583 REFERENCE **CONTENTS** 

**DESCRIPTION** 

LEGEND (SOIL & ROCK)

LABORATORY SUMMARY SHEET

TITLE SHEET

SITE PLAN

BORELOGS

SHEET NO.

#### STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS** GEOTECHNICAL ENGINEERING UNIT

### **STRUCTURE** SUBSURFACE INVESTIGATION

COUNTY RUTHERFORD

PROJECT DESCRIPTION WIDENING OF SR 2241 (OAK STREET EXTENSION) FROM SR 2159 TO US 74 ALTERNATE

SITE DESCRIPTION WALL FROM -L- STA. 41 + 54 TO STA. 43 + 00 (-WALL 1-)

STATE PROJECT REFERENCE NO. U-5833 6

#### **CAUTION NOTICE**

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT 1991 707-680. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BORCHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE DISTORMENT OF THE STANDARD TEST METHOD. THE DISTORMENT OF THE STANDARD TEST METHOD. THE STANDARD TEST METHOD. THE STANDARD TEST METHOD. SOIL MOISTURE CONDITIONS NIDICATED IN THE SUBSURFACE INVESTIGATIONS ANE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT, FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DIES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE THE SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR IS ALL HAVE NO CLAIM FOR ADDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

- NOTES:

  1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N.C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.

  BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

| HPC               |
|-------------------|
| M. BREWER, P.E.   |
| J. ERICKSON, E.I. |
|                   |

INVESTIGATED BY ECS SOUTHEAST, LLP

DRAWN BY \_M. BREWER, P.E.

CHECKED BY \_M. WALKO, P.E.

SUBMITTED BY ECS SOUTHEAST, LLP

DATE NOVEMBER 2017

#### Prepared in the Office of:



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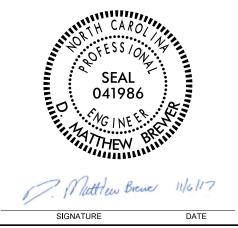
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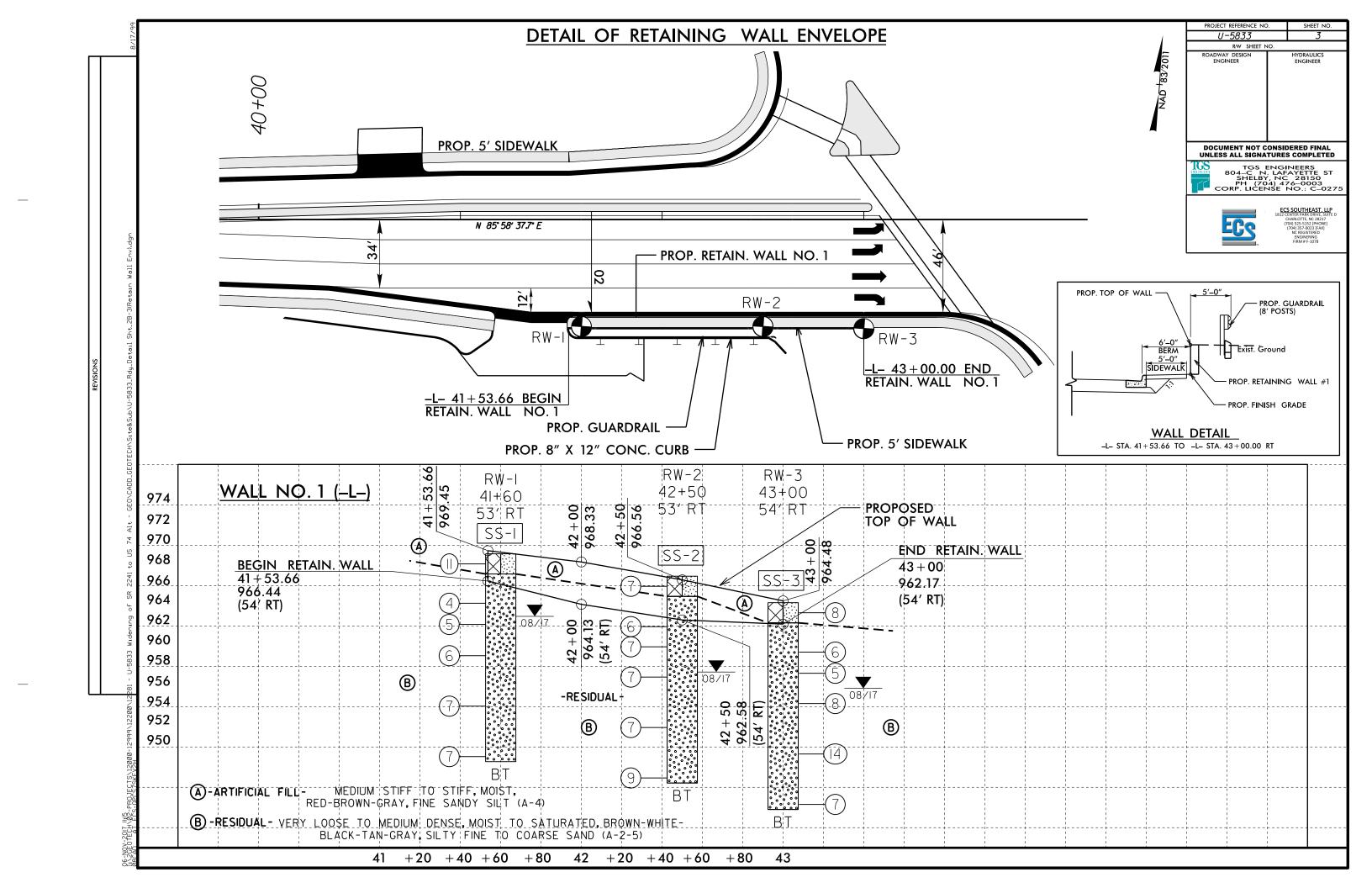
U-5833 2

# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT

### SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

| SOIL DESCRIPTION  | GRADATION  | ROCK DESCRIPTION  | TERMS AND DEFINITIONS   |
|---|--|---|---|
| SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT | <u>WELL GRADED</u> - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.<br>UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.   | HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL.        | ALLUYIUM (ALLUY.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.  |
| ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION  | GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.   | SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN                  | AQUIFER - A WATER BEARING FORMATION OR STRATA.  |
| IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH     | ANGULARITY OF GRAINS   | REPRESENTED BY A ZONE OF WEATHERED ROCK.  | ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.  |
| AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE,<br>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6    | THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS:   | ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:  | ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.              |
| SOIL LEGEND AND AASHTO CLASSIFICATION   | ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.   | WEATHERED /// NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > ROCK (WR) 100 BLOWS PER FOOT IF TESTED.  | ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT  |
| GENERAL GRANULAR MATERIALS SILT-CLAY MATERIALS ORGANIC MATERIALS  | MINERALOGICAL COMPOSITION  | CRYSTALLINE CRYSTALLINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT   | WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND   |
| LLASS. (\$\\\\) 29/ PASSING "200) (\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\   | MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC.  ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.   | ROCK (CR) WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.   | SURFACE.  CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.   |
| GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5 CLASS. A-1-0 A-1-1 A-2-4 A-2-5 A-2-6 A-2-7 A-1-3-5 A-3 A-6, A-7   | COMPRESSIBILITY  | NON-CRYSTALLINE FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YELLD SPT REFUSAL IF TESTED.   | COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM   |
| SYMBOL 000000000  | SLIGHTLY COMPRESSIBLE LL < 31  | ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.   | OF SLOPE.   |
| 555566565G  | MODERATELY COMPRESSIBLE LL = 31 - 50 HIGHLY COMPRESSIBLE LL > 50   | COASTAL PLAIN COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SEDIMENTARY ROCK SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED                                   | CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.                               |
| % PASSING "10 50 MX GRANULAR SILT- MUCK,  | PERCENTAGE OF MATERIAL   | (CP) SHELL BEDS, ETC.   | DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT  |
| *40 30 MX 50 MX 51 MN   | GRANULAR SILT - CLAY ORGANIC MATERIAL SOILS SOILS OTHER MATERIAL   | WEATHERING  | ROCKS OR CUTS MASSIVE ROCK.   |
| MATERIAL MATERIAL   | TRACE OF ORGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10%  | FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.   | DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE   |
| PASSING *40 SOILS WITH  | LITTLE ORGANIC MATTER 3 - 5% 5 - 12% LITTLE 10 - 20% MODERATELY ORGANIC 5 - 10% 12 - 20% SOME 20 - 35%   | VERY SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN.  | HORIZONTAL.  DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE  |
| LL — — 40 MX 41 MN 40 MX 41 MN 40 MX 41 MN 40 MX 41 MN LITTLE OR LITCHLY  | HIGHLY ORGANIC > 10% > 20% HIGHLY 35% AND ABOVE  | (V SLI.) CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.   | LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.   |
| CROILE TAIREY A A A MY B MY 12 MY 16 MY NO MY AMOUNTS OF  | GROUND WATER   | SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO   | FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE  |
| USUAL TYPES STONE FRACS. FINE SILTY OR CLAYEY SILTY CLAYEY MATTER   | ▼ WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING  | (SLI.) I INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR  | SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.   |
| OF MAJOR GRAVEL, AND SAND GRAVEL AND SAND SOILS SOILS   | ▼ STATIC WATER LEVEL AFTER 24 HOURS  | CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.  MODERATE SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN                             | FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.  FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM                        |
| CEN BATING FAIR TO  | ─────────────────────────────────────  | (MOD.) GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS  | PARENT MATERIAL.  |
| AS SUBGRADE EXCELLENT TO GOOD FAIR TO POOR POOR UNSUITABL   | SPRING OR SEEP   | DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.   | FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.   |
| PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30   | <u> </u>   | MODERATELY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL   | FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE   |
| CONSISTENCY OR DENSENESS  | MISCELLANEOUS SYMBOLS  | SEVERE AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION, ROCK SHOWS SEVERE LOSS OF STRENGTH (MOD. SEV.)  AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK, ROCK GIVES "CLUNK" SOUND WHEN STRUCK,  | FIELD.  JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.  |
| PRIMARY SOIL TYPE COMPACTNESS OR RANGE OF STANDARD RANGE OF UNCONFINED PENETRATION RESISTENCE COMPRESSIVE STRENGTH  | ROADWAY EMBANKMENT (RE) 25/025 DIP & DIP DIRECTION   | IF TESTED, WOULD YIELD SPT REFUSAL  | LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO   |
| CONSISTENCY CONSISTENCY (N-VALUE) (TONS/FT <sup>2</sup> )   | WITH SOIL DESCRIPTION OF ROCK STRUCTURES   | SEVERE ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED, ROCK FABRIC CLEAR AND EVIDENT BUT  | ITS LATERAL EXTENT.   |
| GENERALLY VERY LOOSE 4 TO 10  | SOIL SYMBOL  OPT DMT TEST BORING  SLOPE INDICATOR INSTALLATION   | (SEV.) REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN.                                      | LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.   |
| MEDIUM DENSE 10 TO 30 N/A   | ARTIFICIAL FILL (AF) OTHER AUGER PORTING ONE PENETROMETER  | IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF   | MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.                                  |
| (NON-COHESIVE) DENSE 30 TO 50  VERY DENSE > 50  | THAN ROADWAY EMBANKMENT TEST   | VERY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE SEVERE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK             | PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE  |
| VERY SOFT < 2 < 0.25  | — INFERRED SOIL BOUNDARY — CORE BORING SOUNDING ROD  | (V SEV.) REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR   | OF AN INTERVENING IMPERVIOUS STRATUM.   |
| GENERALLY SOFT 2 TO 4 0.25 TO 0.5 SILT-CLAY MEDIUM STIFF 4 TO 8 0.5 TO 1.0  | INFERRED ROCK LINE MONITORING WELL TEST BORING   | VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <u>IF TESTED, WOULD YIELD SPT N VALUES &lt; 100 BFF</u> COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND | RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.  |
| MATERIAL STIFF 8 TO 15 1 TO 2   | A DIEZOMETED   | SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS   | ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE       |
| (COHESIVE)  | ***** ALLUVIAL SOIL BOUNDARY \( \triangle \tri | ALSO AN EXAMPLE.  | RUN AND EXPRESSED AS A PERCENTAGE.  |
| TEXTURE OR GRAIN SIZE   | RECOMMENDATION SYMBOLS   | ROCK HARDNESS   | SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.   |
| U.S. STD. SIEVE SIZE 4 10 40 60 200 270   | UNDERCUT UNCLASSIFIED EXCAVATION -   | VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.   | SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND   |
| OPENING (MM) 4.76 2.00 0.42 0.25 0.075 0.053  | IISED IN THE TOP 2 FEET OF   | HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED   | RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO  |
| BOULDER COBBLE GRAVEL COARSE FINE SILT CLAY   | SHALLOW UNDERCUT UNCLASSIFIED EXCAVATION - EMBANKMENT OR BACKFILL  | TO DETACH HAND SPECIMEN.  | THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.  SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT   |
| (BLDR.) (COB.) (GR.) (CSE. SD.) (F SD.) (SL.) (CL.)   | ABBREVIATIONS  | MODERATELY CAN BE SCRATCHED BY KNIFE OR PICK, GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE HARD EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK, HAND SPECIMENS CAN BE DETACHED                  | OR SLIP PLANE.  |
| GRAIN MM 305 75 2.0 0.25 0.05 0.005   | AR - AUGER REFUSAL MED MEDIUM VST - VANE SHEAR TEST  | BY MODERATE BLOWS.  | STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB, HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL |
| SIZE IN. 12 3   | BT - BORING TERMINATED MICA MICACEOUS WEA WEATHERED  CL CLAY MOD MODERATELY 7 - UNIT WEIGHT  | MEDIUM CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT.  HARD CAN BE EXCAVATED IN SMALL CHIPS TO PEICES I INCH MAXIMUM SIZE BY HARD BLOWS OF THE            | WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL  |
| SOIL MOISTURE - CORRELATION OF TERMS  | CPT - CONE PENETRATION TEST NP - NON PLASTIC $\dot{\gamma}_{\sf d}$ - DRY UNIT WEIGHT  | POINT OF A GEOLOGIST'S PICK.  | TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.  |
| SOIL MOISTURE SCALE FIELD MOISTURE GUIDE FOR FIELD MOISTURE DESCRIPTION  (ATTERBERG LIMITS) DESCRIPTION   | CSE COARSE ORG ORGANIC  DMT - DILATOMETER TEST PMT - PRESSUREMETER TEST SAMPLE ABBREVIATIONS   | SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN                      | STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.  |
| - SATURATED - USUALLY LIQUID; VERY WET, USUALLY   | DPT - DYNAMIC PENETRATION TEST SAP SAPROLITIC S - BULK   | PIECES CAN BE BROKEN BY FINGER PRESSURE.  | STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL   |
| (SAT.) FROM BELOW THE GROUND WATER TABLE  | F - FINE SL SILT, SILTY ST - SHELBY TUBE   | VERY CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK, PIECES I INCH SOFT OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY             | TENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.                                   |
| PLASTIC PLOUID LIMIT  | FOSS FOSSILIFEROUS SLI SLIGHTLY RS - ROCK FRAC FRACTURED, FRACTURES TCR - TRICONE REFUSAL RT - RECOMPACTED TRIAXIAL  | FINGERNAIL.   | TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.  |
| RANGE - WET - (W) SEMISOLID; REGUIRES DRYING TO   | FRAGS FRAGMENTS $\omega$ - MOISTURE CONTENT CBR - CALIFORNIA BEARING   | FRACTURE SPACING BEDDING  | BENCH MARK: BM #3   |
| (PI) PL PLASTIC LIMIT ATTAIN OPTIMUM MOISTURE   | HI HIGHLY V - VERY RATIO   | TERM SPACING TERM THICKNESS   | N-588,934.373I E-I,I37,644.6809   |
| OM OPTIMUM MOISTURE - MOIST - (M) SOLID; AT OR NEAR OPTIMUM MOISTURE  | EQUIPMENT USED ON SUBJECT PROJECT  DRILL UNITS: ADVANCING TOOLS: HAMMER TYPE:  | VERY WIDE MORE THAN 10 FEET VERY THICKLY BEDDED 4 FEET WIDE 3 TO 10 FEET THICKLY BEDDED 1.5 - 4 FEET  | ELEVATION: 981.12 FEET  |
| SL _ SHRINKAGE LIMIT  | DRILL UNITS: ADVANCING TOOLS: HAMMER TYPE:    X DIEDRICH D-50   CLAY BITS   X AUTOMATIC   MANUAL   | MODERATELY CLOSE  | NOTES:  |
| - DRY - (D) REQUIRES ADDITIONAL WATER TO  | CI CONTINUOUS ELICIT AUSED   | VERY CLOSE LESS THAN 0.16 FEET THICKLY LAMINATED 0.008 - 0.03 FEET  | ROADWAY DESIGN AND SURVEY INFORMATION PROVIDED<br>BY TGS ENGINEERS  |
| ATTAIN OPTIMUM MOISTURE   | CME-55     CORE SIZE:  | THINLY LAMINATED < 0.008 FEET  INDURATION   | ומן וט בואטואצבאט   |
| PLASTICITY  | <b>-</b>   | FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.   | 1   |
| PLASTICITY INDEX (PI) DRY STRENGTH NON PLASTIC 0-5 VERY LOW   | CME-550 HARD FACED FINGER BITS -N  | FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS:  |   |
| SLIGHTLY PLASTIC 6-15 SLIGHT  | VANE SHEAR TEST CASING W/ ADVANCER HAND TOOLS:   | GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.   |   |
| MODERATELY PLASTIC 16-25 MEDIUM HIGHLY PLASTIC 26 OR MORE HIGH  | POST HOLE DIGGER   | MODERATELY INDURATED  GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER,   |   |
| COLOR   | TRICOUS AND AUGER  | CRAINC ARE DIFFICULT TO SEPARATE WITH STEEL PROPE.  |   |
|   | The solution rob   | INDURATED DIFFICULT TO BREAK WITH HAMMER.   |   |
| DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY).  MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.             | CORE BIT VANE SHEAR TEST   | EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE;  |   |
| FIGURE 1213 SOCIETAS ELOTTE DETECT FOR SECURE FOR DESCRIBE FOR DESCRIBE   |  | SAMPLE BREAKS ACROSS GRAINS.  | DATE: 8-15-1  |



### GEOTECHNICAL BORING REPORT BORE LOG

| WD0 50005 4.4                                       | BORE LOC                  |  |                    | WD0 500        | 25.4.4   |            |             | 11.5000   | INTERVALENCE | 25000        | 2501 20125     |   |
|---|---------------------------|--|--------------------|----------------|--|------------|-------------|---|--------------|--------------|----------------|---|
| WBS 50225.1.1 TIP U-5                               |                           |  | 201112 1455 (6)    | WBS 5022       |  | 100        |             |   | JNTY RUTHER  |              | GEOLOGIST      |   |
| SITE DESCRIPTION Widening of SR 2241 (              |                           | · · · · · · · · · · · · · · · · · · ·                              | ` ' [              |                |  |            | <del></del> | 41 (Oak Street Extension  |              |              |                | GROUND WTR (ft)   |
| BORING NO. RW-1 STATION                             |                           |  |                    | BORING N       |  |            |             | TION 42+50  | OFFSET       |              | ALIGNMENT      |   |
|   | EPTH 20.6 ft NORTHING 58  |  |                    | COLLAR E       |  |            |             | AL DEPTH 20.5 ft  | NORTHING     |              | EASTING 1      |   |
| DRILL RIG/HAMMER EFF./DATE HPC0279 Diedrich         |                           |  |                    |                |  | F./DATE    |             | edrich D50 88% 11/02/2016   |              | DRILL METHOD |                | HAMMER TYPE Automatic   |
| DDIVE   | ATE 08/21/17 COMP. DATE ( |  |                    | DRILLER  DRIVE | - 1 1  |            |             | RT DATE 08/21/17  |              | TE 08/21/17  | SURFACE W      | ATER DEPTH N/A  |
| ELEV (ft) DEPTH BLOW COUNT (ft) 0.5ft 0.5ft 0.5ft 0 |                           | AMP. L O SOIL AND ROCK DESCRIPTI                                   | TION<br>DEPTH (ft) | ELEV ELEV (ft) | ,  טבי ייין  | 0.5ft 0.5f |             | BLOWS PER F<br>25 50  | 75 100       | NO. MOI      |                | OIL AND ROCK DESCRIPTION  |
| 970   |                           | 969.2 GROUND SURFACE   | 0.0                | 970            |  |            |             |   |              |              |                |   |
| 969.2 0.0 2 5 6                                     | 1.                        | M ARTIFICIAL FILL  967.2 Stiff, Red-Brown, Fine Sandy SILT (       | (A-4), with2.0     | 966.9          | $\begin{array}{c c} & \downarrow \\ 0.0 \end{array}$ |            |             |   |              |              | 966.9          | GROUND SURFACE 0.0  |
| 965 965.3 3.9 7.                                    |                           | trace clay, mica, and grave  | <u>/el</u> /       | 965            | <u> </u>   | 3 4        | 3           | <b>•</b> 7 · · · · · · · · · · · · · · · · · · ·  |              | М            | 964.9 _ Mediun | ARTIFICIAL FILL  n Stiff, Red-Brown-Gray, Fine Sandy 2.0_               |
| 963.2 + 6.0   3   2   2   44.                       |                           | Very Loose to Loose, Brown-White Silty Fine to Coarse SAND (A-2-5) | ite-Black,         | 962.9          | 4.0  |            |             | •   |              |              | SILT (A        | N-4), with trace clay, mica, and gravel  RESIDUAL                       |
|   |                           | M trace mica and gravel-sized rock fra                             |                    | 960.9          | 6.0  | 3 3        |             | <b>Y</b> <sup>0</sup>   |              | SS-2 31%     |                | Tan-Gray-White, Silty Fine to Coarse ND (A-2-5(0)), with trace mica and |
| 960 960.1 7 9.1 3 3 3 3                             |                           | w  |                    | 960            | <b>†</b>   | 3   3      | 4           | . 7   |              | W            |                | gravel-sized rock fragments   |
|   |                           |  |                    | 957.9          | 9.0  | 3 3        | 4           | :   |              |              | _              |   |
| 955 955.1 14.1                                      |                           |  |                    | 955            | <b>‡</b>   |            |             | <u> </u>  |              |              |                |   |
| 3 3 4   |                           | w .  |                    | 952.9          | 14.0   |            |             |   |              |              | _              |   |
|   |                           |  |                    | 050            | ‡  | 3 3        | 4           | •   |              | W            | _              |   |
| 950 950.1 19.1 3 3 4 7                              |                           | W  | 20.6               | 950            | †  |            |             | <del>   .                       .  </del> |              |              |                |   |
|   |                           | - Boring Terminated at Elevation 94<br>Residual Silty SAND (A-2-5  | 948.6 ft In<br>-5) | 947.9          | 19.0   | 3 4        | 5           |   |              | w            | 946.4          | 20.5  |
|   |                           | 1   <del>L</del>   | ,                  |                | # 1  |            |             | <u> </u>  |              |              | Boring         | Terminated at Elevation 946.4 ft In<br>Residual Silty SAND (A-2-5)      |
|   |                           |  |                    |                | ‡  |            |             |   |              |              | -              | residual only of the (112 of  |
|   |                           |  |                    |                | ‡  |            |             |   |              |              | ‡              |   |
|   |                           |  |                    |                | ‡  |            |             |   |              |              | <u> </u>       |   |
|   |                           |  |                    |                | ‡  |            |             |   |              |              | ţ              |   |
|   |                           |  |                    |                | <b>‡</b>   |            |             |   |              |              | Ł              |   |
|   |                           |  |                    |                | ‡  |            |             |   |              |              | -              |   |
|   |                           |  |                    |                | ‡  |            |             |   |              |              | ţ              |   |
|   |                           |  |                    |                | †  |            |             |   |              |              | -              |   |
|   |                           |  |                    |                | ‡  |            |             |   |              |              | ţ              |   |
|   |                           | <u> </u>   |                    |                | <b>‡</b>   |            |             |   |              |              | Ł              |   |
|   |                           |  |                    |                | ‡  |            |             |   |              |              | ţ              |   |
| 127   |                           |  |                    |                | <u>†</u>   |            |             |   |              |              | E              |   |
|   |                           |  |                    |                | †  |            |             |   |              |              | F              |   |
|   |                           |  |                    |                | <u>†</u>   |            |             |   |              |              | ŧ              |   |
|   |                           | <u>-</u>   |                    |                | <u>†</u>   |            |             |   |              |              | _              |   |
| ž   |                           |  |                    |                | <u>†</u>   |            |             |   |              |              | _              |   |
| 8   |                           |  |                    |                | ± 1  |            |             |   |              |              | E              |   |
|   |                           |  |                    |                | ± 1  |            |             |   |              |              | F              |   |
|   |                           |  |                    |                | ± 1  |            |             |   |              |              | E              |   |
| <u> </u>  |                           |  |                    |                | <del>-</del> 1                                       |            |             |   |              |              | -              |   |
|   |                           |  |                    |                | Ŧ  |            |             |   |              |              | F              |   |
|   |                           |  |                    |                | <u> </u>   |            |             |   |              |              | E              |   |
|   |                           |  |                    |                | Ŧ  |            |             |   |              |              | E              |   |
|   |                           | [  |                    |                | I  |            |             |   |              |              | E              |   |
|   |                           |  |                    |                | Ţ  |            |             |   |              |              | E              |   |
|   |                           |  |                    |                | Ŧ  |            |             |   |              |              | E              |   |
|   |                           |  |                    |                | <b>†</b>   |            |             |   |              |              | F              |   |
| <u> </u>  |                           |  |                    |                | İ  |            |             |   |              |              |                |   |



## GEOTECHNICAL BORING REPORT BORE LOG

SHEET 5

|              |                    |               |        |       |              |                 |           | В              | ORE L     | .OG      |       |       |  |                              |                        |            |
|--------------|--------------------|---------------|--------|-------|--------------|-----------------|-----------|----------------|-----------|----------|-------|-------|--|------------------------------|------------------------|------------|
| WBS          | 50225              | 5.1.1         |        |       | TI           | <b>P</b> U-5833 |           | COUNT          | Y RUTHER  | RFORD    |       |       | GEOLOGIST J. Ericks                                      | on                           |                        |            |
|              |                    |               |        | ening | of SR        | 2241 (Oak       | Street Ex | tension) F     | rom SR 21 | 59 to US | 74 AI | terna | te (-WALL 1-)  |                              | GROUN                  | D WTR (ft) |
| BOR          | ING NO.            | RW-           | 3      |       | S.           | TATION 43       | 3+00      |                | OFFSET    | 54 ft RT |       |       | ALIGNMENT -L-  |                              | 0 HR.                  | 12.5       |
|              | LAR ELE            |               |        |       |              | OTAL DEPT       |           |                | NORTHING  |          |       |       | <b>EASTING</b> 1,137,969                                 |                              | 24 HR.                 | 8.5        |
|              |                    |               | FF./DA | TE HI |              | Diedrich D50    |           |                | T         |          |       |       | .S. Augers   |                              |                        | Automatic  |
| DRIL         | LER J.             | 1             | ı      |       |              | TART DATE       |           |                | COMP. DA  |          |       | 4     | SURFACE WATER DEF  | PTH N/                       | A                      |            |
| ELEV<br>(ft) | LLEV               | DEPTH<br>(ft) | 0.5ft  | 0.5ft | UNT<br>0.5ft |                 |           | PER FOOT<br>50 | 75 100    | SAMP.    | '/    | O     | SOIL AND RO  | CK DESC                      | CRIPTION               |            |
| (1-7)        | (ft)               | (1.7)         | 0.511  | 0.511 | 0.511        |                 | Ĭ .       |                | 100       | NO.      | /MOI  | G     | ELEV. (ft)   |                              |                        | DEPTH (ft  |
|              |                    |               |        |       |              |                 |           |                |           |          |       |       |  |                              |                        |            |
| 965          | 964.3              | 0.0           | 3      | 4     | 4            |                 |           | · · · · ·      |           |          |       | MIN I |  | D SURFA                      |                        | 0.0        |
|              | -                  | _             | 3      | 7     | "            | . • 8           |           |                |           |          | М     |       | 962.3 Medium Stiff, Red-I                                | Brown, Fii                   | ne Sandy S             | SILT2.0    |
| 960          | 960.4              | 3.9           | 3      | 3     | 3            | :¦ · · ·        |           |                |           | 00.0     | 0.40/ |       |  | ith trace o                  |                        | /          |
|              | 958.3              | 6.0           | 3      | 2     | 3            | <b>9</b> 6      |           |                |           | SS-3     | 34%   |       | Loose to N<br>Brown-White-Blac                           | k, Silty Fi                  | ne to Coar             | se         |
| 055          | 955.3 <sup>-</sup> |               |        | _     |              | 5               |           |                |           |          | W     |       | - SAND (A-2-5(0))<br>- gravel-sized                      | , with trace<br>I rock frace | ce mica and<br>gments  | d          |
| 955          | 955.5              | 9.0           | 3      | 3     | 5            | . •8            |           |                |           |          | W     |       | _<br>-   |                              |                        |            |
|              | -                  | _             |        |       |              | : 1 : :         |           |                |           |          |       |       | -<br>-   |                              |                        |            |
| 950          | 950.3              | 14.0          | 4      | 6     | 8            |                 |           |                |           |          |       |       | -<br>_   |                              |                        |            |
|              | -                  | _             | "      | "     | °            | 14.<br><b>/</b> |           |                |           |          | W     |       | <u>-</u><br>-  |                              |                        |            |
|              | -                  | 40.0          |        |       |              | . /             |           |                |           |          |       |       | <u>.</u>   |                              |                        |            |
| 945          | 945.3              | 19.0          | 4      | 3     | 4            | 7               |           |                |           |          | Sat.  |       | <br>_ 943.8  |                              |                        | 20.5       |
|              | -                  | _             |        |       |              |                 |           |                |           |          |       |       | <ul><li>Boring Terminated</li><li>Residual Sil</li></ul> | at Elevat<br>ty SAND         | ion 943.8 f<br>(A-2-5) | t In       |
|              | _                  | L             |        |       |              |                 |           |                |           |          |       |       | -<br><del>-</del>  | •                            | , ,                    |            |
|              | -                  | _             |        |       |              |                 |           |                |           |          |       |       | <u>-</u><br>-  |                              |                        |            |
|              | -                  | <u> </u>      |        |       |              |                 |           |                |           |          |       |       | <u>.</u>   |                              |                        |            |
|              | _                  |               |        |       |              |                 |           |                |           |          |       |       | <u>-</u><br>-  |                              |                        |            |
|              | -                  |               |        |       |              |                 |           |                |           |          |       |       | <b>-</b><br>-  |                              |                        |            |
|              | -                  |               |        |       |              |                 |           |                |           |          |       |       | _  |                              |                        |            |
|              | -                  | F             |        |       |              |                 |           |                |           |          |       |       | -  |                              |                        |            |
|              | -                  | F             |        |       |              |                 |           |                |           |          |       |       | -  |                              |                        |            |
|              | _                  | F             |        |       |              |                 |           |                |           |          |       |       | -<br>-   |                              |                        |            |
|              | -                  | F             |        |       |              |                 |           |                |           |          |       |       | -  |                              |                        |            |
|              | -                  | F             |        |       |              |                 |           |                |           |          |       |       | -  |                              |                        |            |
|              | -                  | F             |        |       |              |                 |           |                |           |          |       |       | <del>-</del><br>-  |                              |                        |            |
|              | -                  | F             |        |       |              |                 |           |                |           |          |       |       | -<br>-   |                              |                        |            |
|              | _                  | F             |        |       |              |                 |           |                |           |          |       |       | <u>-</u>   |                              |                        |            |
|              | -                  | -             |        |       |              |                 |           |                |           |          |       |       | <del>-</del><br>-  |                              |                        |            |
|              | -                  | <u> </u>      |        |       |              |                 |           |                |           |          |       |       | -<br>-   |                              |                        |            |
|              | -                  | -             |        |       |              |                 |           |                |           |          |       |       | <del>-</del><br>-  |                              |                        |            |
|              | -                  | ļ.            |        |       |              |                 |           |                |           |          |       |       | <del>-</del><br>-  |                              |                        |            |
|              | _                  | _             |        |       |              |                 |           |                |           |          |       |       | -<br>-   |                              |                        |            |
|              | -                  | <b>†</b>      |        |       |              |                 |           |                |           |          |       |       | <del>-</del><br>-  |                              |                        |            |
|              | -                  | <u> </u>      |        |       |              |                 |           |                |           |          |       |       | <del>-</del><br>-  |                              |                        |            |
|              | _                  | ‡<br>F        |        |       |              |                 |           |                |           |          |       |       | <del>-</del><br>-  |                              |                        |            |
|              | -                  | <u> </u>      |        |       |              |                 |           |                |           |          |       |       | <del>-</del><br>-  |                              |                        |            |
|              | _                  | <u> </u>      |        |       |              |                 |           |                |           |          |       |       | -<br><del>-</del>  |                              |                        |            |
|              | -                  | <u> </u>      |        |       |              |                 |           |                |           |          |       |       | -<br>-   |                              |                        |            |
|              | -                  | <u> </u>      |        |       |              |                 |           |                |           |          |       |       | -<br>-   |                              |                        |            |
|              | _                  | <u> </u>      |        |       |              |                 |           |                |           |          |       |       | <br>-  |                              |                        |            |
|              | -                  | ‡             |        |       |              |                 |           |                |           |          |       |       | -<br>-   |                              |                        |            |
|              | -                  | +             |        |       |              |                 |           |                |           |          |       |       | -  |                              |                        |            |

| PROJECT REFERENCE NO. | SHEET NO. |
|-----------------------|-----------|
| U-5833                | 6         |

| SOIL TEST RESULTS |        |          |           |            |          |             |      |         |         |      |                    |      |      |      |          |         |
|-------------------|--------|----------|-----------|------------|----------|-------------|------|---------|---------|------|--------------------|------|------|------|----------|---------|
| BORING            | SAMPLE | OFFSET   | STATION   | DEPTH      | AASHTO   | т т         | D I  |         | % BY W  |      | % PASSING (SIEVES) |      |      | %    | %        |         |
| NO.               | NO.    | OFFSEI   |           | INTERVAL   | CLASS.   | $\mid L.L.$ | P.I. | C. SAND | F. SAND | SILT | CLAY               | 10   | 40   | 200  | MOISTURE | ORGANIC |
| RW-1              | SS-1   | 53' RT   | 41+60 -L- | 3.9 - 5.4' | A-2-5(0) | 48          | 1    | 37.5    | 32.0    | 7.2  | 23.3               | 91.0 | 65.0 | 35.0 | 35.7     | _       |
| RW-2              | SS-2   | 53' RT   | 42+50 -L- | 4.0 - 5.5' | A-2-5(0) | 44          | NP   | 27.1    | 45.7    | 5.1  | 22.1               | 97.0 | 82.0 | 35.0 | 30.6     | _       |
| RW-3              | SS-3   | 54' $RT$ | 43+00 -L- | 3.9 - 5.4' | A-2-5(0) | 46          | NP   | 42.4    | 30.2    | 12.0 | 15.5               | 95.0 | 65.0 | 32.0 | 34.0     | _       |

LAB TECHNICIAN: AMANDA ROTH NCDOT CERTIFICATION NO. 112-09-1003

SIGNATURE: