### SEE SHEET 3 FOR PLAN SHEET LAYOUT AT TIME OF INVESTIGATION

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# STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT** 

# **STRUCTURE** SUBSURFACE INVESTIGATION

COUNTY LENOIR

PROJECT DESCRIPTION C.F. HARVEY PARKWAY AND NC 58 TO INTERSECTION OF NC 11 AND GRANGER STATION ROAD GRADING, PAVING, DRAINAGE, STRUCTURES AND SIGNALS SITE DESCRIPTION BRIDGE NO. 208 AND NO. 209 ON -L-(FELIX HARVEY PARKWAY) OVER -Y1- (NC 58) BETWEEN SR 1581 AND SR 1730

**INVENTORY** 

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5703	1	42

### CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF PREPARING THE SCOPE OF WORK TO BE INCLUDED IN THE REQUEST FOR PROPOSAL. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVEMED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT 1919/107-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

SOIL AND ROCK BOUNDARIES WITHIN A BOREHOLE ARE BASED ON GEOTECHNICAL INTERPRETATION UNLESS ENCOUNTERED IN A SAMPLE. INTERPRETED BOUNDARIES MAY NOT NECESSARILY REFLECT ACTUAL SUBSURFACE CONDITIONS BETWEEN SAMPLED STRATA AND BOREHOLE INFORMATION MAY NOT NECESSARILY REFLECT ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABULTY INHERENT IN THE STADNARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL WOISTURE CONDITIONS. BINICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING THMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT, FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONS TO BE ENCOUNTERED ON THE EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL COMPENSATION OF FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SIDER FRING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION,

- NOTES: I. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N.C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT. 2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE. DEPCONNETI

PERSONNEL

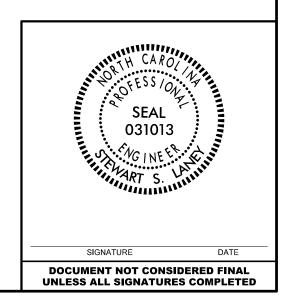
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SUBMITTED BY \_\_\_\_\_S&ME, INC.



# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION

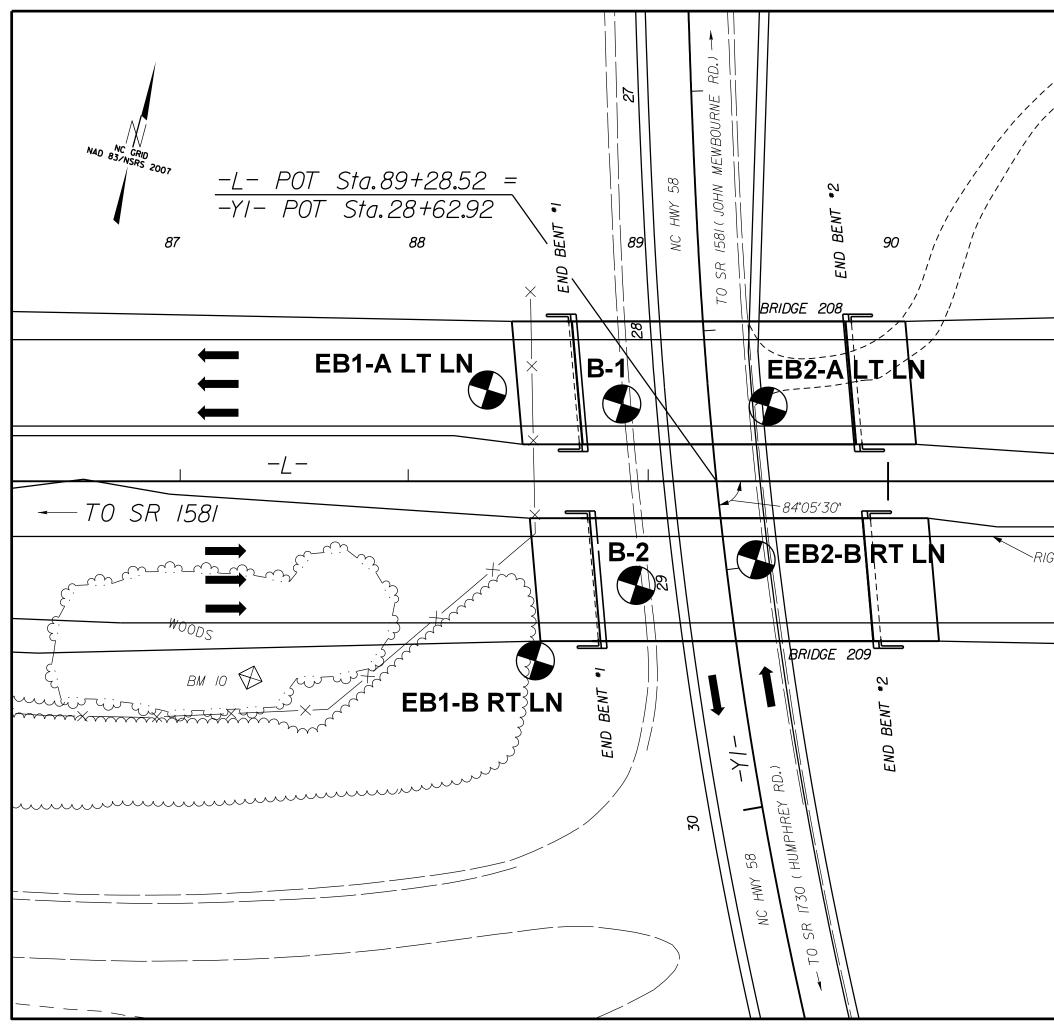
SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION	GRADATION	ROCK DESCRIPTION							
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN	WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.	HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD S							
BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM DI586). SOIL CLASSIFICATION	UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.	SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 F							
IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH	ANGULARITY OF GRAINS	BLOWS IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK IS REPRESENTED BY A ZONE OF WEATHERED ROCK.							
AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE,	THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS:	ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:							
VERY STIFF.GRAY.SILTY CLAY.MOIST WITH INTERBEDDED FINE SAND LAYERS.HIGHLY PLASTIC.A-7-6	ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.	WEATHERED NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N							
SOIL LEGEND AND AASHTO CLASSIFICATION	MINERALOGICAL COMPOSITION	ROCK (WR) 100 BLOWS PER FOOT IF TESTED.							
GENERAL         GRANULAR MATERIALS         SILT-CLAY MATERIALS         ORGANIC MATERIALS           CLASS.         ( ≤ 35% PASSING *200)         ( > 35% PASSING *200)         ORGANIC MATERIALS	MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC.	CRYSTALLINE FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK ROCK (CR) FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK							
GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5	ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.	COLE COLOR C							
CLASS. A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-7-5 A-3 A-6, A-7	COMPRESSIBILITY	POCK (NCP)							
SYMBOL SCORE	SLIGHTLY COMPRESSIBLE LL < 31 MODERATELY COMPRESSIBLE LL = 31 - 50	COASTAL PLAIN COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT M.							
2, PASSING	HIGHLY COMPRESSIBLE LL > 50	SEDIMENTARY ROCK SPT REFUSAL, ROCK TYPE INCLUDES LIMESTONE, SANDSTO							
*10 50 MX GRANULAR SIL1- MUCK.	PERCENTAGE OF MATERIAL	(CP) HELL BEDS, ETC.							
*40 30 MX 50 MX 51 MN *200 15 MX 25 MX 10 MX 35 MX 35 MX 35 MX 35 MX 36 MN 36 MN 36 MN 36 MN	GRANULAR SILT - CLAY ORGANIC MATERIAL SOILS OTHER MATERIAL								
	<u>ORGANIC MATERIAL</u> <u>SOILS</u> <u>OTHER MATERIAL</u> TRACE OF ORGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10%	FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RII HAMMER IF CRYSTALLINE.							
PASSING #40	LITTLE ORGANIC MATTER 3 - 5% 5 - 12% LITTLE 10 - 20%	VERY SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COA							
LL – – 40 MX 41 MN LLITLE OR PI 6 MX NP 10 MX 10 MX 11 MN 11 MN 10 MX 10 MX 11 MN 11 MN LLITLE OR HIGHLY	MODERATELY         ORGANIC         5         - 10%         12         - 20%         SOME         20         - 35%           HIGHLY         ORGANIC         > 10%         > 20%         HIGHLY         35%         AND ABOVE	(V SLI.) CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY, ROCK RINGS UNDER HAM							
GROUP INDEX 0 0 0 4 MX 8 MX 12 MX 16 MX 0 MX AMOUNTS OF	GROUND WATER	OF A CRYSTALLINE NATURE.							
ORGANIC SUILS		SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK (SLI.) 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL I							
USUAL TYPES STONE FRAGS. FINE SILTY OR CLAYEY SILTY CLAYEY MATTER	✓ WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING	CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER B							
MATERIALS SAND SAND GRAVEL AND SAND SOILS SOILS	STATIC WATER LEVEL AFTER HOURS	MODERATE SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS.							
GEN. RATING EXCELLENT TO GOOD FAIR TO POOR POOR UNSUITABLE	$\nabla PW$ PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA	(MOD.) GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH A							
	SPRING OR SEEP	WITH FRESH ROCK.							
PI OF A-7-5 SUBGROUP IS $\leq$ LL - 30 ;PI OF A-7-6 SUBGROUP IS > LL - 30		MODERATELY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FEL							
CONSISTENCY OR DENSENESS	MISCELLANEOUS SYMBOLS	SEVERE AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOS: (MOD. SEV.) AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WH							
PRIMARY SOIL TYPE COMPACTNESS OR CONSISTENCY PENETRATION RESISTENCE COMPRESSIVE STRENGTH	ROADWAY EMBANKMENT (RE) 25/025 DIP & DIP DIRECTION	IF TESTED, WOULD YIELD SPT REFUSAL							
(TONS/FT <sup>2</sup> )	WITH SOIL DESCRIPTION DE ROCK STRUCTURES	SEVERE ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVID							
GENERALLY VERY LOOSE < 4 DOUBLE 4 TO 10	SOIL SYMBOL	(SEV.) REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN.							
GRANULAR MEDIUM DENSE 10 TO 30 N/A		IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF							
MATERIAL DENSE 30 TO 50		VERY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE							
VERY DENSE > 50	I INFERRED SOIL BOUNDARY - CORE BORING • SOUNDING ROD	SEVERE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF S (V SEV.) REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT O							
VERY SOFT         < 2         < 0.25           GENERALLY         SOFT         2 TO 4         0.25 TO 0.5	Ý	VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. IF TESTED, WOULD YIELD SPT N VAL							
SILT-CLAY MEDIUM STIFF 4 TO 8 0.5 TO 1.0	TITE/TTE INFERRED ROCK LINE MONITORING WELL TEST BORING WITH CORE	COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN							
MATERIAL         STIFF         8 T0 15         1 T0 2           (COHESIVE)         VERY STIFF         15 T0 30         2 T0 4		SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS.							
HARD > 30 > 4	INSTALLATION	ROCK HARDNESS							
TEXTURE OR GRAIN SIZE	RECOMMENDATION SYMBOLS	VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS F							
U.S. STD. SIEVE SIZE 4 10 40 60 200 270	UNDERCUT UNCLASSIFIED EXCAVATION - UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE	SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.							
OPENING (MM)         4.76         2.00         0.42         0.25         0.075         0.053	SHALLOW INCLASSIFIED EXCAVATION - USED IN THE TUP 3 FEET OF	HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOD							
BOULDER COBBLE GRAVEL COARSE FINE SILT CLAY	UNDERCUT ACCEPTABLE DEGRADABLE ROCK EMBANKMENT OR BACKFILL	TO DETACH HAND SPECIMEN.							
(BLDR.) (COB.) (GR.) (CSE. SD.) (F SD.) (CL.)	ABBREVIATIONS	MODERATELY CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEF HARD EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DET							
GRAIN MM 305 75 2.0 0.25 0.05 0.005	AR - AUGER REFUSAL MED MEDIUM VST - VANE SHEAR TEST	BY MODERATE BLOWS.							
SIZE IN. 12 3	BT - BORING TERMINATED MICA MICACEOUS WEA WEATHERED	MEDIUM CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR							
SOIL MOISTURE - CORRELATION OF TERMS	CLCLAY MODMODERATELY $\gamma$ -UNIT WEIGHT CPT - CONE PENETRATION TEST NP - NON PLASTIC $\gamma_{ m A}$ -DRY UNIT WEIGHT	HARD CAN BE EXCAVATED IN SMALL CHIPS TO PEICES 1 INCH MAXIMUM SIZE BY HARD BL POINT OF A GEOLOGIST'S PICK.							
SOIL MOISTURE SCALE FIELD MOISTURE CHIDE FOR FIELD MOISTURE DESCRIPTION	CSE COARSE ORG ORGANIC	SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FF							
(ATTERBERG LIMITS) DESCRIPTION BOILD + 6K FIELD HOISTOKE DESCRIPTION	DMT - DILATOMETER TEST PMT - PRESSUREMETER TEST <u>SAMPLE ABBREVIATIONS</u> DPT - DYNAMIC PENETRATION TEST SAP SAPROLITIC S - BULK	FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT.							
- SATURATED - USUALLY LIQUID; VERY WET, USUALLY	DPT         - DYNAMIC         PENETRATION         TEST         SAP SAPROLITIC         S - BULK           e         - VOID         RATIO         SD SAND, SANDY         SS - SPLIT         SPOON	PIECES CAN BE BROKEN BY FINGER PRESSURE.							
(SAT.) FROM BELOW THE GROUND WATER TABLE	F - FINE SL SILT, SILTY ST - SHELBY TUBE	VERY CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PI SOFT OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED							
	FOSS FOSSILIFEROUS SLI SLIGHTLY RS - ROCK FRAC FRACTURED, FRACTURES TCR - TRICONE REFUSAL RT - RECOMPACTED TRIAXIAL	FINGERNAIL.							
RANGE - WET - (W) SEMISOLID; REOUIRES DRYING TO ATTAIN OPTIMUM MOISTURE	FRAGS FRAGMENTS W - MOISTURE CONTENT CBR - CALIFORNIA BEARING	FRACTURE SPACING BEDDING							
	HI HIGHLY V - VERY RATIO	TERM SPACING TERM TH							
- MOIST - (M) SOLID: AT OR NEAR OPTIMUM MOISTURE	EQUIPMENT USED ON SUBJECT PROJECT	VERY WIDE MORE THAN 10 FEET VERY THICKLY BEDDED 4 WIDE 3 TO 10 FEET THICKLY BEDDED 1.5							
	DRILL UNITS: ADVANCING TOOLS: HAMMER TYPE:	MODERATELY CLOSE 1 TO 3 FEET THINLY BEDDED 0.16							
	CME-45C CLAY BITS X AUTOMATIC MANUAL	CLOSE         Ø.16 TO 1 FOOT         VERY THINLY BEDDED         Ø.03           VERY CLOSE         LESS THAN Ø.16 FEET         THICKLY LAMINATED         Ø.008							
- DRY - (D) ATTAIN OPTIMUM MOISTURE	CME-55 G* CONTINUOUS FLIGHT AUGER CORE SIZE:	THINKET EMMINITED 40.							
PLASTICITY	8" HOLLOW AUGERS	INDURATION							
PLASTICITY INDEX (PI) DRY STRENGTH	CME-550     HARD FACED FINGER BITS	FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT							
NON PLASTIC 0-5 VERY LOW	TUNGCARBIDE INSERTS	FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS;							
SLIGHTLY PLASTIC 6-15 SLIGHT		GENILE BLUW BY HAMMER DISINIEGRAIES SAMPLE.							
MODERATELY PLASTIC 16-25 MEDIUM HIGHLY PLASTIC 26 OR MORE HIGH		MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEE BREAKS EASILY WHEN HIT WITH HAMMER,							
COLOR									
		INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PR DIFFICULT TO BREAK WITH HAMMER.							
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY).									
MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.	X <u>D-25</u>	EXTREMELY INDURATED SAMPLE BREAKS ACROSS GRAINS.							

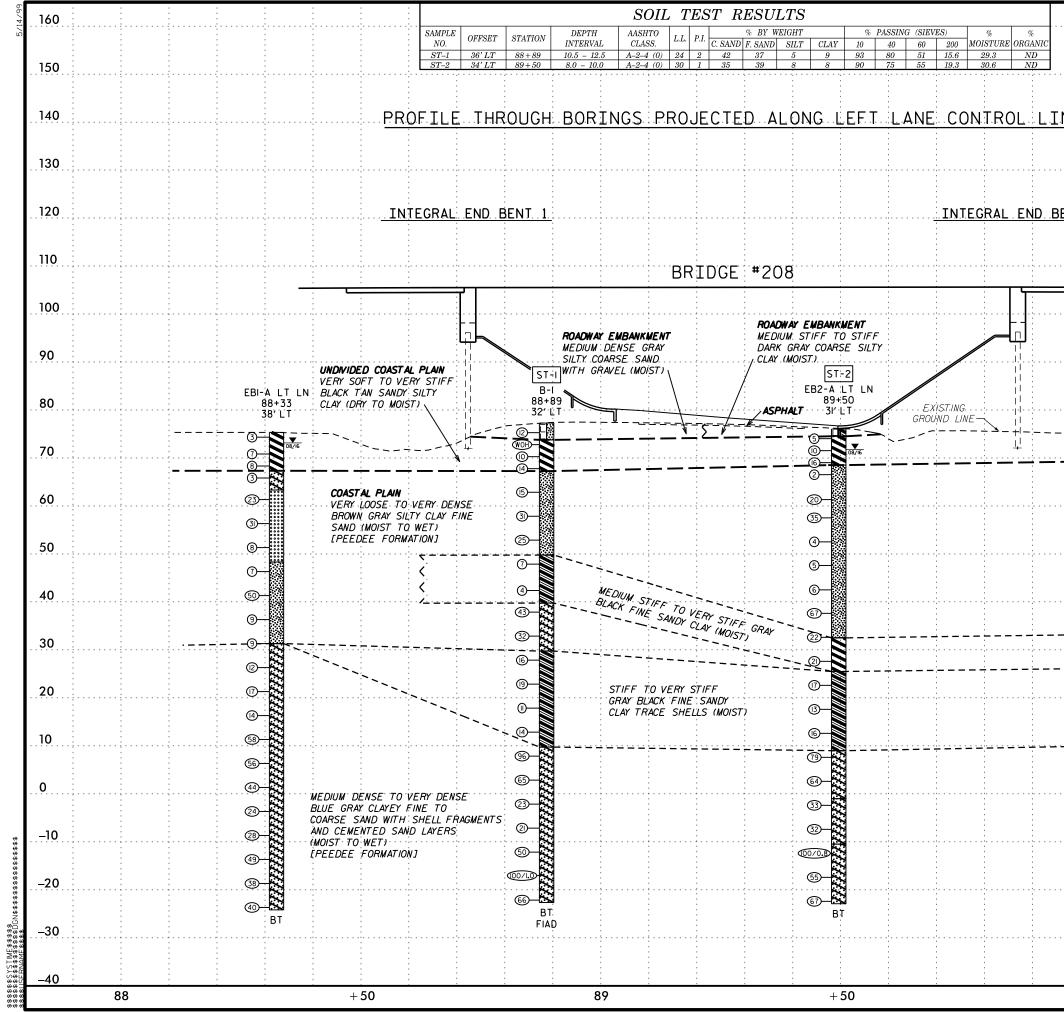




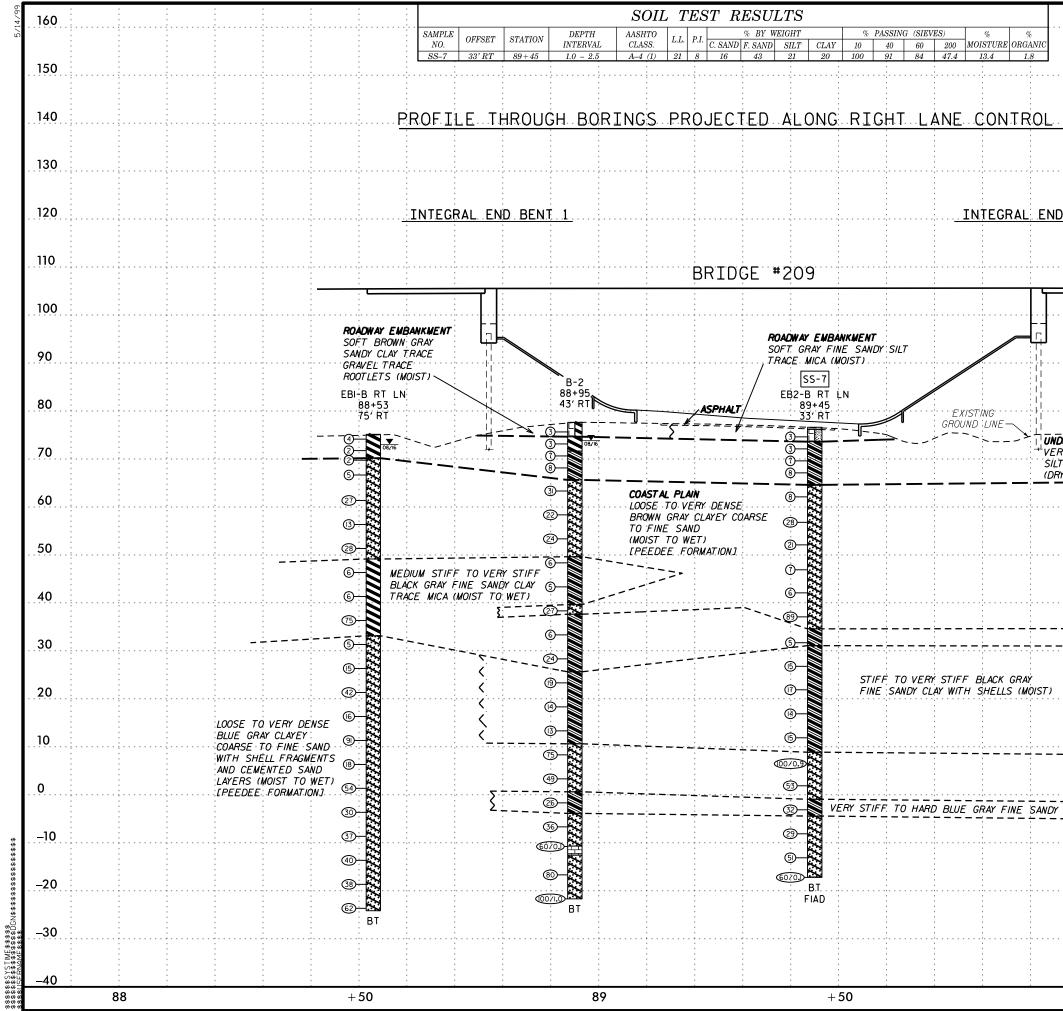
	TERMS AND DEFINITIONS
TED. AN INFERRED .D SPT REFUSAL.	ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
0.1 FOOT PER 60	AUUIFER - A WATER BEARING FORMATION OR STRATA.
< IS OFTEN	ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
	ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING
PT N VALUES >	A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. <u>ARTESIAN</u> - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT
ROCK THAT INCLUDES GRANITE,	WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
TAL PLAIN	CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
. IF TESTED. TC.	$\underline{\text{COLLUVIUM}}$ - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.
T MAY NOT YIELD DSTONE, CEMENTED	CORE RECOVERY (REC.)- TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
	DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
K RINGS UNDER	$\underline{\text{DIP}}$ - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.
COATINGS IF OPEN, HAMMER BLOWS IF	DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
Rock up to NAL Feldspar	FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
ER BLOWS.	FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.
TS. IN _AY. ROCK HAS	FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.
TH AS COMPARED	FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM,
FELDSPARS DULL LOSS OF STRENGTH	FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.
) WHEN STRUCK.	JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
EVIDENT BUT ARE KAOLINIZED	<u>LEDEC</u> - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOLL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
	MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS
	USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
ARE DISCERNIBLE OF STRONG ROCK	PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE
AT ONLY MINOR	OF AN INTERVENING IMPERVIOUS STRATUM.
VALUES < 100 BPF	RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
Y IN SMALL AND RS. SAPROLITE IS	ROCK DUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SECMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
INS REQUIRES	SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
BLOWS REQUIRED	<u>SILL</u> - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEODING OR SCHISTOSITY OF THE INTRUDED ROCKS.
DEEP CAN BE	SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
DETACHED	ON SLIF PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE)(SPT) - NUMBER OF BLOWS (N OR BPF)OF
OR PICK POINT. D BLOWS OF THE	STANDARD FENETATION TEST FRENETATION RESISTANCE/TSFT) - NOMBER OF BLOWS IN OR BFF.OF A 140 LB.HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
N FRAGMENTS INT. SMALL, THIN	<u>STRATA CORE RECOVERY (SREC.)</u> - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
K. PIECES 1 INCH	STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
CHED READILY BY	TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
	BENCH MARK: 81.85 FEET RIGHT -L- 87+34 BM IO RR SPIKE IN BASE
THICKNESS 4 FEET	OF 24" PINE
1.5 - 4 FEET	<u>N 577,986.3920 E 2,422,782.2840</u> ELEVATION: 76.99 FEET
0.16 - 1.5 FEET	NOTES:
.03 - 0.16 FEET 008 - 0.03 FEET	FIAD - FILLED IMMEDIATLEY AFTER DRILLING
< 0.008 FEET	
HEAT, PRESSURE, ETC.	
-	
E.	
STEEL PROBE:	
PROBE:	



	PROJECT REFERENCE NO. SHEET NO.
	R-5703 3
	SITE PLAN
	FEET
	SKEW 84°05′30"
	SITE I
91	92
51	52
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	CONTROLINE
	CONTROL LINE
	TO SR 1004
IGHT CONTROL LINE	
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			FROM PR FOR BRID OVER NC SR 1730	LINE 23 ELIMINARY GE ON C. HWY 58	FEET LEF ( GENERAL F.HARVE) BETWEEN	T OF -L DRAWING PARKWA SR 1581 A	Y ND	_20 _30
								_10
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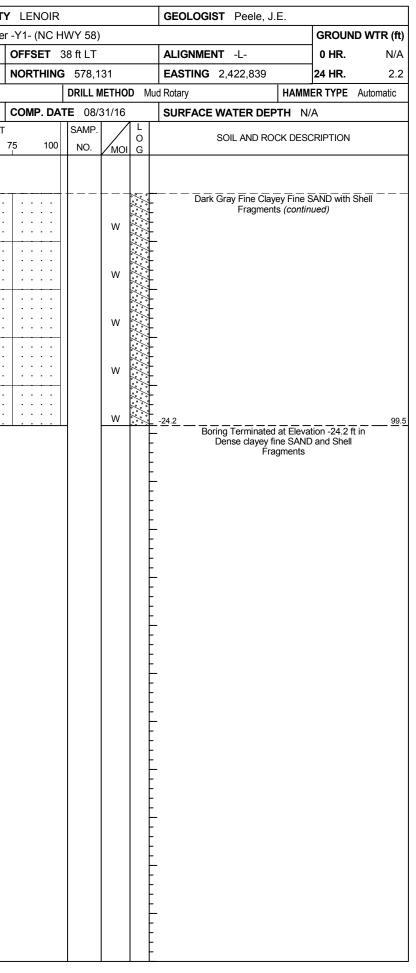


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			REFERENCE NO	). 	sheet no. 5
		ROADWAY ENGIN			D RAULICS GINEER
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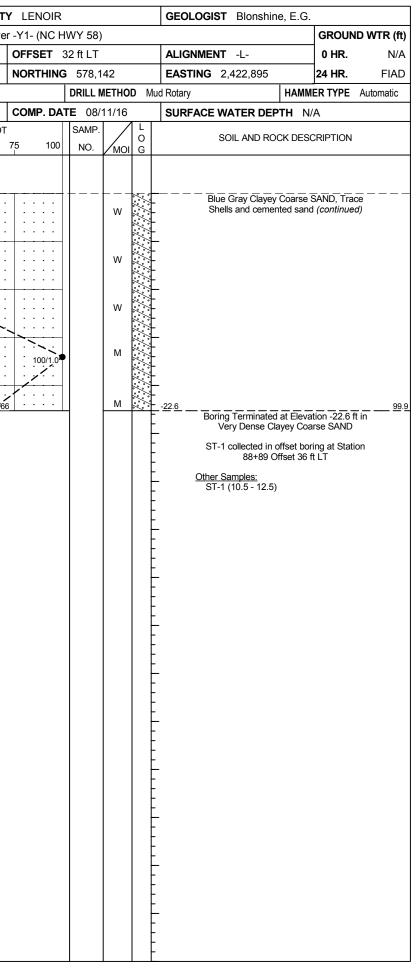
STE BESCHTUN Horse hourse hour	WBS	4637	5.1.1		TIP         R-5703         COUNTY         LENOIR           Bridge No. 208 on -L- (Felix Harvey Pkwy) over -Y1- (NC HWY 58)							BEOLOGIST Peele, J.E.						WBS	46375	5.1.1			TIP R-5703 COUNTY				
COLLAR ELEV. 75.1         TOTAL DEFIT: 95.1         MORTING 576.11         EATING 2-422.80         Jale 12.2         COLLAR ELEV. 75.1         TOTAL DEFIT: 95.1         STATT DATE 005016           PELLER FOME: A         STATT DATE 005016         COMP DATE 0050176         SUMPACE WATER DEFIT: NA         STATT DATE 005016         STATT DATE 005016           100         100         200         200         200         100         SUMPACE WATER DEFIT: NA         STATT DATE 0050176           100         200         200         200         200         200         100	SITE	DESCF	RIPTIO	N Brid	lge No	. 208	on -L- (Felix	k Harvey P	vkwy) ove	r -Y1- (NC	HWY 58	3)				GROUND W	TR (ft)	SITE	DESCR		l Brid	ge No	. 208 o	n -L- (Felix	Harvey P	kwy) over	
DBLLB (NUMBER EFF ART. NOVES)         DBLL APTION Los Party         DBLLB (NUMBER EFF ART. NOVES)         DBLL (NUMBER EFF ART. NOVES)         DBLLB (NUMER EFF ART. NOVES)         DBLLB (NUMER EF	BOR	ing no	<b>).</b> EB1	-A Lt.	Ln.	S	TATION 88	8+33		OFFSET	38 ft LT	Г		ALIGN	MENT -L-	0 HR.	N/A	BOR	ING NO.	. EB1-	A Lt. L	.n.	ST	ATION 88	3+33		
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#### SHEET 6 OF 42



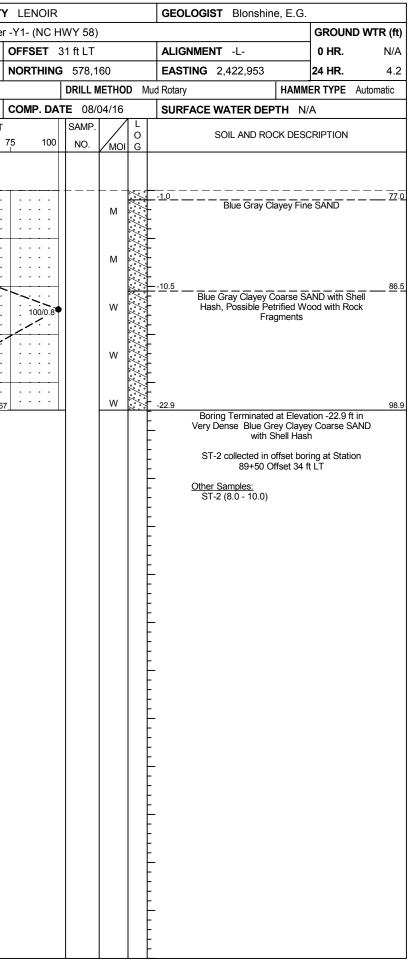
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	NG NO.		Brid	ge No		on -L- (Feli	-	Pkwy) o		OFFSET		-			NMENT -L-		JND WTR (ft)		ING NO		Bric	ige No		on -L- (Felix		Ркwy) с	ver -
	AR ELI		'3ft		_	OTAL DEP		) ft	_	NORTHIN				_	<b>ING</b> 2,422,895	24 HR					7 3 ft		_	TAL DEPI		ft	+
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(ft)	ELEV (ft)	(ft)	0.5ft	0.5ft	0.5ft	0	25	50	7	5 100	NO.	Имс	DI G	ELEV. (f	SOIL AND ROCK	DESCRIPTIC	DEPTH (ft)	(ft)	ELEV (ft)	(ft)	0.5ft	0.5ft	0.5ft	0 2	25	50	7
80		Ļ												_				0		L					Mat	ch Line	
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75	76.3	1.0	7	8	4				· · · ·			м		-	ROADWAY EM Gray Silty Coarse S		avel	-5		ŧ							
-	73.8	3.5	WOH	WOH	WOH									73.8			3.5		-6.1	83.4	6	9	12		<u> </u>		
	71.3	6.0			-	<b>•</b> 0				· · · · ·		M		-	Tan Coarse Sandy Silty					Ŧ					$1 \cdot \cdot$		•
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10	-	ŧ.					- ? ~			 				_ <u>9.8</u>			67.5		·	‡							
	8.9 -	68.4	21	56	40		· · · ·	·   · · ·	:		96	м		-	Blue Gray Clayey Coa Shells and cerr	arse SAND, T nented sand	race		-	‡							
5	-	ŧ				· · · ·		 	I		Ĩ.			-					· ·	‡							
5	3.9	- 73.4	14	00	07		+		. ,		11		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	-					-	‡							
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#### SHEET 7 OF 42



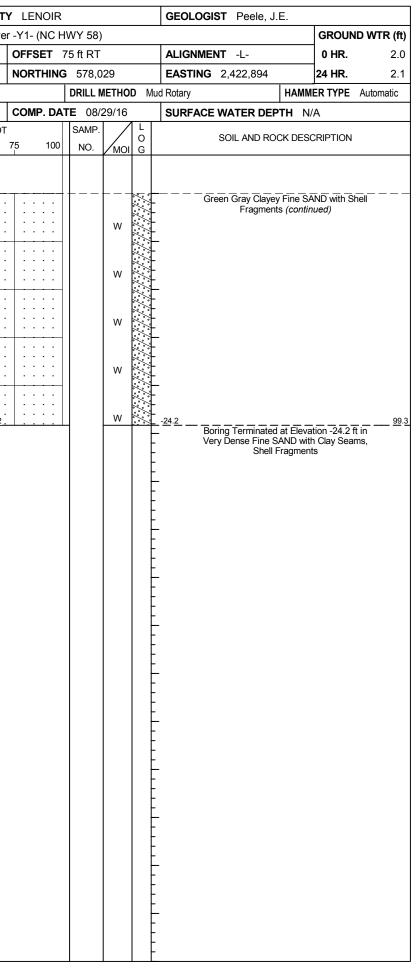
	VBS         46375.1.1         TIP         R-5703         COUNTY         LENOIR           SITE DESCRIPTION         Bridge No. 208 on -L- (Felix Harvey Pkwy) over -Y1- (NC HWY 58)         SORING NO.         EB2-A Lt. Ln.         STATION         89+50         OFFSET         31 ft LT														46375				TI	COUN								
				-		-		-	vkwy) ove				)			NMENT -L-	-									ix Harvey	Pkwy) ov	er -
		EV. 76				OTAL DE			+	NORTHI			60		_	<b>ING</b> 2,422,953	0 HR. 24 HR.	N/A 4.2	-	ING NO.			Ln.			<b>PTH</b> 98.9	#	+
						CME-550								ח חו	Iud Rotary		IER TYPE Autom						TE HE			2% 12/09/20		
		Vhite, J								COMP. D										LER W						E 08/03/		C
	DRIVE			ow co					PER FOOT			SAMP.		1 L					ELEV		DEPTH						PER FOC	
(ft)	ELEV (ft)	(ft)	·		0.5ft	0	25		50			NO.	мо	O I G	ELEV. (f	SOIL AND ROCK DES		PTH (ft)	(ft)	ELEV (ft)	(ft)	·	0.5ft		0	25	50	75
	. ,									-					,	/												
80																			0							Mat	ch Line	
	-	Ŧ													E					-1.4	77.4	8	12	21				·
	-	Ŧ													76.0	GROUND SURF	ACE	0.0		-	F		12			<b>.</b>		
75	75.0	1.0	4	3	2		-						м	Ŧ	- 74.5	ROADWAY EMBAN \ Dark Gray Coarse Sandy CL		1.5	-5	-								
	72.5	3.5	3	3	7						.				F	UNDIVIDED COASTA Gray Fine Sandy (	L PLAIN			-6.4 -	82.4	10	14	18		•32		:
70	70.0	F 6.0		3	'	<u>`</u>							<u>—</u> м–		F	Gray Tille Salidy (			-10	-	F							•
	-	Ŧ	6	8	8		16						м		68.5			7.5		-11.4 -	87.4	12	87/0.3					
	67.5	<u>† 8.5</u> 	2	1	1	• • • •				•   • • • •			w		-	Dark Gray/Black Clayey	Fine SAND			-	Ŧ		01/0.3					
65	-	Ŧ					•								-	[Peedee Format	ion]		-15		<b>F</b>							
	62.3	† † 13.7					-				.				-					-16.4 -	92.4	24	25	30			<b>4</b> 55	
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	58.5	17.5						<u>,</u>							-					-21.4 -	97.4		07					
	-	ŧ	14	15	20		•	<b>3</b> 5		· · · · ·	•		M		-						<u>+</u>	49	37	30				67
55	-	‡					./	· · · ·			·				-					-	ŧ							
-	53.5	22.5	3	2	2			· · · · ·			.		м		F					-	ŧ							
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-	43.5	32.5	WOH	2	4			· · · ·							L					-	Ł							
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	-	Ī			Ű		. <b>●</b> 22						M		- 52.5	Dark Gray/Black Fine Sa	andy CLAY	43.5		-	E							
30	28.6 -	Ŧ,,													F					_	F							
	- 20.0	+ 47.4 T	5	11	10		↓ ↓21				.		м		F					-	F							
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┝	8.6	+ 67.4 +	24	29	50			· · · · · · · ·			:		м		⊢≝.º	Blueish Dark Gray Clayey Co	arse SAND with	<u>67</u> .0		-	ŧ							
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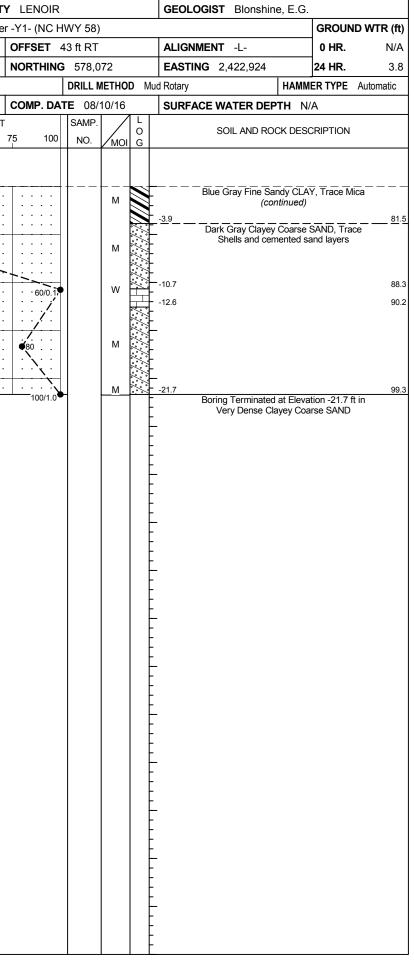


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	ING NO.			-		TATION 8		Pkwy) Ove	OFFSET		-			SNMENT -L-		0 HR.	• •		ING NO					ATION 8		-kwy) over
-				_11.	_			<i>c</i> .					_				2.0	-				LN.				
								π	NORTHIN				LAS Iud Rotar	TING 2,422,894		24 HR. ER TYPE Autom	2.1							DTAL DEP		t l
						D-25 90% 08/		10					_	,			atic									
				W COL				PER FOOT	COMP. DA	SAMP.		) / [ ]	SUR	FACE WATER DEF	IH N/	A			LER F			W COL				PER FOOT
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80		-											_					0		<u>+</u>			i — — †			h Line
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	70.7	- 4.4	1	1	1						м		-						-7.7	<u>† 82.8</u> 1	8	13	24	· · · ·	÷.	
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	62.3	- 12.8	7	14	13						W		-						-17.7	<u>† 92.8</u> †	13	16	22		· · · · · · · · · · · · · · · · · · ·	
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STE DESCRIPTION       Biology No. 200 or 1 (Feld, Harvey Phany Cover V <sup>+</sup> ): (V PWY SP)       OPCURE VM PW SP         DERUND VM, PM       TOTAL DEPTH       0.1       DATE DESCRIPTION       Disclamation         DERUND VM, PM       TOTAL DEPTH       0.1       DATE DESCRIPTION       Disclamation         DERUND VM, PM       TOTAL DEPTH       0.1       DERUND VM, PM       Disclamation         DERUND VM, PM       TOTAL DEPTH       0.1       DERUND VM, PM       Disclamation         DERUND VM, PM       TOTAL DEPTH       0.1       DERUND VM, PM       Disclamation         DERUND VM, PM       TOTAL DEPTH       0.1       DERUND VM, PM       Disclamation         DERUND VM, PM       TOTAL DEPTH       0.1       DISCLAMATION VM, PM       DISCLAMATION VM, PM         DERUND VM, PM       TOTAL DEPTH       DISCLAMATION VM, PM       DISCLAMATION VM, PM       DISCLAMATION VM, PM         DERUND VM, PM       TOTAL DEPTH       DISCLAMATION VM, PM       DISCLAMATION VM, PM       DISCLAMATION VM, PM         DERUND VM, PM       TOTAL DEPTH       DISCLAMATION VM, PM       DISCLAMATION VM, PM       DISCLAMATION VM, PM       DISCLAMATION VM, PM         DERUND VM, PM       TOTAL DEPTH       DISCLAMATION VM, PM       DISCLAMATION VM, PM       DISCLAMATION VM, PM       DISCLAMATION VM, PM	WRS	46375	511			Т	<b>P</b> R-5703	-	COLINT	Y LENOIR	2			GEOLOGIST Blonshine, E.G.	]	WRS	46375	i 1 1			ТІ	P R-5703		COUNTY
DOESNO. 0: 2         STATION. 89:65         OFFER 143.81T         ALLONET 1				Brid	ge No							5)			GROUND WTR (ft)				Bride	qe No				
COLLAGE LEV. 77.81         TOTAL DEPTH 99.81         NORTHNO 75.072         LATING 7.022 MIL 104         DOLAR ELV. 77.81         TOTAL DEPTH 99.81           DOULL DEVENDENCE COLVE COLVO.         TATAT DATE COLLEGE/LY 77.81         TOTAL DEPTH 99.81         DOULL DEVENDENCE COLVO.         DOULL DEVENDENCE COLVO. <td></td> <td></td> <td></td> <td></td> <td><u>.</u></td> <td></td> <td></td> <td></td> <td>,,</td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td>. ,</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td>,,</td>					<u>.</u>				,,			-			. ,							-	-	,,
DBLL BWINDS EFF.DAT. IPC201 OL: 50275 (2007):         DBLL BWINDS         DML BWINDS EFF.DAT. IPC201 OL: 50275 (2007):           DBLL BWINDS (FF.DAT. IPC207)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)           DBLL BWINDS (FF.DAT. IPC207)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)           DBLL BWINDS (FF.DAT. IPC207)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)           DBLL BWINDS (FF.DAT. IPC207)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)           DBLL BWINDS (FF.DAT. IPC207)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)         SUB OL: 500 (0000)           DBLL BWINDS (FF.DAT. IPC207)         SUB OL: 500 (0000)           DBLL BWINDS (FF.DAT. IPC207)         SUB OL: 500 (0000)           DBLL BWINDS (FF.DAT. IPC207)         SUB OL: 500 (0000)         SUB OL: 500 (0000				'.6 ft					ft										7.6 ft		_			t l
Have         Party         BLANE SERVICE         SALE         SOL AND FOR COCK DESCRIPTION         Have         Description         D	DRILI	L RIG/HA	MMER E	FF./DA	TE HI	PC2473	CME-550 92	2% 12/09/20	015	1	DRILL	METHO	DD N	Mud Rotary	R TYPE Automatic	DRILL	RIG/HAN	MMER E	FF./DAT	TE HP				
Image:	DRIL	LER V	Vhite, J.			S		E 08/10/	/16	COMP. DA	TE 08	/10/16	;	SURFACE WATER DEPTH N/A	Α	DRIL	LER W	/hite, J			ST	ART DATE	08/10/1	16
10       10 <th10< th="">       10       10       <th1< td=""><td></td><td>DRIVE</td><td></td><td>BLC</td><td>w co</td><td>UNT</td><td></td><td>BLOWS</td><td>PER FOOT</td><td>ſ</td><td>SAMP</td><td>. 🔨</td><td>L</td><td></td><td></td><td></td><td>DRIVE</td><td></td><td>BLO</td><td>w cou</td><td>INT</td><td></td><td>BLOWS</td><td>PER FOOT</td></th1<></th10<>		DRIVE		BLC	w co	UNT		BLOWS	PER FOOT	ſ	SAMP	. 🔨	L				DRIVE		BLO	w cou	INT		BLOWS	PER FOOT
77.       76.       10.       5       2       1       2       1       10.	(ft)		(ft)	0.5ft	0.5ft	0.5ft	0	25	50	75 100	NO.	мо				(ft)		(ft)	0.5ft	0.5ft	0.5ft	0 2	25 !	50 7
77.       76.       10.       5       2       1       2       1       10.																								
10       10 <td< td=""><td>80</td><td></td><td>Ļ</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>L</td><td></td><td>0</td><td>-07-</td><td>78.3</td><td> </td><td>  </td><td>+</td><td></td><td>Matc</td><td>h Line</td></td<>	80		Ļ											L		0	-07-	78.3			+		Matc	h Line
m       1/2       2       1       1/2 <td></td> <td>-</td> <td>‡</td> <td></td> <td>-</td> <td>-</td> <td>9</td> <td>11</td> <td>15</td> <td></td> <td><b>2</b>6</td> <td></td>		-	‡														-	-	9	11	15		<b>2</b> 6	
713       10       2       1       2       1       2       1	75	76.6	+ 1.0 +	5	2	1						м		<ul> <li>Brown Gray Tan Sandy CLAY,</li> </ul>	, Trace Gravel,	-5	-	-						
TR.       D.       D. <thd.< th=""> <thd.< th="">       D.       <th< td=""><td>10</td><td>74.1</td><td>3.5</td><td>2</td><td>1</td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td>N</td><td></td><td>/</td><td></td><td>-5.7</td><td>83.3</td><td>8</td><td>15</td><td>21</td><td></td><td></td><td></td></th<></thd.<></thd.<>	10	74.1	3.5	2	1	2							N		/		-5.7	83.3	8	15	21			
00.1       03       3       4       4       1 <td></td> <td>71.6</td> <td><b>-</b> 6.0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>·   · · · · ·</td> <td>.  </td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		71.6	<b>-</b> 6.0						·   · · · · ·	.							-	-						
00       40       4       10	70	69.1	+ 85	2	3	4	••• <u>•</u> ••		• • • • •		-	D		<ul> <li>Tan Coarse Sandy Silty CLA</li> <li>Smoothed Granules (P</li> </ul>	Y with Larger Pebbles)	-10	-10.7	- 88.3				· · · · ·	+ • • • •	
65       64.3       11.3       11       15			+ 0.0	3	4	4			·   · · · · ·	.		м					-		60/0.1					
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00       01       11       12       12       13       14       12 <td< td=""><td></td><td>64.3</td><td>+ 13.3 +</td><td>11</td><td>15</td><td>16</td><td> <b>`</b></td><td>· · · ·</td><td></td><td></td><td></td><td>l w</td><td></td><td>Dark Gray Clayey Fine</td><td>e SAND</td><td>10</td><td>-15.7</td><td>93.3</td><td>22</td><td>35</td><td>45</td><td></td><td></td><td></td></td<>		64.3	+ 13.3 +	11	15	16	<b>`</b>	· · · ·				l w		Dark Gray Clayey Fine	e SAND	10	-15.7	93.3	22	35	45			
100       93.3       14.3       7       0       13         15       94.1       23.3       11       12       12       11       12       12         150       90.1       28.3       3       3       3       3       3       3       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       14       15       12       15       14       15       12       14       15       14       15       14       15       14       15       14       15       14       14       15       12       14       14       15       14       14       15       14       15       14       15       14			ŧ					<i>I</i>	·   · · · · ·	.				F [Peedee Formatic	on]		-	-						
1       7       9       13       1       12       1       13       14       15       12       1       12       1       12       1       12       1       12       1       12       1       12       1       12       12       12       13       14       15       12       15       16       12       16       16       16       16       16       16       16       16       16       16       16       16       16       16       16       16       16	60	- 59.3 -	+ 18.3					/			-			<u>+</u> 		-20	-20.7	- 98.3					+ • • • •	
65       54.3       7.3       11       12       13       12		-	ŧ	7	9	13		22		.		W						-	46	54/0.5		<u> </u>	<u>  · · · ·</u>	
64.3       73.3       11       12       72.0       84.1       73.3       73.1       74.1       12       75.1       120.1	55	-	ŧ						·   · · · · ·								-	-						
60       49.3       28.3       3       3       3         45       44.3       33.3       2       2       3         40       39.3       38.8       14       15       12         40       39.3       38.8       14       15       12         50       43.4       3       3       3       3         30       22.6       48.8       13       11         20       19.3       48.8       7       9       10         45       19.3       48.8       7       9       10         46       19.4       49.3       10       10.6       10.7       10.7       10.0         40       9.3       48.3       7       9       10       10.6       10.7       10.7       10.7       10.7         30       22.4       48.3       7       9       10       10.6       10.7 <td></td> <td>54.3</td> <td>† 23.3 †</td> <td>11</td> <td>12</td> <td>12</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>l w</td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		54.3	† 23.3 †	11	12	12						l w					-	-						
30       40.3       20.3       3       3       3         45       44.3       33.3       2       2       3         40       30.3       33.3       14       15       12         35       34.3       43.3       3       3       3         36       43.3       3       3       3       3         36       30.3       24.3       43.3       3       3         36       23.4       43.3       3       3       3         30       29.3       48.3       8       13       11         25       24.3       53.3       7       7       44       40         15       14.3       63.3       5       7       7       44       40         16       19.3       58.3       5       7       7       44       40       40         15       14.3       63.3       5       6       7       44       40       40         19.4       45.3       6       7       44       40       40       40       40         19.4       40.4       40.4       40.4       40.4       40.4       40.4 <td></td> <td></td> <td>ŧ</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>·   · · · · ·</td> <td>.  </td> <td></td> <td> </td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>			ŧ						·   · · · · ·	.							-	-						
45       44.3       33.3       2       2       3         40       30.3       30.3       14       15       12         35       34.3       43.3       3       3       3         30       29.3       44.3       3       3       3         30       29.3       44.3       3       3       3         30       29.3       44.3       11       12.6       Biack Fine Sandy CLAY         40       30.3       3       3       3       3       4         30       29.3       44.3       11       14.4       14.4       14.4       14.4         45       24.3       53.3       7       9       10       10.6       Biack-Dark Gray Fine Sandy CLAY, Trace       52.9         10       9.3       66.3       15       11.4       10.6       Biack-Dark Gray Fine Sandy CLAY, Trace       52.9         10       9.3       66.3       10       10.6       Biack-Dark Gray Fine Sandy CLAY, Trace       52.9         10       9.3       66.3       10       10.6       Biack-Dark Gray Fine Sandy CLAY, Trace       52.9         10       9.3       66.3       10       10.6       B	50	49.3	+ 28.3								-						-	-						
45       43       333       2       2       3         40       30.3       38.3       14       15       12         35       34.3       43.3       3       3         30       28.3       48.3       8       13       11         25       24.3       53.3       7       9       10         25       24.3       53.3       7       9       10         20       18.3       56.3       5       7       7         44		-	ŧ	3	3	3	<b>•</b> 6		·   · · · · ·	.		W		Blue Black Fine Sandy	/ CLAY		-	-						
44.3       33.3       2       2       3         40       38.3       14       15       12         35       34.3       3       3       3         36       34.3       3       3       3         30       29.3       48.3       8       13       11         25       24.3       53.3       7       9       10         26       20       19.3       68.3       7       7         10       9.3       68.3       68.3       10       10	45	-	ŧ						·   · · · · ·								-	-						
40       38.3       14       15       12         25       34.3       3       3       3         30       29.3       48.3       8       13       11         25       24.3       53.3       7       9       10         15       24.3       53.3       7       9       10         15       14.3       56.3       7       7         10              10              10              11              15       14.3       63.3       5       6       7         10              11               10               14               14		44.3	+ 33.3 +	2	2	3						М					-	F						
40       39.3       38.3		-	ŧ				•••••••••••••••••••••••••••••••••••			.							-	-						
35     34.3     43.3     3     3       30     29.3     48.3     8     13     11       25     24.3     53.3     7     9     10       25     24.3     58.3     5     7     7       10     9.3     66.3     1     1	40	39.3	+ - 38.3					· · · ·		· · · · · ·	-			<u>-</u> <u>39.6</u>	38.0		-	-						
35     34.3     43.3     3     3     3       30     29.3     48.3     8     13     11       25     24.3     53.3			Ŧ	14	15	12		27.		.		M		° <b>↓</b> 37.6	40.0			-						
30       29.3       48.3       3<	35		Ŧ											- Black Fine Sandy C	LAY		-	F						
30     29.3     48.3     8     13     11       25     24.3     53.3     7     9     10       20     19.3     58.3     5     7     7       10     9.3     68.3     5     6     7       10     9.3     68.3     10     11.3     11.3		34.3	+ 43.3 +	3	3	3	· / · · ·					м					-	-						
30       29.3       48.3			Ŧ							.							-	-						
25       24.3       53.3       7       9       10         20       19.3       58.3       5       7       7         10       9.3       66.3       -       -       -       -         10       9.3       66.3       -       -       -       -       -       -         10       9.3       66.3       -<	30	29.3	48.3					<u> </u>		· · · · · ·				-			-	F						
25     24.3     53.3     7     9     10       20     19.3     58.3     7     7       10     9.3     68.3     68.3     10.6			Ŧ	8	13	11		24	.	.		M					-	F						
20     19.3     58.3     7     9     10       10     9.3     68.3     68.3     10	25		Ŧ					i	.						<u>52.0</u>			F						
20     19.3     58.3     5     7     7       10     9.3     68.3     68.3     10			T 53.3	7	9	10	· · · •	19			]	м		Shells, Trace Mic			-	E						
19.3       58.3	3/17		Ŧ							.														
Image: Second		19.3	T 58.3	<u> </u>	<u> </u>	<u> </u>		+ • • •		· · · · · ·				<b>F</b>			-	F						
Image: Second	DT.GL	-	Ŧ	5	7	7	14		.			M					-	F						
Image: Second	ပီ ပါ 15		Ŧ						.									F						
		14.3	† 63.3 †	5	6	7					1	м		-				F						
	1.G		ŧ						.	.								F						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		9.3	68.3					+ • • •		· · · · · ·				Blue Gray Clayey Fine SAND	, Trace Shells67.0			F						
0     5     4.3     73.3     19     22     27      49        M     49	JBLE		Ŧ	18	39	36			$\left  \begin{array}{c} \cdot \\ \cdot \end{array} \right  \left  \begin{array}{c} \cdot \\ \cdot \\ \cdot \end{array} \right  \left  \begin{array}{c} \cdot \\ \cdot \end{array} \right  \left  \begin{array}{c} \cdot \\ \cdot \\ \cdot \end{array} \right  \left  \left  \begin{array}{c} \cdot \\ \cdot \\ \cdot \end{array} \right  \left  \left  \begin{array}{c} \cdot \\ \cdot \\ \cdot \end{array} \right  \left  \left  \begin{array}{c} \cdot \\ \cdot \\ \cdot \end{array} \right  \left  \left  \begin{array}{c} \cdot \\ \cdot \\ \cdot \\ \cdot \end{array} \right  \left  \left  \left  \begin{array}{c} \cdot \\ \cdot \\ \cdot \\ \cdot \end{array} \right  \left  \left $	75		М	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~					-						
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			ŧ						·   · · · · ·	.								F						
$\overline{5}$   $1$	BORE	4.3	† 73.3 †	19	22	27		· · ·			1	м	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<u>↓</u> -				F						
	DOT		ŧ							·   · · · · ·								-						
	0 N	-	†											• <u>0.6</u>	77.0		-	-						



	4637					<b>P</b> R-5703			Y LENOI				GEOLOGIST Blonshine, E.				<b>3</b> 46375					<b>P</b> R-5703		COUNT	
				-			-	vkwy) ove	er -Y1- (NC		-			-	ID WTR (ft)	-				-		on -L- (Felix		kwy) ove	
-	ING NO LAR EL			Ln.	_	TATION 8		+	OFFSET				ALIGNMENT -L- EASTING 2,422,968	0 HR. 24 HR.	N/A FIAD		LAR ELI			Ln.		TATION 89 OTAL DEPT			OFF NOR
				TE HE		CME-550 92						ע סנ		MER TYPE						TE HI		CME-550 92			NOR
	LER V								COMP. D				SURFACE WATER DEPTH		Automatic		LER W								CON
ELEV	DRIVE ELEV			W COL				PER FOO		SAMP		1 L	1			ELEV	DRIVE		1	W CO				PER FOOT	I
(ft)	ELEV (ft)	(ft)		0.5ft	0.5ft	0 :	25	50	75 10	0 NO.	мо	O I G	SOIL AND ROCK DE	SCRIPTION	DEPTH (ft)	(ft)	ELEV (ft)	(ft)		0.5ft	0.5ft	0 2	25 £	50	75 I
80		+											-			0	+ <del>_</del>	┢───					Matc	h Line	
		Ŧ											C - 7 <u>8.9</u> GROUND SUF	ACE	0.0		-2.1	78.7	10	14	18		• • • • • • • • • • •		
75	75.6	1.0	3	1	2	1					13%		ASPHAL ROADWAY EMBA			-5	-	Į					1		
	73.1	3.5	WOH	1	2	<b>•</b> 3 • • •	· · · · ·	· · · ·	·   · · · · ·   · · · ·	00-7	1		Gray Fine Sandy SILT Tra	e Mica and	little 3.0		-7.1	83.7	9	10	47		: : :		
70	70.6	+ - 6.0				<b>•</b> <sup>3</sup> · · · ·	· · · · ·	· · · ·	·   · · · · ·		M		UNDIVIDED COAS	AL PLAIN	with	-10	-	ŧ	9	12	17		•29 · · ·		
-10	- 68.1	+ + 8.5	2	4	3						D		Tan Gray Fine to Coarse Gravel	anuy CLAT	with	10	-12.1	88.7							-
		+ 0.0	5	4	4				· · · · · ·		D		1- -				- 12. 1 -	+ 00./ +	10	16	35			•••••	
65	-	ŧ												<u></u>	<u>12.0</u>	-15	-	ŧ							+
	63.1	13.5 T	1	3	5						l w		Blue Gray Clayey Co	arse SAND			-17.1	93.7	60/0.1						
60	_	Ŧ												luonj			-	I		1					
	57.8	   18.8						· · ·									-	ŧ							
		ŧ	4	12	16		28: : :	· · ·	·   · · · · ·		W						-	ŧ							
55	-	+ 1 23.5					<u>;</u>						/ / +				-	ŧ							
	53.1	+ 23.5 +	4	9	12	:::;	 21	· · · ·	·   · · · · ·		w						-	ŧ							
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	47.9	28.7	3	3	4												-	ŧ							
45		ŧ	ľ	Ŭ	.	$\begin{array}{c c} \bullet 7 & \cdot & \cdot \\ \cdot & \cdot & \cdot \end{array}$					W						-	Ŧ							
	43.1	33.5															-	Ŧ							
		Ŧ	2	2	4	<b>●</b> 6_ · · ·					м							Ŧ							
40	-	+					<u> </u>										-	ŧ							
	38.1	<u> </u>	12	33	56		· · · · ·				м						-	ŧ							
35	-	ŧ							· · · · · · · · · · · · · · · · · · ·						42.0		-	ŧ							
	32.7	+ + 43.9					· · · · · · ·		·   · · · · ·				Black Fine Sandy CLA	Trace Mica	a		-	ŧ							
30		‡	2	2	3	• <sup>5</sup> ····	· · · · ·	· · ·   · · ·	·   · · · · ·		М		31.1		ith 45.5		-	‡				l			
- 50		‡				· \ · ·							Black/Dark Gray Fine Sa Shells					ŧ				l			
	27.8	<u>+ 48.8</u> +	5	7	8	· · · • 15					м						-	ŧ				l			
25	-	Ŧ							· · · · · ·				1				-	Ŧ				l			
2	22.9	53.7	6	8	9				· · · · · · ·		м		Į				-	Ŧ				l			
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.601	17.9	58.7		_	-			· · ·   · · ·	:   : :								-	ŧ							
		‡	6	6	8	• • • 14		· · ·			м						-	ŧ							
2 15 2	-	<b>†</b> .					· · · · ·	· · ·										ŧ							
- -	12.9	<u> </u>	6	7	8	· · · • 15	· · · · ·	· · ·   · · ·	·   · · · · ·		м						-	‡				l			
10	-	‡				· · · · ·	1		·   · · · ·	_			- 		67 7		-	‡				l			
	7.9	68.7	31	42	57/0.4				÷				Blue Gray Clayey Coarse	AND with S	hells 67.7		-	ŧ				l			
5		ŧ		40	51/0.4		· · · · ·			9	M						-	ŧ				l			
	29	+ 						,		1								ŧ				l			
20 15 10 10 10 0 10 10 10 10 10 10	2.9	<u> </u>	16	26	27			●53· ·	· · · · · ·		М						-	Ŧ				l			
У O		T					· · · · ·					~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1					Τ				<u> </u>			

#### SHEET 11 OF 42

NT	<b>Y</b> LENOIR				GEOLOGI	ST	Blonshine	e, E.G.		
ove	r -Y1- (NC H	WY 58)							GROUN	ID WTR (ft)
	OFFSET 3	3 ft RT			ALIGNME	ΝТ	-L-		0 HR.	N/A
	NORTHING	578,0	97		EASTING	2,4	22,968		24 HR.	FIAD
		DRILL N	IETHO	D Mud	d Rotary			HAMM	ER TYPE	Automatic
	COMP. DAT	<b>FE</b> 08/0	08/16		SURFACE	WA	TER DEP	TH N/	Ą	
ют		SAMP.		L		0.01				
	75 100	NO.	моі	O G		501	L AND ROO	K DESC	RIPTION	
•										
		<b>F</b>			- <u>0.9</u> BI		ray Fine Sa		Y with She	77.5
· ·			м					,		
					- <u>4.4</u> Blue	Gray	Clayey Fin	e SAND	with Shells	s and <u>81.0</u>
· ·							Cemen	ted Laye	ſS	
· · · ·			М							
· ·			w							
<u>``</u>	<u> </u>									
· ·				~~~	-17.1 -17.2 Bo					93.7 tin 93.8
	60/0.1				-17.2 Bo Ver	ring 7 v Der	Ferminated	at Elevat	ion -17.2 f arse sand	t in <sup>93.8</sup> with
						<b>,</b> -	nse clayey f	hells		-
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Revision Date: 12/20/09

Revision No. 0

**Particle Size Analysis of Soils** 



# **Oedometer Settlement Tests**

AASHTO T88 as Modified by NCDOT

Sa	&MF Inc Raleid	gh, 3201 Spring Fore	st Road Ral	eigh North (	~	ality Assu 6	unce
S&ME Project #:	6235-16-010	31, 5201 Spring Fore	si Kuau, Kai	0,	rt Date:	12/27	/16
Project Name:		arkway Extension R-5	703			12/24 - 12	
State Project #:	N/A	F.A. Project No:			• NO: N/A		
Client Name:	Michael Baker						
Address:	Raleigh, NC	0 0		_			
Boring #:	B-1	Sample #:	ST-1		Sample Date	: 1	N/A
Location:	88+89	Offset:	36 LT		Depth (ft)	: 10.5 -	· 12.5 ft.
Sample Description:			Gray Silty C	Clayey Fine to	Coarse SANE	D A-2-4	(0)
1.5"	1"3/4" 1/2'3/8" #	4 #10 #20 #	40 #60 #100	#200 #270			
100%			· <u>· · · · · · · · · · · · · · · · · · ·</u>	· · · · · · · · · · · · · · · · · · ·			
90%							
80%							
70%							
50 E							
·is 60%							
A 40%							
erce			+				
<b>⊷</b> 40%							
30%							
20%							
10%						•	
0%	10	1		0.1	0.01	*	0.0
		Particle S	ze (mm)				
1	As Defined by NCDC	)T	Fine	e Sand	< 0.25 m	m and $> 0.0$	)5 mm
Gravel		mm and > 2.00 mm	2	Silt	< 0.05 a	and > 0.005	
Coarse Sand		) mm and >0.25 mm		Clay		0.005 mm	<b>-</b>
Maximum Particle S		Coarse S		42%	Silt		5%
Gravel	7%	Fine Sar		37%	Clay		9%
Apparent Relative D	•		e Content	29.3%	% Passing #		15.6%
Liquid Limit	24	Plastic I		22	Plastic Index	K	2
~ ~ ~ .	450/		(-#10 Sieve)	0.1	50/	<u>C1</u>	1.00/
	45%	Fine Sand	40%	Silt	5%	Clay	10% ×
Coarse Sand	Pr Crowal Dortialas				Angula		
Description of Sand			-	Wood	barad & Fright		
Description of Sand Hard & Durab	ole 🛛	Soft		Weat	hered & Friable		
Description of Sand Hard & Durab	ole 🛛			Weat	hered & Friable		
Description of Sand Hard & Durab	ole 🗵 / Deviations: N	Soft		Weat			7/2016
Description of Sand Hard & Durab References / Comments	ole 🗵 / Deviations: N	Soft ND=Not Determined.				<u>12/2</u>	7/2016 Date
Description of Sand Hard & Durab References / Comments <u>Mal Kraja</u> Technician	ole 🗵 / <i>Deviations:</i> N nn, ET Name	Soft ND=Not Determined. <u>104-01-0703</u>		Laboratory M Position	anager	<u>12/2</u>	Date
Description of Sand Hard & Durat References / Comments <u>Mal Kraja</u>	ole X / Deviations: N un, ET Name un, ET	Soft ND=Not Determined. <u>104-01-0703</u>		Laboratory M	anager	<u>12/2</u> 1 9/20	

Sample details Sketch showing specimen location in original Sample	Depth Description:	1
	Type Height $H_0$ (in) Diameter $D_0$ (in) Weight $W_0$ (gr) Bulk Density $\rho$ (l Particle Density	PCF)
nitial Conditions		
ettlement Channel	1942	

Settlement Granner	1942
Moisture Content w <sub>0</sub> %	27.6
Dry Density Prd (PCF)	91.91
Voids Ratio e <sub>0</sub>	0.8045
Deg of Saturation S <sub>0</sub> %	91.0
Swelling Pressure Ss (TSF)	0.000

Final Conditions	
Moisture Content w <sub>f</sub> %	24.2
Dry Density Pd (PCF)	100.73
Voids Ratio e <sub>f</sub>	0.6465
Deg of Saturation S <sub>f</sub> %	99.51
Settlement: (in)	0.087
Compression Index C <sub>c</sub>	0.150
Notes:	Test specimen

ASTM D2435-96

Jobfile:

S&ME

3201 Spring Forest Road Raleigh, NC 27616

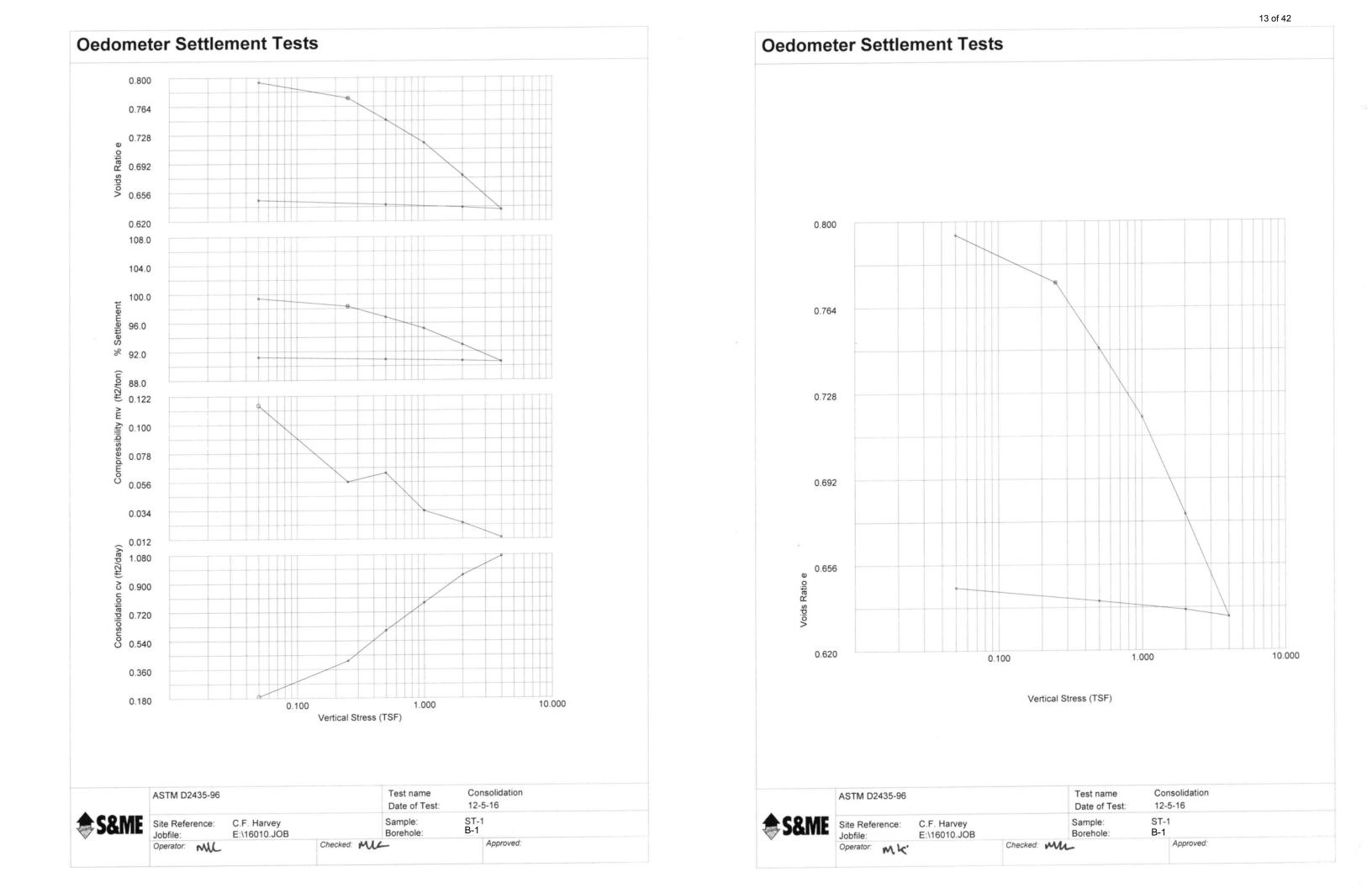
B1 ST-1 (10.5 - 12.5 ft) Classification.xls

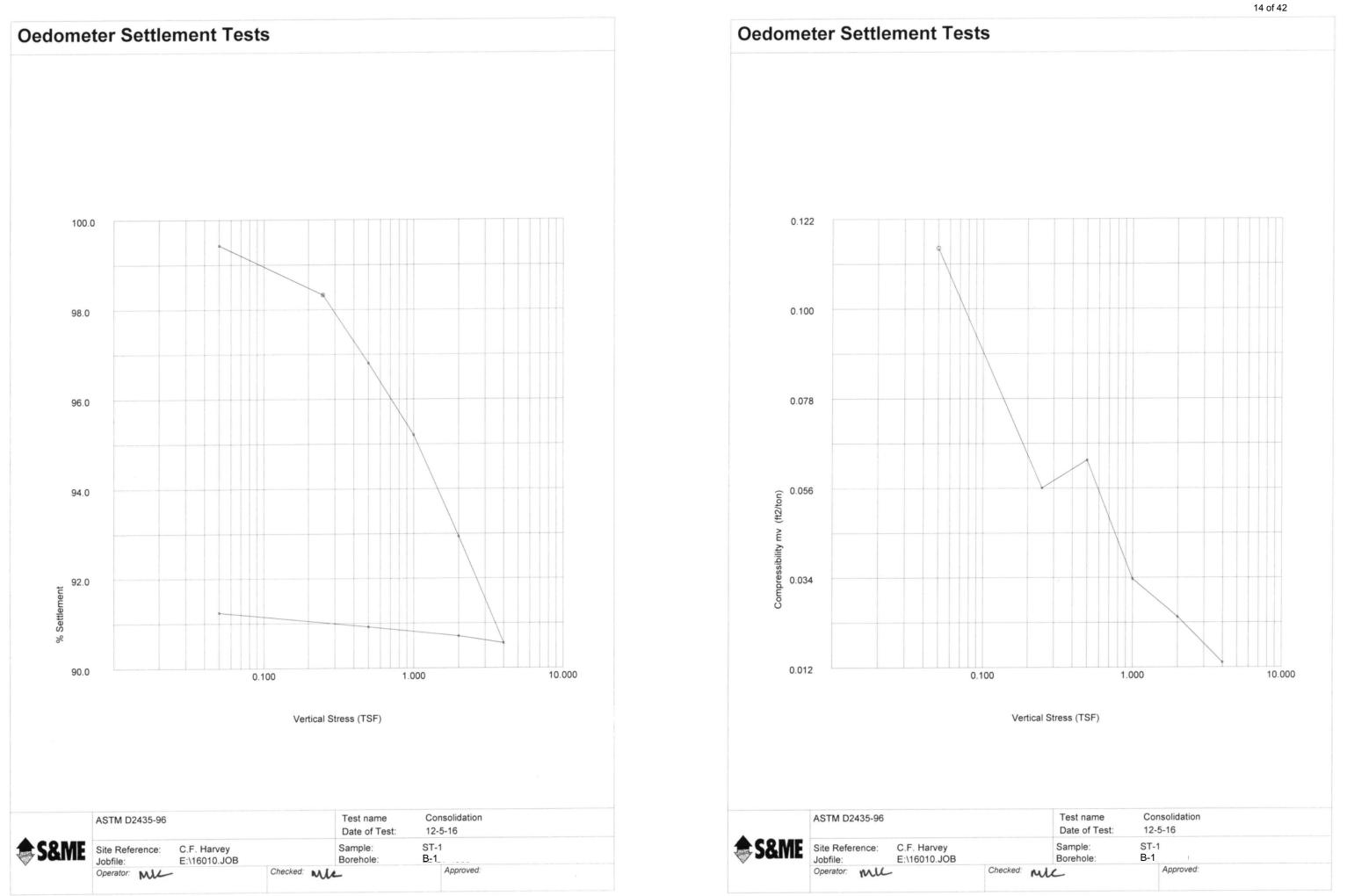
10.5 - 12.5 ft. Gray Silty Clayey Fine to Coarse SAND (A-2-4) (0)

Undisturbed 0.998 2.501 150.89 ) 117.24 2.658 (measured)

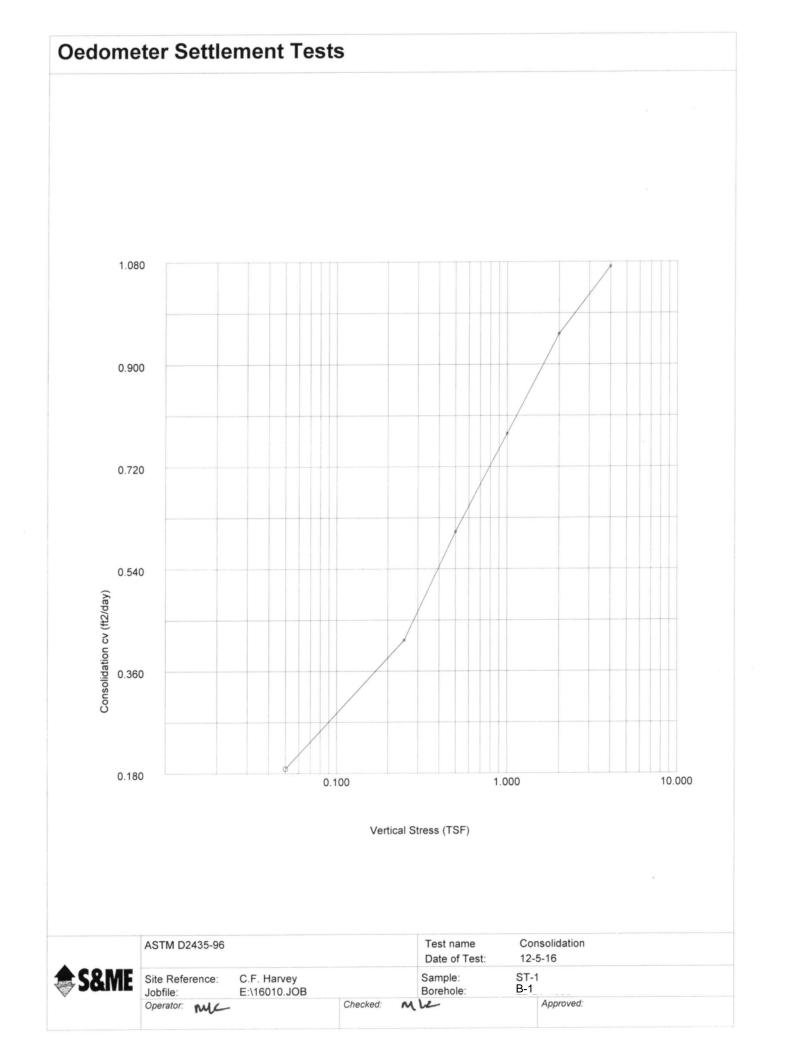
takne from the middle portion of UD tube.

	Test name Date of Test:		nsolidation 5-16	
	Sample: Borehole:	ST-1 B-1	1	
Checked: M	L		Approved:	





	Date of Test.	12-3-10	
	Sample:	ST-1	
	Borehole:	B-1	
hecked:	mic	Approved:	



Stress	Initial	Settlement	Cal Corr.	Final	Voids	t <sub>50</sub>	Secondary	c <sub>v</sub>	m <sub>v</sub>
(TSF)	Temp. oC	Total (in)	(in)	Temp. oC	Ratio e <sub>f</sub>	(mins)	Compr C <sub>sec</sub>	(ft2/day)	(ft2/ton)
0.050 0.250 0.500 1.000 2.000 4.000 2.000 0.500 0.050	21.6 21.6 21.6 21.6 21.6 21.6 21.6 21.6	0.0057 0.0167 0.0319 0.0479 0.0705 0.0943 0.0927 0.0906 0.0874	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	21.6 21.6 21.6 21.6 21.6 21.6 21.6 21.6	0.7942 0.7743 0.7468 0.7179 0.6771 0.6340 0.6369 0.6407 0.6465	2.630 1.175 0.783 0.590 0.462 0.391	0.0006 0.0006 0.0008 0.0007 0.0079 0.0001	0.188 0.415 0.605 0.779 0.953 1.072	0.115 0.056 0.063 0.034 0.024 0.013 0.001 0.002 0.008

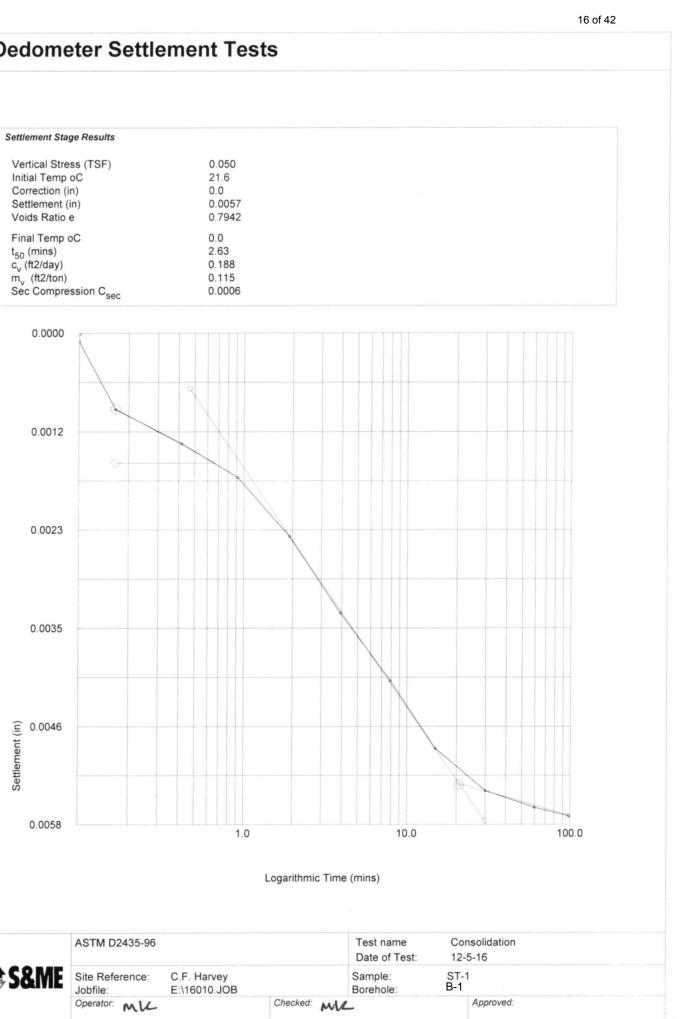
ASTM	D2435-96

Same Site Reference: C.F. Harvey Jobfile: E:\16010.JOB

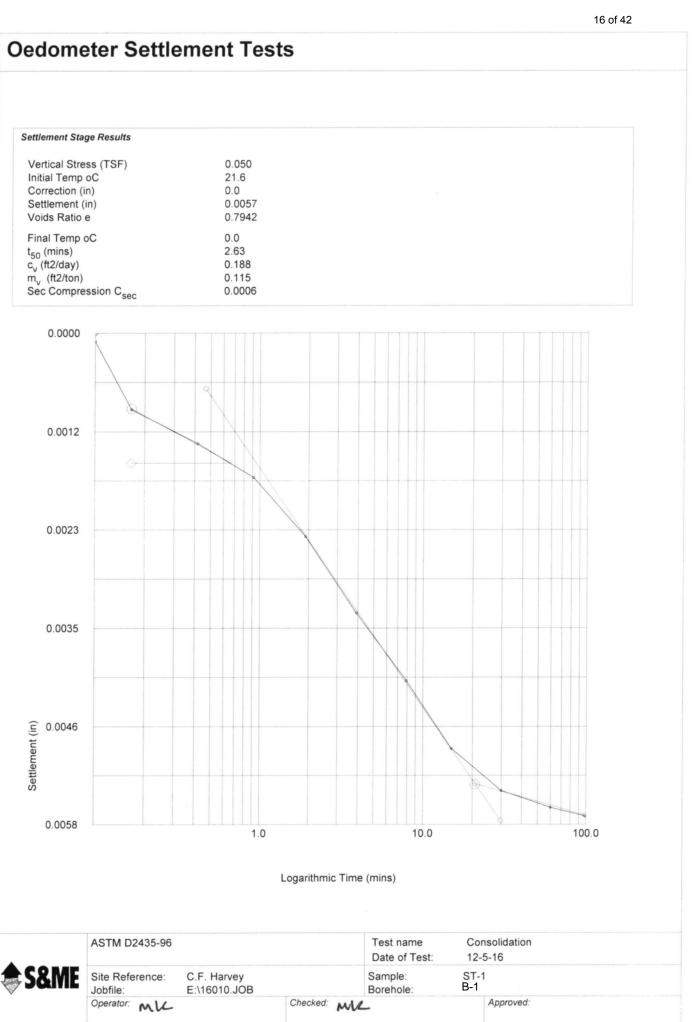
	Test name Date of Test:	Consolidation 12-5-16	
	Sample: Borehole:	ST-1 B-1	
Checked: 🔨	۱۲	Approved:	

No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	0	0.0000	0.0000
2	0.017	1	0.0001	0.0001
3	0.167	9	0.0009	0.0009
4	0.417	13	0.0013	0.0013
5	0.917	17	0.0017	0.0017
6	1.917	24	0.0024	0.0024
7	3.917	33	0.0033	0.0033
8	7.917	41	0.0041	0.0041
9	14.917	49	0.0049	0.0049
10	29.917	54	0.0054	0.0054
11	59.917	56	0.0056	0.0056
12	98.200	57	0.0057	0.0057

Settlement Stage Results	
Vertical Stress (TSF) Initial Temp oC	0.050
Correction (in)	0.0
Settlement (in) Voids Ratio e	0.0057 0.7942
Final Temp oC	0.0
t <sub>50</sub> (mins)	2.63
c <sub>v</sub> (ft2/day)	0.188
m <sub>v</sub> (ft2/ton) Sec Compression C <sub>sec</sub>	0.115 0.0006
300	



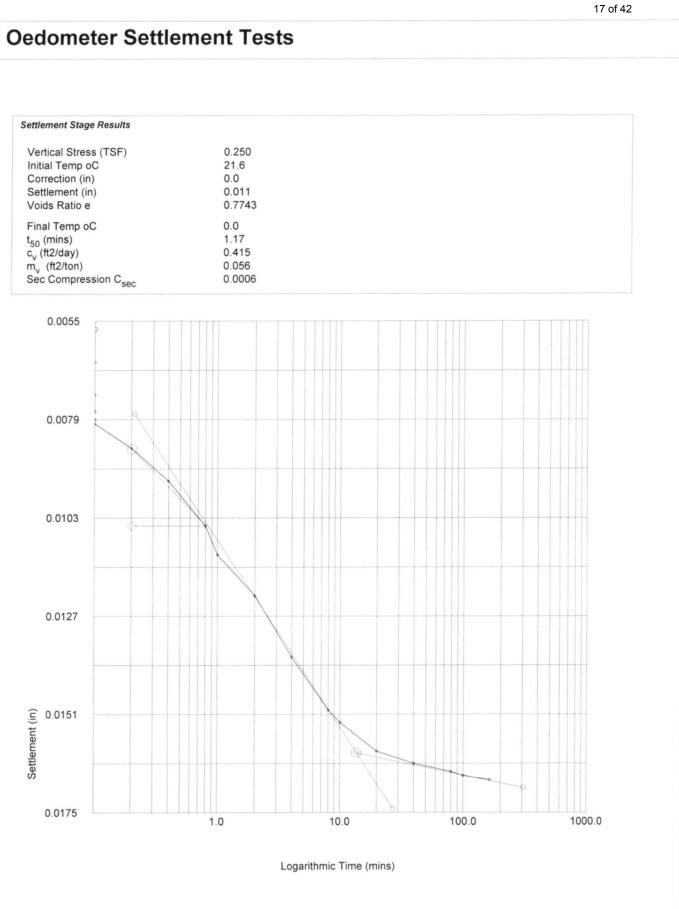
Consolidation Load: 0.050 (TSF) Test name ASTM D2435-96 12-5-16 Date of Test: ST-1 B-1 S&ME Sample: Site Reference: C.F. Harvey E:\16010.JOB Borehole: Jobfile: Checked: MK Approved: Operator: MLC



No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	57	0.0057	0.0057
2	0.017	65	0.0065	0.0065
3	0.033	65	0.0065	0.0065
4	0.050	73	0.0073	0.0073
5	0.067	77	0.0077	0.0077
6	0.083	79	0.0079	0.0079
7	0.100	80	0.0080	0.0080
8	0.200	86	0.0086	0.0086
9	0.400	94	0.0094	0.0094
10	0.800	105	0.0105	0.0105
11	1.000	112	0.0112	0.0112
12	2.000	122	0.0122	0.0122
13	4.000	137	0.0137	0.0137
14	8.000	150	0.0150	0.0150
15	10.000	153	0.0153	0.0153
16	20.000	160	0.0160	0.0160
17	40.000	163	0.0163	0.0163
18	80.000	165	0.0165	0.0165
19	100.000	166	0.0166	0.0166
20	163.170	167	0.0167	0.0167

	ASTM D2435-96			Test name Date of Test:		-5-16
S&ME	Site Reference: Jobfile:	C.F. Harvey E:\16010.JOB		Sample: Borehole:	ST- B-1	
	Operator: MLC		Checked: M	12		Approved:

0.250
21.6
0.0
0.011
0.7743
0.0
1.17
0.415
0.056
0.0006

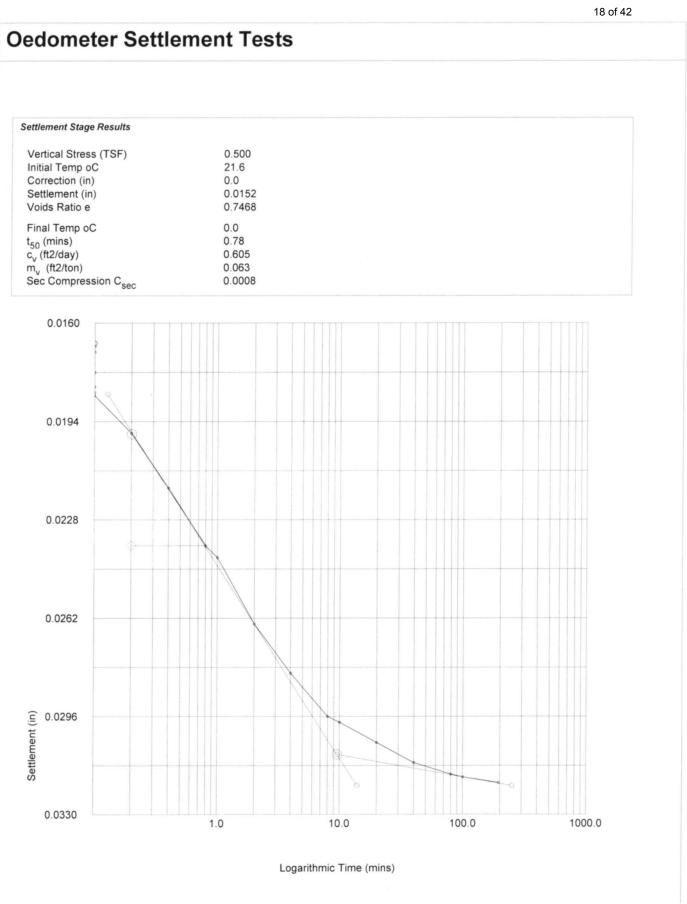


ASTM D2435-96		
Site Reference: Jobfile:	C.F. Harvey E:\16010.JOB	
Operator: MK		Che
	Site Reference: Jobfile:	Site Reference: C.F. Harvey Jobfile: E:\16010.JOB

	Test name Date of Test:	Consolidation 12-5-16	
	Sample: Borehole:	ST-1 B-1	
hecked:	uc	Approved:	

No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	167	0.0167	0.0167
2	0.017	168	0.0168	0.0168
3	0.033	170	0.0170	0.0170
4	0.050	177	0.0177	0.0177
5	0.067	182	0.0182	0.0182
6	0.083	184	0.0184	0.0184
7	0.100	185	0.0185	0.0185
8	0.200	198	0.0198	0.0198
9	0.400	217	0.0217	0.0217
10	0.800	237	0.0237	0.0237
11	1.000	241	0.0241	0.0241
12	2.000	264	0.0264	0.0264
13	4.000	281	0.0281	0.0281
14	8.000	296	0.0296	0.0296
15	10.000	298	0.0298	0.0298
16	20.000	305	0.0305	0.0305
17	40.000	312	0.0312	0.0312
18	80.000	316	0.0316	0.0316
19	100.000	317	0.0317	0.0317
20	196.000	319	0.0319	0.0319

Settlement Stage Results		
Vertical Stress (TSF)	0.500	
Initial Temp oC	21.6	
Correction (in)	0.0	
Settlement (in)	0.0152	
Voids Ratio e	0.7468	
Final Temp oC	0.0	
t <sub>50</sub> (mins)	0.78	
c <sub>v</sub> (ft2/day)	0.605	
m <sub>y</sub> (ft2/ton)	0.063	
Sec Compression C <sub>sec</sub>	0.0008	



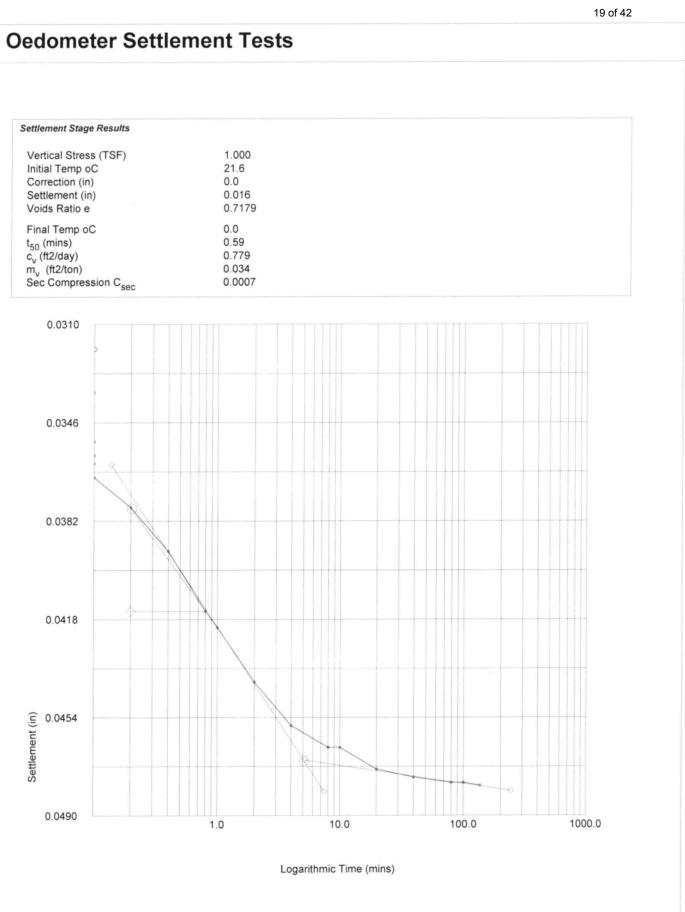
Consolidation Load: 0.500 (TSF) ASTM D2435-96 Test name 12-5-16 Date of Test: ST-1 B-1 Site Reference: C.F. Harvey Jobfile: E:\16010.JOB Sample: S&ME Borehole: Checked: MLC Approved: Operator: MK



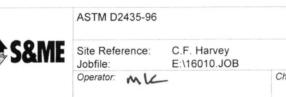
	Test name Date of Test:	Consolidation 12-5-16	
	Sample: Borehole:	ST-1 B-1	
Checked:	mk	Approved:	

No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	319	0.0319	0.0319
2	0.017	335	0.0335	0.0335
3	0.033	335	0.0335	0.0335
4	0.050	353	0.0353	0.0353
5	0.067	358	0.0358	0.0358
6	0.083	361	0.0361	0.0361
7	0.100	366	0.0366	0.0366
8	0.200	377	0.0377	0.0377
9	0.400	393	0.0393	0.0393
10	0.800	415	0.0415	0.0415
11	1.000	421	0.0421	0.0421
12	2.000	441	0.0441	0.0441
13	4.000	457	0.0457	0.0457
14	8.000	465	0.0465	0.0465
15	10.000	465	0.0465	0.0465
16	20.000	473	0.0473	0.0473
17	40.000	476	0.0476	0.0476
18	80.000	478	0.0478	0.0478
19	100.000	478	0.0478	0.0478
20	136.630	479	0.0479	0.0479

Settlement Stage Results	
Vertical Stress (TSF)	1.000
Initial Temp oC	21.6
Correction (in)	0.0
Settlement (in)	0.016
Voids Ratio e	0.7179
Final Temp oC	0.0
t <sub>50</sub> (mins)	0.59
c <sub>v</sub> (ft2/day)	0.779
m <sub>v</sub> (ft2/ton)	0.034
Sec Compression C <sub>sec</sub>	0.0007



Consolidation Load: 1.000 (TSF) Test name ASTM D2435-96 12-5-16 Date of Test: ST-1 B-1 Sample: Same Site Reference: C.F. Harvey Jobfile: E:\16010.JOB Borehole: Checked: MK Approved: Operator: MLC

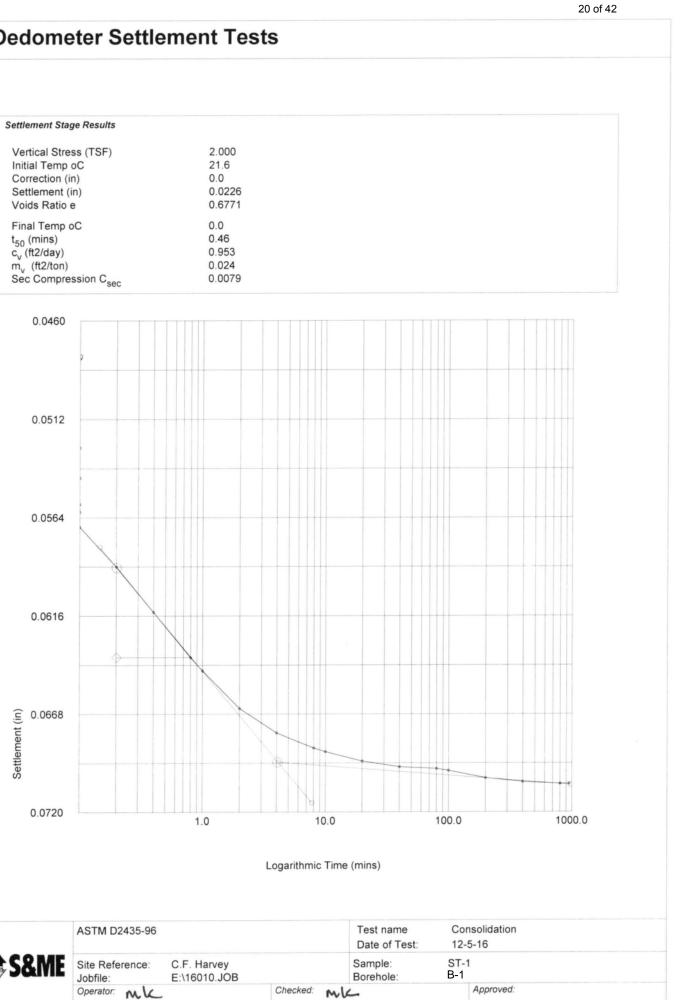


	Test name Date of Test:	Consolidation 12-5-16	
	Sample: Borehole:	ST-1 B-1	
Checked: MLL		Approved:	

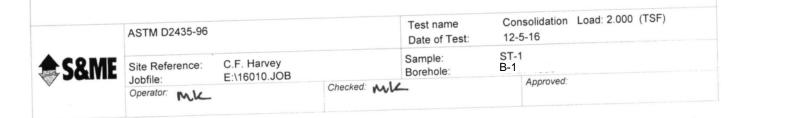
No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
	0.000	479	0.0479	0.0479
1		480	0.0480	0.0480
2	0.017	527	0.0527	0.0527
3	0.033	543	0.0543	0.0543
4	0.050 0.067	557	0.0557	0.0557
5	0.083	561	0.0561	0.0561
6	0.100	569	0.0569	0.0569
7	0.200	590	0.0590	0.0590
8	0.400	614	0.0614	0.0614
9	0.800	638	0.0638	0.0638
10	1.000	645	0.0645	0.0645
12	2.000	665	0.0665	0.0665
12	4.000	678	0.0678	0.0678
14	8.000	686	0.0686	0.0686
	10.000	688	0.0688	0.0688
15	20.000	693	0.0693	0.0693
16	40.000	696	0.0696	0.0696
17	80.000	697	0.0697	0.0697
18	100.000	698	0.0698	0.0698
19		702	0.0702	0.0702
20	200.000	704	0.0704	0.0704
21	400.000	705	0.0705	0.0705
22	800.000 949.100	705	0.0705	0.0705
23	545.150			

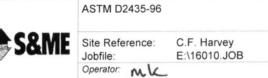
Oedometer :	Settlement	Tests
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.000 1.6
.0
0226
.6771
.0
46
953
024
0079



Approved:

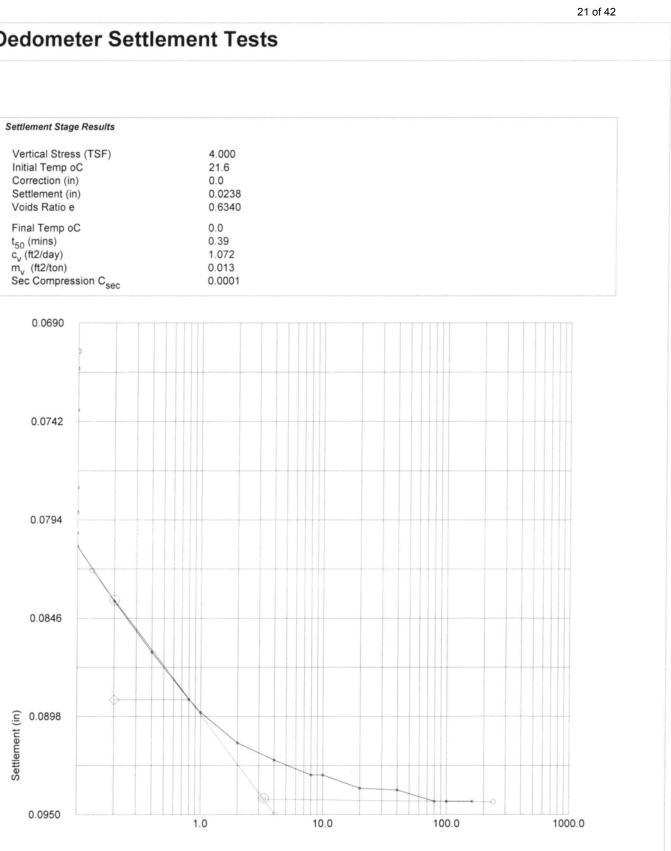




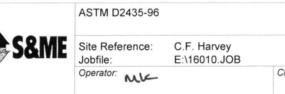
No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	705	0.0705	0.0705
2	0.017	714	0.0714	0.0714
3	0.033	736	0.0736	0.0736
4	0.050	777	0.0777	0.0777
5	0.067	790	0.0790	0.0790
6	0.083	801	0.0801	0.0801
7	0.100	808	0.0808	0.0808
8	0.200	837	0.0837	0.0837
9	0.400	864	0.0864	0.0864
10	0.800	889	0.0889	0.0889
11	1.000	896	0.0896	0.0896
12	2.000	912	0.0912	0.0912
13	4.000	921	0.0921	0.0921
14	8.000	929	0.0929	0.0929
15	10.000	929	0.0929	0.0929
16	20.000	936	0.0936	0.0936
17	40.000	937	0.0937	0.0937
18	80.000	943	0.0943	0.0943
19	100.000	943	0.0943	0.0943
20	161.130	943	0.0943	0.0943

	Oed	lometer	Settlement	Tests
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Settlement Stage Results	
Vertical Stress (TSF) Initial Temp oC	4.000
Correction (in)	0.0
Settlement (in) Voids Ratio e	0.0238 0.6340
Final Temp oC	0.0
t <sub>50</sub> (mins)	0.39
c <sub>v</sub> (ft2/day) m <sub>v</sub> (ft2/ton)	1.072 0.013
Sec Compression C <sub>sec</sub>	0.0001
000	



Consolidation Load: 4.000 (TSF) ASTM D2435-96 Test name 12-5-16 Date of Test: SRAME Site Reference: C.F. Harvey Jobfile: E:\16010.JOB ST-1 B-1 Sample: Borehole: Checked: mlc Operator: MK Approved:

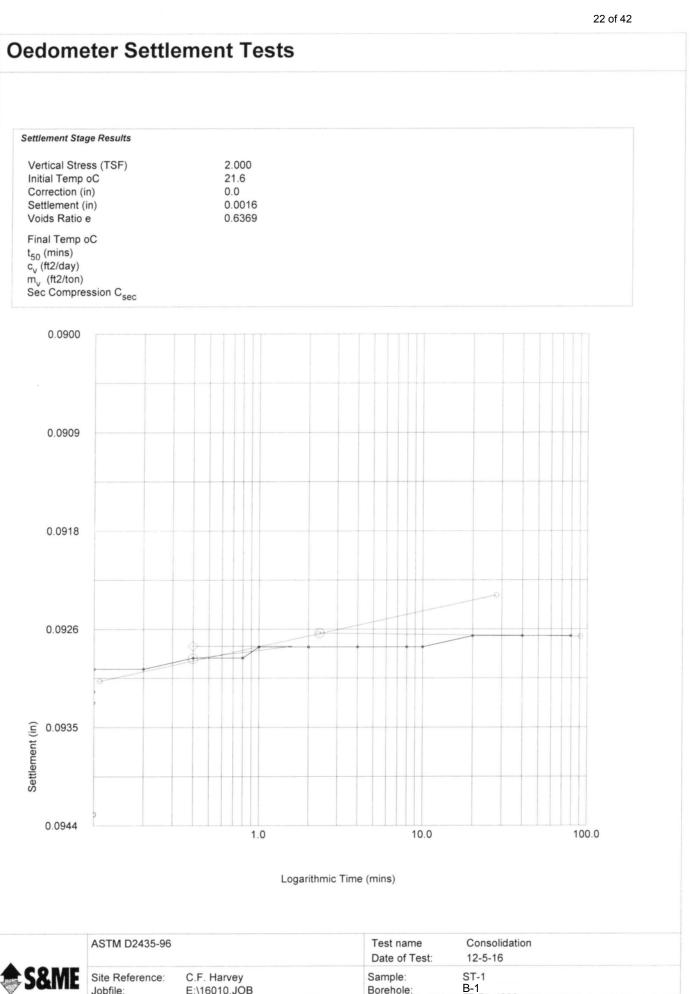


Logarithmic Time (mins)

	Test name Date of Test:	Cons 12-5-	olidation 16	
Sample: Borehole:		ST-1 B-1		
Checked:	mic	1	Approved:	

No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	943	0.0943	0.0943
2	0.017	933	0.0933	0.0933
3	0.033	933	0.0933	0.0933
4	0.050	932	0.0932	0.0932
5	0.067	930	0.0930	0.0930
6	0.083	930	0.0930	0.0930
7	0.100	930	0.0930	0.0930
8	0.200	930	0.0930	0.0930
9	0.400	929	0.0929	0.0929
10	0.800	929	0.0929	0.0929
11	1.000	928	0.0928	0.0928
12	2.000	928	0.0928	0.0928
13	4.000	928	0.0928	0.0928
14	8.000	928	0.0928	0.0928
15	10.000	928	0.0928	0.0928
16	20.000	927	0.0927	0.0927
17	40.000	927	0.0927	0.0927
18	79.330	927	0.0927	0.0927

	Oed	lometer	Settlem	ent <sup>-</sup>	Tests
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E:\16010.JOB

Jobfile:

Operator: MIC

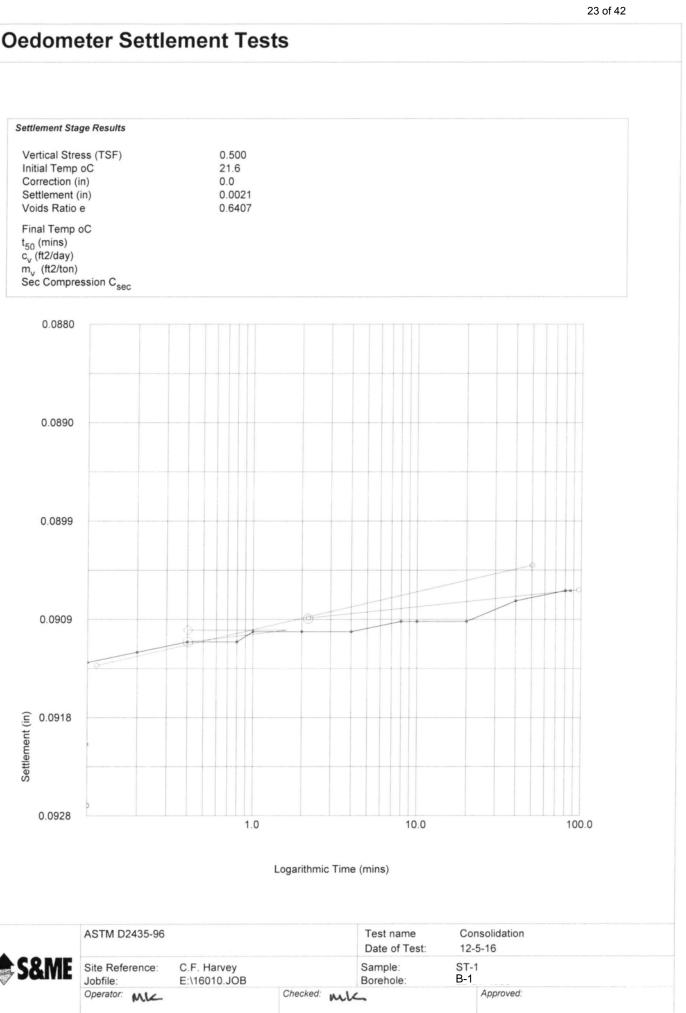
	ASTM D2435-96			Test name Date of Test:		nsolidation Load: 2.000 (TSF) 5-16
S&ME	Site Reference: Jobfile:	C.F. Harvey E:\16010.JOB		Sample: Borehole:	ST- B-1	1
	Operator: MK		Checked: MLC	-		Approved:

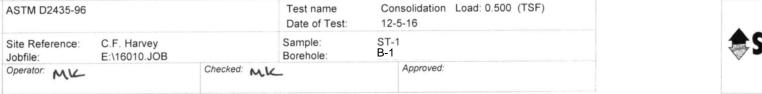
		mple: rehole:	ST-1 B-1	
Checked:	MIL			Approved:

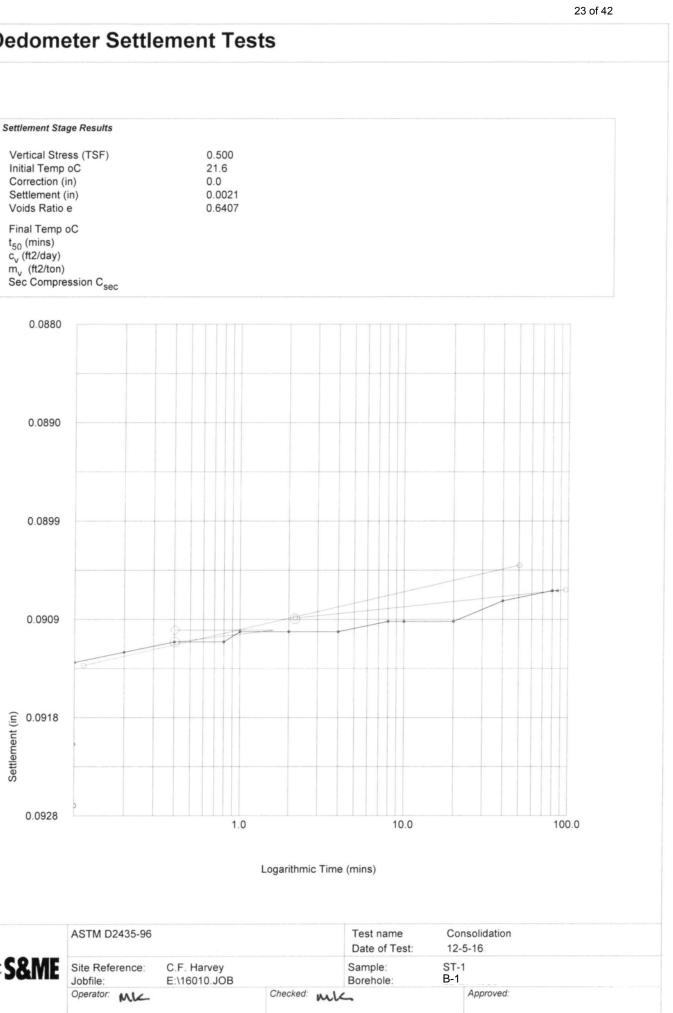
S&ME

No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	927	0.0927	0.0927
2	0.017	921	0.0921	0.0921
3	0.033	921	0.0921	0.0921
4	0.050	913	0.0913	0.0913
5	0.067	913	0.0913	0.0913
6	0.083	913	0.0913	0.0913
7	0.100	913	0.0913	0.0913
8	0.200	912	0.0912	0.0912
9	0.400	911	0.0911	0.0911
10	0.800	911	0.0911	0.0911
11	1.000	910	0.0910	0.0910
12	2.000	910	0.0910	0.0910
13	4.000	910	0.0910	0.0910
14	8.000	909	0.0909	0.0909
15	10.000	909	0.0909	0.0909
16	20.000	909	0.0909	0.0909
17	40.000	907	0.0907	0.0907
18	80.000	906	0.0906	0.0906
19	86.333	906	0.0906	0.0906

Oedometer	Settlement	Tests







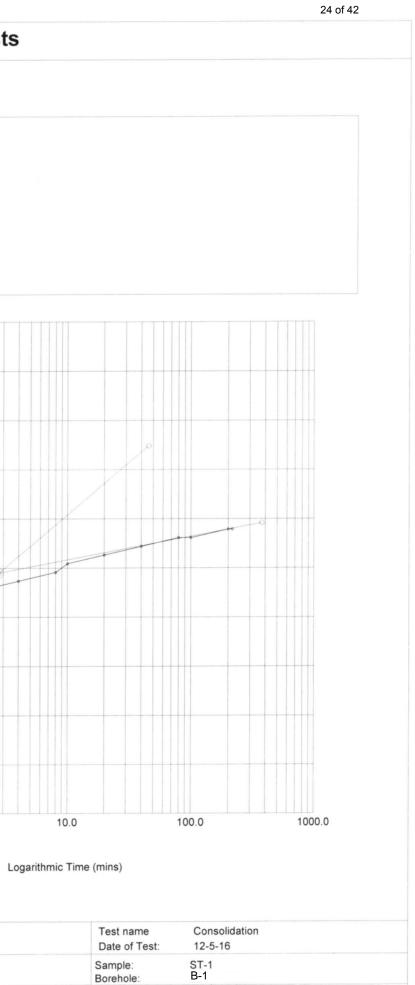
No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	906	0.0906	0.0906
2	0.017	902	0.0902	0.0902
3	0.033	902	0.0902	0.0902
4	0.050	897	0.0897	0.0897
5	0.067	896	0.0896	0.0896
6	0.083	895	0.0895	0.0895
7	0.100	894	0.0894	0.0894
8	0.200	891	0.0891	0.0891
9	0.400	889	0.0889	0.0889
10	0.800	886	0.0886	0.0886
11	1.000	884	0.0884	0.0884
12	2.000	881	0.0881	0.0881
13	4.000	880	0.0880	0.0880
14	8.000	879	0.0879	0.0879
15	10.000	878	0.0878	0.0878
16	20.000	877	0.0877	0.0877
17	40.000	876	0.0876	0.0876
18	80.000	875	0.0875	0.0875
19	100.000	875	0.0875	0.0875
20	200.000	874	0.0874	0.0874
21	216.330	874	0.0874	0.0874

# **Oedometer Settlement Tests**

np oC	21.0	
		132
y) on)		
50		
1		
3		
		- Of
		A
4		
<b>~</b>		
6		
5		
	itress (TSF)         np oC         n (in)         nt (in)         nt (in)         ito e         np oC         (y)         nn)         pression C <sub>sec</sub> 50         51         53         6	n (in)     0.0       n (in)     0.0       nt (in)     0.00       itio e     0.64       np oC     (in)       (in)     0.64       (in)     0.64 </td

Consolidation Load: 0.050 (TSF) ASTM D2435-96 Test name Date of Test: 12-5-16 S&ME ST-1 B-1 Sample: Site Reference: C.F. Harvey E:\16010.JOB Borehole: Jobfile: Checked: ML Operator: MLL Approved:



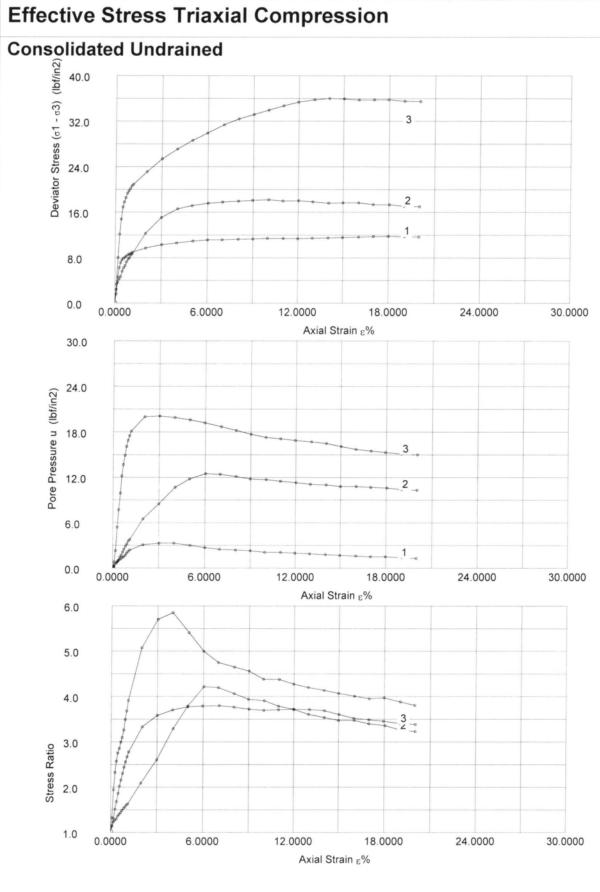


Checked:	ALL.
	· ~ ~

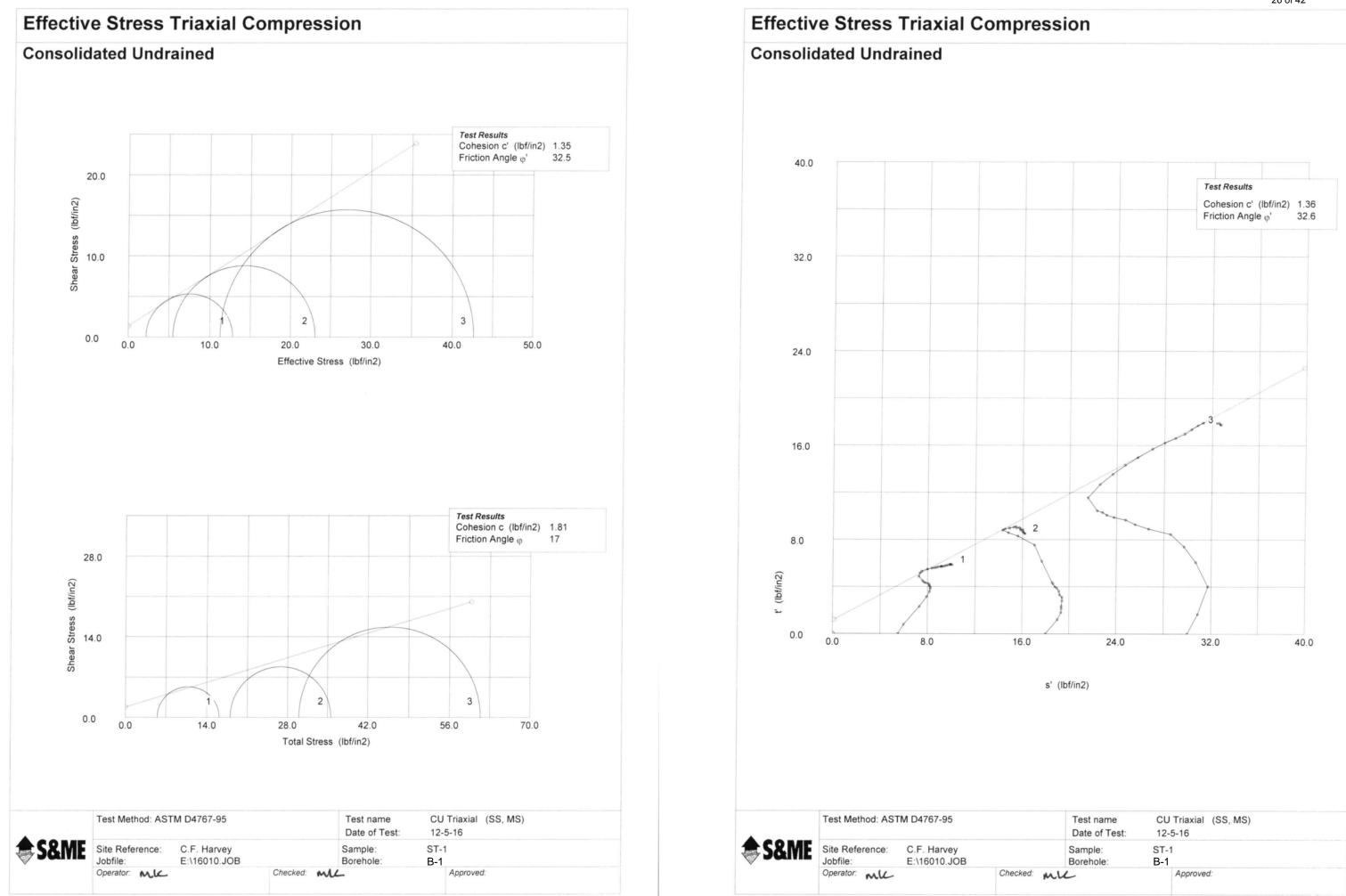
# **Effective Stress Triaxial Compression**

### **Consolidated Undrained**

Sketch sho		Depth	10	.5 - 12.5	5 ft			
location in	wing specimen original Sample	Description:				Fine to Coarse	SAND (A	A-2-4) (0)
		Type Height H <sub>0</sub> (in) Diameter D <sub>0</sub> ( Weight W <sub>0</sub> (g Bulk Density Particle Dens	(in) r) o (PCF)	Specir Undist 5.9714 2.863 1181.6 117.09 2.658 (meas	urbed 4 6	Specimen 2 Undisturbed 6.034 2.863 1184.6 116.17 2.658 (measured)	Specir Undist 5.923 2.867 1182.4 117.80 2.658 (meas	turbed
nitial Conditio	2005							
intiar conditio	<i>///3</i>	Specimen 1	Specim	nen 2	Specim	nen 3		
Pore Pressur		5.5 0.0 0.0059 1	18.0 0.0 0.0051 1		30.0 0.0 0.0061 1			
	. ,	0.012	0.012		0.012			
Strain Chann		1798 1776	1798 1776		1798 1776			
Pore P. Char	inel	1779	1779		1779			
/olume Char	nnel	Volume Chang	y Volume	Chang	Volume	Chang		
Moisture Con Dry Density <sub>ρ</sub> /oids Ratio e	do (PCF)	29.3 90.53 0.83	29.8 89.50 0.85		28.9 91.41 0.81			
eg of Satura inal B Value	ation S <sub>0</sub> %	93.74 0.98	92.85 0.99		94.22 0.99			
<i>Final Condition</i> Moisture Con Dry Density ρ /oids Ratio e	tent w <sub>f</sub> % <sub>d</sub> (PCF) f	Specimen 1 28.8 93.06 0.78	Specim 27.3 94.57 0.75	en 2	Specime 25.3 97.44 0.70	en 3		Failure Sketch Sp 1 Sp 2
eg of Satura	ition S <sub>f</sub> %	97.97	96.20		95.80			(=)
ailure Criteri xial Strain Ef		Mx Stress Rati 4.0	oMx Stre 6.0	ss Ratio	Mx Stre 7.0	ss Ratio		(=/=/
	ss (σ <sub>1</sub> - σ <sub>3</sub> )f (lbf/in2)		17.6		31.4			Sp 3
linor Stress	o <sub>3f</sub> (lbf/in2)	2.2	5.5		11.3			
lajor Stress ( tress Ratio (	σ <sub>1f</sub> (IDT/IN2) σ <sub>1</sub> /σ <sub>2</sub> ) <sub>f</sub>	12.8 5.8	23.1 4.2		42.7 3.8			$(\simeq)$
lotes:	-1-51							(=)



	Test Method: AST	M D4767-95		Test name Date of Test:		Triaxial (SS, MS) 5-16
S&ME	Site Reference: Jobfile:	C.F. Harvey E:\16010.JOB		Sample: Borehole:	ST- B-1	1
	Operator: MLL		Checked:	me		Approved:



	Test name Date of Test:	CU Triaxial (SS, MS) 12-5-16	
	Sample: Borehole:	ST-1 B-1	
Checked:	mic	Approved:	

# **Effective Stress Triaxial Compression**

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# **Consolidated Undrained Shear (Specimen 1)**

	No.	Strain (divs)	$\underset{\epsilon\%}{\text{Strain}}$	Load (divs)	Load (Ibs)	Pore Prs (divs)	Pore Prs (lbf/in2)	D. Stress (σ <sub>1</sub> - σ <sub>3</sub> ) <sub>m</sub>	D. Stress $(\sigma_1 - \sigma_3)_c$	Minor Str σ <sub>3</sub> ΄	Major Str σ <sub>1</sub> ΄	Ratio $\sigma_1' \sigma_3'$
								(lbf/in2)	(lbf/in2)	(lbf/in2)	(lbf/in2)	
	1	41	0.00	519	0.0	0	0.0	0.0	0.0	5.50	5.50	1.00
	2	91	0.08	619	10.0	3	0.3	1.6	1.6	5.20	6.78	1.30
L	3	145	0.18	811	29.2	5	0.5	4.6	4.6	5.00	9.61	1.92
	4	201	0.27	917	39.8	7	0.7	6.3	6.3	4.80	11.08	2.31
	5	252	0.36	972	45.3	9	0.9	7.1	7.1	4.60	11.74	2.55
	6	306	0.45	1003	48.4	11	1.1	7.6	7.6	4.40	12.02	2.73
	7	365	0.55	1031	51.2	12	1.2	8.1	7.9	4.30	12.20	2.84
	8	420	0.64	1045	52.6	14	1.4	8.3	8.1	4.10	12.21	2.98
	9	474	0.73	1058	53.9	15	1.5	8.5	8.3	4.00	12.31	3.08
	10	534	0.83	1072	55.3	17	1.7	8.7	8.5	3.80	12.32	3.24
	11	587	0.92	1081	56.2	20	2.0	8.8	8.7	3.50	12.15	3.47
	12	642	1.02	1089	57.0	22	2.2	8.9	8.8	3.30	12.07	3.66
	13	702	1.12	1103	58.4	24	2.4	9.1	9.0	3.10	12.08	3.90
	14	1210	1.98	1164	64.5	31	3.1	10.0	9.7	2.40	12.12	5.05
	15	1830	3.02	1214	69.5	33	3.3	10.7	10.3	2.20	12.51	5.68
	16	2397	3.98	1250	73.1	33	3.3	11.1	10.6	2.20	12.83	5.83
	17	3025	5.04	1286	76.7	30	3.0	11.5	11.0	2.50	13.47	5.39
	18	3592	6.00	1311	79.2	27	2.7	11.8	11.1	2.80	13.94	4.98
	19	4164	6.97	1328	80.9	25	2.5	11.9	11.2	3.00	14.19	4.73
	20	4791	8.03	1347	82.8	24	2.4	12.0	11.3	3.10	14.35	4.63
	21	5364	9.00	1367	84.8	23	2.3	12.2	11.3	3.20	14.53	4.54
	22	5933	9.96	1389	87.0	21	2.1	12.4	11.4	3.40	14.84	4.36
	23	6563	11.02	1403	88.4	21	2.1	12.4	11.4	3.40	14.81	4.36
	24	7132	11.98	1417	89.8	20	2.0	12.5	11.4	3.50	14.89	4.25
	25	7703	12.95	1436	91.7	19	1.9	12.6	11.5	3.60	15.05	4.18
	26	8330	14.01	1459	94.0	18	1.8	12.8	11.5	3.70	15.23	4.12
	27	8901	14.97	1478	95.9	17	1.7	12.9	11.6	3.80	15.39	4.05
	28	9530	16.04	1500	98.1	16	1.6	13.0	11.7	3.90	15.55	3.99
	29	10102	17.00	1523	100.4	15	1.5	13.2	11.7	4.00	15.73	3.93
	30	10675	17.97	1545	102.6	15	1.5	13.3	11.8	4.00	15.80	3.95
	31	11303	19.03	1556	103.7	14	1.4	13.3		4.10	15.83	3.86
	32	11865	19.98	1569	105.0	13	1.3	13.3		4.20	15.90	3.79

Effective Stress Tr	riaxial	Com
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# **Consolidated Undrained Shear (Specimen 2)**

	No.	Strain (divs)	$\underset{\epsilon \%}{\text{Strain}}$	Load (divs)	Load (Ibs)	Pore Prs (divs)	Pore Prs (Ibf/in2)	D. Stress $(\sigma_1 - \sigma_3)_m$ (Ibf/in2)	D. Stress $(\sigma_1 - \sigma_3)_c$ (lbf/in2)	Minor Str σ <sub>3</sub> ΄ (Ibf/in2)	Major Str <sup>σ</sup> 1 <sup>'</sup> (Ibf/in2)	Ratio $\sigma_1'' \sigma_3'$
	1	35	0.00	602	0.0	0	0.0	0.0	0.0	18.00	18.00	1.00
	2	90	0.09	753	15.1	2	0.2	2.4	2.4	17.80	20.23	1.14
	3	143	0.18	828	22.6	5	0.5	3.6	3.6	17.50	21.14	1.21
	4	201	0.28	869	26.7	8	0.8	4.3	4.3	17.20	21.49	1.25
	5	255	0.37	894	29.2	10	1.0	4.7	4.7	17.00	21.69	1.28
	6	308	0.46	952	35.0	14	1.4	5.6	5.6	16.60	22.21	1.34
	7	367	0.56	999	39.7	17	1.7	6.4	6.2	16.30	22.50	1.38
	8	421	0.65	1025	42.3	21	2.1	6.8	6.6	15.90	22.51	1.42
	9	475	0.74	1065	46.3	25	2.5	7.4	7.2	15.50	22.75	1.47
L	10	534	0.84	1096	49.4	29	2.9	7.9	7.7	15.10	22.83	1.51
	11	587	0.93	1112	51.0	32	3.2	8.1	8.0	14.80	22.78	1.54
	12	642	1.02	1143	54.1	36	3.6	8.6	8.5	14.40	22.87	1.59
	13	699	1.12	1158	55.6	38	3.8	8.9	8.7	14.20	22.90	1.61
	14	1203	1.97	1399	79.7	65	6.5	12.6	12.3	11.50	23.81	2.07
	15	1811	3.00	1589	98.7	85	8.5	15.4	15.1	9.50	24.57	2.59
	16	2427	4.04	1706	110.4	107	10.7	17.1	16.6	7.30	23.90	3.27
	17	2987	4.98	1759	115.7	118	11.8	17.7	17.2	6.20	23.36	3.77
	18	3608	6.03	1806	120.4	125	12.5	18.2	17.6	5.50	23.10	4.20
	19	4168	6.98	1837	123.5	124	12.4	18.5	17.8	5.60	23.40	4.18
	20	4788	8.02	1867	126.5	121	12.1	18.8	18.0	5.90	23.85	4.04
	21	5350	8.97	1895	129.3	118	11.8	19.0	18.1	6.20	24.29	3.92
	22	5972	10.02	1923	132.1	117	11.7	19.2	18.2	6.30	24.50	3.89
	23	6537	10.97	1928	132.6	115	11.5	19.0	18.0	6.50	24.49	3.77
	24	7160	12.03	1953	135.1	113	11.3	19.2	18.0	6.70	24.74	3.69
	25	7724	12.98	1959	135.7	111	11.1	19.0	17.9	6.90	24.75	3.59
	26	8347	14.03	1964	136.2	110	11.0	18.9	17.6	7.00	24.61	3.52
	27	8913	14.98	1987	138.5	108	10.8	19.0	17.7	7.20	24.86	3.45
	28	9536	16.04	2009	140.7	108	10.8	19.0	17.7	7.20	24.86	3.45
	29	10100	16.99	2009	140.7	107	10.7	18.8	17.4	7.30	24.67	3.38
E	30	10725	18.04	2028	142.6	106	10.6	18.8	17.3	7.40	24.72	3.34
	31	11293	19.00	2030	142.8	104	10.4	18.6	17.1	7.60	24.69	3.25
	32	11898	20.02	2045	144.3	103	10.3	18.6	17.0	7.70	24.71	3.21

	Test Method: AST	M D4767-95		Test name Date of Test:		Triaxial (SS, MS) Shear (Specimen 1) 5-16
S&ME	Site Reference: Jobfile:	C.F. Harvey E:\16010.JOB		Sample: Borehole:	ST- B-1	1
	Operator: MK		Checked: ML	<u>_</u>		Approved:



Site Reference: C.F. Harvey Jobfile: E:\16010.JOB S&ME Operator: ML

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# npression

	Test name Date of Test:	CU Triaxial (SS, MS) Shear (Specimen 2) 12-5-16		
	Sample: Borehole:	ST-1 B-1		
hecked:	mic	Approved:	Approved	

# **Effective Stress Triaxial Compression**

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# **Consolidated Undrained Shear (Specimen 3)**

No.	Strain (divs)	Strain ε%	Load (divs)	Load (Ibs)	Pore Prs (divs)	Pore Prs (Ibf/in2)	D. Stress (σ <sub>1</sub> - σ <sub>3</sub> ) <sub>m</sub> (Ibf/in2)	D. Stress (σ <sub>1</sub> - σ <sub>3</sub> ) <sub>c</sub> (lbf/in2)	Minor Str σ <sub>3</sub> ΄ (Ibf/in2)	Major Str <sup>σ</sup> 1 <sup>'</sup> (lbf/in2)	Ratio $\sigma_1' \sigma_3'$
1	247	0.00	688	0.0	0	0.0	0.0	0.0	30.00	30.00	1.00
2	302	0.09	894	20.6	8	0.8	3.3	3.3	29.20	32.53	1.11
3	359	0.19	1186	49.8	23	2.3	8.0	8.0	27.70	35.74	1.29
4	414	0.29	1442	75.4	54	5.4	12.2	12.2	24.60	36.76	1.49
5	468	0.38	1606	91.8	77	7.7	14.8	14.8	22.30	37.09	1.66
6	526	0.48	1739	105.1	99	9.9	16.9	16.9	20.10	37.01	1.84
7	580	0.57	1806	111.8	122	12.2	18.0	17.8	17.80	35.61	2.00
8	634	0.67	1853	116.5	137	13.7	18.7	18.6	16.30	34.85	2.14
9	694	0.77	1903	121.5	149	14.9	19.5	19.3	15.10	34.44	2.28
10	749	0.87	1931	124.3	161	16.1	19.9	19.8	13.90	33.67	2.42
11	805	0.96	1956	126.8	169	16.9	20.3	20.1	13.10	33.25	2.54
12	863	1.06	1987	129.9	175	17.5	20.8	20.6	12.50	33.12	2.65
13	919	1.16	2006	131.8	181	18.1	21.1	20.9	11.90	32.81	2.76
14	1428	2.04	2165	147.7	200	20.0	23.4	23.1	10.00	33.12	3.31
14	1994	3.01	2329	164.1	201	20.1	25.7	25.4	9.90	35.28	3.56
16	2566	4.00	2465	177.7	199	19.9	27.6	27.1	10.10	37.21	3.68
17	3134	4.00	2587	189.9	196	19.6	29.2	28.6	10.40	39.02	3.75
18	3702	5.96	2698	201.0	192	19.2	30.6	29.9	10.80	40.73	3.77
	4330	7.04	2823	213.5	187	18.7	32.1	31.4	11.30	42.68	3.78
19	4330	8.02	2921	223.3	182	18.2	33.2	32.4	11.80	44.22	3.75
20	5472	9.02	3004	231.6	177	17.7	34.1	33.2	12.30	45.50	3.70
21	6039	9.99	3087	239.9	173	17.3	34.9	34.0	12.70	46.66	3.67
22				239.9	173	17.1	35.7	34.7	12.90	47.61	3.69
23	6609	10.97	3171			16.9	36.5	35.4	13.10	48.47	3.70
24	7183	11.96	3251	256.3	169	16.7	37.0	35.8	13.30	49.10	3.69
25	7808	13.04	3318	263.0	167			36.0	13.50	49.51	3.67
26	8383	14.03	3369	268.1	165	16.5	37.3		13.90	49.84	3.59
27	8952	15.01	3399	271.1	161	16.1	37.3	35.9	14.30	50.03	3.59
28	9523	16.00	3420	273.2	157	15.7	37.1	35.7		50.03	3.47
29	10100	16.99	3460	277.2	155	15.5	37.2	35.8	14.50		3.47
30	10654	17.95	3499	281.1	153	15.3	37.3	35.8	14.70	50.48	
31	11260	18.99	3520	283.2	151	15.1	37.1	35.5	14.90	50.44	3.39
32	11863	20.03	3555	286.7	150	15.0	37.1	35.5	15.00	50.48	3.37

	Test Method: AS	TM D4767-95		Test name Date of Test:	CU Triax 12-5-16	ial (SS, MS) Shear (Specimen 3)
S&ME	Site Reference:			Sample:	ST-1	
	Jobfile:	E:\16010.JOB		Borehole:	B-1	
	Operator: MLL	-	Checked: M	le	Appr	oved:

Form No. TR-T88 Revision No. 0

Revision Date: 12/20/09

### **Particle Size Analysis of Soils**

S&ME, I	nc. Raleigh, 3	201 Spring For	est Road, Ral	eigh, North C	Carolina 27	616	
S&ME Project #: 6235	5-16-010			Repo	rt Date:	12/2	27/16
Project Name: C.F.	Harvey Parkw	ay Extension R-	5703	Test l	Date(s):	12/24 -	12/27/16
State Project #: N/A	-	F.A. Project No	: N/A	TIF	NO: 1	N/A	
Client Name: Mich	nael Baker Eng	ineering					
Address: Rale	igh, NC						
Boring #: EB2	-A LT LN	Sample #:	ST-2		Sample Da	ate:	N/A
Location: 89+5	50	Offset:	34 LT		Depth (		- 10.0 ft.
Sample Description:			Gray Silty C	Clayey Coarse	to Fine SA	ND A-2-	4 (0)
1.5" 1"3/4" 1 100%	/2'3/8" #4	#10 #20	#40 #60 #100	#200 #270			
90%							
80%							
70%							
Passi							
60%							
40%							
30%							
				$\mathbf{N}$			
20%							
10%							
0%			*				
100	10	1		0.1	0.01		0.0
		Particle	Size (mm)				
As Define	ed by NCDOT			e Sand	< 0.25	5 mm and $>$	0.05 mm
Gravel		nd > 2.00 mm		Silt	< 0.0	$0.0000 \pm 0.0000$	
Coarse Sand Maximum Particle Size	<u> &lt; 2.00 mm</u> #4	and >0.25 mm Coarse		Clay 35%	Silt	< 0.005 m	n 8%
Gravel	10%	Fine Sa		39%	Clay		8%
Apparent Relative Density	ND		re Content	30.6%	% Passing	#200	19.3%
Liquid Limit	30	Plastic		29	Plastic Inc		1
.1	- •		r (-#10 Sieve)				-
Coarse Sand	39%	Fine Sand	44%	Silt	8%	Clay	9%
Description of Sand & Grav	el Particles:	Rounded			Ang		X
Hard & Durable	X	Soft		Weat	hered & Fria	able	
References / Comments / Deviation	ons: ND=N	ot Determined.					
<u>Mal Krajan, ET</u>		104-01-0703		Laboratory M	anager	<u>12</u>	/27/2016
Technician Name		Certification No.		Position			Date
<u>Mal Krajan, ET</u>	(	ME	5	Laboratory M	anager	9/	26/2016
Technical Responsibility		Signature		Position		<u></u>	Date
reenneur nesponsionny							



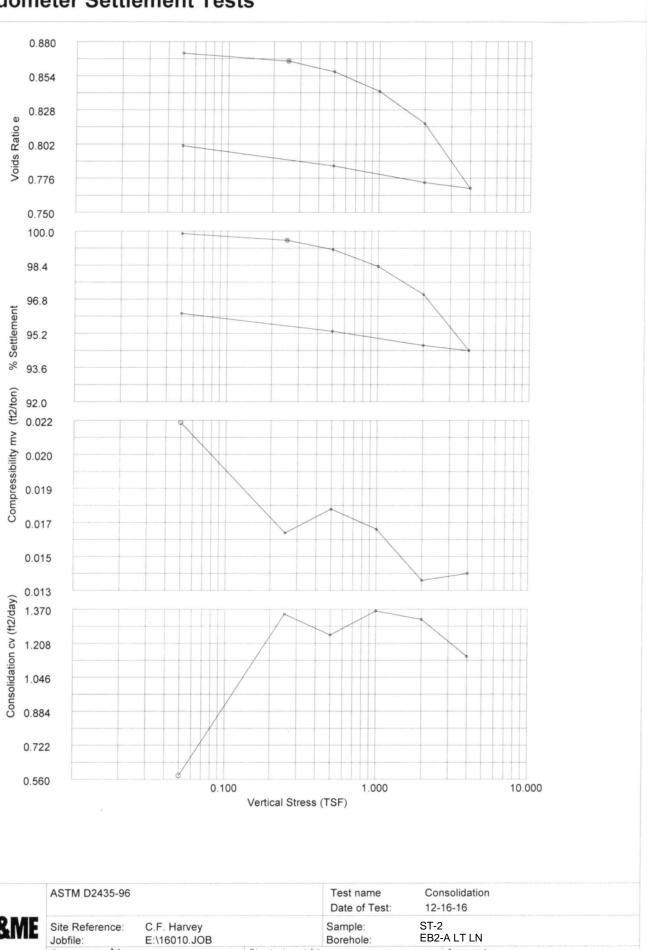
AASHTO T88 as Modified by NCDOT

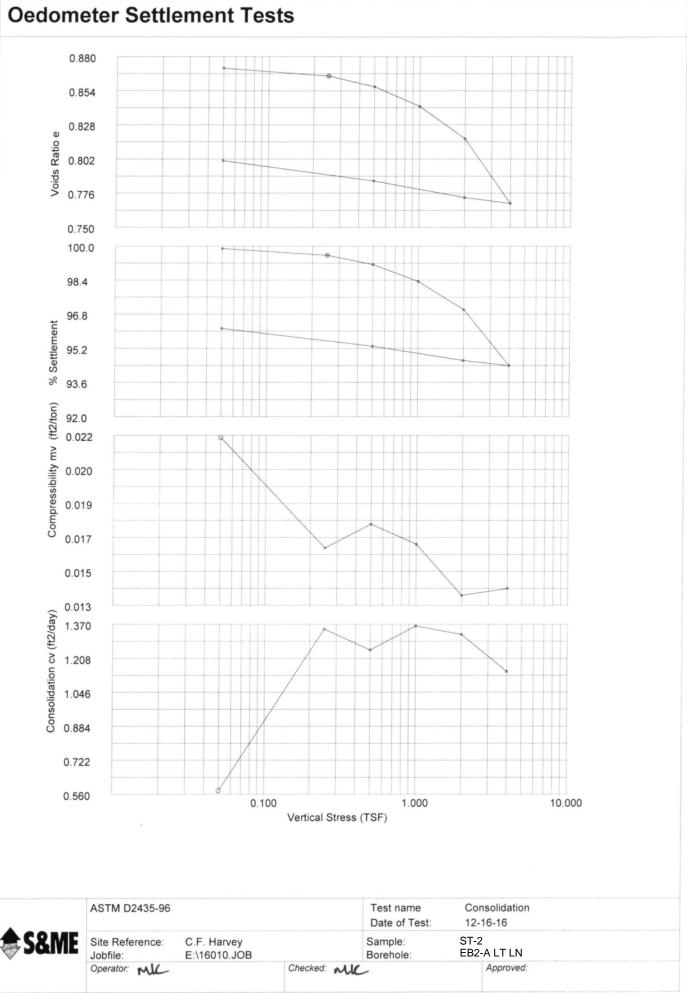
Quality Assur	rance
---------------	-------

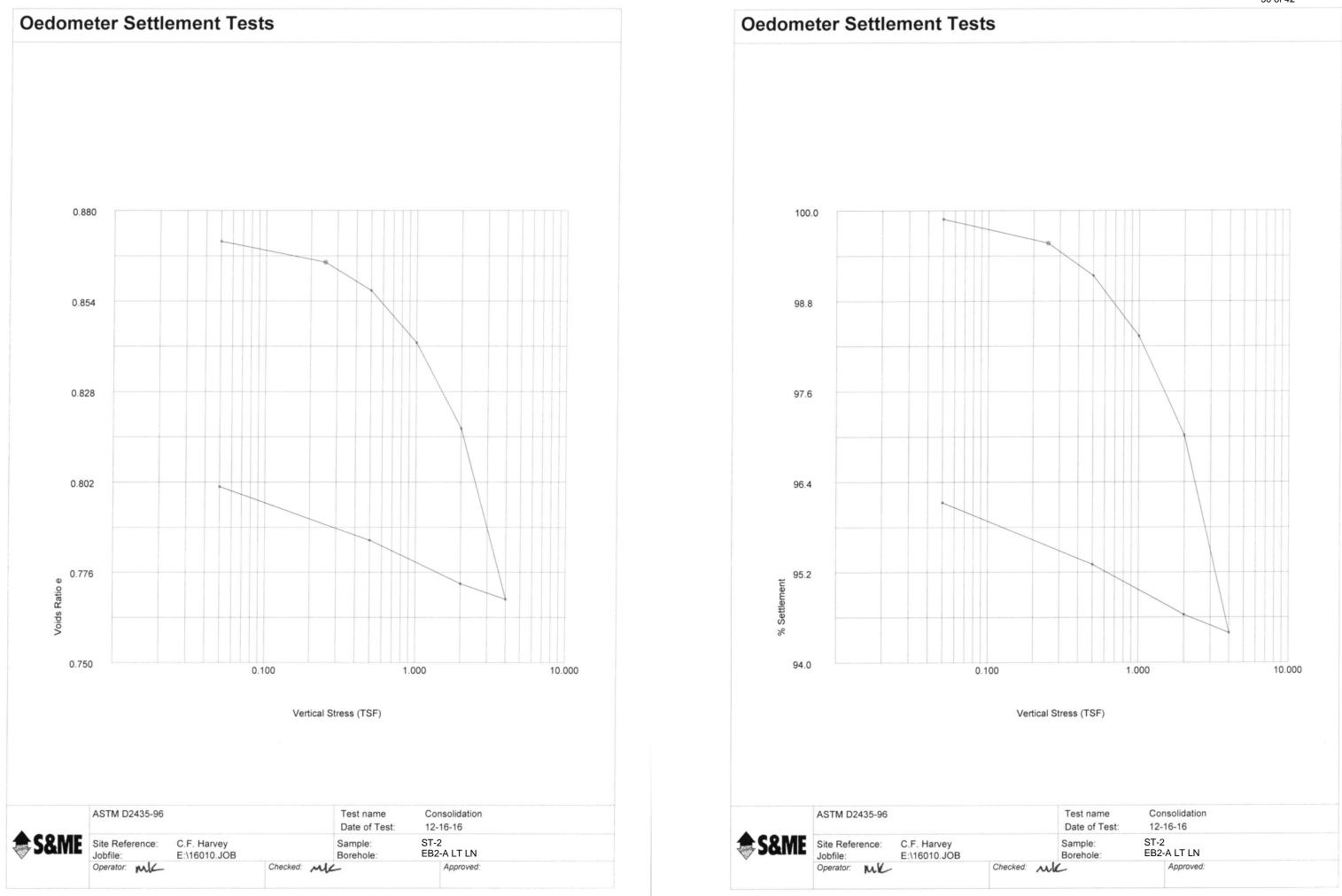
3201 Spring Forest Road Raleigh, NC 27616

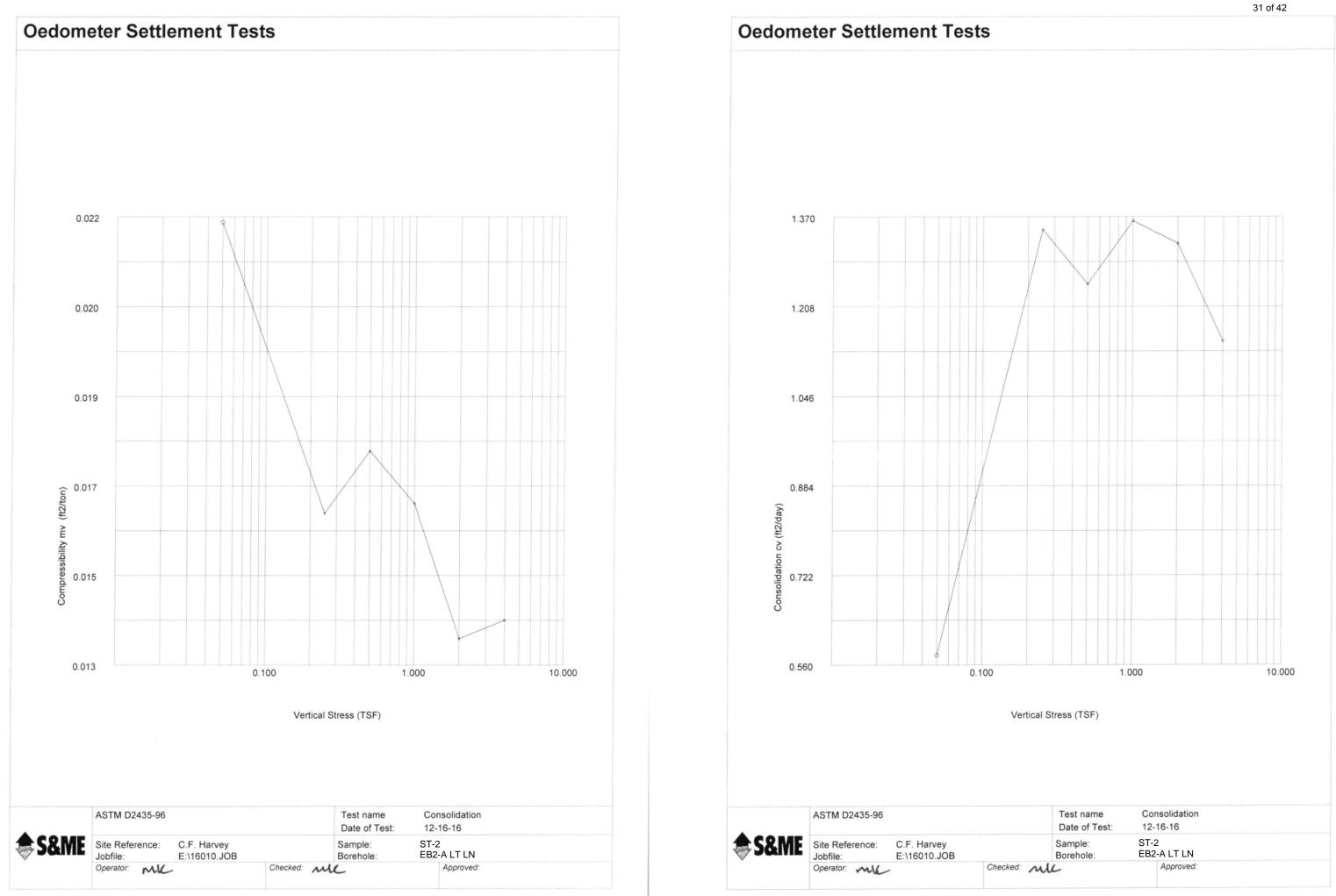
EB2-A-LT LN ST-2 (8.0 - 10.0 ft) Classification.xls

Sample details	Depth	8.0 - 10.0 ft.	
Sketch showing specimen location in original Sample		Gray Silty Clayey Coarse to Fine SAND (A	-2-4) (0)
	Type Height $H_0$ (in) Diameter $D_0$ (in) Weight $W_0$ (gr) Bulk Density $\rho$ (PCF Particle Density $\rho_s$	148.43	
itial Conditions			
ettlement Channel	1065		
oisture Content w <sub>0</sub> %	30.6		
ry Density <sub>ρd</sub> (PCF) oids Ratio e <sub>0</sub>	88.38 0.8732		
eg of Saturation S <sub>0</sub> %	93.1		
welling Pressure Ss (TSF)	0.000		
oisture Content w <sub>f</sub> % ry Density <sub>Pd</sub> (PCF) pids Ratio e <sub>f</sub>	34.0 91.94 0.8007		
oisture Content w <sub>f</sub> % ry Density $\rho_d$ (PCF) oids Ratio e <sub>f</sub> eg of Saturation S <sub>f</sub> %	91.94		
oisture Content $w_f$ % ry Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f$ % ettlement: (in)	91.94 0.8007 100.00		
oisture Content $w_f$ % ry Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f$ % ettlement: (in) pompression Index $C_c$	91.94 0.8007 100.00 0.039 0.168	en taken from the middle portion of UD tub	Э.
oisture Content $w_f$ % ry Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f$ % ettlement: (in) compression Index $C_c$	91.94 0.8007 100.00 0.039 0.168	en taken from the middle portion of UD tub	9.
oisture Content $w_f$ % y Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f$ % ettlement: (in) pmpression Index $C_c$	91.94 0.8007 100.00 0.039 0.168	en taken from the middle portion of UD tub	Э.
oisture Content $w_f$ % y Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f$ % ettlement: (in) pmpression Index $C_c$	91.94 0.8007 100.00 0.039 0.168	en taken from the middle portion of UD tub	9.
oisture Content $w_f$ % y Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f$ % ettlement: (in) pmpression Index $C_c$	91.94 0.8007 100.00 0.039 0.168	en taken from the middle portion of UD tub	9.
oisture Content $w_f$ % y Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f$ % ettlement: (in) pmpression Index $C_c$	91.94 0.8007 100.00 0.039 0.168	en taken from the middle portion of UD tub	Э.
poisture Content $w_f\%$ y Density $\rho_d$ (PCF) poids Ratio $e_f$ eg of Saturation $S_f\%$ ettlement: (in) pompression Index $C_c$	91.94 0.8007 100.00 0.039 0.168	en taken from the middle portion of UD tub	9.
poisture Content $w_f\%$ y Density $\rho_d$ (PCF) poids Ratio $e_f$ eg of Saturation $S_f\%$ ettlement: (in) pompression Index $C_c$	91.94 0.8007 100.00 0.039 0.168	en taken from the middle portion of UD tub	9.
oisture Content $w_f$ % ry Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f$ % ettlement: (in) compression Index $C_c$	91.94 0.8007 100.00 0.039 0.168 Test specime	Test name Cor	solidation
inal Conditions loisture Content $w_f^{\%}$ ry Density $\rho_d$ (PCF) oids Ratio $e_f$ eg of Saturation $S_f^{\%}$ ettlement: (in) ompression Index $C_c$ otes: ASTM D2435 SENFE	91.94 0.8007 100.00 0.039 0.168 Test specime	Test name Cor	solidation 16-16









	Test name Date of Test:	Consolidation 12-16-16	
	Sample: Borehole:	ST-2 EB2-A LT LN	
checked:	nic	Approved:	

Stress (TSF)	Initial Temp. oC	Settlement Total (in)	Cal Corr. (in)	Final Temp. oC	Voids Ratio e <sub>f</sub>	t <sub>50</sub> (mins)	Secondary Compr C <sub>sec</sub>	c <sub>v</sub> (ft2/day)	m <sub>v</sub> (ft2/ton)
0.050	21.6	0.0011	0.0	21.6	0.8712	0.860	0.00	0.577	0.022
0.250	21.6	0.0043	0.0	21.6	0.8651	0.367	0.0001	1.347	0.016
0.500	21.6	0.0086	0.0	21.6	0.8571	0.393	0.0002	1.248	0.017
1.000	21.6	0.0166	0.0	21.6	0.8420	0.356	0.0002	1.362	0.016
2.000	21.6	0.0297	0.0	21.6	0.8174	0.359	0.0002	1.322	0.014
4.000	21.6	0.0559	0.0	21.6	0.7682	0.398	0.0011	1.145	0.014
2.000	21.6	0.0535	0.0	21.6	0.7727				0.001
0.500	21.6	0.0468	0.0	21.6	0.7853				0.005
0.050	21.6	0.0386	0.0	21.6	0.8007				0.019

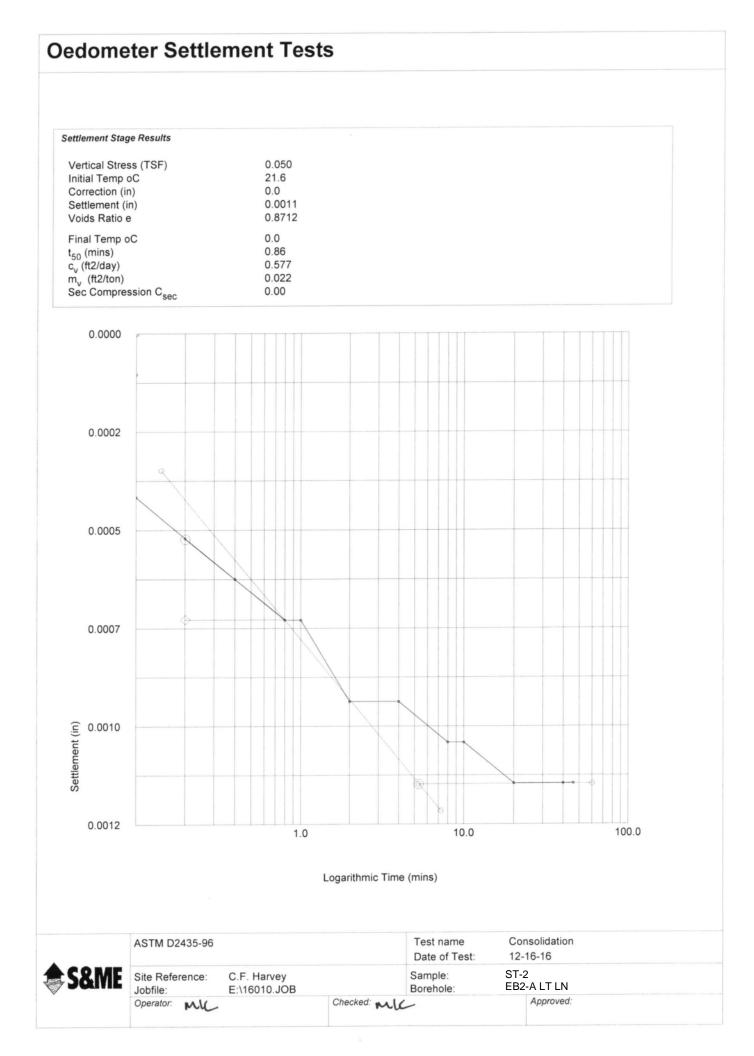
# **Oedometer Settlement Tests**

No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	0	0.0000	0.0000
2	0.017	1	0.0001	0.0001
3	0.033	1	0.0001	0.0001
4	0.050	1	0.0001	0.0001
5	0.067	1	0.0001	0.0001
6	0.083	1	0.0001	0.0001
7	0.100	4	0.0004	0.0004
8	0.200	5	0.0005	0.0005
9	0.400	6	0.0006	0.0006
10	0.800	7	0.0007	0.0007
11	1.000	7	0.0007	0.0007
12	2.000	9	0.0009	0.0009
13	4.000	9	0.0009	0.0009
14	8.000	10	0.0010	0.0010
15	10.000	10	0.0010	0.0010
16	20.000	11	0.0011	0.0011
17	40.000	11	0.0011	0.0011
18	46.167	11	0.0011	0.0011

• • • • • • • • • • • • • • • • • • • •	ASTM D2435-96			Test name Date of Test:		nsolidation 16-16	
S&ME	Site Reference: Jobfile:	C.F. Harvey E:\16010.JOB		Sample: Borehole:	ST-2 EB2	2 2-A LT LN	
	Operator: ML		Checked: MLC	-		Approved:	



	Test name Date of Test:	Consolidation 12-16-16	Load: 0.050 (TSF)
	Sample: Borehole:	ST-2 EB2-A LT LN	
Checked: M	ic	Approved:	



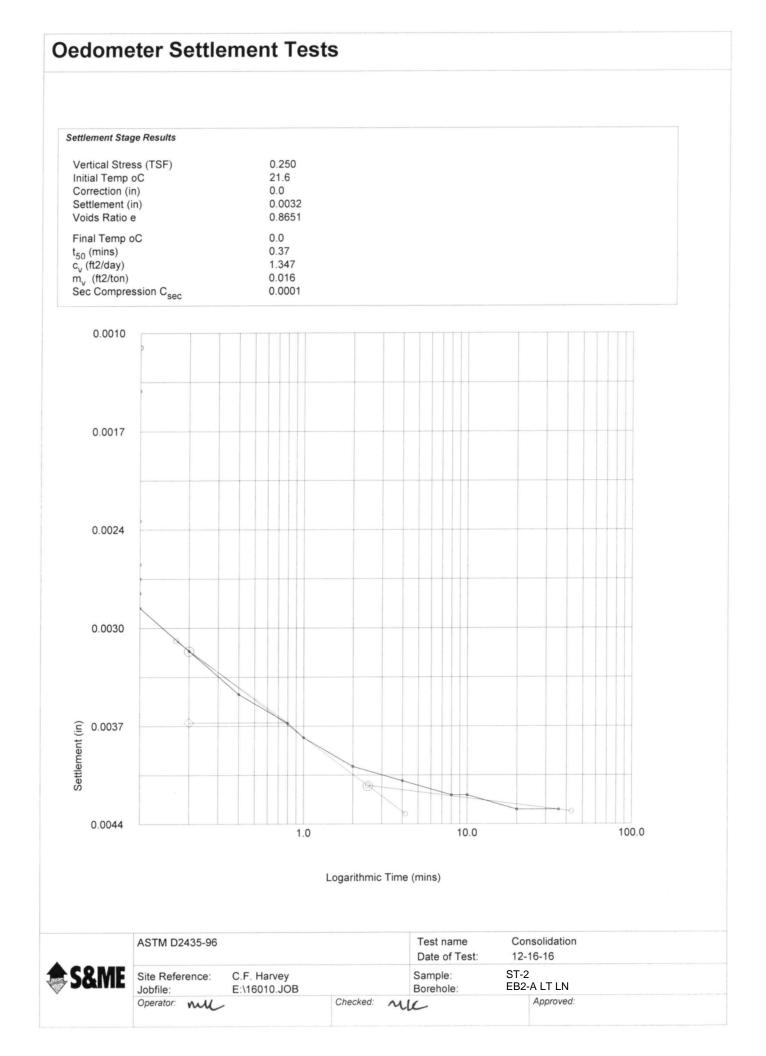
No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	11	0.0011	0.0011
2	0.017	14	0.0014	0.0014
3	0.033	23	0.0023	0.0023
4	0.050	26	0.0026	0.0026
5	0.067	27	0.0027	0.0027
6	0.083	28	0.0028	0.0028
7	0.100	29	0.0029	0.0029
8	0.200	32	0.0032	0.0032
9	0.400	35	0.0035	0.0035
10	0.800	37	0.0037	0.0037
11	1.000	38	0.0038	0.0038
12	2.000	40	0.0040	0.0040
13	4.000	41	0.0041	0.0041
14	8.000	42	0.0042	0.0042
15	10.000	42	0.0042	0.0042
16	20.000	43	0.0043	0.0043
17	35.867	43	0.0043	0.0043

ASTM D2435-96

Same Site Reference: C.F. Harvey Jobfile: E:\16010.JOB

(

	Test name Date of Test:	Consolidation 12-16-16	Load: 0.250 (TSF)
	Sample: Borehole:	ST-2 EB2-A LT LN	
Checked: MLC		Approved:	

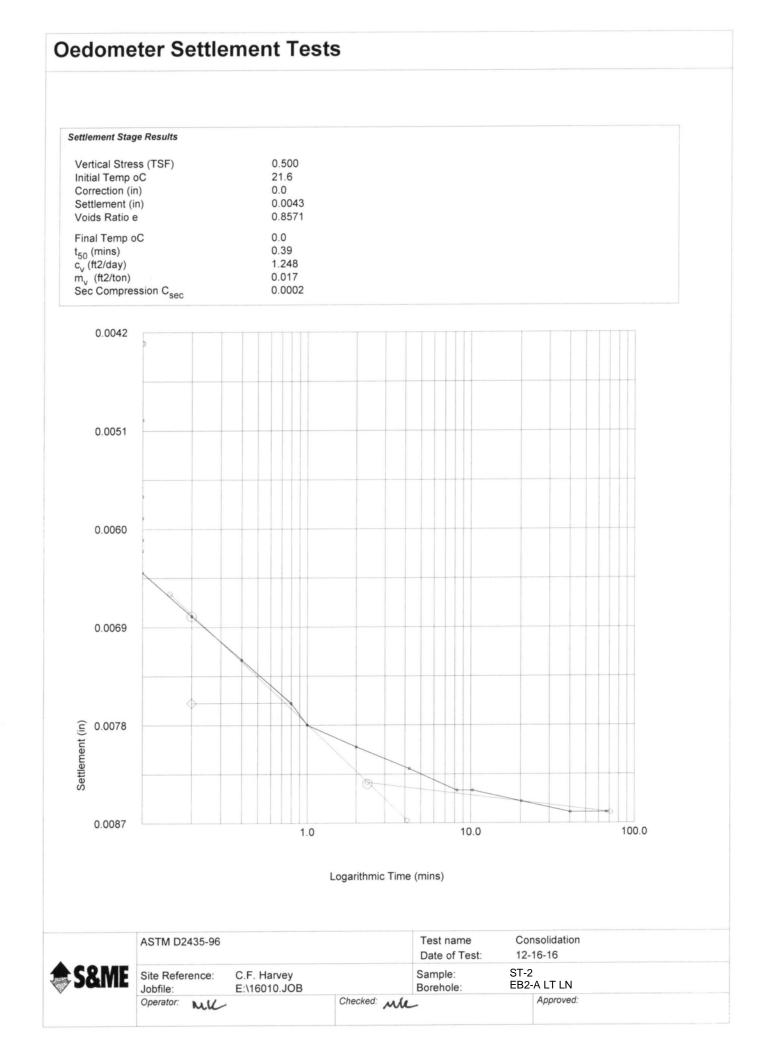


Oedometer	Settlement	Tests
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No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	43	0.0043	0.0043
2	0.017	50	0.0050	0.0050
3	0.033	57	0.0057	0.0057
4	0.050	59	0.0059	0.0059
5	0.067	61	0.0061	0.0061
6	0.083	62	0.0062	0.0062
7	0.100	64	0.0064	0.0064
8	0.200	68	0.0068	0.0068
9	0.400	72	0.0072	0.0072
10	0.800	76	0.0076	0.0076
11	1.000	78	0.0078	0.0078
12	2.000	80	0.0080	0.0080
13	4.250	82	0.0082	0.0082
14	8.250	84	0.0084	0.0084
15	10.250	84	0.0084	0.0084
16	20.250	85	0.0085	0.0085
17	40.250	86	0.0086	0.0086
18	67.350	86	0.0086	0.0086

Same Site Reference: C.F. Harvey E:\16010.JOB

Checked: MC			Approved:	
	Sample: Borehole:	ST-2 EB2	2 2-A LT LN	
	Test name Date of Test:		16-16	Load: 0.500 (TSF)

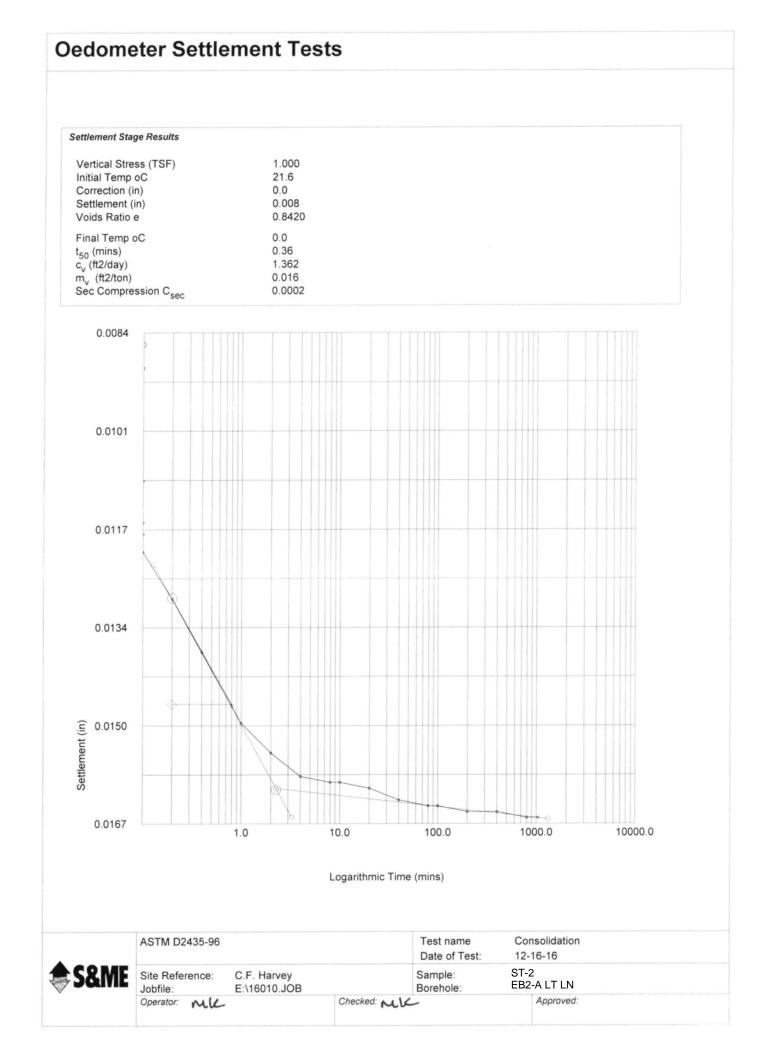


No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	86	0.0086	0.0086
2	0.017	90	0.0090	0.0090
3	0.033	90	0.0090	0.0090
4	0.050	109	0.0109	0.0109
5	0.067	116	0.0116	0.0116
6	0.083	118	0.0118	0.0118
7	0.100	121	0.0121	0.0121
8	0.200	129	0.0129	0.0129
9	0.400	138	0.0138	0.0138
10	0.800	147	0.0147	0.0147
11	1.000	150	0.0150	0.0150
12	2.000	155	0.0155	0.0155
13	4.000	159	0.0159	0.0159
14	8.000	160	0.0160	0.0160
15	10.000	160	0.0160	0.0160
16	20.000	161	0.0161	0.0161
17	40.000	163	0.0163	0.0163
18	80.000	164	0.0164	0.0164
19	100.000	164	0.0164	0.0164
20	200.000	165	0.0165	0.0165
21	400.000	165	0.0165	0.0165
22	800.000	166	0.0166	0.0166
23	1039.917	166	0.0166	0.0166

ASTM D2435-96

Same Site Reference: C.F. Harvey E:\16010.JOB

	Test name Date of Test:	Consolidation 12-16-16	Load: 1.000 (TSF)
	Sample: Borehole:	ST-2 EB2-A LT LN	
Checked: MLC		Approved:	

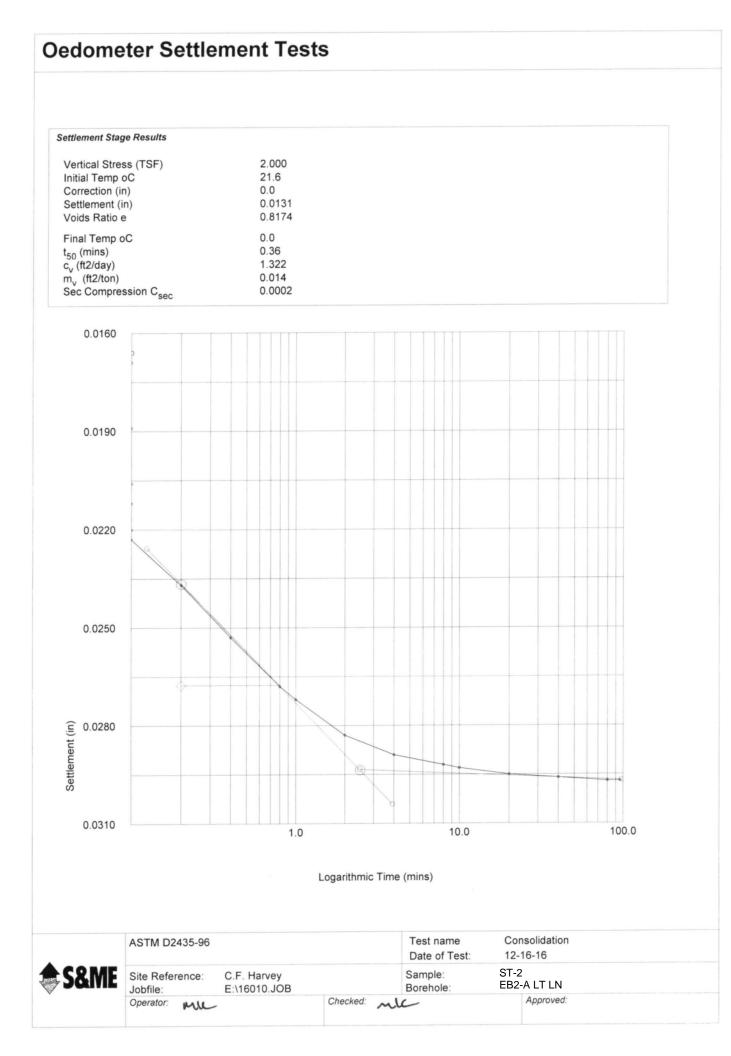


No.	Time (mins)	Dis⊳lacement (divs)	Displacement (in)	Settlement (in)
1	0.000	166	0.0166	0.0166
2	0.017	169	0.0169	0.0169
3	0.033	189	0.0189	0.0189
4	0.050	206	0.0206	0.0206
5	0.067	212	0.0212	0.0212
6	0.083	220	0.0220	0.0220
7	0.100	223	0.0223	0.0223
8	0.200	237	0.0237	0.0237
9	0.400	253	0.0253	0.0253
10	0.800	268	0.0268	0.0268
11	1.000	272	0.0272	0.0272
12	2.000	283	0.0283	0.0283
13	4.000	289	0.0289	0.0289
14	8.000	292	0.0292	0.0292
15	10.000	293	0.0293	0.0293
16	20.000	295	0.0295	0.0295
17	40.000	296	0.0296	0.0296
18	80.000	297	0.0297	0.0297
19	96.330	297	0.0297	0.0297

ASTM	D2435-96

Same Site Reference: C.F. Harvey Jobfile: E:\16010.JOB Operator: MLL

	Test name Date of Test:	Consolidation 12-16-16	Load: 2.000 (TSF)
	Sample: Borehole:	ST-2 EB2-A LT LN	
Checked: MK		Approved:	



Oedometer	Settlement	Tests
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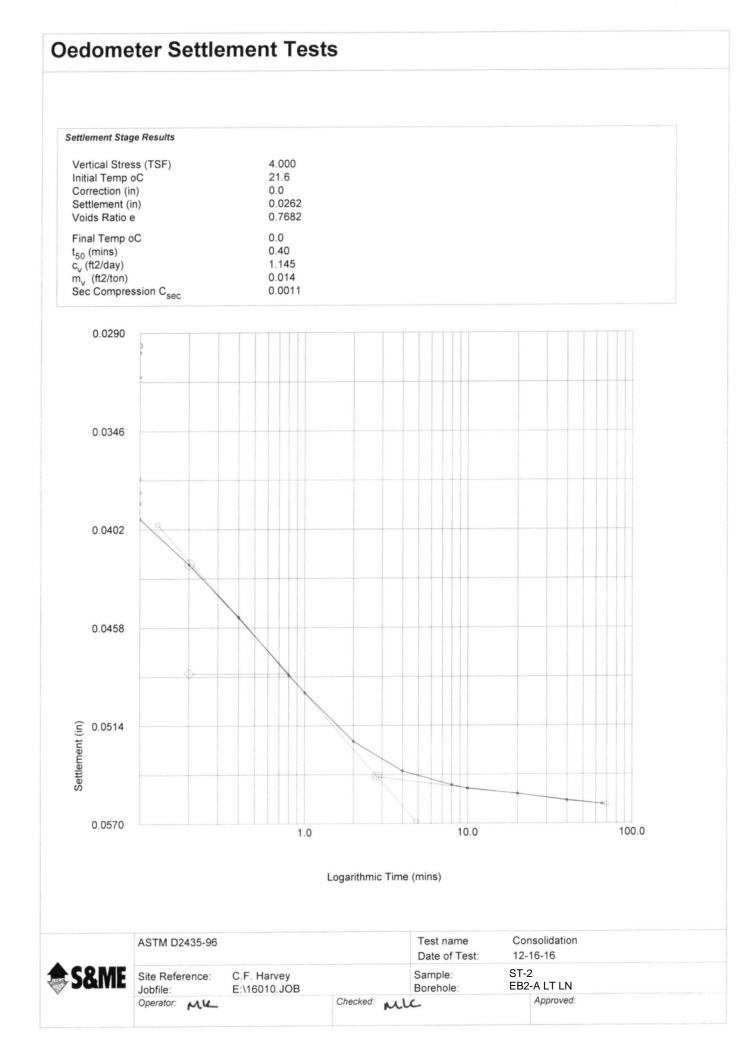
No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
	(11110)	(urre)	()	(,
1	0.000	297	0.0297	0.0297
2	0.017	301	0.0301	0.0301
3	0.033	315	0.0315	0.0315
4	0.050	373	0.0373	0.0373
5	0.067	381	0.0381	0.0381
6	0.083	387	0.0387	0.0387
7	0.100	396	0.0396	0.0396
8	0.200	422	0.0422	0.0422
9	0.400	452	0.0452	0.0452
10	0.800	485	0.0485	0.0485
11	1.000	495	0.0495	0.0495
12	2.000	523	0.0523	0.0523
13	4.000	540	0.0540	0.0540
14	8.000	548	0.0548	0.0548
15	10.000	550	0.0550	0.0550
16	20.000	553	0.0553	0.0553
17	40.000	557	0.0557	0.0557
18	65.600	559	0.0559	0.0559

Same Site Reference: Jobfile: Operator:

# Site Reference: C.F. Harvey Jobfile: E:\16010.JOB

C

Checked: MLL		Approved:		
	Sample: Borehole:	ST-2 EB2-A LT LN		
	Test name Date of Test:	Consolidation 12-16-16	Load: 4.000 (TSF)	

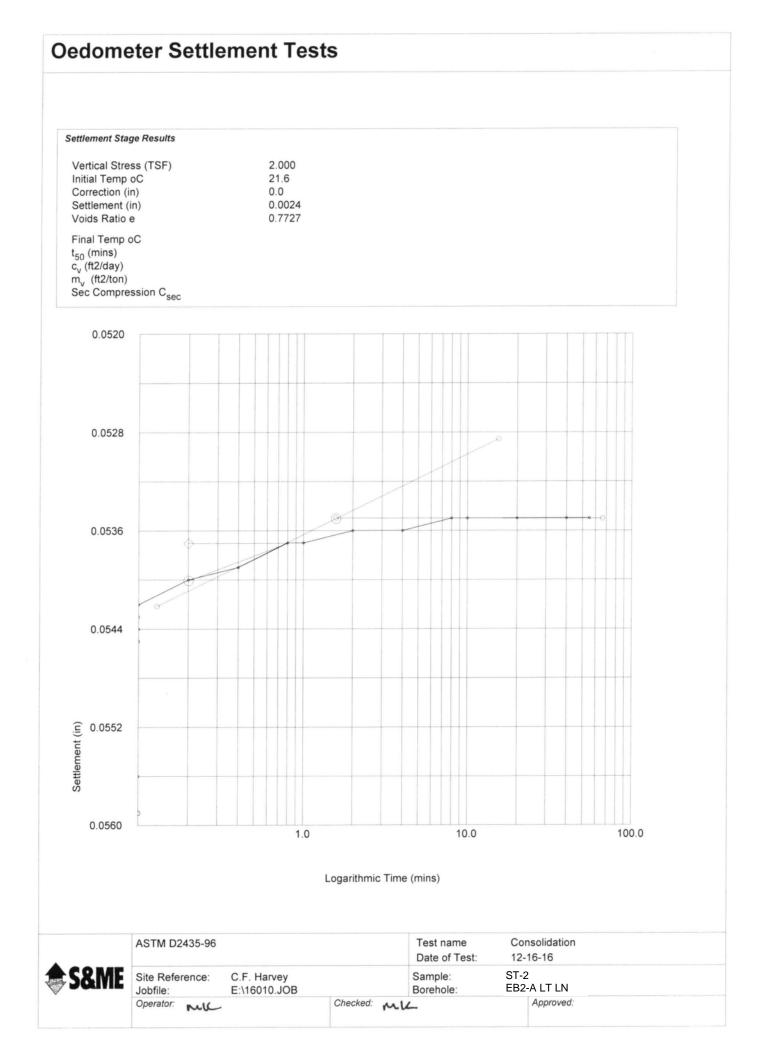


No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	559	0.0559	0.0559
2	0.017	556	0.0556	0.0556
3	0.033	556	0.0556	0.0556
4	0.050	545	0.0545	0.0545
5	0.067	544	0.0544	0.0544
6	0.083	543	0.0543	0.0543
7	0.100	542	0.0542	0.0542
8	0.200	540	0.0540	0.0540
9	0.400	539	0.0539	0.0539
10	0.800	537	0.0537	0.0537
11	1.000	537	0.0537	0.0537
12	2.000	536	0.0536	0.0536
13	4.000	536	0.0536	0.0536
14	8.000	535	0.0535	0.0535
15	10.000	535	0.0535	0.0535
16	20.000	535	0.0535	0.0535
17	40.000	535	0.0535	0.0535
18	55.167	535	0.0535	0.0535

AST	ΜD	243	5-96

Same Site Reference: C.F. Harvey E:\16010.JOB

Checked:	MIC	Approved	d:
	Sample: Borehole:	ST-2 EB2-A LT LN	J
	Test name Date of Test:	Consolidatio 12-16-16	on Load: 2.000 (TSF)



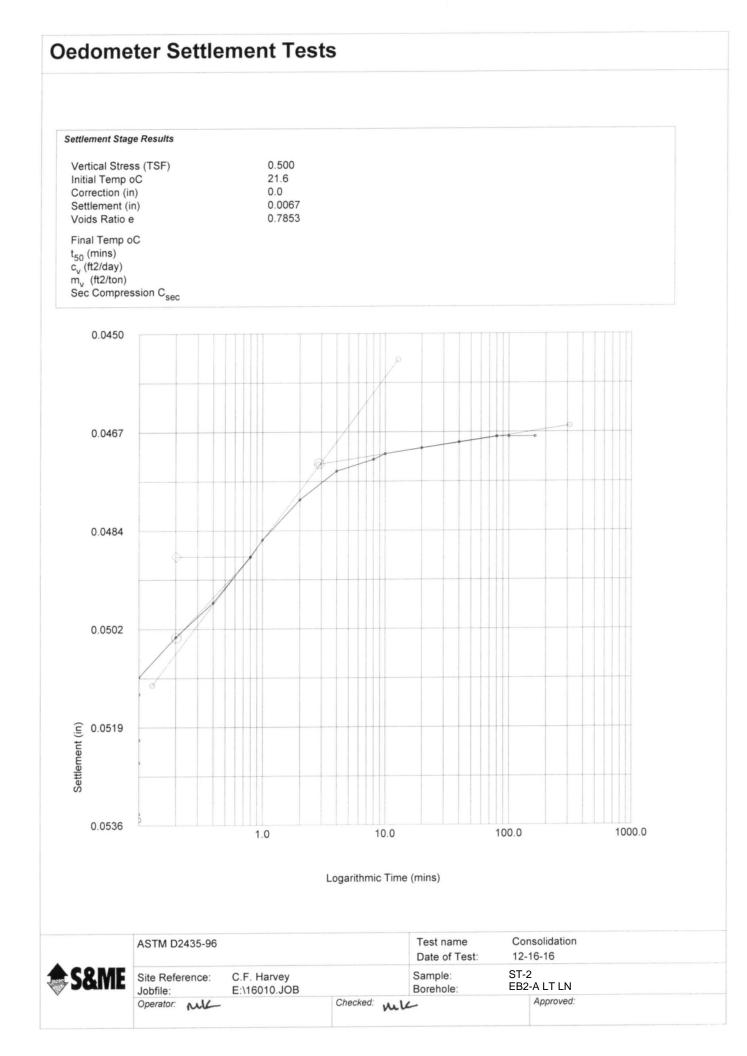
No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	535	0.0535	0.0535
2	0.017	534	0.0534	0.0534
3	0.033	534	0.0534	0.0534
4	0.050	525	0.0525	0.0525
5	0.067	521	0.0521	0.0521
6	0.083	513	0.0513	0.0513
7	0.100	510	0.0510	0.0510
8	0.200	503	0.0503	0.0503
9	0.400	497	0.0497	0.0497
10	0.800	489	0.0489	0.0489
11	1.000	486	0.0486	0.0486
12	2.000	479	0.0479	0.0479
13	4.000	474	0.0474	0.0474
14	8.000	472	0.0472	0.0472
15	10.000	471	0.0471	0.0471
16	20.000	470	0.0470	0.0470
17	40.000	469	0.0469	0.0469
18	80.000	468	0.0468	0.0468
19	100.000	468	0.0468	0.0468
20	163.330	468	0.0468	0.0468

ASTM D2435-96

Jobfile:

Same Site Reference: C.F. Harvey E:\16010.JOB Operator: ML

Checked:	mic	Approved:	
	Sample: Borehole:	ST-2 EB2-A LT LN	
	Test name Date of Test:	Consolidation Load: 0 12-16-16	.500 (TSF)



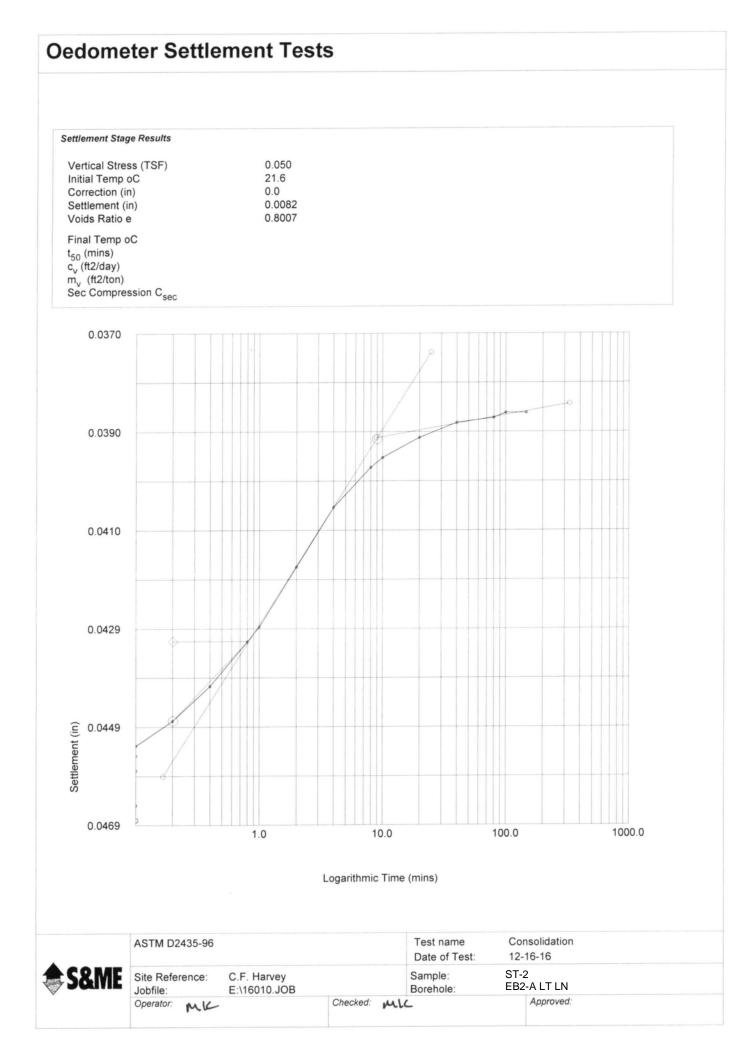
No.	Time (mins)	Displacement (divs)	Displacement (in)	Settlement (in)
1	0.000	468	0.0468	0.0468
2	0.017	465	0.0465	0.0465
3	0.033	465	0.0465	0.0465
4	0.050	458	0.0458	0.0458
5	0.067	455	0.0455	0.0455
6	0.083	453	0.0453	0.0453
7	0.100	453	0.0453	0.0453
8	0.200	448	0.0448	0.0448
9	0.400	441	0.0441	0.0441
10	0.800	432	0.0432	0.0432
11	1.000	429	0.0429	0.0429
12	2.000	417	0.0417	0.0417
13	4.000	405	0.0405	0.0405
14	8.000	397	0.0397	0.0397
15	10.000	395	0.0395	0.0395
16	20.000	391	0.0391	0.0391
17	40.000	388	0.0388	0.0388
18	80.000	387	0.0387	0.0387
19	100.000	386	0.0386	0.0386
20	147.470	386	0.0386	0.0386

ASTM D2435-96

Same Site Ref Jobfile: Operator:

Site Reference: C.F. Harvey Jobfile: E:\16010.JOB Operator: MC

Sample: ST-2	Sample: ST-2	CT 0
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Form No. TR-T88

Revision Date: 12/20/09

Revision No. 0

### **Particle Size Analysis of Soils**

S&M	Tinc Raleigh	, 3201 Spring Fore	st Road Rale	high North (		Juality Assi 516	irunce
	235-16-010	, Jaor Spring Fold	st Koau, Kalt	0,	rt Date:	11/1	4/16
5		way Extension R-5	703	*	Date(s):	10/7 - 1	
0	/A	F.A. Project No:			. ,	J/A	1/1/10
0	fichael Baker E	v	1 1/2 1		1101 1		
	aleigh, NC						
	B2-B RT LN	Sample #:	SS-7	_	Sample Da	te:	N/A
0	9+45	Offset:	33 RT		Depth (1		) - 2.5
Sample Description:				to Fine Sandy	A	/	(1)
1.5" 1"2/	4" 1/2'3/8" #4	#10 #20 #	40 #60 #100	#200 #270			
	+ 1/23/8 #4	#10 #20 #	40 #60 #100	#200 #270			
90%			$\searrow$				
80%							
			+				
70%							
4 00%			+				_
L L L L L L L L L L L L L L L L L L L				N			
50%				N			
ā 40%							
30%							
20%							
10%							
0%			*				
100	10	1 Particle Si		.1	0.01		0.0
		i ai ucic bi	× ,		-		
As De Gravel	fined by NCDOT	n and > 2.00 mm		Sand ilt		$\frac{\text{mm and} > 0}{5 \text{ and} > 0.00}$	
Coarse Sand		m and > 0.25 mm		lay	< 0.0	< 0.005  mm	
Maximum Particle Size	#4	Coarse S	•	16%	Silt		21%
Gravel	0%	Fine San	d	43%	Clay		20%
Apparent Relative Densi			Content	13.4%	% Passing	#200	47.4%
Liquid Limit	21	Plastic L		13	Plastic Ind		8
			(-#10 Sieve)	10	T fublic file	.on	0
Coarse Sand	16%	Fine Sand	43%	Silt	21%	Clay	20%
Description of Sand & G	ravel Particles:	Rounded			Angu	ılar	
Hard & Durable		Soft		Weat	hered & Fria	ble	
		=Not Determined.					
	iations: ND	-Not Determined.				-	
References / Comments / Dev				1. <b>.</b> .		4 4 /	14/001-
References / Comments / Dev <u>Mal Krajan, E</u>		<u>104-01-0703</u>	I	Laboratory M	anager	<u>11/</u>	<u>14/2016</u>
References / Comments / Dev			<u>]</u>	Laboratory M Position	anager	<u>11/</u>	<u>14/2016</u> Date
References / Comments / Dev <u>Mal Krajan, E</u> Technician Name	<u>T</u>	<u>104-01-0703</u>	-	Position			Date
References / Comments / Dev <u>Mal Krajan, E</u>	T T	<u>104-01-0703</u>	-	•			

S&ME, Inc.



AASHTO T88 as Modified by NCDOT

3201 Spring Forest Road Raleigh, NC 27616

EB2-B RT LN SS-7 (0.5 - 2 ft) Classification.xls

#### Form No: TR-T267

Revision No. 0

Revision Date: 07/10/08

# Moisture, Ash, and Organic Matter



Revision D	<i>uie</i> . 07/1	0/00							
				AA	SHTO T-267			Quality A	Assurance
		S&ME, I	nc. Raleigh	n, 3201 Spring F	orest Raod,	Raleigh,	North Caroli	na 27616	
Project #	:	6235-16-	010				Report Date:	10/2	21/16
Project Na	ame:	C.F. Harv	ey Parkwag	y Extension R-57	703		Test Date(s):	10/18 -	10/21/16
Client Nat	me:	Michael E	Baker Engir	neering					
Client Ad	dress:	Raleigh, N	٩C						
Boring #:		EB2-B R	Γ LN	Sample #:	SS	5-7	Samj	ple Date:	N/A
Location:		89+45		Offset:	33	RT	D	epth (ft):	1.0 - 2.5
Sample D	escription	on: Gray	Coarse to I	Fine Sandy Clay	ey SILT (A-4	)(1)			
Equipment	<i>t:</i>	Balance: 0	.01 g.Reada	bility, 500g. Minin	num Capaccity	,			
Balance:	S&	ME ID #:	1024	Cal. Date:	11/06/16	Due:	11/06/17		
Metho	d A: M	oisture Co	ontent Det	termination	Re	equired C	oven Temperati	ure:105 <u>+</u> 5	° C
		Ove	en Tempera	ature: 105	°C		<i>Tare</i> #	h	
	t	Tare	Weight (D	ish plus Aluminu	m Foil Cover	.)	grams	45.60	
	а	Mass	of As-Rec	eived Specimen	+ Tare Wt.		grams	91.99	
	b	Mass	of Oven D	Dry Specimen + 7	Tare Wt.		grams	86.51	
Γ	W	Wate	r Weight				( <i>a</i> - <i>b</i> )	5.48	
	Α	Mass	of As-Rec	eived Specimen			( <i>a</i> - <i>t</i> )	46.39	
	В	Mass	of Oven D	Dry Specimen			( <i>b</i> - <i>t</i> )	40.91	
	% N	Aoisture C	ontent as a	a % of As Receiv	ed or Total M	<b>I</b> ass	(w/A)*100	11.8%	
		% Moistu	re Content	t as a % of Oven	-dried Mass		(w/B)*100	13.4%	
Oven	S&	ME ID #:	1454	Cal. Date:	10/7/16	Due:	10/7/17		
	1	Method C (	(440 ° C) or	· D (750 ° C): Ast	h Content and	d Organi	ic Matter Deter	rmination	

	Muffle Furnace: 455 °C	<i>Tare</i> #	84
t	Tare Weight (Dish plus Aluminum Foil Cover)	grams	49.60
b	Mass of Oven Dry Specimen + Tare Wt.	grams	85.32
С	Ash Weight + Tare Wt.	grams	84.68
С	Ash Weight	c-t	35.08
В	Mass of Oven Dry Specimen	( <i>b</i> - <i>t</i> )	35.72
D	% Ash Content	(C/B)*100	98.2%
	% Organic Matter	100-D	1.8%

Muffle Furnace: *S&ME ID #:* 

Notes / Deviations / References:

	$\cap$	
N	-Cr	-
	C	

Signature

<u>Mal Krajan, ET</u> Technical Responsibility Laboratory Manager Position

11/14/2016 Date

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### Form No: TR-T289-1 Revision No. 0 Revision Date: 07/10/08

Revision Duie. 0	,,,10,00						
		A	ASHTO T2	89		Quality	Assurance
	S&ME, I	S&ME, Inc. Raleigh, 3201 Spring Forest Road, Raleigh, North Carolin			na 27616		
Project #:	6235-16-	6235-16-010			Report Date: 11/7/		1/7/16
Project Name:	ect Name: C.F. Harvey Parkway Extension R-570		R-5703		Test Date(s):	11/5	- 11/7/16
Client Name:	Michael E	Baker Engineering					
Client Address	: Raleigh, N	NC					
Boring #: E	EB2-B RT LN	Sample	e #: SS-7		Sample D	ate:	N/A
Location: 8	89+45	Offs	set: 33 RT		Depth	(ft):	1.0 - 2.5
Sample Descrip	ption: (	Gray Coarse to Fine Sar	ndy Clayey	SILT (A-4) (1)	)		
Equipment:							
Balance		S&ME ID#	1024	Cal. Date:	11/6/16	Due:	11/6/17
Sieve:	#10	S&ME ID#	13223	Cal. Date:	6/11/16	Due:	6/11/17
pH Meter:		S&ME ID#	1365	Cal. Date:	11/7/16	Due:	NA

### pH Meter Calibration

Buffer Solution	Results
pH buffer 7.0	7.02
pH buffer 4.01	4.01
pH buffer 10.0	10.03
Buffer Temperature <sup>0</sup> C	22.4

### Measuring pH of Soil

Meas
9: Deterr
•

<u>Mal Krajan, ET</u> Technical Responsibility

N	t
	Signatu

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### pH of Soil



surements		
	30.00	
	30.01	
	22.2	
	5.69	

mining pH of Soil for Use in Corrosion Testing

Laboratory Manager

Position

<u>11/14/201</u>6

Date