are not anticipated to be significant enough to warrant investigation.

<u>Alignment</u>	<u>Station (ft)</u>
-L- (NC 24-27)	19+61.00—396+23.00
-Y8- (Stony Gap Rd)	10+00.00—27+09.00
-Y11- (Stony Mountain Rd)	10+00.00—12+75.00
-Y12- (Indian Mound Rd)	10+00.00—16+72.00
-Y16- (NC 73)	10+00.00—16+05.54
-DRW14-	10+00.00—11+30.00
-DRW15-	10+00.00—11+25.00

AREAS OF SPECIAL GEOTECHNICAL INTEREST

- I. The following locations contain highly plastic soils with plasticity indices (PI) greater than 25 within 3 feet of proposed subgrade elevations:

<u>Alignment</u>	<u>Station (ft)</u>
-L-	123+00 to 125+00
-L-	174+50 to 179+00
-L-	185+00 to 188+00
-L-	189+25 to 193+75

- II. The following locations contain very soft to soft/very loose soils with an N-value less than 4 near the ground surface:

<u>Alignment</u>	<u>Station (ft)</u>
-L-	36+00
-L-	66+00
-L-	112+00

- III. Shallow ground water was measured within the following areas and may cause groundwater related stability problems during construction:

<u>Alignment</u>	<u>Station (ft)</u>
-L-	34+00

-L-	52+74
-L-	93+45
-L-	238+00
-L-	293+70
-L-	305+35

- IV. Alluvial soils were encountered near the following locations. The potential for wet, soft or organic soils should be anticipated at these locations:

<u>Alignment</u>	<u>Station (ft)</u>
-L-	116+00
-L-	305+35
-L-	363+00

Isolated alluvial soils are likely to exist elsewhere on the site between borings in proximity to natural waterways.

- V. Artificial fill was encountered at the following locations:

<u>Alignment</u>	<u>Station (ft)</u>
30+00	30+00
32+00 to 41+00	32+00 to 41+00
46+00	46+00
66+00	66+00
96+00	96+00
104+00	104+00
142+00	142+00
286+00	286+00
293+70 to 296+00	293+70 to 296+00

PHYSIOGRAPHY AND GEOLOGY

The project site is in the Carolina Slate Belt Physiographic Province of North Carolina. According to the *Geologic Map of North Carolina* (1985), the site is underlain by three major geologic units in the Carolina Slate Belt Physiographic Province. The site transitions from west to east across the Floyd Church Formation (**CZmd3**), two units of the Cid Formation (**CZmd2** and **CZfv2**) and the Tillery Formation (**CZmd1**). These units are all of the Cambrian/Late Proterozoic Period. In addition, the *Geologic Map of the Albemarle Quadrangle, North Carolina* indicates linear intrusions consisting of Rhyolite dikes (porphyritic rhyolite composed of phenocrysts of orthoclase, oligoclase, and beta quartz in an aphanitic groundmass) and Gabbro sills (hornblende gabbro, sometimes amygdaloidal). These materials form the majority of the notable outcrops and exposed bedrock in roadway cuts which observed along the alignment.

The Floyd Church, Cid and Tillery formations are noted to consist of Metamudstone and Meta-Argillite, thin to thick bedded, bedding plane and axial-planar cleavage common, interbedded with metasandstone, metaconglomerate and metavolcanic rock. A felsic metavolcanic portion of the Cid Formation (**CZfv2**) crosses the central portion of the project site and is noted to consist of Felsic Metavolcanic Rock, metamorphosed dactylic to rhyolitic flows and tuffs, light gray to greenish gray, interbedded with mafic and intermediate metavolcanic rock, meta-argillite and metamudstone.

Existing site topography is typical of North Carolina's foothills region. The site lies along the southern portion of the Uwharrie Mountains, an ancient mountain range that has been heavily eroded to elevations not exceeding 1,200 feet. While not comparable to larger ranges in the mountain region of North Carolina, the terrain in this area is more rugged than the surrounding piedmont terrain. The corridor begins from near the center of the Town of Albemarle, and various residential and commercial properties border the corridor. As the corridor progresses westward, bordering properties become gradually more agricultural and/or undeveloped and wooded in nature. The corridor crosses Lake Tillery (an impoundment of the Pee Dee River) between approximate stations 335+00 and 347+00, before reaching the eastern project terminus around 4,900 feet beyond the eastern bank of the Lake. Topography generally grades upward in either direction away from Lake Tillery.

SOIL PROPERTIES

A variety of soils were encountered along the project, including existing roadway embankments, alluvial deposits, residual soils, weathered rock and crystalline and non-crystalline rock. Areas where soils at the ground surface are of a unique origin (i.e. not residual soils) are approximately delineated on the boring location plans based on subsurface conditions encountered in nearby borings, and various topographical, vegetative, or other visual surface features.

Topsoil and rootmat was encountered in grassy, brushy, and wooded areas ranging in thickness from 0.1 to 1.0 feet, and typically on the order of 0.4 to 0.7 feet.

Cultivated soils were in agricultural lands ranging in thickness from 0.3 to 1.2 feet, and typically on the order of 0.8 feet. These soils consist of wet, silty sand (A-2-4) and sandy silt (A-4) with organic staining and some vegetative matter from recent crops.

Artificial Fill soils were encountered at the ground surface beneath and adjacent to existing roadways. These consist of 3 to 10 feet of moist, loose to medium dense, silty sand (A-2-4) and moist, very soft to very stiff, sandy silt and sandy and silty clay (A-4, A-5, A-6, A-7).

Roadway Embankment soils were encountered at the ground surface beneath and adjacent to existing roadways. These consist of 3 to 17 feet of moist, loose to medium dense, silty sand (A-2-4) and moist, soft to very stiff, sandy silt (A-4 and A-5).

Alluvial soils were encountered at the ground surface near the historic floodplains of natural waterways and presumably extend beneath nearby roadway embankments at the locations encountered. These soils extended to depths of up to approximately 4 feet and consist of moist to wet, medium soft to stiff sandy silt (A-4) with trace amounts of organic material.

Residual soils were encountered at the ground surface, or beneath artificial fill, roadway embankments or alluvial deposits. These soils consist of dry to saturated, very loose to very dense, clayey and silty sand (A-2-6, A-2-7, A-2-4, A-2-5) and very soft to hard, sandy clay and silt, clayey silt and silty clays (A-4, A-5, A-6, A-7).

Weathered Rock (WR) is a very hard material with properties intermediate of soil and rock. WR is classified as having an N-value of greater than 100 blows per one foot. WR encountered on the project generally consists of tan and gray weathered metamudstone or metavolcanic rock.



Non-Crystalline rock, in the form of metamudstone and metavolcanic rock, and Crystalline Rock, in the form of Gabbro, was encountered beneath weathered rock, residual soils, or alluvial soils at various locations throughout the site, and is visible in various outcrops and cut exposures along the corridor. Surficial rock exposures are approximately mapped on the boring location plans, including strike and dip measurements where discernable.

GROUNDWATER PROPERTIES

Groundwater levels were measured at the time of boring completion, and in many cases after a waiting period of at least 24 hours. Borings drilled within and in close proximity to existing roadways, and within residential or livestock areas were backfilled immediately after completion due to safety considerations.

The project crosses small streams and tributaries as well as roadway drainage ditches. Groundwater was observed at shallow depths near these streams and in low lying areas. Detailed groundwater measurements are included in the attached subsurface profiles and cross sections, and noted areas of shallow groundwater are included in the Areas of Special Geotechnical Interest earlier in this report.

ADDITIONAL LABORATORY TESTING

The following bulk samples were obtained:

Sample	Location	Depth (ft)	Test
BS-1	78+00, 20' RT, -L-	1 – 6.0	California Bearing Ratio, Standard Proctor
BS-2	188+00, 5' RT, -L-	1 – 13.0	California Bearing Ratio, Standard Proctor

Classification test results for bulk samples are included in the subsurface profiles and cross sections and Standard Proctor and California Bearing Ratio (CBR) data is attached in the Appendix.

CLOSING

Falcon appreciates the opportunity to have provided our geotechnical engineering services for the above referenced project. If you have any questions concerning the contents of this report or need additional information, please do not hesitate to contact our office.

FALCON ENGINEERING, INC.

Report Prepared By:

Report Reviewed By:

DocuSigned by:
W. Scott Hunsberger
EA39AB9EDF5845A...

W. Scott Hunsberger, PE
Geotechnical Engineer

DocuSigned by:
Jeremy R. Hamm
ED7938089E22487...

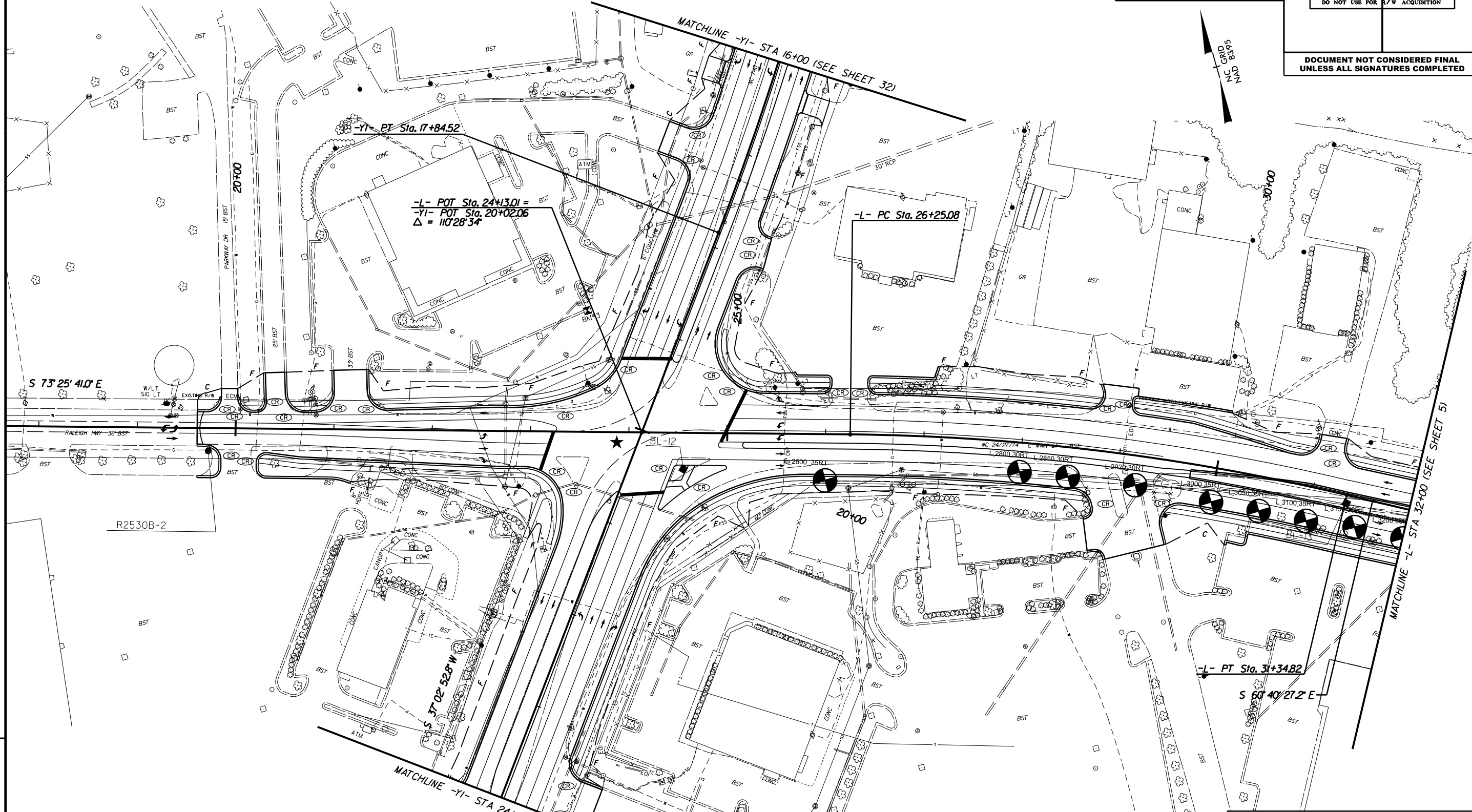
Jeremy R. Hamm, PE
Geotechnical Engineering Manager

Investigated By:

DocuSigned by:
Dana J. Goodnight
A184F26E82914E7...

Dana J. Goodnight, PG
Engineering Geologist





REVISIONS

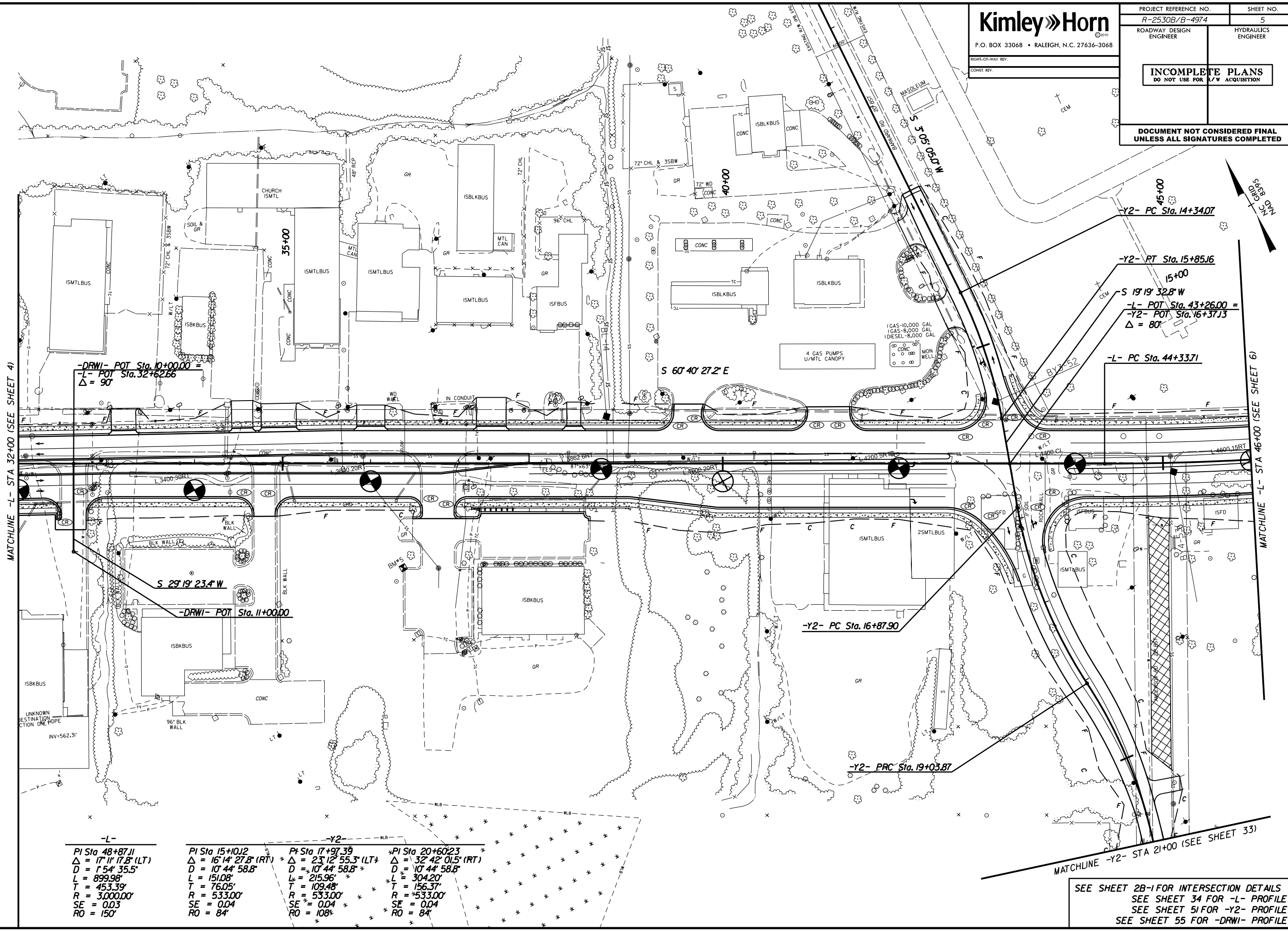
-L-
 PI Sta 28+81.01
 $\Delta = 12^\circ 45' 13.8" (RT)$
 D = 2' 30" 07.2"
 L = 509.75'
 T = 255.93'
 R = 2,290.00'
 SE = 0.03
 RO = 150'

-YI-
 PI Sta 14+21.57
 $\Delta = 13^\circ 55' 57.9" (RT)$
 D = 1' 54" 35.5"
 L = 729.52'
 T = 366.57'
 R = 3,000.00'
 SE = 0.03
 RO = 138'

★ TRAFFIC SIGNAL
 RADI DIMENSIONS ARE TO THE EDGE OF PAVEMENT UNLESS OTHERWISE NOTED (APPLIES TO ALL SHEETS)
 ALL DRIVEWAY RADII ARE 10' UNLESS OTHERWISE NOTED (APPLIES TO ALL SHEETS)
 SEE SHEET 2B-I FOR INTERSECTION DETAILS
 SEE SHEET 34 FOR -L- PROFILE
 SEE SHEETS 50 & 51 FOR -YI- PROFILE

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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 5
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



REVISIONS

MATCHLINE -L- STA 32+00 (SEE SHEET 4)

MATCHLINE -L- STA 46+00 (SEE SHEET 6)

MATCHLINE -Y2- STA 21+00 (SEE SHEET 33)

-L-	-Y2-			
PI Sta 48+87.11 Δ = 17° 11' 17.8" (LT) D = 1° 54' 35.5" L = 899.98' T = 453.39' R = 3,000.00' SE = 0.03 RO = 150'	<table border="0"> <tr> <td>PI Sta 15+10.12 Δ = 16° 14' 27.8" (RT) D = 10° 44' 58.8" L = 151.08' T = 76.05' R = 533.00' SE = 0.04 RO = 84'</td> <td>PI Sta 17+97.39 Δ = 23° 12' 55.3" (LT) D = 10° 44' 58.8" L = 215.96' T = 109.48' R = 533.00' SE = 0.04 RO = 108'</td> <td>PI Sta 20+60.23 Δ = 32° 42' 01.5" (RT) D = 10° 44' 58.8" L = 304.20' T = 156.37' R = 533.00' SE = 0.04 RO = 84'</td> </tr> </table>	PI Sta 15+10.12 Δ = 16° 14' 27.8" (RT) D = 10° 44' 58.8" L = 151.08' T = 76.05' R = 533.00' SE = 0.04 RO = 84'	PI Sta 17+97.39 Δ = 23° 12' 55.3" (LT) D = 10° 44' 58.8" L = 215.96' T = 109.48' R = 533.00' SE = 0.04 RO = 108'	PI Sta 20+60.23 Δ = 32° 42' 01.5" (RT) D = 10° 44' 58.8" L = 304.20' T = 156.37' R = 533.00' SE = 0.04 RO = 84'
PI Sta 15+10.12 Δ = 16° 14' 27.8" (RT) D = 10° 44' 58.8" L = 151.08' T = 76.05' R = 533.00' SE = 0.04 RO = 84'	PI Sta 17+97.39 Δ = 23° 12' 55.3" (LT) D = 10° 44' 58.8" L = 215.96' T = 109.48' R = 533.00' SE = 0.04 RO = 108'	PI Sta 20+60.23 Δ = 32° 42' 01.5" (RT) D = 10° 44' 58.8" L = 304.20' T = 156.37' R = 533.00' SE = 0.04 RO = 84'		

SEE SHEET 2B-1 FOR INTERSECTION DETAILS
 SEE SHEET 34 FOR -L- PROFILE
 SEE SHEET 51 FOR -Y2- PROFILE
 SEE SHEET 55 FOR -DRWI- PROFILE

\$DATE\$

5/14/99

CE1	582911.01	1654979.28	553.50
HW1	582910.69	1654979.09	555.18
CUL3	582858.86	1654964.91	547.83
CUL4	582857.73	1654970.61	547.86
CE2	582858.31	1654967.75	553.83
HW2	582858.53	1654967.82	555.41

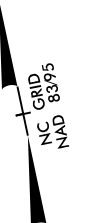
Kimley»Horn
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 ROADWAY DESIGN ENGINEER
 HYDRAULICS ENGINEER

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 6
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR A/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

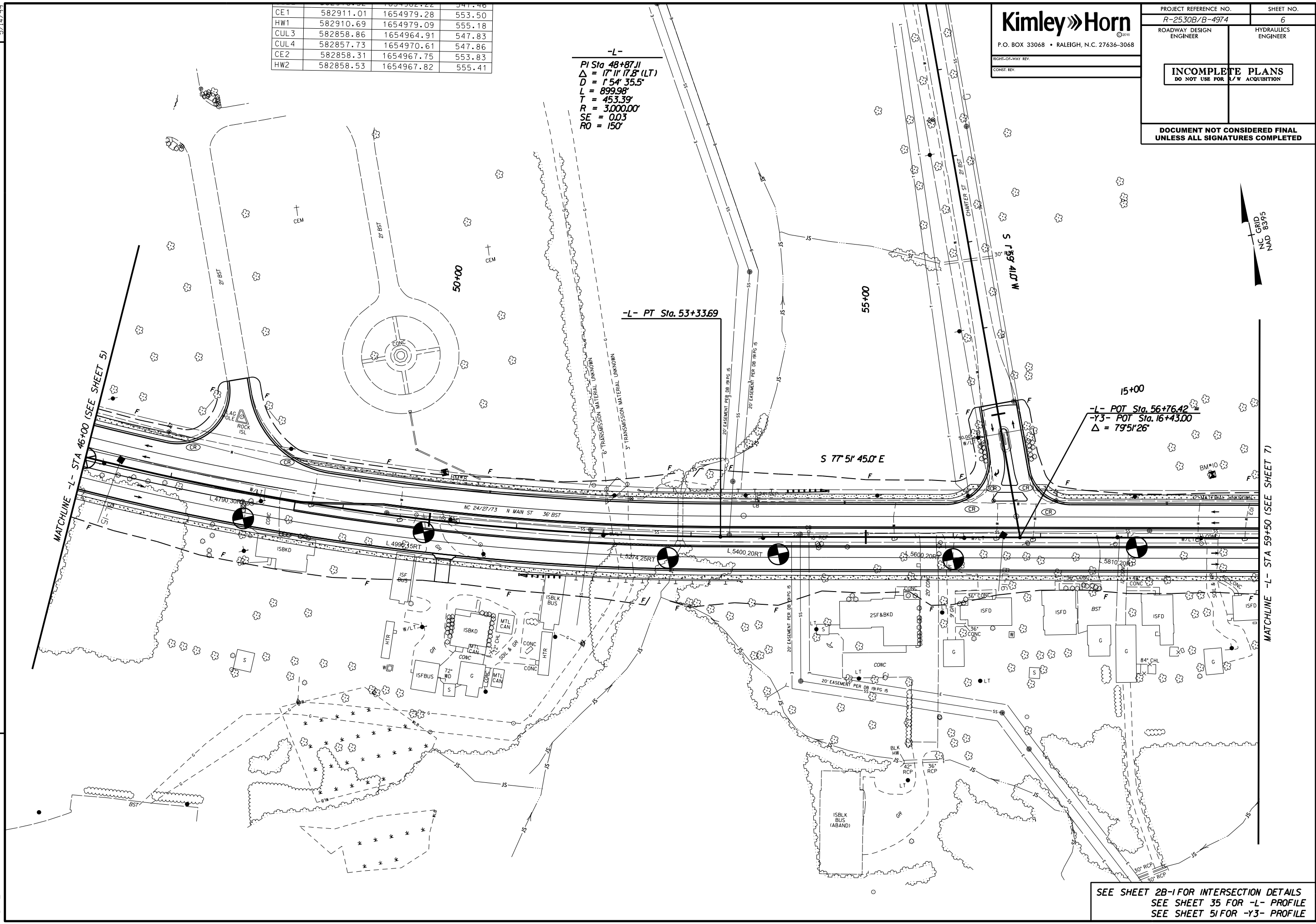
-L-
 PI Sta 48+87.11
 $\Delta = 17^{\circ}11'17.8''$ (LT)
 D = 154'35.5"
 L = 899.98'
 T = 453.39'
 R = 3,000.00'
 SE = 0.03
 RO = 150'

-L- PT Sta. 53+33.69

15+00
 -L- POT Sta. 56+76.42
 -Y3- POT Sta. 16+43.00
 $\Delta = 79^{\circ}51'26''$



REVISIONS



MATCHLINE -L- STA 46+00 (SEE SHEET 5)

MATCHLINE -L- STA 59+50 (SEE SHEET 7)

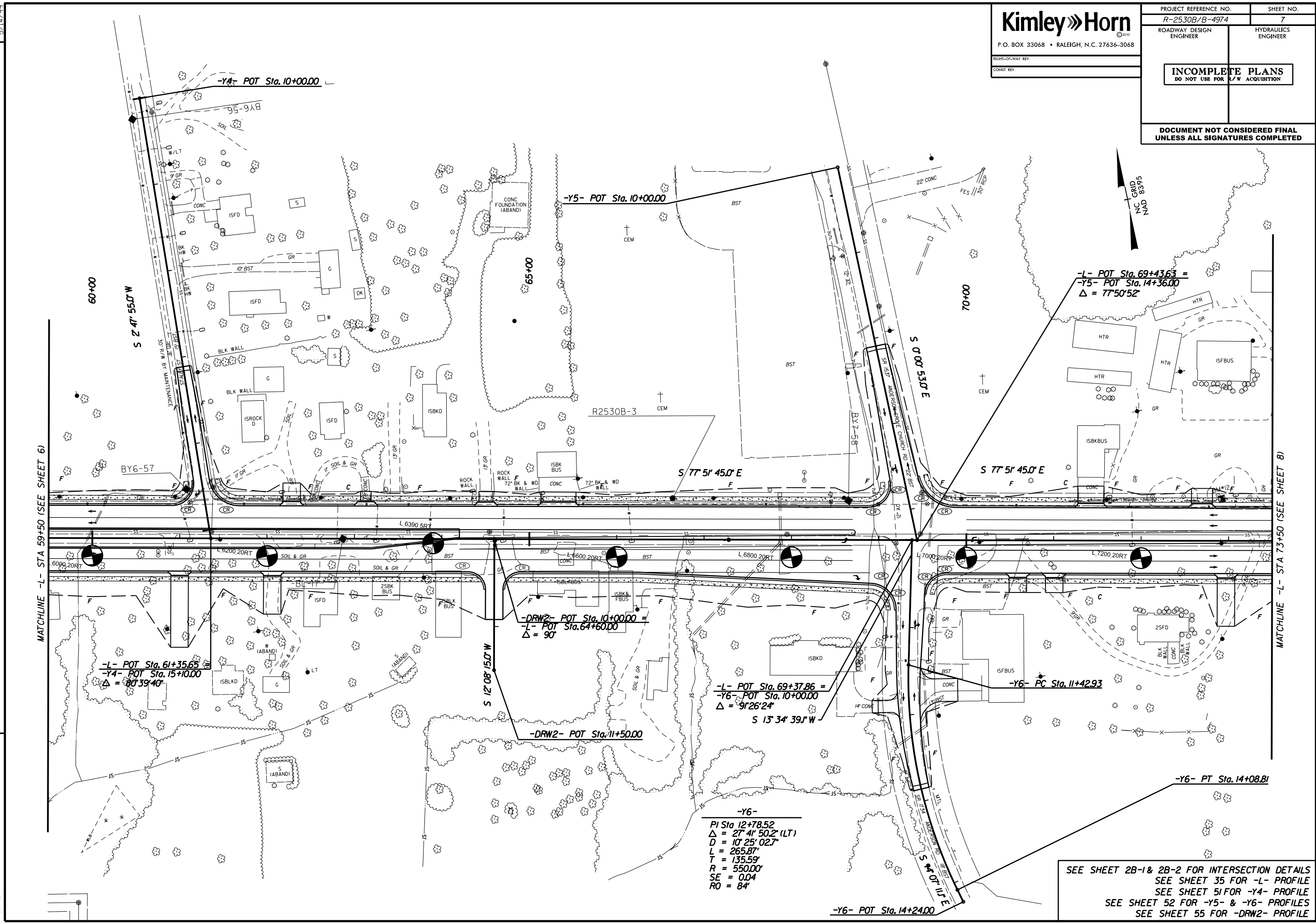
SEE SHEET 2B-1 FOR INTERSECTION DETAILS
 SEE SHEET 35 FOR -L- PROFILE
 SEE SHEET 51 FOR -Y3- PROFILE

\$DATE\$

5/14/99

INCOMPLETE PLANS
DO NOT USE FOR A/W ACQUISITION

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REVISIONS

\$DATE\$

SEE SHEET 2B-1 & 2B-2 FOR INTERSECTION DETAILS
 SEE SHEET 35 FOR -L- PROFILE
 SEE SHEET 51 FOR -Y4- PROFILE
 SEE SHEET 52 FOR -Y5- & -Y6- PROFILES
 SEE SHEET 55 FOR -DRW2- PROFILE

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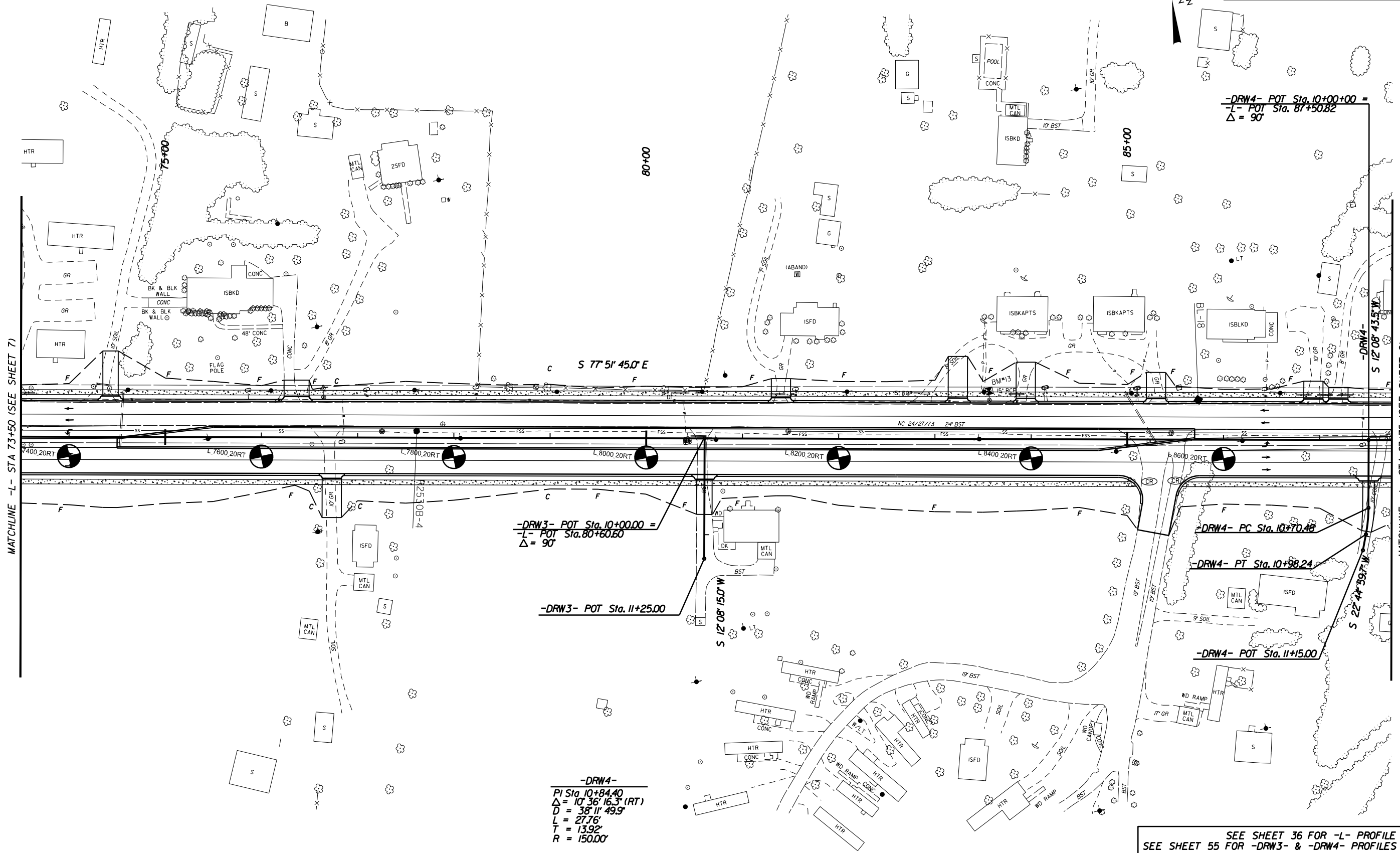
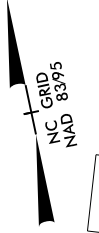
RIGHT-OF-WAY REV.
CONST. REV.

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 8
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ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
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INCOMPLETE PLANS
DO NOT USE FOR R/W ACQUISITION

DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED



MATCHLINE -L- STA 73+50 (SEE SHEET 7)

MATCHLINE -L- STA 87+75 (SEE SHEET 9)

-DRW3- POT Sta. 10+00.00 =
-L- POT Sta. 80+60.60
Δ = 90°

-DRW3- POT Sta. 11+25.00

-DRW4- PC Sta. 10+70.48

-DRW4- PT Sta. 10+98.24

-DRW4- POT Sta. 11+15.00

-DRW4-
PI Sta. 10+84.40
Δ = 10° 36' 16.3" (RT)
D = 38° 11' 49.9"
L = 27.76'
T = 13.92'
R = 150.00'

SEE SHEET 36 FOR -L- PROFILE
SEE SHEET 55 FOR -DRW3- & -DRW4- PROFILES

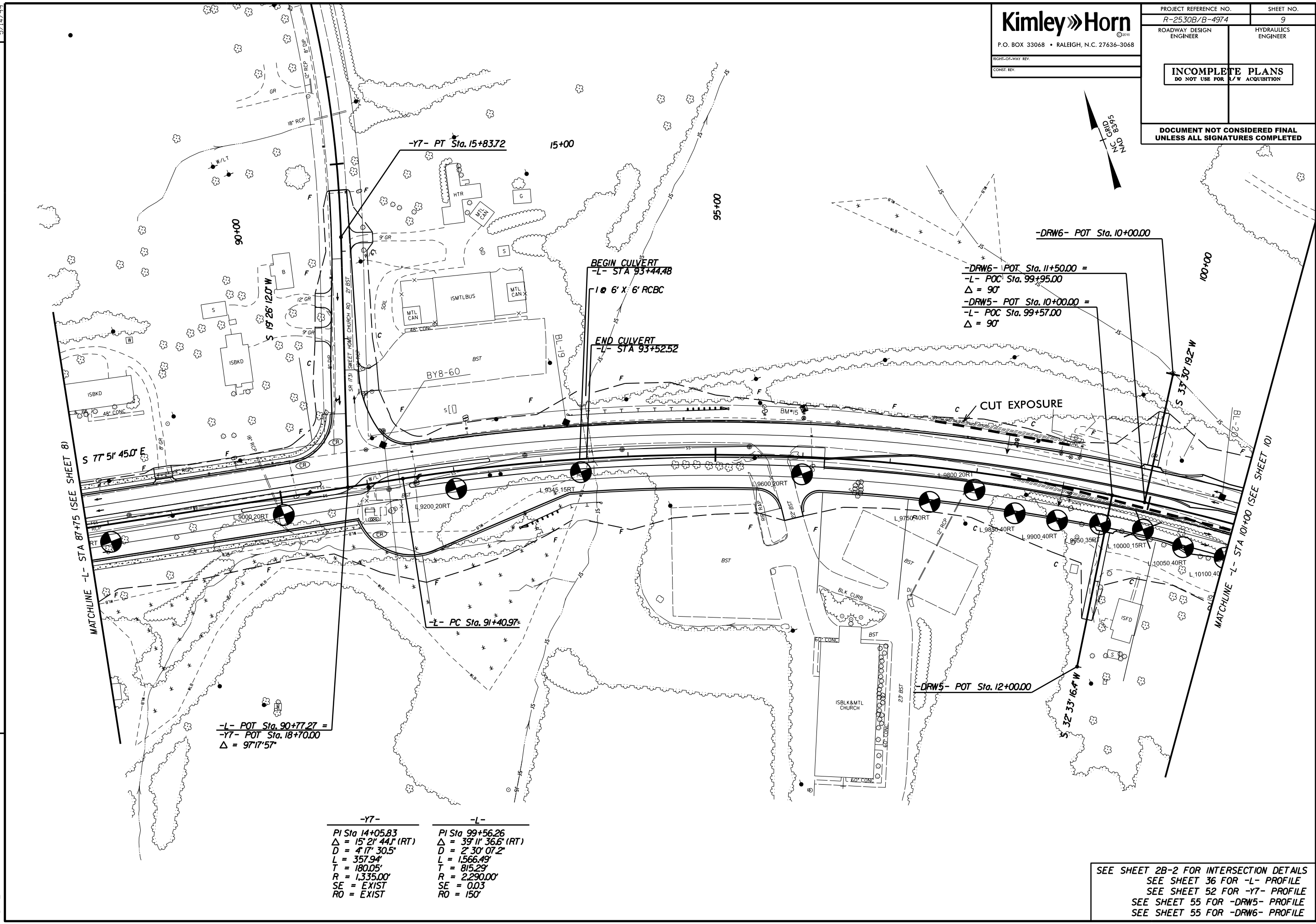
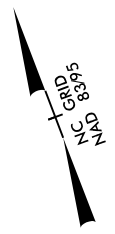
REVISIONS

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INCOMPLETE PLANS
 DO NOT USE FOR S/W ACQUISITION

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REVISIONS

-L- POT Sta. 90+77.27 =
 -Y7- POT Sta. 18+70.00
 Δ = 97°17'57"

-DRW6- POT Sta. 11+50.00 =
 -L- POC Sta. 99+95.00
 Δ = 90°
 -DRW5- POT Sta. 10+00.00 =
 -L- POC Sta. 99+57.00
 Δ = 90°

-Y7-	-L-
PI Sta 14+05.83	PI Sta 99+56.26
Δ = 15° 21' 44" (RT)	Δ = 39° 11' 36.6" (RT)
D = 4' 17" 30.5"	D = 2' 30" 07.2"
L = 357.94'	L = 1566.49'
T = 180.05'	T = 815.29'
R = 1,335.00'	R = 2,290.00'
SE = EXIST	SE = 0.03
RO = EXIST	RO = 150'

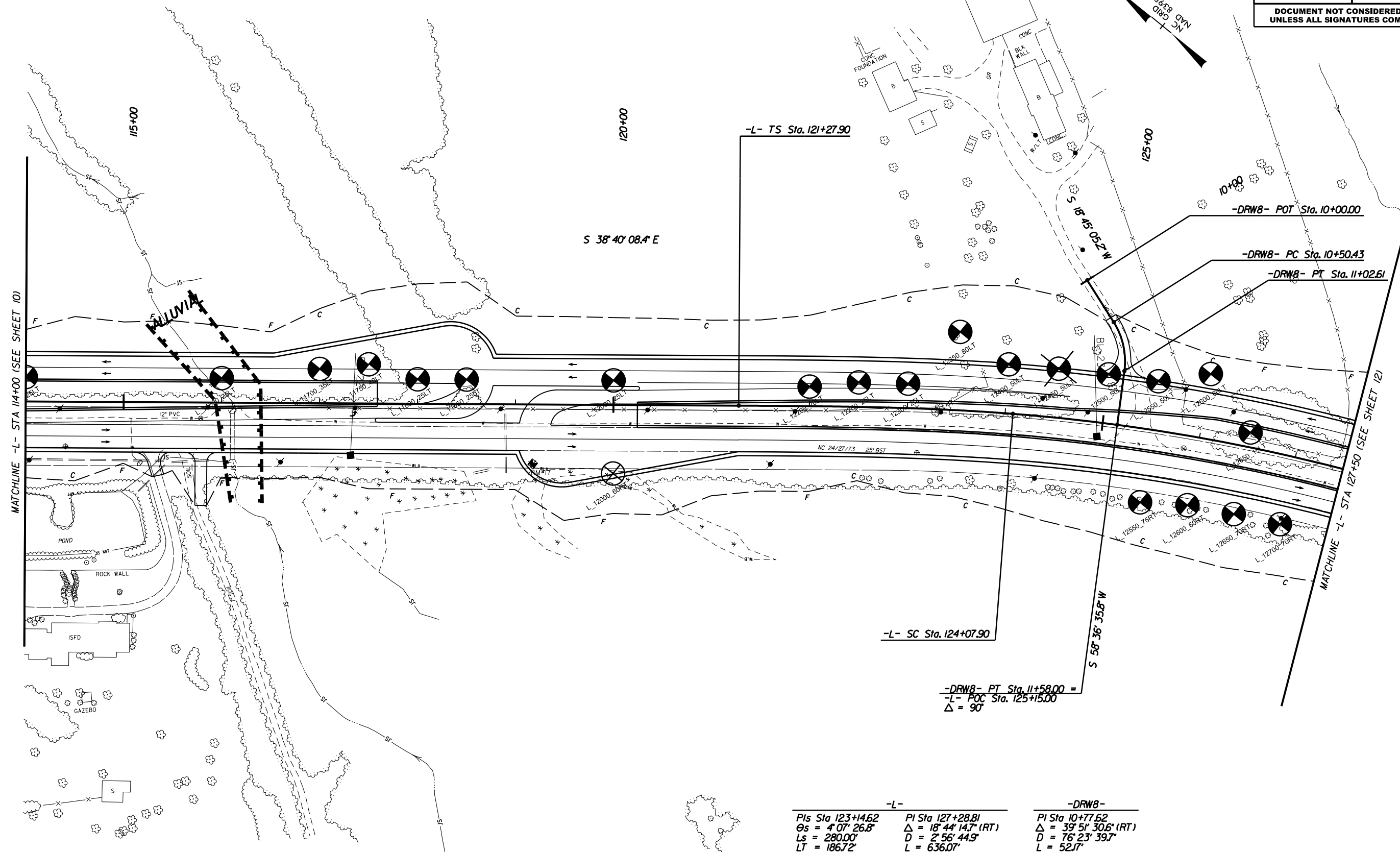
SEE SHEET 2B-2 FOR INTERSECTION DETAILS
 SEE SHEET 36 FOR -L- PROFILE
 SEE SHEET 52 FOR -Y7- PROFILE
 SEE SHEET 55 FOR -DRW5- PROFILE
 SEE SHEET 55 FOR -DRW6- PROFILE

\$DATE\$

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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. II
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DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



REVISIONS

\$DATE\$

-L-	-L-	-DRW8-
PI Sta 123+1462	PI Sta 127+28.81	PI Sta 10+77.62
Os = 4' 07' 26.8"	Δ = 18' 44' 14.7" (RT)	Δ = 39' 51' 30.6" (RT)
Ls = 280.00'	D = 2' 56' 44.9"	D = 76' 23' 39.7"
LT = 186.72'	L = 636.07'	L = 52.17'
ST = 93.38'	T = 320.90'	T = 27.19'
	R = 1,945.00'	R = 75.00'
	SE = 0.07	

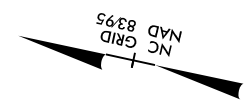
SEE SHEET 37 FOR -L- PROFILE
 SEE SHEET 56 FOR -DRW8- PROFILE

5/14/99

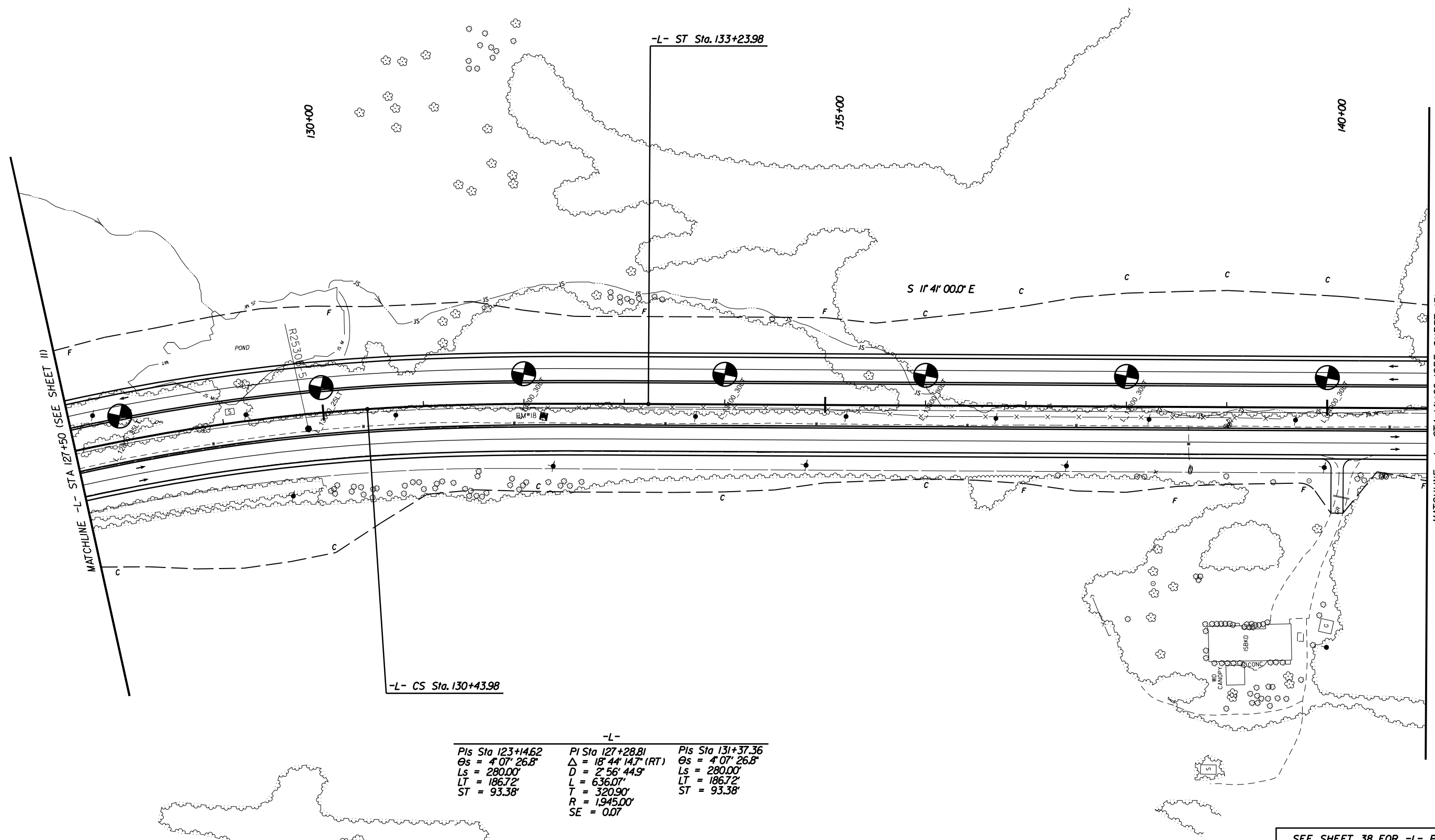
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RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 12
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



REVISIONS



-L- CS Sta. 130+43.98

-L-

PIs Sta 123+14.62	PI Sta 127+28.81	PIs Sta 131+37.36
$\theta_s = 4^\circ 07' 26.8''$	$\Delta = 18^\circ 44' 14.7''$ (RT)	$\theta_s = 4^\circ 07' 26.8''$
$L_s = 280.00'$	$D = 2^\circ 56' 44.9''$	$L_s = 280.00'$
$LT = 186.72'$	$L = 636.07'$	$LT = 186.72'$
$ST = 93.38'$	$T = 320.90'$	$ST = 93.38'$
	$R = 1,945.00'$	
	$SE = 0.07$	

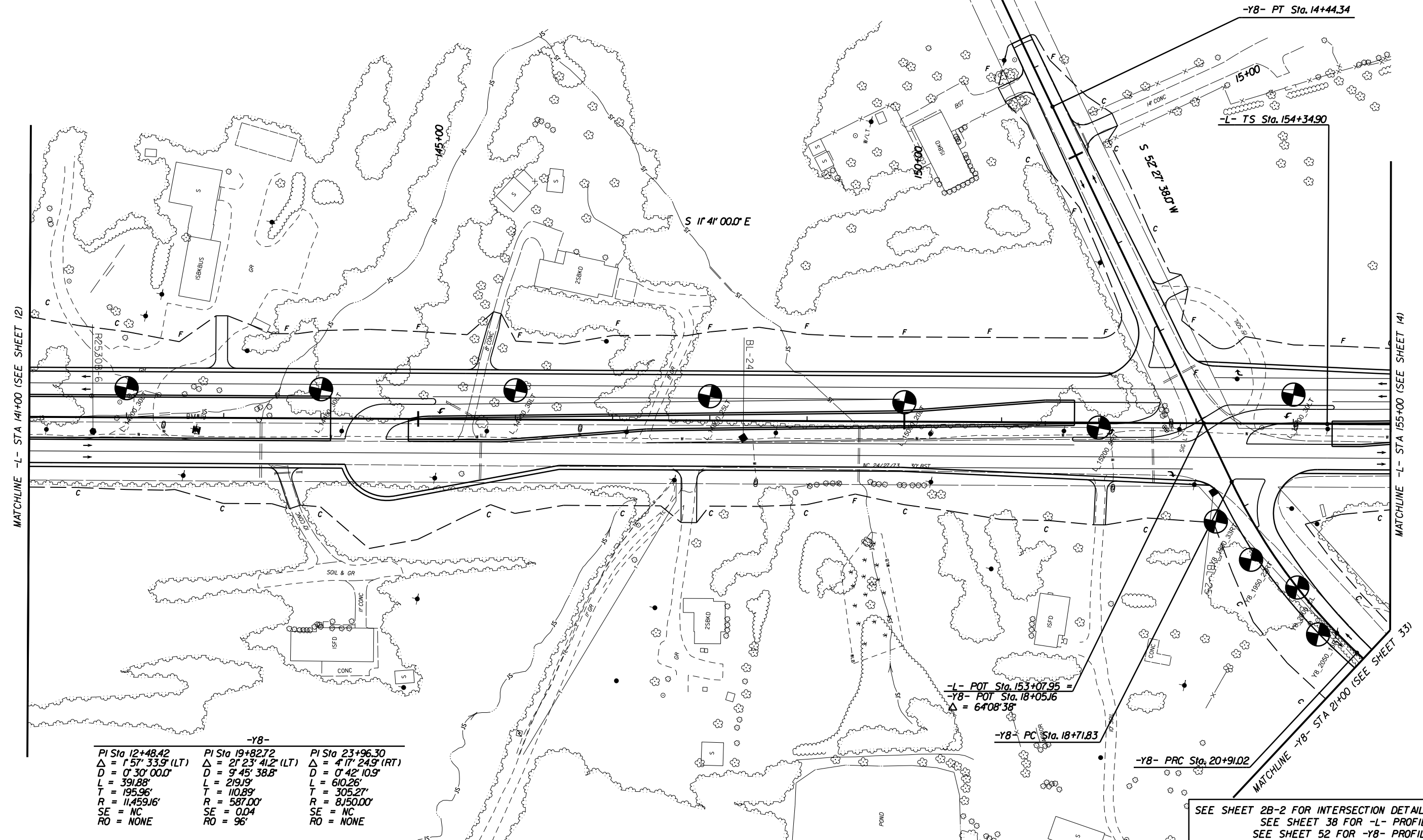
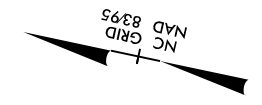
\$DATE\$

SEE SHEET 38 FOR -L- PROFILE

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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 13
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



REVISIONS

-Y8-		
PI Sta 12+48.42	PI Sta 19+82.72	PI Sta 23+96.30
Δ = 1° 57' 33.9" (LT)	Δ = 2° 23' 41.2" (LT)	Δ = 4° 17' 24.9" (RT)
D = 0° 30' 00.0"	D = 9° 45' 38.8"	D = 0° 42' 10.9"
L = 391.88'	L = 219.19'	L = 610.26'
T = 195.96'	T = 110.89'	T = 305.27'
R = 11,459.16'	R = 587.00'	R = 8150.00'
SE = NC	SE = 0.04	SE = NC
RO = NONE	RO = 96'	RO = NONE

SEE SHEET 2B-2 FOR INTERSECTION DETAILS
 SEE SHEET 38 FOR -L- PROFILE
 SEE SHEET 52 FOR -Y8- PROFILE

\$DATE\$

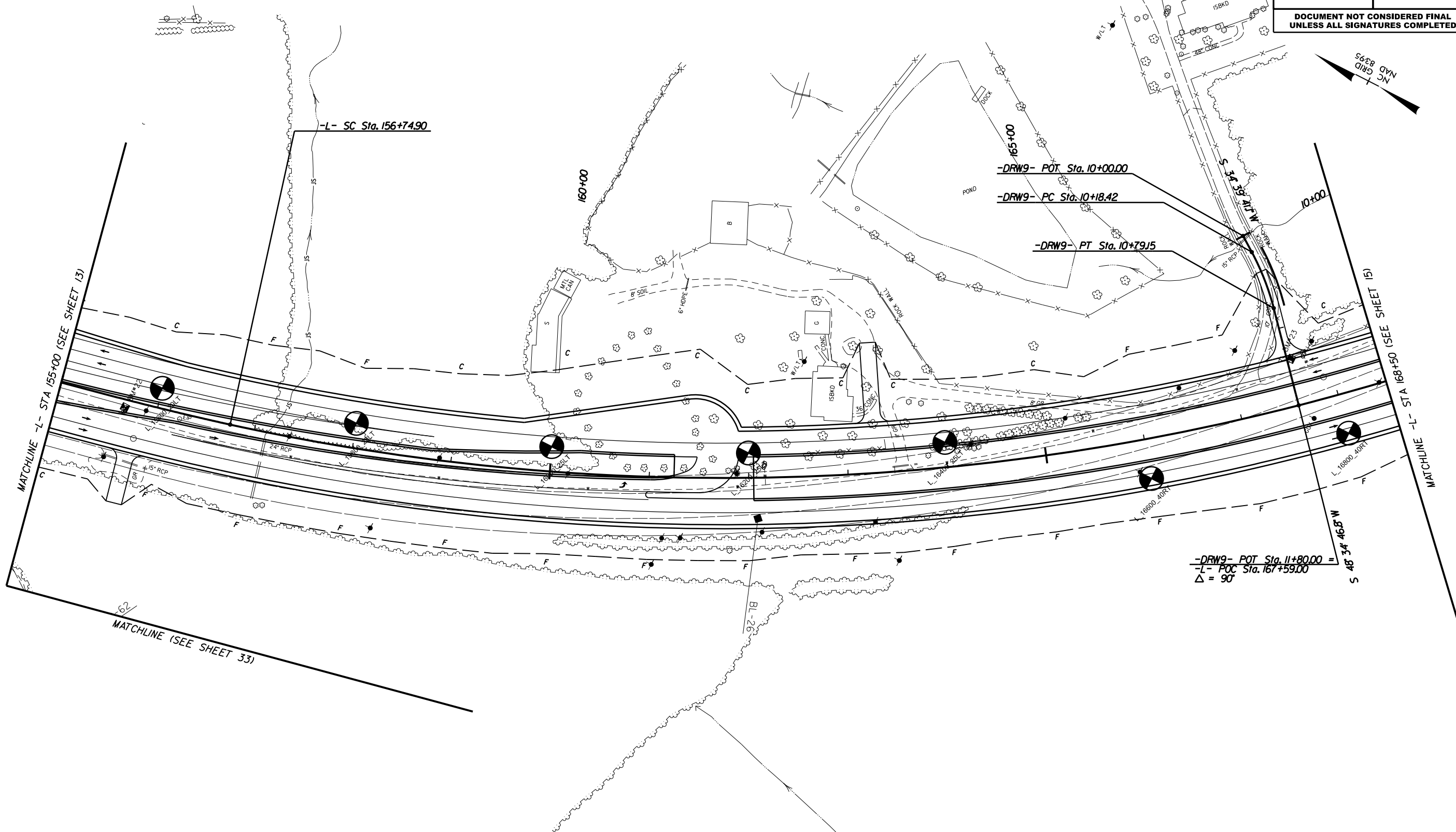
5/14/99

-DRW9-
 PI Sta 10+48.93
 $\Delta = 13^{\circ} 55' 05.7" (RT)$
 $D = 22^{\circ} 55' 05.9"$
 $L = 60.73'$
 $T = 30.52'$
 $R = 250.00'$

-L-
 PIs Sta 155+94.92 PI Sta 163+10.12
 $\Theta_s = 2^{\circ} 57' 48.9"$ $\Delta = 30^{\circ} 37' 29.5" (LT)$
 $L_s = 240.00'$ $D = 2^{\circ} 28' 10.7"$
 $LT = 160.02'$ $L = 1240.05'$
 $ST = 80.02'$ $T = 635.22'$
 $R = 2,320.00'$
 $SE = 0.06$

PROJECT REFERENCE NO. R-2530B/B-4974		SHEET NO. 14	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			

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 RIGHT-OF-WAY REV.
 CONST. REV.



MATCHLINE -L- STA 155+00 (SEE SHEET 13)

MATCHLINE -L- STA 168+50 (SEE SHEET 15)

MATCHLINE (SEE SHEET 33)

-DRW9- POT Sta. 11+80.00 =
 -L- POC Sta. 167+59.00
 $\Delta = 90^{\circ}$

REVISIONS

\$DATE\$

SEE SHEET 39 FOR -L- PROFILE
 SEE SHEET 56 FOR -DRW9- PROFILE

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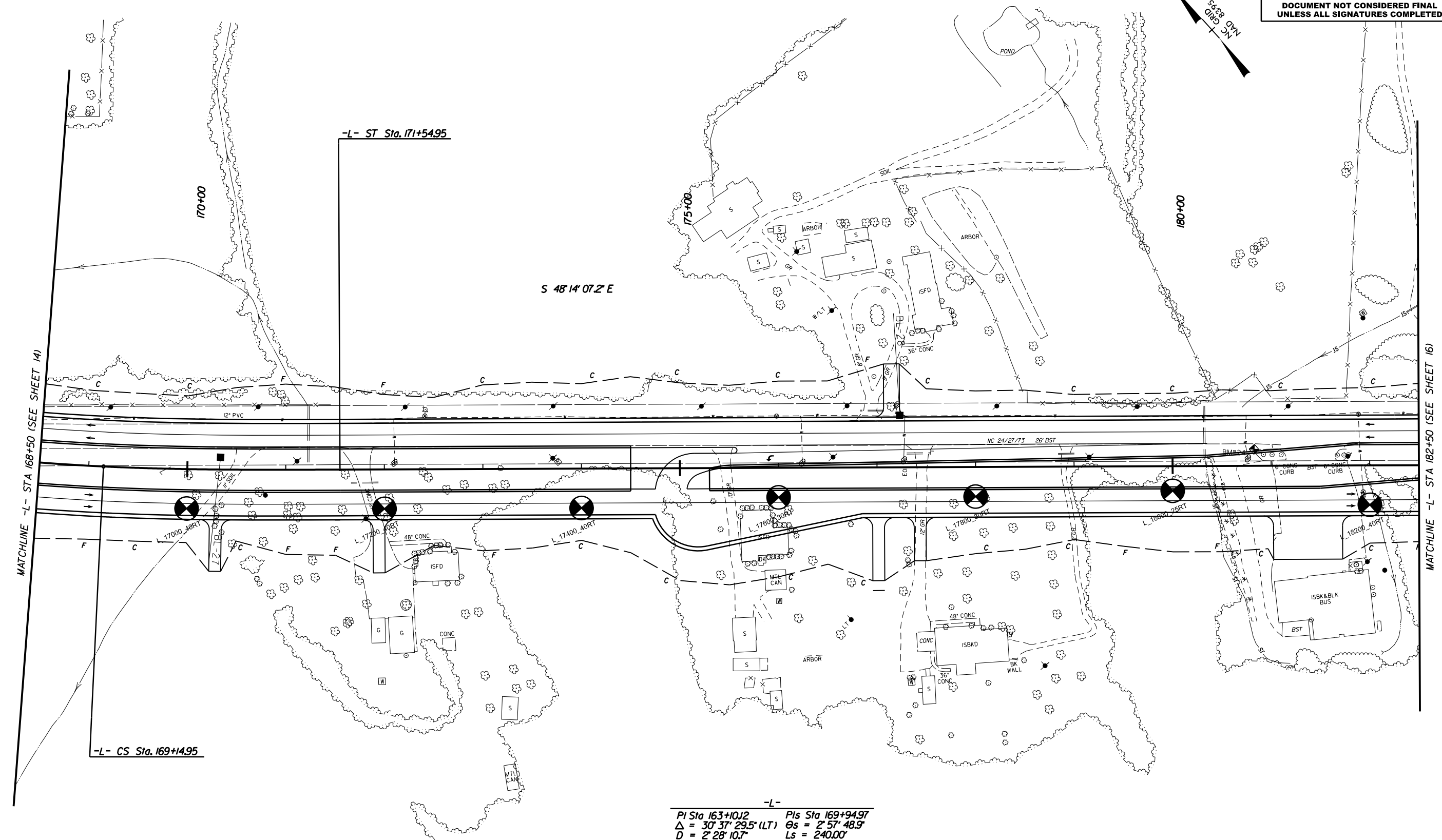
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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 15
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

INCOMPLETE PLANS
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REVISIONS



MATCHLINE -L- STA 168+50 (SEE SHEET 14)

MATCHLINE -L- STA 182+50 (SEE SHEET 16)

-L- ST Sta. 171+54.95

S 48°14'07.2" E

-L- CS Sta. 169+14.95

-L-
 PI Sta 163+10.12 Pis Sta 169+94.97
 $\Delta = 30' 37" 29.5'$ (LT) $\Theta_s = 2' 57" 48.9'$
 $D = 2' 28" 10.7'$ $L_s = 240.00'$
 $L = 1240.05'$ $LT = 160.02'$
 $T = 635.22'$ $ST = 80.02'$
 $R = 2,320.00'$
 $SE = 0.06$

SEE SHEET 39 FOR -L- PROFILE

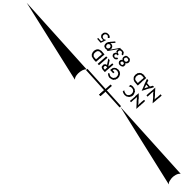
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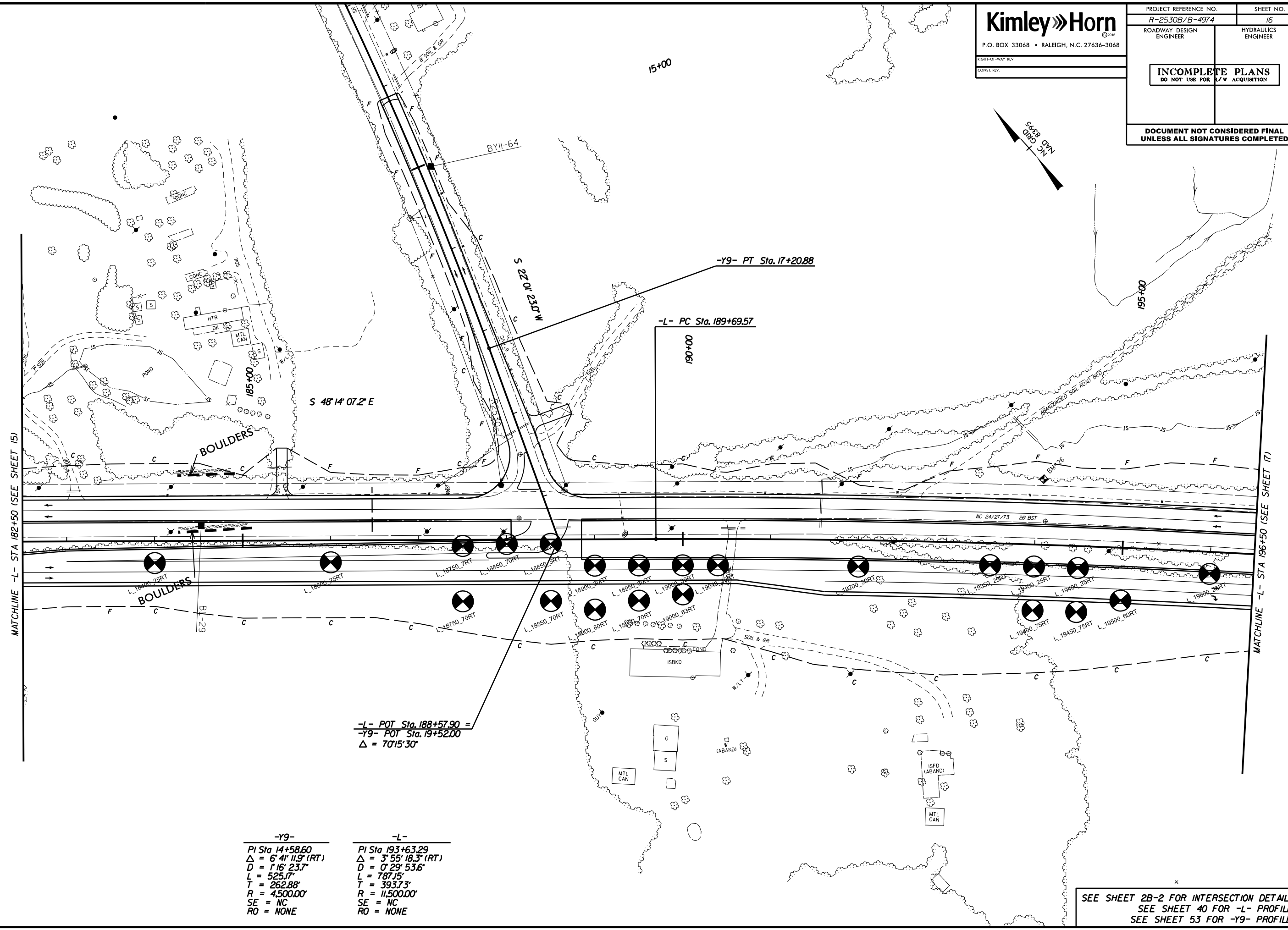
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RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 16
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



REVISIONS



-L- POT Sta. 188+57.90 =
 -Y9- POT Sta. 19+52.00
 $\Delta = 70'15''30''$

-Y9-	-L-
PI Sta 14+58.60	PI Sta 193+63.29
$\Delta = 6' 41'' 11.9'' (RT)$	$\Delta = 3' 55'' 18.3'' (RT)$
$D = 1' 16'' 23.7''$	$D = 0' 29'' 53.6''$
$L = 525.17'$	$L = 787.15'$
$T = 262.88'$	$T = 393.73'$
$R = 4500.00'$	$R = 11,500.00'$
SE = NC	SE = NC
RO = NONE	RO = NONE

SEE SHEET 2B-2 FOR INTERSECTION DETAILS
 SEE SHEET 40 FOR -L- PROFILE
 SEE SHEET 53 FOR -Y9- PROFILE

\$DATE\$

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 ROADWAY DESIGN ENGINEER
 HYDRAULICS ENGINEER

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 17
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

REVISIONS

MATCHLINE -L- STA 196+50 (SEE SHEET 16)

MATCHLINE -L- STA 210+00 (SEE SHEET 18)

-L- PT Sta. 197+56.71

200+00

S 44° 18' 48.9" E

R2530B-8

205+00

BY13-66

548.88' NAD 83/95

ROADWAY EMBANKMENT

-L- POT Sta. 197+69.10 =
-Y10- POT Sta. 10+00.00
Δ = 82° 52' 26"

-L- TS Sta. 203+20.18

-L- SC Sta. 206+00.18

S 38° 33' 37.0" W

L_20100_70RT L_20150_70RT L_20200_70RT L_20250_70RT L_20300_70RT

BL-30

L_20800_25RT

60" CONC

12" CONC

BY12-65

15+00

-L-
 PIs Sta 205+06.90 PIs Sta 210+41.13
 θs = 4° 07' 26.8" Δ = 25° 32' 49.4" (LT)
 Ls = 280.00' D = 2° 56' 44.9"
 LT = 186.72' L = 867.24'
 ST = 93.38' T = 440.95'
 R = 1,945.00'
 SE = 0.07

\$DATE\$

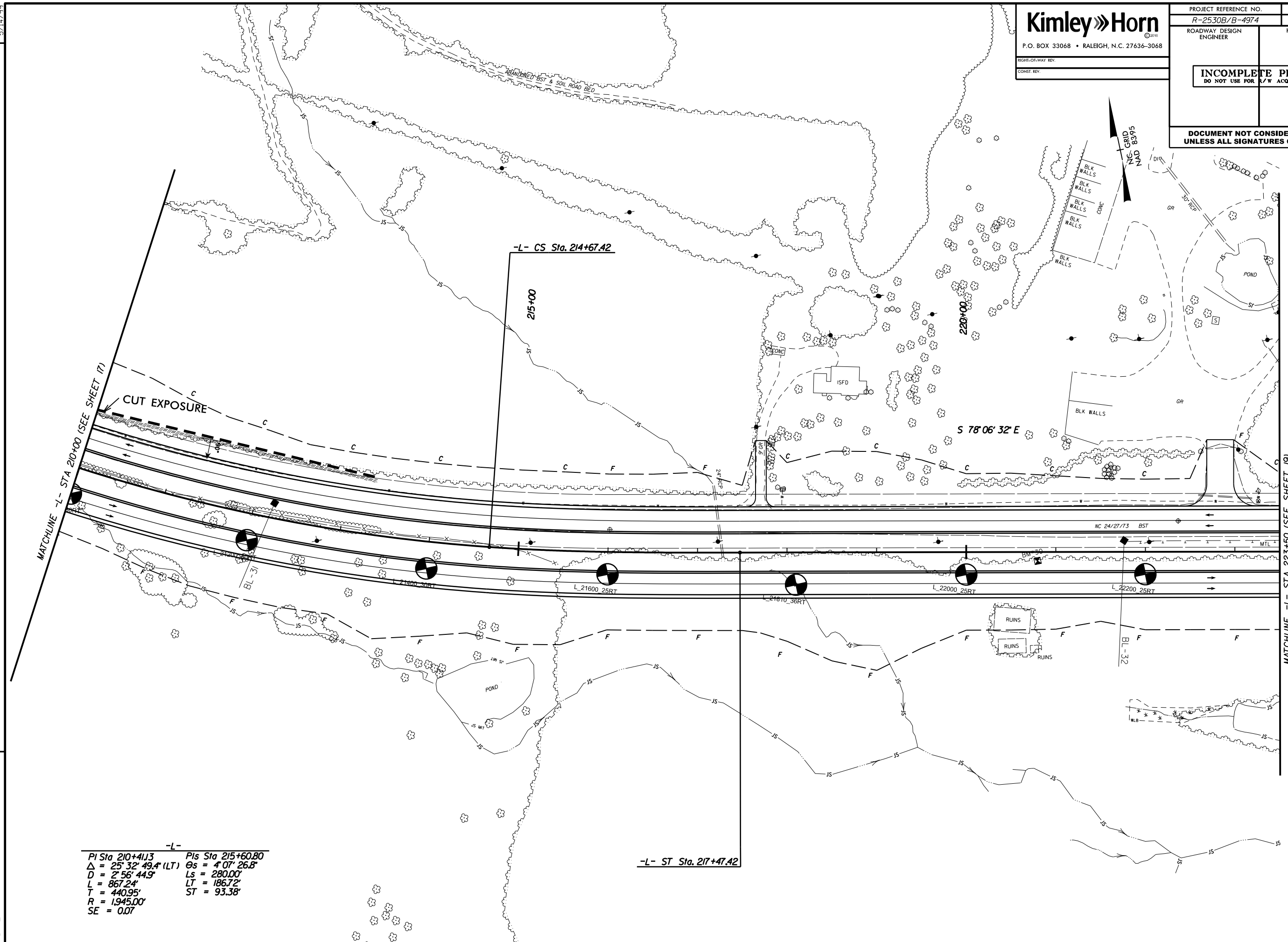
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RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 18
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

REVISIONS



-L-

PI Sta 210+41.13	PIs Sta 215+60.80
$\Delta = 25^{\circ} 32' 49.4''$ (LT)	$\Theta_s = 4^{\circ} 07' 26.8''$
$D = 2^{\circ} 56' 44.9''$	$L_s = 280.00'$
$L = 867.24'$	$LT = 186.72'$
$T = 440.95'$	$ST = 93.38'$
$R = 1,945.00'$	
$SE = 0.07$	

-L- ST Sta. 217+47.42

\$DATE\$

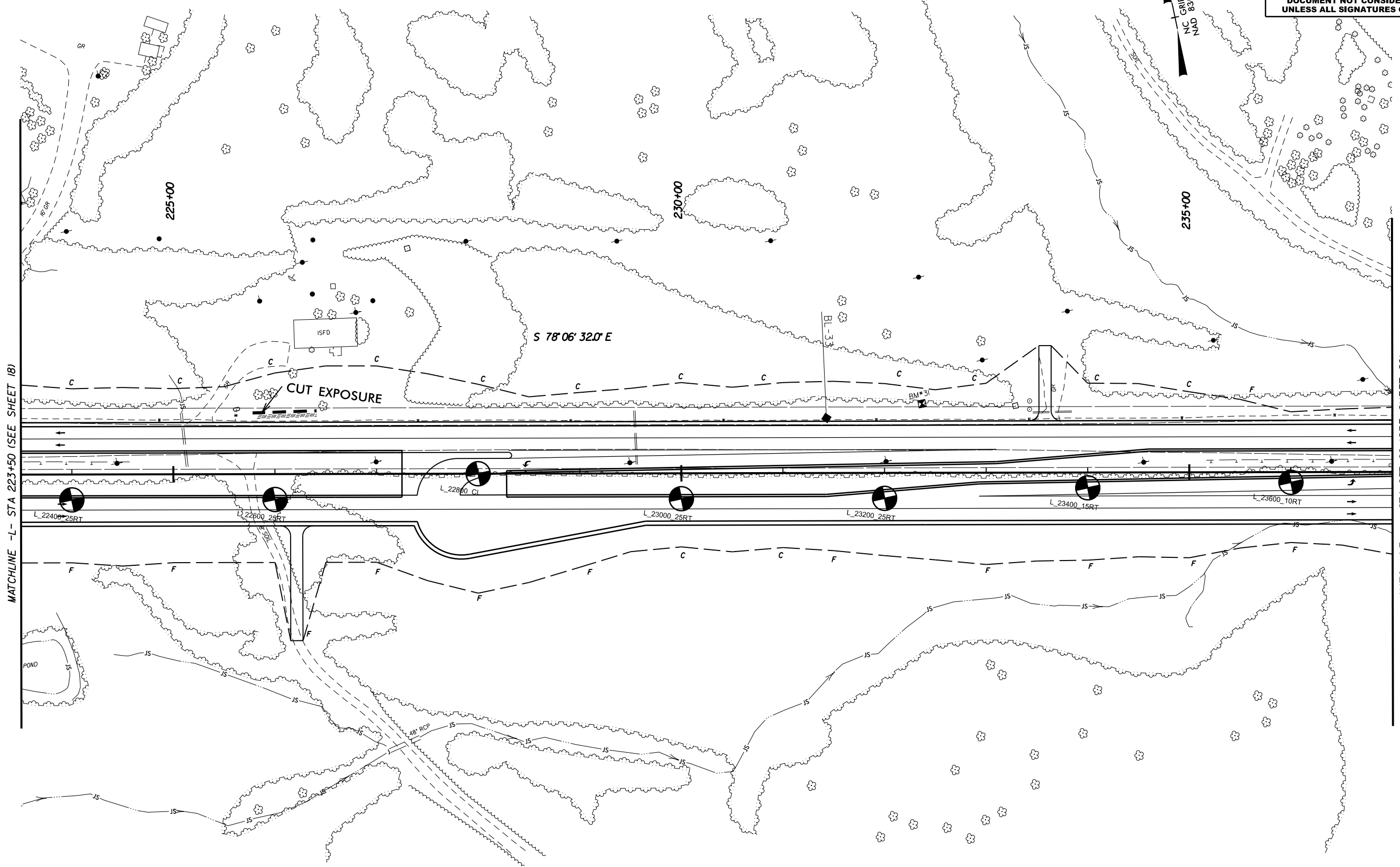
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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 19
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

INCOMPLETE PLANS
DO NOT USE FOR R/W ACQUISITION

DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED



REVISIONS

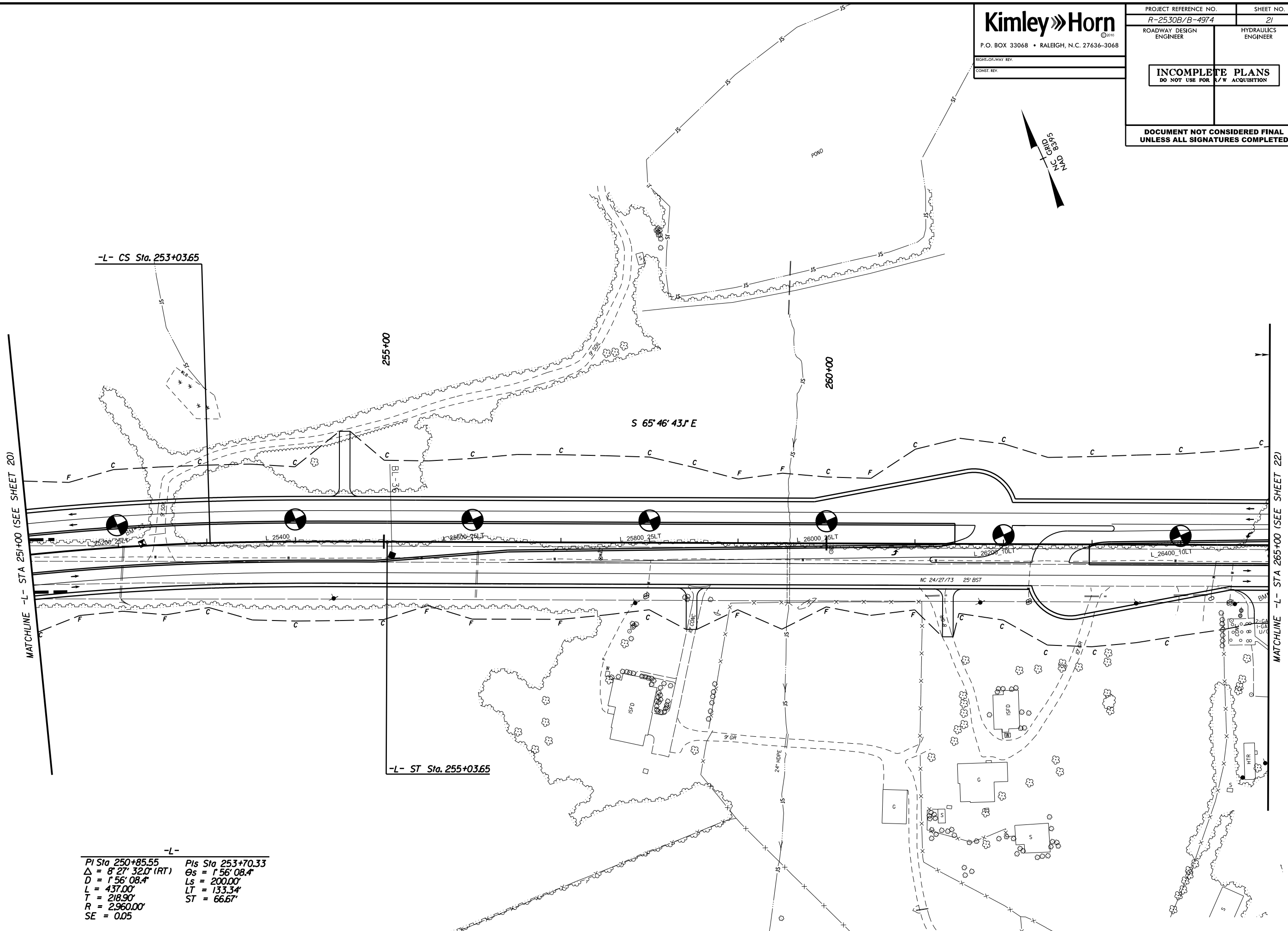
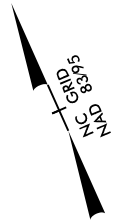
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RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 21
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



-L- CS Sta. 253+03.65

255+00

260+00

S 65° 46' 43.1° E

MATCHLINE -L- STA 251+00 (SEE SHEET 20)

MATCHLINE -L- STA 265+00 (SEE SHEET 22)

-L- ST Sta. 255+03.65

-L-

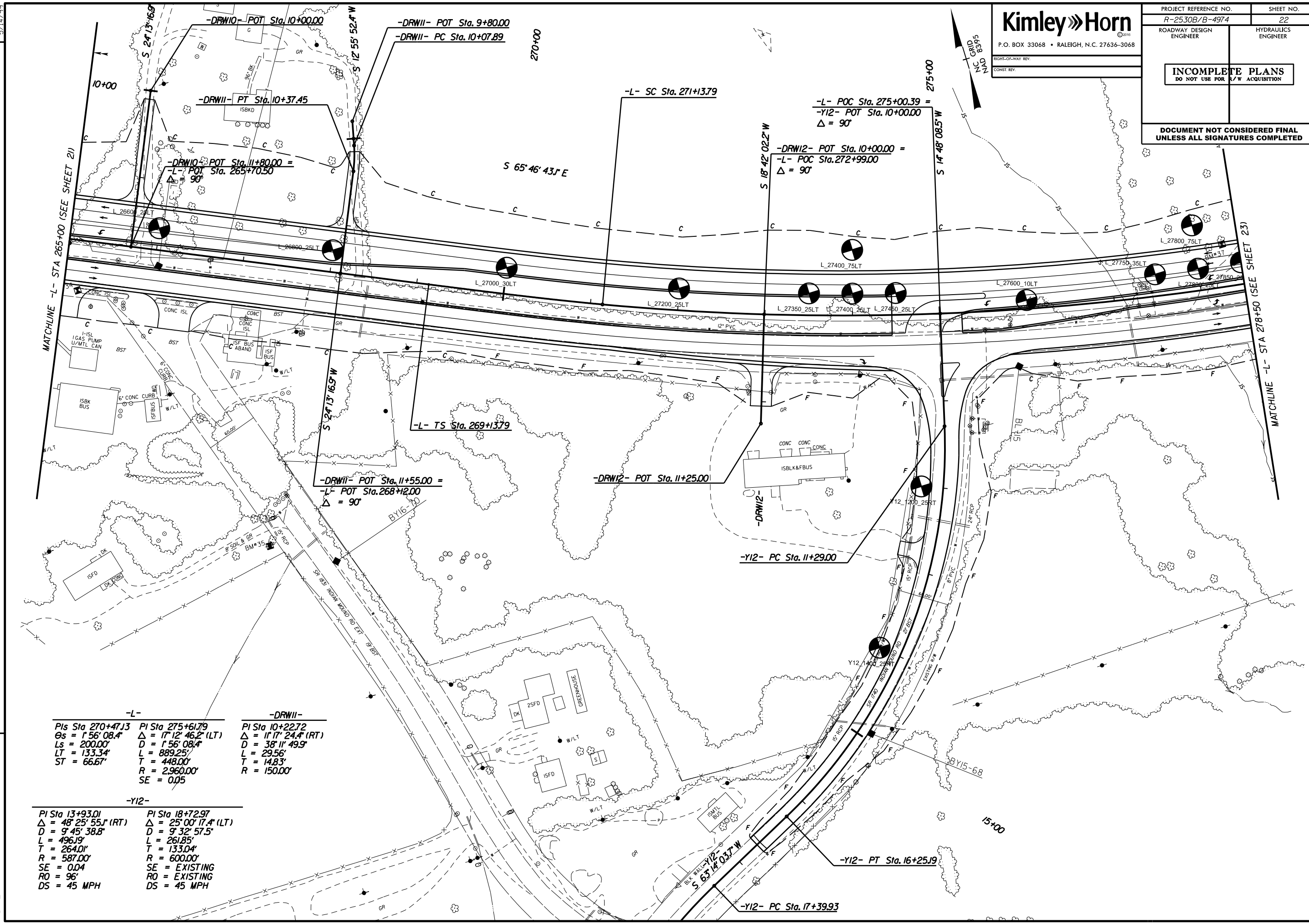
PI Sta 250+85.55	PIs Sta 253+70.33
$\Delta = 8' 27' 32.0''$ (RT)	$\Theta_s = 1' 56' 08.4''$
$D = 1' 56' 08.4''$	$L_s = 200.00'$
$L = 437.00'$	$LT = 133.34'$
$T = 218.90'$	$ST = 66.67'$
$R = 2960.00'$	
$SE = 0.05$	

REVISIONS

\$DATE\$

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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 22
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



-L-		-DRW11-	
PI Sta 270+47.13	PI Sta 275+61.79	PI Sta 10+22.72	
Δ = 1° 56' 08.4"	Δ = 17° 12' 46.2" (LT)	Δ = 11° 17' 24.4" (RT)	
Ls = 200.00'	D = 1° 56' 08.4"	D = 38° 11' 49.9"	
LT = 133.34'	L = 889.25'	L = 29.56'	
ST = 66.67'	T = 448.00'	T = 14.83'	
	R = 2,960.00'	R = 150.00'	
	SE = 0.05		
-Y12-			
PI Sta 13+93.01	PI Sta 18+72.97		
Δ = 48° 25' 55.1" (RT)	Δ = 25° 00' 17.4" (LT)		
D = 9° 45' 38.8"	D = 9° 32' 57.5"		
L = 496.19'	L = 261.85'		
T = 264.01'	L = 133.04'		
R = 587.00'	R = 600.00'		
SE = 0.04	SE = EXISTING		
RO = 96'	RO = EXISTING		
DS = 45 MPH	DS = 45 MPH		

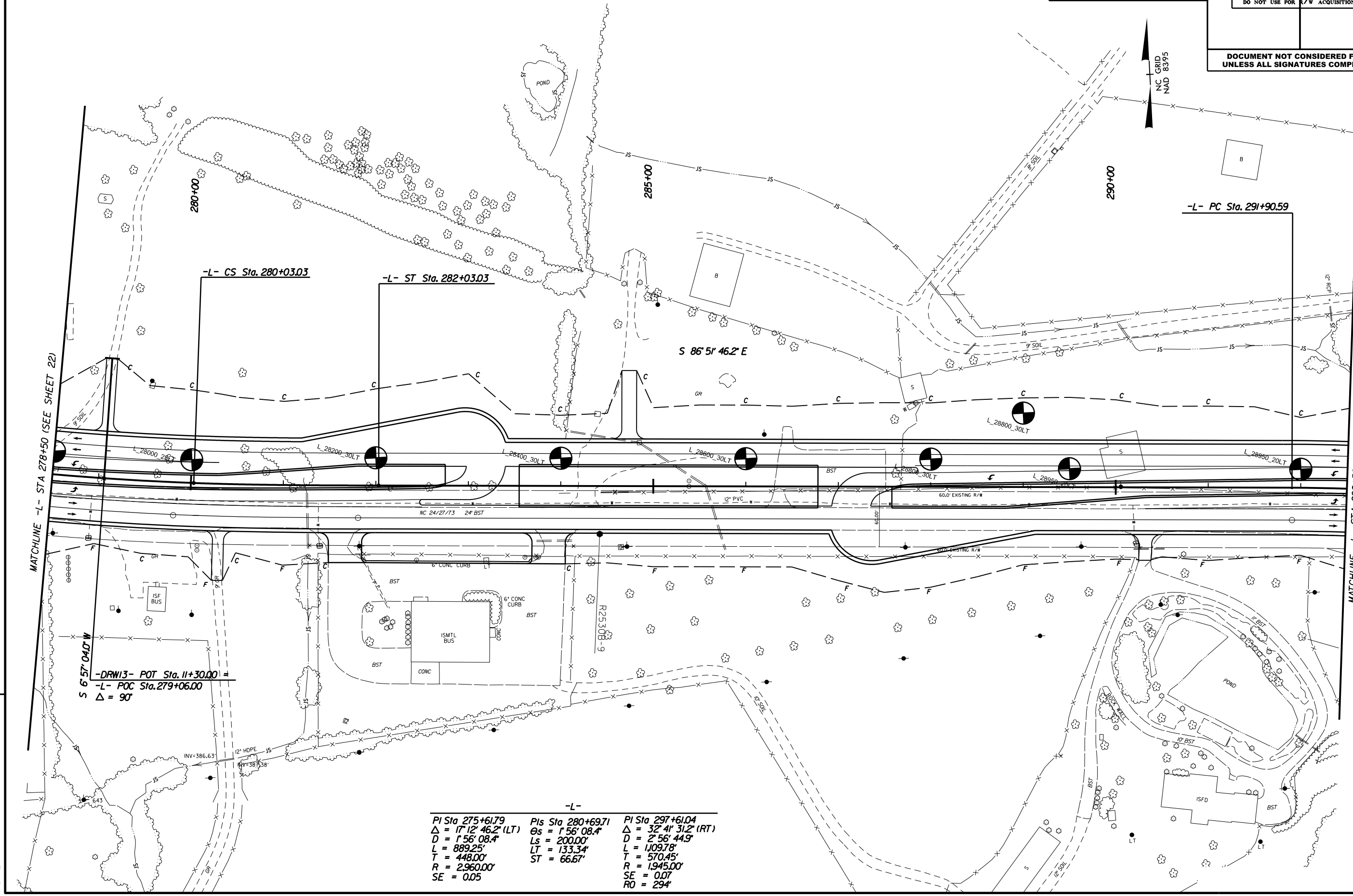
REVISIONS

\$DATE\$

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DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED

REVISIONS



MATCHLINE -L- STA 278+50 (SEE SHEET 22)

MATCHLINE -L- STA 292+50 (SEE SHEET 24)

-DRW13- POT Sta. 11+30.00
 -L- POC Sta. 279+06.00
 $\Delta = 90^\circ$

-L-		
PI Sta 275+61.79	PIs Sta 280+69.71	PI Sta 297+61.04
$\Delta = 17^\circ 12' 46.2"$ (LT)	$\Theta_s = 1^\circ 56' 08.4"$	$\Delta = 32^\circ 41' 31.2"$ (RT)
D = 1' 56' 08.4"	Ls = 200.00'	D = 2' 56' 44.9"
L = 889.25'	LT = 133.34'	L = 1109.78'
T = 448.00'	ST = 66.67'	T = 570.45'
R = 2,960.00'		R = 1,945.00'
SE = 0.05		SE = 0.07
		RO = 294'

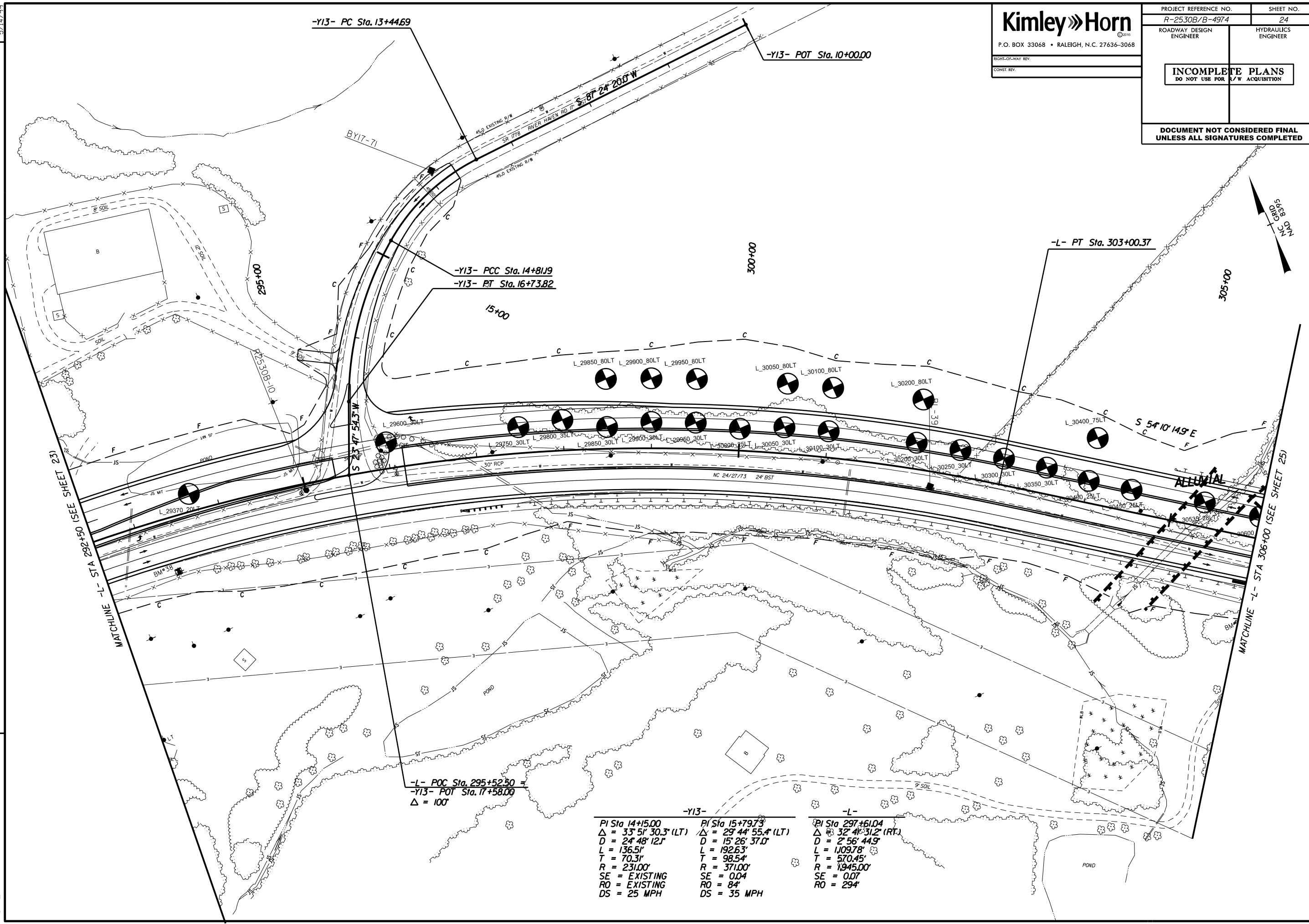
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 ROADWAY DESIGN ENGINEER
 HYDRAULICS ENGINEER

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 24
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

REVISIONS

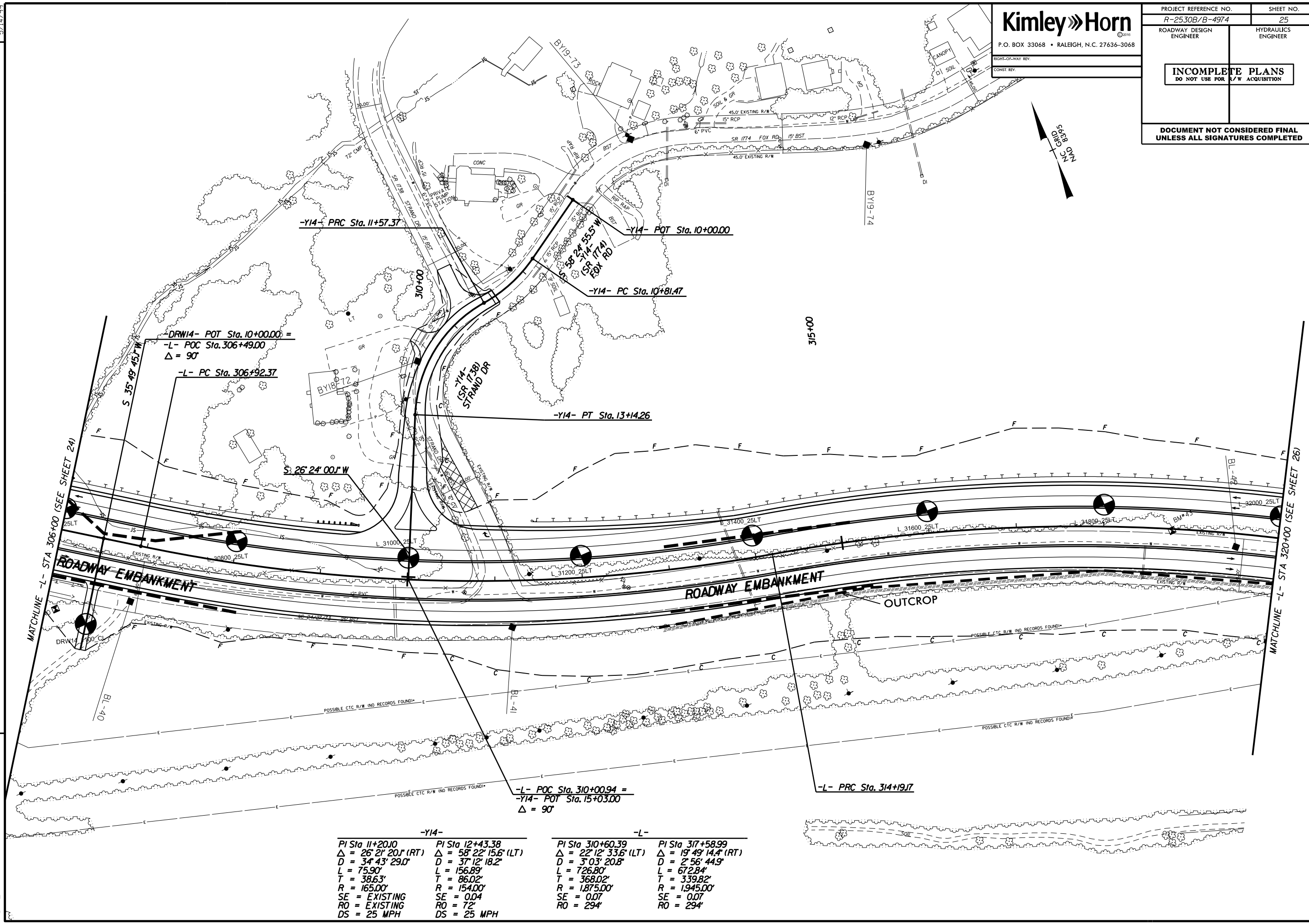


-Y13-	-L-
PI Sta 14+15.00	PI Sta 297+61.04
$\Delta = 33^\circ 51' 30.3" (LT)$	$\Delta = 32^\circ 41' 31.2" (RT)$
D = 24' 48" 12.1'	D = 2' 56" 44.9'
L = 136.51'	L = 1,109.78'
T = 70.31'	T = 570.45'
R = 231.00'	R = 1,945.00'
SE = EXISTING	SE = 0.07
RO = EXISTING	RO = 294'
DS = 25 MPH	

\$DATE\$

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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 25
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



DRW14- POT Sta. 10+00.00 =
 -L- POC Sta. 306+49.00
 $\Delta = 90^\circ$
 -L- PC Sta. 306+92.37

-L- POC Sta. 310+00.94 =
 -Y14- POT Sta. 15+03.00
 $\Delta = 90^\circ$

-Y14-		-L-	
PI Sta 11+20.10	PI Sta 12+43.38	PI Sta 310+60.39	PI Sta 317+58.99
$\Delta = 26^\circ 21' 20.1^\circ$ (RT)	$\Delta = 58^\circ 22' 15.6^\circ$ (LT)	$\Delta = 22^\circ 12' 33.6^\circ$ (LT)	$\Delta = 19^\circ 49' 14.4^\circ$ (RT)
D = 34' 43" 29.0"	D = 37' 12" 18.2"	D = 3' 03" 20.8"	D = 2' 56" 44.9"
L = 75.90'	L = 156.89'	L = 726.80'	L = 672.84'
T = 38.63'	T = 86.02'	T = 368.02'	T = 339.82'
R = 165.00'	R = 154.00'	R = 1,875.00'	R = 1,945.00'
SE = EXISTING	SE = 0.04	SE = 0.07	SE = 0.07
RO = EXISTING	RO = 72'	RO = 294'	RO = 294'
DS = 25 MPH	DS = 25 MPH		

REVISIONS

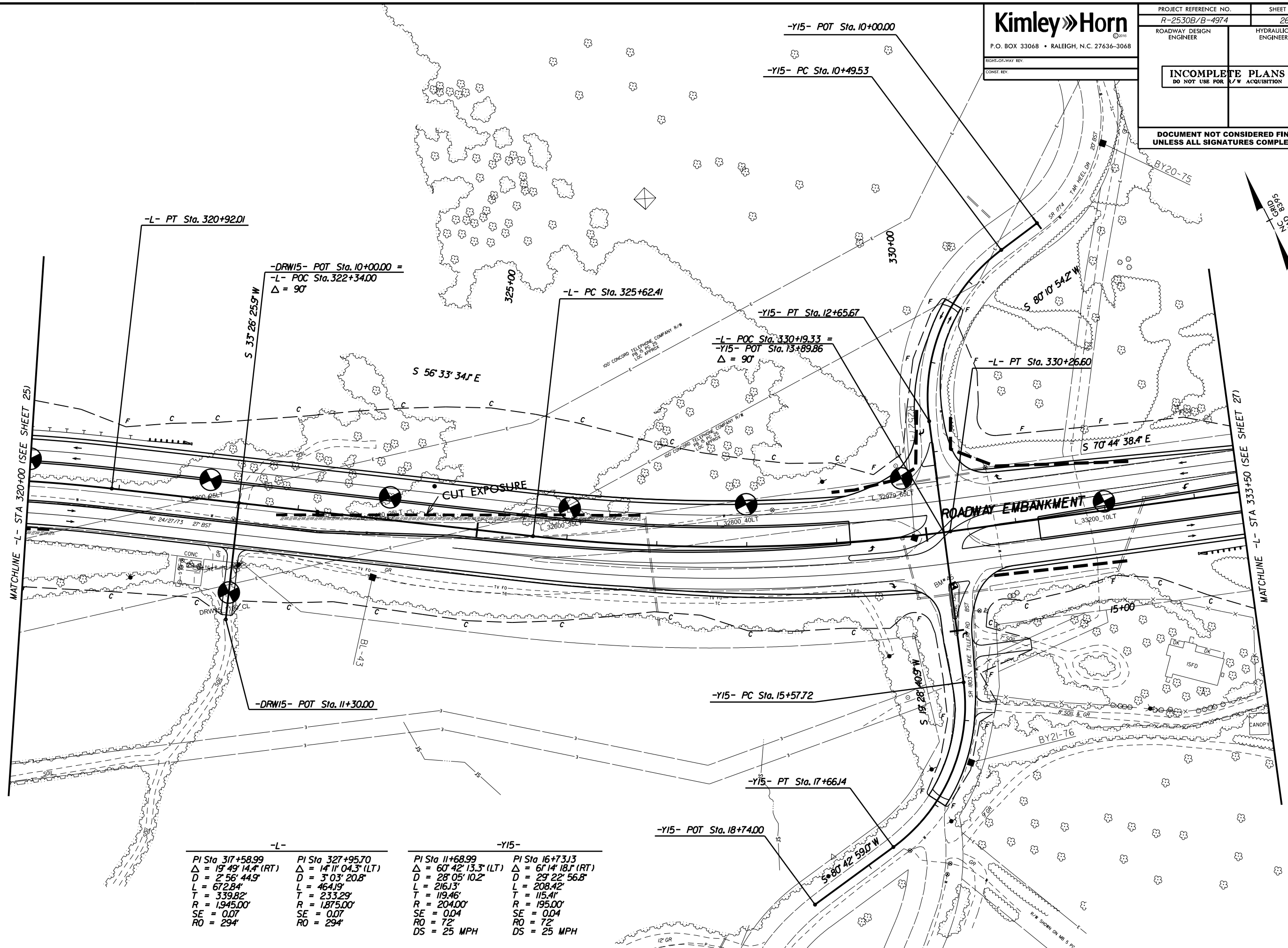
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 ROADWAY DESIGN ENGINEER
 HYDRAULICS ENGINEER

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 26
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

REVISIONS



-L-		-Y15-	
PI Sta 317+58.99	PI Sta 327+95.70	PI Sta 11+68.99	PI Sta 16+73.13
$\Delta = 19^\circ 49' 14.4''$ (RT)	$\Delta = 14^\circ 11' 04.3''$ (LT)	$\Delta = 60^\circ 42' 13.3''$ (LT)	$\Delta = 6^\circ 14' 18.1''$ (RT)
D = 2' 56' 44.9"	D = 3' 03' 20.8"	D = 28' 05' 10.2"	D = 29' 22' 56.8"
L = 672.84'	L = 464.19'	L = 216.13'	L = 208.42'
T = 339.82'	T = 233.29'	T = 119.46'	T = 115.41'
R = 1,945.00'	R = 1,875.00'	R = 204.00'	R = 195.00'
SE = 0.07	SE = 0.07	SE = 0.04	SE = 0.04
RO = 294'	RO = 294'	RO = 72'	RO = 72'
		DS = 25 MPH	DS = 25 MPH

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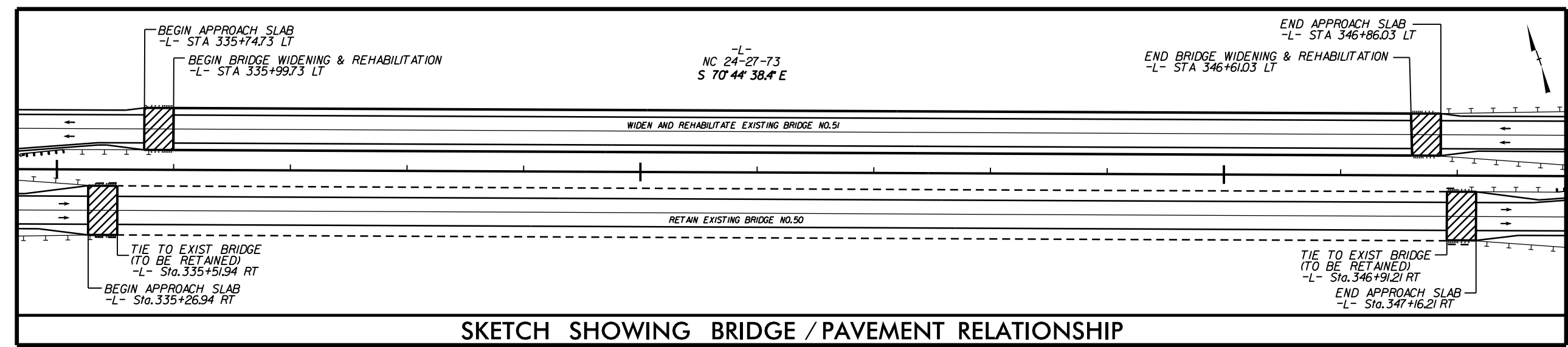
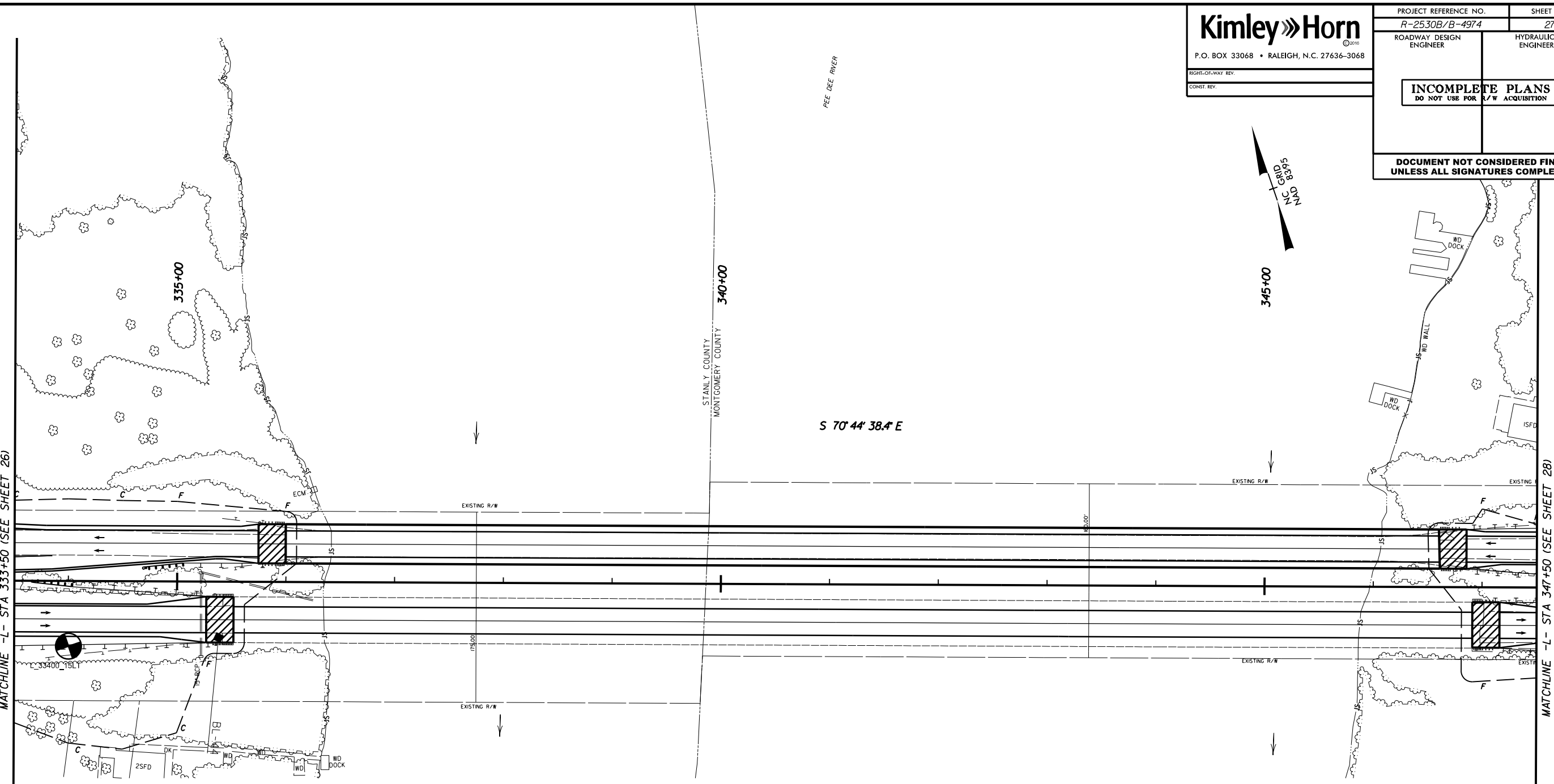
RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 27
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

REVISIONS

MATCHLINE -L- STA 333+50 (SEE SHEET 26)

MATCHLINE -L- STA 347+50 (SEE SHEET 28)



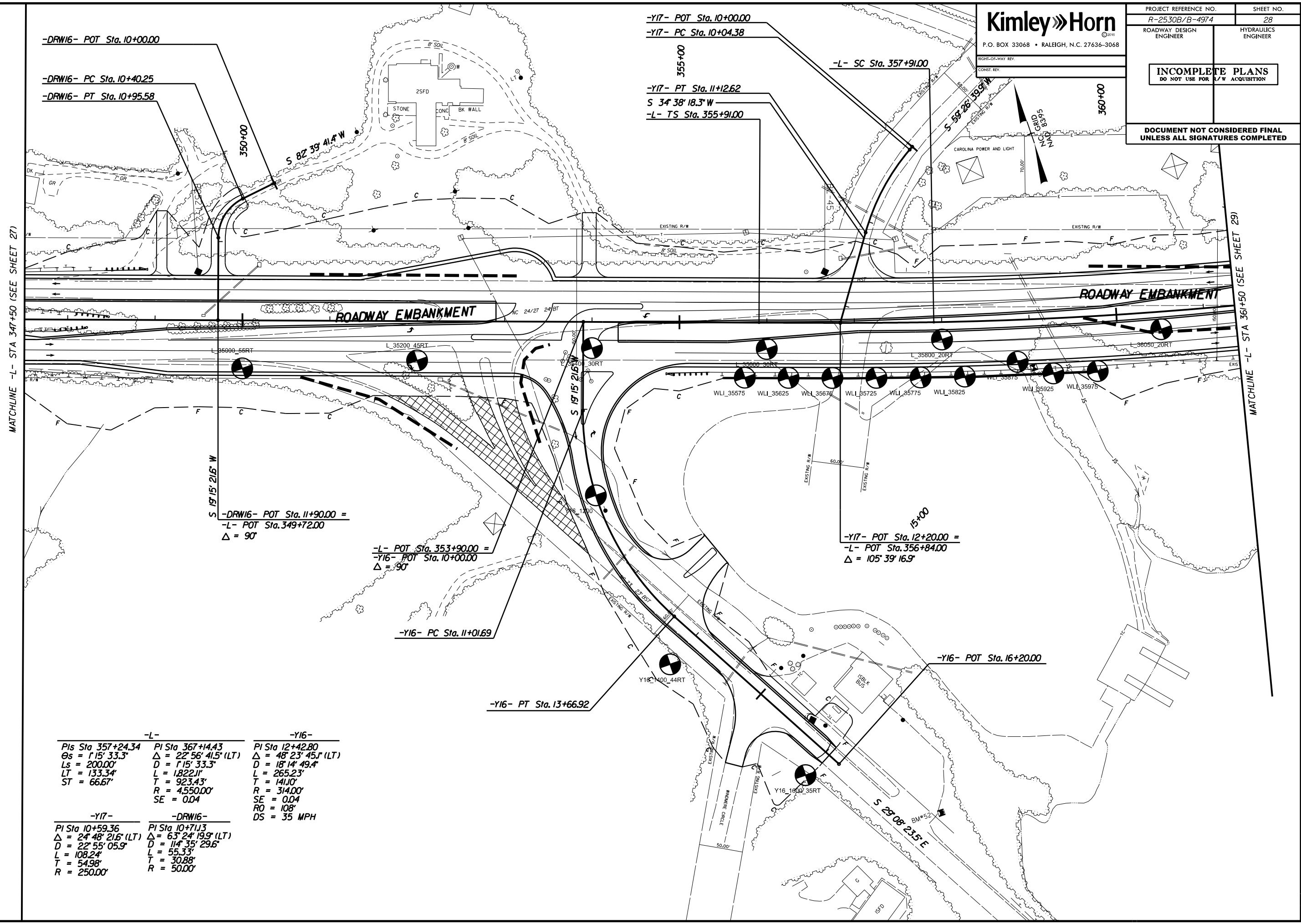
SKETCH SHOWING BRIDGE / PAVEMENT RELATIONSHIP

\$DATE\$

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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 28
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



-DRW16- POT Sta. 10+00.00
 -DRW16- PC Sta. 10+40.25
 -DRW16- PT Sta. 10+95.58

-Y17- POT Sta. 10+00.00
 -Y17- PC Sta. 10+04.38
 355+00
 -Y17- PT Sta. 11+12.62
 S 34° 38' 18.3" W
 -L- TS Sta. 355+91.00

-L- SC Sta. 357+91.00

360+00

MATCHLINE -L- STA 347+50 (SEE SHEET 27)

MATCHLINE -L- STA 361+50 (SEE SHEET 29)

-DRW16- POT Sta. 11+90.00 =
 -L- POT Sta. 349+72.00
 Δ = 90°

-L- POT Sta. 353+90.00 =
 -Y16- POT Sta. 10+00.00
 Δ = 90°

-Y17- POT Sta. 12+20.00 =
 -L- POT Sta. 356+84.00
 Δ = 105° 39' 16.9"

-Y16- PC Sta. 11+01.69

-Y16- PT Sta. 13+66.92

-Y16- POT Sta. 16+20.00

-L-		-Y16-	
PI Sta 357+24.34	PI Sta 367+14.43	PI Sta 12+42.80	PI Sta 16+20.00
θs = 1° 15' 33.3"	Δ = 22° 56' 41.5" (LT)	Δ = 48° 23' 45.1" (LT)	Δ = 105° 39' 16.9" (LT)
Ls = 200.00'	D = 1° 15' 33.3"	D = 18° 14' 49.4"	D = 114° 35' 29.6"
LT = 133.34'	L = 1,822.11'	L = 265.23'	L = 55.33'
ST = 66.67'	T = 923.43'	T = 141.0'	T = 30.88'
	R = 4,550.00'	R = 314.00'	R = 50.00'
	SE = 0.04	SE = 0.04	SE = 0.04
		RO = 108°	RO = 108°
		DS = 35 MPH	DS = 35 MPH
-Y17-		-DRW16-	
PI Sta 10+59.36	PI Sta 10+71.13	PI Sta 10+71.13	PI Sta 10+71.13
Δ = 24° 48' 21.6" (LT)	Δ = 63° 24' 19.9" (LT)	Δ = 63° 24' 19.9" (LT)	Δ = 63° 24' 19.9" (LT)
D = 22° 55' 05.9"	D = 114° 35' 29.6"	D = 114° 35' 29.6"	D = 114° 35' 29.6"
L = 108.24'	L = 55.33'	L = 55.33'	L = 55.33'
T = 54.98'	T = 30.88'	T = 30.88'	T = 30.88'
R = 250.00'	R = 50.00'	R = 50.00'	R = 50.00'

REVISIONS

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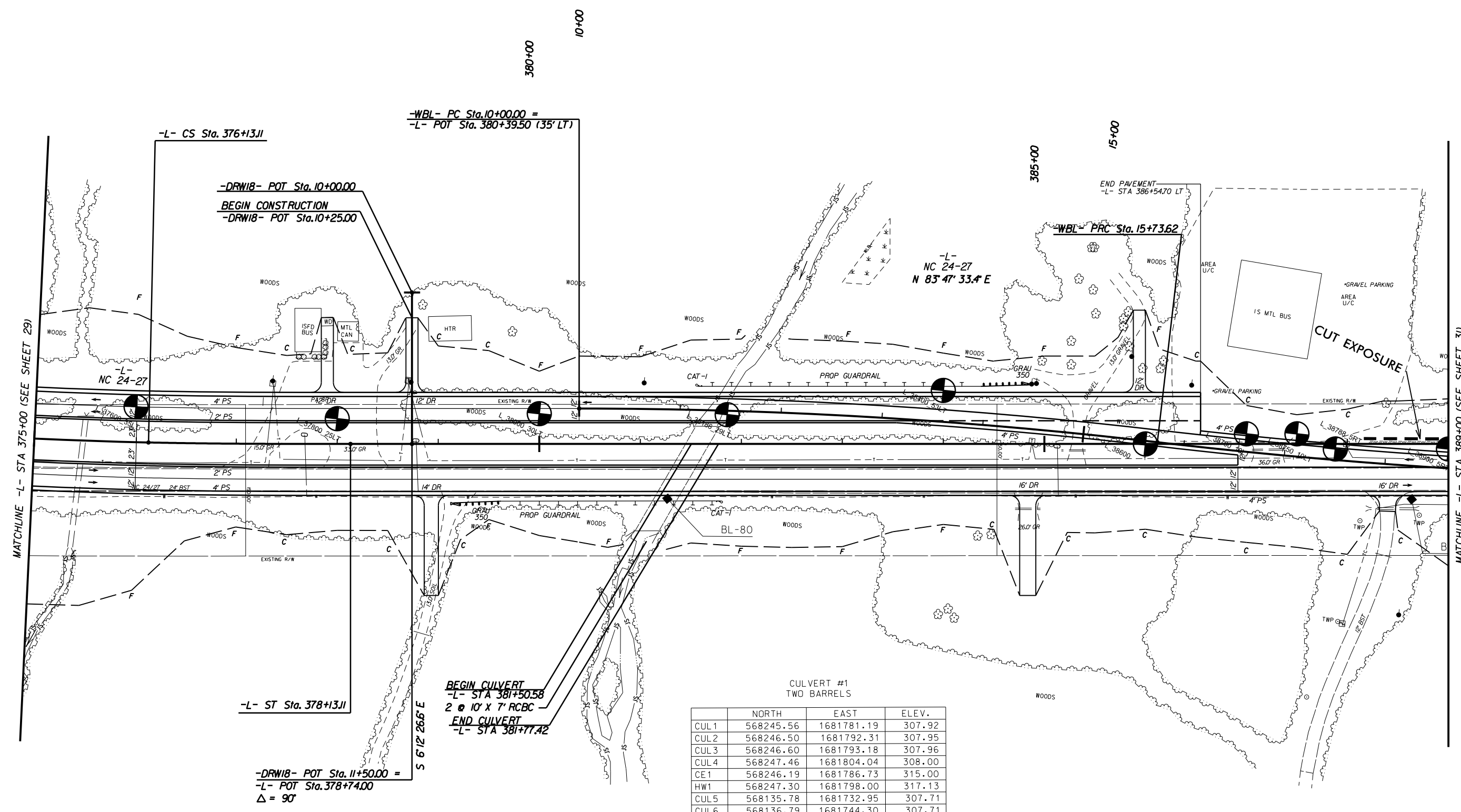
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 ROADWAY DESIGN ENGINEER
 HYDRAULICS ENGINEER

PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 30
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

-L-		-WBL-	
PI Sta 367+14.43	PIs Sta 376+79.78	PI Sta 12+87.13	PI Sta 18+90.68
$\Delta = 22^{\circ} 56' 41.5" (LT)$	$\Theta_s = 1^{\circ} 15' 33.3"$	$\Delta = 6^{\circ} 39' 10.8" (RT)$	$\Delta = 6^{\circ} 39' 10.8" (LT)$
$D = 1^{\circ} 15' 33.3"$	$L_s = 200.00'$	$D = 1^{\circ} 09' 35.4"$	$D = 1^{\circ} 03' 01.2"$
$L = 1822.11'$	$LT = 133.34'$	$L = 573.62'$	$L = 633.42'$
$T = 923.43'$	$ST = 66.67'$	$T = 287.13'$	$T = 317.07'$
$R = 4,550.00'$		$R = 4,940.00'$	$R = 5,455.00'$
$SE = 0.04$		$SE = RC$	$SE = RC$
		$RO = 48'$	$RO = 48'$
		$DS = 50 MPH$	$DS = 50 MPH$



REVISIONS



BEGIN CULVERT
 -L- STA 381+50.58
2 @ 10' x 7' RCBC
END CULVERT
 -L- STA 381+77.42

CULVERT #1
TWO BARRELS

	NORTH	EAST	ELEV.
CUL1	568245.56	1681781.19	307.92
CUL2	568246.50	1681792.31	307.95
CUL3	568246.60	1681793.18	307.96
CUL4	568247.46	1681804.04	308.00
CE1	568246.19	1681786.73	315.00
HW1	568247.30	1681798.00	317.13
CUL5	568135.78	1681732.95	307.71
CUL6	568136.79	1681744.30	307.71
CUL7	568136.98	1681744.94	307.67
CUL8	568138.21	1681756.32	307.70
CE2	568136.71	1681738.98	314.70
HW2	568137.59	1681744.59	316.84

\$DATE\$

MATCHLINE -L- STA 375+00 (SEE SHEET 29)

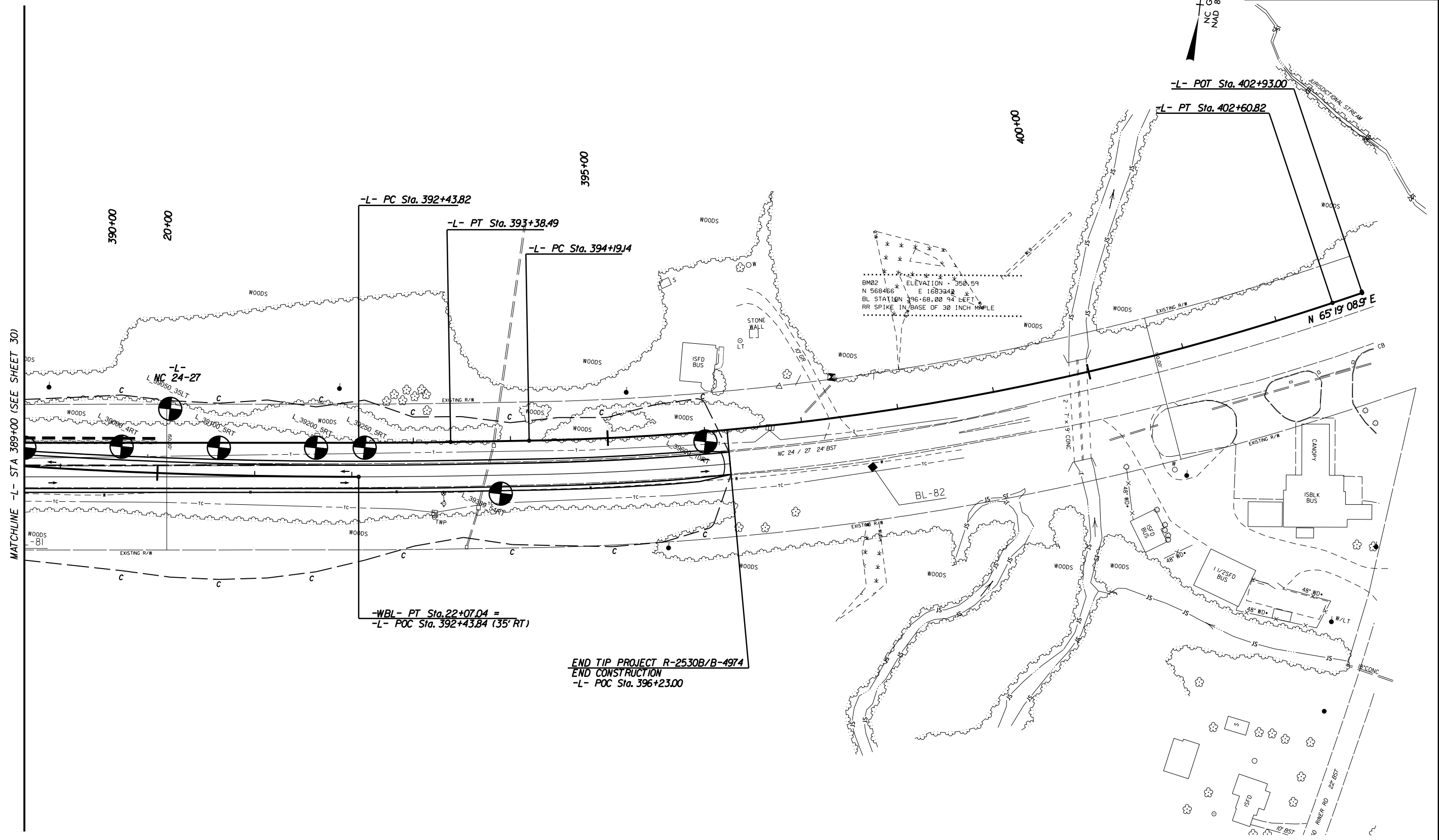
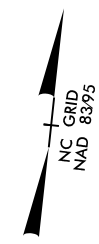
MATCHLINE -L- STA 389+00 (SEE SHEET 31)

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PROJECT REFERENCE NO. R-2530B/B-4974	SHEET NO. 31
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

-L-		-WBL-	
PI Sta 392+91.16	PI Sta 398+43.27	PI Sta 18+90.68	
$\Delta = 1^{\circ}00'02.4"$ (LT)	$\Delta = 1^{\circ}28'22.1"$ (LT)	$\Delta = 6^{\circ}39'10.8"$ (LT)	
D = 1'03'25.6"	D = 2'04'33.4"	D = 1'03'01.2"	
L = 94.66'	L = 841.68'	L = 633.42'	
T = 47.33'	T = 424.13'	T = 317.07'	
R = 5,420.00'	R = 2,760.00'	R = 5,455.00'	
SE = 0.03	SE = 0.03	SE = RC	
RO = 126'	RO = 210'	RO = 48'	
		DS = 50 MPH	



MATCHLINE -L- STA 389+00 (SEE SHEET 30)

END TIP PROJECT R-2530B/B-4974
END CONSTRUCTION
 -L- POC Sta. 396+23.00

REVISIONS

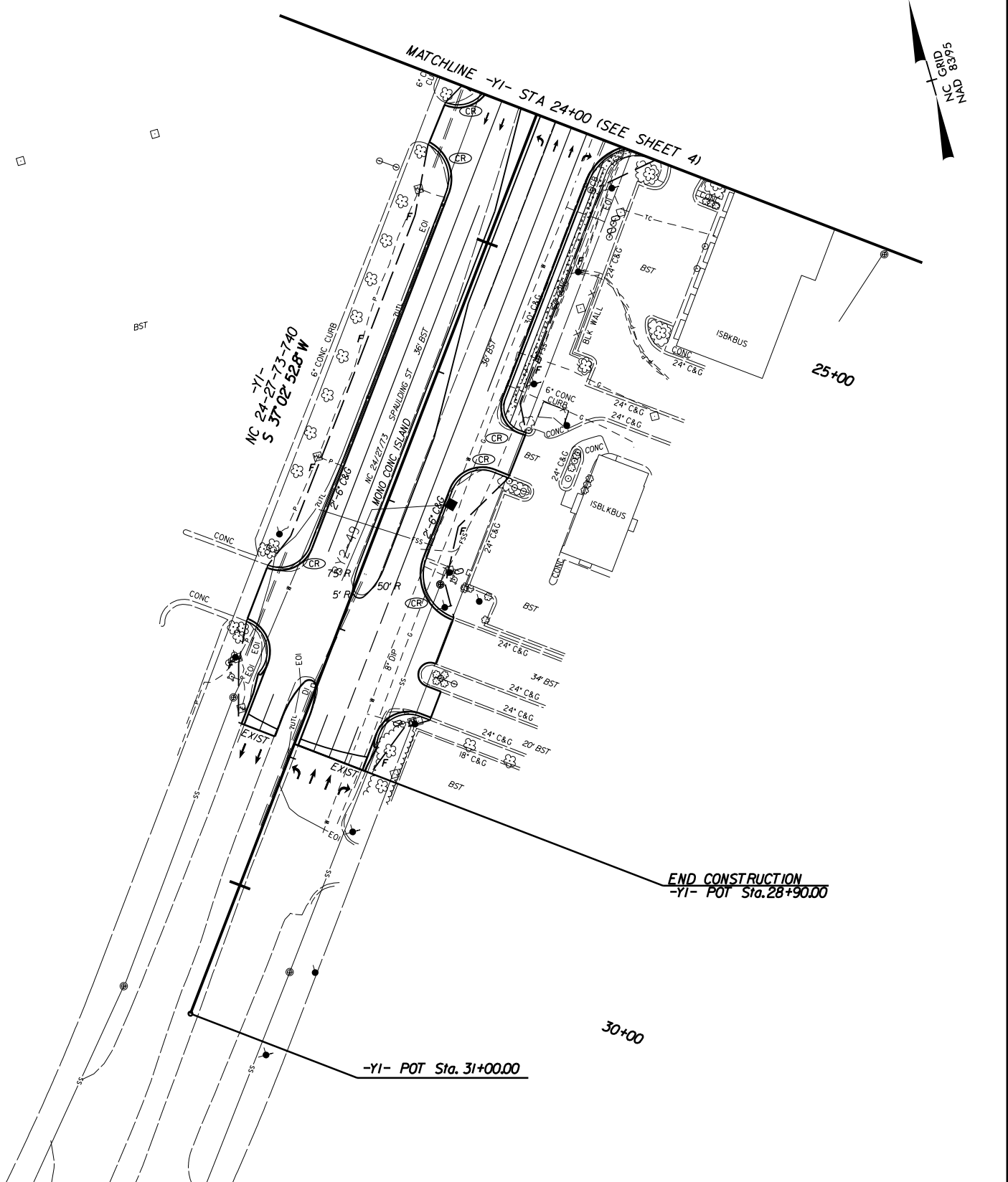
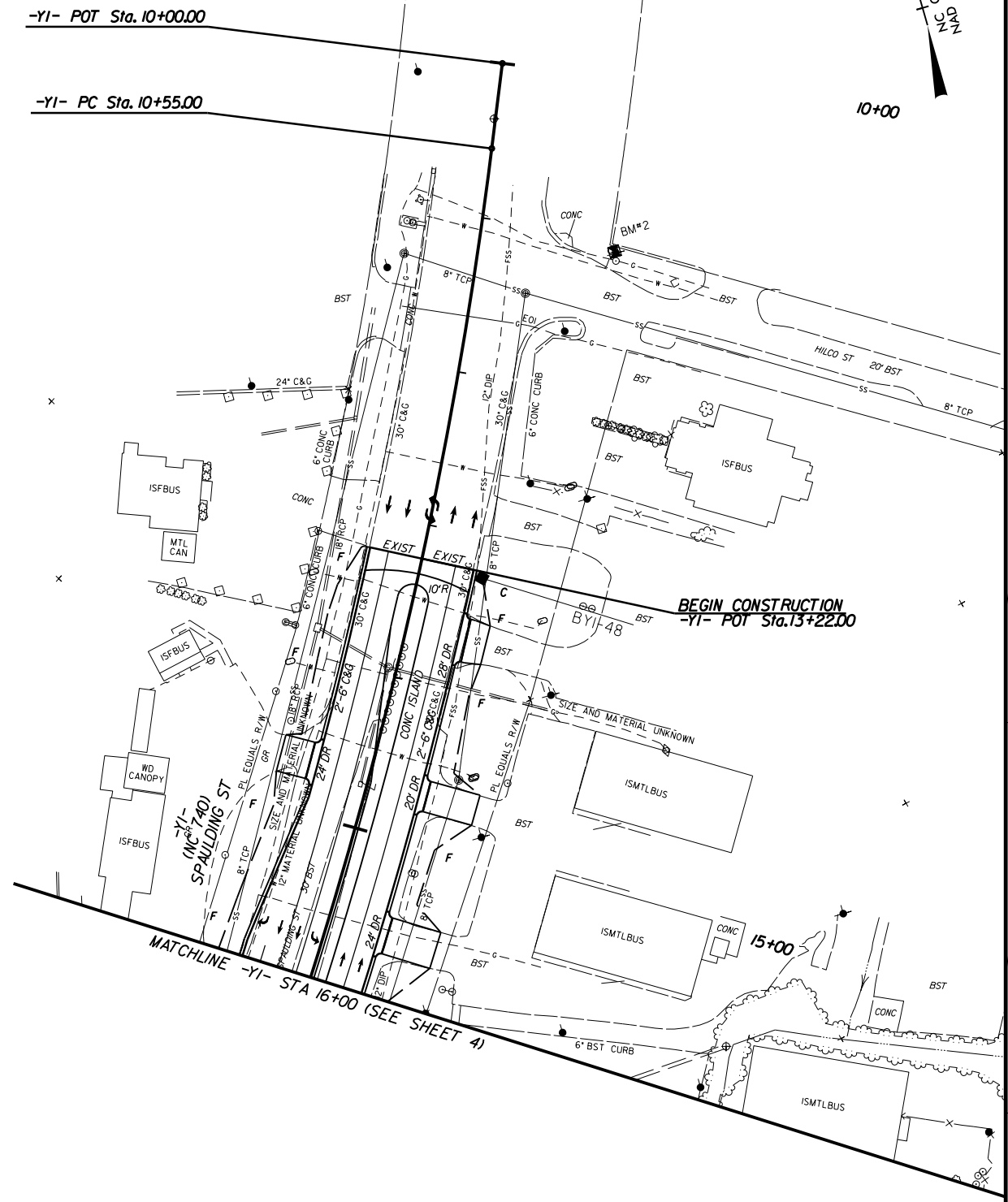
\$DATE\$

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-YI-
 PI Sta 14+21.57
 $\Delta = 13^{\circ} 55' 57.9''$ (RT)
 $D = 1^{\circ} 54' 35.5''$
 $L = 729.52'$
 $T = 366.57'$
 $R = 3,000.00'$
 $SE = 0.03$
 $RO = 138'$

PROJECT REFERENCE NO. R-2530B/B-4974		SHEET NO. 32	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
P.O. BOX 33068 • RALEIGH, N.C. 27636-3068			
RIGHT-OF-WAY REV.			
CONST. REV.			
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			

REVISIONS

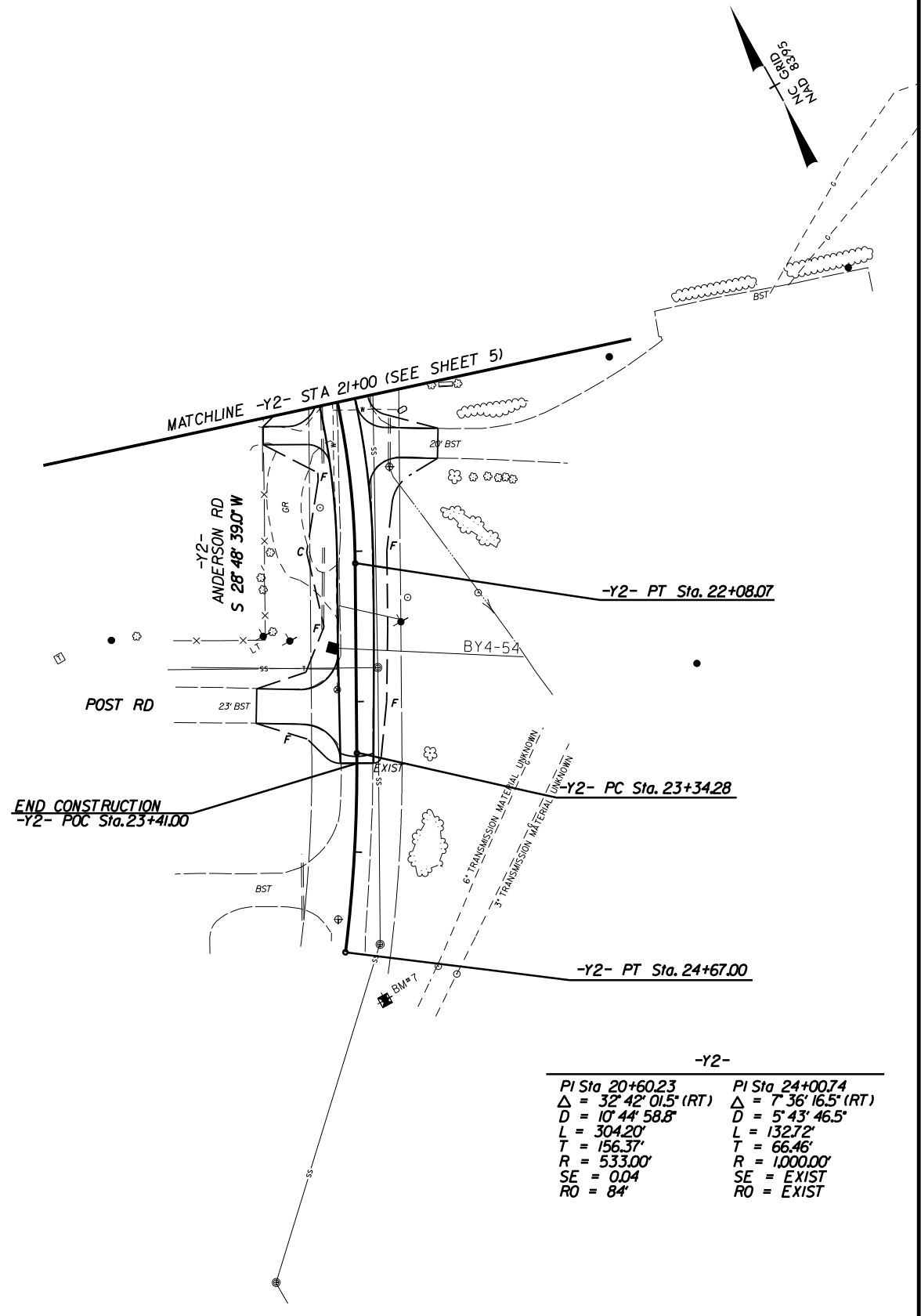


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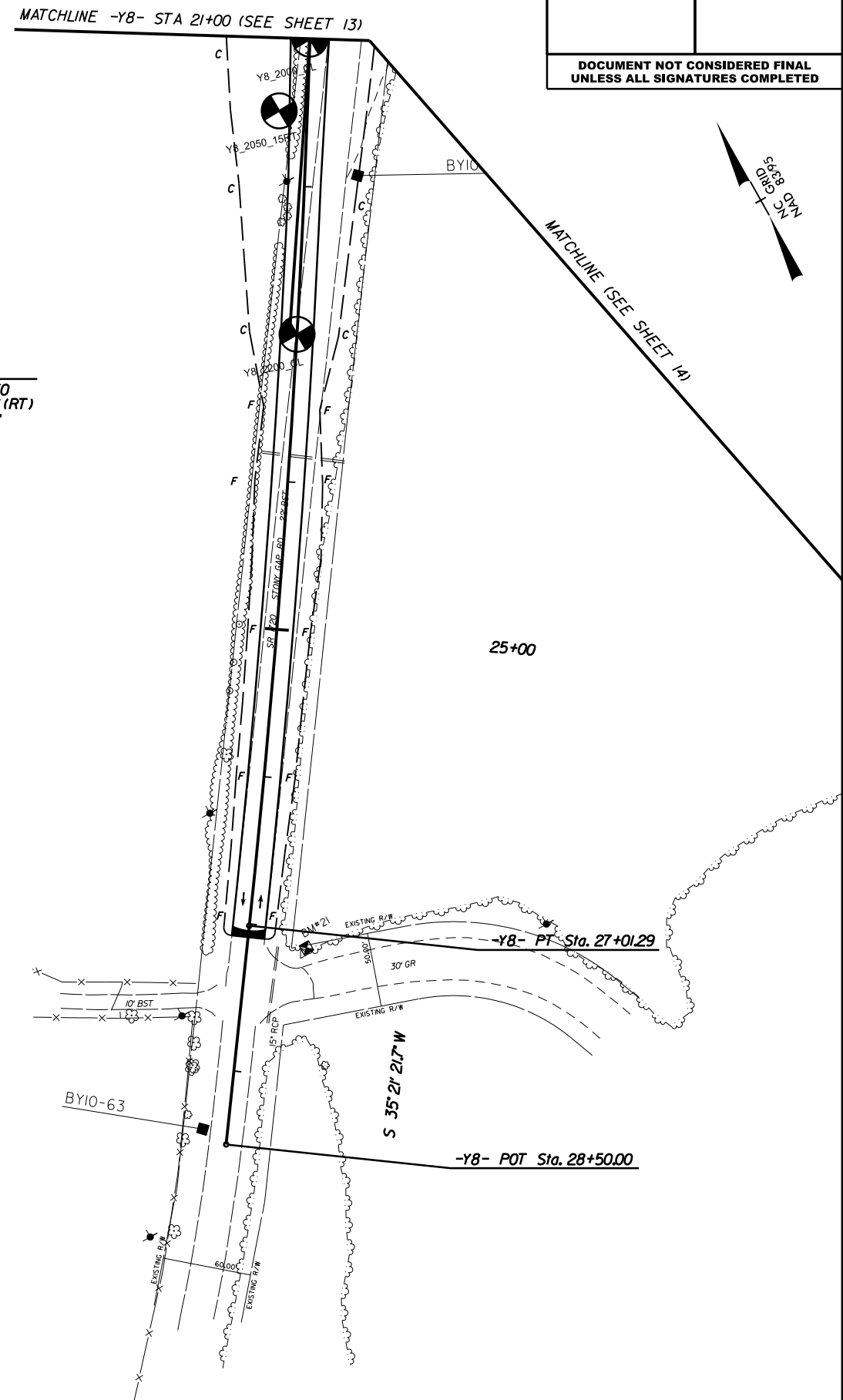
\$DATE\$

REVISIONS



-Y2-

PI Sta 20+60.23	PI Sta 24+00.74
$\Delta = 32^\circ 42' 01.5"$ (RT)	$\Delta = 7^\circ 36' 16.5"$ (RT)
$D = 10^\circ 44' 58.8"$	$D = 5^\circ 43' 46.5"$
$L = 304.20'$	$L = 132.72'$
$T = 156.37'$	$T = 66.46'$
$R = 533.00'$	$R = 1,000.00'$
$SE = 0.04$	$SE = EXIST$
$RO = 8'$	$RO = EXIST$



-Y8-

PI Sta 23+96.30
$\Delta = 4^\circ 17' 24.9"$ (RT)
$D = 0^\circ 42' 10.9"$
$L = 610.26'$
$T = 305.27'$
$R = 8,150.00'$
$SE = NC$
$RO = NONE$

Kimley»Horn

P.O. BOX 33068 • RALEIGH, N.C. 27636-3068

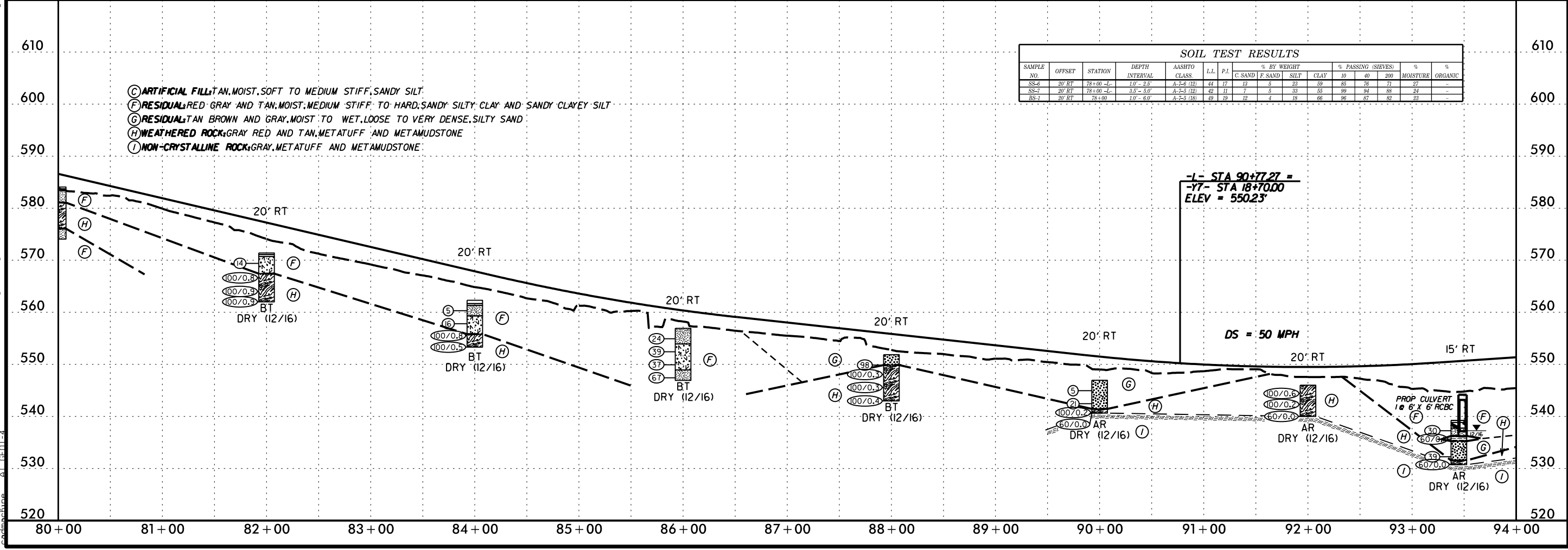
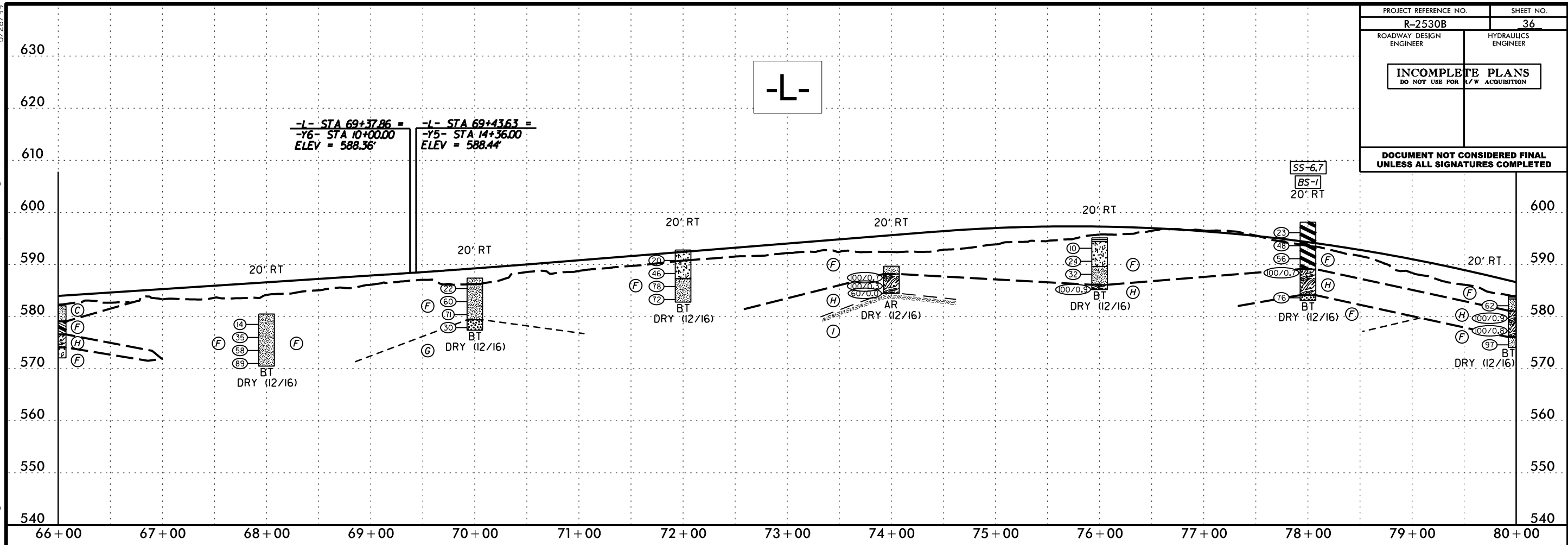
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ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

INCOMPLETE PLANS
DO NOT USE FOR R/W ACQUISITION

DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED

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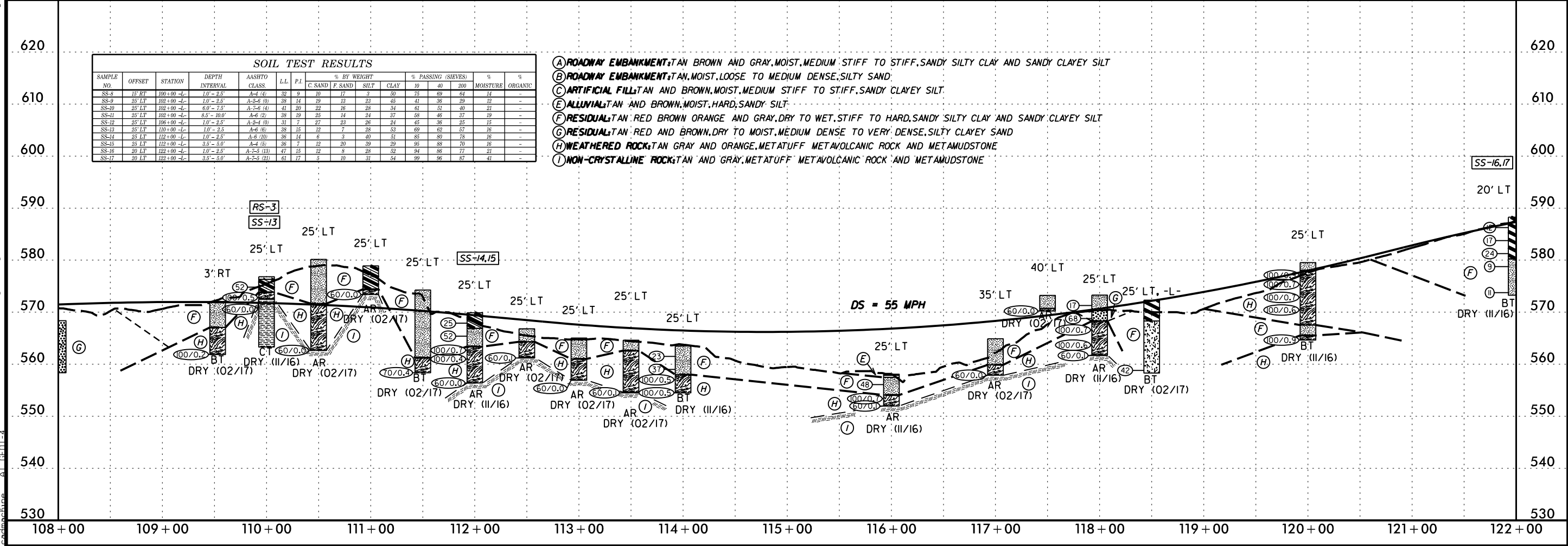
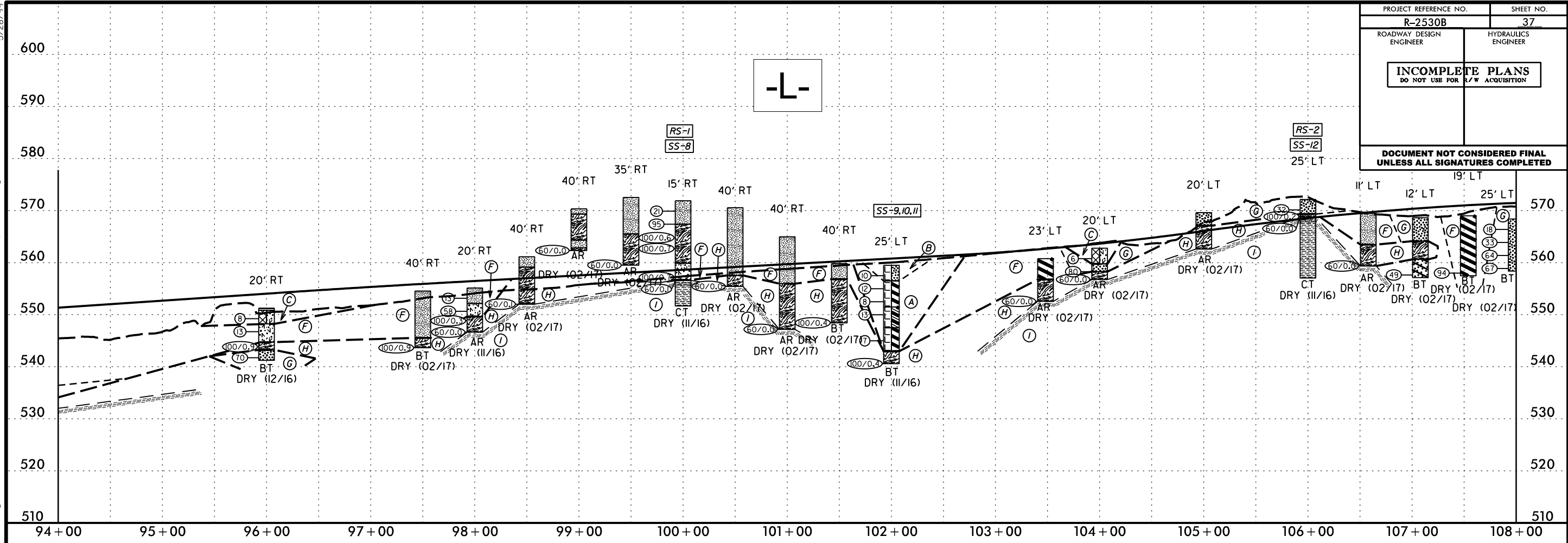
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ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



- (C) ARTIFICIAL FILL: TAN, MOIST, SOFT TO MEDIUM STIFF, SANDY SILT.
- (F) RESIDUAL: RED GRAY AND TAN, MOIST, MEDIUM STIFF TO HARD, SANDY SILTY CLAY AND SANDY CLAYEY SILT.
- (G) RESIDUAL: TAN BROWN AND GRAY, MOIST TO WET, LOOSE TO VERY DENSE, SILTY SAND.
- (H) WEATHERED ROCK: GRAY RED AND TAN, METATUFF AND METAMUDSTONE.
- (I) NON-CRYSTALLINE ROCK: GRAY, METATUFF AND METAMUDSTONE.

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	L.L.	P.L.	% BY WEIGHT			% PASSING (SIEVES)			MOISTURE	% ORGANIC	
							C SAND	F SAND	SILT	CLAY	10	40			200
SS-6	20 RT	78+00	1.0' - 2.5'	A-7-6 (12)	44	17	13	5	23	59	85	76	71	27	-
SS-7	20 RT	78+00	3.5' - 5.0'	A-7-6 (12)	42	11	7	5	33	55	99	84	88	24	-
BS-1	20 RT	78+00	1.0' - 6.0'	A-7-5 (18)	49	19	12	4	38	66	96	87	82	23	-

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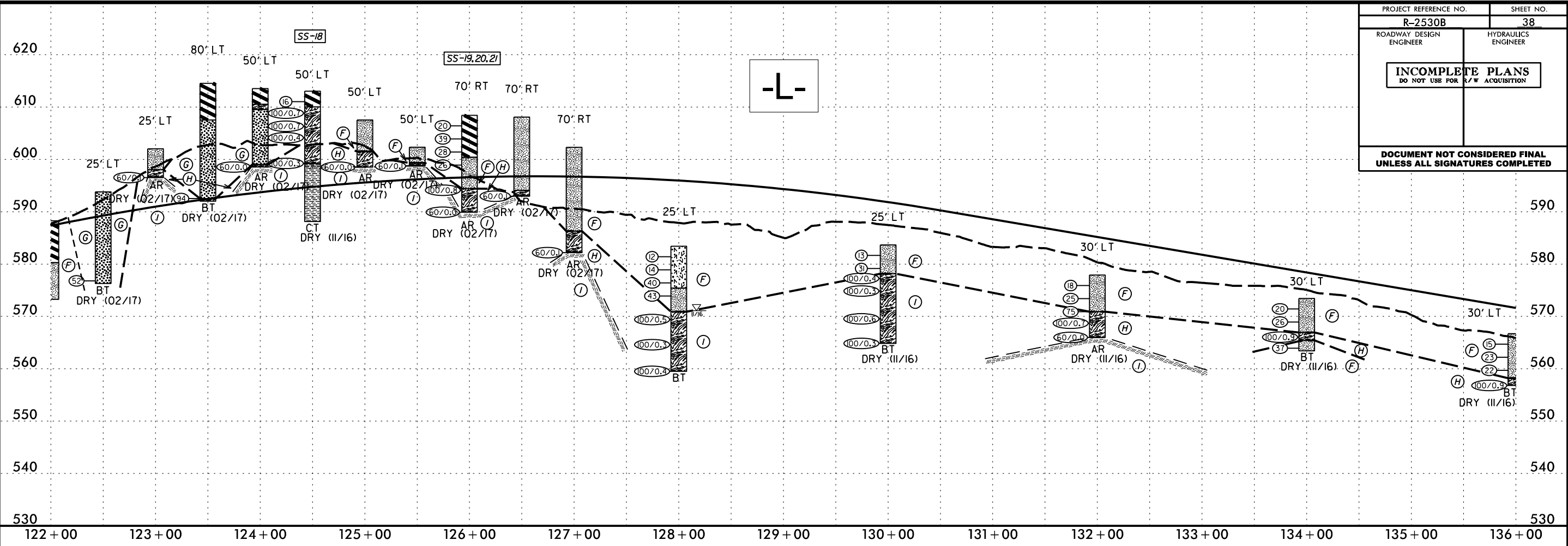


SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	PI	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-8	15 RT	100+00 -L-	1.0' - 2.5'	A-4 (4)	32	9	10	17	3	50	75	69	64	14	-
SS-9	25 LT	102+00 -L-	1.0' - 2.5'	A-2-5 (10)	38	14	29	10	22	45	41	36	29	12	-
SS-10	25 LT	102+00 -L-	6.0' - 7.5'	A-2-5 (4)	41	20	22	18	28	34	61	51	40	21	-
SS-11	25 LT	102+00 -L-	8.5' - 10.0'	A-6 (2)	38	19	25	14	24	37	58	46	37	19	-
SS-12	25 LT	106+00 -L-	1.0' - 2.5'	A-2-4 (0)	31	7	27	23	26	24	45	36	25	15	-
SS-13	25 LT	110+00 -L-	1.0' - 2.5'	A-6 (6)	38	15	12	7	28	53	69	62	57	16	-
SS-14	25 LT	112+00 -L-	1.0' - 2.5'	A-6 (10)	36	14	8	3	40	51	85	89	78	16	-
SS-15	25 LT	112+00 -L-	3.5' - 5.0'	A-4 (5)	36	7	12	20	39	39	85	88	79	16	-
SS-16	20 LT	122+00 -L-	1.0' - 2.5'	A-2-5 (13)	47	15	12	8	28	52	94	88	77	21	-
SS-17	20 LT	122+00 -L-	3.5' - 5.0'	A-2-5 (21)	61	17	5	10	31	54	99	96	87	41	-

- (A) ROADWAY EMBANKMENT: TAN BROWN AND GRAY, MOIST, MEDIUM STIFF TO STIFF, SANDY SILTY CLAY AND SANDY CLAYEY SILT
- (B) ROADWAY EMBANKMENT: TAN, MOIST, LOOSE TO MEDIUM DENSE, SILTY SAND
- (C) ARTIFICIAL FILL: TAN AND BROWN, MOIST, MEDIUM STIFF TO STIFF, SANDY CLAYEY SILT
- (E) ALLUVIAL: TAN AND BROWN, MOIST, HARD, SANDY SILT
- (F) RESIDUAL: TAN, RED BROWN ORANGE AND GRAY, DRY TO WET, STIFF TO HARD, SANDY SILTY CLAY AND SANDY CLAYEY SILT
- (G) RESIDUAL: TAN, RED AND BROWN, DRY TO MOIST, MEDIUM DENSE TO VERY DENSE, SILTY CLAYEY SAND
- (H) WEATHERED ROCK: TAN GRAY AND ORANGE, METATUFF, METAVOLCANIC ROCK AND METAMUDSTONE
- (I) NON-CRYSTALLINE ROCK: TAN AND GRAY, METATUFF, METAVOLCANIC ROCK AND METAMUDSTONE

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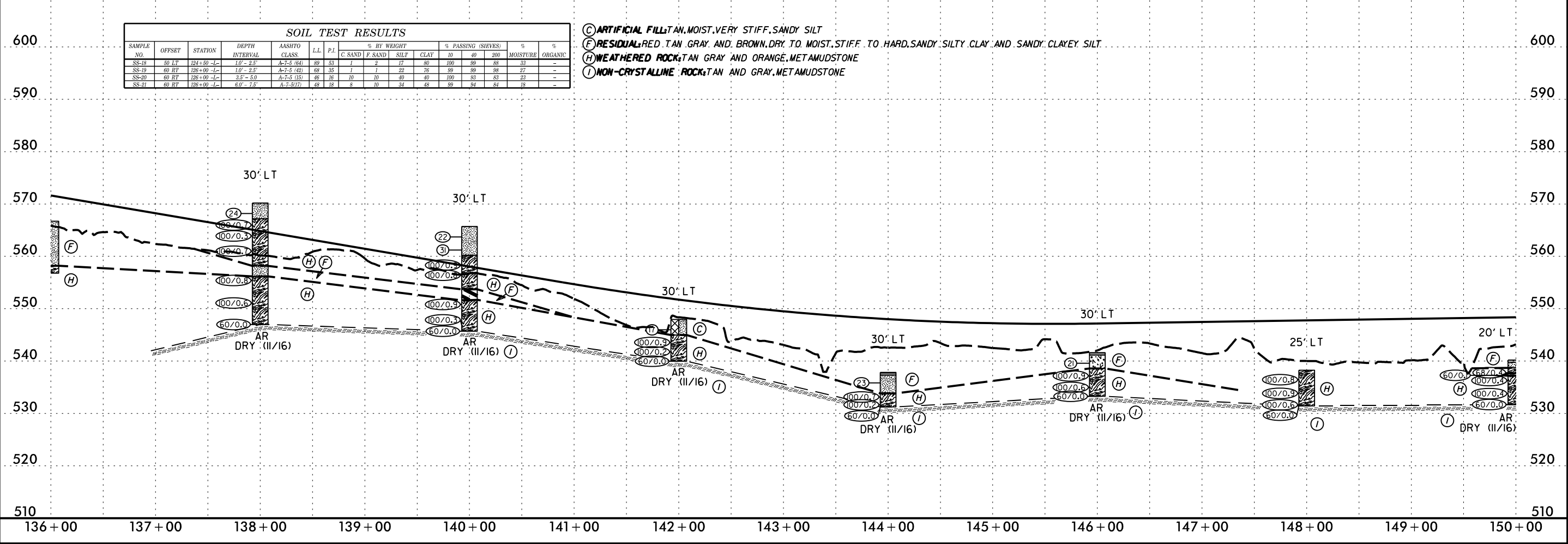
PROJECT REFERENCE NO.	SHEET NO.
R-2530B	38
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS	
DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL	
UNLESS ALL SIGNATURES COMPLETED	

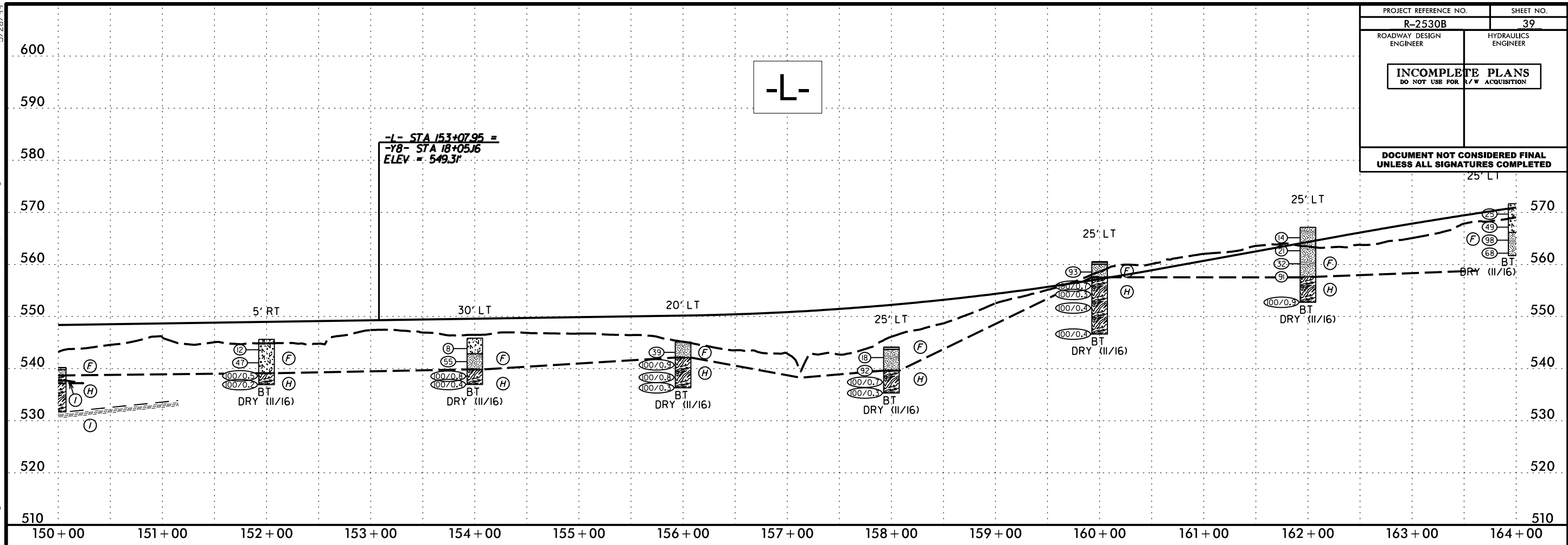


SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)		% MOISTURE ORGANIC		
							C. SAND	F. SAND	SILT	CLAY	10	200			
SS-18	50' LT	124+00	1.0' - 2.5'	A-7.5 (64)	89	13	1	2	17	80	100	59	88	23	-
SS-19	60' RT	126+00	1.0' - 2.5'	A-7.5 (42)	68	35	1	1	22	76	99	99	58	27	-
SS-20	80' RT	128+00	3.5' - 5.0'	A-7.5 (15)	46	16	10	10	40	100	83	83	23	-	
SS-21	80' RT	128+00	6.0' - 7.5'	A-7.5 (17)	48	18	8	10	34	68	99	94	84	18	-

- (C) ARTIFICIAL FILL, TAN, MOIST, VERY STIFF, SANDY SILT
- (F) RESIDUAL, RED, TAN, GRAY AND BROWN, DRY TO MOIST, STIFF TO HARD, SANDY, SILTY CLAY AND SANDY, CLAYEY SILT
- (H) WEATHERED ROCK, TAN, GRAY AND ORANGE, METAMUDSTONE
- (I) NON-CRYSTALLINE ROCK, TAN AND GRAY, METAMUDSTONE

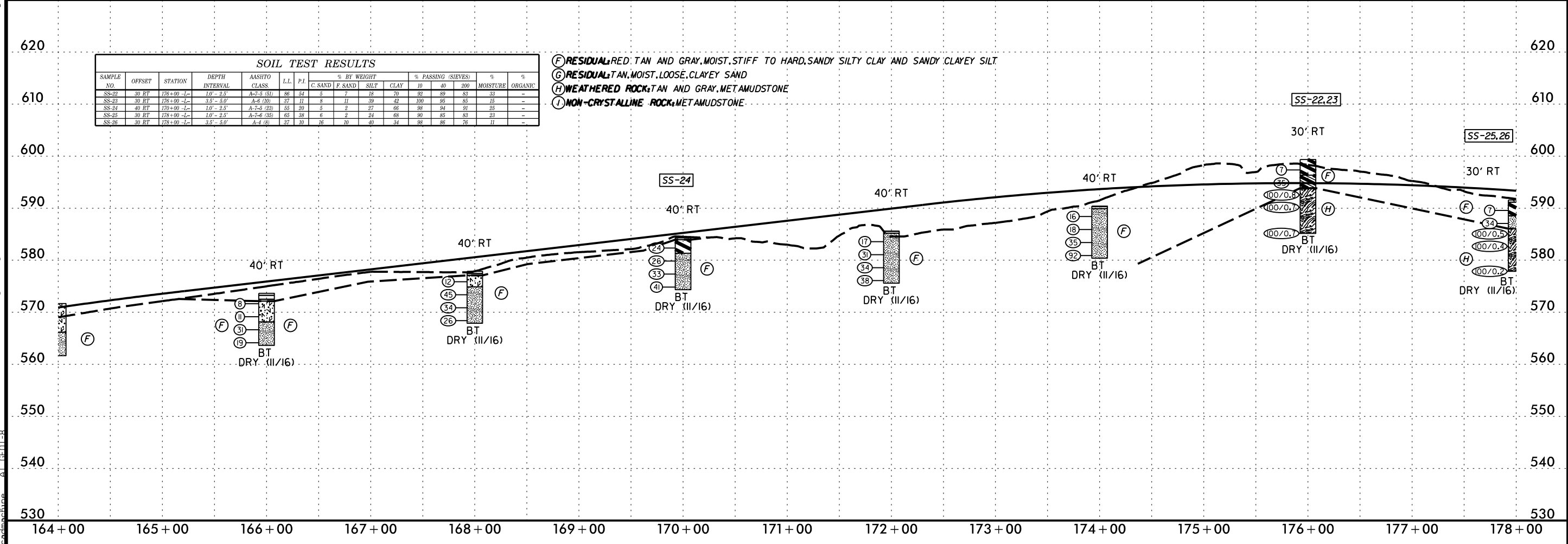




SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE ORGANIC	
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-22	30 RT	176+00	10' - 2.5'	A-7.5 (SI)	86	54	5	7	18	70	92	88	83	33	-
SS-23	30 RT	176+00	3.5' - 5.0'	A-6 (IO)	37	11	8	11	39	42	100	85	85	15	-
SS-24	40 RT	170+00	10' - 2.5'	A-7.5 (SI)	55	30	5	2	27	65	98	94	91	25	-
SS-25	30 RT	178+00	10' - 2.5'	A-7.6 (SI)	65	38	6	2	24	68	90	85	83	23	-
SS-26	30 RT	178+00	3.5' - 5.0'	A-4 (S)	37	10	16	10	40	34	98	86	76	11	-

- (F) RESIDUAL RED, TAN AND GRAY, MOIST, STIFF TO HARD, SANDY SILTY CLAY AND SANDY CLAYEY SILT
- (G) RESIDUAL TAN, MOIST, LOOSE, CLAYEY SAND
- (H) WEATHERED ROCK, TAN AND GRAY, METAMUDSTONE
- (I) NON-CRYSTALLINE ROCK, METAMUDSTONE

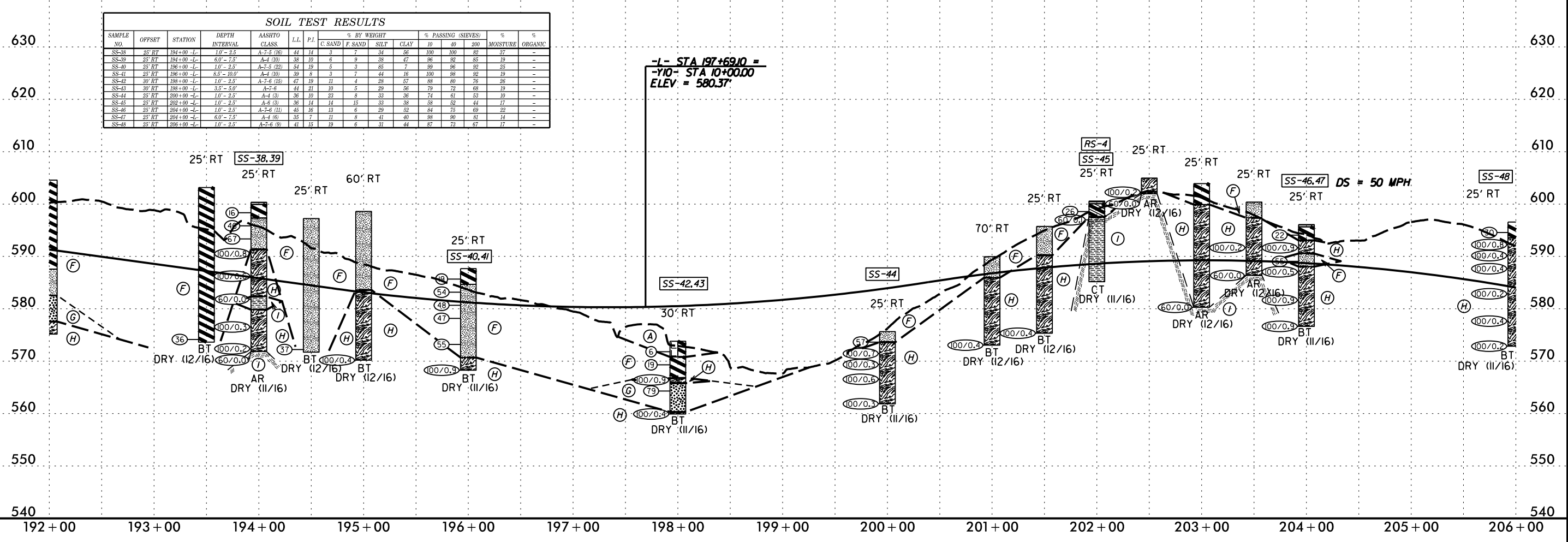
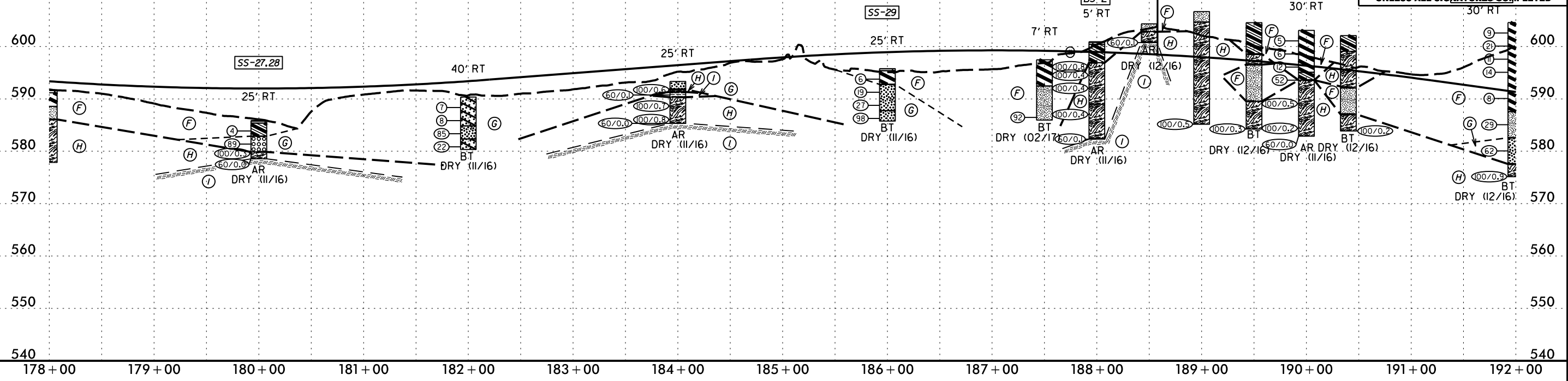


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SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)		%	%	
							C. SAND	F. SAND	SILT	CLAY	10	40	200	MOISTURE	ORGANIC
SS-27	25 RT	180+00	1.0' - 2.5'	A-4 (11)	34	11	2	3	45	50	89	97	94	25	-
SS-28	25 RT	180+00	3.5' - 5.0'	A-1-2 (10)	27	6	46	9	39	25	88	93	88	4	-
SS-29	25 RT	186+00	1.0' - 2.5'	A-7-6 (34)	56	36	5	9	32	54	88	85	88	22	-
SS-30	60 RT	120+00	2.5' - 3.0'	A-7-6 (31)	54	30	3	4	36	57	88	86	82	20	-
SS-31	5 RT	188+00	1.0' - 2.5'	A-6 (18)	40	12	9	19	35	37	91	86	71	19	-
SS-32	30 RT	180+00	1.0' - 2.5'	A-7-5 (15)	83	23	3	4	59	34	99	97	83	34	-
SS-33	30 RT	180+00	6.0' - 7.5'	A-7-5 (11)	49	20	18	24	30	25	88	88	62	28	-
SS-34	30 RT	180+00	8.5' - 10.0'	A-6 (3)	37	12	26	28	24	22	89	74	46	20	-
SS-35	30 RT	182+00	1.0' - 2.5'	A-7-5 (45)	82	40	2	11	18	69	100	99	90	40	-
SS-36	30 RT	182+00	6.0' - 7.5'	A-7-5 (11)	63	19	3	18	40	40	100	99	86	-	-
SS-37	30 RT	182+00	13.5' - 15.0'	A-7-5 (11)	44	11	1	26	47	26	100	100	82	37	-
BS-2	5 RT	188+00	1.0' - 13.0'	A-5 (2)	30	11	27	19	24	30	75	60	45	6	-

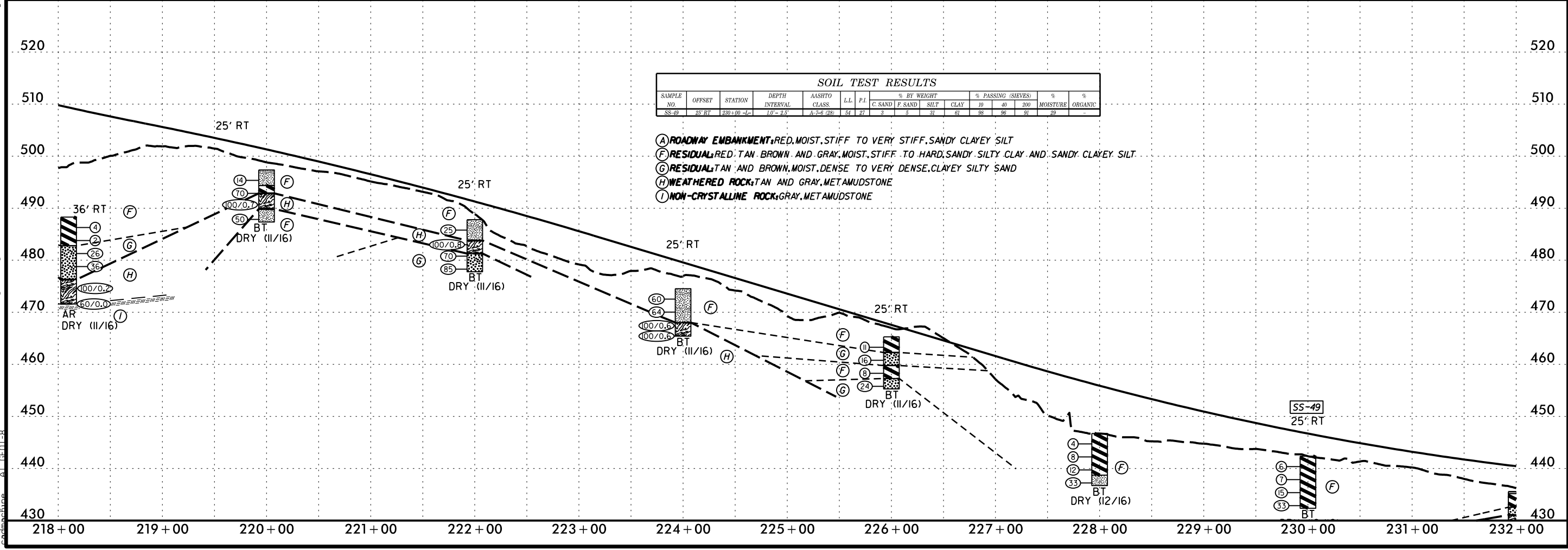
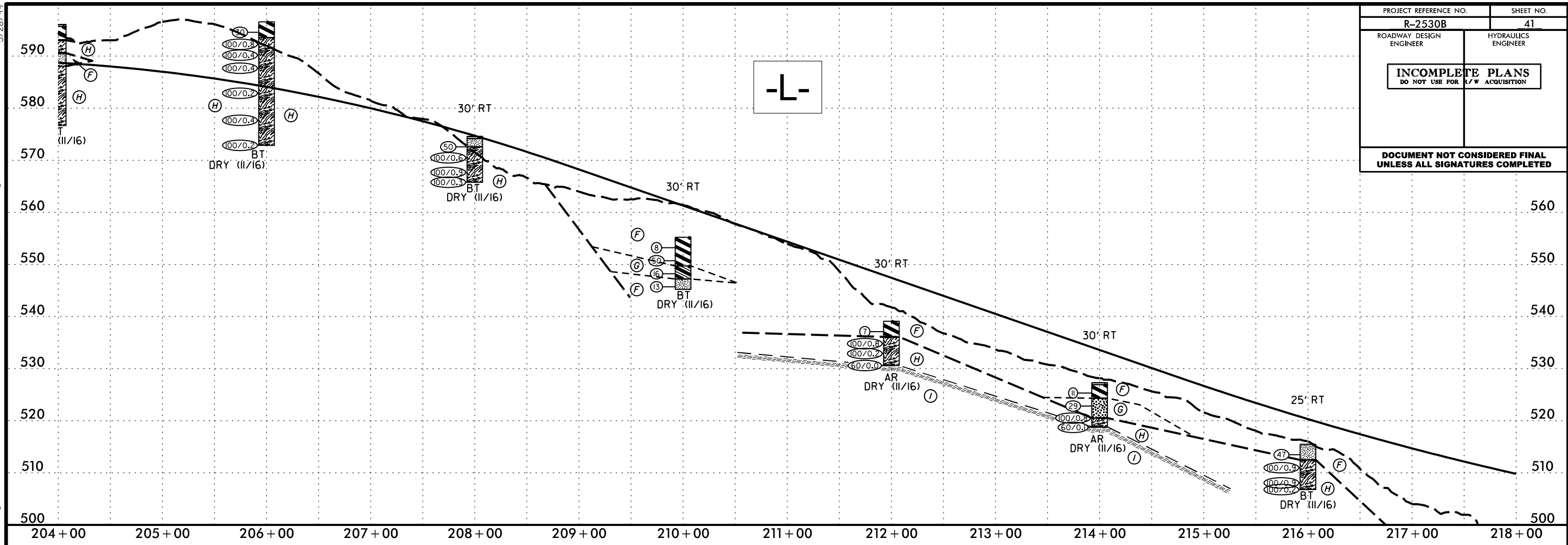
- (A) ROADWAY EMBANKMENT: TAN, MOIST, MEDIUM STIFF, SANDY SILTY CLAY
- (F) RESIDUAL: RED TAN AND GRAY, MOIST, SOFT TO HARD, SANDY SILTY CLAY AND SANDY CLAYEY SILT
- (G) RESIDUAL: TAN AND BROWN, MOIST, LOOSE TO VERY DENSE, SILTY CLAYEY SAND
- (H) WEATHERED ROCK: TAN AND GRAY, METAMUDSTONE AND METASANDSTONE
- (I) NON-CRYSTALLINE ROCK: TAN AND GRAY, METAMUDSTONE AND METASANDSTONE

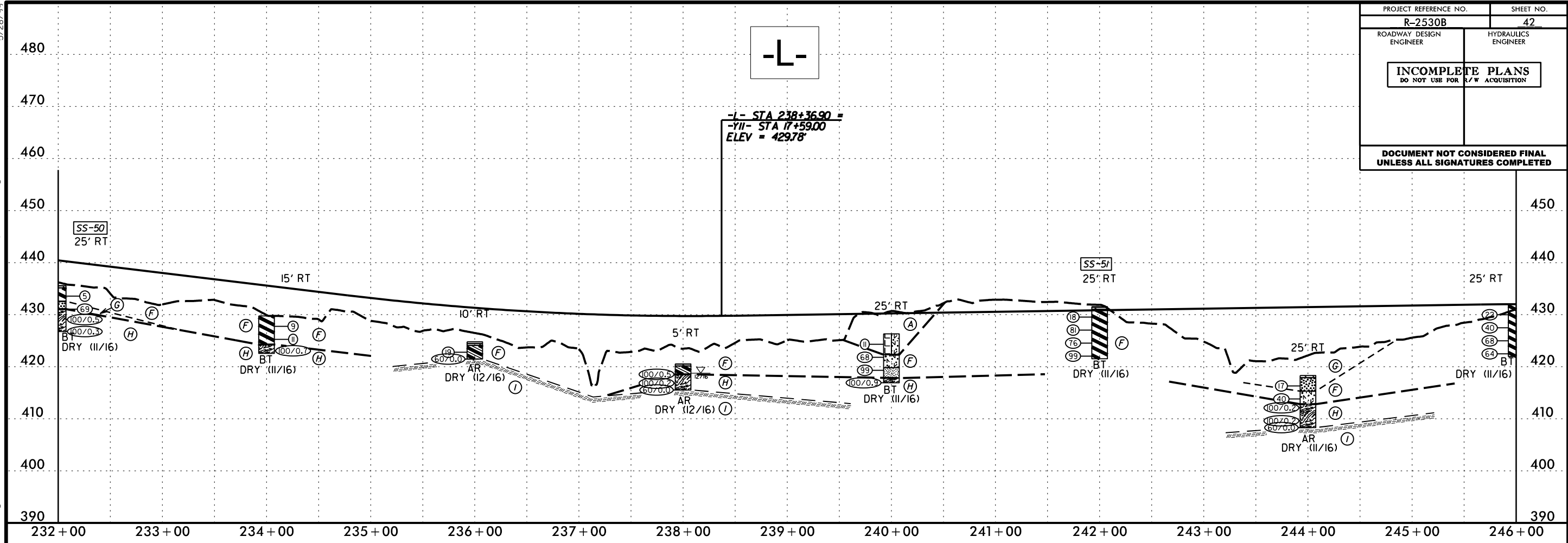


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INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	630
620	610
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

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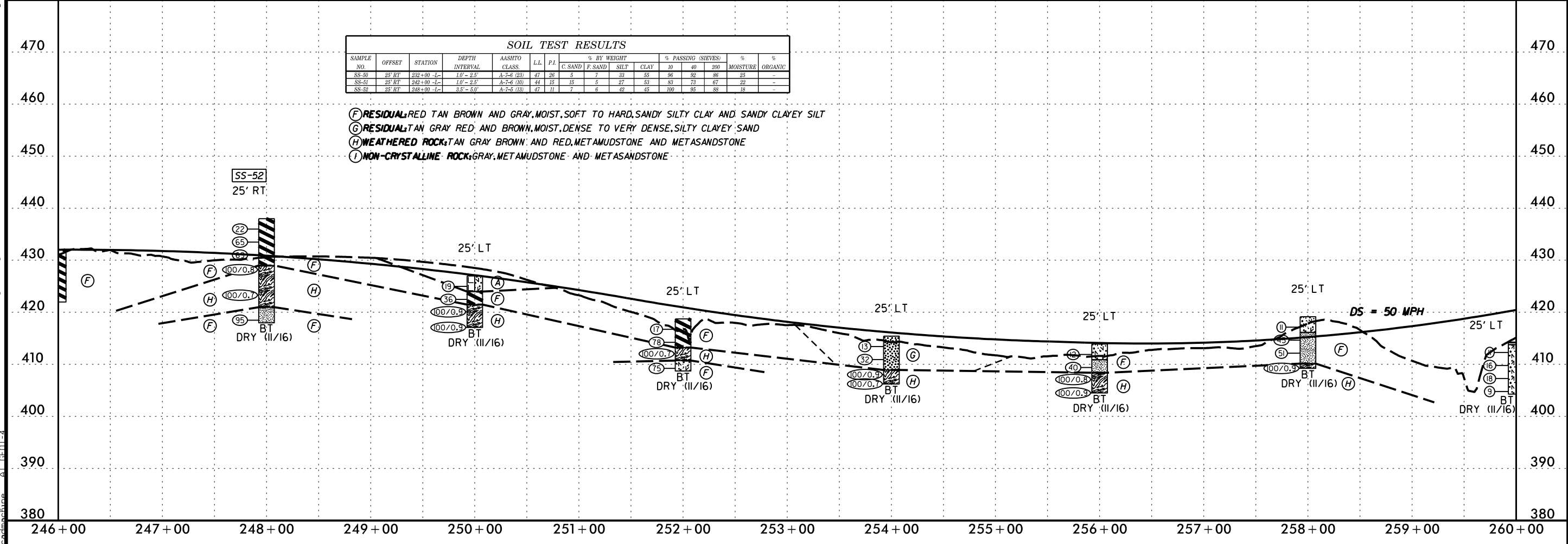
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ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	





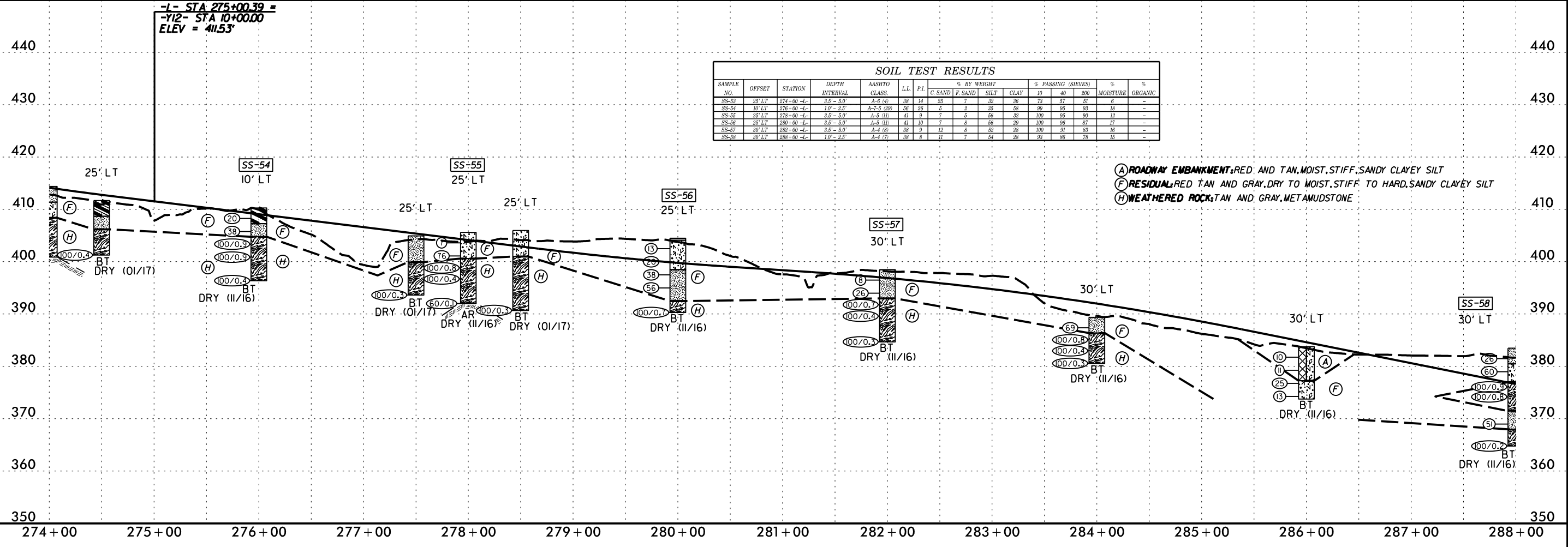
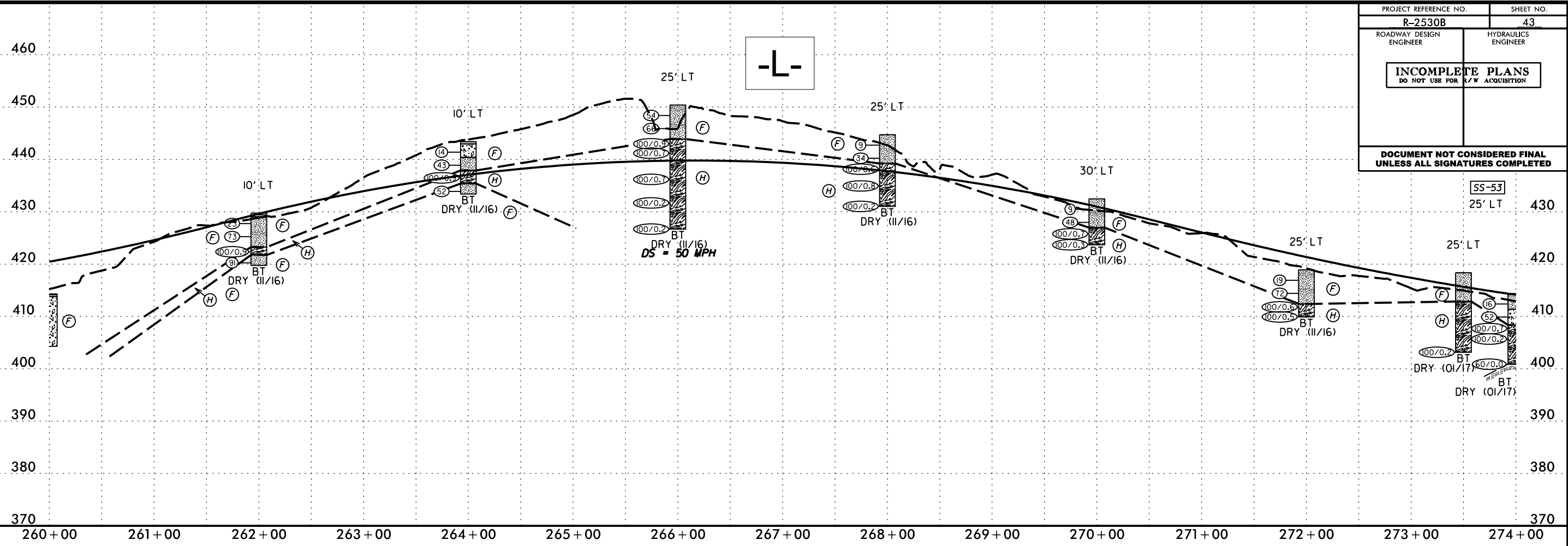
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	PI	% BY WEIGHT				% PASSING (SIEVES)			MOISTURE	ORGANIC
							C SAND	F SAND	SILT	CLAY	10	40	200		
SS-50	25' RT	232+00 -1-	1.0' - 2.5'	A-7-6 (23)	47	26	5	7	33	55	96	92	86	25	-
SS-51	25' RT	242+00 -1-	1.0' - 2.5'	A-7-6 (30)	44	15	5	27	33	83	75	67	22	-	
SS-52	25' RT	242+00 -1-	3.5' - 5.0'	A-7-6 (31)	47	11	7	8	42	100	95	88	16	-	

- (F) RESIDUAL: RED TAN BROWN AND GRAY, MOIST, SOFT TO HARD, SANDY SILTY CLAY AND SANDY CLAYEY SILT
- (G) RESIDUAL: TAN GRAY RED AND BROWN, MOIST, DENSE TO VERY DENSE, SILTY CLAYEY SAND
- (H) WEATHERED ROCK: TAN GRAY BROWN AND RED, METAMUDSTONE AND METASANDSTONE
- (I) NON-CRYSTALLINE ROCK: GRAY, METAMUDSTONE AND METASANDSTONE

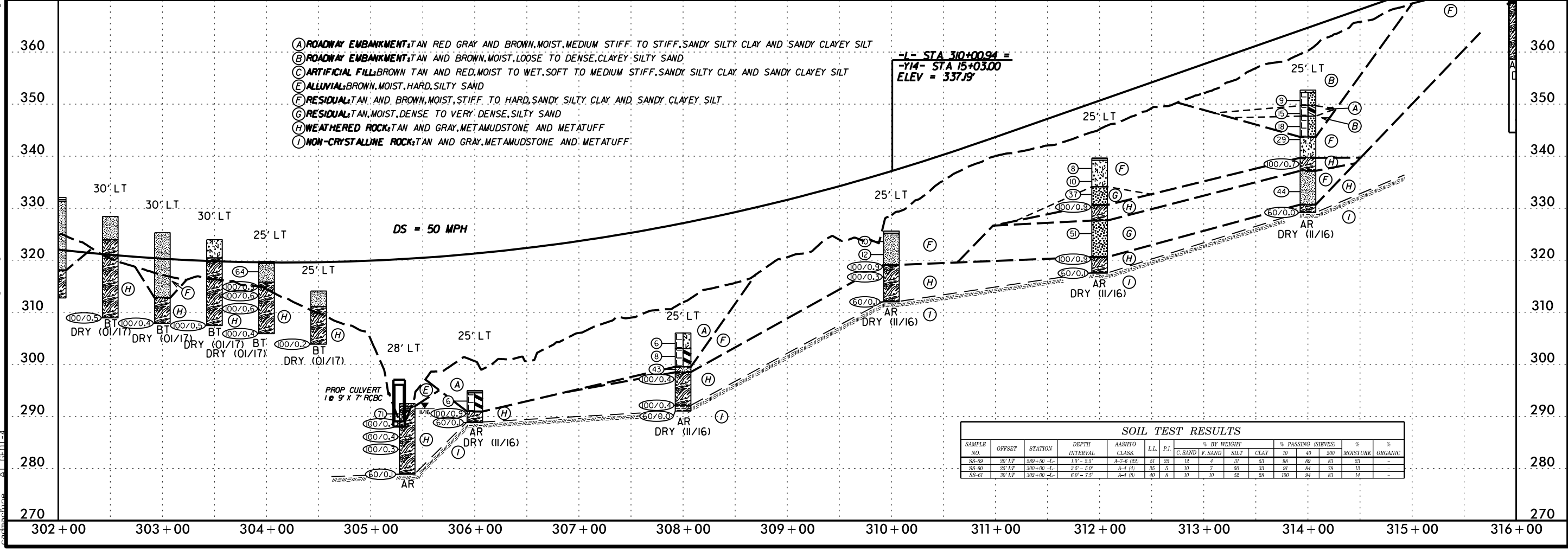
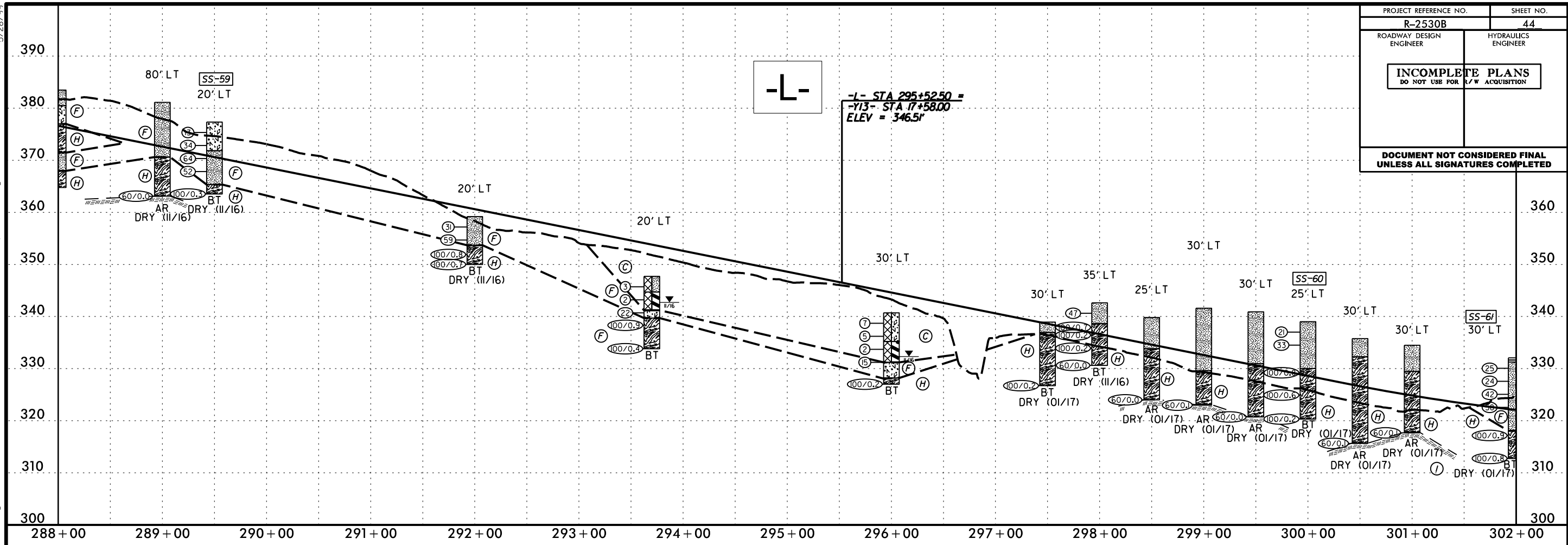


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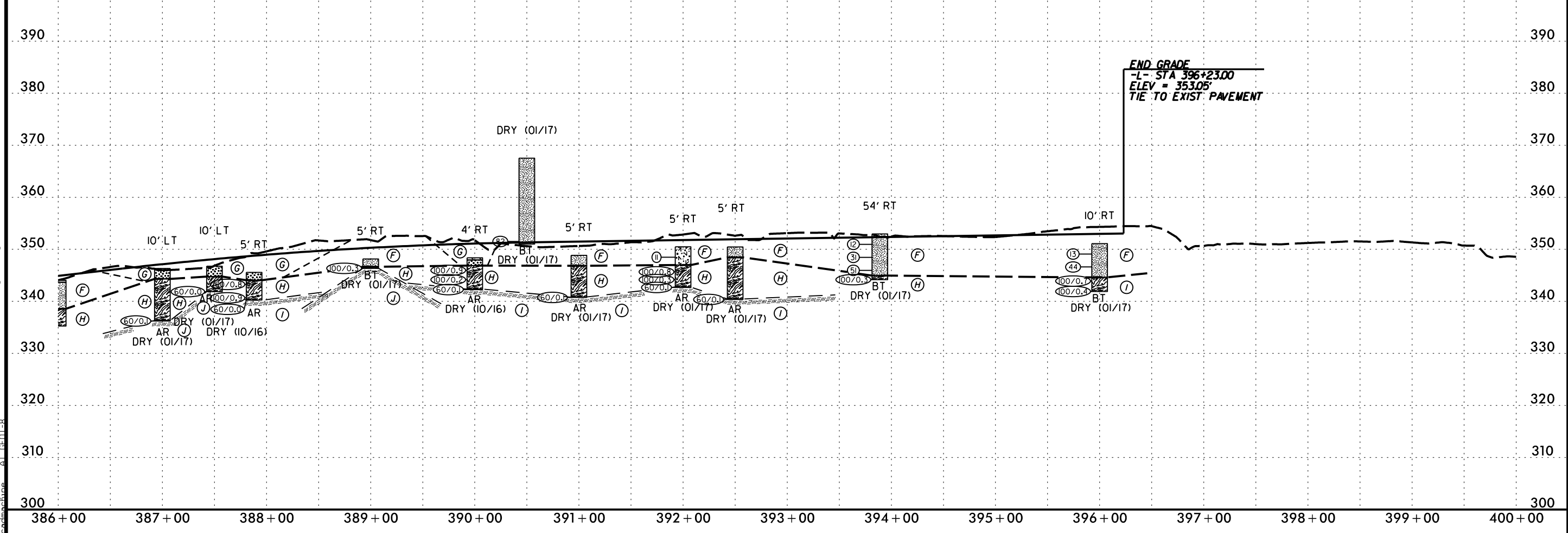
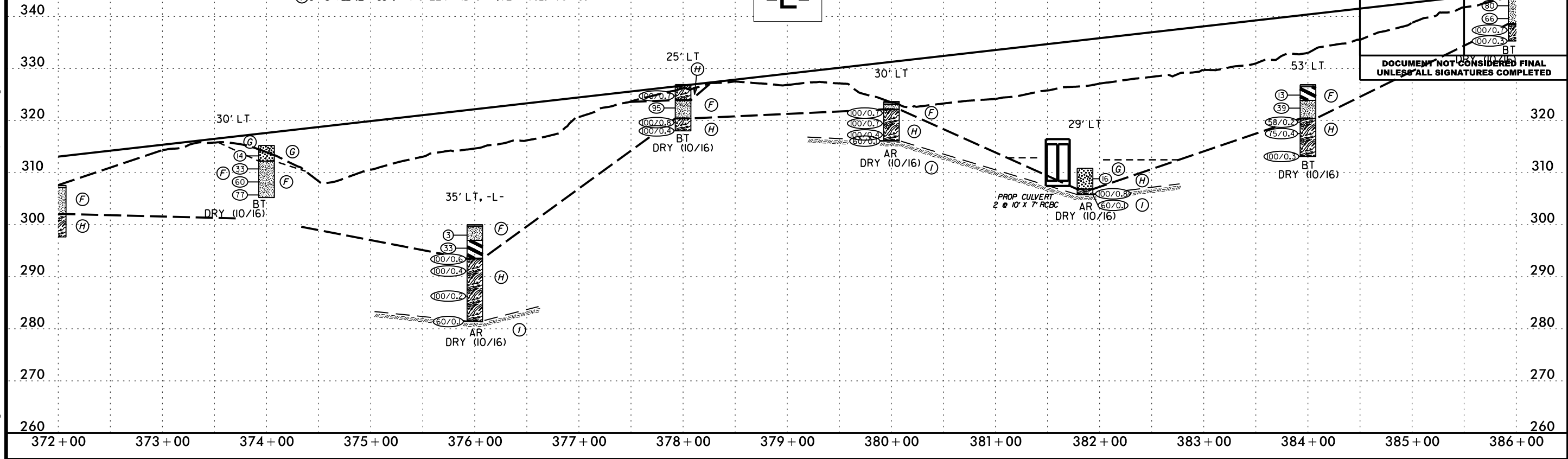
- (A) ROADWAY EMBANKMENT: TAN RED GRAY AND BROWN, MOIST, MEDIUM STIFF TO STIFF, SANDY SILTY CLAY AND SANDY CLAYEY SILT
- (B) ROADWAY EMBANKMENT: TAN AND BROWN, MOIST, LOOSE TO DENSE, CLAYEY SILTY SAND
- (C) ARTIFICIAL FILL: BROWN TAN AND RED, MOIST TO WET, SOFT TO MEDIUM STIFF, SANDY SILTY CLAY AND SANDY CLAYEY SILT
- (E) ALLUVIAL: BROWN, MOIST, HARD, SILTY SAND
- (F) RESIDUAL: TAN AND BROWN, MOIST, STIFF TO HARD, SANDY SILTY CLAY AND SANDY CLAYEY SILT
- (G) RESIDUAL: TAN, MOIST, DENSE TO VERY DENSE, SILTY SAND
- (H) WEATHERED ROCK: TAN AND GRAY, METAMUDSTONE AND METATUFF
- (I) NON-CRYSTALLINE ROCK: TAN AND GRAY, METAMUDSTONE AND METATUFF

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F SAND	SILT	CLAY	10	40	200		
SS-59	30' LT	289+00 -L-	1.0' - 2.5'	A-7-6 (22)	31	36	12	4	31	53	98	89	83	23	-
SS-60	25' LT	300+00 -L-	3.5' - 5.0'	A-1 (4)	35	5	10	7	50	33	91	84	78	13	-
SS-61	30' LT	302+00 -L-	6.0' - 7.5'	A-1 (8)	40	8	10	10	52	28	100	94	83	14	-

5/28/99
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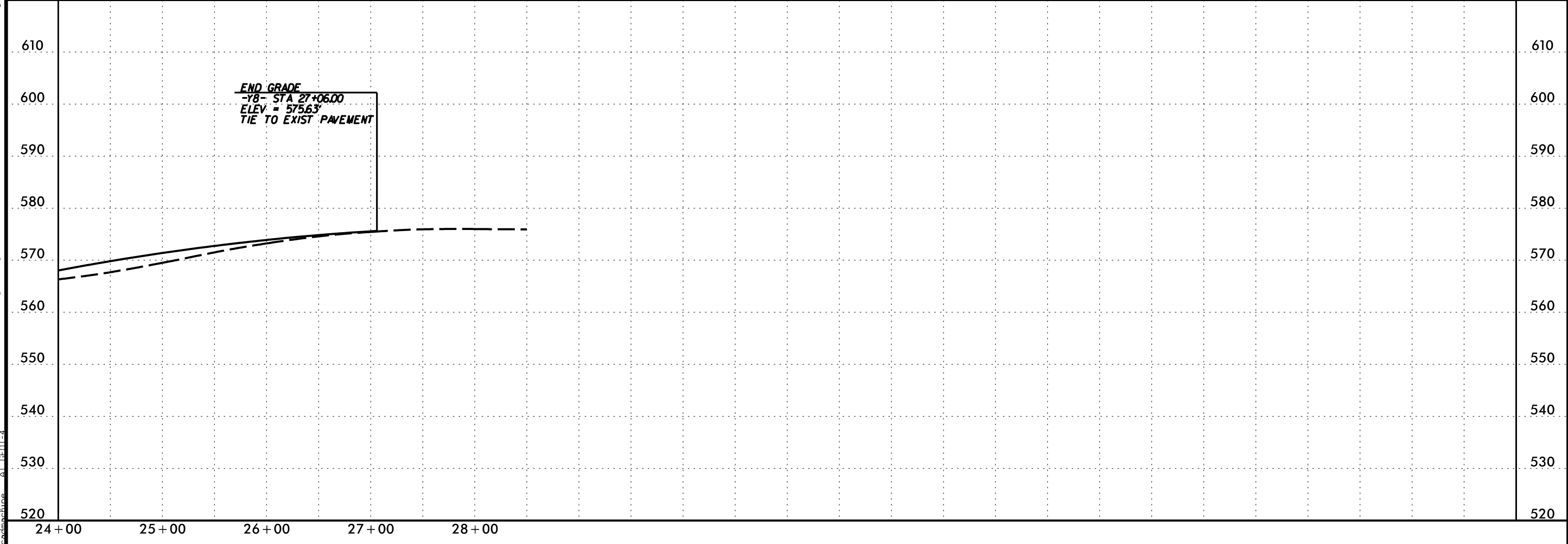
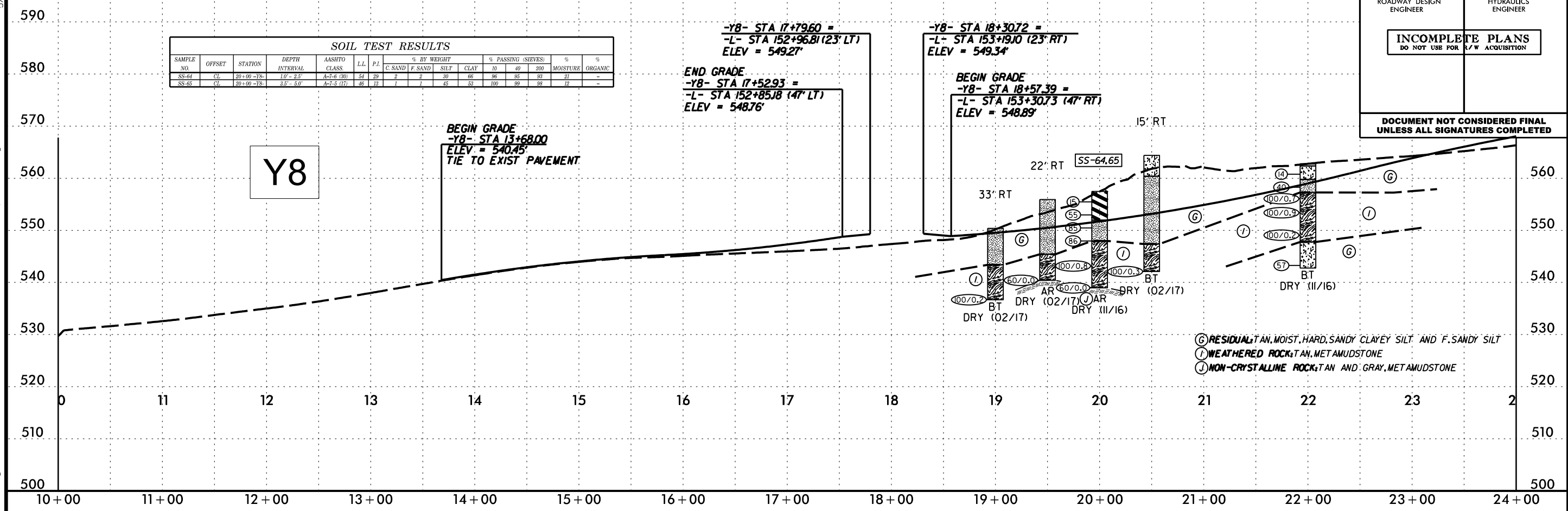
- (F) RESIDUAL RED TAN AND BROWN, DRY TO WET, SOFT TO HARD, SANDY SILTY CLAY AND SANDY SILT
- (G) RESIDUAL RED BROWN AND TAN, MOIST, MEDIUM DENSE, CLAYEY SAND AND SILTY SAND
- (H) WEATHERED ROCK, TAN GRAY AND BROWN, METAMUDSTONE
- (I) NON-CRYSTALLINE ROCK, TAN AND GRAY, METAMUDSTONE
- (J) CRYSTALLINE ROCK, TAN GREEN AND GRAY, META-VOLCANIC ROCK

PROJECT REFERENCE NO. R-2530B	SHEET NO. 47
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

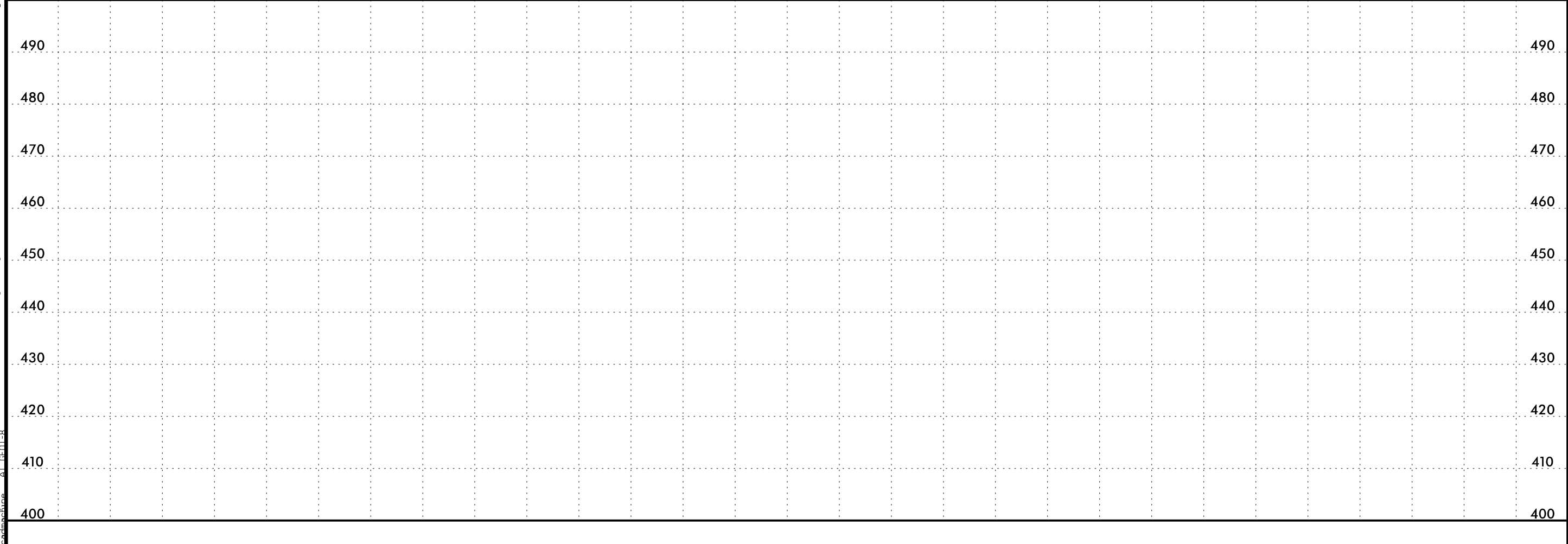
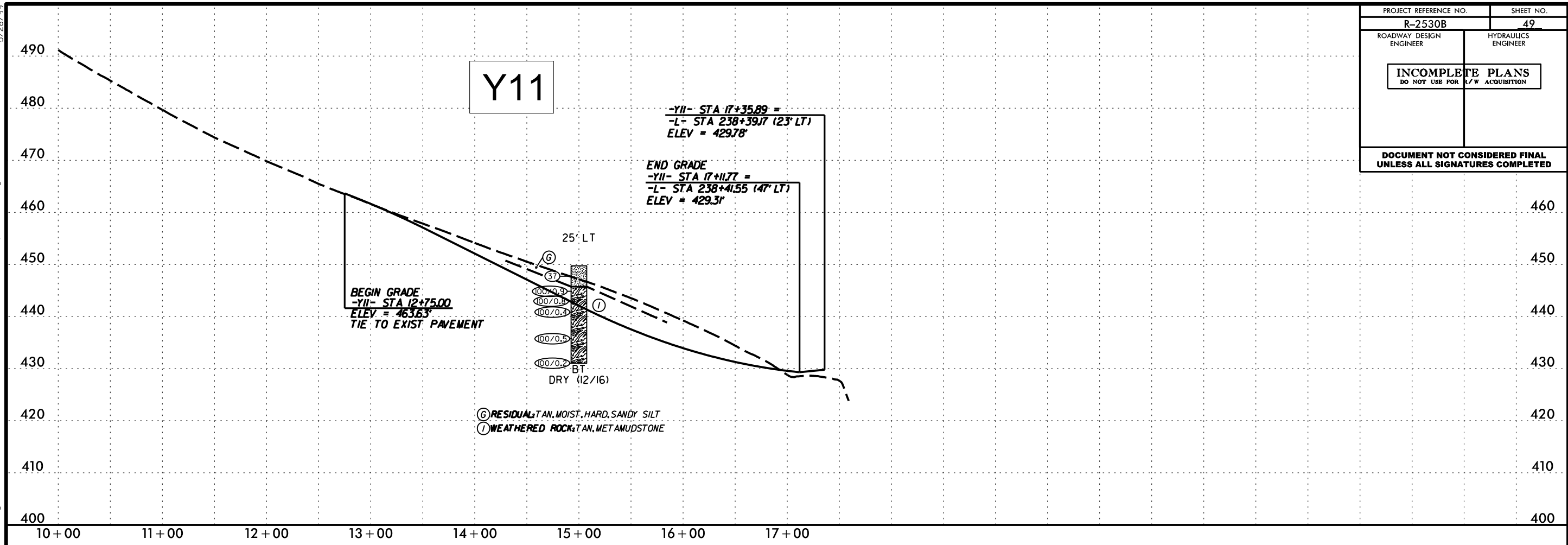


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PROJECT REFERENCE NO. R-2530B	SHEET NO. 48
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



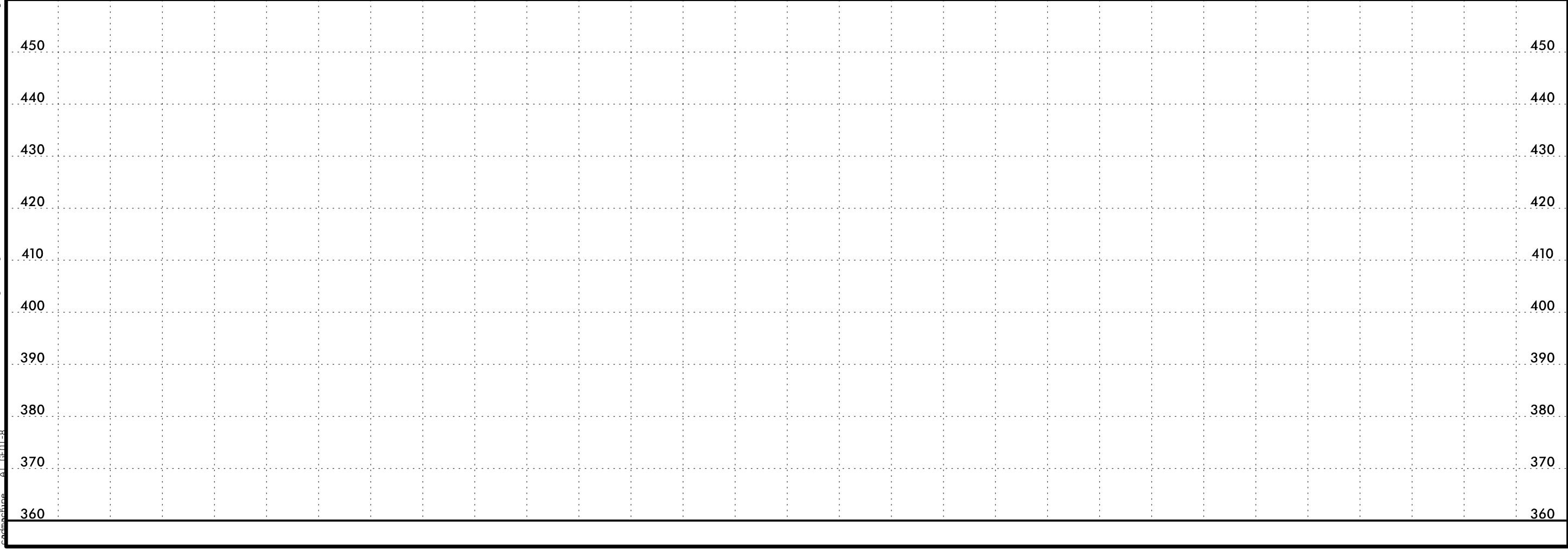
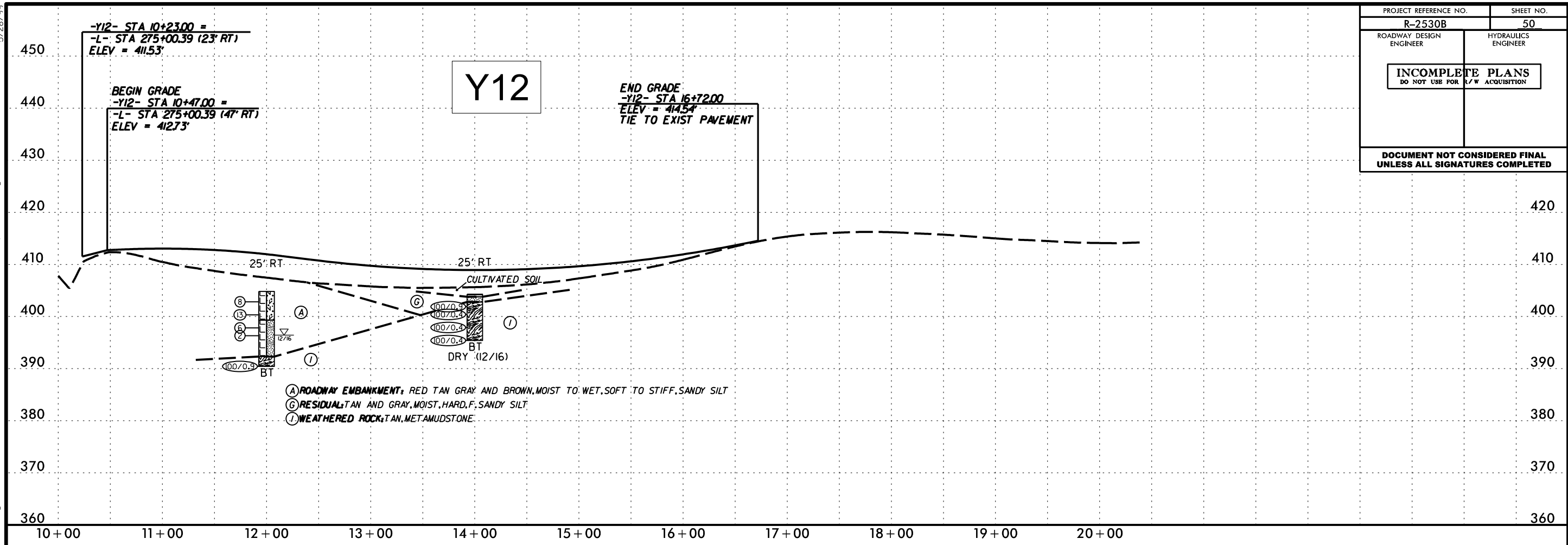
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R-2530B	49
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DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



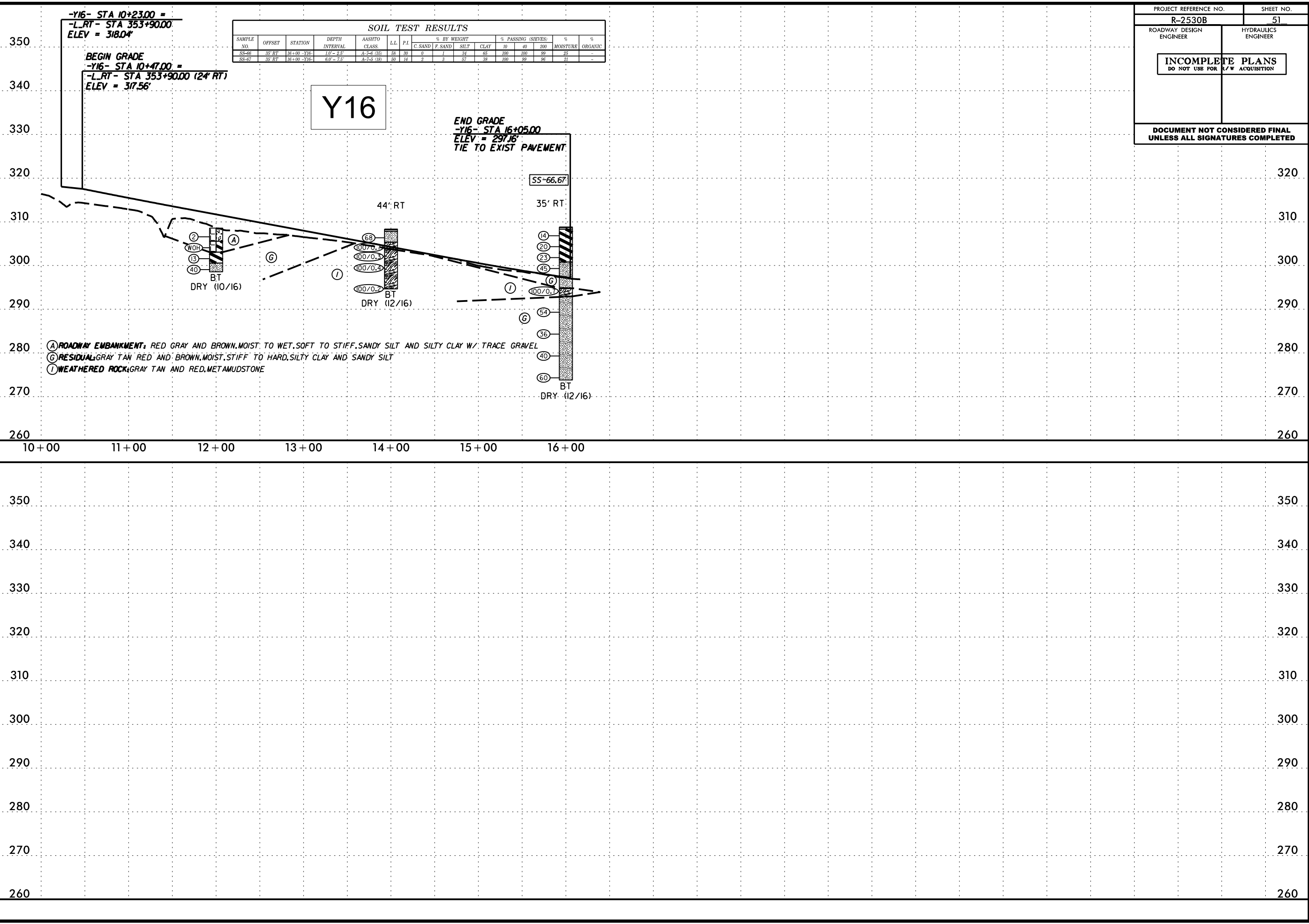
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PROJECT REFERENCE NO.	SHEET NO.
R-2530B	50
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



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 cadman@p

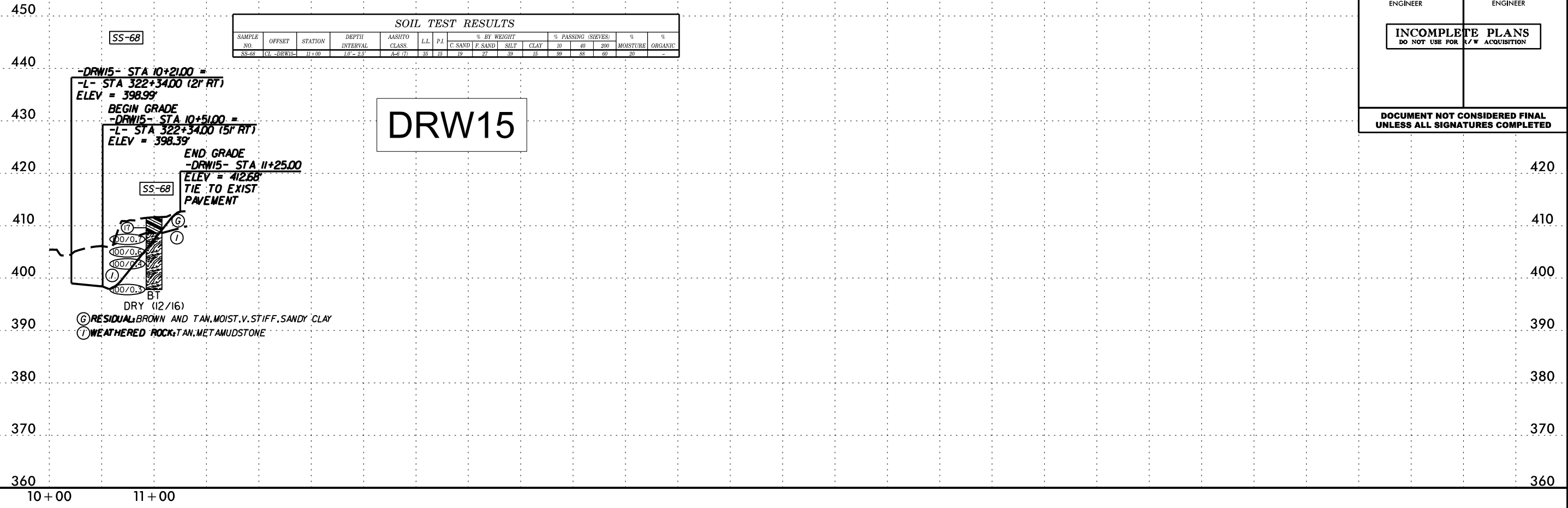


PROJECT REFERENCE NO. R-2530B	SHEET NO. 51
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DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

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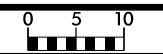
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R-2530B	53
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	PI	% BY WEIGHT				% PASSING (SIRYES)		% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	200		
SS-68	CL - DRW15-	11+00	1'0" - 2'5"	A-6 (7)	35	15	19	27	39	15	99	88	60	-

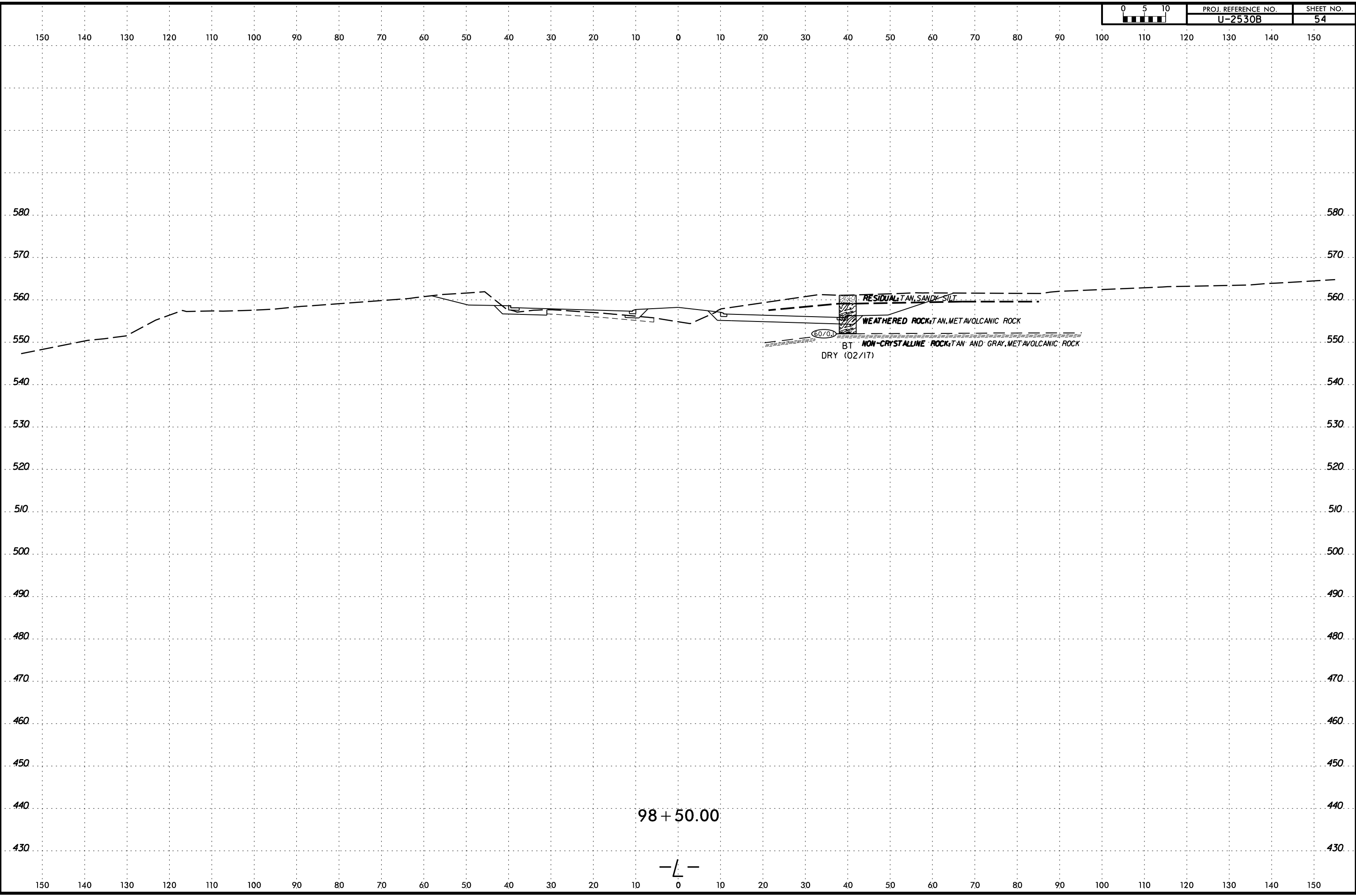


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 370
 360

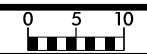
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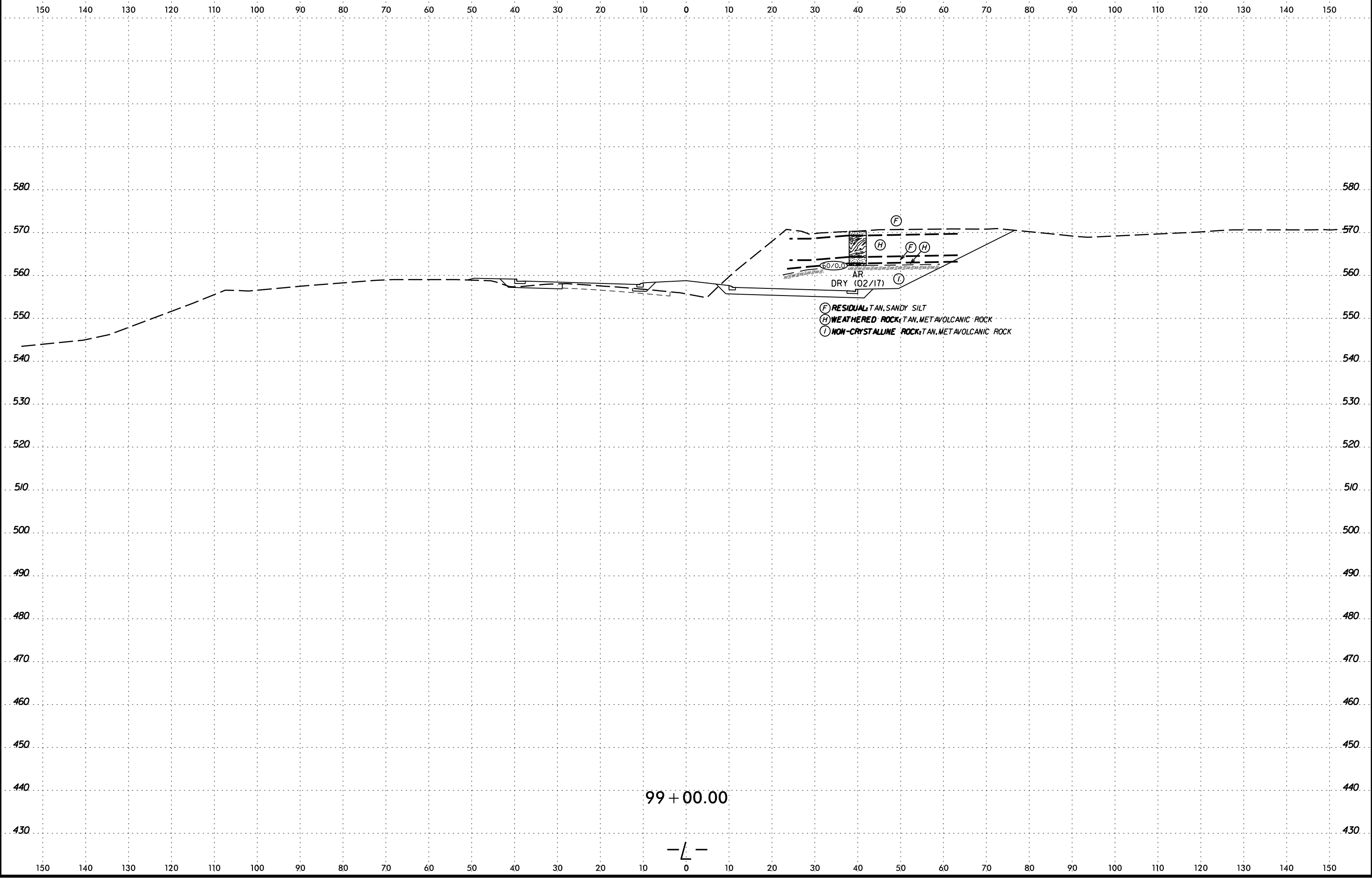
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U-2530B	54



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6/23/16
6/23/16



PROJ. REFERENCE NO.	SHEET NO.
U-2530B	55

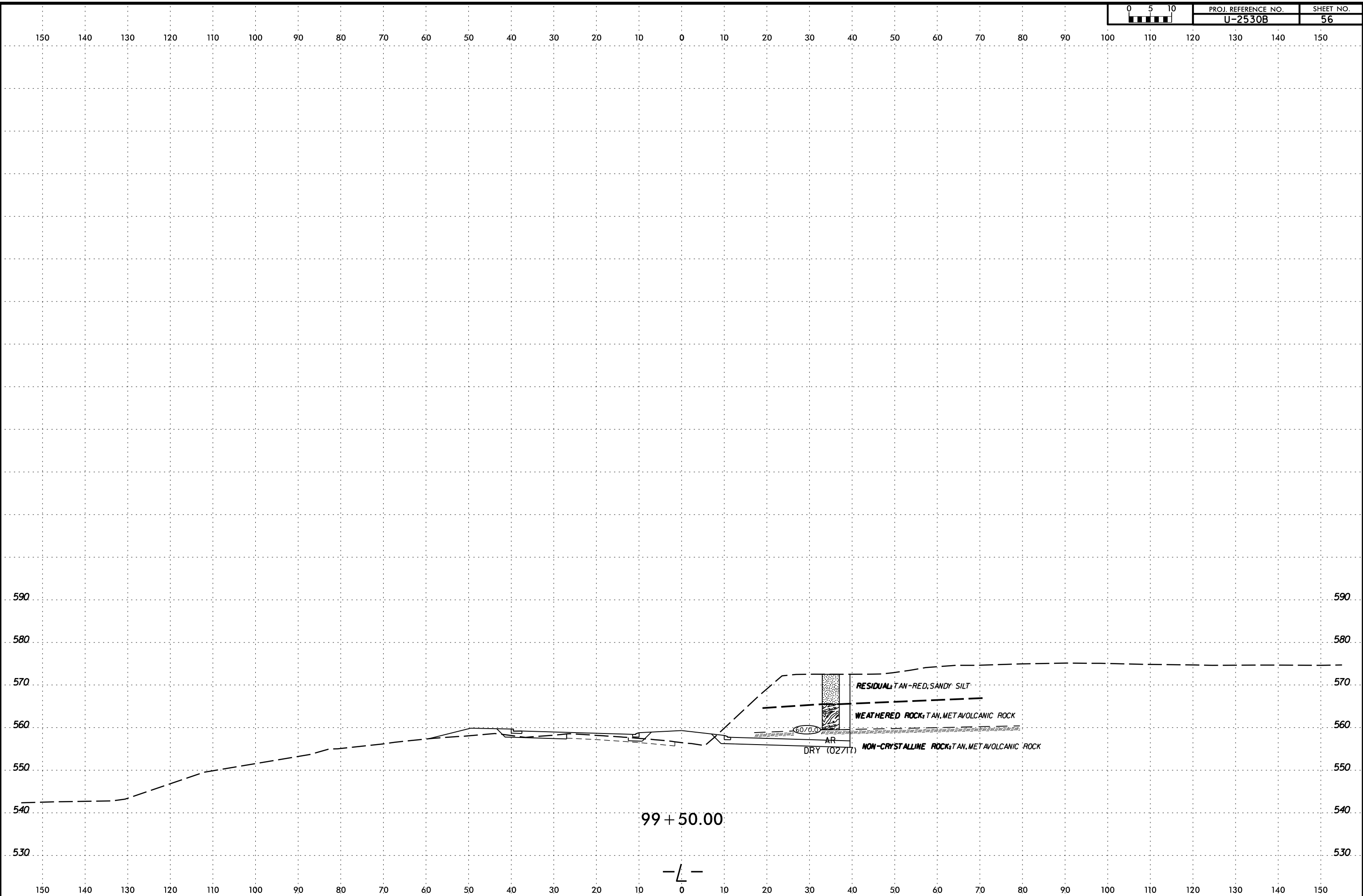


99 + 00.00

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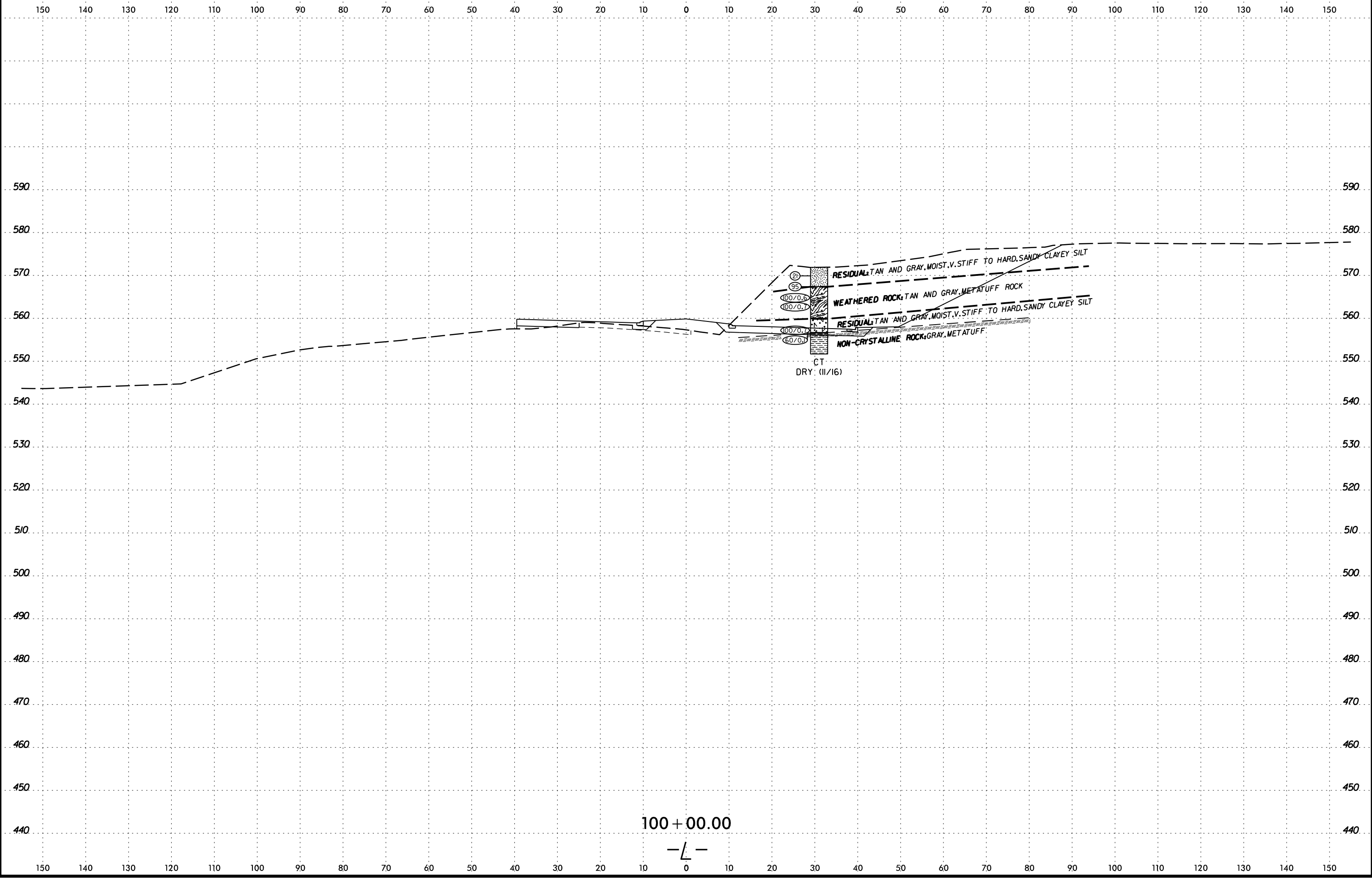
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	U-2530B	56



6/23/16
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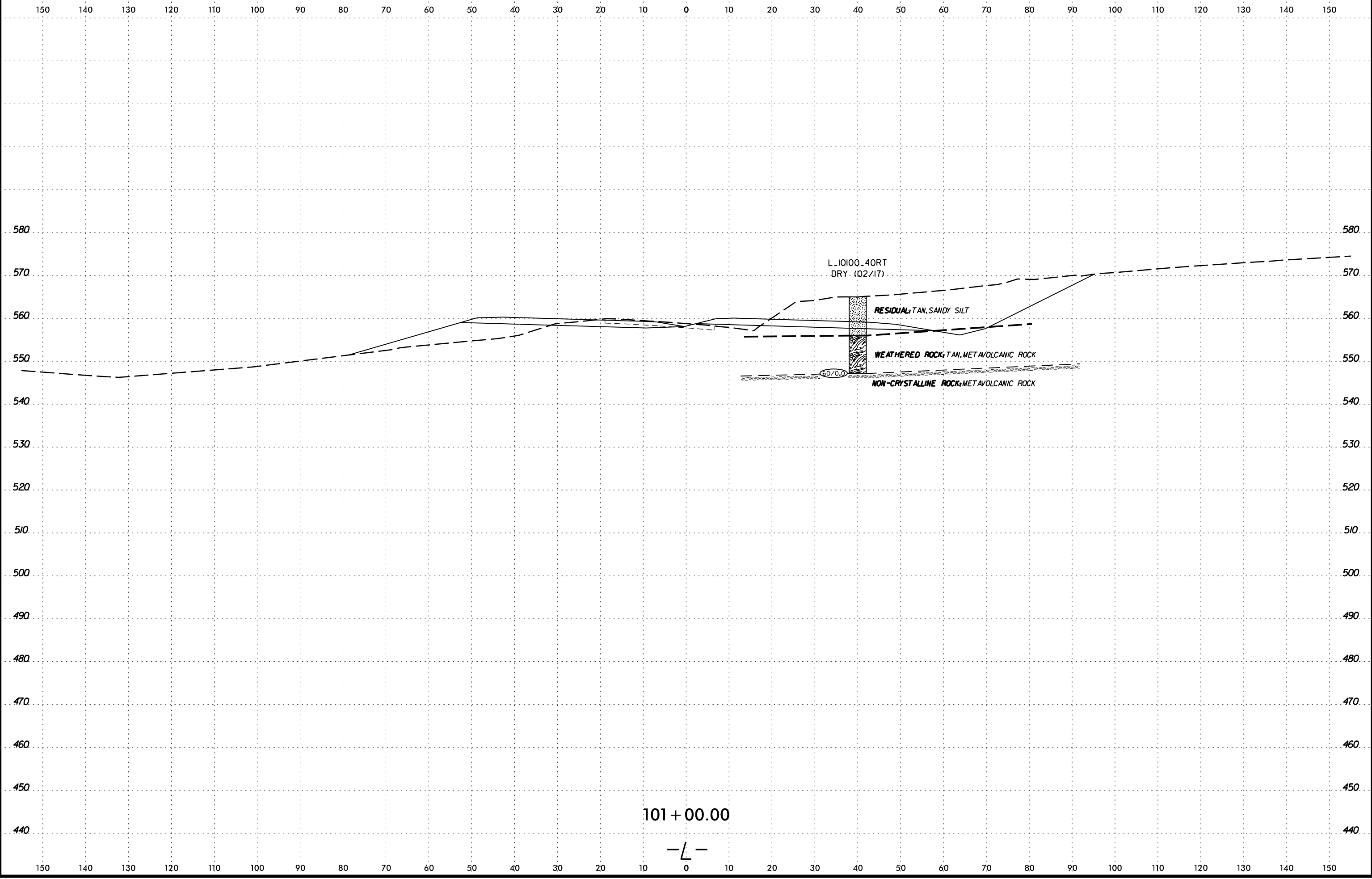
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	U-2530B	57

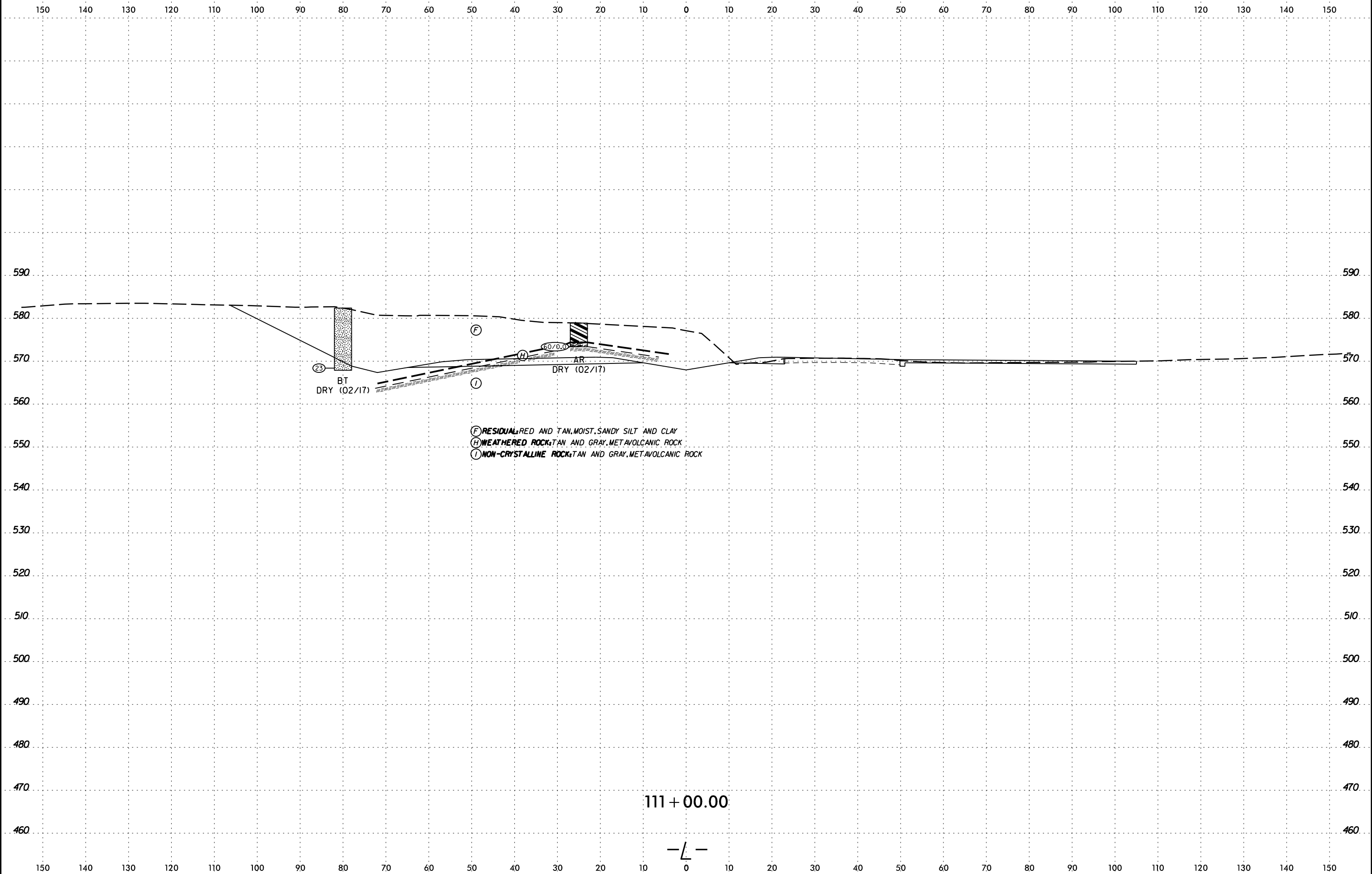


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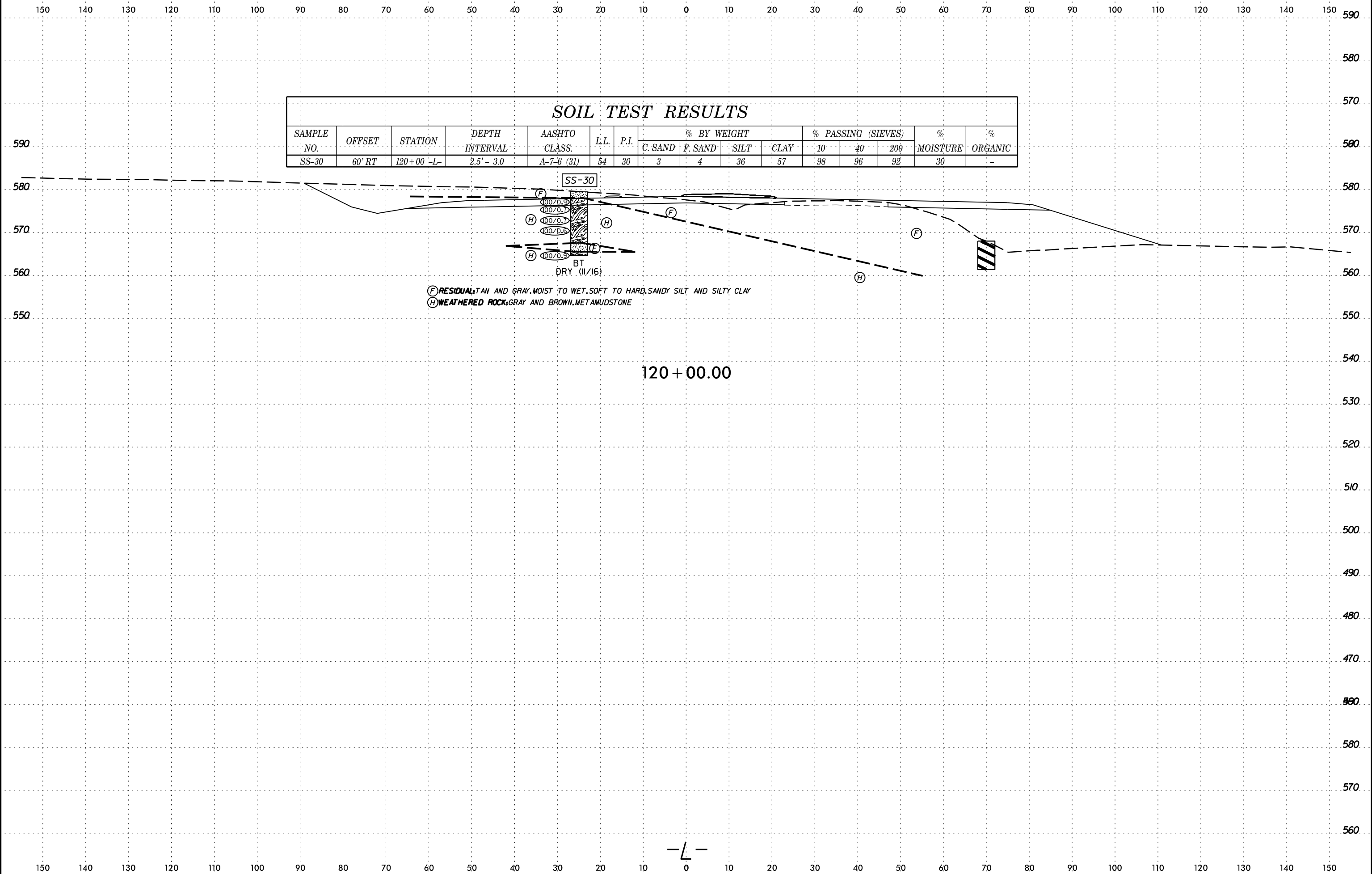
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6/23/16
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 cadmachine AI GEO-8

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-30	60' RT	120+00 -L-	2.5' - 3.0	A-7-6 (31)	54	30	3	4	36	57	98	96	92	30	-

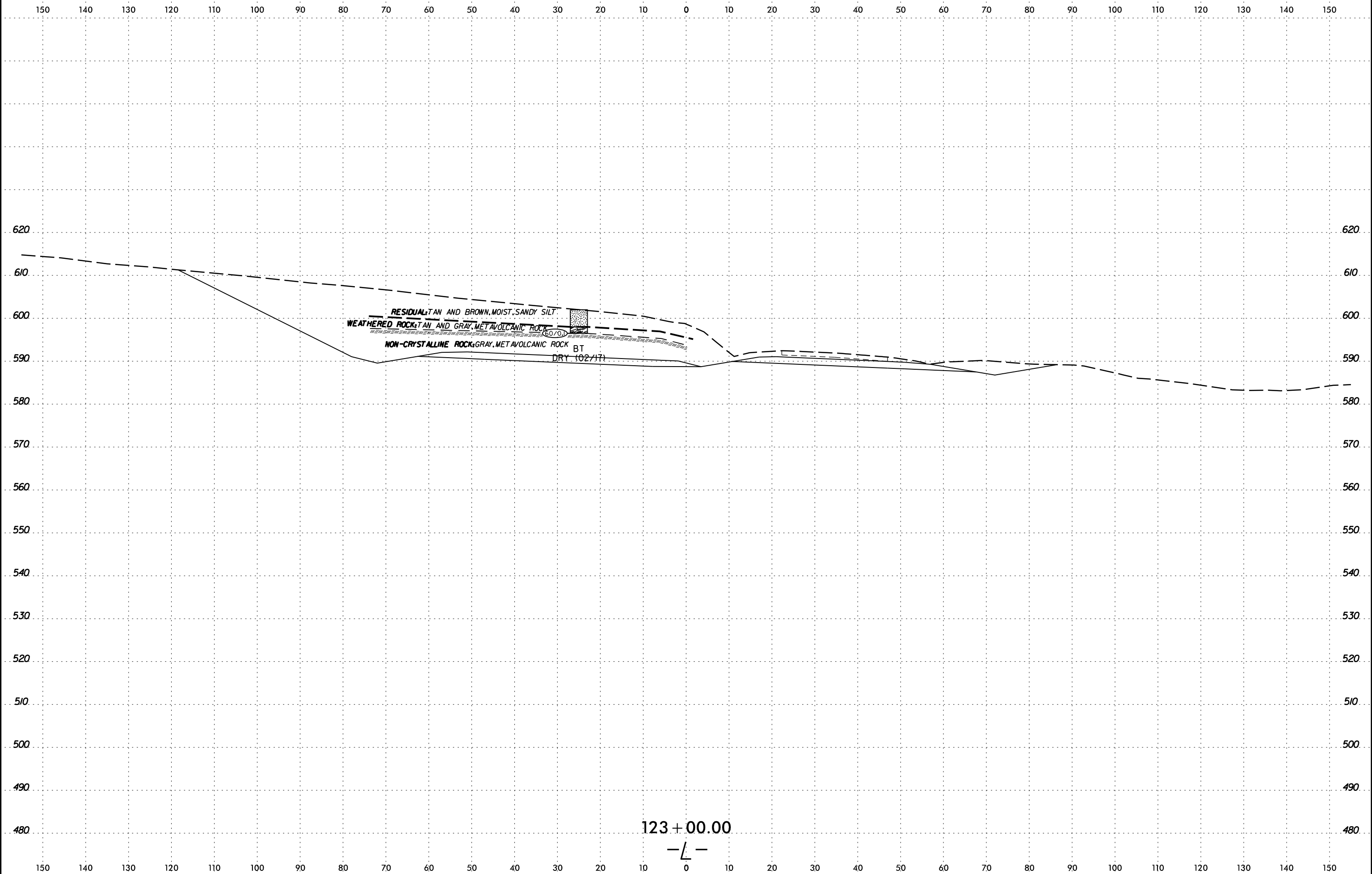


(F) RESIDUAL TAN AND GRAY, MOIST TO WET, SOFT TO HARD, SANDY SILT AND SILTY CLAY
 (H) WEATHERED ROCK, GRAY AND BROWN, METAMUDSTONE

120 + 00.00

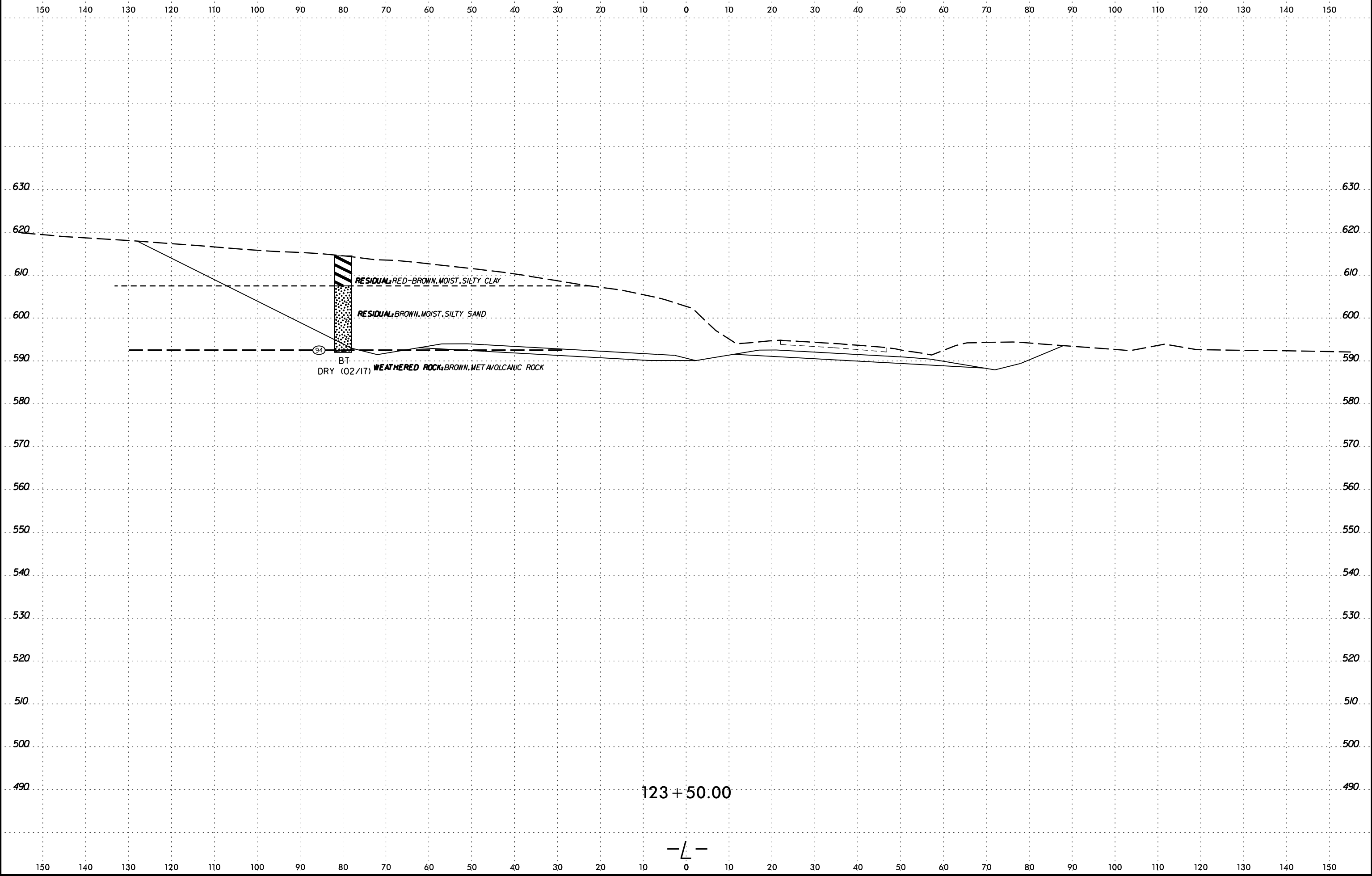
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 cadmachine AI GEO-4



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 cadmachine AJ GEOI-8

6/23/16
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geomachline AT GEOI-8



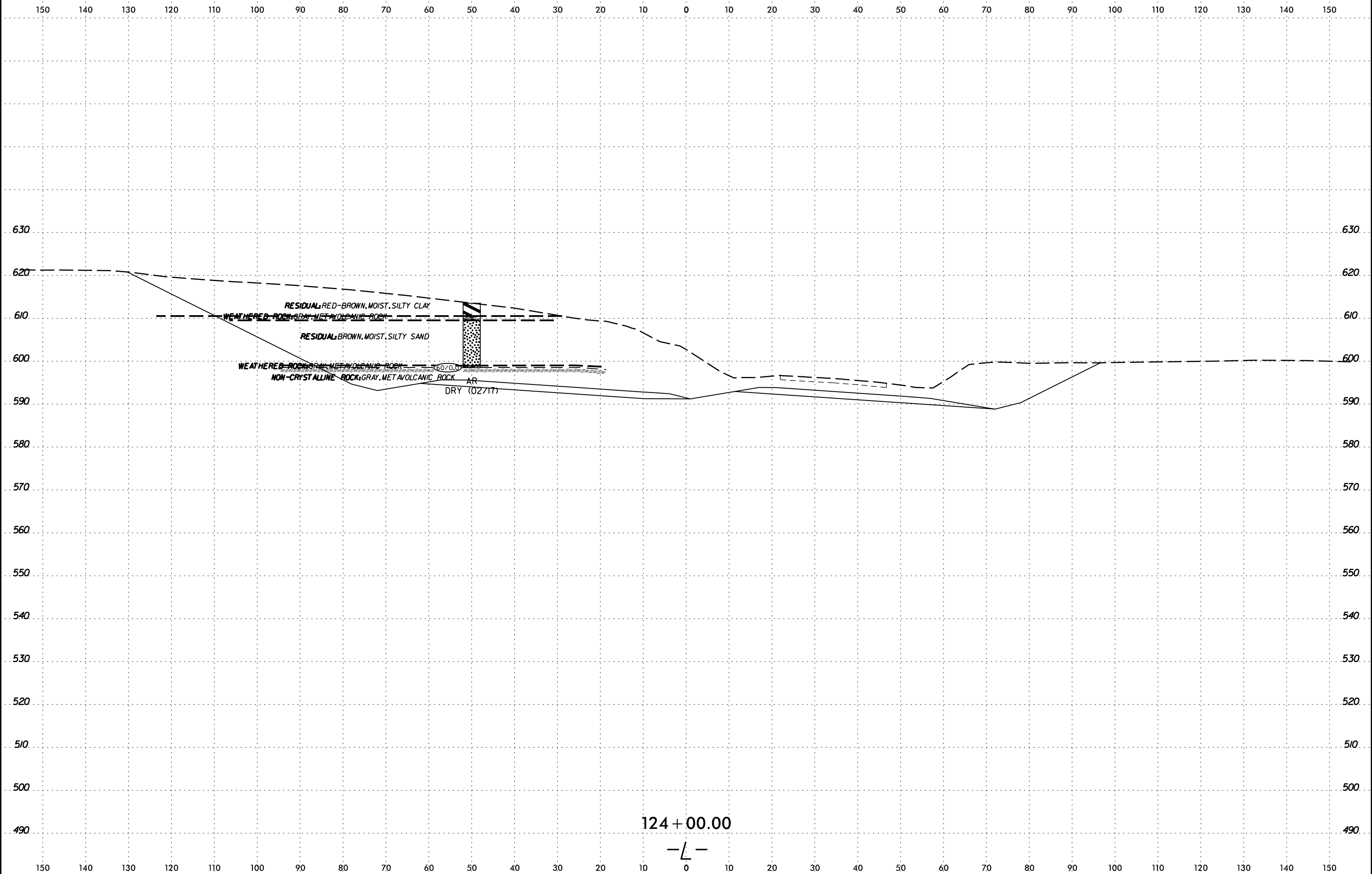
123 + 50.00

— L —

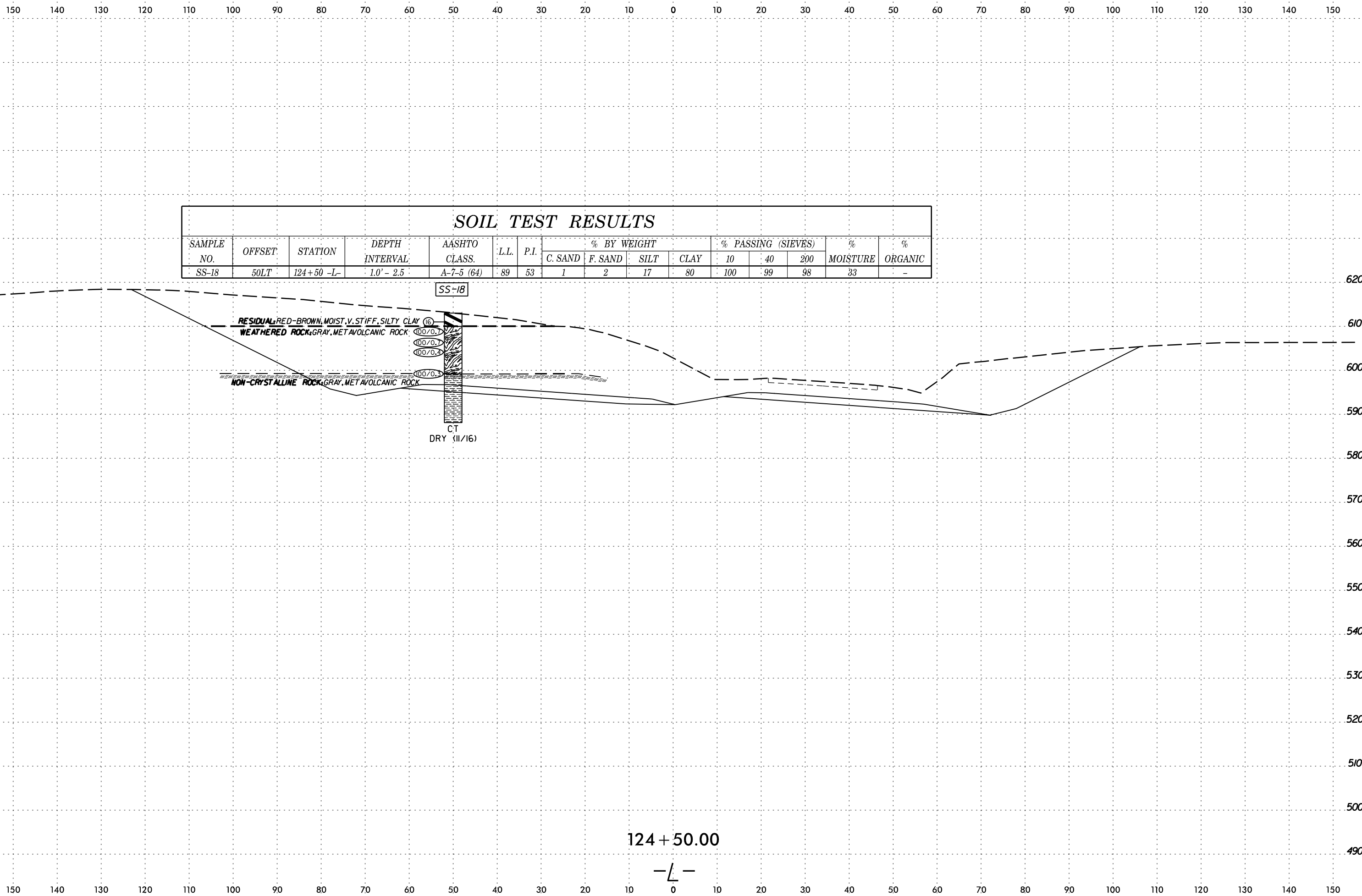
6/23/16



PROJ. REFERENCE NO.	SHEET NO.
R-2530B	64



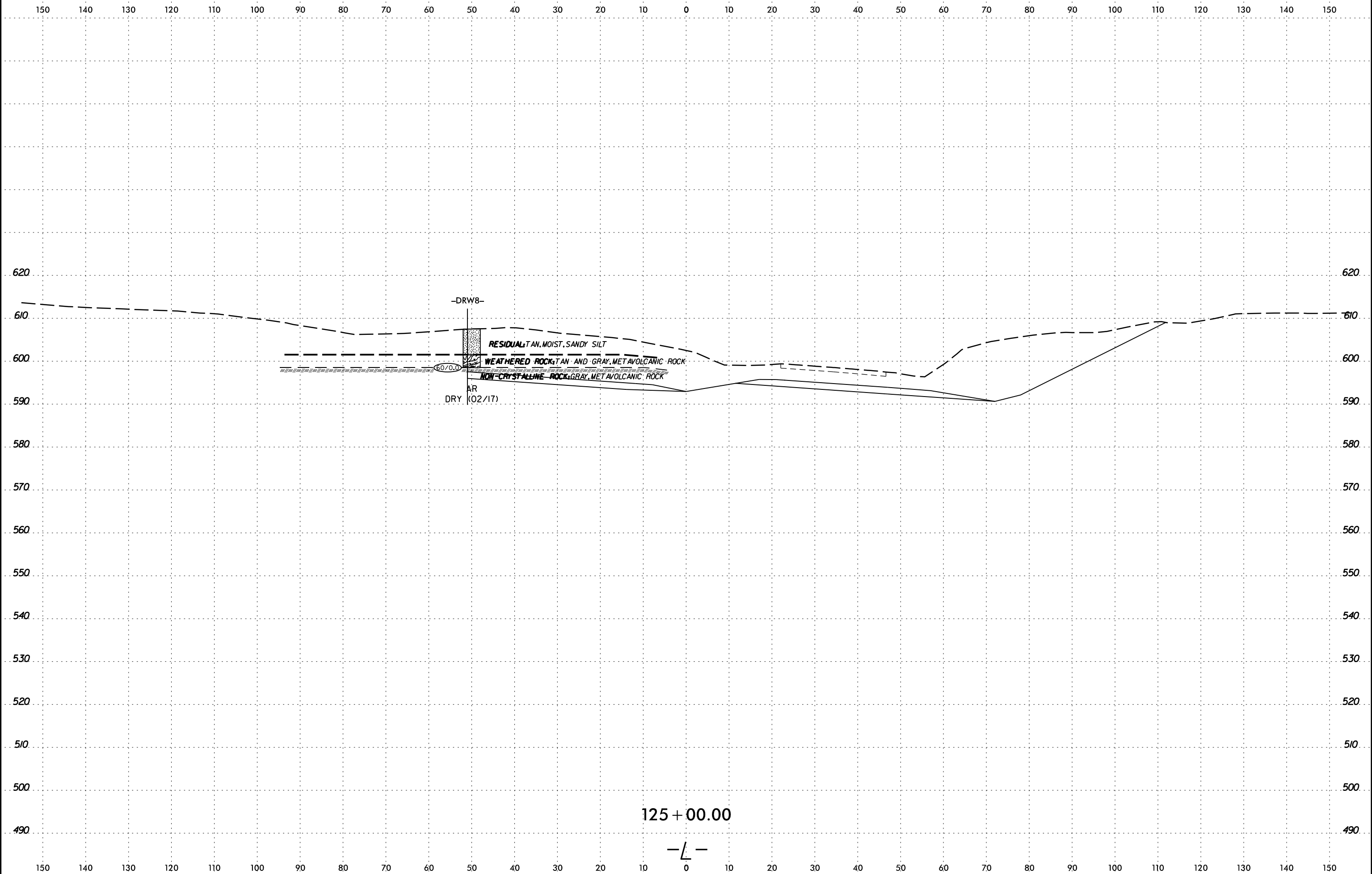
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 cadman@stnly.com



SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-18	50LT	124+50 -L-	1.0' - 2.5'	A-7-5 (64)	89	53	1	2	17	80	100	99	98	33	-

2:\APR-2017 10:07 I:\Projects\2016\G16055-00 R-2530B US 24-27 Stanly County\Projects\2016\G16055-00 R-2530B\NCDOT\Electronic\File_Tree\Geotech\Investigation\Design\R2530B.GEO\RDWY\CADD.GEOTECH\SS-18.dgn
 cadmachine AI GEO-18

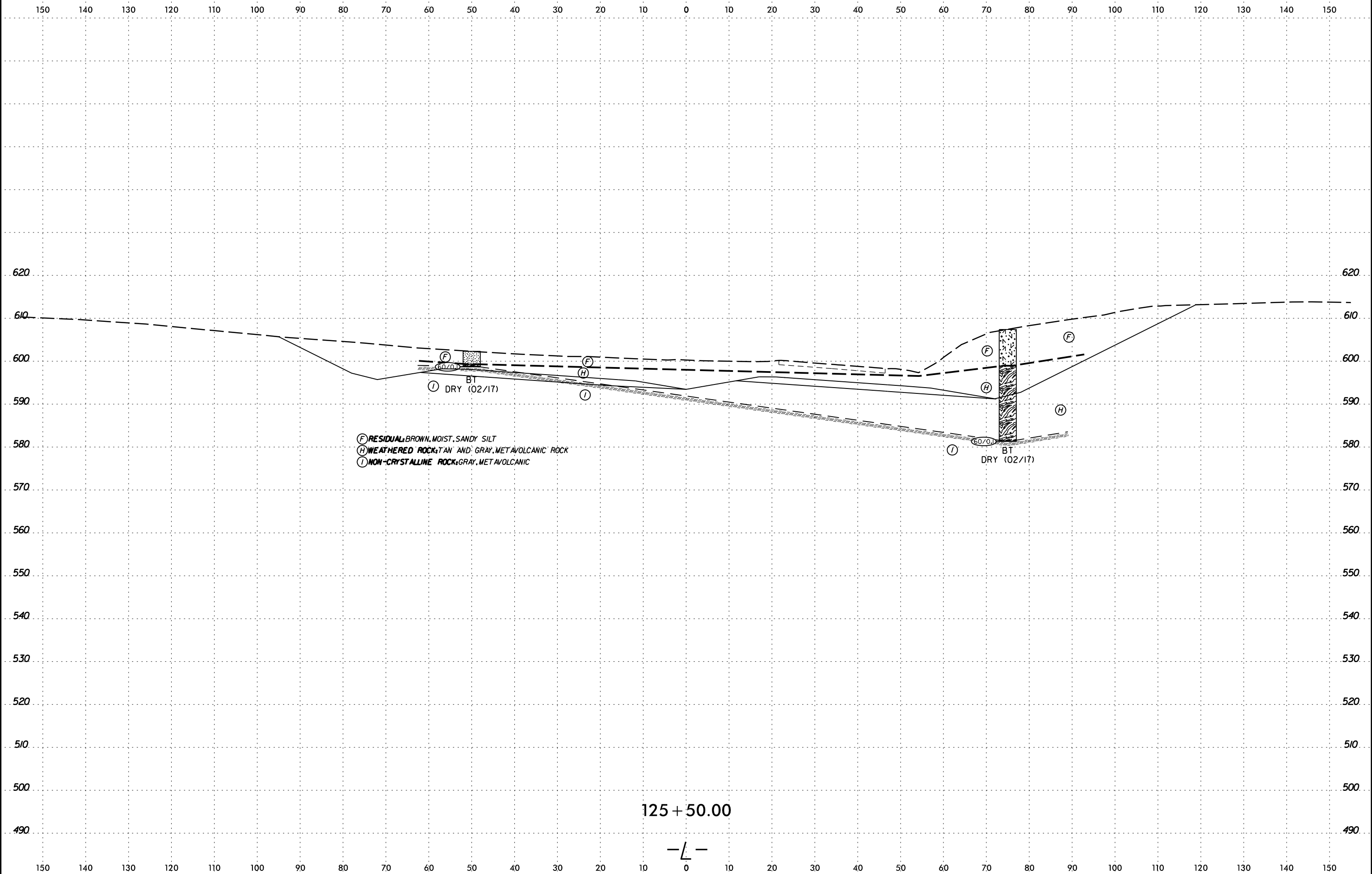
124 + 50.00
-L-



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 cadmachine AT GEOI-8

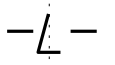
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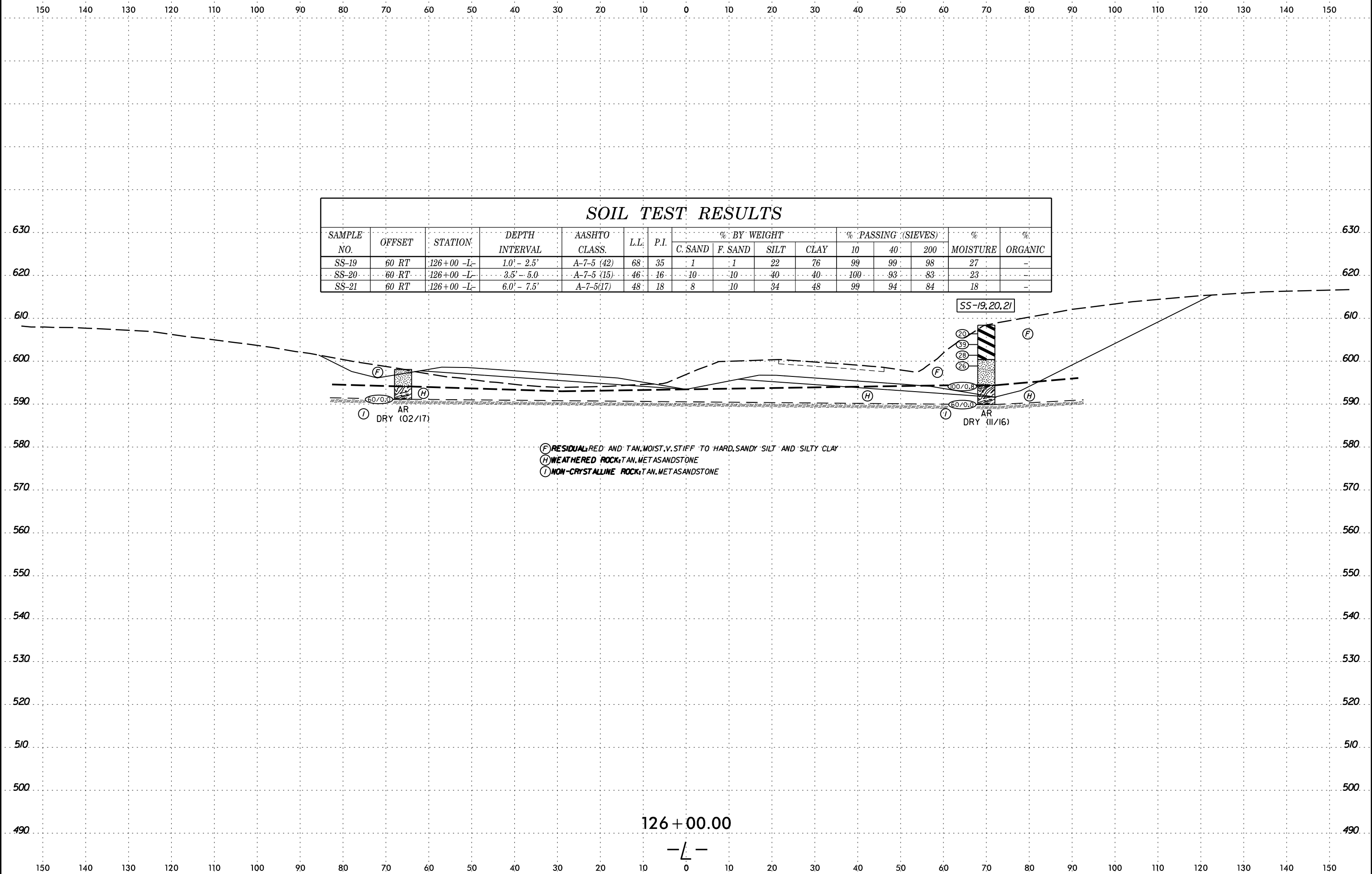


- (F) RESIDUAL BROWN, MOIST, SANDY SILT
- (H) WEATHERED ROCK, TAN AND GRAY, METAVOLCANIC ROCK
- (I) NON-CRYSTALLINE ROCK, GRAY, METAVOLCANIC

125 + 50.00



2:\APR-2017 10:09 I:\Projects\2016\G16055-00 R-2530B US 24-27 Stanly County\2530B.NCDDT.Electronic.File.Tree\Geotech\Investigation\Design\2530B.GEO.RD.WY\CADD.GEOTECH\XSEC\2530B.Geo.XSI.L.dgn
 6/23/16
 cadmachine AT GEO-18



SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-19	60 RT	126+00 -L-	1.0' - 2.5'	A-7-5 (42)	68	35	1	1	22	76	99	99	98	27	-
SS-20	60 RT	126+00 -L-	3.5' - 5.0'	A-7-5 (15)	46	16	10	10	40	40	100	93	83	23	-
SS-21	60 RT	126+00 -L-	6.0' - 7.5'	A-7-5(17)	48	18	8	10	34	48	99	94	84	18	-

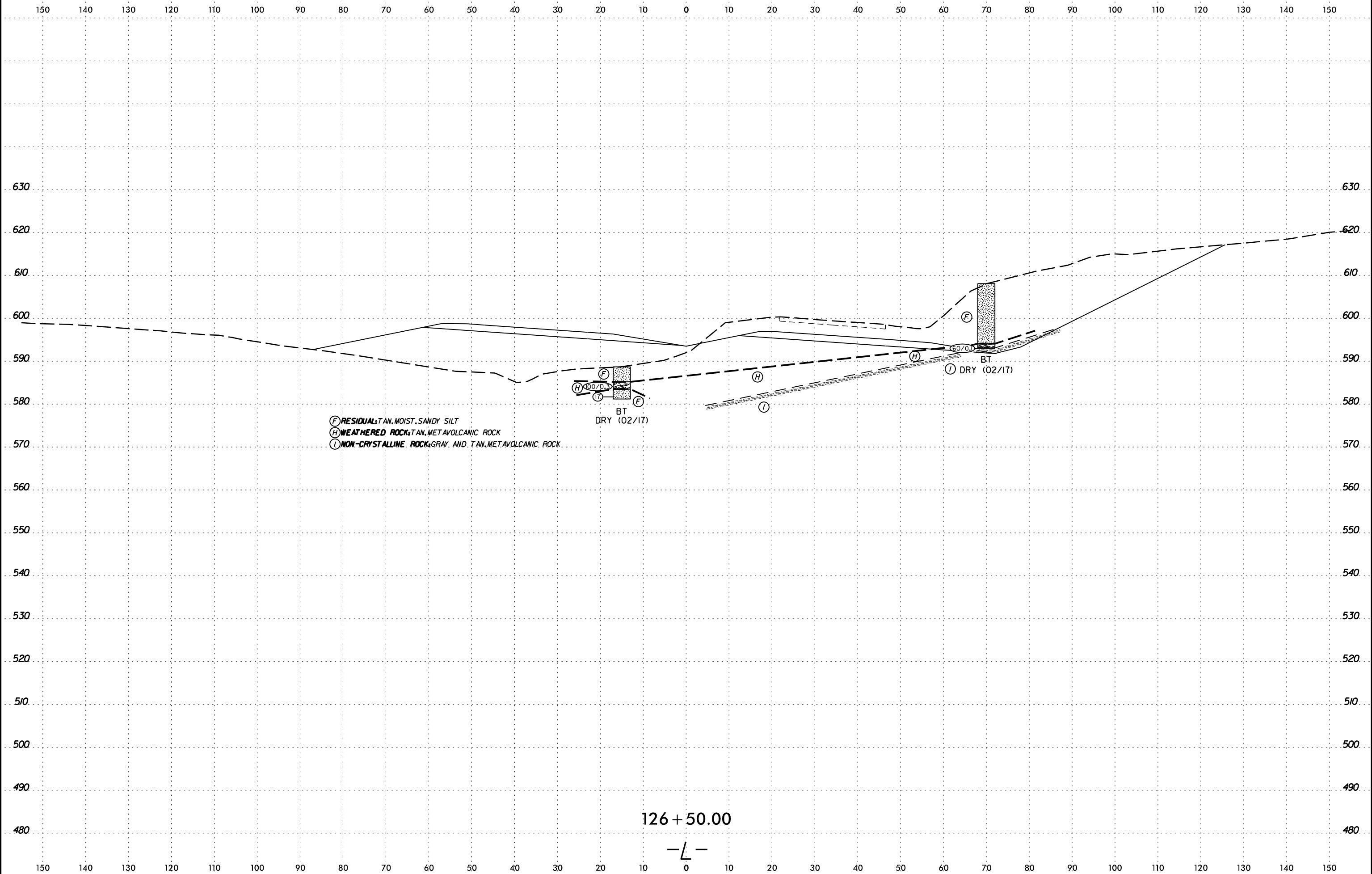
- (F) RESIDUAL RED AND TAN, MOIST, V. STIFF TO HARD, SANDY SILT AND SILTY CLAY
- (H) WEATHERED ROCK, TAN, METASANDSTONE
- (I) NON-CRYSTALLINE ROCK, TAN, METASANDSTONE

126 + 00.00
-L-

6/23/16



PROJ. REFERENCE NO.	SHEET NO.
R-2530B	69



- (F) RESIDUAL TAN, MOIST, SANDY SILT
- (H) WEATHERED ROCK, TAN, METAVOLCANIC ROCK
- (L) NON-CRYSTALLINE ROCK, GRAY AND TAN, METAVOLCANIC ROCK

BT
 DRY (02/17)

BT
 DRY (02/17)

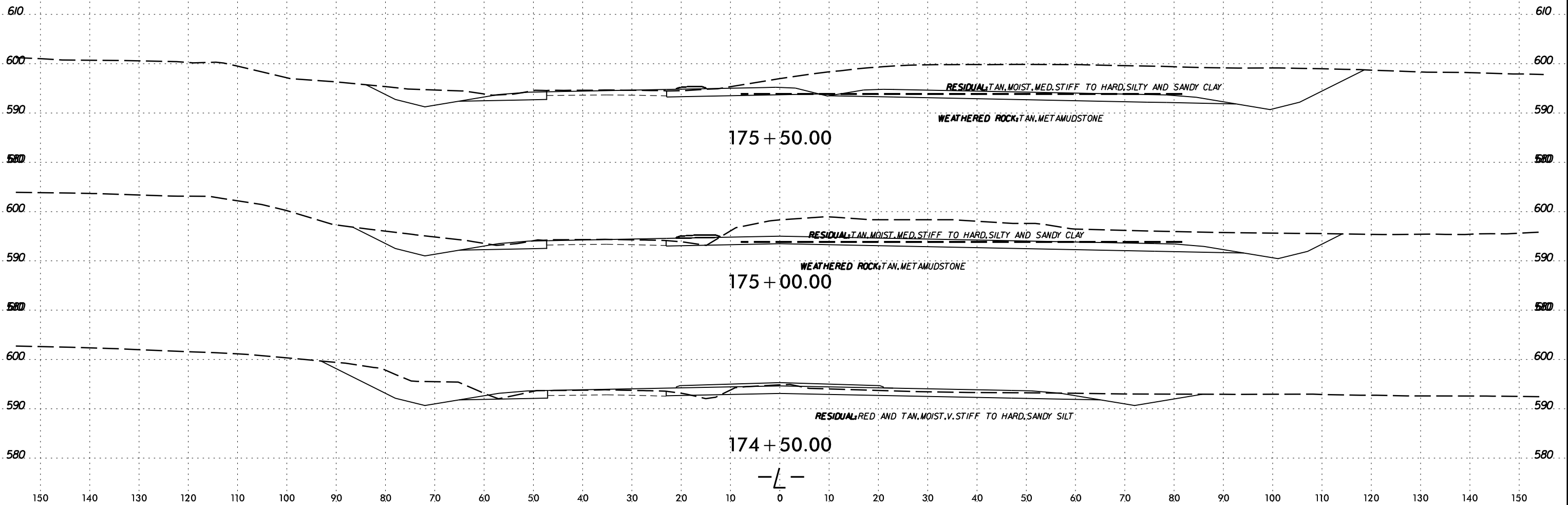
126+50.00

-L-

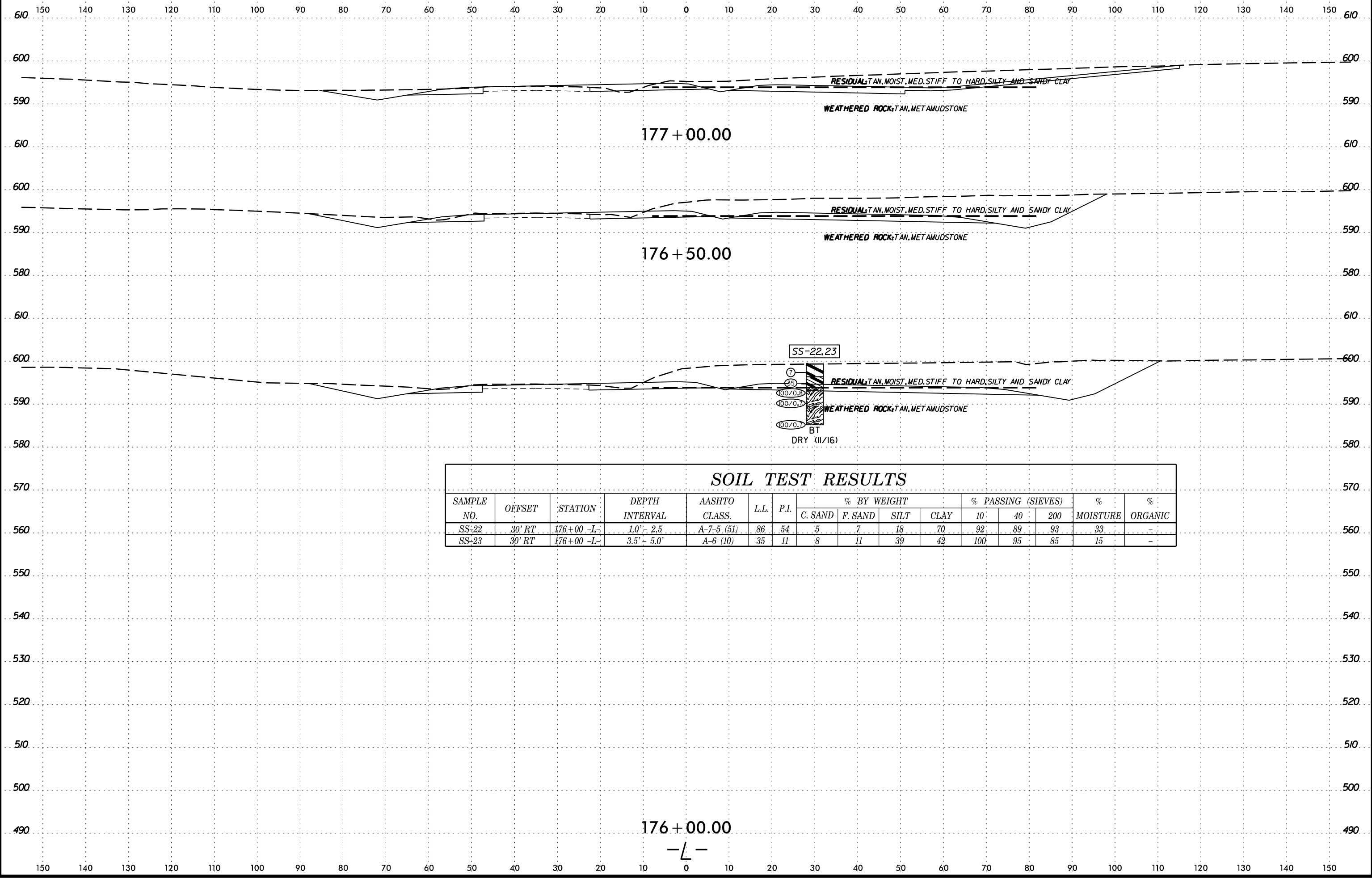
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 cadman@time



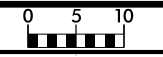
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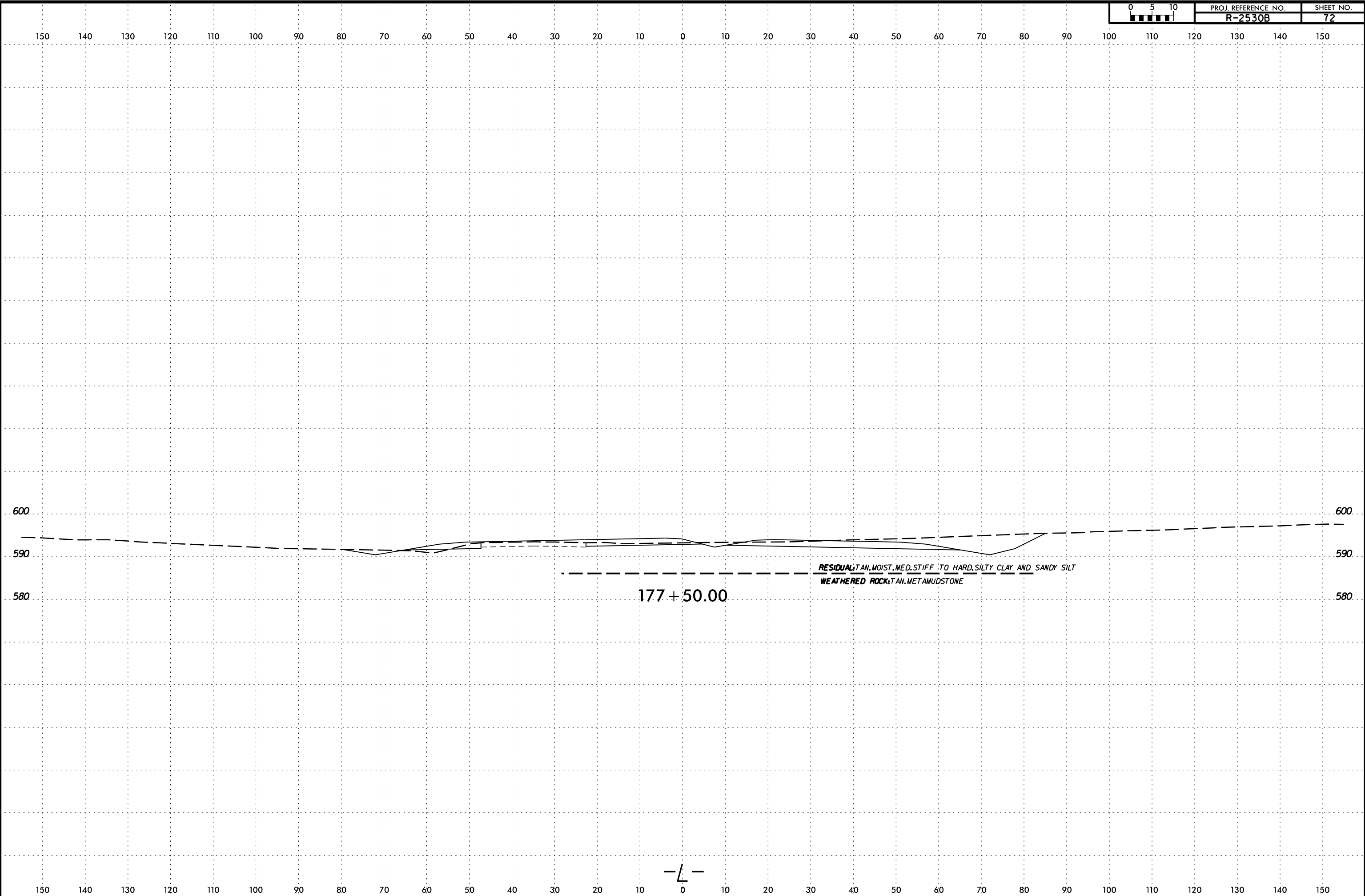
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 6/23/16
 cadmachine AI GEO-8



SOIL TEST RESULTS																
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC	
							C. SAND	F. SAND	SILT	CLAY	10'	40	200			
SS-22	30' RT	176+00 -L-	1.0' - 2.5'	A-7-5 (51)	86	54	5	7	18	70	92	89	93	33	-	
SS-23	30' RT	176+00 -L-	3.5' - 5.0'	A-6 (10)	35	11	8	11	39	42	100	95	85	15	-	

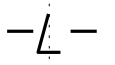


PROJ. REFERENCE NO.	SHEET NO.
R-2530B	72

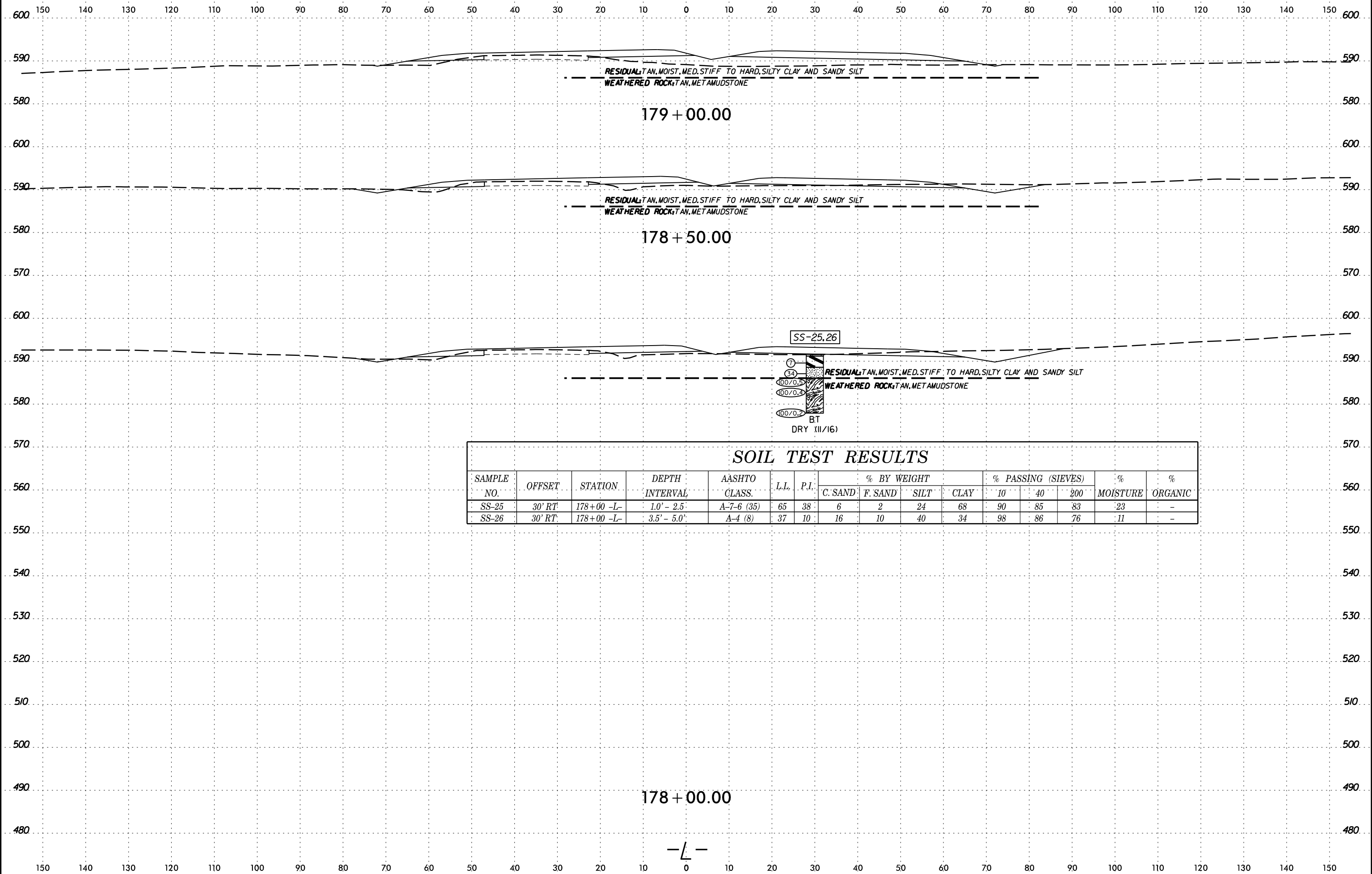


RESIDUAL TAN. MOIST. MED. STIFF TO HARD, SILTY CLAY AND SANDY SILT
WEATHERED ROCK TAN. METAMUDSTONE

177+50.00



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 6/23/16
 cadmachine



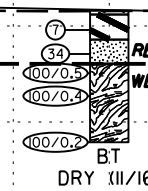
RESIDUAL TAN. MOIST. MED. STIFF TO HARD. SILTY CLAY AND SANDY SILT
 WEATHERED ROCK TAN. METAMUDSTONE

179 + 00.00

RESIDUAL TAN. MOIST. MED. STIFF TO HARD. SILTY CLAY AND SANDY SILT
 WEATHERED ROCK TAN. METAMUDSTONE

178 + 50.00

SS-25,26



RESIDUAL TAN. MOIST. MED. STIFF TO HARD. SILTY CLAY AND SANDY SILT
 WEATHERED ROCK TAN. METAMUDSTONE

SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	PI	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-25	30' RT	178+00 -L-	1.0' - 2.5'	A-7-6 (35)	65	38	6	2	24	68	90	85	83	23	-
SS-26	30' RT	178+00 -L-	3.5' - 5.0'	A-4 (8)	37	10	16	10	40	34	98	86	76	11	-

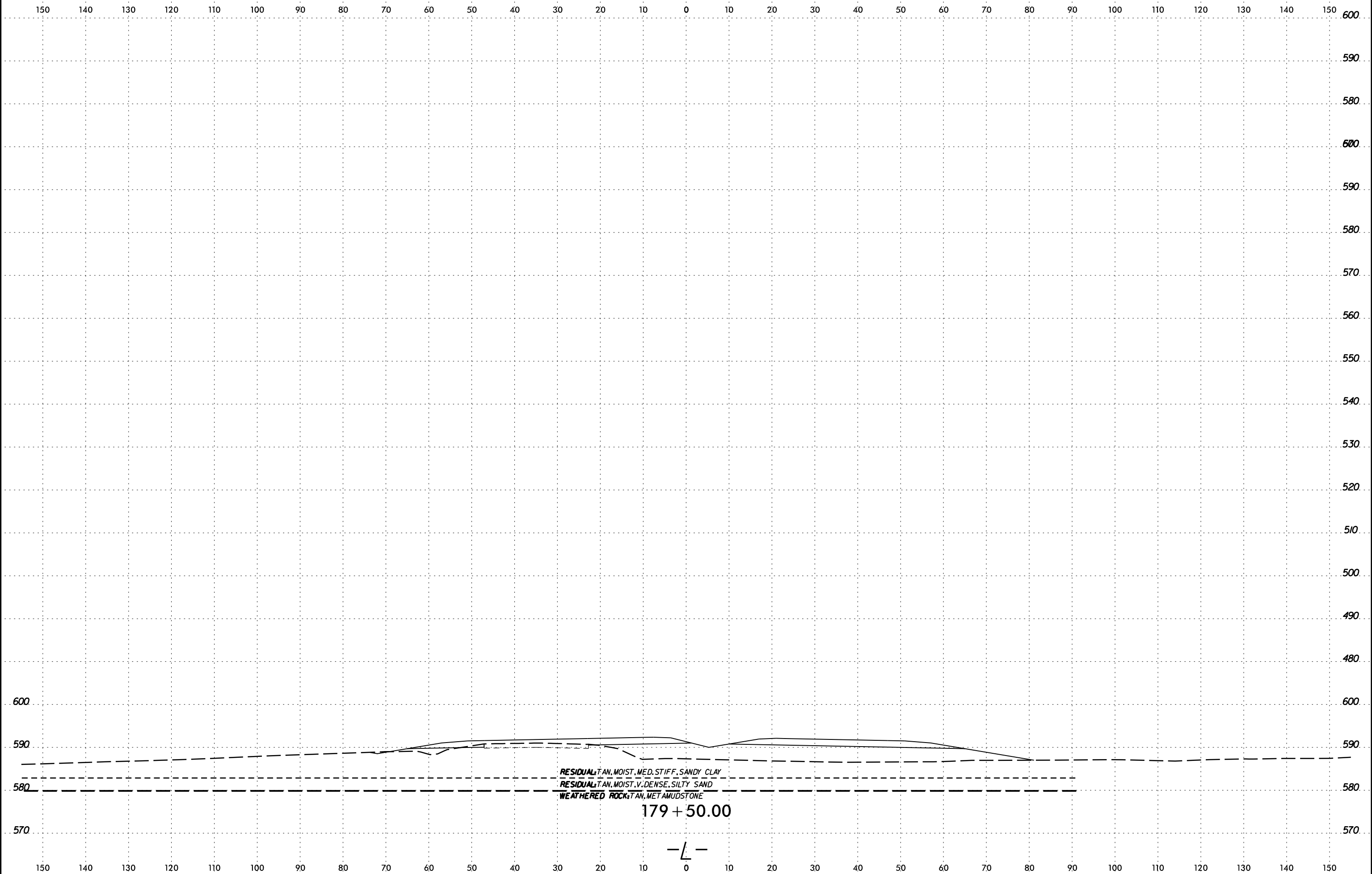
178 + 00.00

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6/23/16
6/23/16

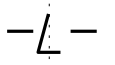


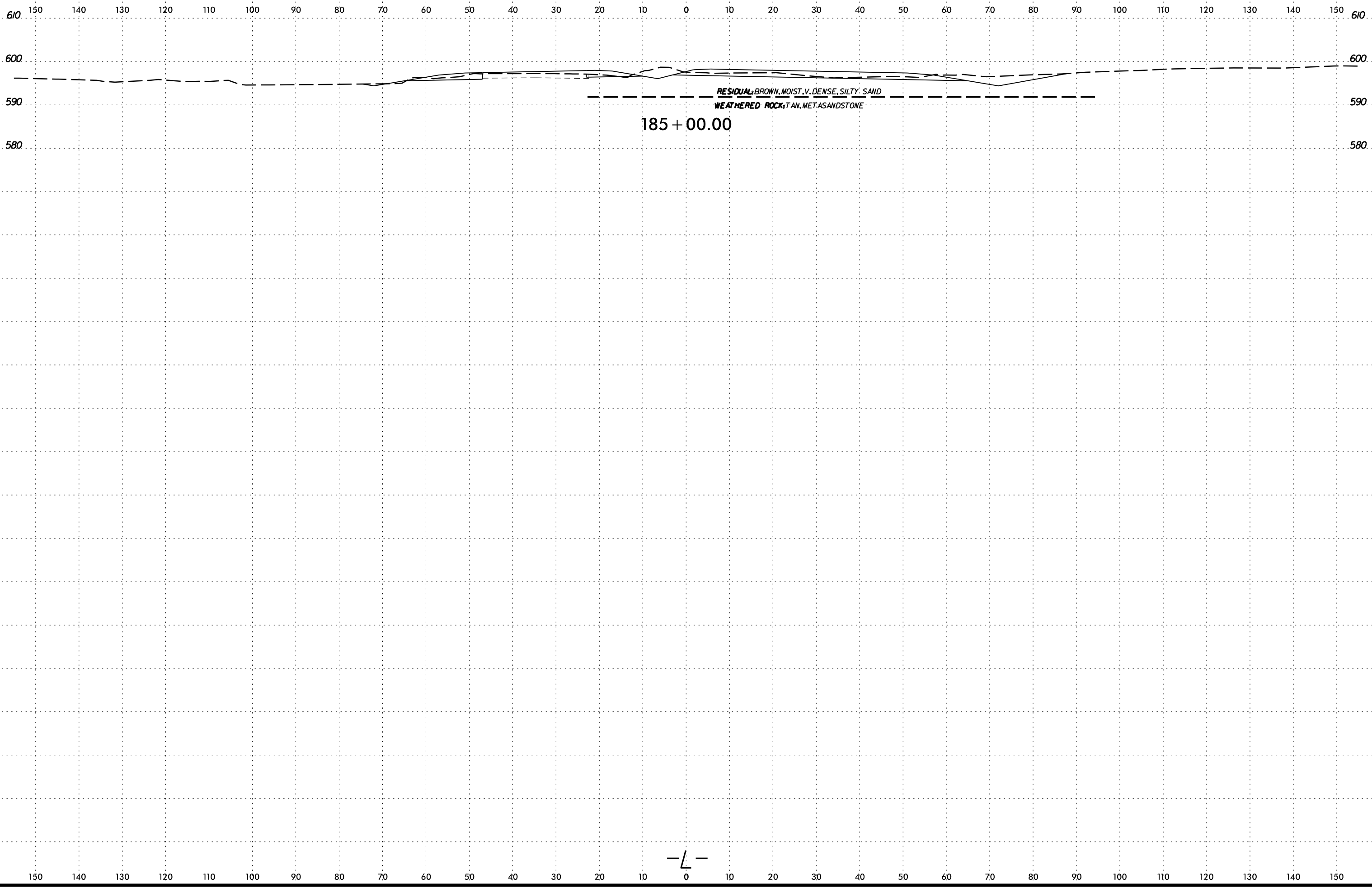
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R-2530B	74

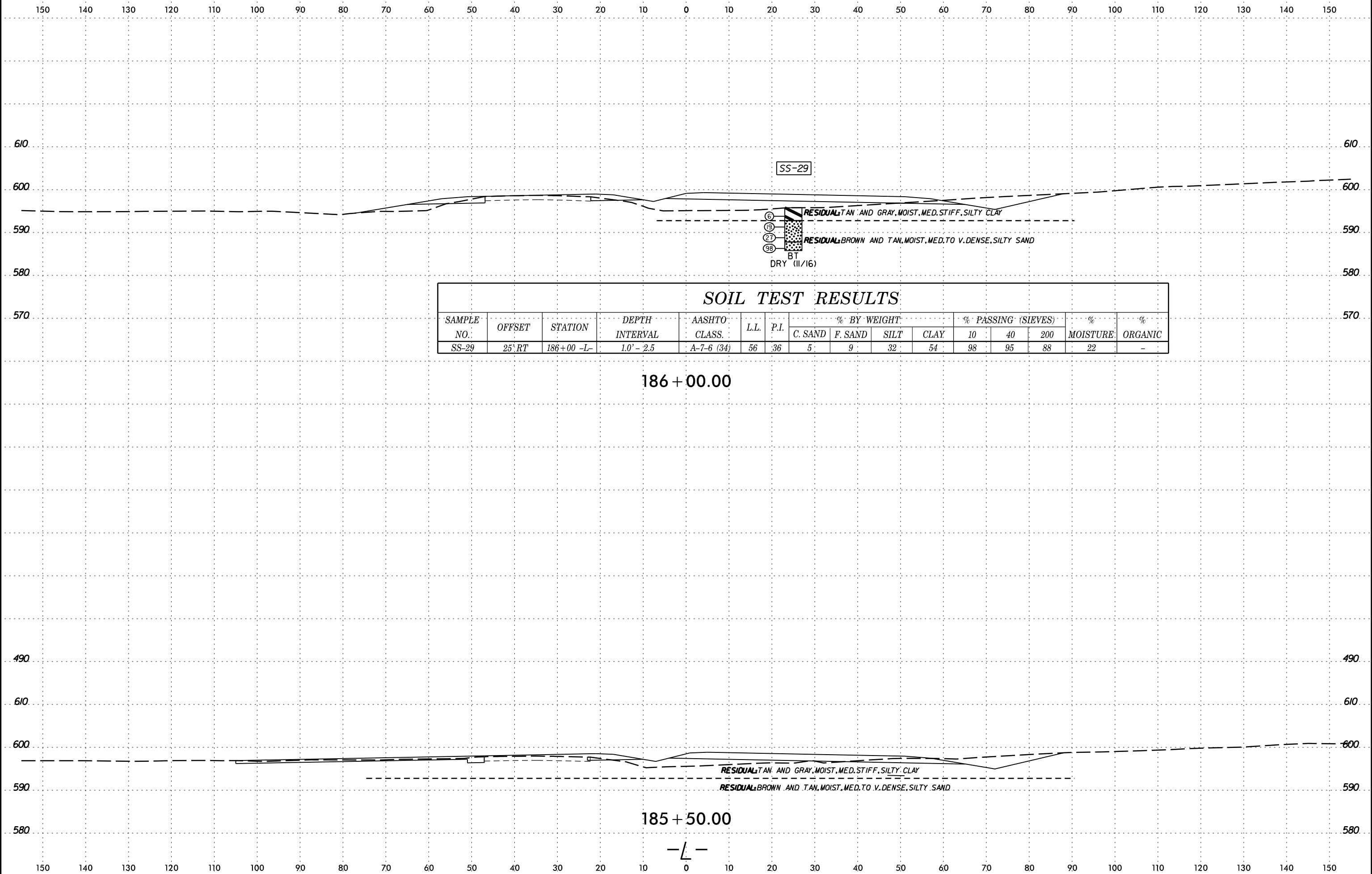


RESIDUAL TAN, MOIST, MED. STIFF, SANDY CLAY
RESIDUAL TAN, MOIST, V. DENSE, SILTY SAND
WEATHERED ROCK, TAN, MET. MUDSTONE

179 + 50.00







SOIL TEST RESULTS

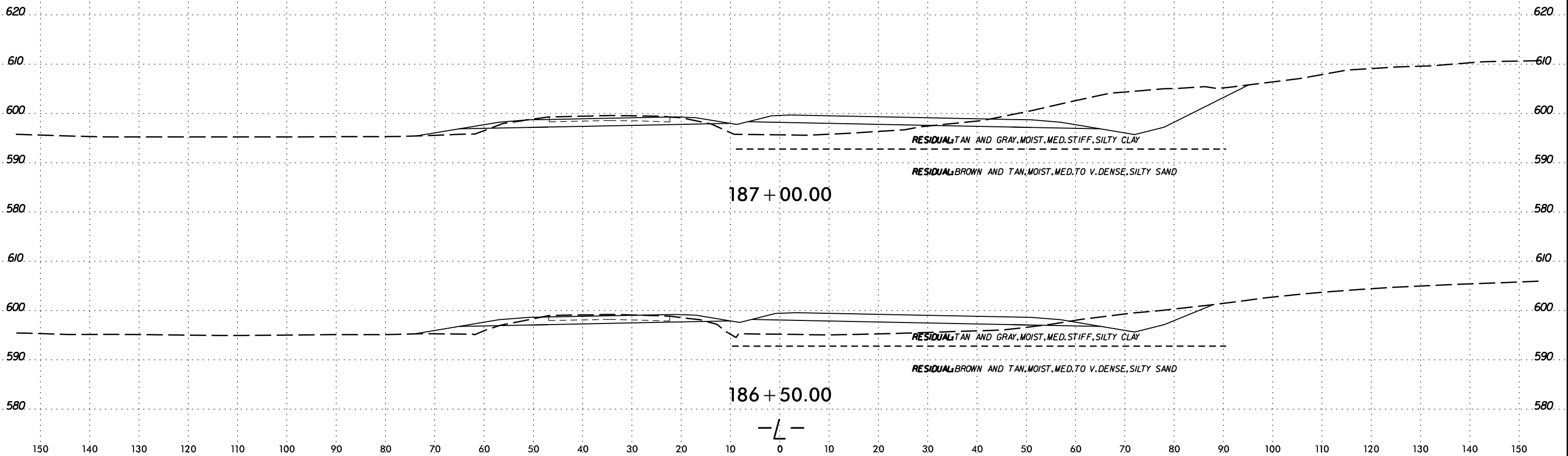
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-29	25' RT	186+00 -L-	1.0' - 2.5'	A-7-6 (34)	56	36	5	9	32	54	98	95	88	22	-

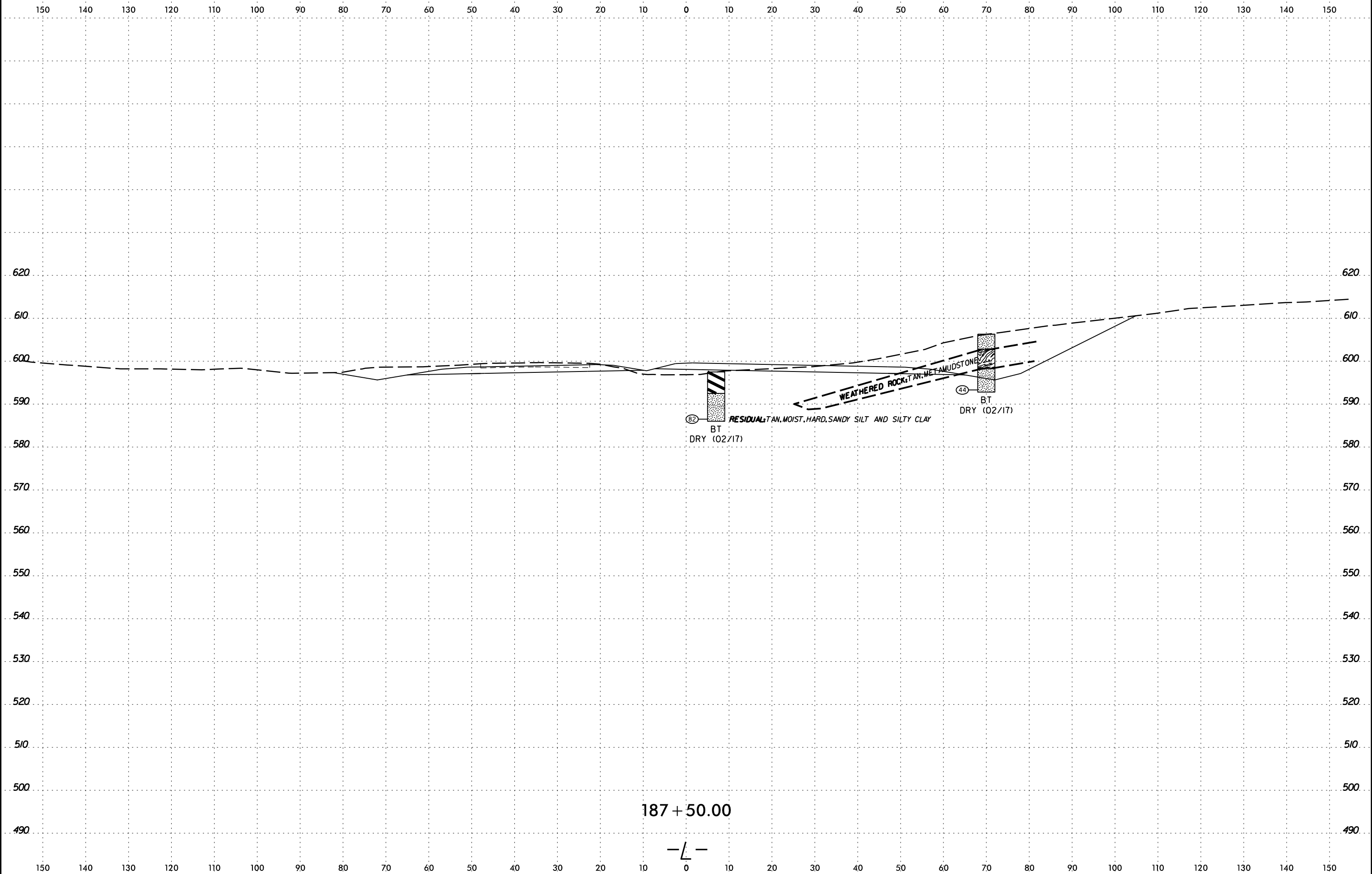
186 + 00.00

185 + 50.00



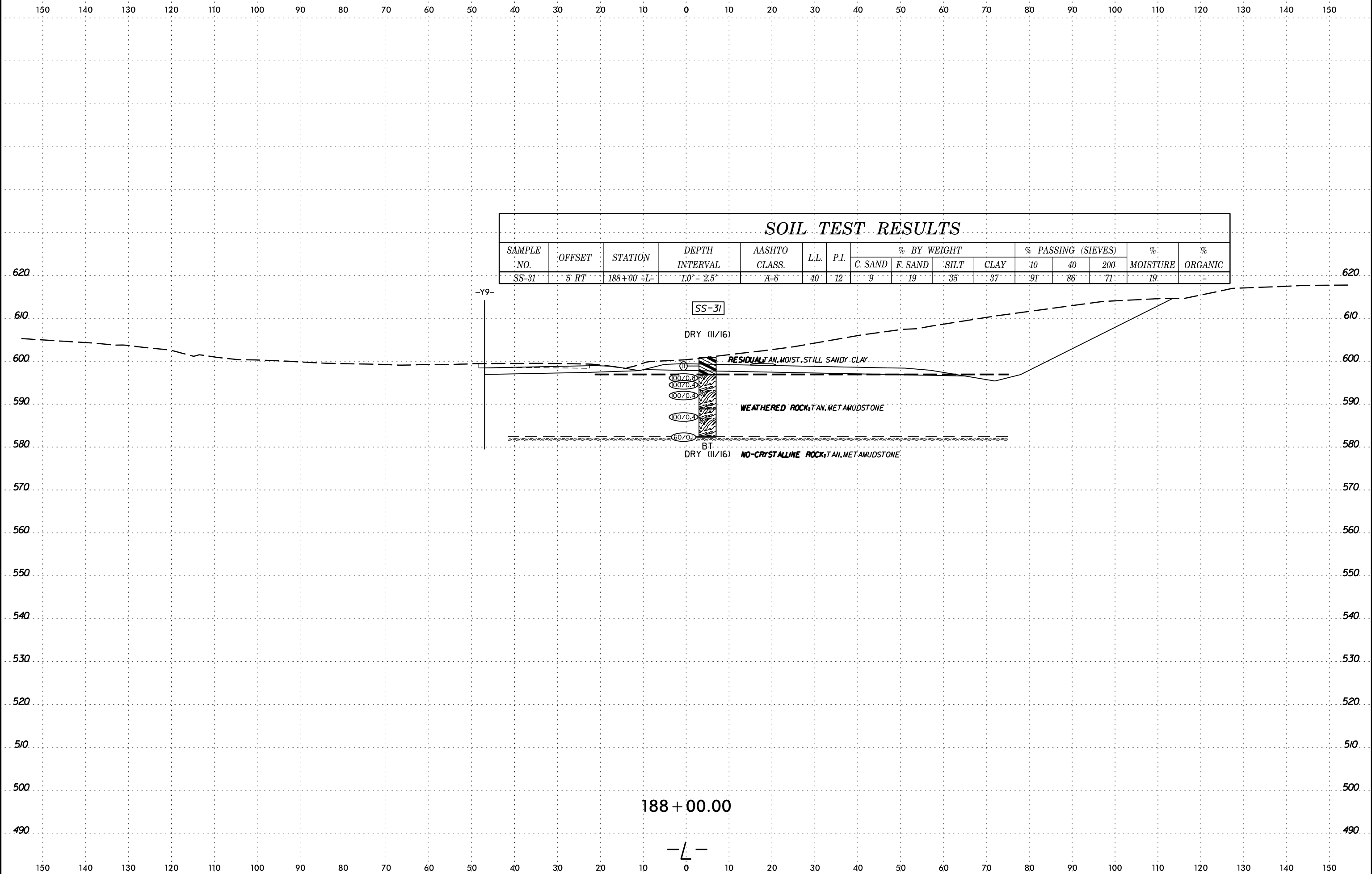
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 6/23/16
 cadmachine AI GEO1-8



SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	#10	#40	#200		
SS-31	5 RT	188+00 ±L-	1.0' - 2.5'	A-6	40	12	9	19	35	37	91	86	71	19	-

SS-31

DRY (11/16)

RESIDUAL TAN, MOIST, STILL SANDY CLAY

WEATHERED ROCK, TAN, METAMUDSTONE

BT

NO-CRYSTALLINE ROCK, TAN, METAMUDSTONE

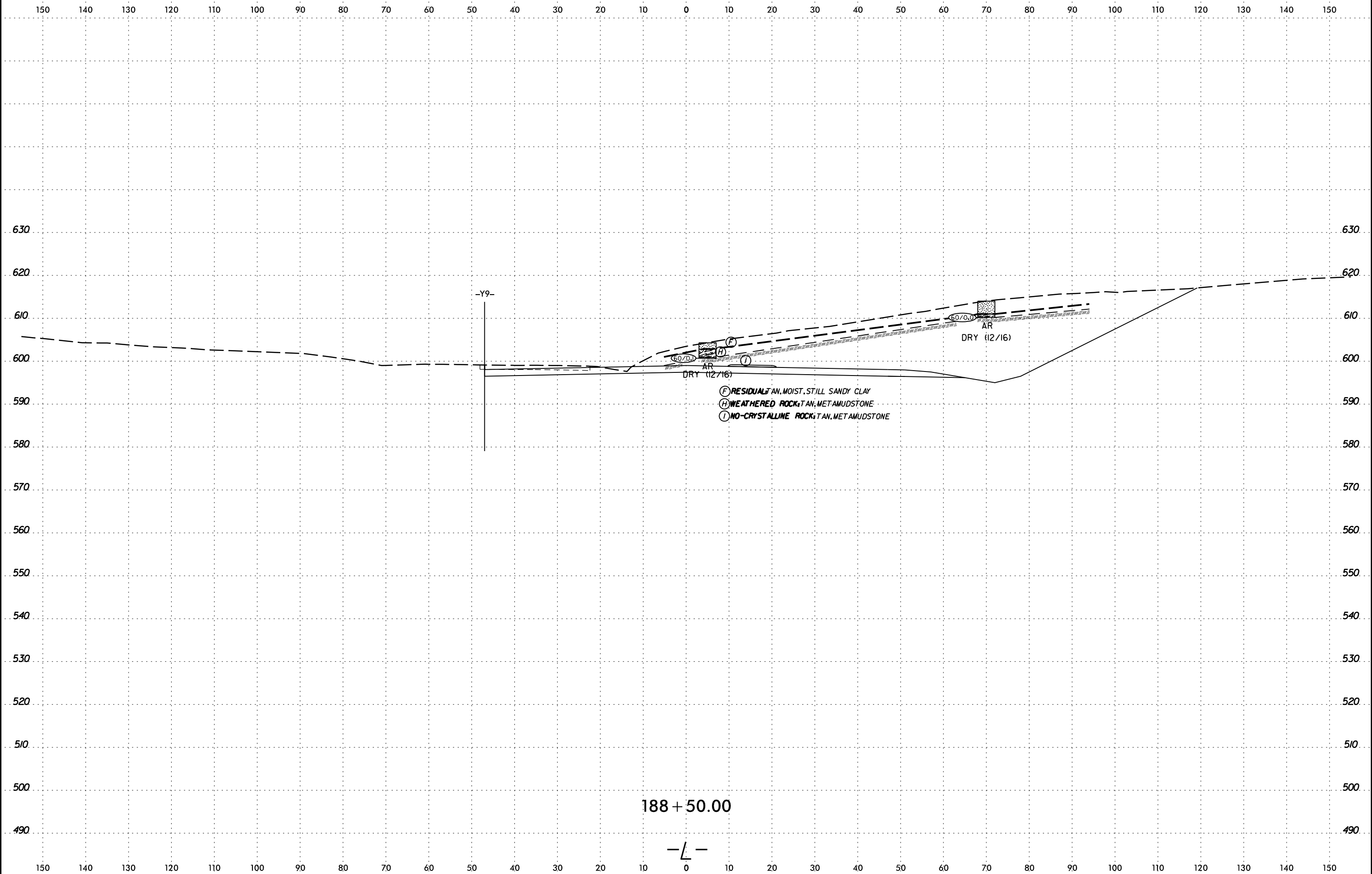
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—L—

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6/23/16
6/23/16



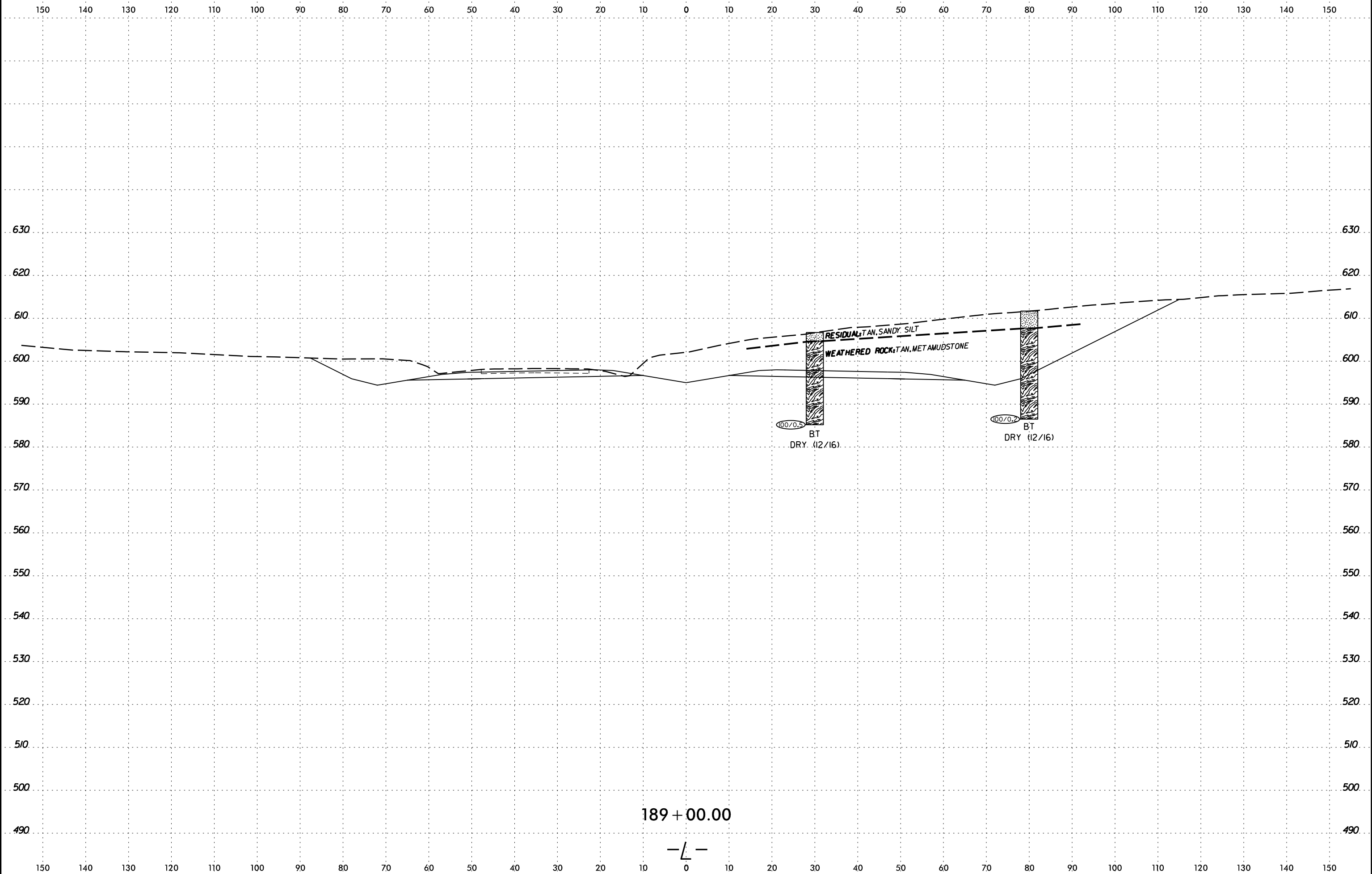
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R-2530B	80



6/23/16



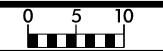
PROJ. REFERENCE NO.	SHEET NO.
R-2530B	81



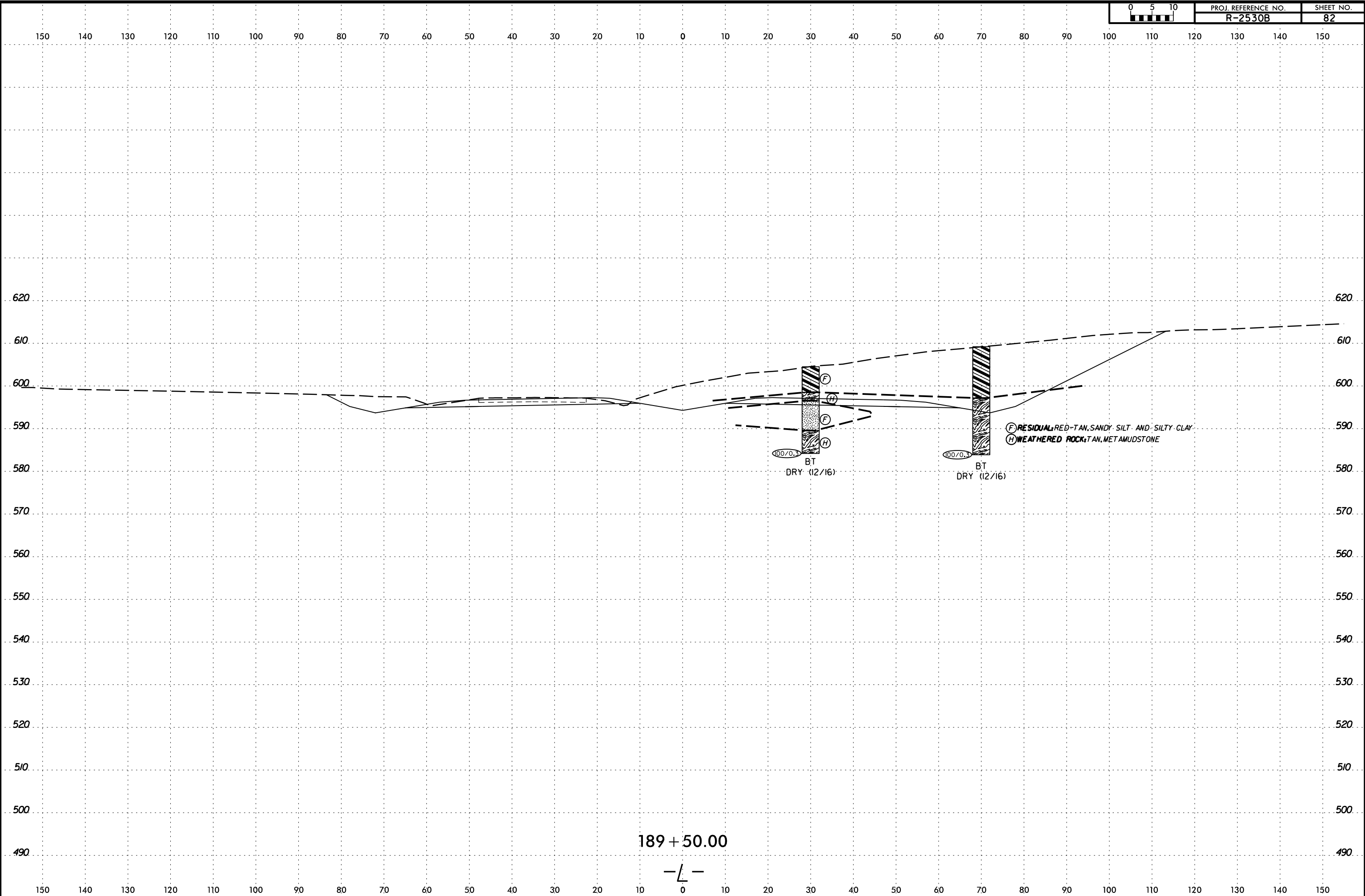
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 cadmachine AI GEO 18

6/23/16

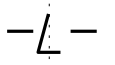
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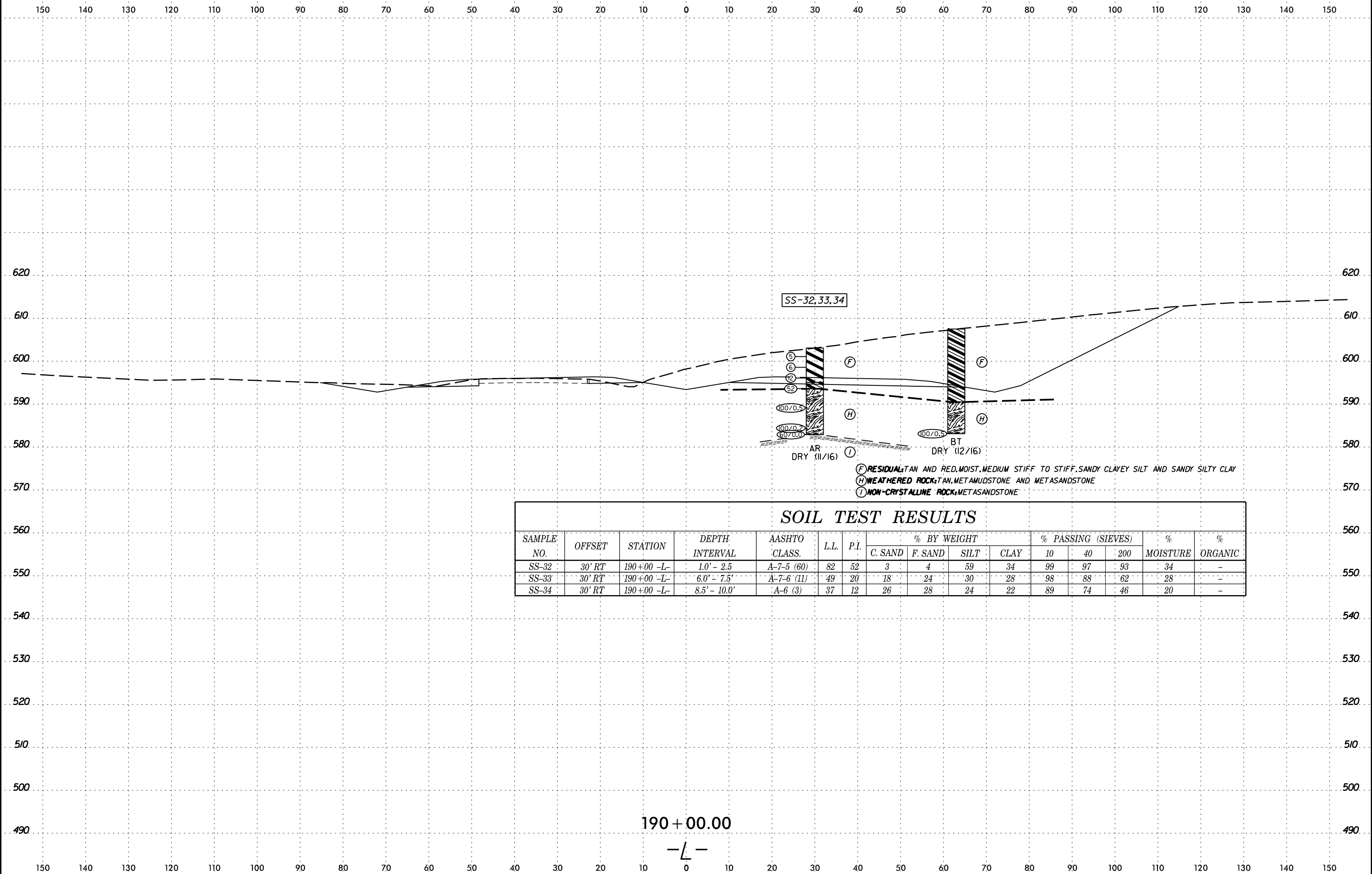
PROJ. REFERENCE NO.	SHEET NO.
R-2530B	82



189+50.00



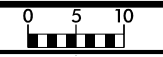
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 6/23/16
 cadmachine AT GEOT-8



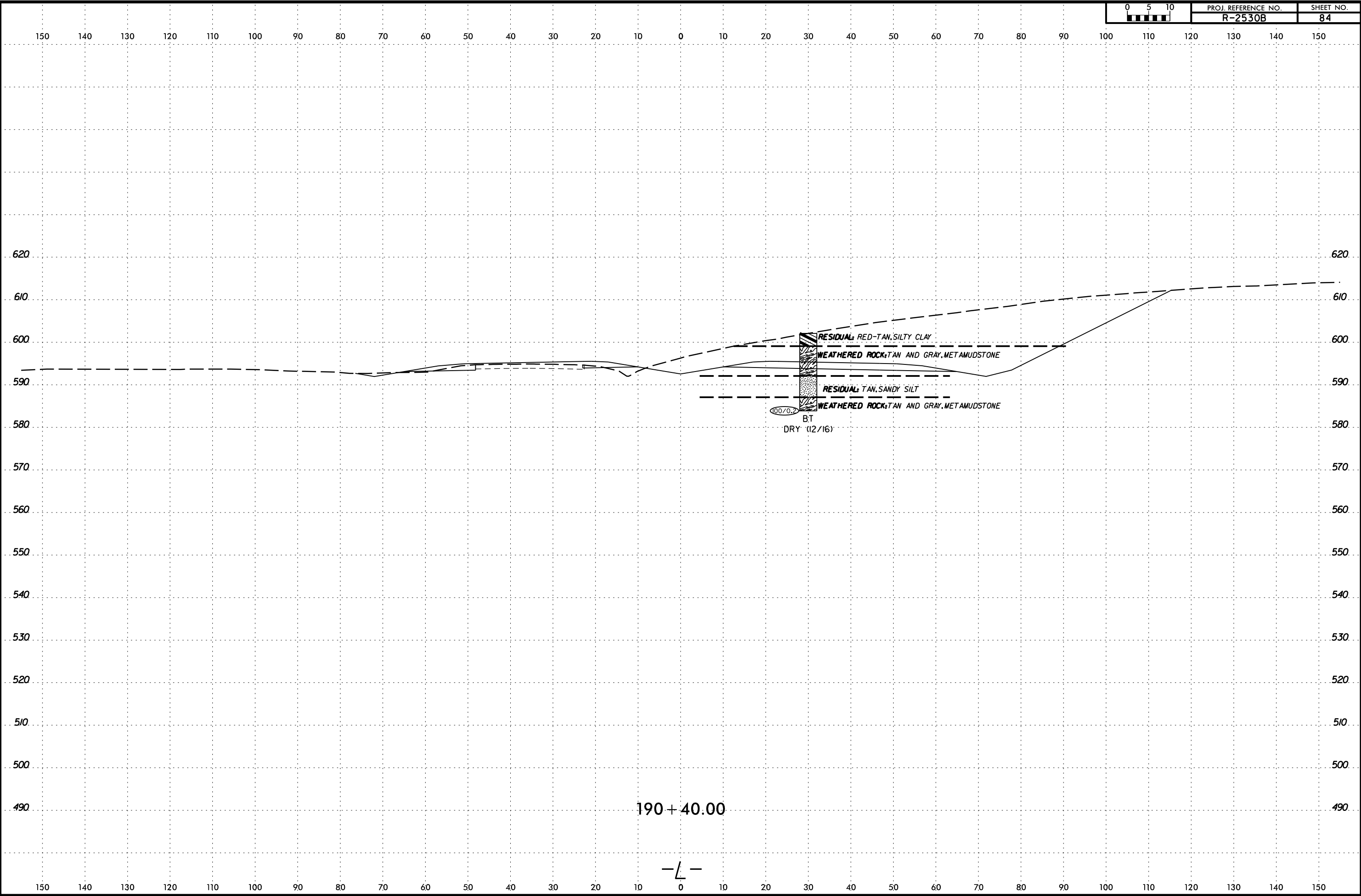
- (F) RESIDUAL TAN AND RED, MOIST, MEDIUM STIFF TO STIFF, SANDY CLAYEY SILT AND SANDY SILTY CLAY
- (H) WEATHERED ROCK, TAN, METAMUDSTONE AND METASANDSTONE
- (I) NON-CRYSTALLINE ROCK, METASANDSTONE

SOIL TEST RESULTS

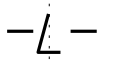
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-32	30' RT	190+00 -L-	1.0' - 2.5'	A-7-5 (60)	82	52	3	4	59	34	99	97	93	34	-
SS-33	30' RT	190+00 -L-	6.0' - 7.5'	A-7-6 (11)	49	20	18	24	30	28	98	88	62	28	-
SS-34	30' RT	190+00 -L-	8.5' - 10.0'	A-6 (3)	37	12	26	28	24	22	89	74	46	20	-



PROJ. REFERENCE NO.	SHEET NO.
R-2530B	84



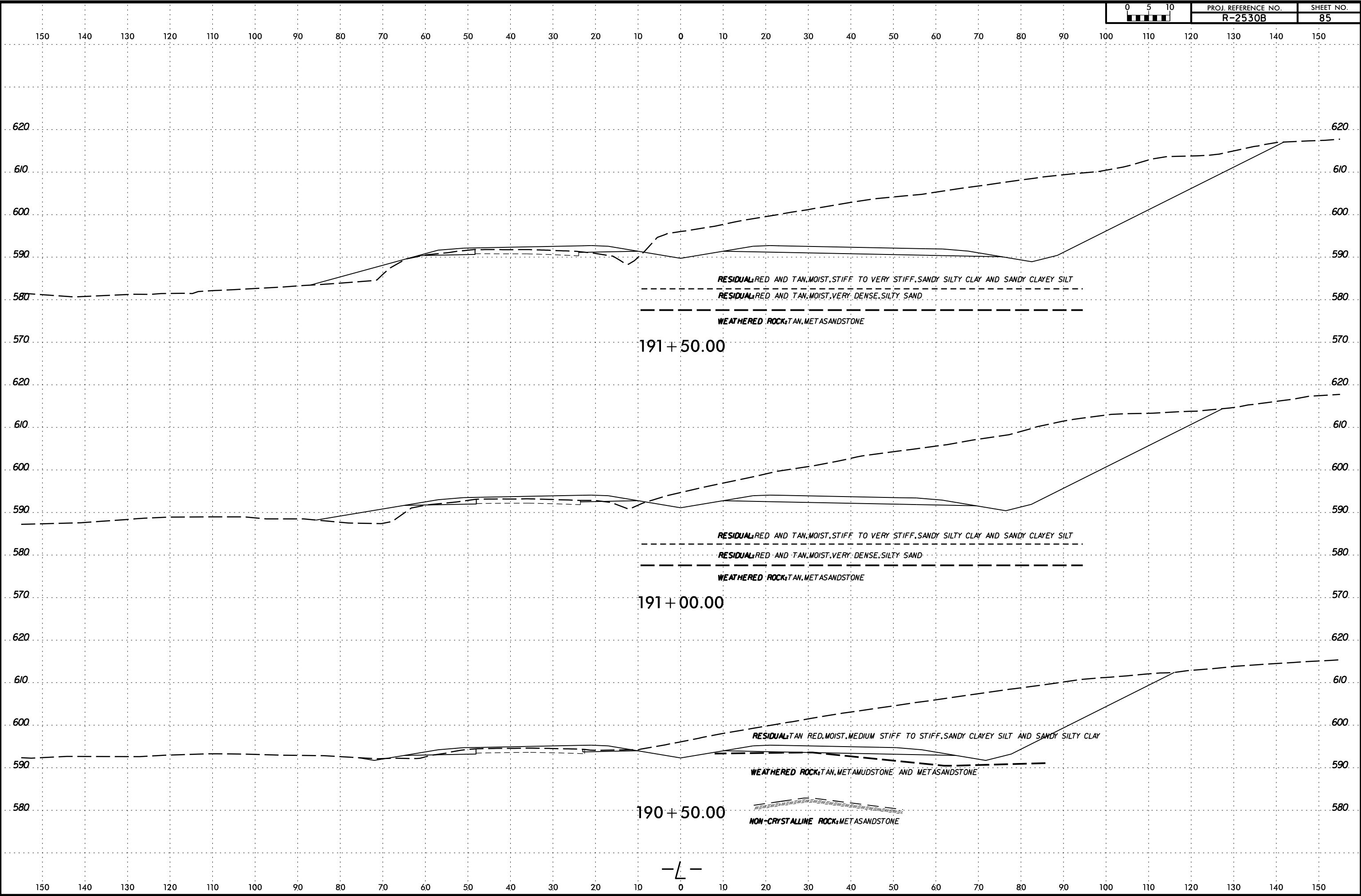
190+40.00



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c:\machine



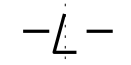
PROJ. REFERENCE NO.	SHEET NO.
R-2530B	85



RESIDUAL RED AND TAN, MOIST, STIFF TO VERY STIFF, SANDY SILTY CLAY AND SANDY CLAYEY SILT
RESIDUAL RED AND TAN, MOIST, VERY DENSE, SILTY SAND
WEATHERED ROCK, TAN, METASANDSTONE

RESIDUAL RED AND TAN, MOIST, STIFF TO VERY STIFF, SANDY SILTY CLAY AND SANDY CLAYEY SILT
RESIDUAL RED AND TAN, MOIST, VERY DENSE, SILTY SAND
WEATHERED ROCK, TAN, METASANDSTONE

RESIDUAL TAN RED, MOIST, MEDIUM STIFF TO STIFF, SANDY CLAYEY SILT AND SANDY SILTY CLAY
WEATHERED ROCK, TAN, METAMUDSTONE, AND METASANDSTONE
NON-CRYSTALLINE ROCK, METASANDSTONE



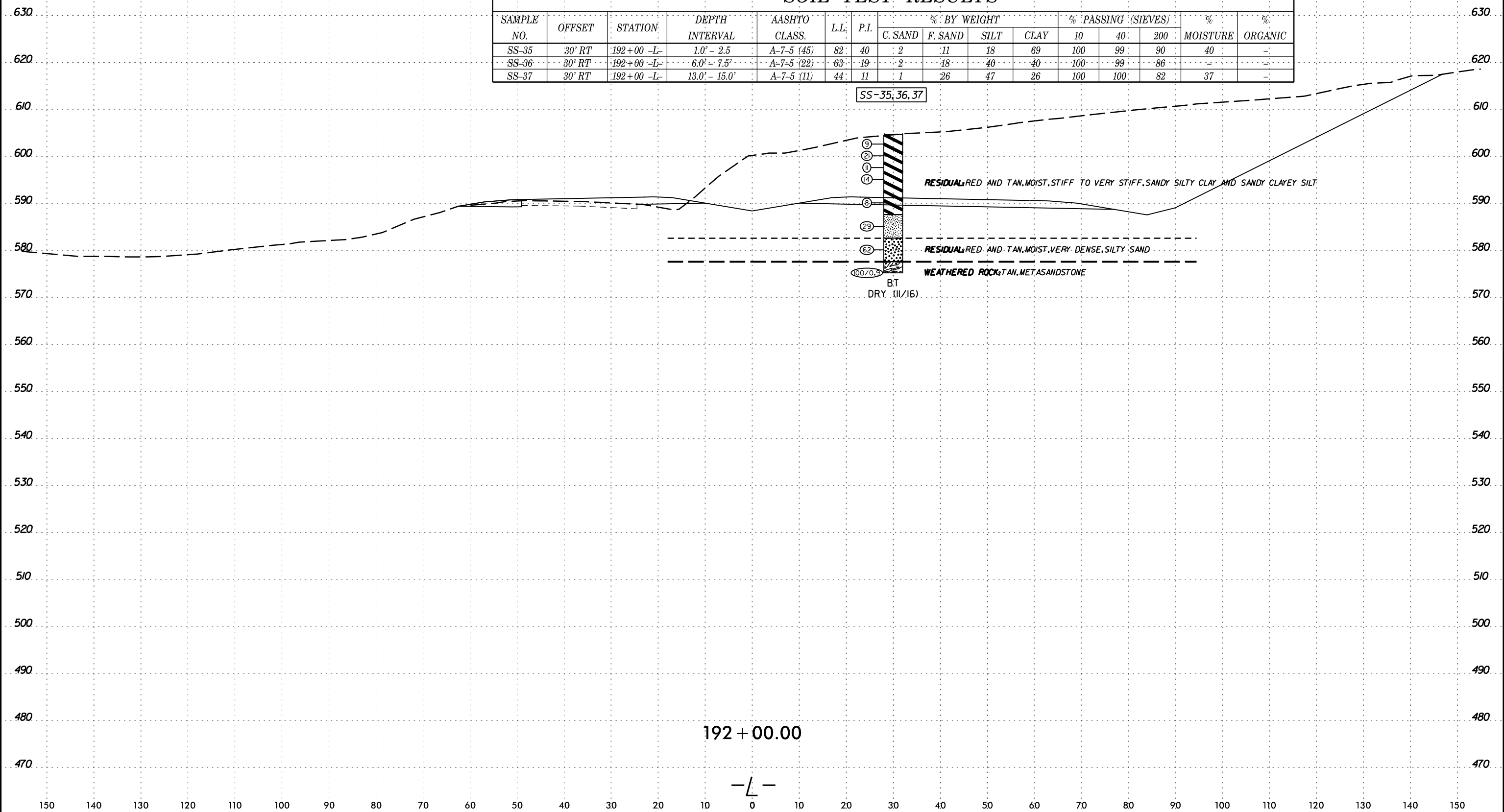
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 cadmachine AT GEOI-8



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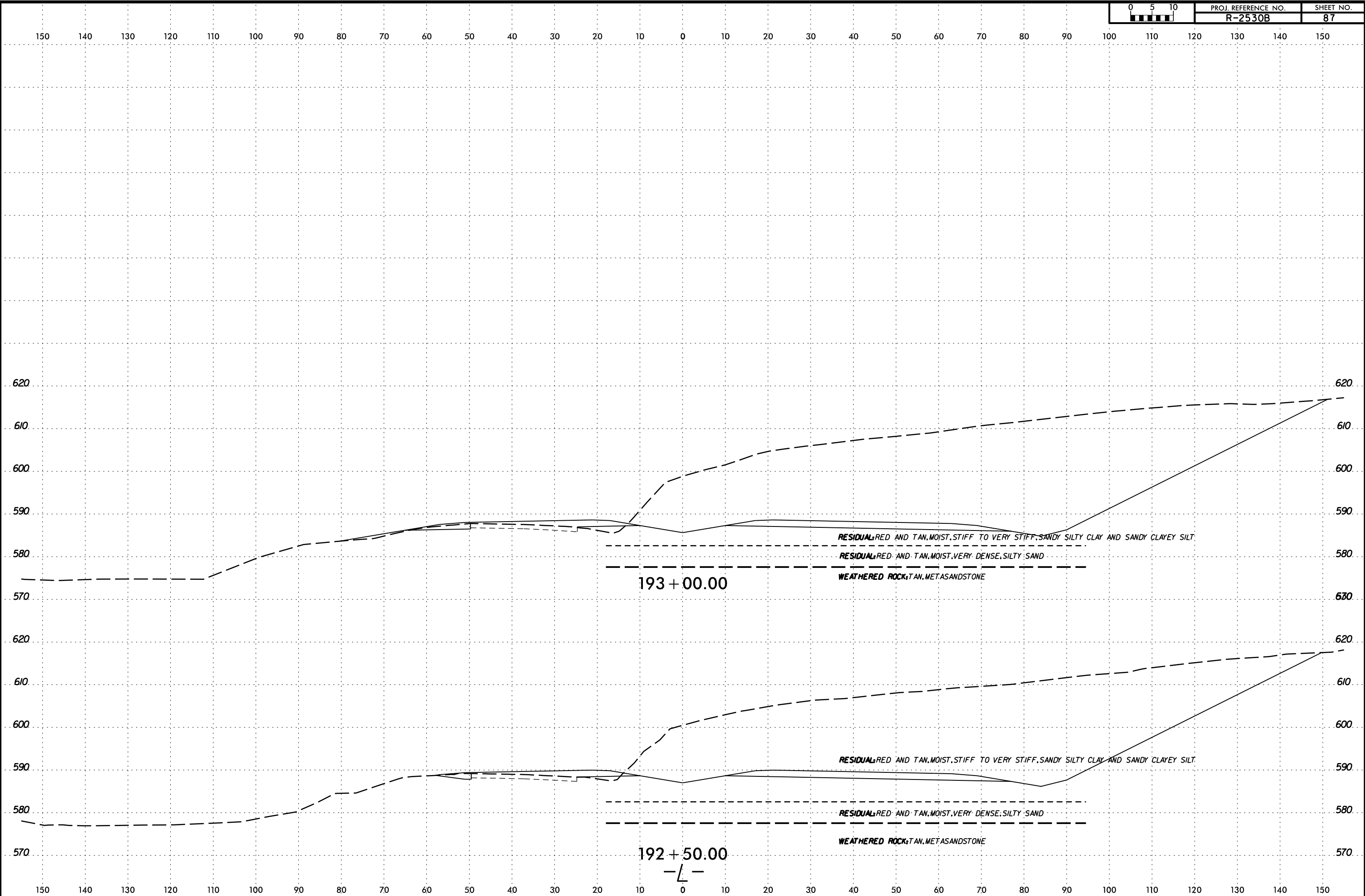
SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-35	30' RT	192+00 -L-	1.0' - 2.5'	A-7-5 (45)	82	40	2	11	18	69	100	99	90	40	-
SS-36	30' RT	192+00 -L-	6.0' - 7.5'	A-7-5 (22)	63	19	2	18	40	40	100	99	86	-	-
SS-37	30' RT	192+00 -L-	13.0' - 15.0'	A-7-5 (11)	44	11	1	26	47	26	100	100	82	37	-

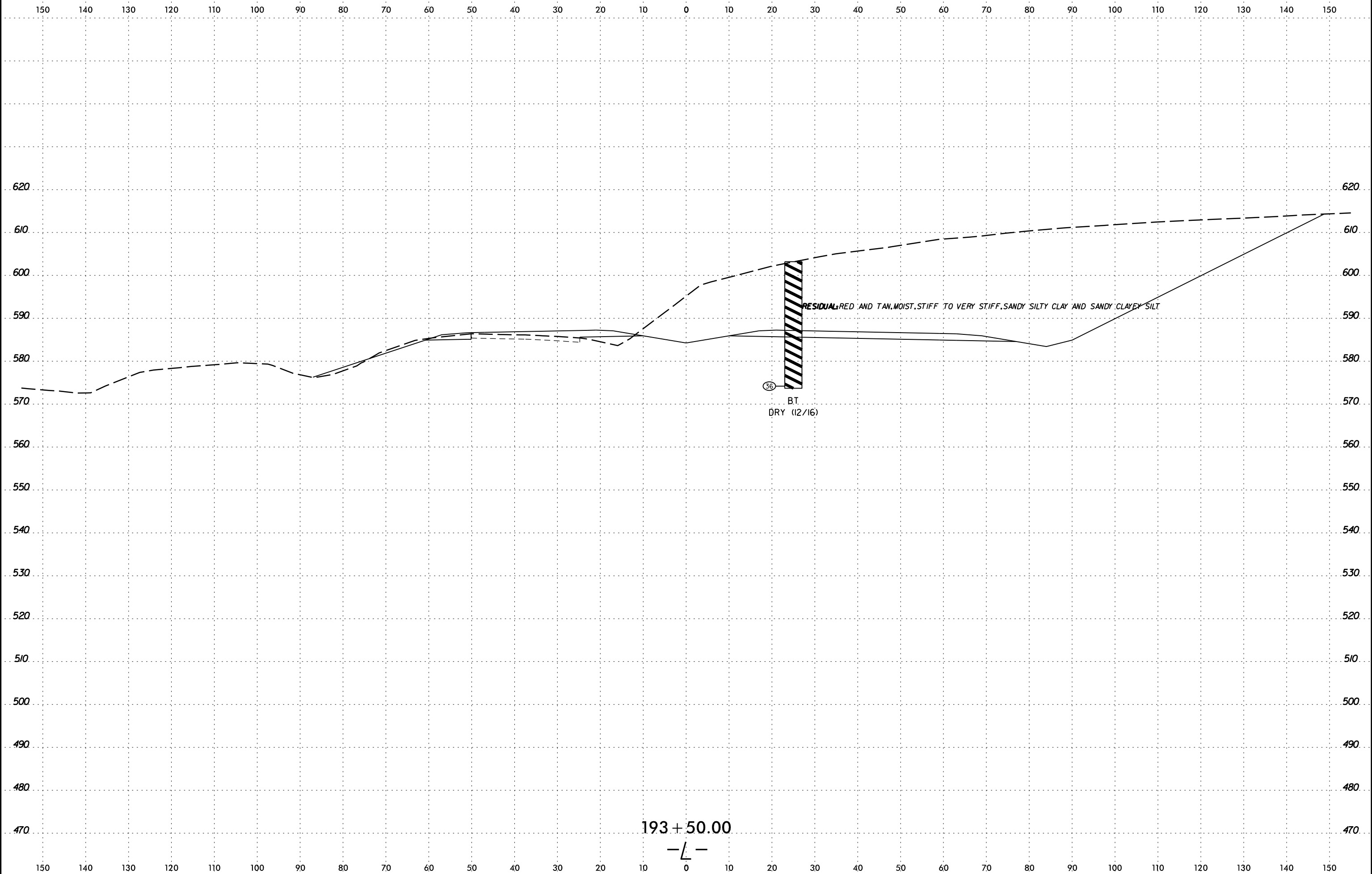
SS-35, 36, 37



192 + 00.00

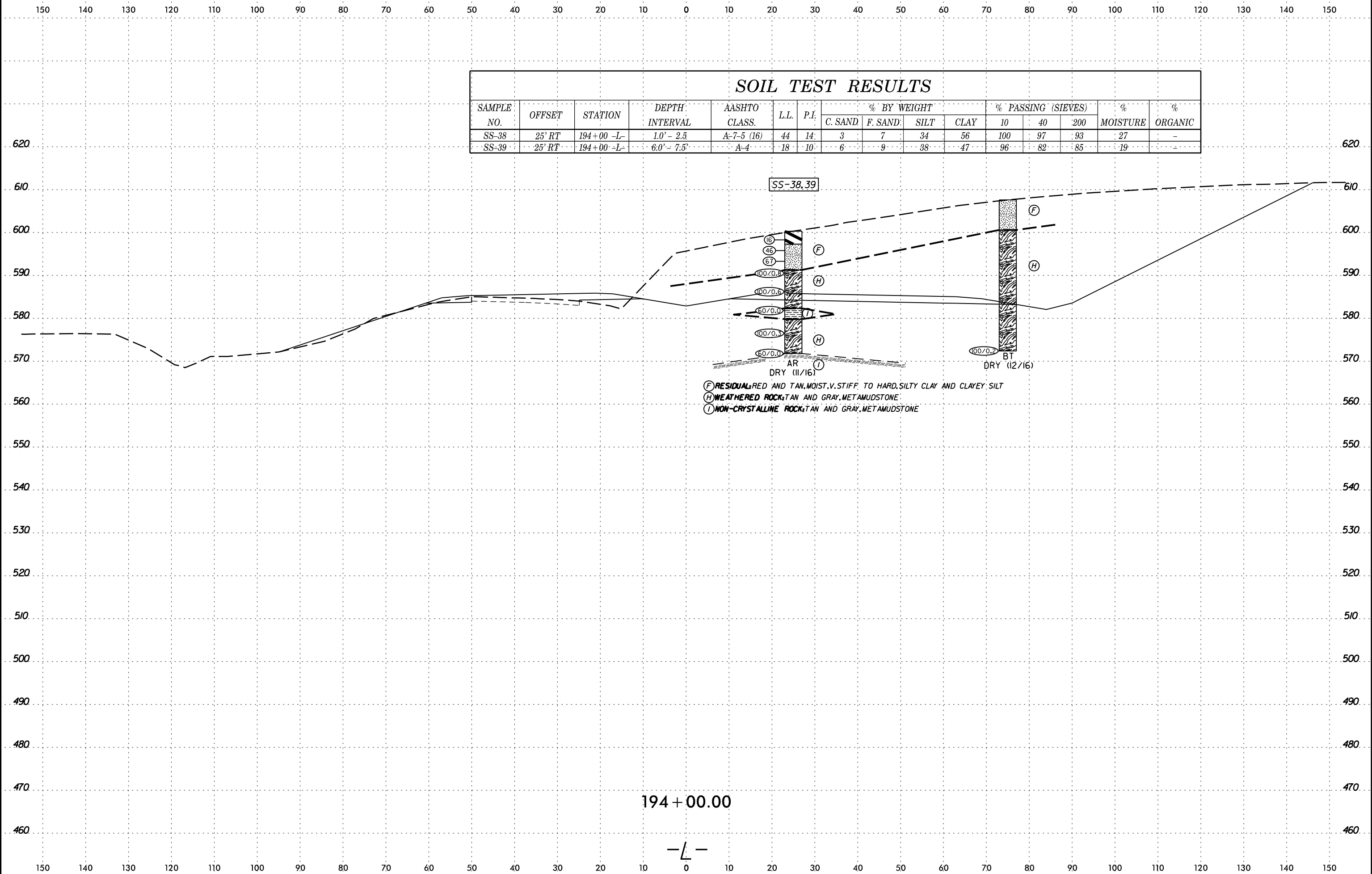
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 cadmachine AI GEO1-8

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 6/23/16
 cadmachine AI GEO-18



SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-38	25' RT	194+00 -L-	1.0' - 2.5'	A-7-5 (16)	44	14	3	7	34	56	100	97	93	27	-
SS-39	25' RT	194+00 -L-	6.0' - 7.5'	A-4	18	10	6	9	38	47	96	82	85	19	-

- (F) RESIDUAL RED AND TAN, MOIST, V. STIFF TO HARD, SILTY CLAY AND CLAYEY SILT
- (H) WEATHERED ROCK, TAN AND GRAY, METAMUDSTONE
- (I) NON-CRYSTALLINE ROCK, TAN AND GRAY, METAMUDSTONE

194 + 00.00

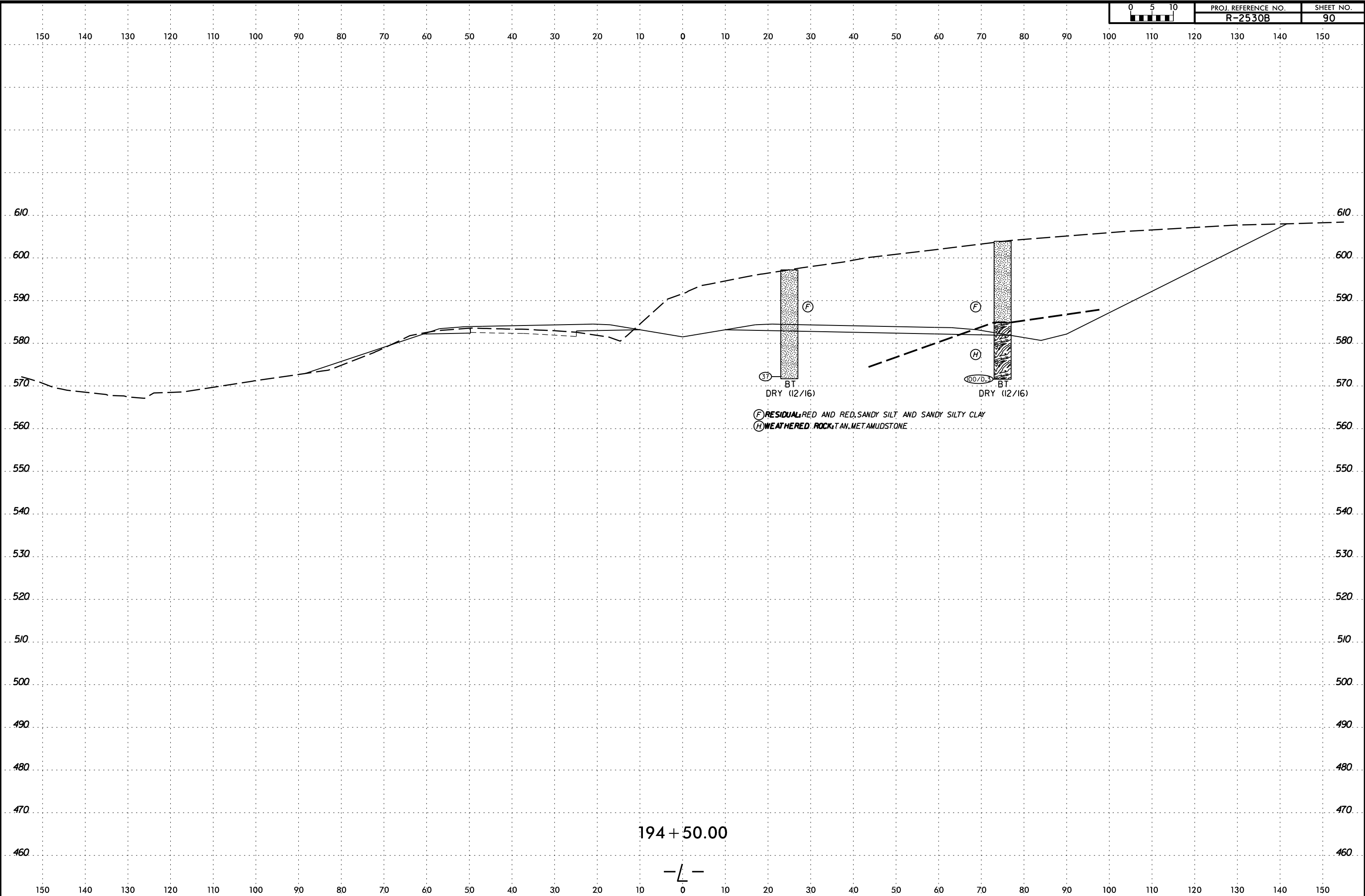
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6/23/16



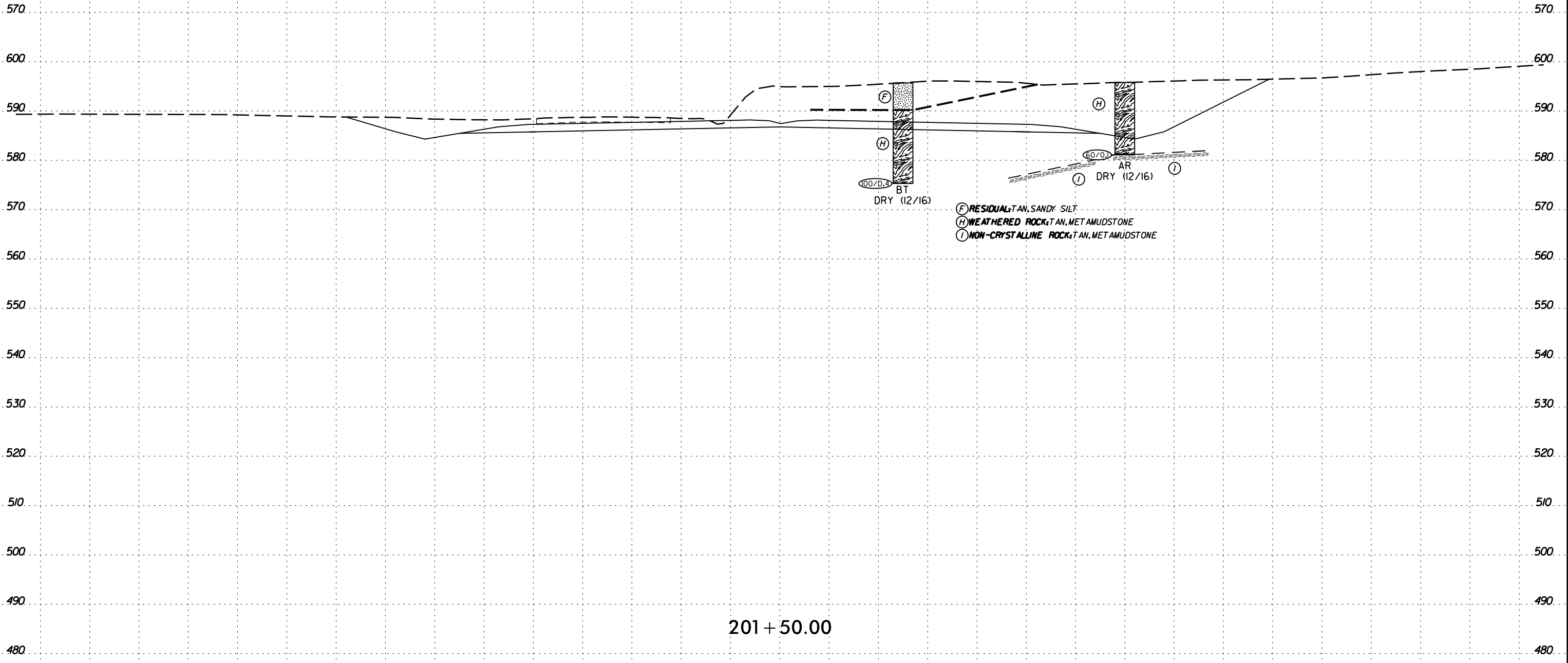
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R-2530B	90

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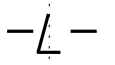




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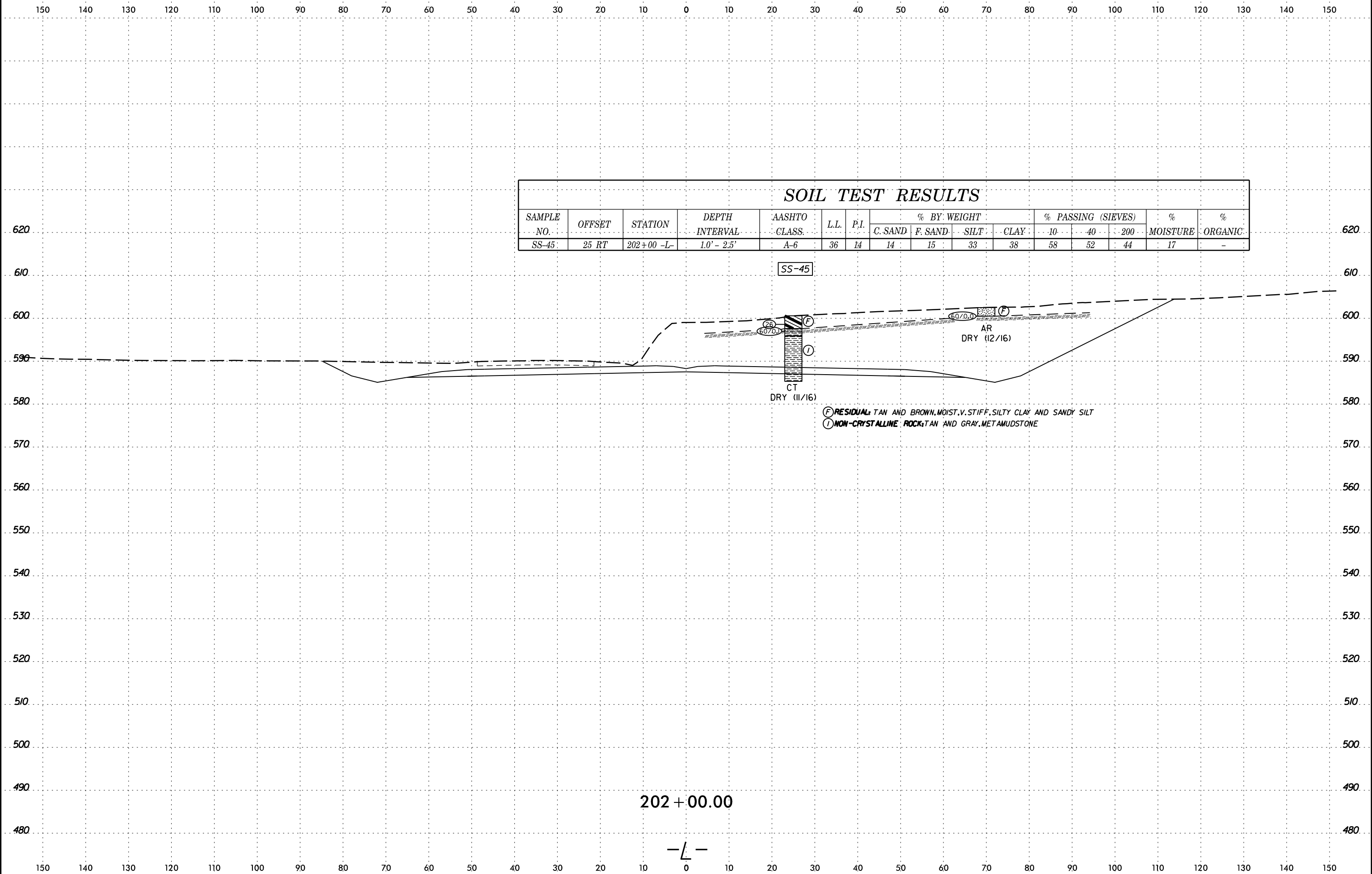


201 + 50.00



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 6/23/16
 cadmachine AI GEO-18



SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	-10	-40	-200		
SS-45	25 RT	202+00 -L-	1.0' - 2.5'	A-6	36	14	14	15	33	38	58	52	44	17	-

SS-45

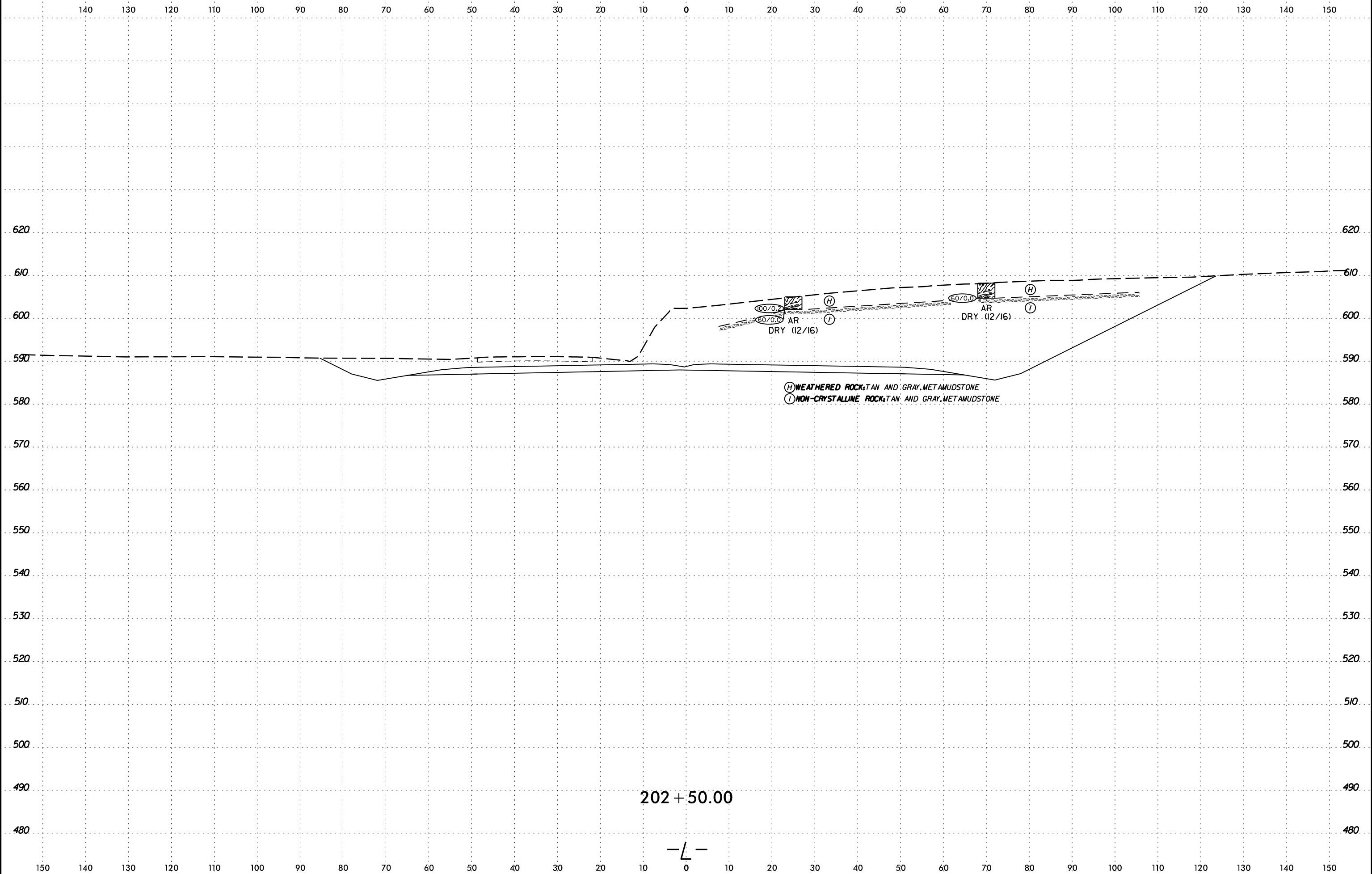
(28)
 (60/0.0)
 (F)
 (L)
 CT
 DRY (11/16)

(60/0.0)
 (F)
 AR
 DRY (12/16)

- (F) RESIDUAL TAN AND BROWN, MOIST, V. STIFF, SILTY CLAY AND SANDY SILT
- (L) NON-CRYSTALLINE ROCK, TAN AND GRAY, METAMUDSTONE

202+00.00

-L-



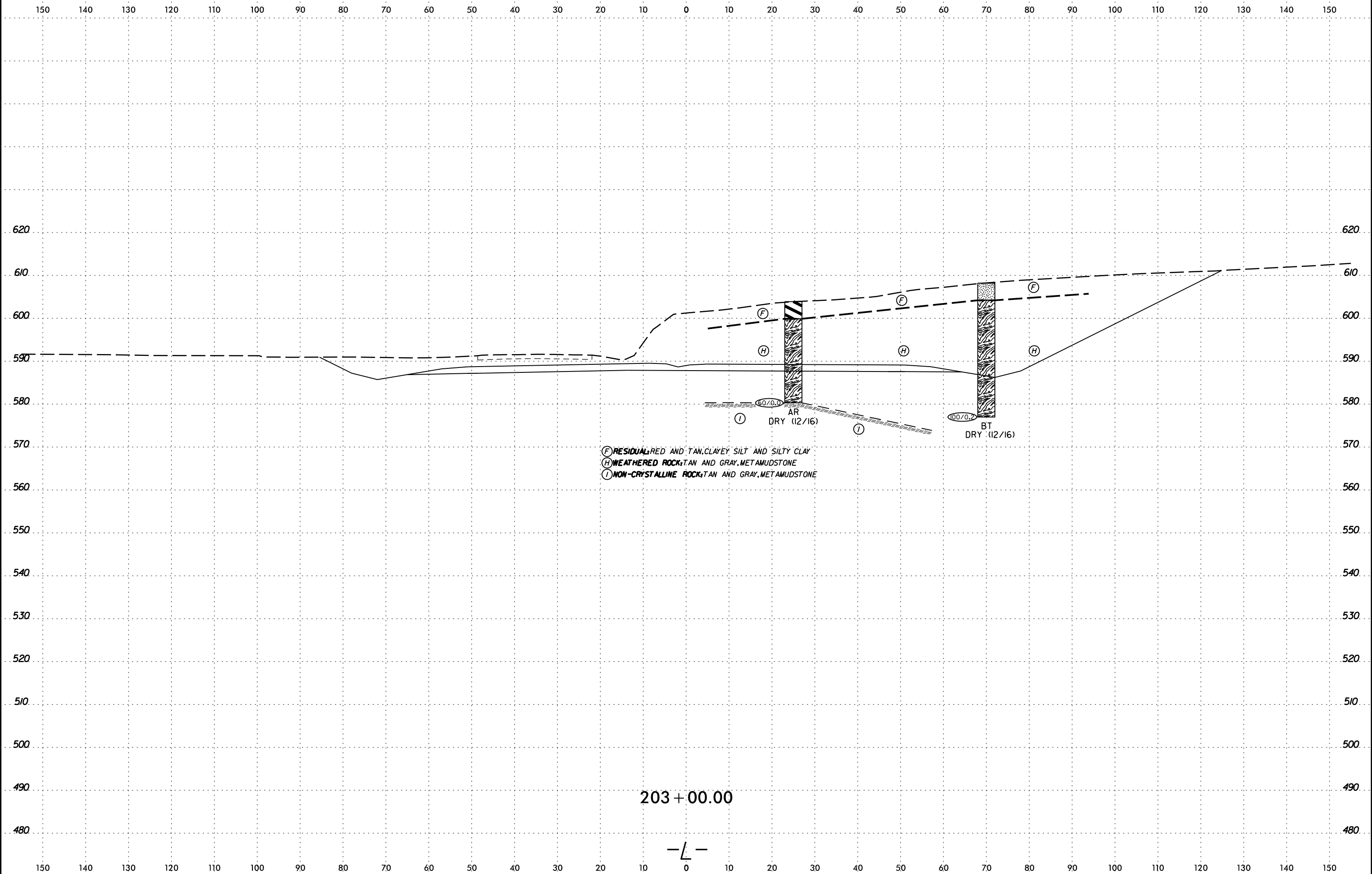
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 cadmachine AI GEO-18

6/23/16

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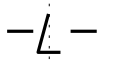


PROJ. REFERENCE NO.	SHEET NO.
R-2530B	94



- (F) RESIDUAL, RED AND TAN, CLAYEY SILT AND SILTY CLAY
- (H) WEATHERED ROCK, TAN AND GRAY, METAMUDSTONE
- (L) NON-CRYSTALLINE ROCK, TAN AND GRAY, METAMUDSTONE

203+00.00

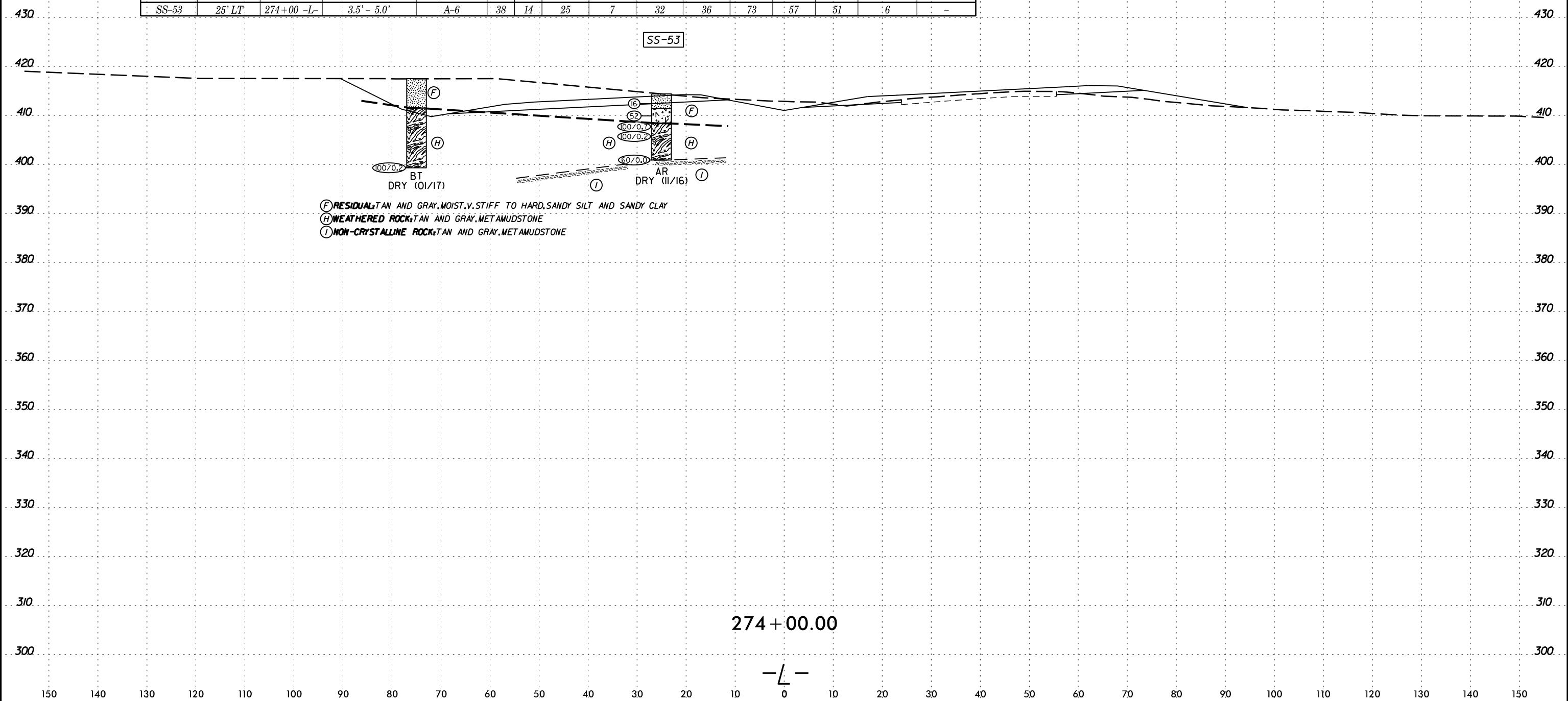


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SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-53	25' LT	274+00 -L-	3.5' - 5.0'	A-6	38	14	25	7	32	36	73	57	51	6	-

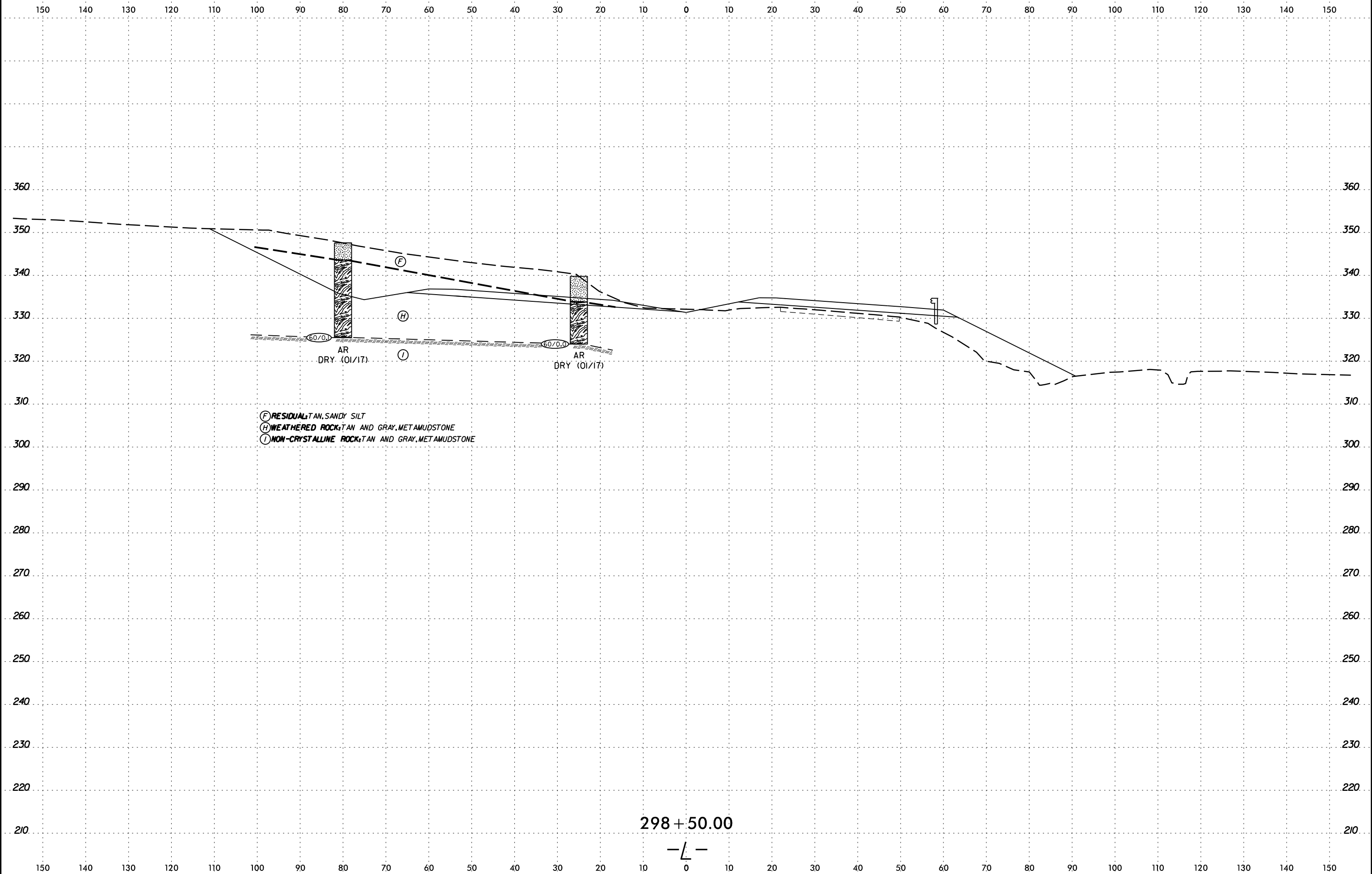
SS-53



- (F) RESIDUAL TAN AND GRAY, MOIST, V. STIFF TO HARD, SANDY SILT AND SANDY CLAY
- (H) WEATHERED ROCK, TAN AND GRAY, METAMUDSTONE
- (I) NON-CRYSTALLINE ROCK, TAN AND GRAY, METAMUDSTONE

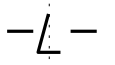
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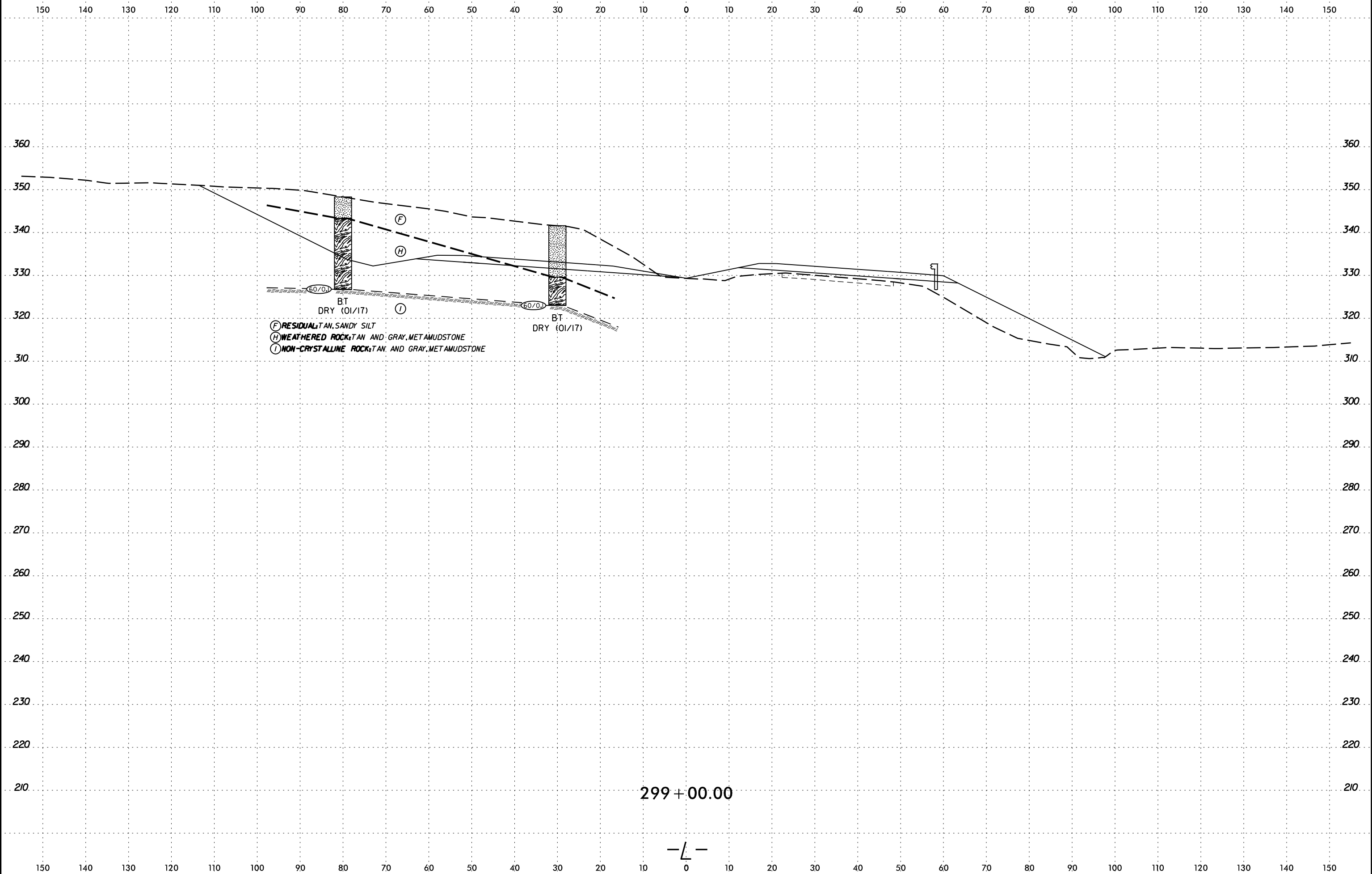
-L-



- (F) RESIDUAL TAN, SANDY SILT
- (H) WEATHERED ROCK TAN AND GRAY, METAMUDSTONE
- (L) NON-CRYSTALLINE ROCK TAN AND GRAY, METAMUDSTONE

298+50.00





BT
DRY (01/17)

BT
DRY (01/17)

(F) RESIDUAL TAN. SANDY SILT
(H) WEATHERED ROCK, TAN AND GRAY, METAMUDSTONE
(I) NON-CRYSTALLINE ROCK, TAN AND GRAY, METAMUDSTONE

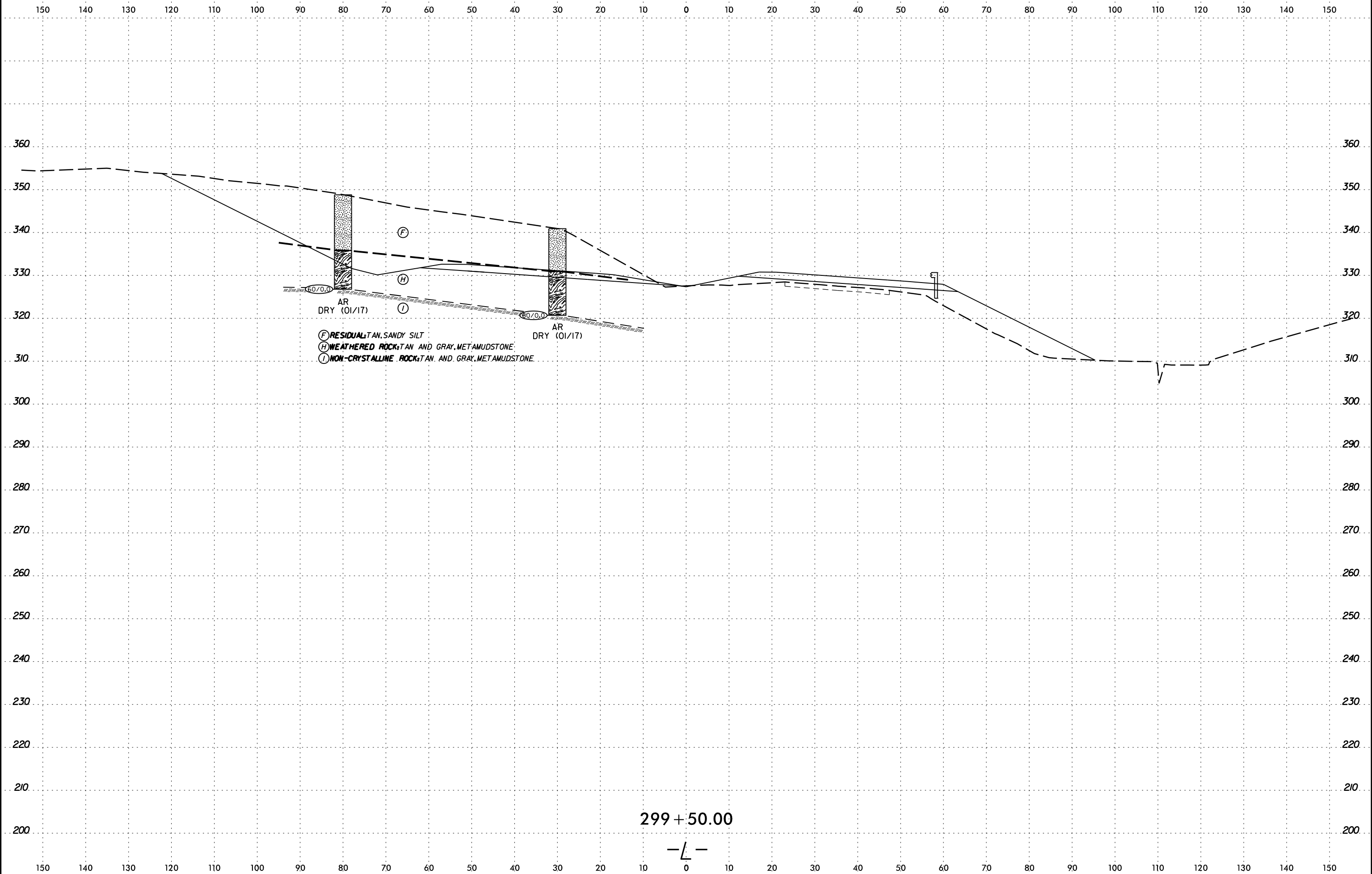
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-L-

6/23/16



PROJ. REFERENCE NO.	SHEET NO.
R-2530B	99



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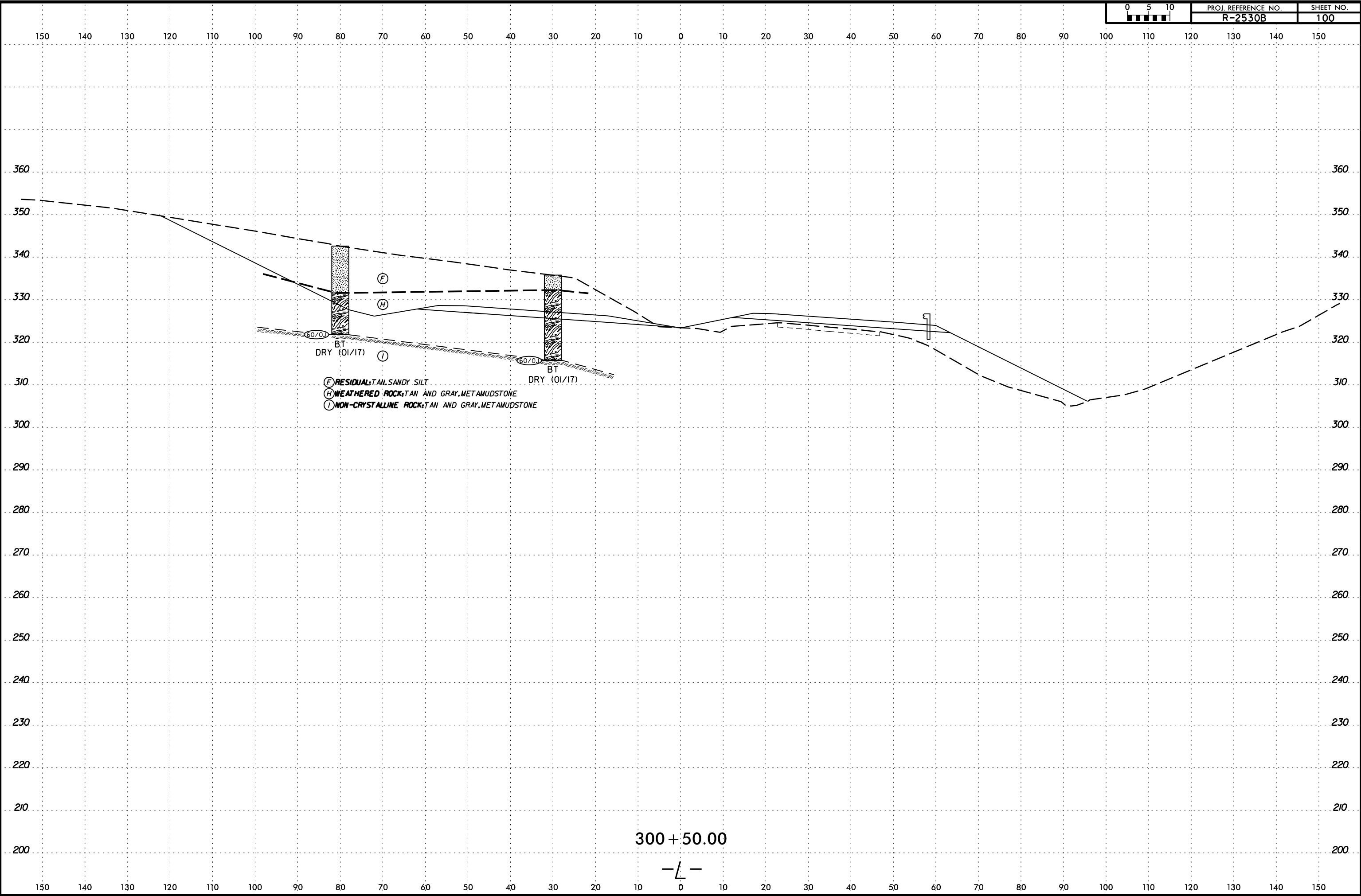
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-L-

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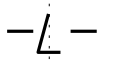


PROJ. REFERENCE NO.	SHEET NO.
R-2530B	100



- (F) RESIDUAL TAN, SANDY SILT
- (H) WEATHERED ROCK TAN AND GRAY, METAMUDSTONE
- (I) NON-CRYSTALLINE ROCK TAN AND GRAY, METAMUDSTONE

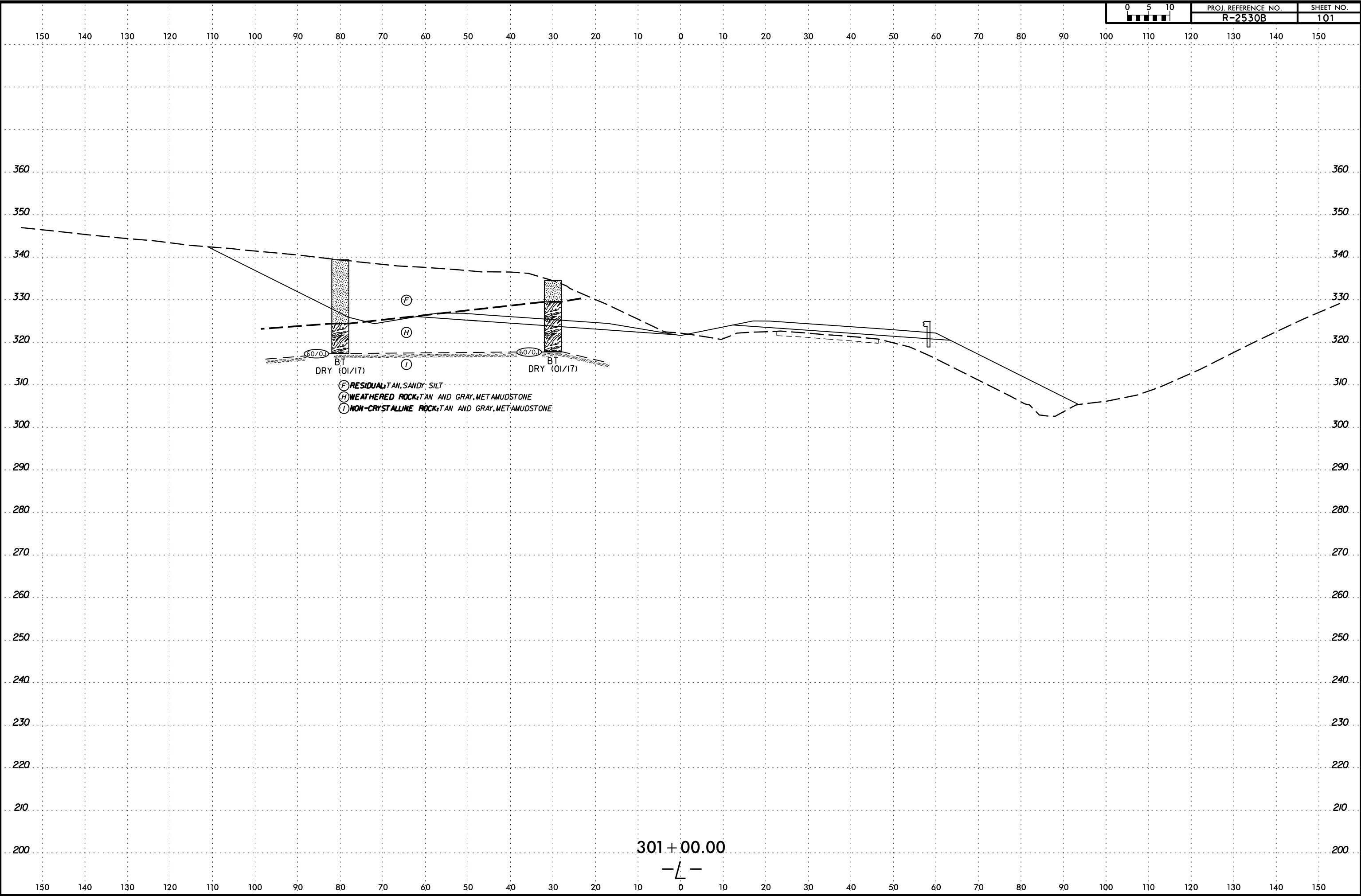
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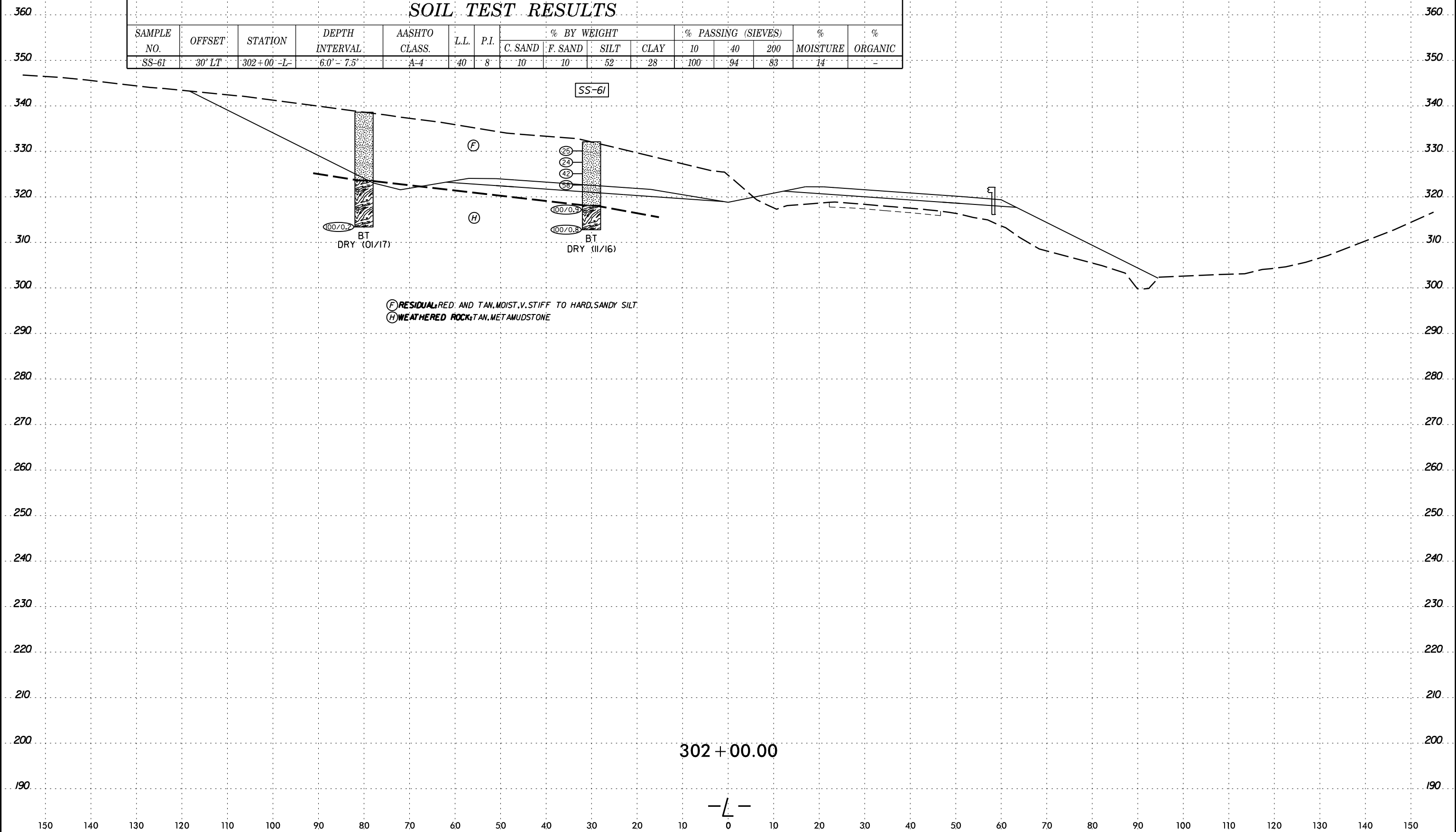
PROJ. REFERENCE NO.	SHEET NO.
R-2530B	101



301+00.00
-L-

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-61	30' LT	302+00 -L-	6.0' - 7.5'	A-4	40	8	10	10	52	28	100	94	83	14	-

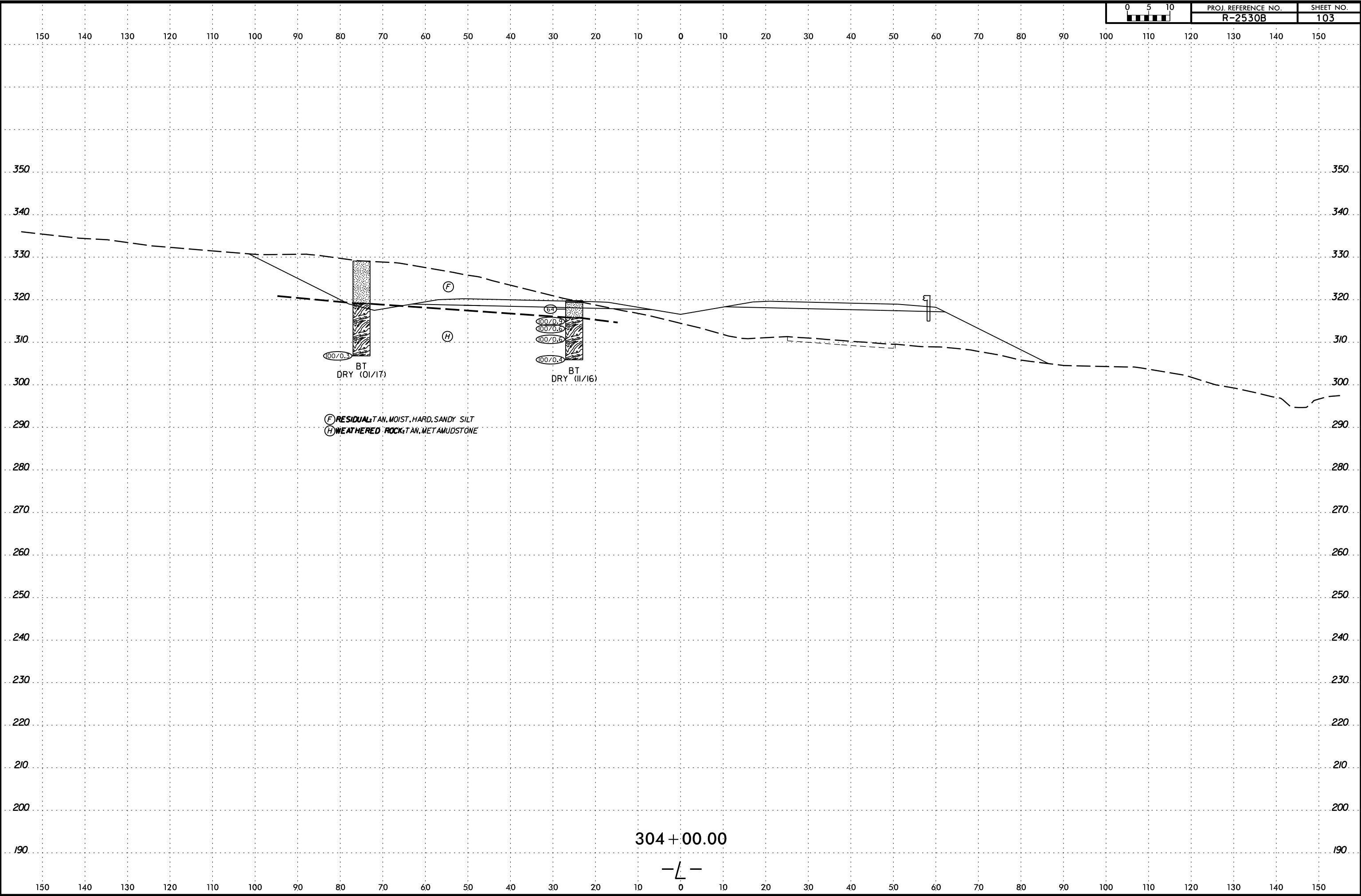


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PROJ. REFERENCE NO.	SHEET NO.
R-2530B	103

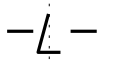


BT
DRY (01/17)

BT
DRY (11/16)

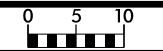
(F) RESIDUAL TAN. MOIST. HARD. SANDY SILT
(H) WEATHERED ROCK TAN. METAMUDSTONE

304+00.00

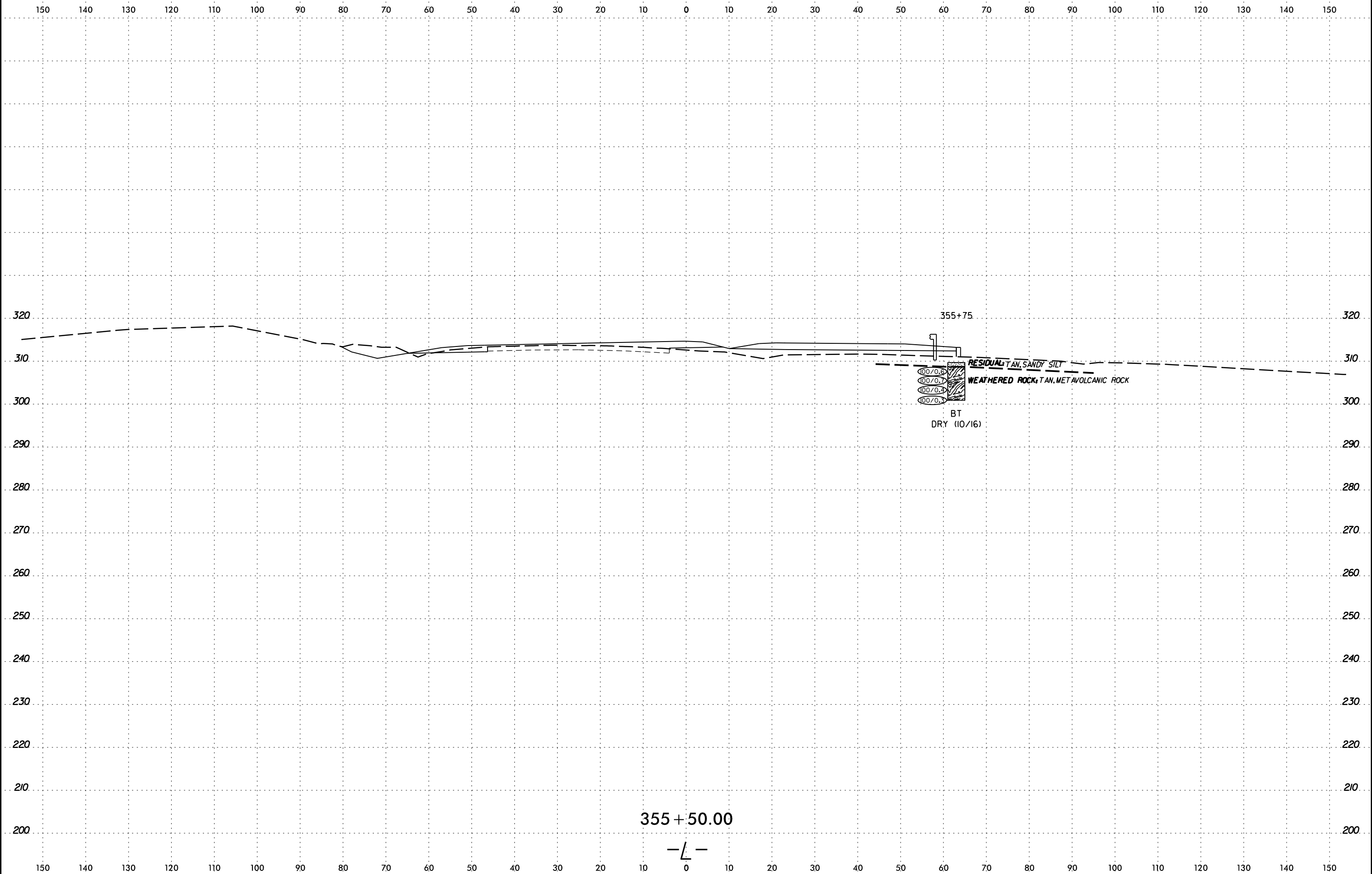


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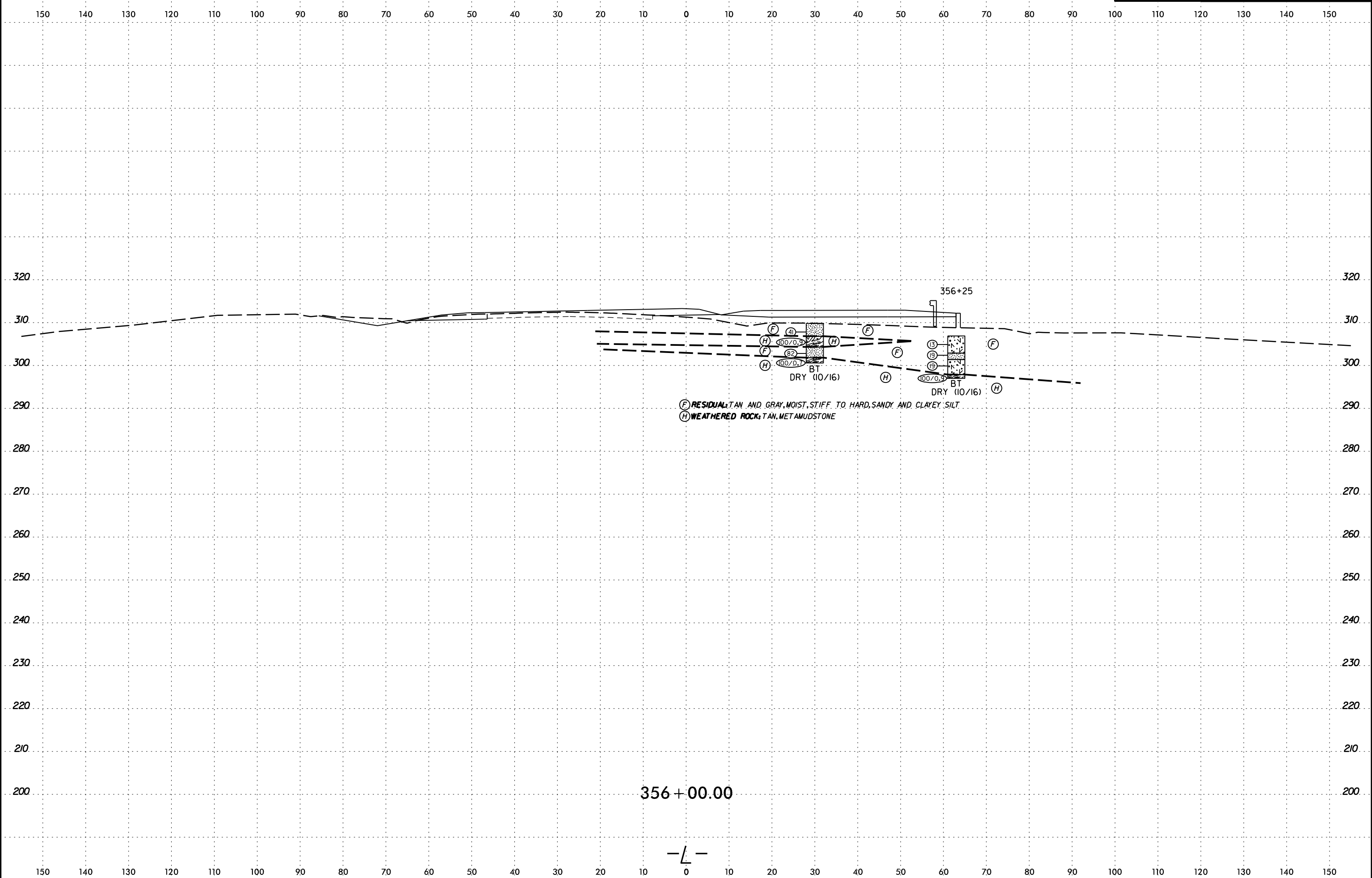


PROJ. REFERENCE NO.	SHEET NO.
U-2530B	104



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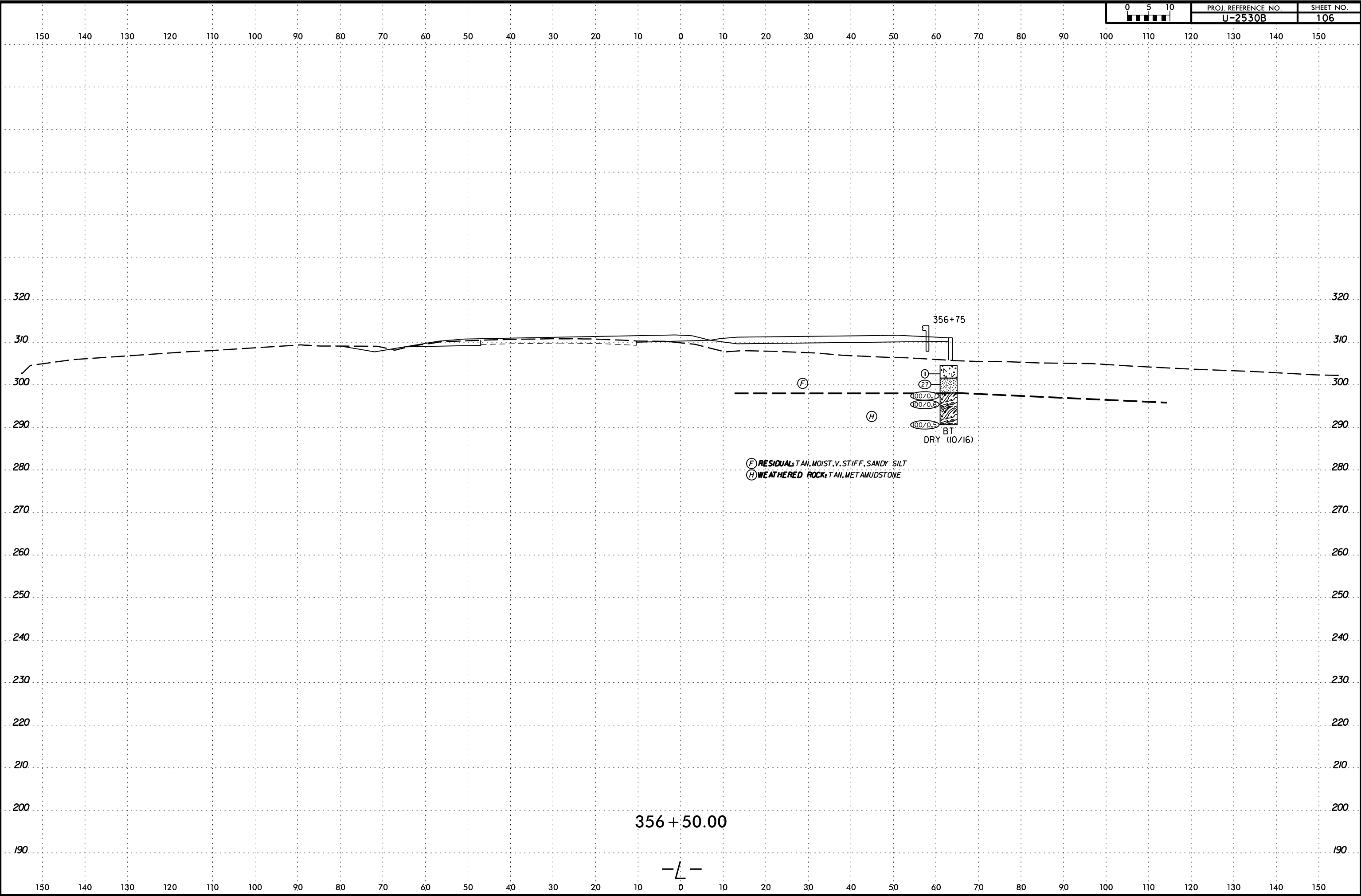
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6/23/16



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PROJ. REFERENCE NO.	SHEET NO.
U-2530B	106



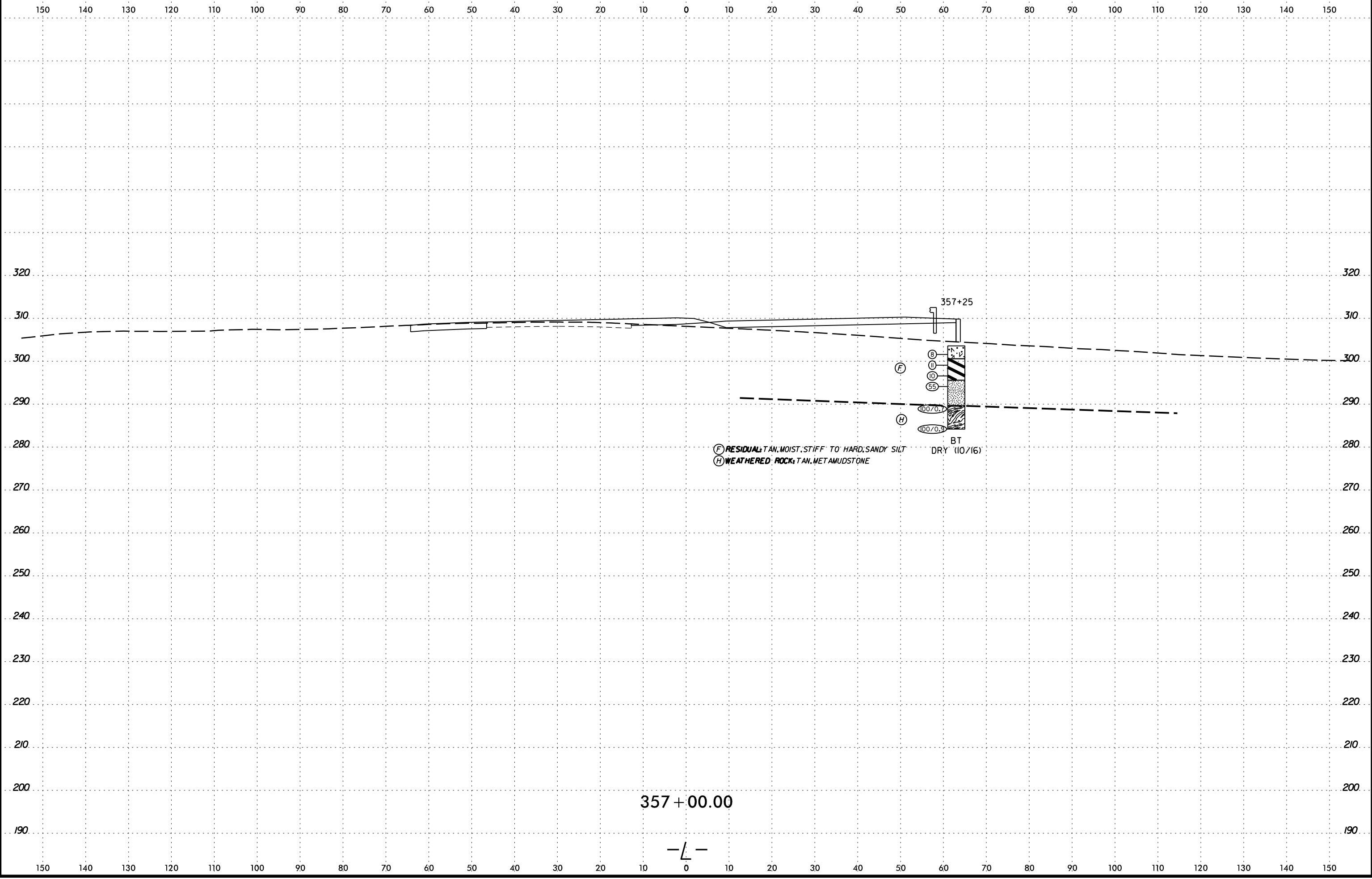
- (F) RESIDUAL TAN, MOIST, V. STIFF, SANDY SILT
- (H) WEATHERED ROCK, TAN, METAMUDSTONE

BT
DRY (10/16)

356+50.00

-L-

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6/23/16
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6/23/16



(F) RESIDUAL TAN. MOIST. STIFF TO HARD. SANDY SILT
(H) WEATHERED ROCK TAN. METAMUDSTONE

357+25

BT
DRY (10/16)

357+00.00

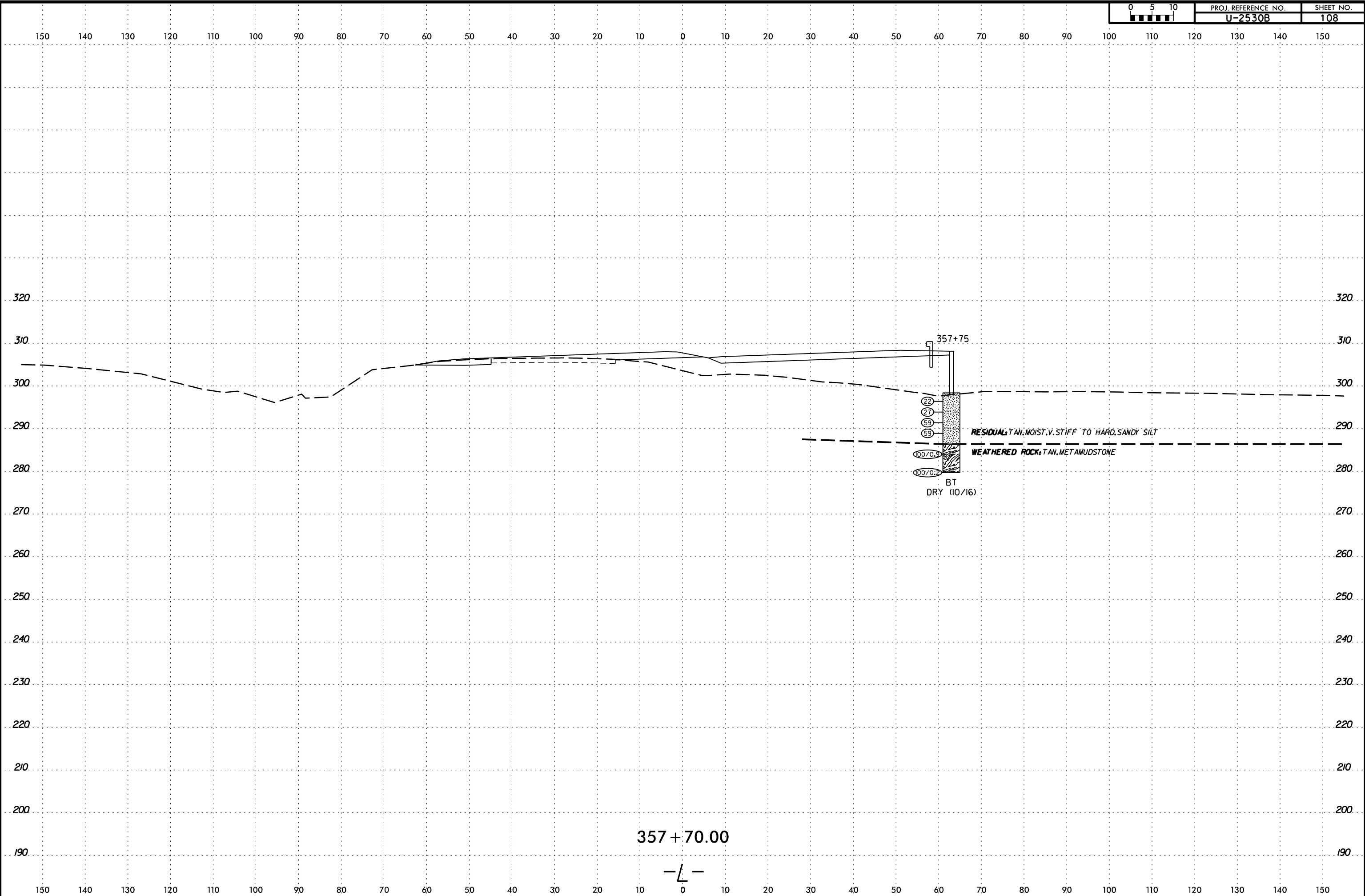
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6/23/16



PROJ. REFERENCE NO.	SHEET NO.
U-2530B	108

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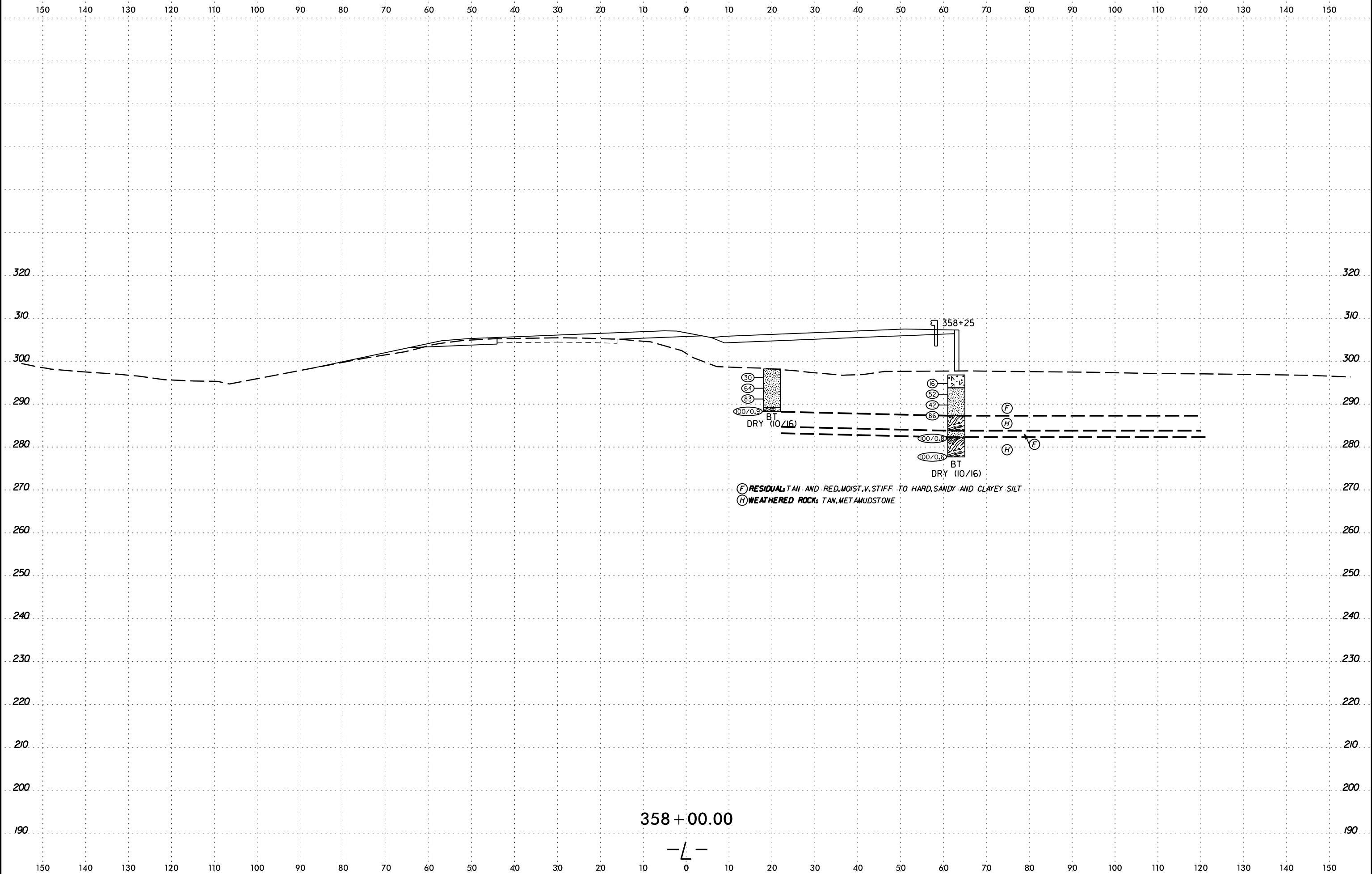
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6/23/16

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PROJ. REFERENCE NO.	SHEET NO.
U-2530B	109



358+00.00

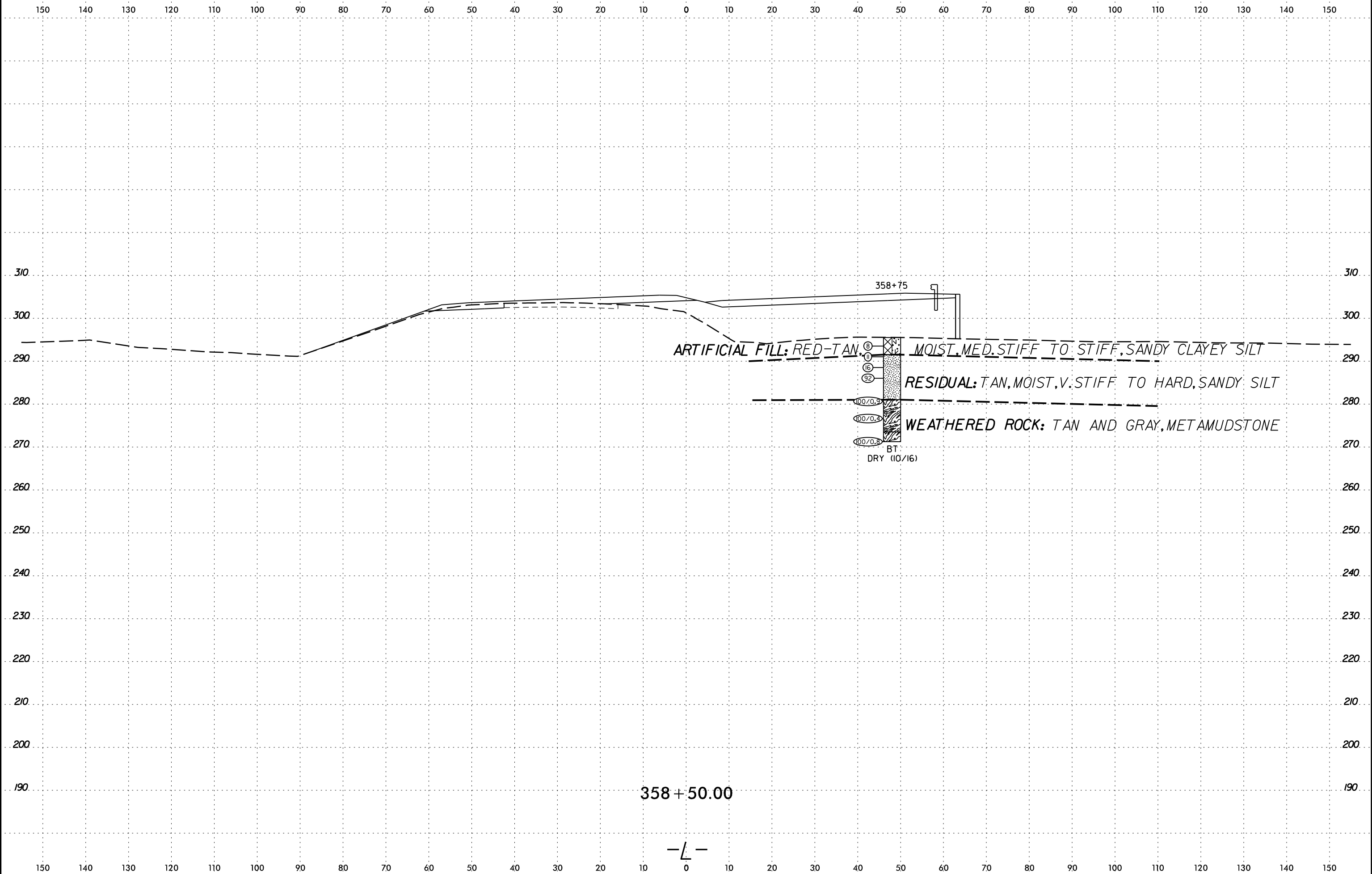
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6/23/16

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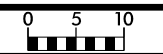


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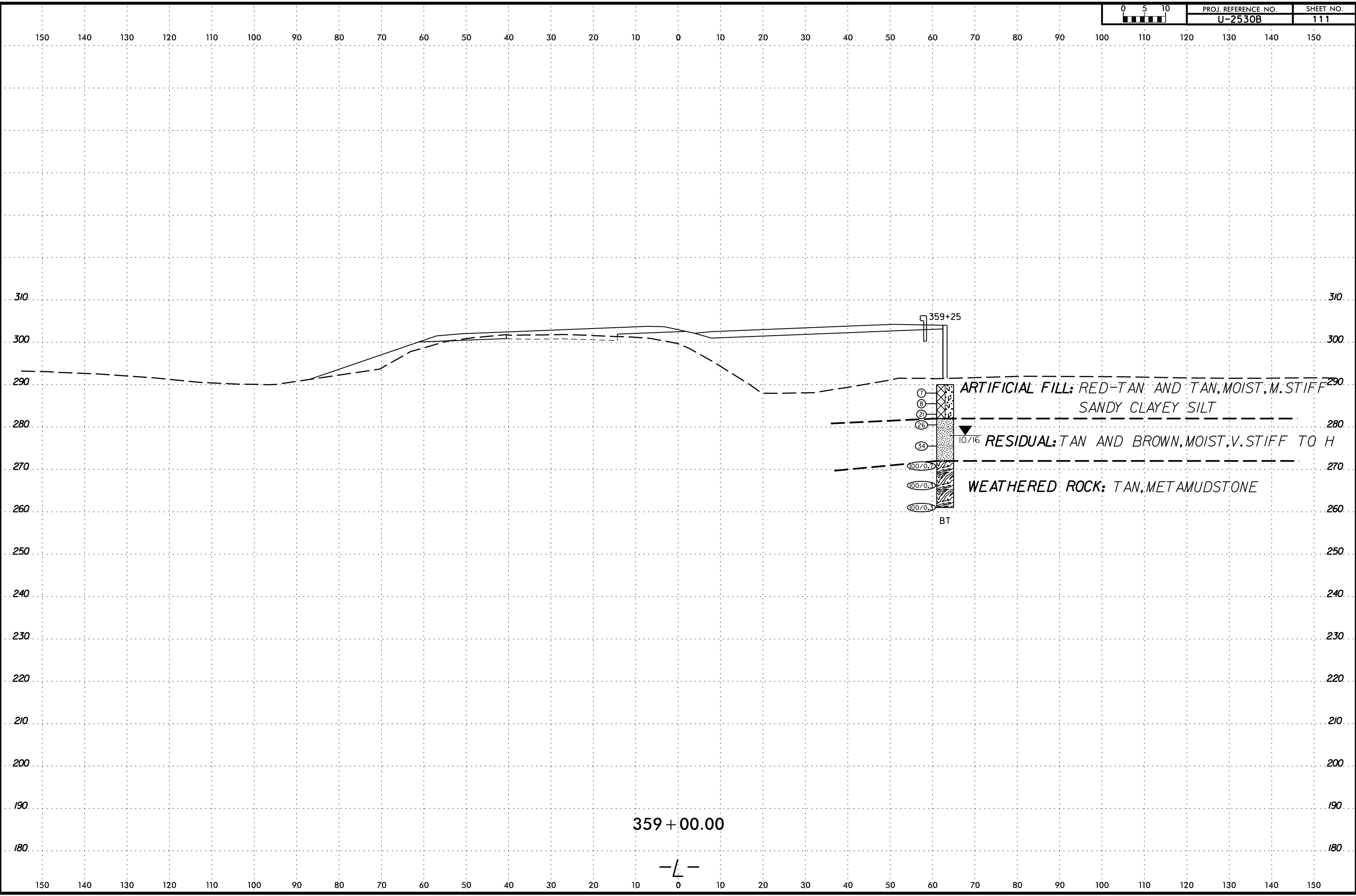


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PROJ. REFERENCE NO.	SHEET NO.
U-2530B	111



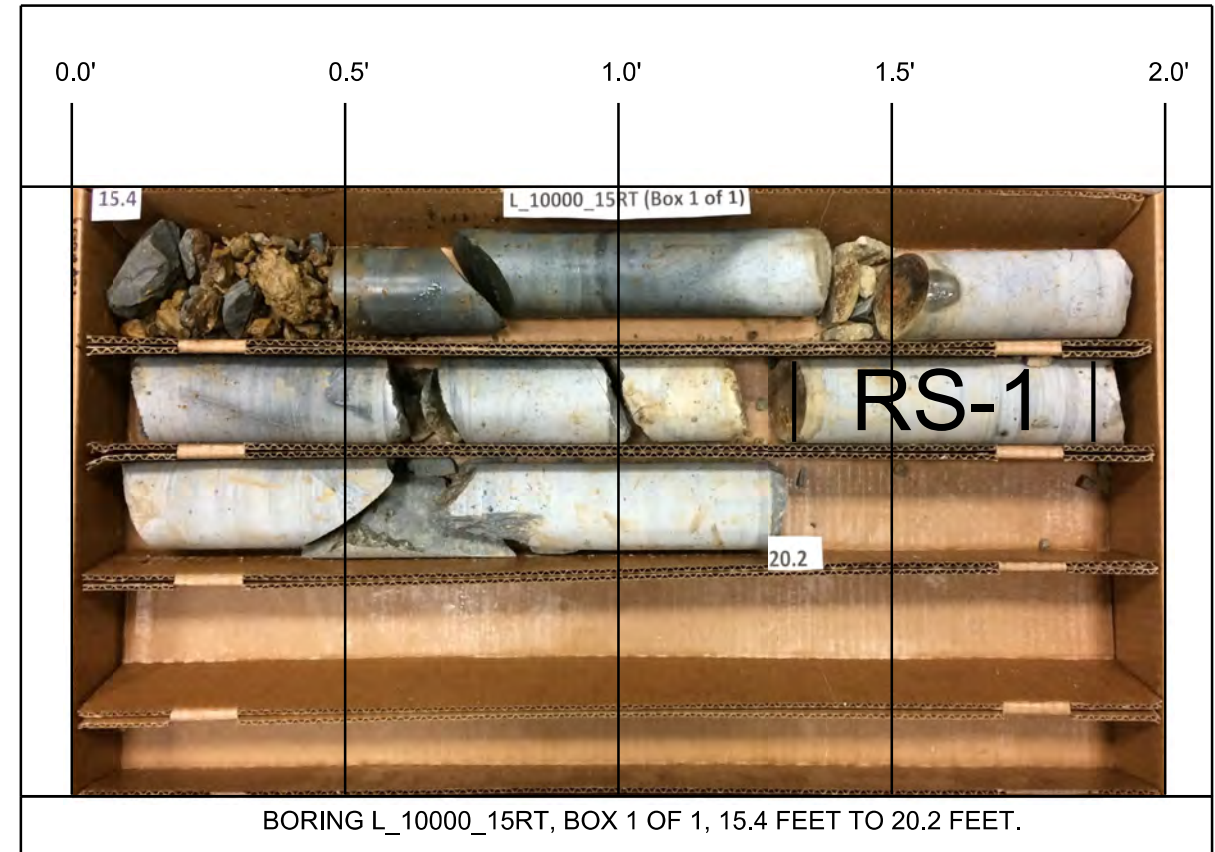
NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT
SUBSURFACE INVESTIGATION
APPENDIX A
CORE LOGS AND PHOTOGRAPHS

REFERENCE: R-2530B

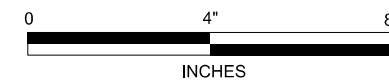
PROJECT: 34446

GEOTECHNICAL BORING REPORT CORE LOG

WBS 34446.1.6		TIP R-2530B		COUNTY STANLY		GEOLOGIST Goodnight, D						
SITE DESCRIPTION NC 24-27 FROM NC 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER							GROUND WTR (ft)					
BORING NO. L_10000_15RT		STATION 100+00		OFFSET 31 ft RT		ALIGNMENT -L-						
COLLAR ELEV. N/A		TOTAL DEPTH 20.2 ft		NORTHING 581,694		EASTING 1,659,506						
DRILL RIG/HAMMER EFF./DATE HPC2473 CME-550 92% 12/09/2015				DRILL METHOD H.S. Augers		HAMMER TYPE Automatic						
DRILLER Contract Driller		START DATE 11/30/16		COMP. DATE 11/30/16		SURFACE WATER DEPTH N/A						
CORE SIZE NQ2		TOTAL RUN 4.8 ft										
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) %	RQD (ft) %	SAMP. NO.	STRATA REC. (ft) %	RQD (ft) %	LOG	DESCRIPTION AND REMARKS	DEPTH (ft)
		15.4	4.8	1:49/1.0 1:40/1.0 1:44/1.0 1:41/1.0 1:29/0.8	(4.6) 96%	(3.8) 79%		(4.6) 96%	(3.8) 79%		Begin Coring @ 15.4 ft NON-CRYSTALLINE ROCK GRAY, SLIGHT TO VERY SLIGHTLY WEATHERED, HARD, VERY CLOSE TO CLOSELY FRACTURED, METATUFF <i>(continued)</i>	20.2
		20.2					RS-1				Boring Terminated at Depth 20.2 ft IN: NCR META MUDSTONE	



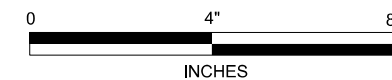
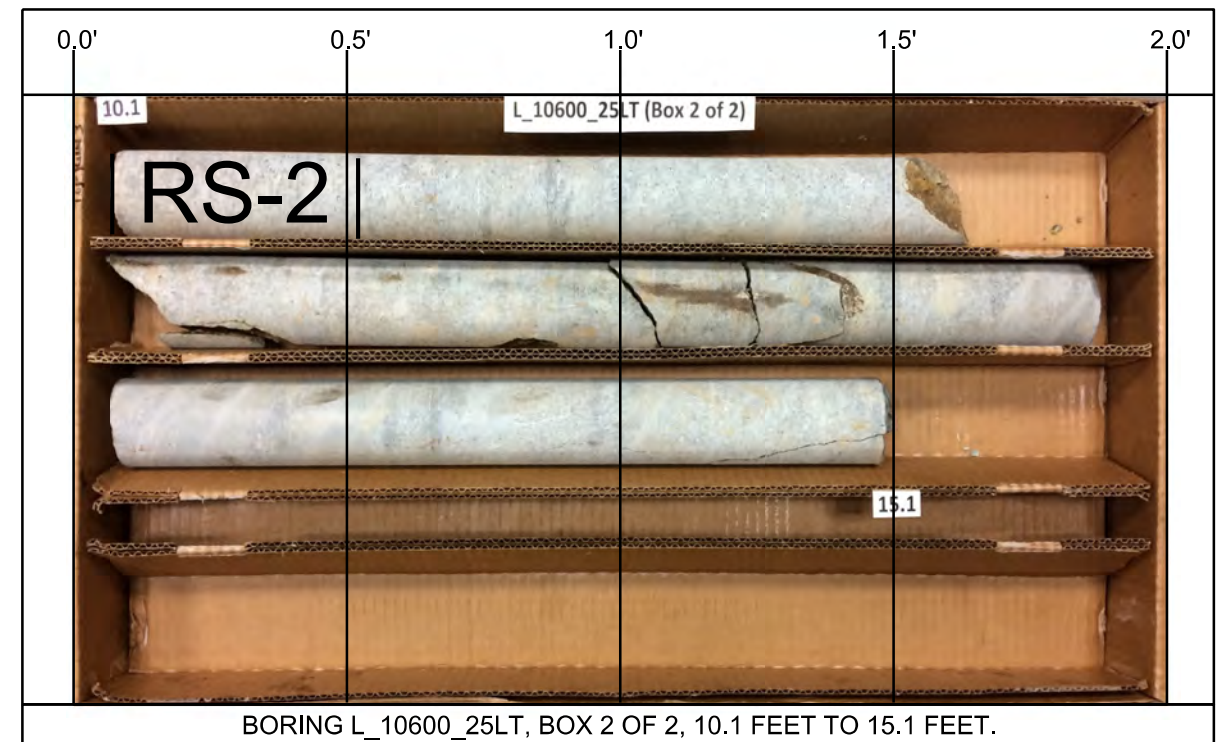
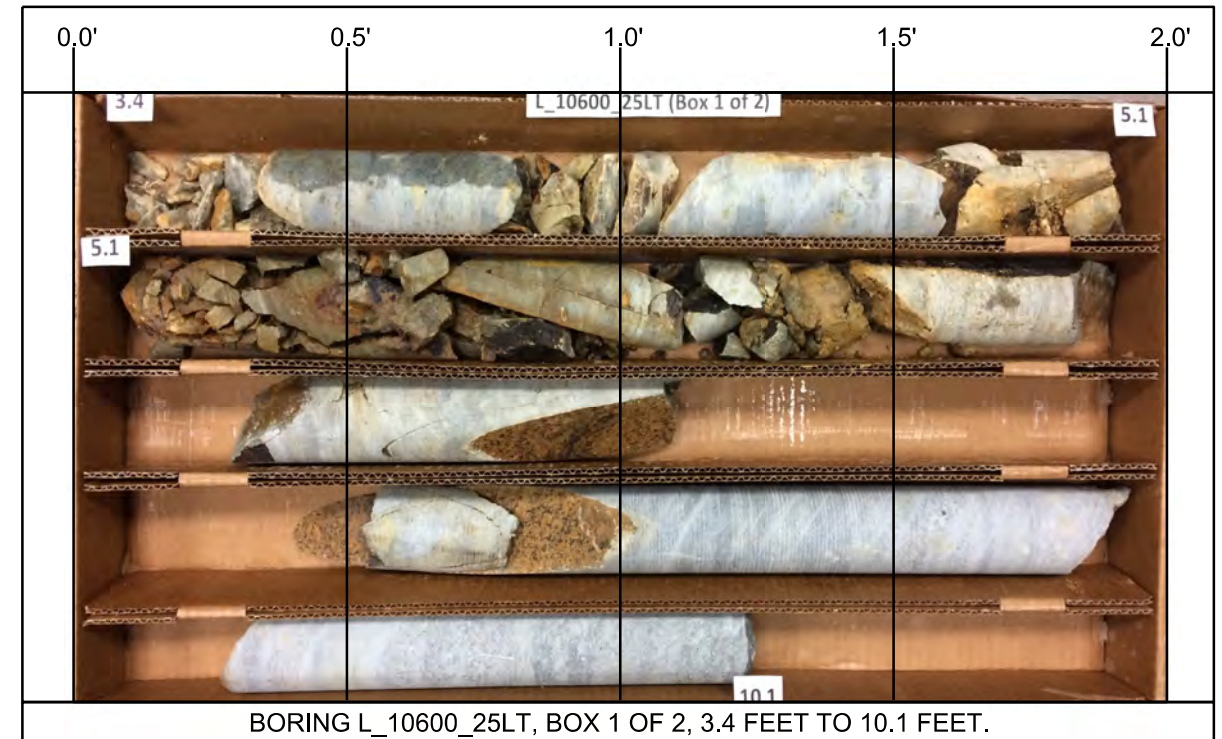
NCDOT CORE DOUBLE R2530B_GEO_BORINGS.GPJ NC_DOT.GDT 3/3/17



<p style="font-size: 8px;">FALCON ENGINEERING, INC. 1210 TRINITY ROAD, SUITE 110 RALEIGH, NC 27607 PHONE: 919.871.0800 FAX: 919.871.0803</p>	<p>ROCK CORE PHOTOS</p> <p style="font-size: 8px;">NC 24-27 FROM 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER STANLY AND MONTGOMERY COUNTIES WBS: 34446.1.6 & TIP: R-2530B FALCON PROJECT NO. G16056.00</p>
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GEOTECHNICAL BORING REPORT CORE LOG

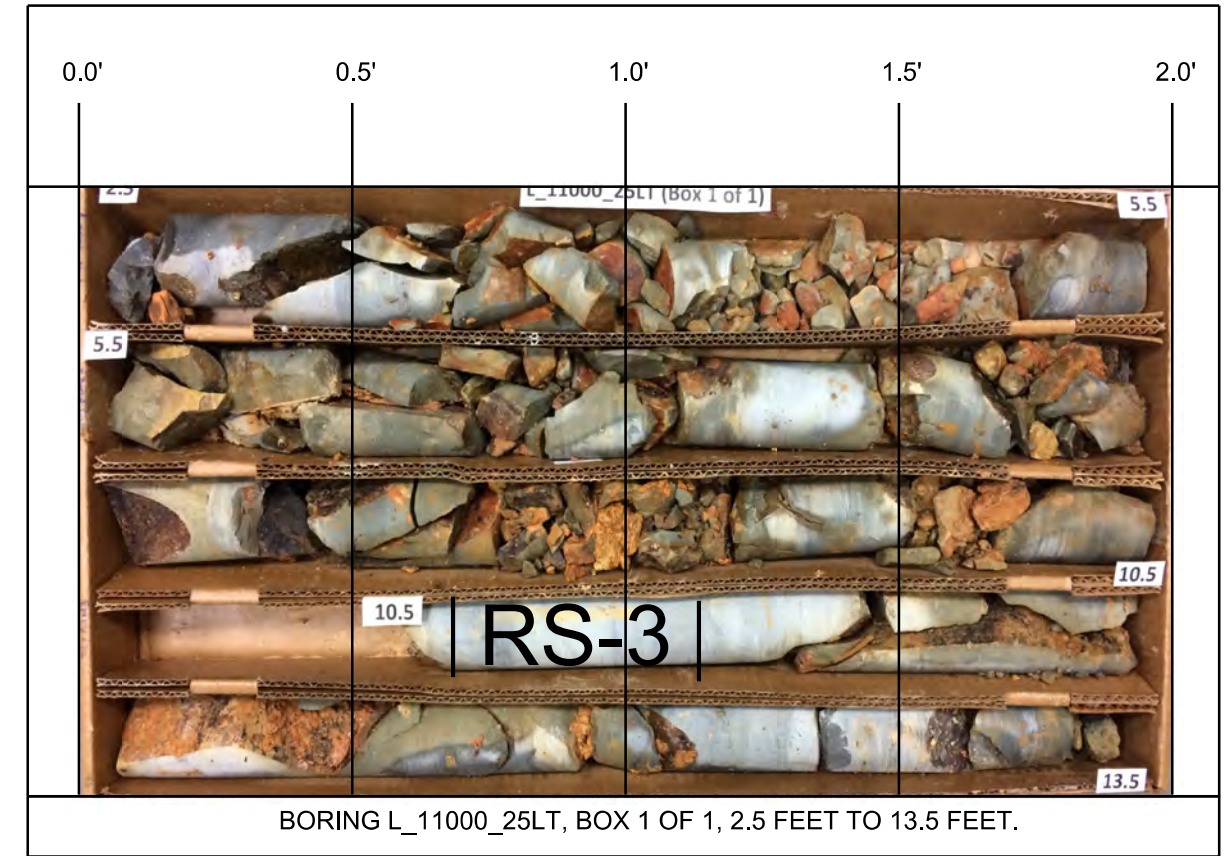
WBS 34446.1.6		TIP R-2530B		COUNTY STANLY		GEOLOGIST Goodnight, D					
SITE DESCRIPTION NC 24-27 FROM NC 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER							GROUND WTR (ft)				
BORING NO. L_10600_25LT		STATION 106+00		OFFSET 25 ft LT		ALIGNMENT -L-					
COLLAR ELEV. N/A		TOTAL DEPTH 15.1 ft		NORTHING 5,813,443		EASTING 1,659,992					
DRILL RIG/HAMMER EFF./DATE HPC2473 CME-550 92% 12/09/2015				DRILL METHOD H.S. Augers		HAMMER TYPE Automatic					
DRILLER Contract Driller		START DATE 11/30/16		COMP. DATE 11/30/16		SURFACE WATER DEPTH N/A					
CORE SIZE NQ2		TOTAL RUN 11.7 ft									
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) %	RQD (ft) %	SAMP. NO.	STRATA REC. (ft) %	RQD (ft) %	LOG	DESCRIPTION AND REMARKS
		3.4	1.7	2:05/1.0	(1.6)	(0.0)		(3.0)	(0.0)		Begin Coring @ 3.4 ft NON-CRYSTALLINE ROCK GRAY AND TAN, MODERATE TO MODERATELY SEVERELY WEATHERED, MODERATELY HARD TO HARD, V. CLOSE TO CLOSELY FRACTURED, METATUFF GRAY AND TAN, SLIGHT TO VERY SLIGHTLY WEATHERED, HARD, MODERATELY CLOSE TO CLOSELY FRACTURED, METATUFF
		5.1	5.0	2:52/0.7	94%	0%		176%	0%		
				2:34/1.0	(4.9)	(2.9)		(8.5)	(7.4)		
				1:54/1.0	98%	58%		85%	74%		
		10.1		2:14/1.0							
				1:29/1.0							
				1:32/1.0							
			5.0	1:34/1.0	(5.0)	(4.5)	RS-2				
				2:11/1.0	100%	90%					
				1:41/1.0							
		15.1		2:22/1.0							
				3:29/1.0							
Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Depth 15.1 ft IN: NCR META MUDSTONE											



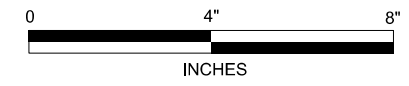
<p style="font-size: 8px;">FALCON ENGINEERING, INC. 1210 TRINITY ROAD, SUITE 110 RALEIGH, NC 27607 PHONE: 919.871.2800 FAX: 919.871.0803</p>	<p>ROCK CORE PHOTOS</p> <p style="font-size: 8px;">NC 24-27 FROM 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER STANLY AND MONTGOMERY COUNTIES WBS: 34446.1.6 & TIP: R-2530B FALCON PROJECT NO. G16056.00</p>
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GEOTECHNICAL BORING REPORT CORE LOG

WBS 34446.1.6		TIP R-2530B		COUNTY STANLY		GEOLOGIST Goodnight, D						
SITE DESCRIPTION NC 24-27 FROM NC 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER							GROUND WTR (ft)					
BORING NO. L_11000_25LT		STATION 110+00		OFFSET 25 ft LT		ALIGNMENT -L-						
COLLAR ELEV. N/A		TOTAL DEPTH 13.5 ft		NORTHING 581,032		EASTING 1,660,245						
DRILL RIG/HAMMER EFF./DATE HPC2473 CME-550 92% 12/09/2015				DRILL METHOD H.S. Augers		HAMMER TYPE Automatic						
DRILLER Contract Driller		START DATE 11/29/16		COMP. DATE 11/29/16		SURFACE WATER DEPTH N/A						
CORE SIZE NQ2		TOTAL RUN 11.0 ft										
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) %	RQD (ft) %	SAMP. NO.	STRATA REC. (ft) %	RQD (ft) %	LOG	DESCRIPTION AND REMARKS	DEPTH (ft)
		2.5	3.0	2:20/1.0 1:54/1.0 2:08/1.0	(1.7) 57%	(0.0) 0%		(8.5) 77%	(1.4) 13%		NON-CRYSTALLINE ROCK GRAY AND TAN, MODERATE TO MODERATELY SEVERE WEATHERING, MODERATELY HARD TO HARD, V. CLOSE TO CLOSELY FRACTURED, METATUFF	
		5.5	5.0	2:26/1.0 1:53/1.0 1:54/1.0 1:40/1.0 3:08/1.0	(3.9) 78%	(0.3) 6%						
		10.5	3.0	1:43/1.0 1:32/1.0 1:56/1.0	(2.9) 97%	(1.1) 37%	RS-3					
		13.5										Boring Terminated at Depth 13.5 ft IN: NCR META MUDSTONE



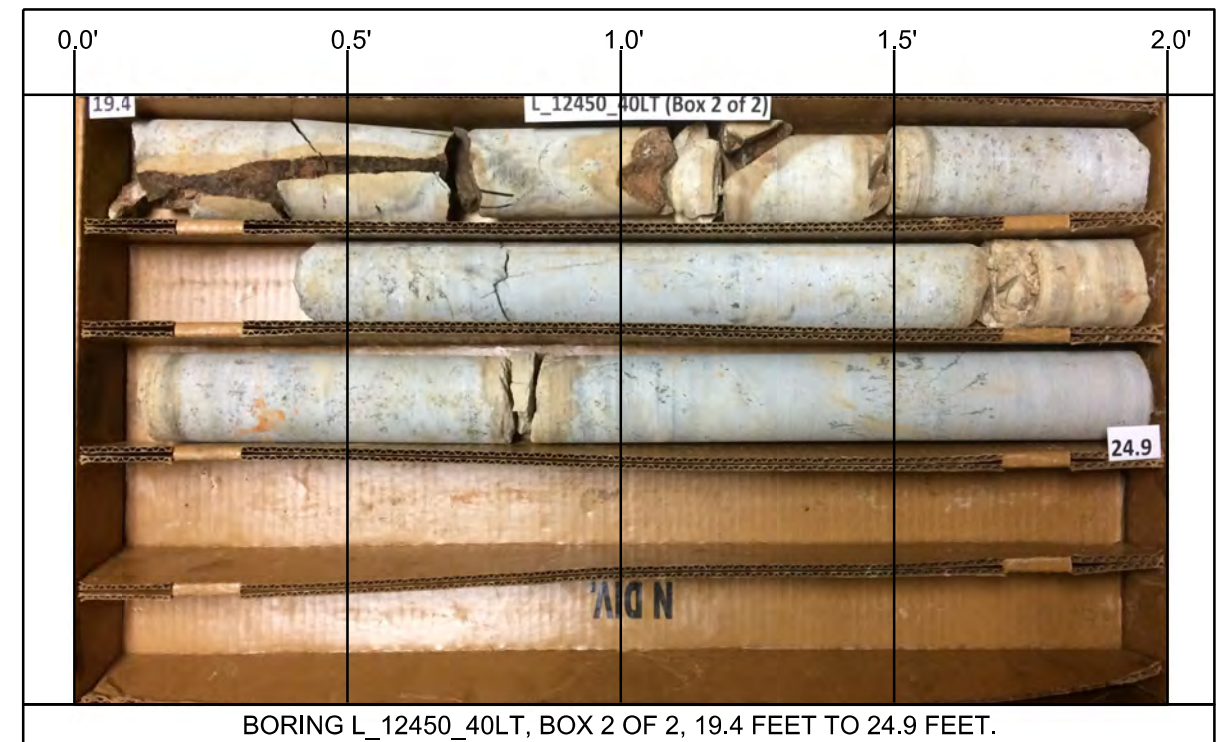
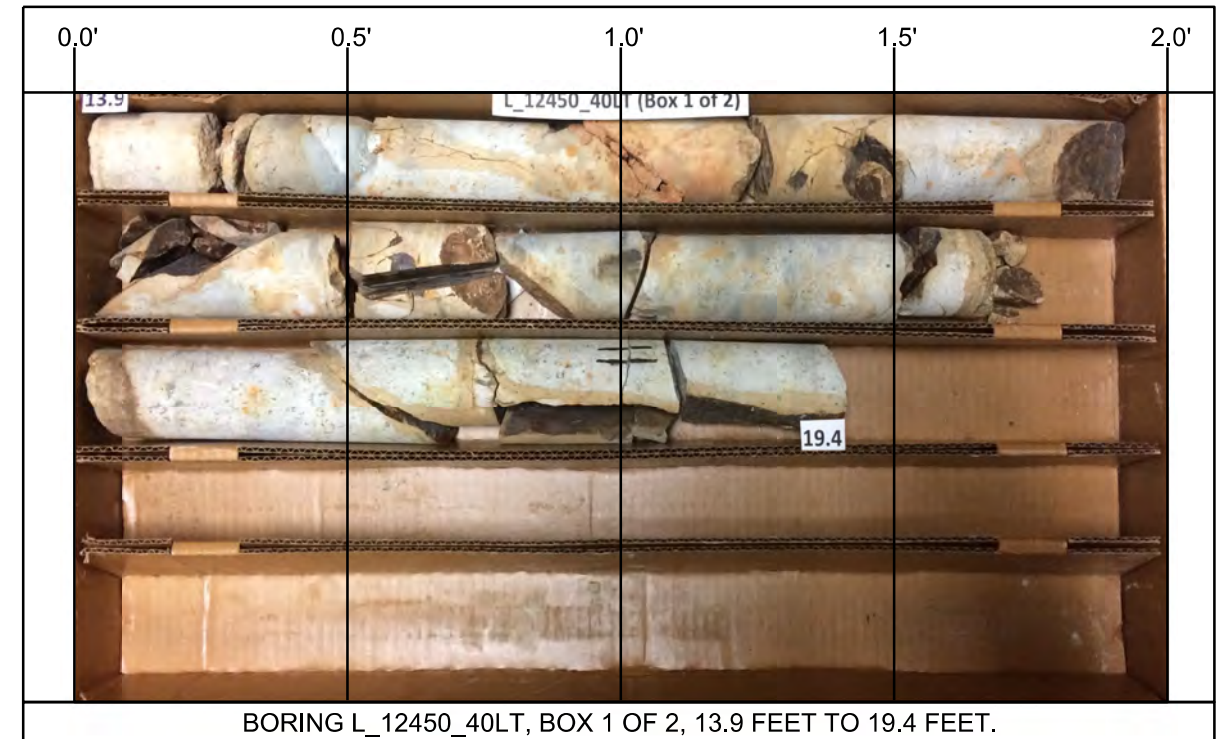
NCDOT CORE DOUBLE R2530B_GEO_BORINGS.GPJ NC_DOT.GDT 3/3/17



<p style="font-size: 8px;">FALCON ENGINEERING, INC. 1210 TRINITY ROAD, SUITE 110 RALEIGH, NC 27607 PHONE: 919.871.0800 FAX: 919.871.0803</p>	<p>ROCK CORE PHOTOS</p> <p style="font-size: 8px;">NC 24-27 FROM 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER STANLY AND MONTGOMERY COUNTIES WBS: 34446.1.6 & TIP: R-2530B FALCON PROJECT NO. G16056.00</p>
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GEOTECHNICAL BORING REPORT CORE LOG

WBS 34446.1.6		TIP R-2530B		COUNTY STANLY		GEOLOGIST Goodnight, D						
SITE DESCRIPTION NC 24-27 FROM NC 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER							GROUND WTR (ft)					
BORING NO. L_12450_50LT		STATION 124+50		OFFSET 50 ft LT		ALIGNMENT -L-						
COLLAR ELEV. N/A		TOTAL DEPTH 24.9 ft		NORTHING 579,906		EASTING 1,661,164						
DRILL RIG/HAMMER EFF./DATE HPC2473 CME-550 92% 12/09/2015				DRILL METHOD H.S. Augers		HAMMER TYPE Automatic						
DRILLER Contract Driller		START DATE 11/21/16		COMP. DATE 11/23/16		SURFACE WATER DEPTH N/A						
CORE SIZE NQ2		TOTAL RUN 11.0 ft										
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) %	RQD (ft) %	SAMP. NO.	STRATA REC. (ft) %	RQD (ft) %	LOG	DESCRIPTION AND REMARKS	DEPTH (ft)
		13.9	5.5	2:26/1.0 2:32/1.0 2:38/1.0 3:45/1.0 2:30/1.0 -0.5	(4.9) 89%	(2.0) 36%		(10.3) 94%	(6.6) 60%		Begin Coring @ 13.9 ft LIGHT GRAY, MODERATE TO SLIGHTLY WEATHERED, HARD, MODERATELY CLOSE TO CLOSELY FRACTURED, METAVOLCANIC ROCK (continued)	
		19.4	5.5	1:57/1.0 1:39/1.0 1:43/1.0 2:13/1.0 1:58/1.0 -0.5	(5.4) 98%	(4.6) 84%						
		24.9									Boring Terminated at Depth 24.9 ft	24.9

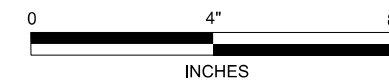
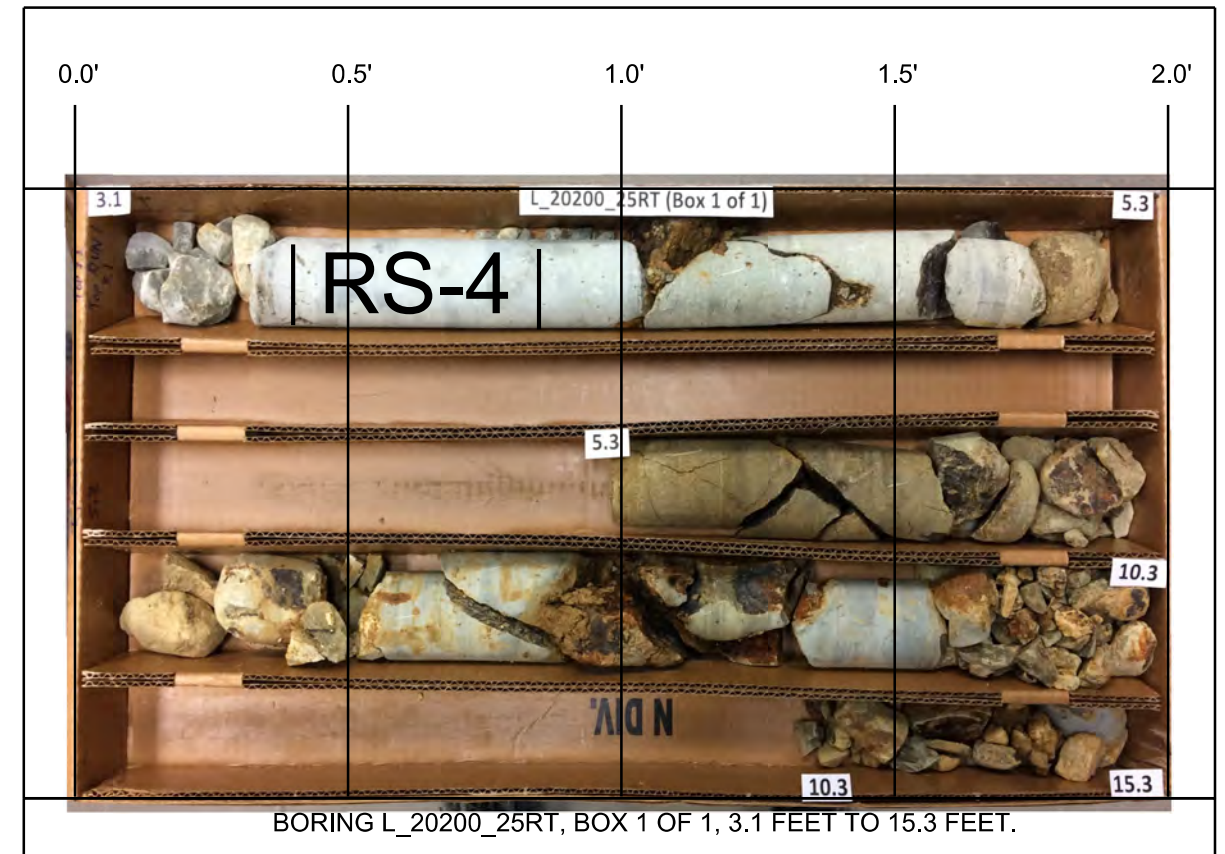


<p style="font-size: 8px;">FALCON ENGINEERING, INC. 1210 TRINITY ROAD, SUITE 110 RALEIGH, NC 27607 PHONE: 919.871.0800 FAX: 919.871.0803</p>	<p>ROCK CORE PHOTOS</p> <p style="font-size: 8px;">NC 24-27 FROM 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER STANLY AND MONTGOMERY COUNTIES WBS: 34446.1.6 & TIP: R-2530B FALCON PROJECT NO. G16056.00</p>
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NCDOT CORE DOUBLE R2530B_GEO_BORINGS.GPJ NC_DOT.GDT 3/3/17

GEOTECHNICAL BORING REPORT CORE LOG

WBS 34446.1.6		TIP R-2530B		COUNTY STANLY		GEOLOGIST Goodnight, D					
SITE DESCRIPTION NC 24-27 FROM NC 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER							GROUND WTR (ft)				
BORING NO. L_20200_25RT		STATION 202+00		OFFSET 25 ft RT		ALIGNMENT -L-					
COLLAR ELEV. N/A		TOTAL DEPTH 15.4 ft		NORTHING 573,454		EASTING 1,664,914					
DRILL RIG/HAMMER EFF./DATE HPC2473 CME-550 92% 12/09/2015				DRILL METHOD H.S. Augers		HAMMER TYPE Automatic					
DRILLER Contract Driller		START DATE 11/14/16		COMP. DATE 11/14/16		SURFACE WATER DEPTH N/A					
CORE SIZE NQ2		TOTAL RUN 12.2 ft									
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) %	RQD (ft) %	SAMP. NO.	STRATA REC. (ft) %	RQD (ft) %	LOG	DESCRIPTION AND REMARKS
		3.1	2.2	2:21/1.0	(1.8)	(0.8)	RS-4	(1.6)	(0.8)		NON-CRYSTALLINE ROCK LT. GRAY, MODERATELY WEATHERED, HARD, CLOSELY FRACTURED, METAMUDSTONE (<i>continued</i>) LT. GRAY AND TAN, MODERATELY SEVERELY WEATHERED, MODERATELY TO MEDIUM HARD, V. CLOSELY TO CLOSELY FRACTURED, METAMUDSTONE
		5.3	5.0	2:17/1.0 0:39/0.2	82%	36%		100%	50%		
		10.3	5.0	4:30/1.0 3:26/1.0 2:43/1.0 3:17/1.0 4:04/1.0	(3.1) 62%	(0.3) 6%		(3.6) 34%	(0.3) 3%		
		15.3	5.0	1:41/1.0 2:54/1.0 3:01/1.0 2:57/1.0 4:00/1.0	(0.3) 6%	(0.0) 0%					
Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Depth 15.4 ft ON: NCR META MUDSTONE											



	FALCON ENGINEERING, INC. 1210 TRINITY ROAD, SUITE 110 RALEIGH, NC 27607 PHONE: 919.871.0800 FAX: 919.871.0803	ROCK CORE PHOTOS NC 24-27 FROM 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER STANLY AND MONTGOMERY COUNTIES WBS: 34446.1,6 & TIP: R-2530B FALCON PROJECT NO. G16056.00
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REFERENCE: R-2530B

PROJECT: 34446

*NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT
SUBSURFACE INVESTIGATION
APPENDIX B
LABORATORY RESULTS*

DS
WSH
INITIALS
4/25/2017
DATE



LABORATORY TEST RESULTS
NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
Stanly County, North Carolina
Project: 34446.1.6 (R-2530B)
Falcon Engineering Project No.: G16056.00

February 21, 2017

SAMPLE			DEPTH	AASHTO	ATTERBERG LIMITS		% BY WEIGHT				% PASSING (SIEVES)			MOISTURE	In-situ Bulk Density	%
NO.	OFFSET	STATION	INTERVAL	CLASS.	L.L.	P.I.	C.SAND	F.SAND	SILT	CLAY	10	40	200	(%)	PCF	ORGANIC
SS-1	30RT	32+00 -L-	1.0-2.5	A-6 (3)	38	12	20	8	26	46	65	55	48	16	-	-
SS-2	35RT	30+00 -L-	3.5-5.0	A-6 (2)	39	14	27	9	22	42	60	47	40	23	-	-
SS-3	CL	44+00 -L-	1.0-2.5	A-7-6 (20)	47	18	4	3	22	71	99	97	94	25	-	-
SS-4	15RT	49+95 -L-	1.0-2.5	A-7-5 (29)	55	24	1	1	23	75	100	99	98	31	-	-
SS-5	20RT	62+00 -L-	1.0-2.5	A-7-5 (12)	61	29	13	5	18	64	62	56	52	20	-	-
SS-6	20RT	78+00 -L-	1.0-2.5	A-7-6 (12)	44	17	13	5	23	59	85	76	71	27	-	-
SS-7	20RT	78+00 -L-	3.5-5.0	A-7-5 (12)	42	11	7	5	33	55	99	94	88	24	-	-
SS-8	15RT	100+00 -L-	1.0-2.5	A-4 (4)	32	9	10	7	33	50	75	69	64	14	-	-
SS-9	25LT	102+00 -L-	1.0-2.5	A-2-6 (0)	38	14	19	13	23	45	41	36	29	12	-	-
SS-10	25LT	102+00 -L-	6.0-7.5	A-7-6 (4)	41	20	22	16	28	34	61	51	40	21	-	-
SS-11	25LT	102+00 -L-	8.5-10.0	A-6 (2)	38	19	25	14	24	37	58	46	37	19	-	-
SS-12	25LT	106+00 -L-	1.0-2.5	A-2-4 (0)	31	7	27	23	26	24	45	36	25	15	-	-
SS-13	25LT	110+00 -L-	1.0-2.5	A-6 (6)	38	15	12	7	28	53	69	62	57	16	-	-
SS-14	25LT	112+00 -L-	1.0-2.5	A-6 (10)	36	14	6	3	40	51	85	80	78	16	-	-
SS-15	25LT	112+00 -L-	3.5-5.0	A-4 (5)	36	7	12	20	39	29	95	88	70	16	-	-
SS-16	20LT	122+00 -L-	1.0-2.5	A-7-5 (13)	47	15	12	8	28	52	94	86	77	21	-	-
SS-17	20LT	122+00 -L-	3.5-5.0	A-7-5 (21)	61	17	5	10	31	54	99	96	87	41	-	-
SS-18	50LT	124+50 -L-	1.0-2.5	A-7-5 (64)	89	53	1	2	17	80	100	99	98	33	-	-
SS-19	60RT	126+00 -L-	1.0-2.5	A-7-5 (42)	68	35	1	1	22	76	99	99	98	27	-	-
SS-20	60RT	126+00 -L-	3.5-5.0	A-7-5 (15)	46	16	10	10	40	40	100	93	83	23	-	-
SS-21	60RT	126+00 -L-	6.0-7.5	A-7-5 (17)	48	18	8	10	34	48	99	94	84	18	-	-
SS-22	30RT	176+00 -L-	1.0-2.5	A-7-5 (51)	86	54	5	7	18	70	92	89	83	33	-	-
SS-23	30RT	176+00 -L-	3.5-5.0	A-6 (10)	37	11	8	11	39	42	100	95	85	15	-	-
SS-24	40RT	170+00 -L-	1.0-2.5	A-7-5 (23)	55	20	5	2	27	66	98	94	91	25	-	-
SS-25	30RT	178+00 -L-	1.0-2.5	A-7-6 (35)	65	38	6	2	24	68	90	85	83	23	-	-

Signature: *John Dailly*

NCDOT No.: 105-03-0803

Notes: LL = Liquid Limit
 PL = Plastic Limit
 PI = Plasticity Index (LL - PL)

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LABORATORY TEST RESULTS
NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
Stanly County, North Carolina
Project: 34446.1.6 (R-2530B)
Falcon Engineering Project No.: G16056.00

February 21, 2017

SAMPLE			DEPTH	AASHTO	ATTERBERG LIMITS		% BY WEIGHT				% PASSING (SIEVES)			MOISTURE	In-situ Bulk Density	%
NO.	OFFSET	STATION	INTERVAL	CLASS.	L.L.	P.I.	C.SAND	F.SAND	SILT	CLAY	10	40	200	(%)	PCF	ORGANIC
SS-26	30RT	178+00 -L-	3.5-5.0	A-4 (8)	37	10	16	10	40	34	98	86	76	11	-	-
SS-27	25RT	180+00 -L-	1.0-2.5	A-6 (11)	34	11	2	3	45	50	99	97	94	25	-	-
SS-28	25RT	180+00 -L-	3.5-5.0	A-1-b (0)	27	6	46	9	20	25	38	23	18	6	-	-
SS-29	25RT	186+00 -L-	1.0-2.5	A-7-6 (34)	56	36	5	9	32	54	98	95	88	22	-	-
SS-30	60RT	120+00 -L-	2.5-3.0	A-7-6 (31)	54	30	3	4	36	57	98	96	92	30	-	-
SS-31	5RT	188+00 -L-	1.0-2.5	A-6 (8)	40	12	9	19	35	37	91	86	71	19	-	-
SS-32	30RT	190+00 -L-	1.0-2.5	A-7-5 (57)	82	52	3	4	59	34	99	97	93	34	-	-
SS-33	30RT	190+00 -L-	6.0-7.5	A-7-6 (11)	49	20	18	24	30	28	98	88	62	28	-	-
SS-34	30RT	190+00 -L-	8.5-10.0	A-6 (3)	37	12	26	28	24	22	89	74	46	20	-	-
SS-35	30RT	192+00 -L-	1.0-2.5	A-7-5 (45)	82	40	2	11	18	69	100	99	90	40	-	-
SS-36	30RT	192+00 -L-	6.0-7.5	A-7-5 (22)	63	19	2	18	40	40	100	99	86	-	-	-
SS-37	30RT	192+00 -L-	13.5-15.0	A-7-5 (11)	44	11	1	26	47	26	100	100	82	37	-	-
SS-38	25RT	194+00 -L-	1.0-2.5	A-7-5 (16)	44	14	3	7	34	56	100	97	93	27	-	-
SS-39	25RT	194+00 -L-	6.0-7.5	A-4 (10)	38	10	6	9	38	47	96	92	85	19	-	-
SS-40	25RT	196+00 -L-	1.0-2.5	A-7-5 (22)	54	19	5	3	85	7	99	96	92	25	-	-
SS-41	25RT	196+00 -L-	8.5-10.0	A-4 (10)	39	8	3	7	44	46	100	98	92	19	-	-
SS-42	30RT	198+00 -L-	1.0-2.5	A-7-6 (15)	47	19	11	4	28	57	88	80	76	26	-	-
SS-43	30RT	198+00 -L-	3.5-5.0	A-7-6 (13)	44	21	10	5	29	56	79	72	68	19	-	-
SS-44	25RT	200+00 -L-	1.0-2.5	A-4 (3)	36	10	23	8	33	36	74	61	53	10	-	-
SS-45	25RT	202+00 -L-	1.0-2.5	A-6 (3)	36	14	14	15	33	38	58	52	44	17	-	-
SS-46	25RT	204+00 -L-	1.0-2.5	A-7-6 (11)	45	16	13	6	29	52	84	75	69	22	-	-
SS-47	25RT	204+00 -L-	6.0-7.5	A-4 (6)	35	7	11	8	41	40	98	90	81	14	-	-
SS-48	25RT	206+00 -L-	1.0-2.5	A-7-6 (9)	41	15	19	6	31	44	87	73	67	17	-	-
SS-49	25RT	230+00 -L-	1.0-2.5	A-7-6 (28)	54	27	3	5	31	61	98	96	91	29	-	-
SS-50	25RT	232+00 -L-	1.0-2.5	A-7-6 (23)	47	26	5	7	33	55	96	92	86	25	-	-

Signature: *John Dailly*

NCDOT No.: 105-03-0803

Notes: LL = Liquid Limit
 PL = Plastic Limit
 PI = Plasticity Index (LL - PL)

Page 2 of 3



LABORATORY TEST RESULTS
NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
Stanly County, North Carolina
Project: 34446.1.6 (R-2530B)
Falcon Engineering Project No.: G16056.00

February 21, 2017

SAMPLE			DEPTH	AASHTO	ATTERBERG LIMITS		% BY WEIGHT				% PASSING (SIEVES)			MOISTURE	In-situ Bulk Density	%
NO.	OFFSET	STATION	INTERVAL	CLASS.	L.L.	P.I.	C.SAND	F.SAND	SILT	CLAY	10	40	200	(%)	PCF	ORGANIC
SS-51	25RT	242+00 -L-	1.0-2.5	A-7-6 (10)	44	15	15	5	27	53	83	73	67	22	-	-
SS-52	25RT	248+00 -L-	3.5-5.0	A-7-5 (13)	47	11	7	6	42	45	100	95	88	18	-	-
SS-53	25LT	274+00 -L-	3.5-5.0	A-6 (4)	38	14	25	7	32	36	73	57	51	6	-	-
SS-54	10LT	276+00 -L-	1.0-2.5	A-7-5 (29)	56	26	5	2	35	58	99	95	93	18	-	-
SS-55	25LT	278+00 -L-	3.5-5.0	A-5 (11)	41	9	7	5	56	32	100	95	90	12	-	-
SS-56	25LT	280+00 -L-	3.5-5.0	A-5 (11)	41	10	7	8	56	29	100	96	87	17	-	-
SS-57	30LT	282+00 -L-	3.5-5.0	A-4 (8)	38	9	12	8	52	28	100	91	83	16	-	-
SS-58	30LT	288+00 -L-	1.0-2.5	A-4 (7)	38	8	11	7	54	28	93	86	78	15	-	-
SS-59	20LT	289+50 -L-	1.0-2.5	A-7-6 (22)	51	25	12	4	31	53	98	89	83	23	-	-
SS-60	25LT	300+00 -L-	3.5-5.0	A-4 (4)	35	5	10	7	50	33	91	84	78	13	-	-
SS-61	30LT	302+00 -L-	6.0-7.5	A-4 (8)	40	8	10	10	52	28	100	94	83	14	-	-
SS-62	35LT	326+00 -L-	1.0-2.5	A-4 (3)	34	9	21	7	38	34	74	61	54	13	-	-
SS-63	35LT	326+00 -L-	6.0-7.5	A-6 (1)	37	14	22	7	39	32	51	42	37	8	-	-
SS-64	CL	20+00 -Y8-	1.0-2.5	A-7-6 (30)	54	29	2	2	30	66	96	95	93	21	-	-
SS-65	CL	20+00 -Y8-	3.5-5.0	A-7-5 (17)	46	13	1	1	45	53	100	99	98	12	-	-
SS-66	35RT	16+00 -Y16-	1.0-2.5	A-7-6 (35)	58	30	0	1	34	65	100	100	99	25	-	-
SS-67	35RT	16+00 -Y16-	6.0-7.5	A-7-5 (18)	50	14	2	3	57	38	100	99	96	21	-	-
SS-68	CL	11+00 -DRW15-	1.0-2.5	A-6 (7)	35	15	19	27	39	15	99	88	60	20	-	-
BS-1	20RT	78+00	1-6	A-7-5 (18)	49	19	12	4	18	66	96	87	82	23	-	-
BS-2	5RT	188+00	1-13	A-6 (2)	30	11	27	19	24	30	75	60	45	6	-	-

Signature: *John Dailly*

NCDOT No.: 105-03-0803

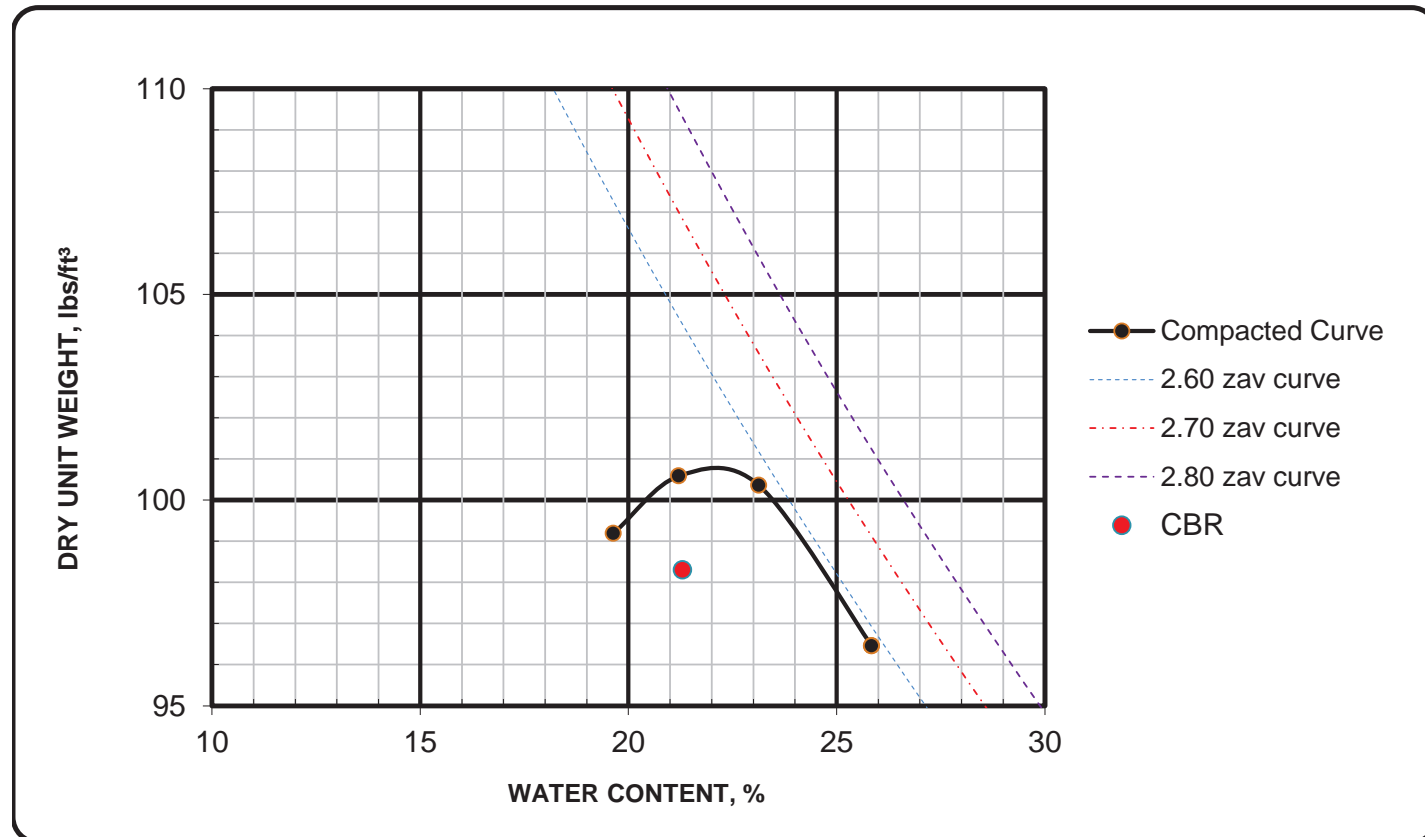
Notes: LL = Liquid Limit
 PL = Plastic Limit
 PI = Plasticity Index (LL - PL)

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**REPORT OF MOISTURE-DENSITY RELATIONS OF SOILS
USING A 5.5-LB RAMMER AND A 12-IN. DROP**
Performed in general accordance with AASHTO T 99, Method C
February 21, 2017



PROJECT NAME: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
PROJECT NUMBER: G16056.00
SAMPLE IDENTIFICATION: BS-1: STA 78+00 -L- 20RT, 1-6'
VISUAL DESCRIPTION: Brown red sandy silty clay



MAXIMUM DENSITY, lbs/ft³: 100.7
OPTIMUM MOISTURE CONTENT, %: 22.1

AS-RECEIVED WATER CONTENT: 23
LIQUID LIMIT: 49
PLASTIC LIMIT: 30
PLASTICITY INDEX: 19
PERCENT FINER NO. 200 82
AASHTO CLASSIFICATION: A-7-5 (18)

REMARKS: NCDOT Project: 34446.1.6 (R-2530B)

Document ID: BS-1 Laboratory Compaction

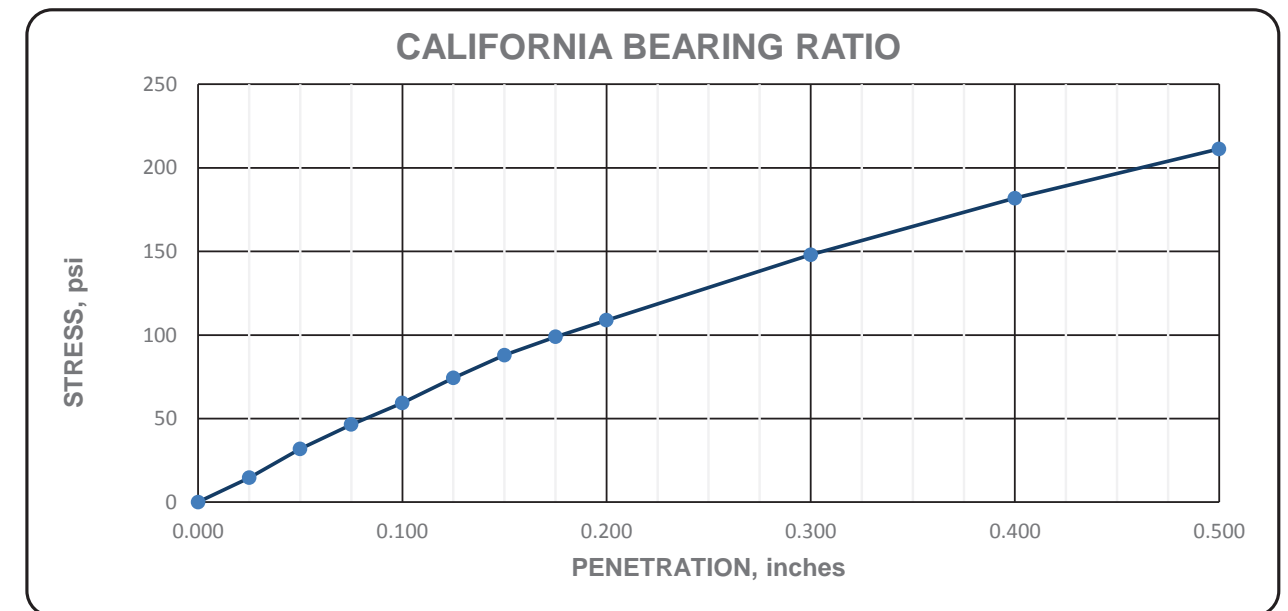
REVIEWED BY: John Dailly



February 21, 2017

**REPORT OF CALIFORNIA BEARING RATIO (CBR)
AASHTO T 193**

PROJECT NAME: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
PROJECT NUMBER: G16056.00
SAMPLE IDENTIFICATION: BS-1: STA 78+00 -L- 20RT, 1-6'



Bearing Ratio: at 0.1 inches of penetration: 5.9
at 0.2 inches of penetration: 7.3

Compaction Method: AASHTO T 99
Maximum Dry Unit Weight, lbs/ft³: 100.7
Optimum Water Content, %: 22.1
Compacted Dry Unit Weight, lbs/ft³: 98.3
Compacted Water Content, %: 21.3
Compaction Percentage: 97.6
Water Content, Top one-inch after test, %: 30.6

Surcharge, lbs: 10
Immersion period, hours: 96
Swell, %: 1.3

Remarks: Soaked specimen
NCDOT Project: 34446.1.6 (R-2530B)

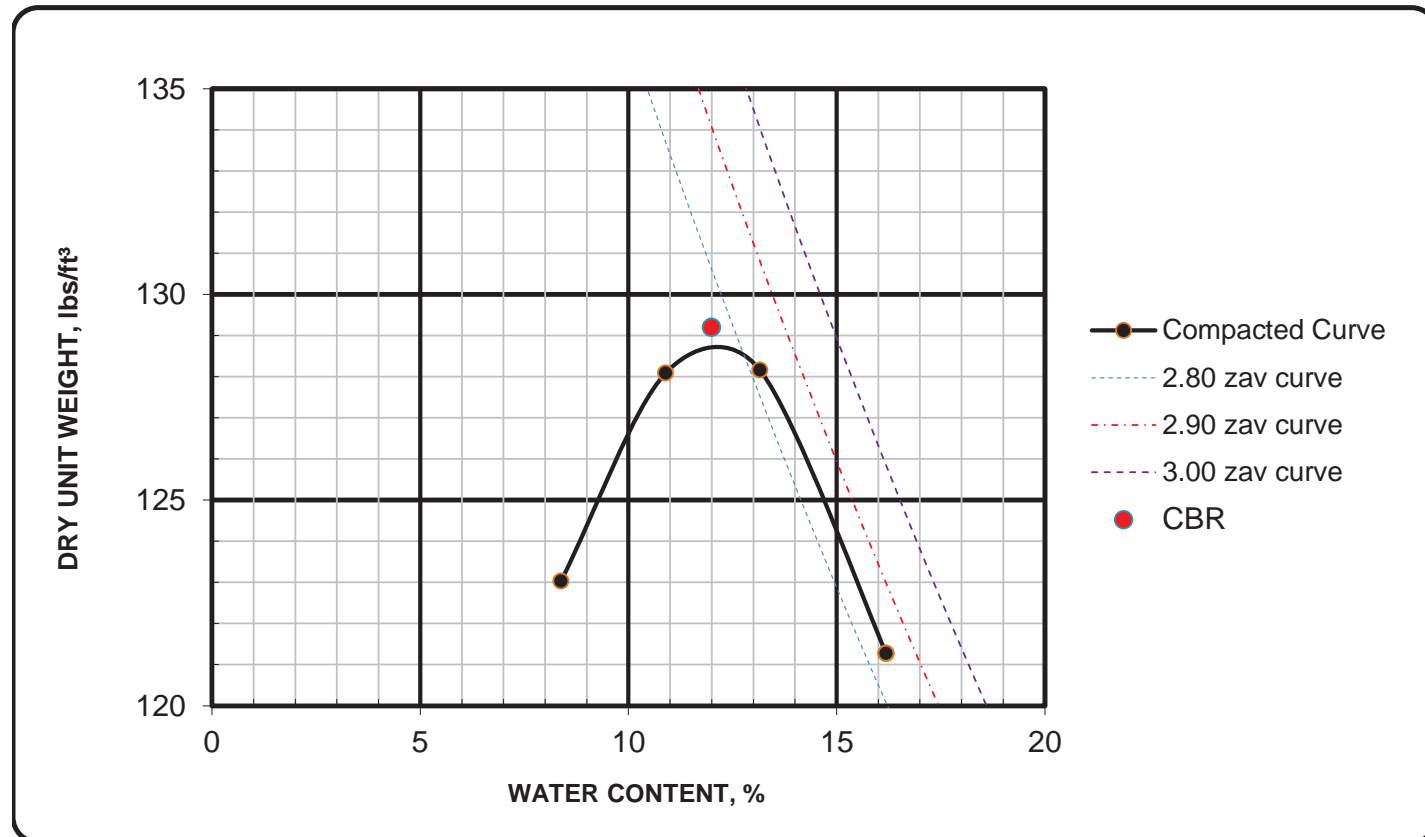
Reviewed by: John Dailly

Document ID: BS-1 California Bearing Ratio

**REPORT OF MOISTURE-DENSITY RELATIONS OF SOILS
USING A 5.5-LB RAMMER AND A 12-IN. DROP**
Performed in general accordance with AASHTO T 99, Method C
February 21, 2017



PROJECT NAME: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
PROJECT NUMBER: G16056.00
SAMPLE IDENTIFICATION: BS-2: STA 188+00 -L- 5RT, 1-13'
VISUAL DESCRIPTION: Brown silty clayey sand



MAXIMUM DENSITY, lbs/ft³: 128.8
OPTIMUM MOISTURE CONTENT, %: 12.2

AS-RECEIVED WATER CONTENT: 6
LIQUID LIMIT: 30
PLASTIC LIMIT: 19
PLASTICITY INDEX: 11
PERCENT FINER NO. 200 45
AASHTO CLASSIFICATION: A-6 (2)

REMARKS: NCDOT Project: 34446.1.6 (R-2530B)

REVIEWED BY: John Dailly

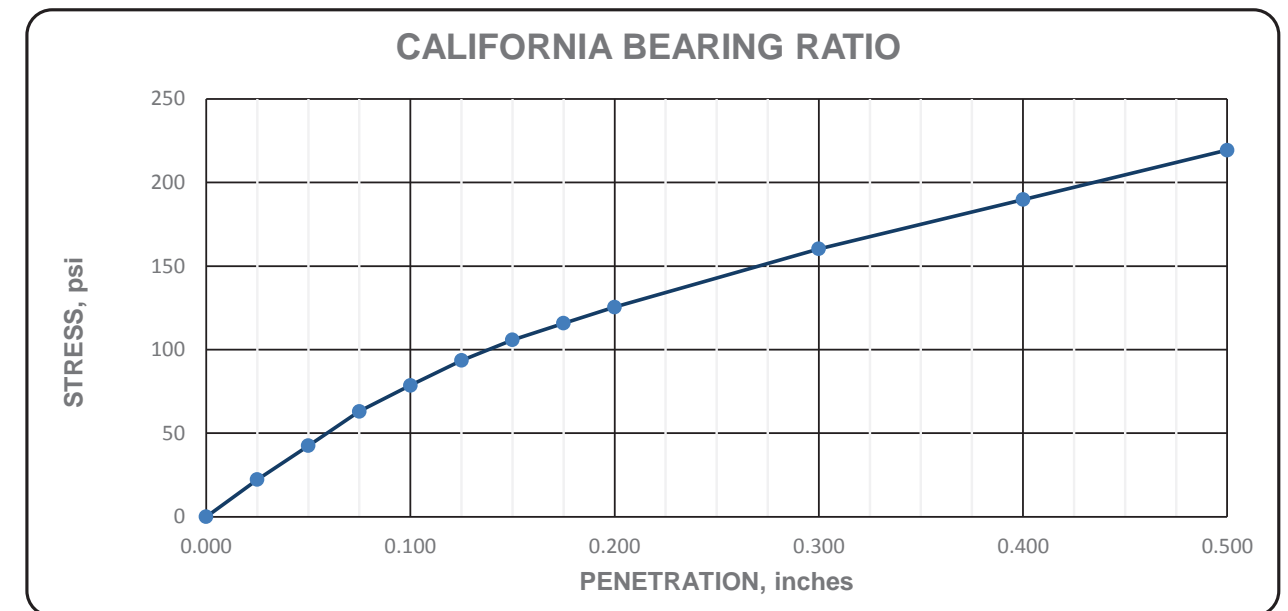
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February 21, 2017

**REPORT OF CALIFORNIA BEARING RATIO (CBR)
AASHTO T 193**

PROJECT NAME: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
PROJECT NUMBER: G16056.00
SAMPLE IDENTIFICATION: BS-2: STA 188+00 -L- 5RT, 1-13'



Bearing Ratio: at 0.1 inches of penetration: 7.9
at 0.2 inches of penetration: 8.4

Compaction Method: AASHTO T 99, AASHTO T 193: 5.1.1
Maximum Dry Unit Weight, lbs/ft³: 128.8
Optimum Water Content, %: 12.2
Compacted Dry Unit Weight, lbs/ft³: 129.2
Compacted Water Content, %: 12.0
Compaction Percentage: 100.3
Water Content, Top one-inch after test, %: 14.8

Surcharge, lbs: 10
Immersion period, hours: 97
Swell, %: 0.7

Remarks: Soaked specimen
NCDOT Project: 34446.1.6 (R-2530B)

Reviewed by: John Dailly

Document ID: BS-2 California Bearing Ratio

SUMMARY OF ROCK CORE TEST RESULTS**NC 24-27 FROM NC 740 IN ALBEMARLE TO EAST OF THE PEE DEE RIVER****WBS: 34446.1.1, TIP NO.: R-2530B****STANLY COUNTY, NORTH CAROLINA****FALCON ENGINEERING, INC. PROJECT NO: G16056.00**

Sample No.	Boring	Station	Offset	Depth (ft)	Rock Type	Geologic Map Unit	Run RQD	Length (ft)	Diameter (ft)	Unit Weight (PCF)	Unconfined Compressive Strength (PSI)	Young's Modulus @ 50% Strain or Less (PSI)	Geological Strength Index (GSI)
RS-1	L_10000_15RT	100+00	15' RT	18.3-18.8	Metatuff	CZfv2	79%	4.15	1.85	170.8	24,230	2,481,700	65
RS-2	L_10600_25LT	106+00	25' LT	10.1-10.6	Metatuff	CZfv2	74%	4.26	1.86	175.6	20,790	1,650,750	65
RS-3	L_11000_25LT	110+00	25' LT	10.5-11.0	Metatuff	CZfv2	13%	4.14	1.86	172.2	21,290	3,622,500	30
RS-4	L_20200_25RT	202+00	25' RT	3.3-3.8	Metamudstone	CZfv2	3%	4.50	1.86	182.7	15,210	1,723,500	20

UNIAXIAL COMPRESSIVE STRENGTH OF INTACT ROCK CORE SPECIMENS

Performed in General Accordance with ASTM D7012



UNIAXIAL COMPRESSIVE STRENGTH OF INTACT ROCK CORE SPECIMENS

Performed in General Accordance with ASTM D7012



Project Name: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
 Project Number: G16056-00
 Sample ID.: RS-1
 Location: STA 100+00 -L- 15RT
 Depth (ft): 18.3-18.8

Length (in.): 4.15
 Diameter (in.): 1.85
 Area (in²): 2.688
 L/D 2.24
 Unit Weight (pcf): 170.8

Compressive Strength (psi): 24230
 Time to Failure, mins:sec: 12:55

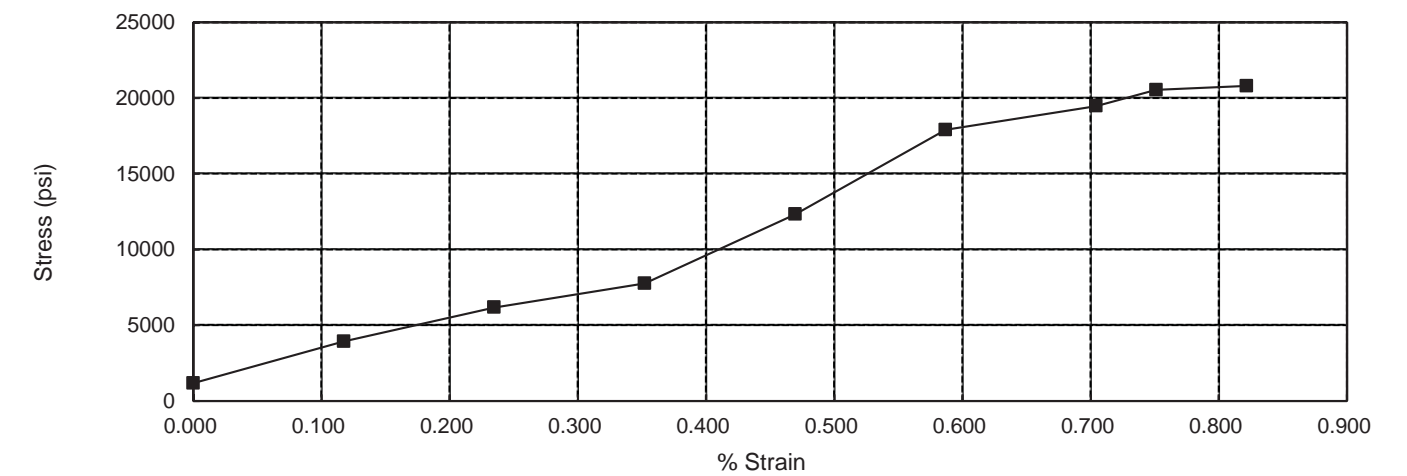
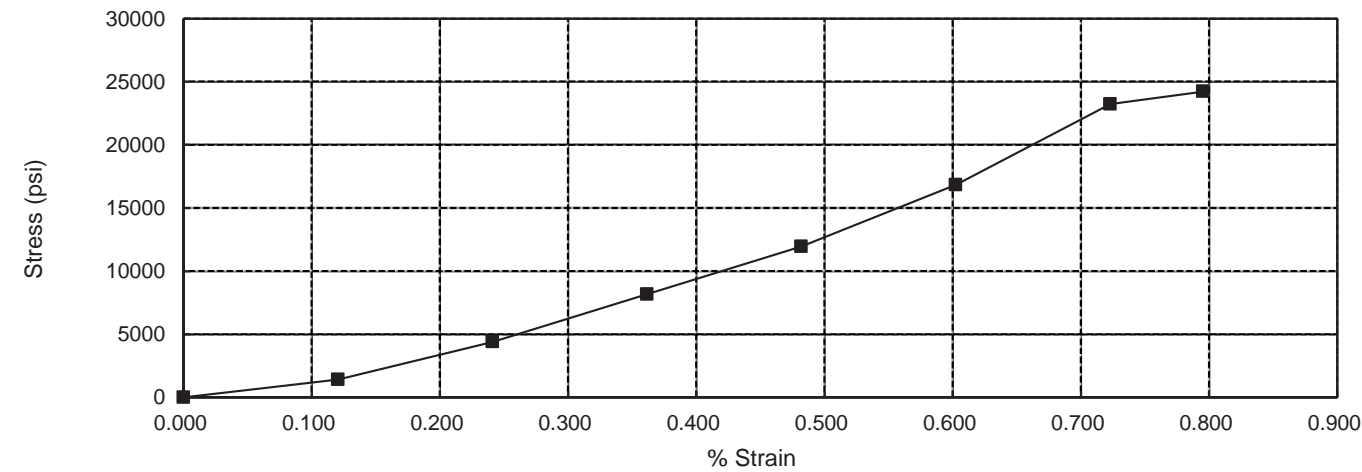
Project Name: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
 Project Number: G16056-00
 Sample ID.: RS-2
 Location: STA 1060+00 -L- 25LT
 Depth (ft): 10.1-10.6

Length (in.): 4.26
 Diameter (in.): 1.86
 Area (in²): 2.717
 L/D 2.29
 Unit Weight (pcf): 175.6

Compressive Strength (psi): 20790
 Time to Failure, mins:sec: 9:45

Deflection (in.)	Strain (%)	Load (lbf)	Compressive Strength (psi)	Young's Modulus (psi)
0.000	0.000	0	0	
0.005	0.120	3810	1420	1,178,600
0.010	0.241	11840	4400	1,826,000
0.015	0.361	21969	8170	2,260,367
0.020	0.482	32140	11960	2,481,700
0.025	0.602	45270	16840	2,795,440
0.030	0.723	62430	23230	3,213,483
0.033	0.795	65140	24230	3,047,106

Deflection (in.)	Strain (%)	Load (lbf)	Compressive Strength (psi)	Young's Modulus (psi)
0.000	0.000	0	0	
0.005	0.117	3190	1170	996,840
0.010	0.235	10640	3920	1,669,920
0.015	0.352	16760	6170	1,752,280
0.020	0.469	21050	7750	1,650,750
0.025	0.587	33480	12320	2,099,328
0.030	0.704	48650	17900	2,541,800
0.032	0.751	52910	19470	2,591,944
0.035	0.822	55780	20530	2,498,794
0.037	0.869	56500	20790	2,393,659



*Young's modulus is calculated using the secant modulus at each data point per Figure 2 (C) in ASMTM D 7012

John Saily

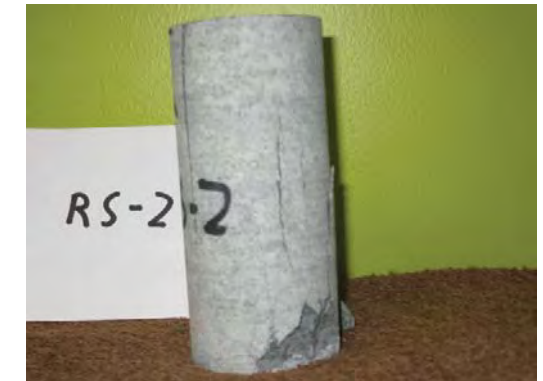
NCDOT CERT No. 105-03-0803



*Young's modulus is calculated using the secant modulus at each data point per Figure 2 (C) in ASMTM D 7012

John Saily

NCDOT CERT No. 105-03-0803



UNIAXIAL COMPRESSIVE STRENGTH OF INTACT ROCK CORE SPECIMENS

Performed in General Accordance with ASTM D7012



Project Name: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
 Project Number: G16056-00
 Sample ID.: RS-3
 Location: STA 110+00 -L- 25LT
 Depth (ft): 10.5-11.0

Length (in.): 4.14
 Diameter (in.): 1.86
 Area (in²): 2.717
 L/D 2.23
 Unit Weight (pcf): 172.2

Compressive Strength (psi): 21290

Time to Failure, mins:sec: 11:35

Deflection (in.)	Strain (%)	Load (lbf)	Compressive Strength (psi)	Young's Modulus (psi)
0.000	0.000	0	0	
0.005	0.121	5250	1930	1,598,040
0.010	0.242	18430	6780	2,806,920
0.015	0.362	35210	12960	3,576,960
0.020	0.483	47540	17500	3,622,500
0.025	0.604	57310	21090	3,492,504
0.027	0.652	57850	21290	3,264,467

UNIAXIAL COMPRESSIVE STRENGTH OF INTACT ROCK CORE SPECIMENS

Performed in General Accordance with ASTM D7012



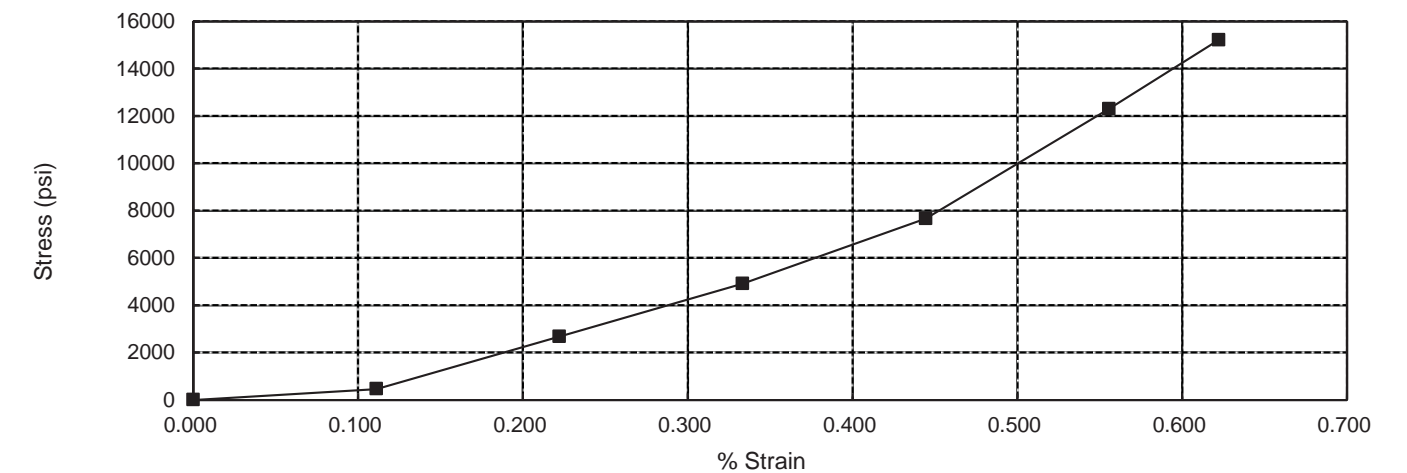
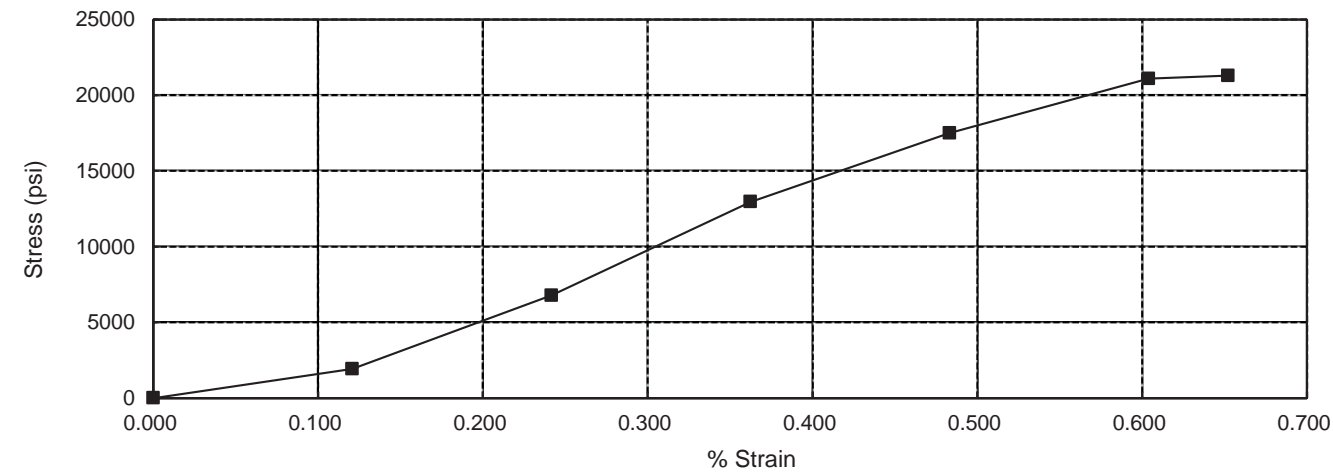
Project Name: NC 24-27 from NC 740 in Albemarle to East of the Pee Dee River
 Project Number: G16056-00
 Sample ID.: RS-4
 Location: STA 202+00 -L- 25RT
 Depth (ft): 3.3-3.8

Length (in.): 4.50
 Diameter (in.): 1.86
 Area (in²): 2.717
 L/D 2.42
 Unit Weight (pcf): 182.7

Compressive Strength (psi): 15210

Time to Failure, mins:sec: 8:30

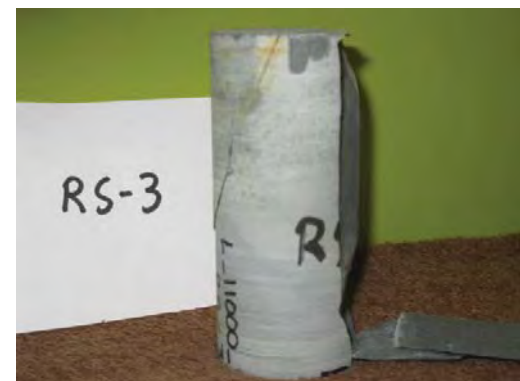
Deflection (in.)	Strain (%)	Load (lbf)	Compressive Strength (psi)	Young's Modulus (psi)
0.000	0.000	0	0	
0.005	0.111	1260	460	414,000
0.010	0.222	7270	2680	1,206,000
0.015	0.333	13350	4910	1,473,000
0.020	0.444	20810	7660	1,723,500
0.025	0.556	33420	12300	2,214,000
0.028	0.622	41320	15210	2,444,464



*Young's modulus is calculated using the secant modulus at each data point per Figure 2 (C) in ASMTM D 7012

John Saily

NCDOT CERT No. 105-03-0803



*Young's modulus is calculated using the secant modulus at each data point per Figure 2 (C) in ASMTM D 7012

John Saily

NCDOT CERT No. 105-03-0803

