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NOTE: SEE SHEET 2A FOR PLAN SHEET LAYOUT AT TIME OF INVESTIGATION

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79C

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STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

ROADWAY SUBSURFACE INVESTIGATION

PROJ. REFERENCE NO. 34839.1.1 (U-2579C) F.A. PROJ.

COUNTY FORSYTH

PROJECT DESCRIPTION WINSTON-SALEM NORTHERN BELTWAY

(EASTERN SECTION) FROM US 311 TO US 158 (FUTURE I-74)

INVENTORY

DIZELE	211111	~ 1 NO.	SHEET	
N.C.	U-2579C			98
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34	839.1.1	39.1.1		P.E.
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CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE NADE FOR THE PURPOSE OF STUDY, PLANNING, AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FILED BORING LOGS, ROCK CORES, AND SOL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, CEOTECHNICAL ENGINEERING UNIT AT 1919 250-4080. RHITHER THE SUBSURFACE PLANS AND REPORTS, NOR THE FIELD BORING LOGS, ROCK CORES, OR SOIL TEST DATA ARE PART OF THE CONTRACT.

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THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT MARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OFINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THIS PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS.

	C.C. MURRAY
	J.E. ESTEP
•	M.R. MOORE
INVESTIGATED I	BY R.Q. CALLAWAY
CHECKED BY	C.B. LITTLE
SUBMITTED BY	C.B. LITTLE
DATE	JUNE 2010
	•

PERSONNEL

DRAWN BY: J.K. McCLURE

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NOTE - BY HAVING REQUESTED THIS INFORMATION THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS
FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE
CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

PROJECT REFERENCE NO. 34839.1.1 (U-2579C) SHEET NO.

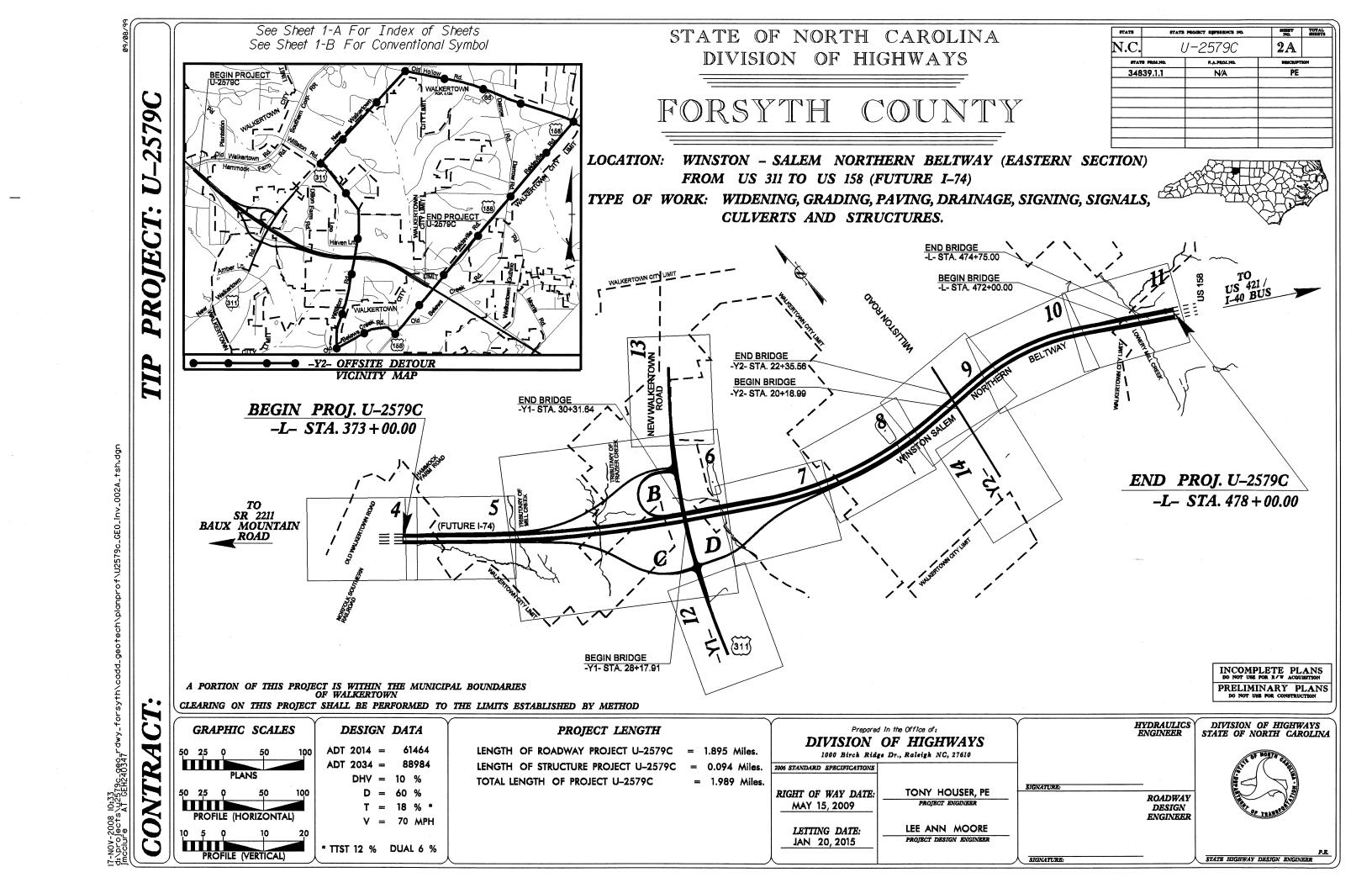
NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

	SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS						
SOIL DESCRIPTION	GRADATION	ROCK DESCRIPTION	TERMS AND DEFINITIONS				
SOIL IS CONSIDERED TO BE THE UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS	WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORM - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. (ALSO	HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT IF TESTED, WOULD YIELD SPT REFUSAL. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL.	ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.				
THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER, AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO STANDARD PENETRATION TEST (AASHTO T206, ASTM D-1586). SOIL	PODRLY GRADED) <u>GAP-GRADED</u> - INDICATES A MIXTURE OF UNIFORM PARTICLES OF TWO OR MORE SIZES.	SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EDUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE	ACCUFER - A WATER BEARING FORMATION OR STRATA.				
CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY SHALL INCLUDE: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH	ANGULARITY OF GRAINS	OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:	ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND, ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS,				
AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. EXAMPLE:	THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBROUNDED, OR ROUNDED.	WEATHERED WISH NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100	OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, AS SHALE, SLATE, ETC.				
VERY STAFF, GRAY, SULY CLAY, WORST WITH WITERBEDDED FINE SAND LAYERS, MISHLY PLASTIC, A-7-6	MINERALOGICAL COMPOSITION	ROCK (WR) BLOWS PER FOOT IF TESTED.	ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL				
SOIL LEGEND AND AASHTO CLASSIFICATION GENERAL GRANULAR MATERIALS SILT-CLAY MATERIALS OPERANC MATERIALS	MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS	CRYSTALLINE POCK (CP) FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED, ROCK TYPE INCLUDES GRANITE,	AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.				
CLASS. (≤ 35% PASSING #200) (> 35% PASSING #200) ORGANIC MATERIALS	WHENEVER THEY ARE CONSIDERED OF SIGNIFICANCE.	GNEISS, GABBRO, SCHIST, ETC.	CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.				
GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5	COMPRESSIBILITY	NON-CRYSTALLINE FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YELLD SPT REFUSAL IF TESTED, ROCK TYPE	COLLUYIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.				
ULASS. A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7	SLIGHTLY COMPRESSIBLE LIQUID LIMIT LESS THAN 31 MODERATELY COMPRESSIBLE LIQUID LIMIT EQUAL TO 31-50	COASTAL PLAIN COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD	CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL				
SYMBOL BOOK BOOK BOOK BOOK BOOK BOOK BOOK B	HIGHLY COMPRESSIBLE LIQUID LIMIT GREATER THAN 50	SEDIMENTARY ROCK SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.	LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.				
% PASSING SILT- MUCK, GRANULAR SILT- MUCK,	PERCENTAGE OF MATERIAL ODCANG MATERIAL GRANULAR SILT - CLAY	WEATHERING	DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.				
# 40 30 MX 50 MX 51 MN SOILS COLLS PEAT	ORGANIC MATERIAL SOILS SOILS DIHER MATERIAL	FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING, ROCK RINGS UNDER	DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE				
- 200 15 MX 25 MX 10 MX 35 MX 35 MX 35 MX 36 MN 36 MN 36 MN 36 MN 36 MN	TRACE OF ORGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10%	HAMMER IF CRYSTALLINE.	HORIZONTAL.				
LIGUID LIMIT	MODERATELY ORGANIC	VERY SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN, (V SLI.) CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF	DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP. MEASURED CLOCKWISE FROM NORTH.				
GROUP INDEX 0 0 0 4 MX 8 MX 12 MX 16 MX No MX MODERATE ORGANIC	GROUND WATER	OF A CRYSTALLINE NATURE.	FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE				
USHAL TYPES STONE FRACE SOILS	WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING	SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO (SLI.) 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR	SIDES RELATIVE TO DNE ANOTHER PARALLEL TO THE FRACTURE.				
OF MAJOR GRAVEL AND SAND GRAVEL AND SAND GRAVEL AND SAND SOILS SOILS MATTER	STATIC WATER LEVEL AFTER 24 HOURS	CRYSTALS ARE DULL AND DISCOLORED, CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.	FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.				
GEN. RATING		MODERATE SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS	FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.				
AS A EXCELLENT TO GOOD FAIR TO POOR POOR POOR UNSUITABLE SUBGRADE	E	DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED	FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY				
PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30	SPRING OR SEEP	WITH FRESH ROCK. MODERATELY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL	THE STREAM.				
CONSISTENCY OR DENSENESS	MISCELLANEOUS SYMBOLS	SEVERE AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH	FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.				
PRIMARY SOIL TYPE COMPACTNESS OR CONSISTENCY PENETRATION RESISTENCE COMPRESSIVE STRENGTH	ROADWAY EMBANKMENT (RE) POPT DATE TEST BORING W/ CORE TEST BORING W/ CORE	(MOD. SEV.) AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES 'CLUNK' SOUND WHEN STRUCK. IF TESTED, WOULD YIELD SPT REFUSAL	JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.				
(N-VALUE) (TORSY-T-)	1 W 2711 SOL 225514 No.	SEVERE ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED, ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED	LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO				
GENERALLY VERY LOOSE 4 LOOSE 4 TO 10	SOIL SYMBOL AUGER BORING SPT N-VALUE	(SEV.) IN STRENGTH TO STRONG SDIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN.	ITS LATERAL EXTENT.				
MATERIAL MEDIUM DENSE 10 TO 30 N/A	ARTIFICIAL FILL (AF) OTHER - CORE BORING REF SPT REFUSAL	IF TESTED, YIELDS SPT N VALUES > 100 BPF	LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTTLING IN				
(NON-COHESIVE) VERY DENSE >50	THAN ROADWAY EMBANKMENT INFERRED SOU ROUNDARY MONITORING WELL	VERY SEVERE ALL ROCK EXCEPT DUARTZ DISCOLORED OR STAINED, ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT (V SEV.) THE MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH DNLY FRAGMENTS OF STRONG ROCK	SDILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.				
VERY SOFT <2 <0.25	THE ENGLE SOIL BOOKBANT	REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE SUCH THAT ONLY MINOR VESTIGES OF THE ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, YIELDS SPT N VALUES < 100 BPF</i>	PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.				
GENERALLY SOFT 2 TO 4 0.25 TO 0.50 SILT-CLAY MEDIUM STIFF 4 TO 8 0.5 TO 1.0	INFERRED ROCK LINE A PIEZOMETER INSTALLATION	COMPLETE ROCK REDUCED TO SOIL, ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND	RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.				
MATERIAL STIFF 8 TO 15 1 TO 2	SLOPE INDICATOR	SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS	ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF				
(COHESIVE) VERY STIFF 15 TO 30 2 TO 4 HARD >30 >4	25/825 DIP & DIP DIRECTION OF	ALSO AN EXAMPLE.	ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.				
TEXTURE OR GRAIN SIZE	ROCK STRUCTURES CONE PENETROMETER TEST	ROCK HARDNESS	SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE				
U.S. STD. SIEVE SIZE 4 10 40 60 200 270	SOUNDING ROD	VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK, BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK,	PARENT ROCK.				
OPENING (MM) 4.76 2.00 0.42 0.25 0.075 0.053	ABBREVIATIONS	HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED	SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL				
BOULDER COBBLE GRAVEL COARSE FINE SILT CLAY	AR - AUGER REFUSAL MED MEDIUM VST - VANE SHEAR TEST	TO DETACH HAND SPECIMEN.	TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.				
(BLDR.) (CDB.) (GR.) (CSE. SD.) (F SD.) (SL.) (CL.)	BT - BORING TERMINATED MICA MICACEOUS WEA WEATHERED CL CLAY MOD MODERATELY 2 - UNIT WEIGHT	MODERATELY CAN BE SCRATCHED BY KNIFE OR PICK, GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE HARD EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK, HAND SPECIMENS CAN BE DETACHED	SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.				
GRAIN MM 305 75 2.0 0.25 0.05 0.005 SIZE IN. 12 3	CPT - CONE PENETRATION TEST NP - NON PLASTIC $\gamma_{ m d}$ - DRY UNIT WEIGHT	BY MODERATE BLOWS. MEDIUM CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT.	STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) DF				
SOIL MOISTURE - CORRELATION OF TERMS	CSE CDARSE ORG ORGANIC DMT - DILATOMETER TEST PMT - PRESSUREMETER TEST SAMPLE ABBREVIATIONS	HARD CAN BE EXCAVATED IN SMALL CHIPS TO PEICES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE	A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER, SPT REFUSAL IS PENETRATION EQUAL TO OR LESS				
SOIL MOISTURE SCALE FIELD MOISTURE CHIDE FOR FIELD MOISTURE DESCRIPTION	DPT - DYNAMIC PENETRATION TEST SAP SAPROLITIC S - BULK	POINT OF A GEOLOGIST'S PICK. SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS	THAN 0.1 FOOT PER 60 BLOWS.				
(ATTERBERG LIMITS) DESCRIPTION GOIDE FOR FIELD MOISTONE DESCRIPTION	F - FINE SL SILT, SILTY ST - SHELBY TUBE	FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT, SMALL, THIN	STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.				
- SATURATED - USUALLY LIQUID; VERY WET, USUALLY	FOSS FOSSILIFEROUS SLI SLIGHTLY RS - ROCK FRAC FRACTURED, FRACTURES TCR - TRICONE REFUSAL RT - RECOMPACTED TRIAXIAL	PIECES CAN BE BROKEN BY FINGER PRESSURE. VERY CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH	STRATA ROCK QUALITY DESIGNATION (SRQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY				
(SAT.) FROM BELOW THE GROUND WATER TABLE	FRAGS FRAGMENTS # - MOISTURE CONTENT CBR - CALIFORNIA BEARING	SOFT OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY	TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.				
PLASTIC SEMISOLIDE REQUIRES DRYING TO	HI HIGHLY V - VERY RATIO	FINGERNAIL. FRACTURE SPACING BEDDING	TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.				
(PI) PLASTIC LIMITATTAIN OPTIMUM MOISTURE	EQUIPMENT USED ON SUBJECT PROJECT	TEDM THICKNESS	DENOM MADY				
COLVE AT OR DEAD COTTABLE MODERNIA	DRILL UNITS: ADVANCING TOOLS: HAMMER TYPE: X AUTOMATIC MANUAL	VERY WIDE MORE THAN 10 FEET VERY THICKLY BEDDED > 4 FEET	BENCH MARK:				
OM OPTIMUM MOISTURE - MOIST - (M) SOLID; AT OR NEAR OPTIMUM MOISTURE SL SHRINKAGE LIMIT	MOBILE B-	MIDE 3 TO 10 FEET THINLY BEDDED 0.16 - 1.5 FEET	ELEVATION: FT.				
REQUIRES ADDITIONAL WATER TO	X 6° CONTINUOUS FLIGHT AUGER CORE SIZE:	CLOSE 0.16 TO 1 FEET VERY THINLY BEDDED 0.03 - 0.15 FEET	NOTES:				
- DRY - (D) ATTAIN OPTIMUM MOISTURE	BK-51 X 8' HOLLOW AUGERS	VERY CLUSE LESS THAN 0.16 FEET THINLY LAMINATED < 0.008 FEET	SoilStrata Shown Thru Borings.				
PLASTICITY	CME-45C HARD FACED FINGER BITS -N	INDURATION					
PLASTICITY INDEX (PJ) DRY STRENGTH	X TUNG-CARRIDE INSERTS	FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF THE MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.					
NONPLASTIC 0-5 VERY LOW LOW PLASTICITY 6-15 SLIGHT	X CME-550	FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS: GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.					
MED. PLASTICITY 16-25 MEDIUM	PORTABLE HOIST TRICONE STEEL TEETH POST HOLE DIGGER	MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE;					
25 37 1312	TRICONE TUNG,-CARB, X HAND AUGER	BREAKS EASILY WHEN HIT WITH HAMMER.	·				
COLOR	CORE BIT SOUNDING ROD	INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.					
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.	VANE SHEAR TEST						
TIODALIZETO SUCIT NO EZOTTI, DITIKA, STINENCEO, ETC. MAE USED TO DESCRIBE METERNANCE.		EXTREMELY INDURATED SHARP HAMMER BLOWS REDUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.					





STATE OF NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

BEVERLY EAVES PERDUE
GOVERNOR

EUGENE A. CONTI, JR. SECRETARY

STATE PROJECT:

34839.1.1 (U-2579C)

FEDERAL PROJECT:

N.A.

COUNTY:

FORSYTH

DESCRIPTION:

WINSTON SALEM NORTHERN BELTWAY (EASTERN SECTION)

(FUTURE I-74) FROM US 311 TO US 158

SUBJECT:

GEOTECHNICAL REPORT – Inventory

PROJECT DESCRIPTION

The U-2579C project is to the northwest of the U-2579B project and connects with it. The aggregate of the U-2579 projects are part of future I-74, and also the eastern half, more or less, of a future Winston–Salem beltway. Predictably enough, the northwest end of "C" will connect to the southeast end of U-2579D and so on, to the end at "F".

From the beginning at station –L- 373+00 to –L- 401+00, the –L- line will be on embankment fill up to 70' thick. This grade is required by a railroad crossing in the following segment: U-2579D. A small amount of alluvial soil was found adjacent to streams, but most of the soil is residual, produced by weathering rock. Where deeper drilling was done the residual soil is up to 50' thick. A succession of soil types from fine to coarse is encountered from the surface to rock. A-7 and A-6 soil is found at the undisturbed surface, followed by A-5 or A-4 then A-2 above rock. Even with the development of the clayey or silty soils in the section, tests of the soil plasticity index (PI) returned values of less than 20. According to the geologic map, biotite gneiss is the rock that disintegrated to form the soil in the project area. The mica that is a constituent of this rock is highly resistant to weathering, contributes to low soil plasticity, and doesn't pack very well.

The field investigation was conducted from July 1, 2008 to August 15, 2008, using a CME-550 drill machine with an automatic hammer. Standard Penetration Tests, (SPT), were performed through hollow stem augers at selected locations. Additional borings were conducted with solid augers for delineation of the limits of rock. Representative soil samples were collected and forwarded to the Materials and Tests Unit laboratory for soil quality analysis, moisture content and ASSHTO classification. All available drill-holes are plotted on the plan view and also appear projected into the profiles.

The following alignments, totaling 5.06 miles, were investigated.

Alignment	Station	to	Station	Length Feet
-L-	369+00.00		478+00	10,900
-Y1-	11+00.00		48+50	4,750
-Y1RPB-	10+00.00		32+88.63	2,288.63
-Y1RPC-	10+00.00		32+95.71	2,295.71
-Y1RPD-	10+00.00		32+31.74	2,231.74
-Y1LPB-	10+00.00		22+19.35	1,219.35
-Y2-	10+00.00		26+50	1,650
-Y1DET-	17+29.79		31+62.46	1,432.67

5.06 miles, or 26,768 feet.

3A

ITEMS OF SPECIAL GEOTECHNICAL INTEREST

1.) Groundwater:

The 24 hr water level was found at or above planned grade in some borings for -L-, -Y1RPB- and -Y1LPB-. The locations are posted on a table in the Physiography and Geology section below.

2.) All-weather spring fed seeps or streams:

There are several streams, seeps and water crossings within the boundaries of this project. The locations are posted on a table in the Physiography and Geology section below.

3.) Wet soil.

Wet soil is adjacent to streams.

4.) Rock within 10' of grade, or above grade.

Rock was found within 10' below grade, or above grade on the project. The locations are posted on a table in the Physiography and Geology section below.

5.) High liquid limit, (LL) low Plasticity Index, (PI), soil.

The high LL, low PI soil test results of this project and the micaceous nature of the rock indicate much of the soil will be low strength and light weight.

6.) Wetlands posted on roadway plans.

The wetlands posted on the roadway plans are not within the National Wetland Inventory. It is possible that they are from a study to identify areas amenable to future wetland mitigation or creation.

7.) Artificial Fill

At –L- 437+50 a section of artificial fill is shown with the water table at the fill/residual soil interface. This location is a topographic low, possibly a wet weather run. There is 30 feet of embankment fill to be placed over 15' of artificial fill soil containing trash, with water at the base.

PHYSIOGRAPHY AND GEOLOGY

Physiography

The project is in the Piedmont Physiographic Province, between the Coastal Plain and the Blue Ridge Provinces. The Piedmont physiographic province is characterized as a peneplane that was eroded flat,

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then uplifted and is now being incised by the reenergized streams. The ridge tops are the remnants of the original planar surface that was continuous across the piedmont. In the eroding terrain of the piedmont, rock is more likely to be near land surface in the valleys than on the ridge tops.

The expectation is that the ridges and valleys would have a northeast – southwest trend, reflecting the "grain" of the underlying metamorphic rock. On the scale of this project, the gross topographic features have a north 20 east alignment rather than the north 45 to 55 east that would be expected. This may be an area of local structural grain. The –L- alignment crosses most of the little valleys at a 90 degree angle.

Geology

Throughout North Carolina the geologic provinces run northeast – southwest and are divided on the basis of metamorphic grade or dominant rock type. According to the 1985 Geologic Map of North America, this project is entirely within the Milton Belt. The Winston-Salem Geologic quadrangle map does not delineate the Milton Belt, and places Winston Salem within the Charlotte Belt. In either case it is mapped as micaceous schist and gneiss. The Sauratown Mountains Anticlinorium is the geologic belt to the northwest, and the granitic rock of the Charlotte belt is to the southeast.

Soil Properties

The first subdivision in the classification of soil is naming it as residual, embankment fill, or alluvial soil. After that the AASHTO classification is partly based on grain size, but is also an attempt to predict the soil behavior as a construction material.

Residual soil is a product of in-place chemical destruction of the original rock. Chemical weathering reduces rock strength making it more susceptible to physical erosion, transport, and removal by natural processes. The present residual soil thickness is influenced by the interaction between chemical weathering processes and physical weathering processes on the various rock types. For example, the preliminary boring for the U.S.311 bridge at -Y1-30+31 elevation 960', (-L- 409), found 40' of residual soil and ended in residual soil. The borings at -L- 406+25, elevation 970', found rock at a depth of 35'. The dominant soil type encountered on the project was low plasticity A-2 micaceous sandy soil, the expected soil derived from weathering the gneiss and schist of this geologic province. Eventually, chemical weathering processes produce the red A-7 cap clay that appears most frequently on the ridge tops.

Alluvial Soil: Soil grains that have been transported by a natural process, water or wind and deposited away from their original location forms alluvial soil. This process of transport and deposition leaves visible layering in the soil defined by a physical characteristic such as color, grain size, density, or sorting. Alluvial soil was found in this project only associated with floodplain areas. Generally it was sand, tending toward A-1 to A-2-4, the clays staying in suspension and being transported downstream, while the sand dropped out.

Roadway Embankment, Construction may require addition of soil to bring the natural ground surface to the desired elevation. When soil is transported to a new site and compacted it is fill soil. If it is handled under the standards or aegis of the NCDOT, it becomes Roadway Embankment. If some other entity is responsible for the fill placement or the conditions are unknown, the fill is classed as Artificial Fill.

Artificial fill was identified on this project, from -L- 434+57 to -L- 438+00. The profile shows this fill to be on one side of an existing drainage with a steep slope at the base.

Rock Properties

This investigation is concerned with the depth to rock and the areal extent of rock at or above grade. Rock samples were not collected or analyzed in this investigation. Rock in this region is strongly foliated micaceous schist and gneiss.

All cross sections that contain a boring terminated on rock above grade, are included as part of this report. The depth to rock indicated by auger refusal is variable in cross section and profile. Rock was found less than 10' below grade, or above grade in the following locations, extracted from an examination of the profile.

Rock at or near grade

Alignment	Station	to	Station	note
-L-	416+50		416+50	Single point
-L-	453+00		459+50	centerline

Groundwater Properties

Water was found less than 10' below grade, or above grade in the following locations

Alignment	Station	to	Station	Location
-L-	404+00		411+00	
-L-	415+50		417+00	Single point
-L-	420+50		425+50	
-L-	446+00		498+00	Above Grade
-Y1RPB-	30+50		31+50	Below Grade
-Y1LPB-	10+50		12+00	Below Grade

All-weather spring fed seeps or streams:

The stations in the table below record the location of springs seeps or streams, some which may not have year round flow.

Line	Station		Size of stream: eg: 1 st order ¹ .
-L-	374+40	384+00	Wetland ² on right side.
-L-	387+50	388+50	1 st order stream, crosses left to right.
-L-	397+75	398+50	2 nd order stream, continues to Y1RPD & Y1RPB
-L-	414+25	414+50	1 st order, continues to -Y1-31+50
-L-	427+00	428+25	Wetland, (footnote 2)

¹ A stream without tributaries is first order. Two first order streams converge to make a second order stream. A third order stream requires two second order streams as tributaries.

² Wetland per Roadway Plan

-L-	438+00	438+25	1 st order stream, crosses left to right
-L-	473+25	473+75	2 nd or 3 rd order stream, Lower Mill Creek
-Y1RMPB-	20+75	21+25	2 nd order stream
-Y1RMPD-	19+75	20+25	2 nd order stream
-Y1RMPD-	27+25	27+75	2 nd order stream plus wetland, (footnote 2)

GEOTECHNICAL DESCRIPTIVE ANALYSIS

Because this project is neither very large nor very complex, it is not broken up and is described here as 1 "segment".

Physical Description

This segment is 10,900' long, all new alignment, beginning at a grade separation over Norfolk Southern Railroad. Access will be provided to New Walkertown Road, (Y1), by an interchange with 3 ramps and a loop.

The Norfolk Southern grade separation requires that the initial 2850' of the –L- alignment be on embankment, much of it up to 80' thick. The 3000' following is built mostly on cut, then 1300' on embankment up to 50' thick, then 2600' on cut, mostly 40' thick, and then an 800' stream valley crossing mostly on fill up to 40' thick. This section ends at 478+50. Rock is encountered in some of the cut sections, as noted in the table below. There are several stream crossings.

-L-

This segment is mapped in plan on sheets 4 through 11, and profile sheets 15 through 21. Cross sections were printed for areas of shallow rock. The –L- alignment begins at station –L-373+00 elevation 1042, and then at station 375+00, it begins a descent to elevation 932 at station –L-415+00. From there, the road climbs back to elevation 948 at station 434+50, then drops to elevation 882' at station 478+00, and the end of this project.

Cuts and Fills

Alignment	Station	to	Station	Note
-L-	373+00		401+50	Fill, maximum 80' thick
-L-	400+50		413+00	Cut, 25 to 30' thick
-L-	413+00		415+50	Fill, one valley, 20' deep
-L-	415+50		427+50	Cut, 20' – 25' two hill tops
-L-	427+50		429+50	Fill, one valley with pond.
-L-	429+50		431+00	Cut, nearly at grade, one hilltop.
-L-	431+00		444+00	Fill, one valley up to 50' deep ³
-L-	444+00		470+00	Cut, 20' to 40'
-L-	470+00		478+00	Bridge approaches and Bridge

Geology

This area is not only covered by the state geologic map, but was also included in the 1° x 2° Winston Salem quadrangle mapping. The mapping shows that the project is on Cambrian age

³ Embankment will be over artificial fill that has unknown subgrade drainage system.

30

metamorphic rocks of the Charlotte belt, northwest of a Pennsylvanian age granite body that intrudes the metamorphic rock.

Soil

Most of this project has residual soil at the surface, and most of the proposed excavation involves residual soil. It is most likely that that the planned embankments will be built from the planned cut areas.

The distribution of soil type for the 226 samples is as follows:

alignment	AASHTO class	Number / total	percent	
-L-	A-2-4	61	27%	Sand
-L-	A-2-5	21	9%	Silty Sand
-L-	A-2-6	2	1%	Silty Sand with Clay
-L-	A-4	39	17%	Silt
-L-	A-5	41	18%	Silt with high LL
-L-	A-6	9	2%	Clayey Silt
-L-	A-7-5	36	16%	Clay
-L-	A-7-6	14	6%	Clay

The samples with less than 36% silt-clay, and PI values less than 11, fall to the sand side, (A-2-4, A-2-5): 36% of total. (Coarser grained, low plasticity)

The clayey or silty sand, (A-2-6, A-2-7) classification specifies no more than 35% silt-clay, and PI greater than 10: Only 2 samples fell in this group. (coarser grained, high plasticity)

Silt soil, (A-4, A-5), specifies more than 35% silt-clay size grains, (-200), and PI values no greater than 10: 35% of total. (Fine grained, low plasticity)

Clay soil, (A-6, A-7), specifies more than 35% clay and PI values above 10: 24% (fine grained, high plasticity)

The total population of soil sample results is skewed toward low PI values, (71%). Only 8 of the 226 samples are Highly Plastic with PI values above PI=30. High liquid limit values are found in 49% of the samples with LL above 41.

No settlement issues are anticipated from the undisturbed residual soil beneath the embankments. The alluvial soil that was encountered adjacent to stream crossings was thin, less than 10' thick, and either loose wet sand or very stiff clay.

When soil with a high liquid limit is compacted, a variation in soil moisture of 1 or 2 percent will not have much effect on the compacted density, but the optimum density (and strength) of this kind of soil, will be relatively low. Historically though, it has been acceptable.

Rock

U-2579C Page - 3 - of 4 Within the cut section from -L- 444+00 to 470+00, from -L- 452+50 to 461+00, rock was found within 10' of grade. Only one boring found rock above grade.

Groundwater

Static water levels measured during drilling indicate that groundwater will be encountered in much of the cut sections, at or near the planned grade elevation, during construction of this segment.

Align	Station	Grd Elevation	SWT ⁴ Elevation	Note
-L-	406+24, 84 Lt	952	948	
-L-	409+01, 110 Lt	942	940	
-L-	416+50, 125 Lt	936	936	
-L-	422+00, CL	939	935	
-L-	425+09, 91 Rt	941	936	
-L-	426+00, CL	942	933	
-L-	447+30, 112 Rt	929	924	
-L-	451+50, 110Rt	920	916	Artesian rise
-L-	453+50 CL	916	920	Artesian rise
-L-	456+50 CL	910	916	Artesian rise
-L-	457+25	908	911	
-L-	459+50	906	908	
-L-	462+75	901	900	
-L-	466+00	895	NM ⁵	
-L-	469+00	891	NM	

All-Weather Spring-Fed Seeps or Streams:

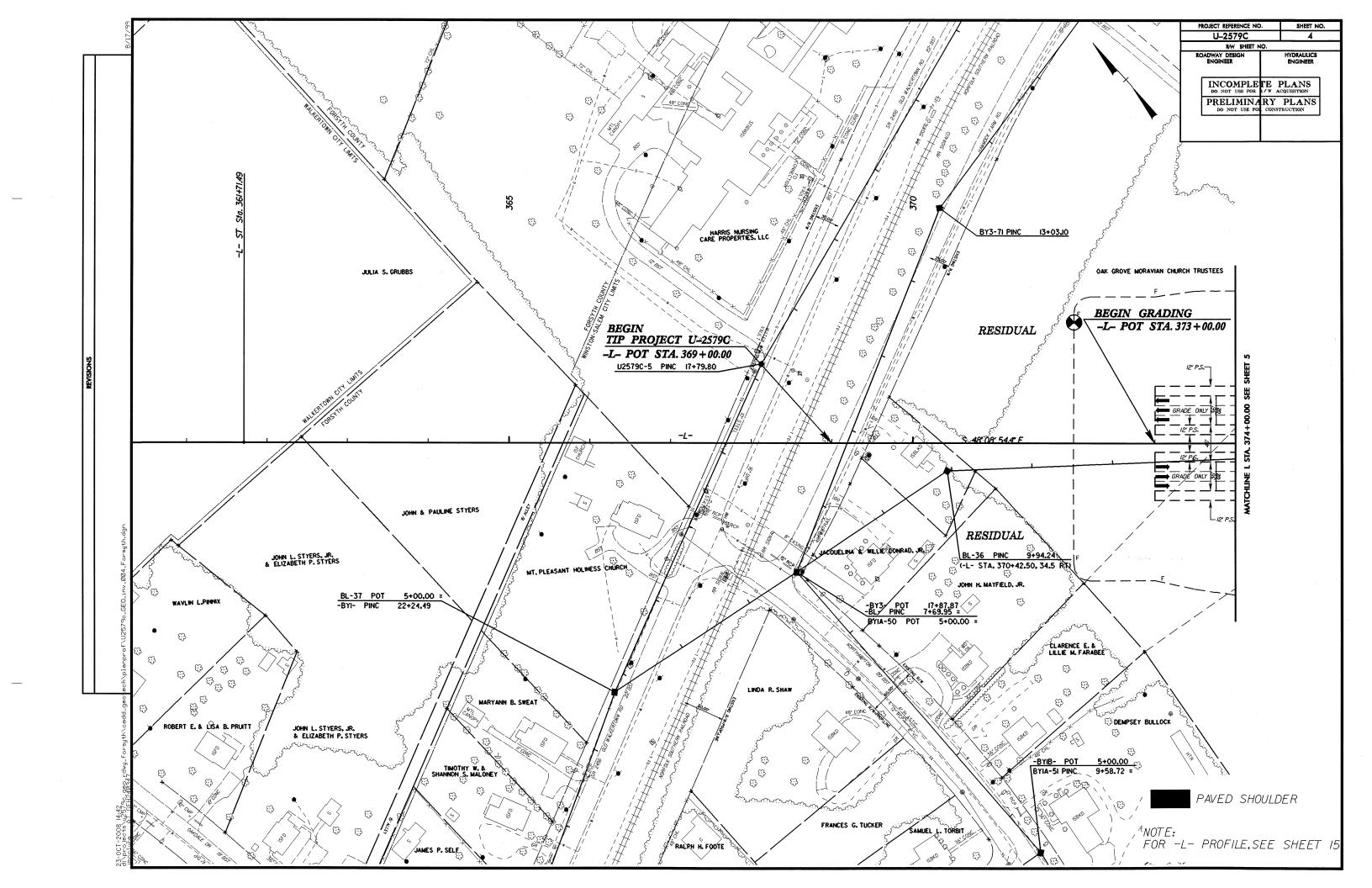
The locations of the water features are recorded in a table within the Physiography and Geology section above.

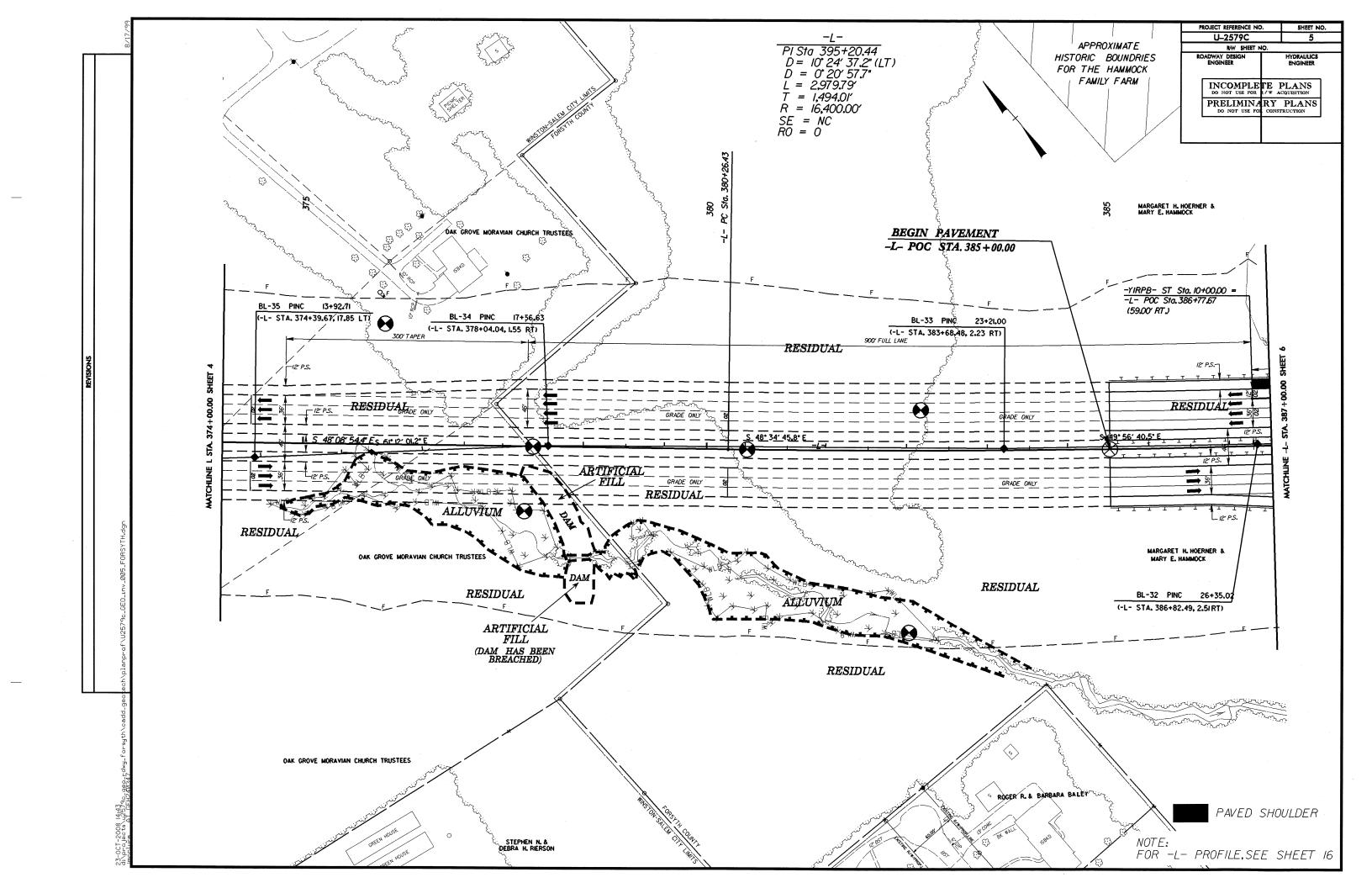


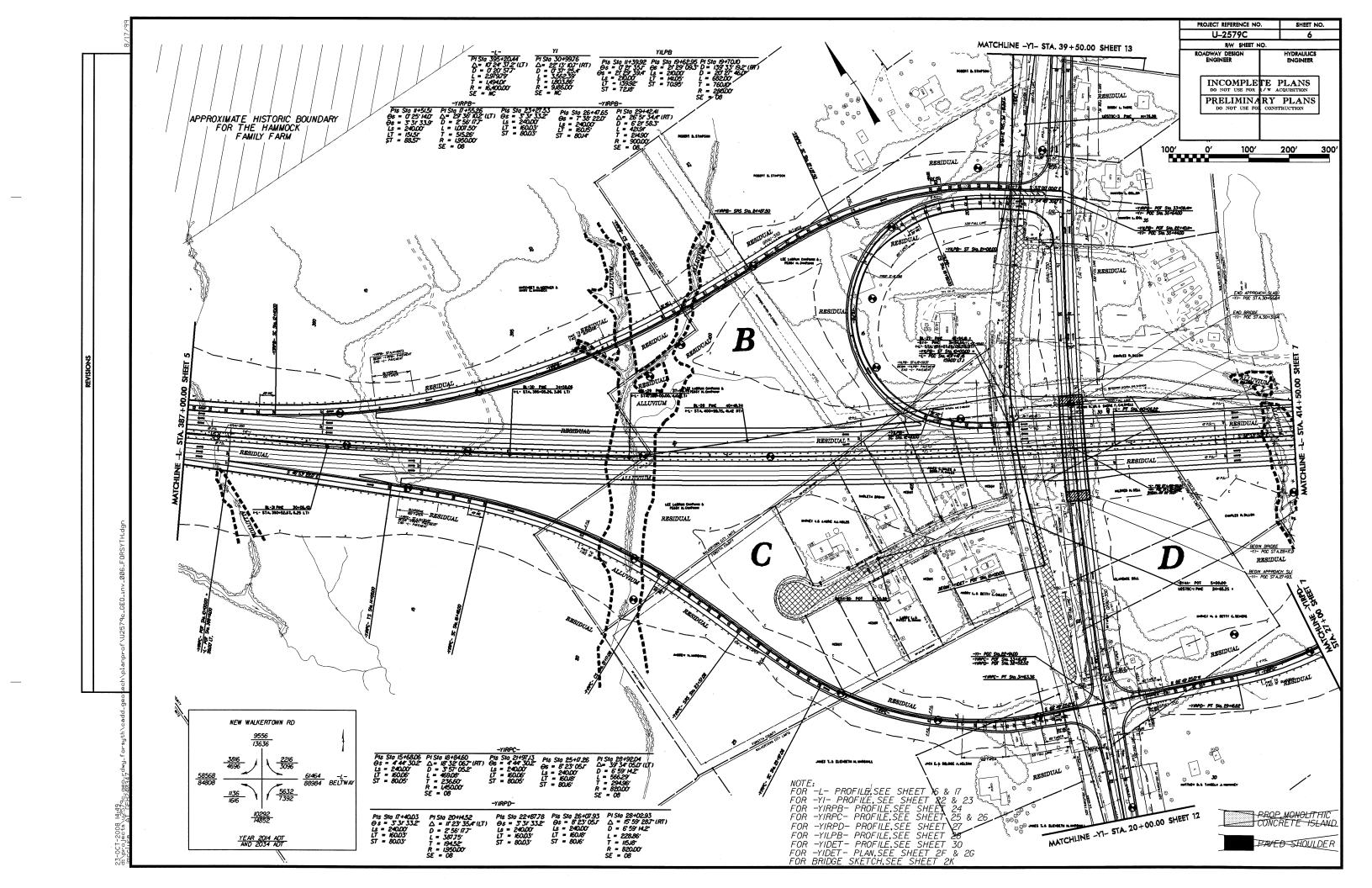
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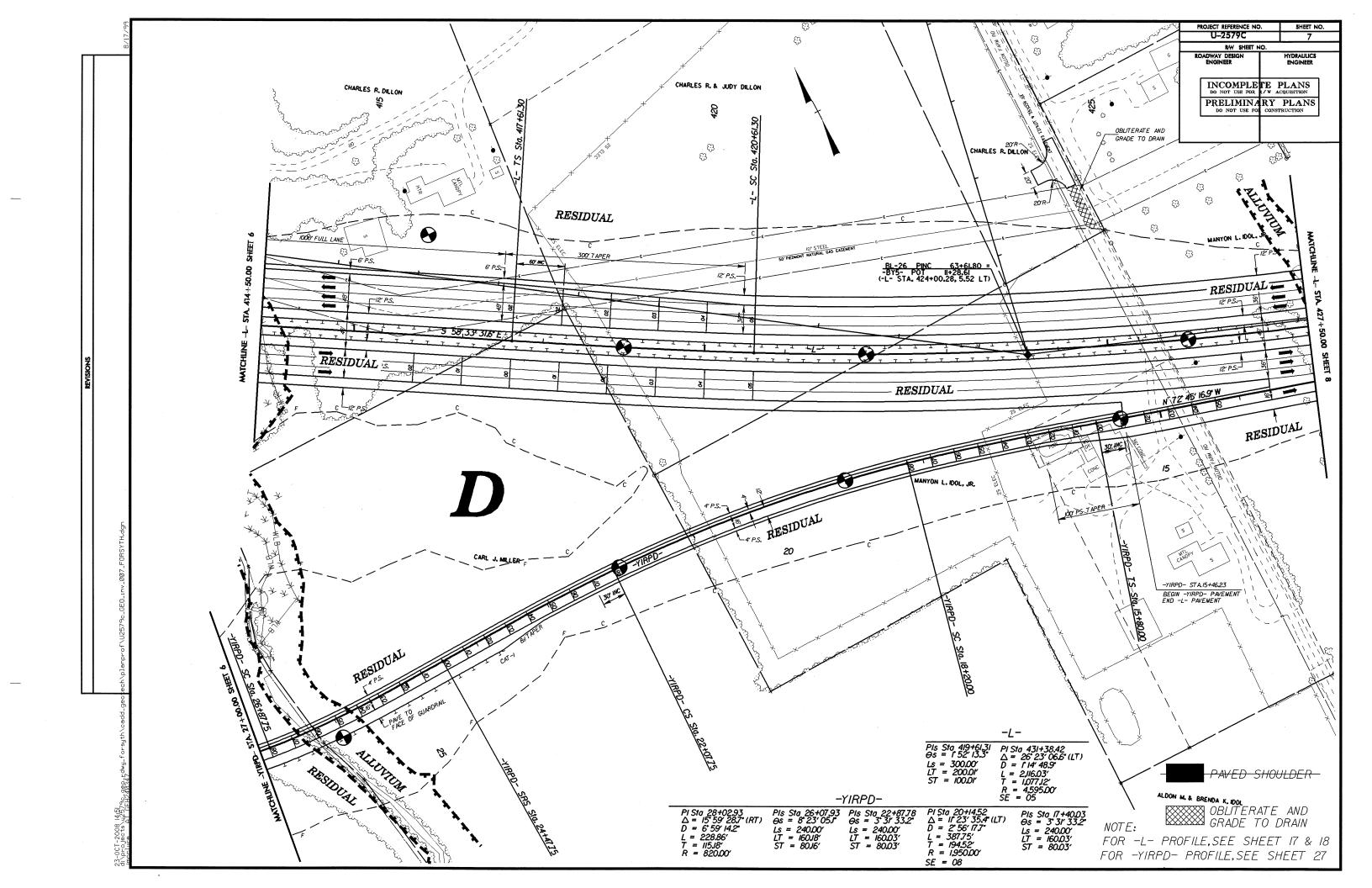
⁴ SWT: Static Water Table

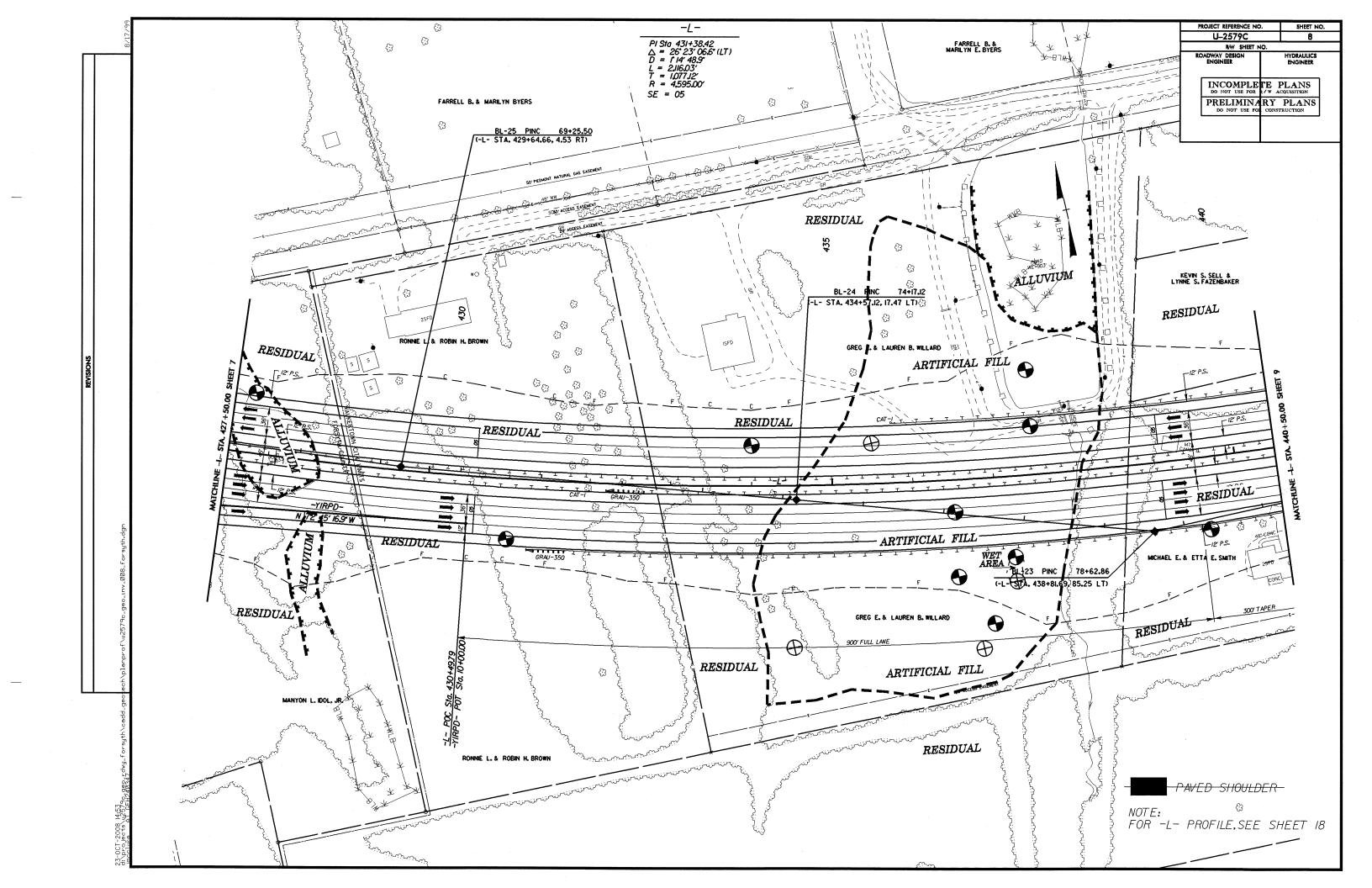
⁵ NM = not measured

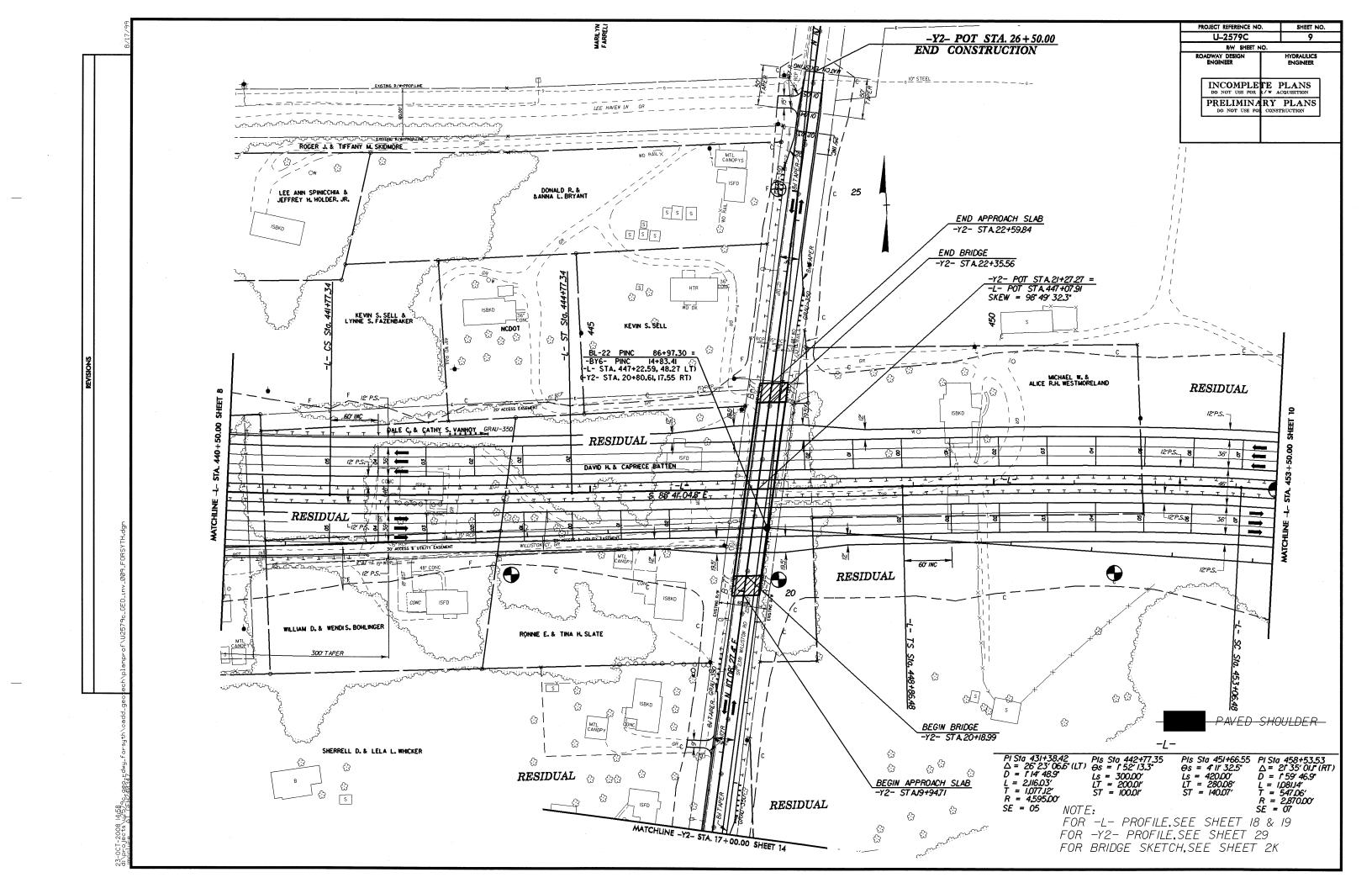


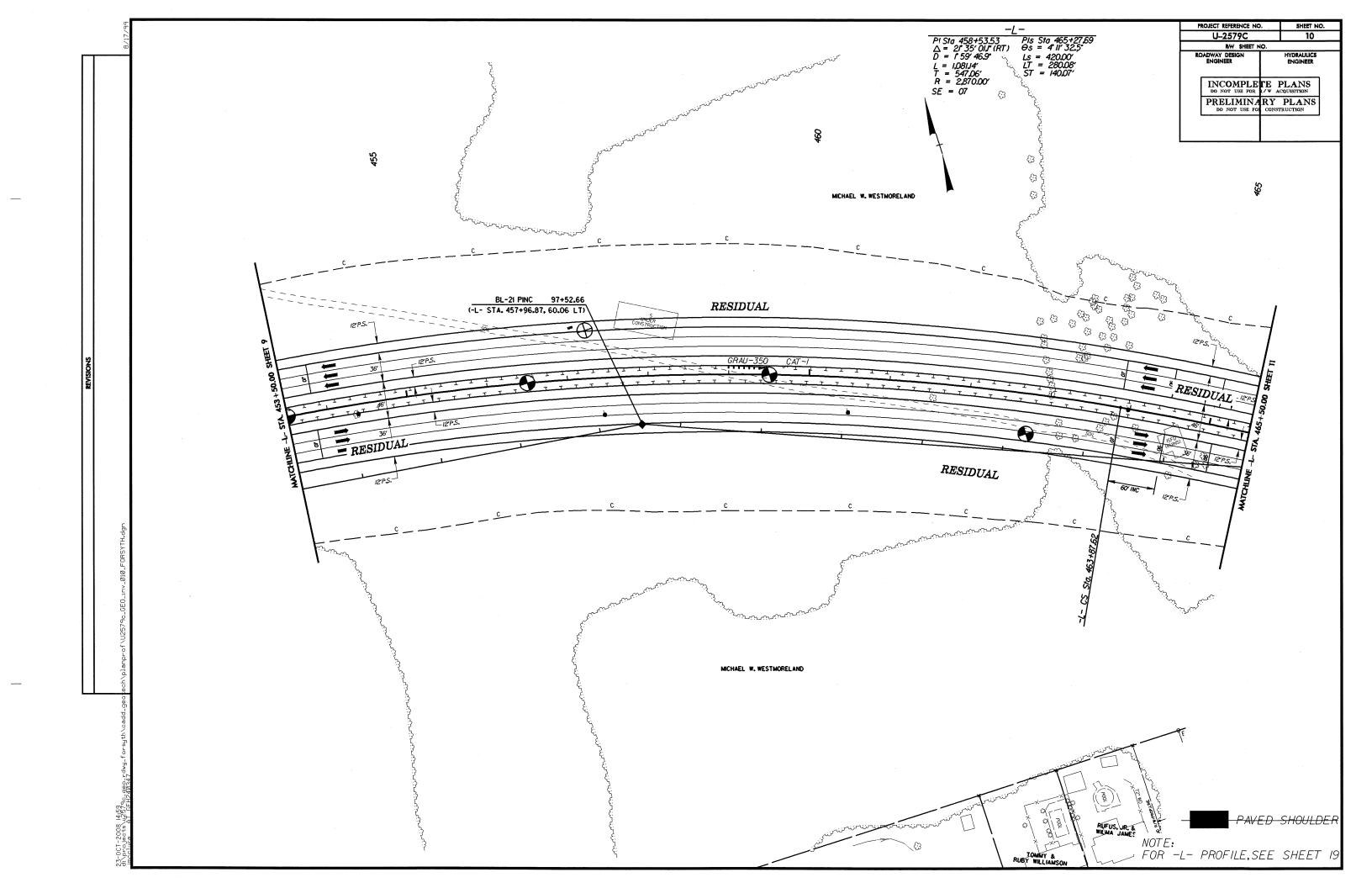


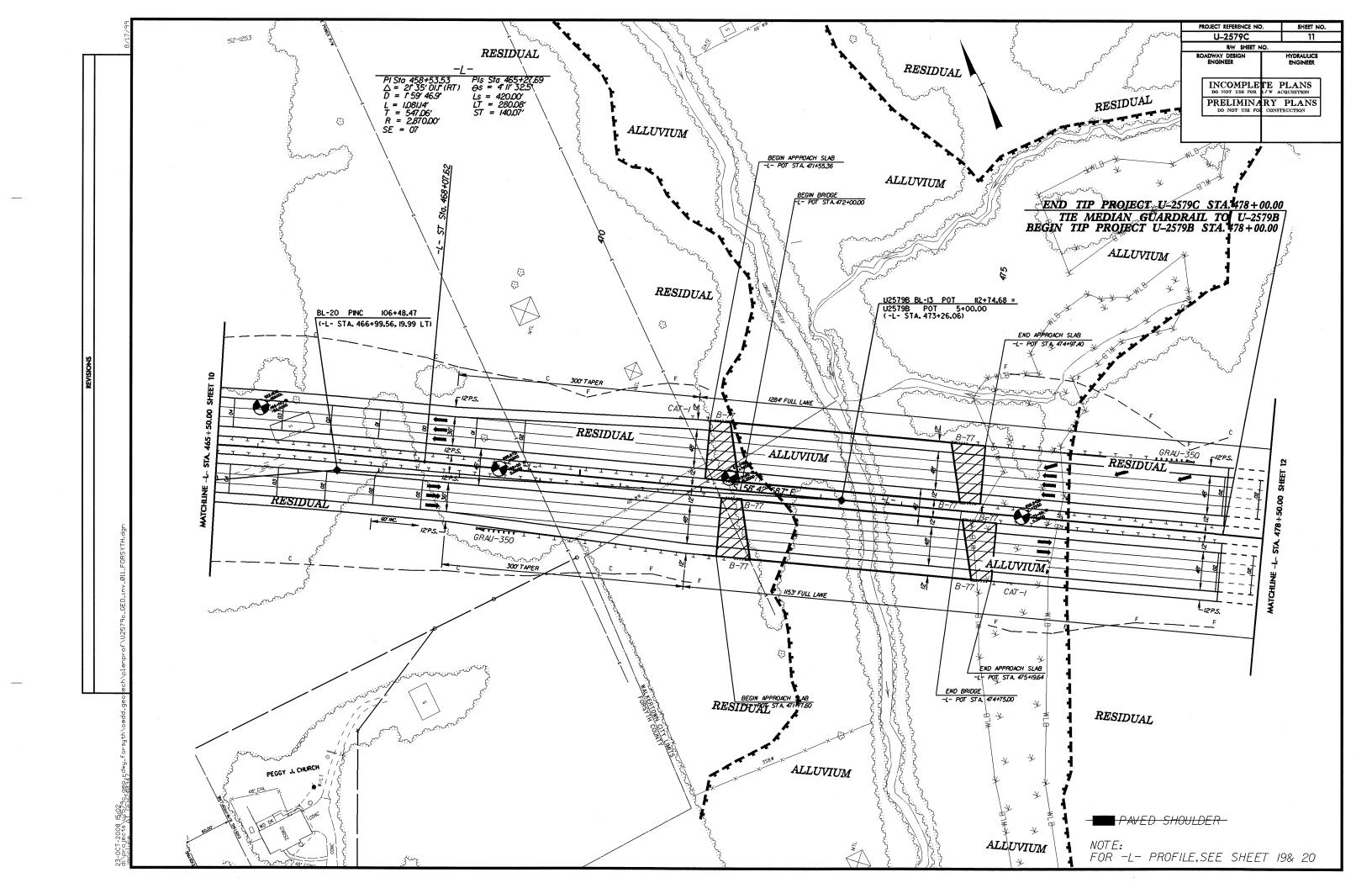


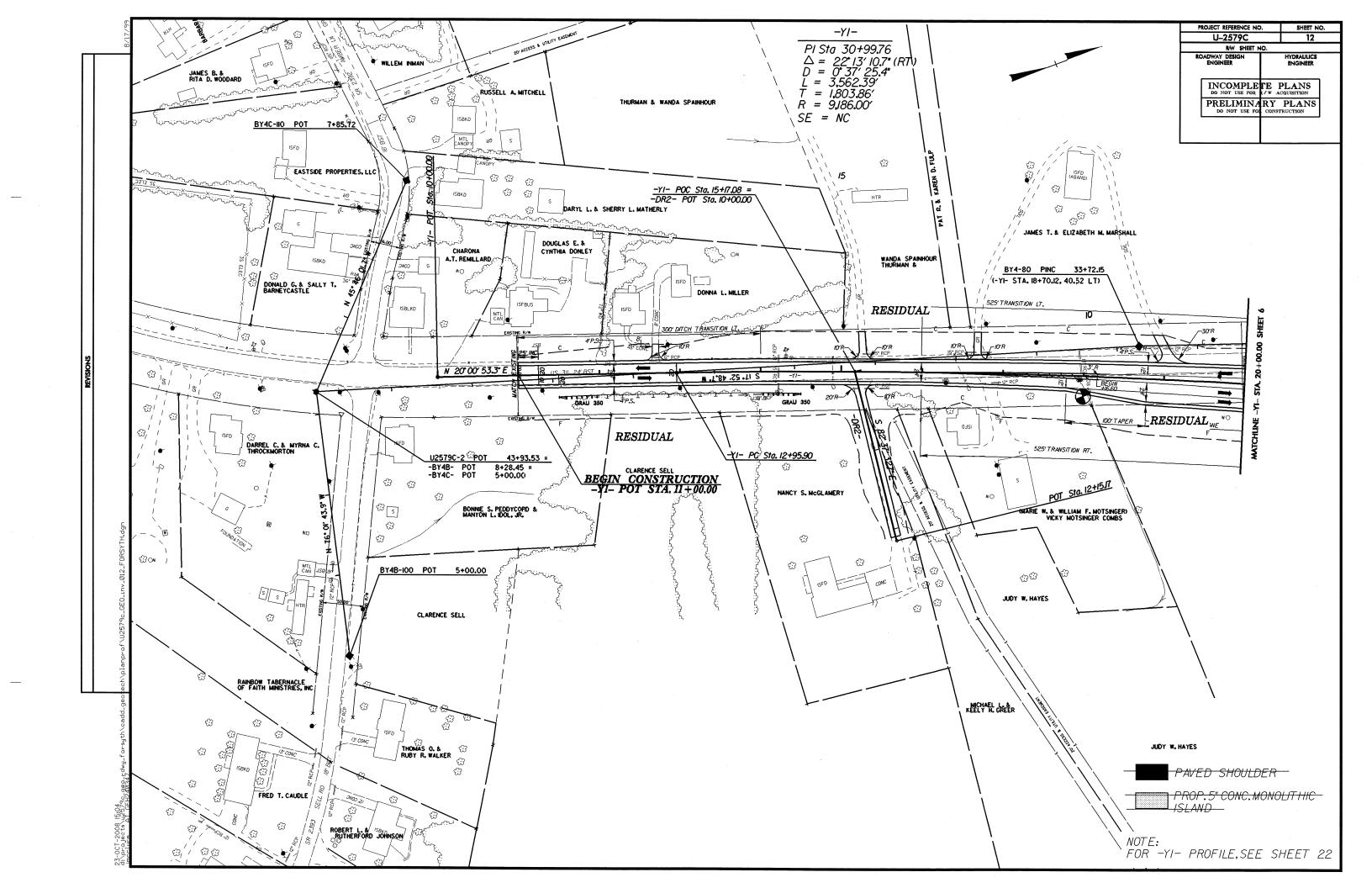


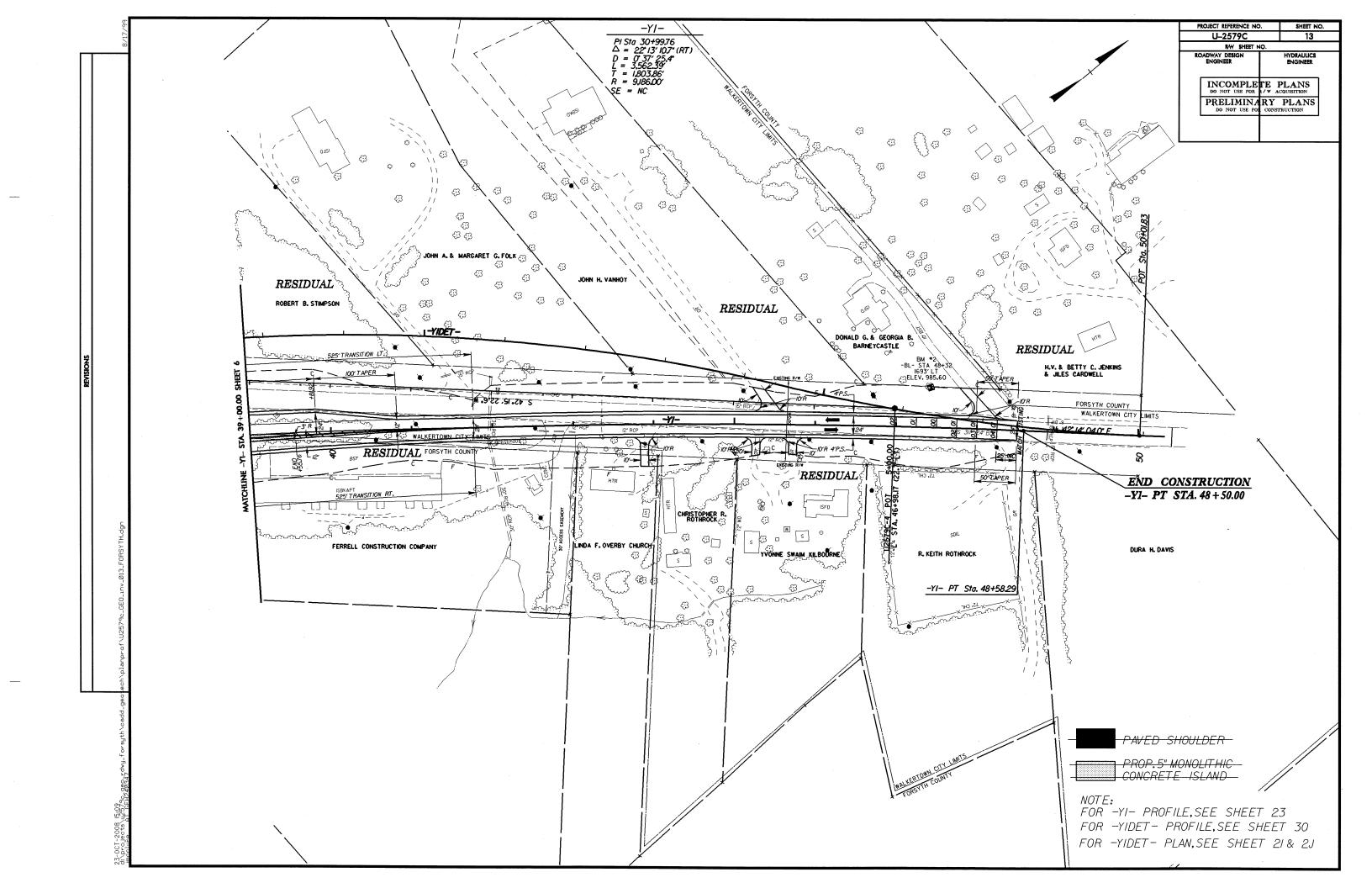


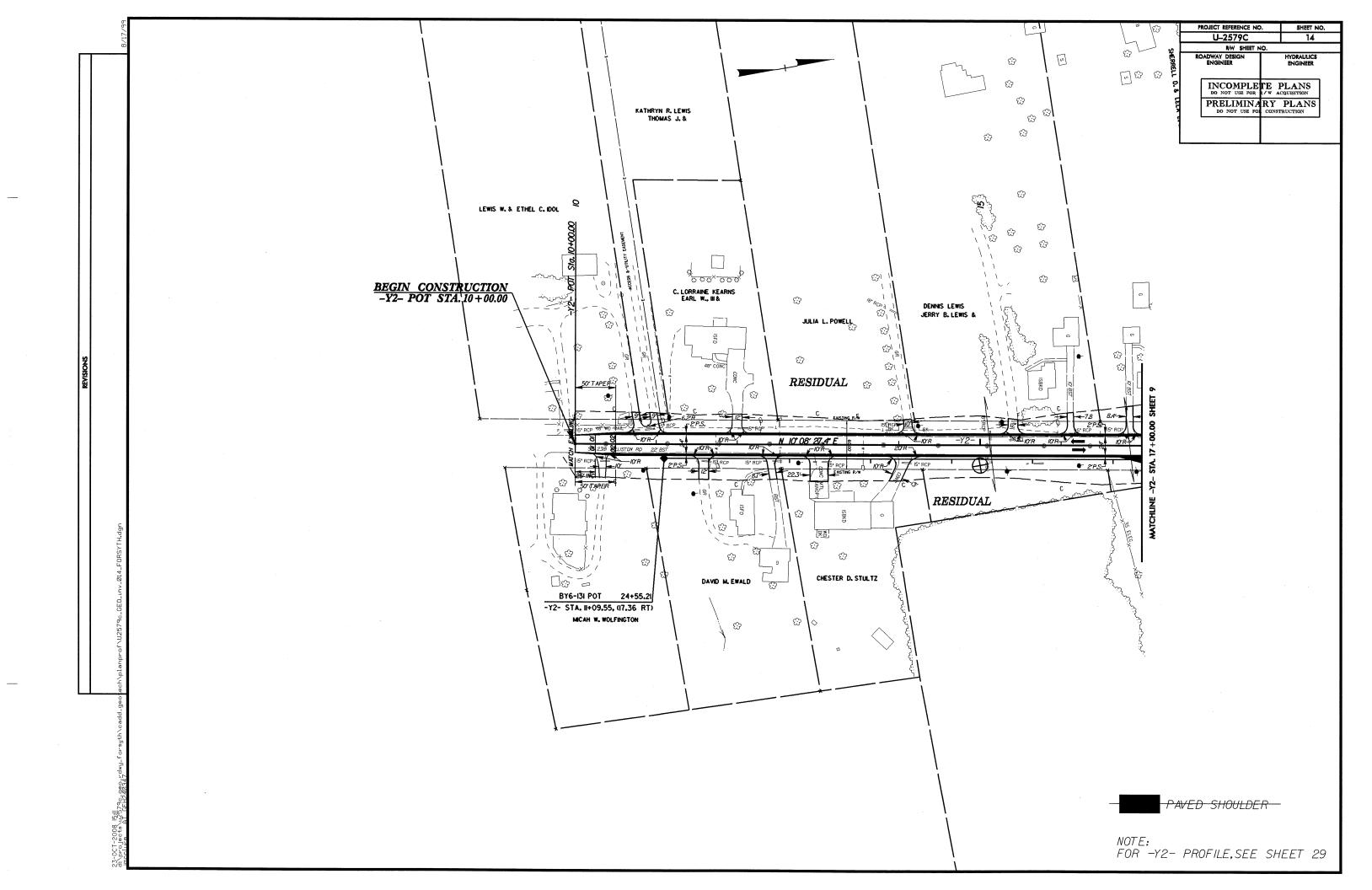


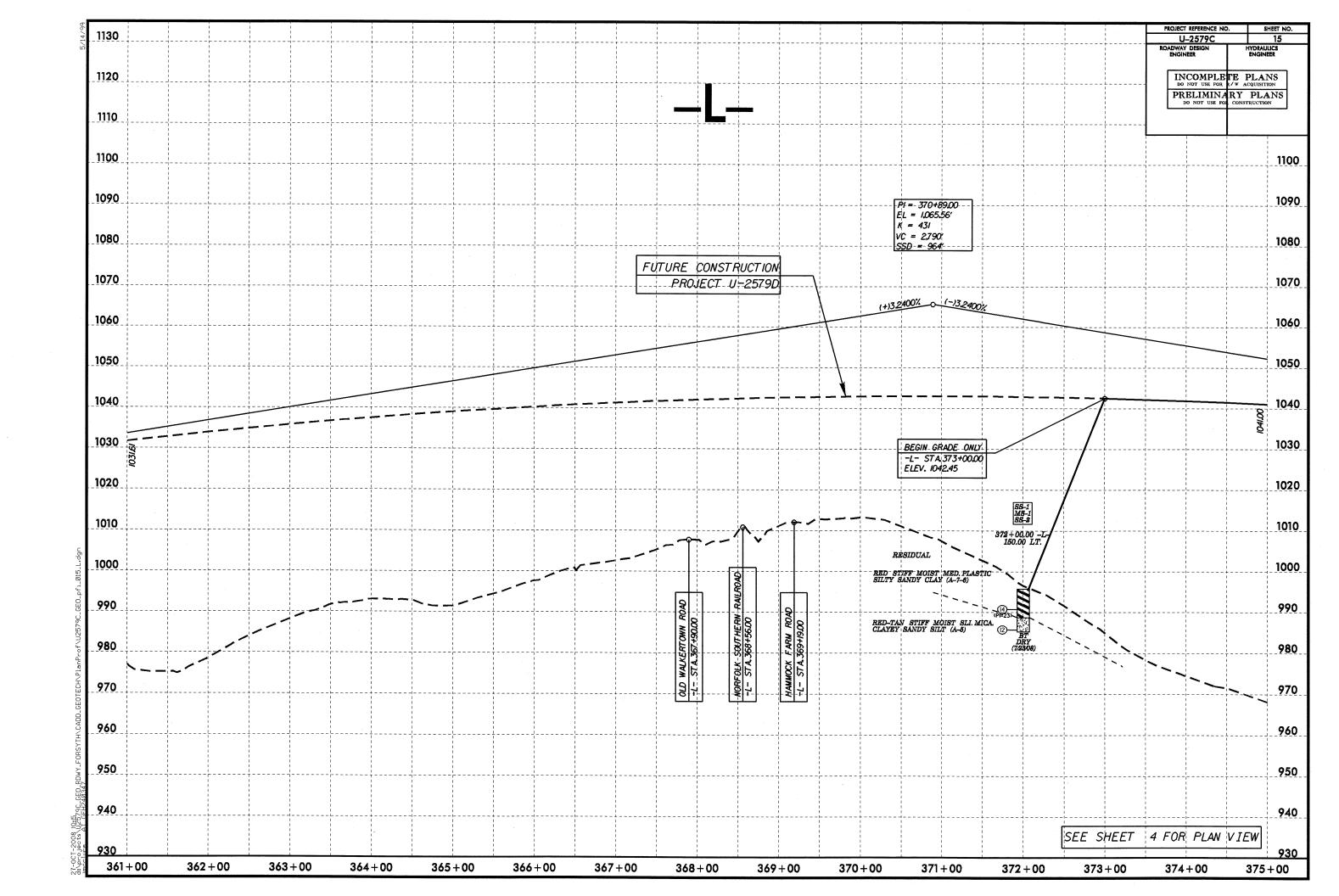


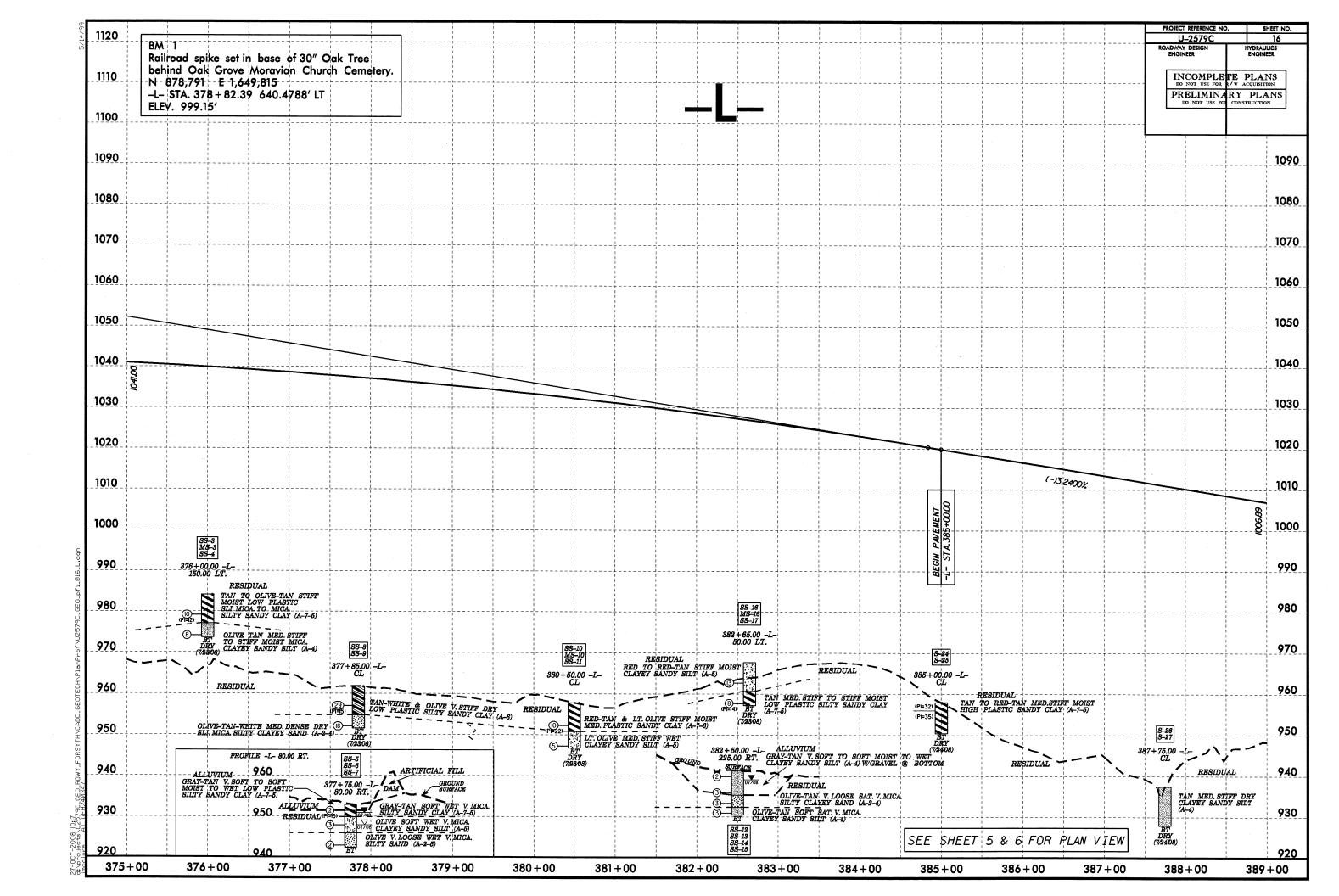


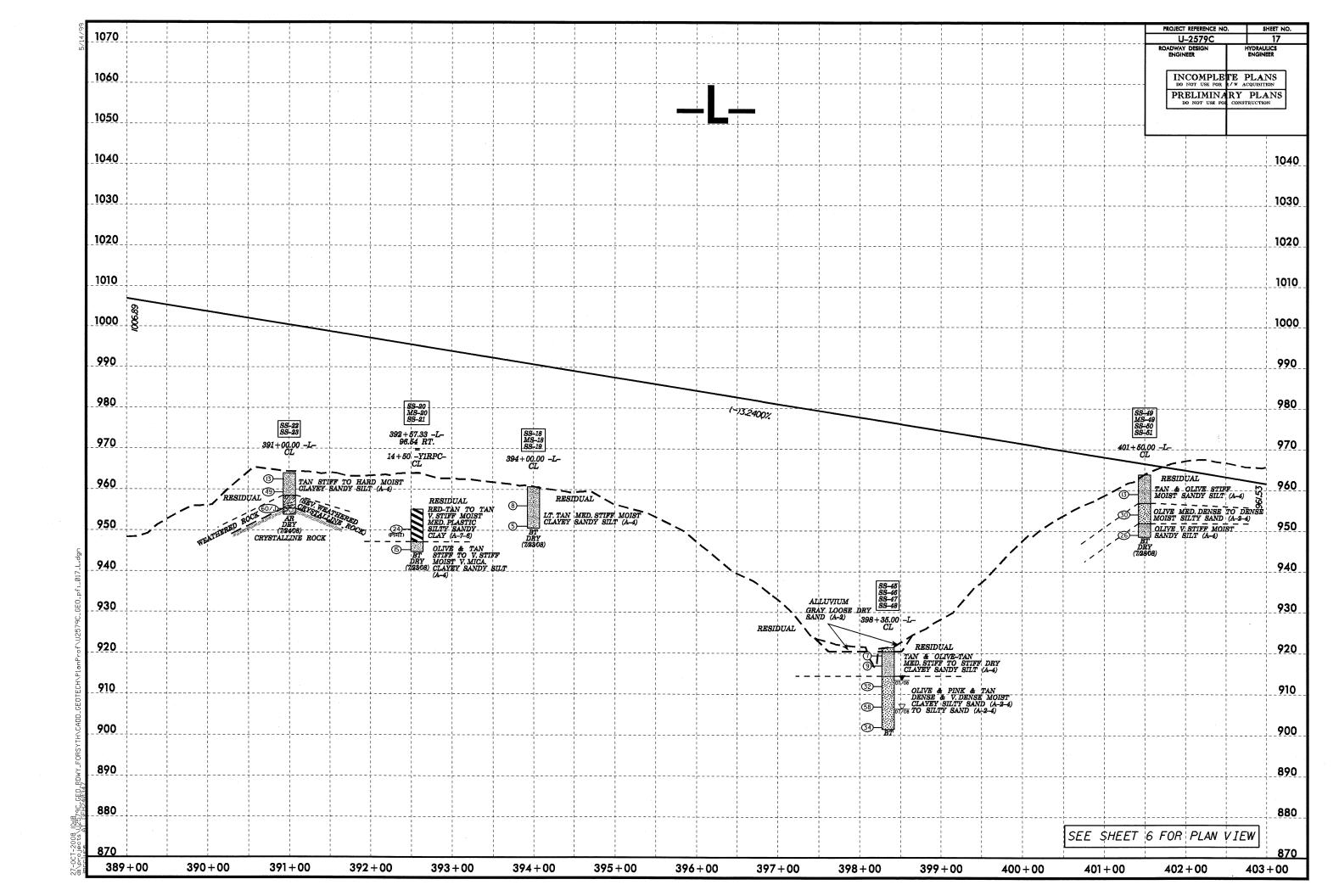


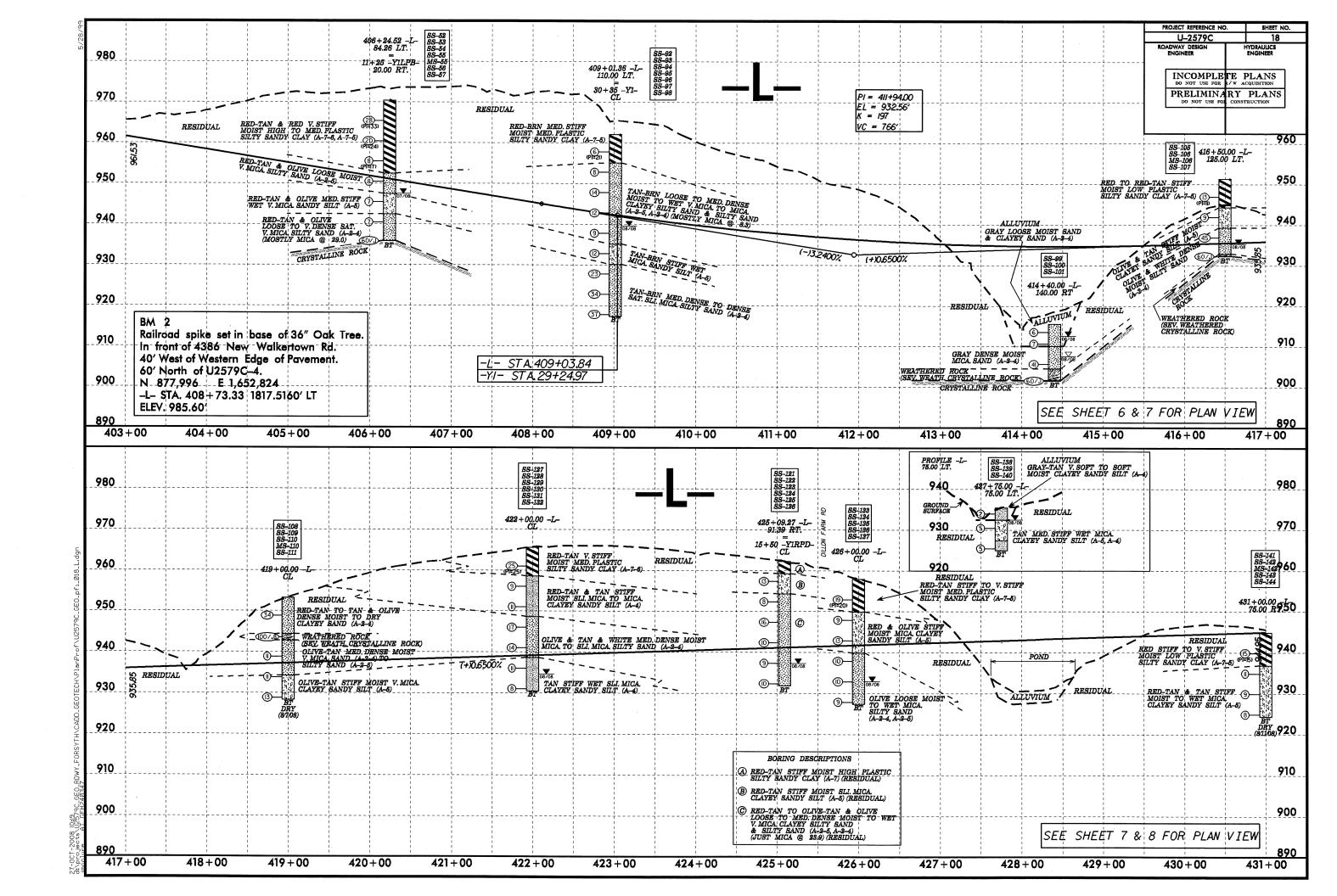


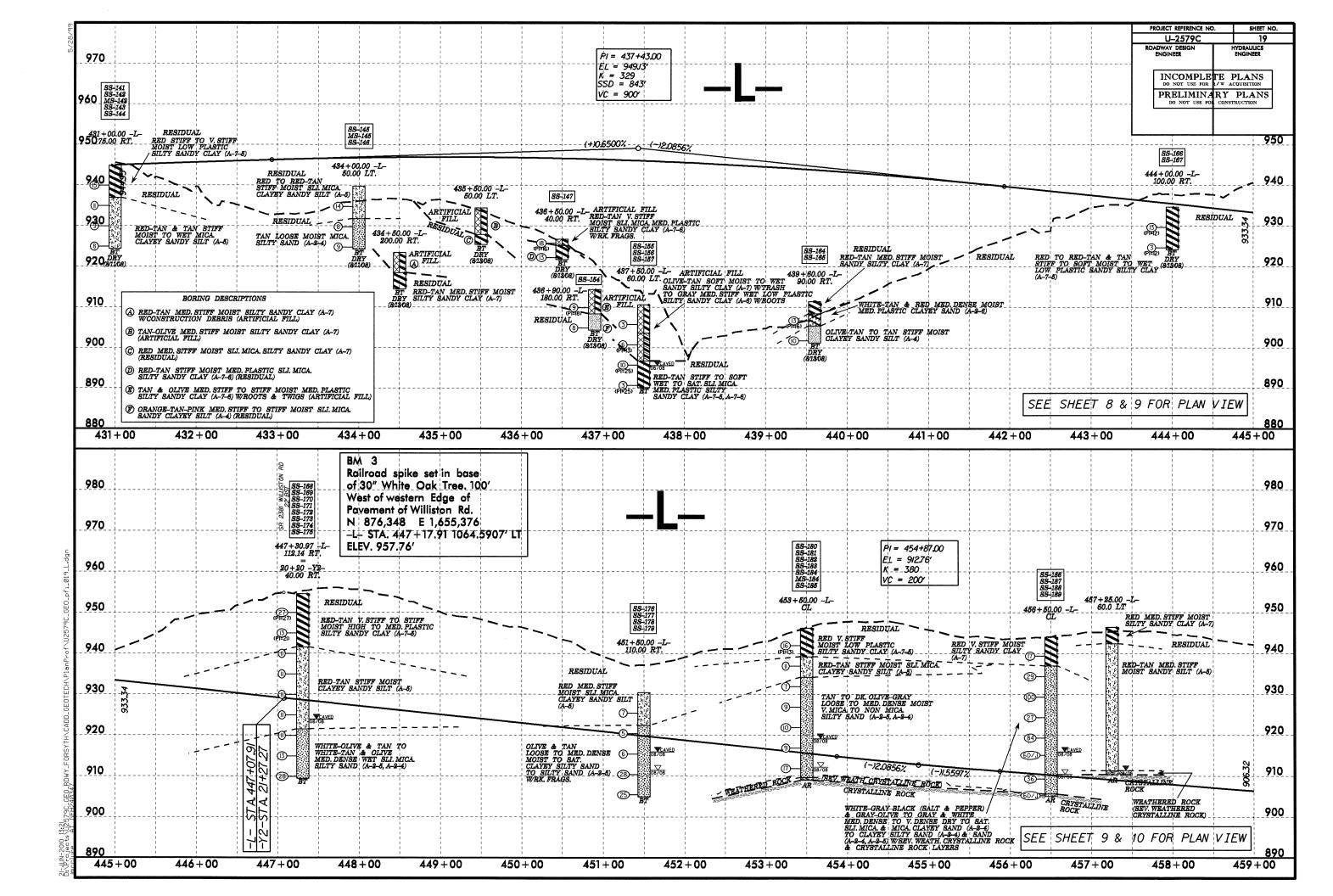


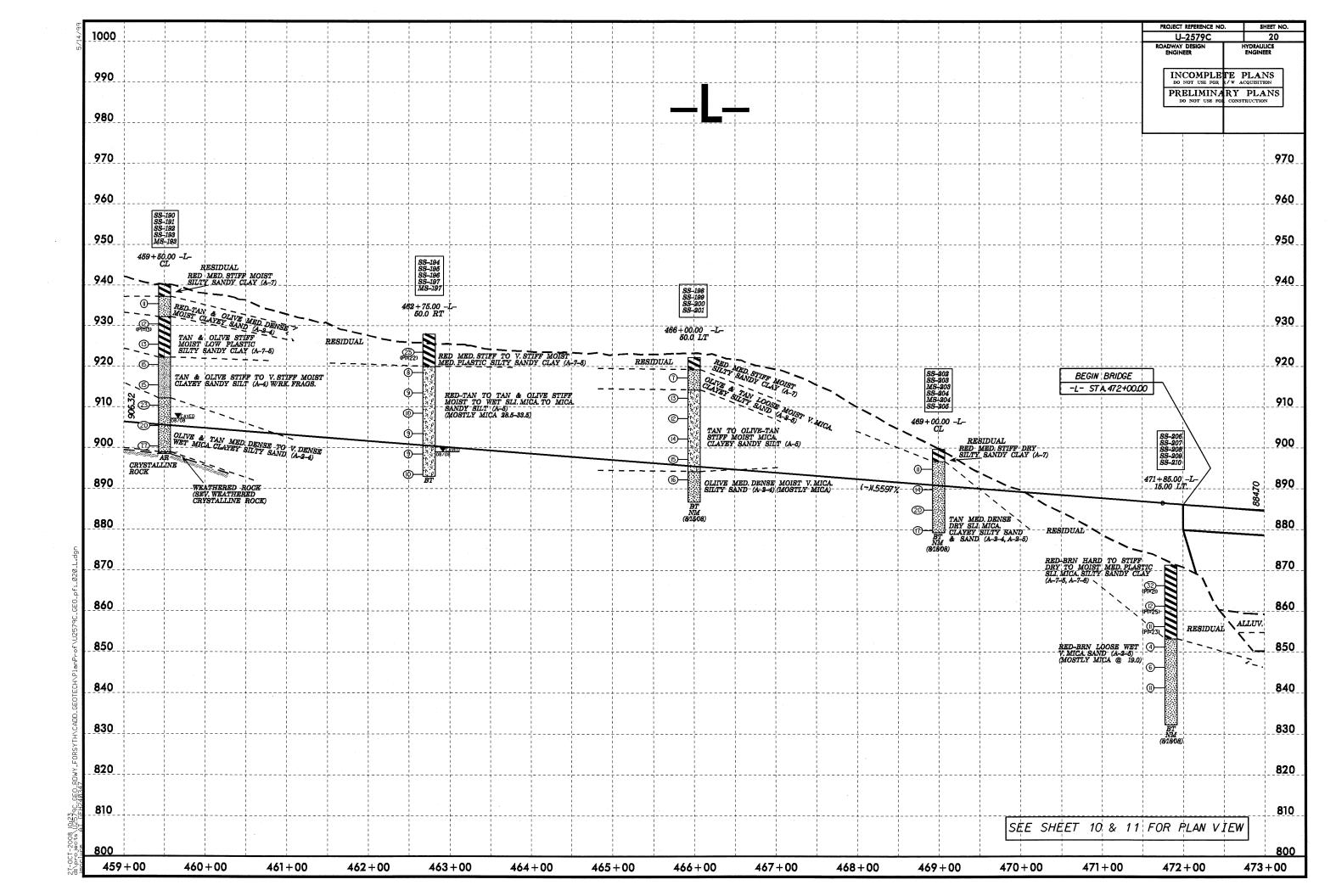


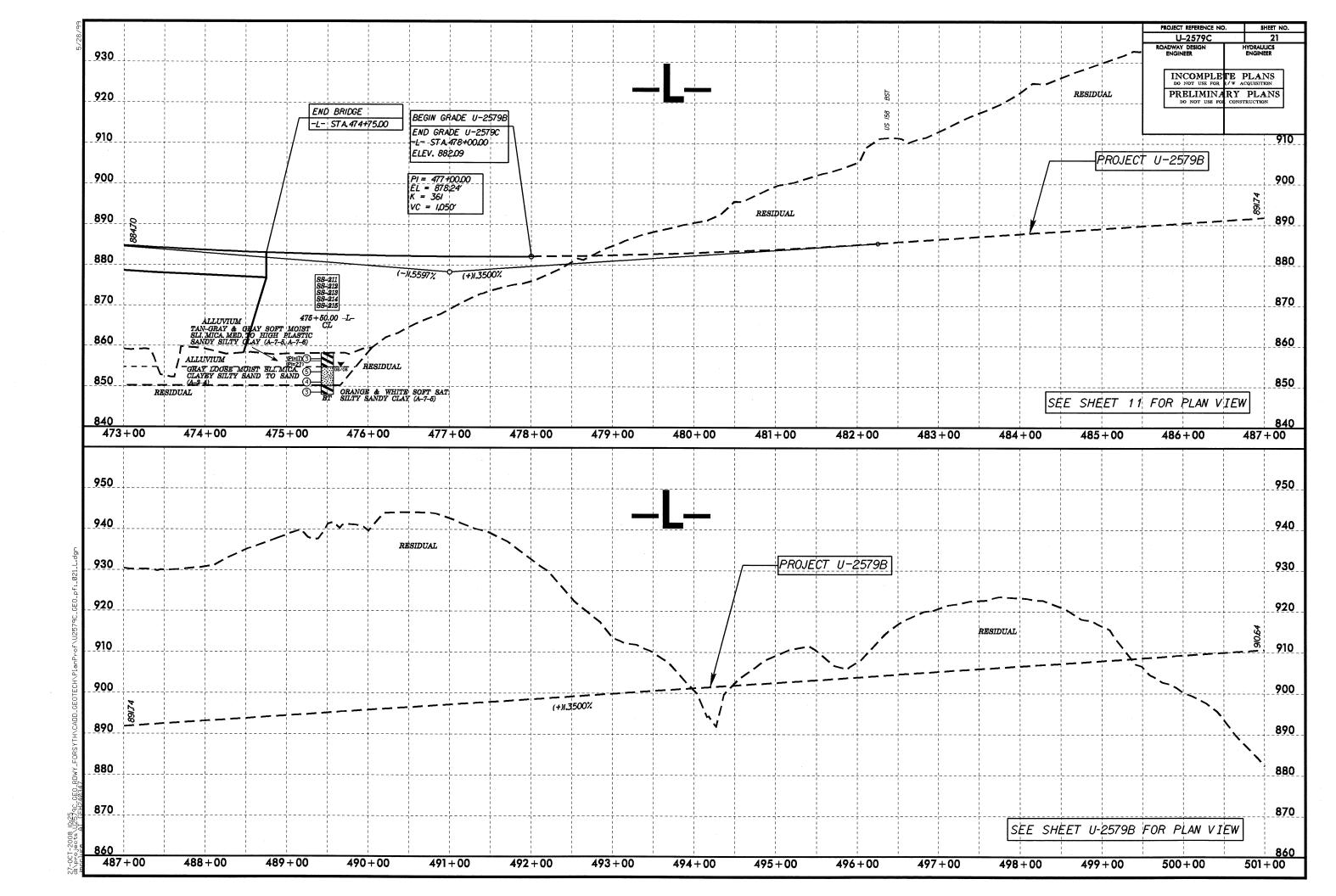


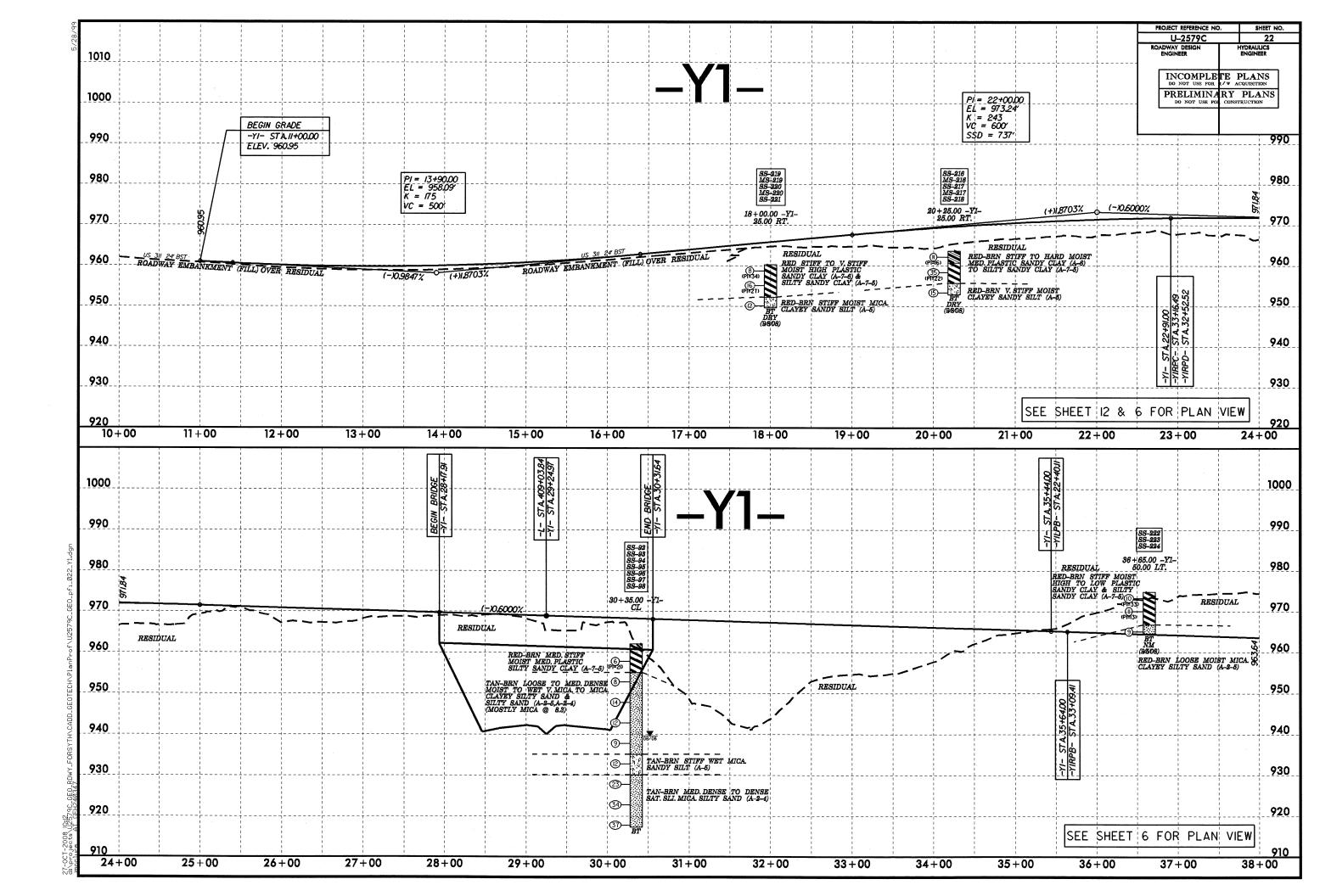


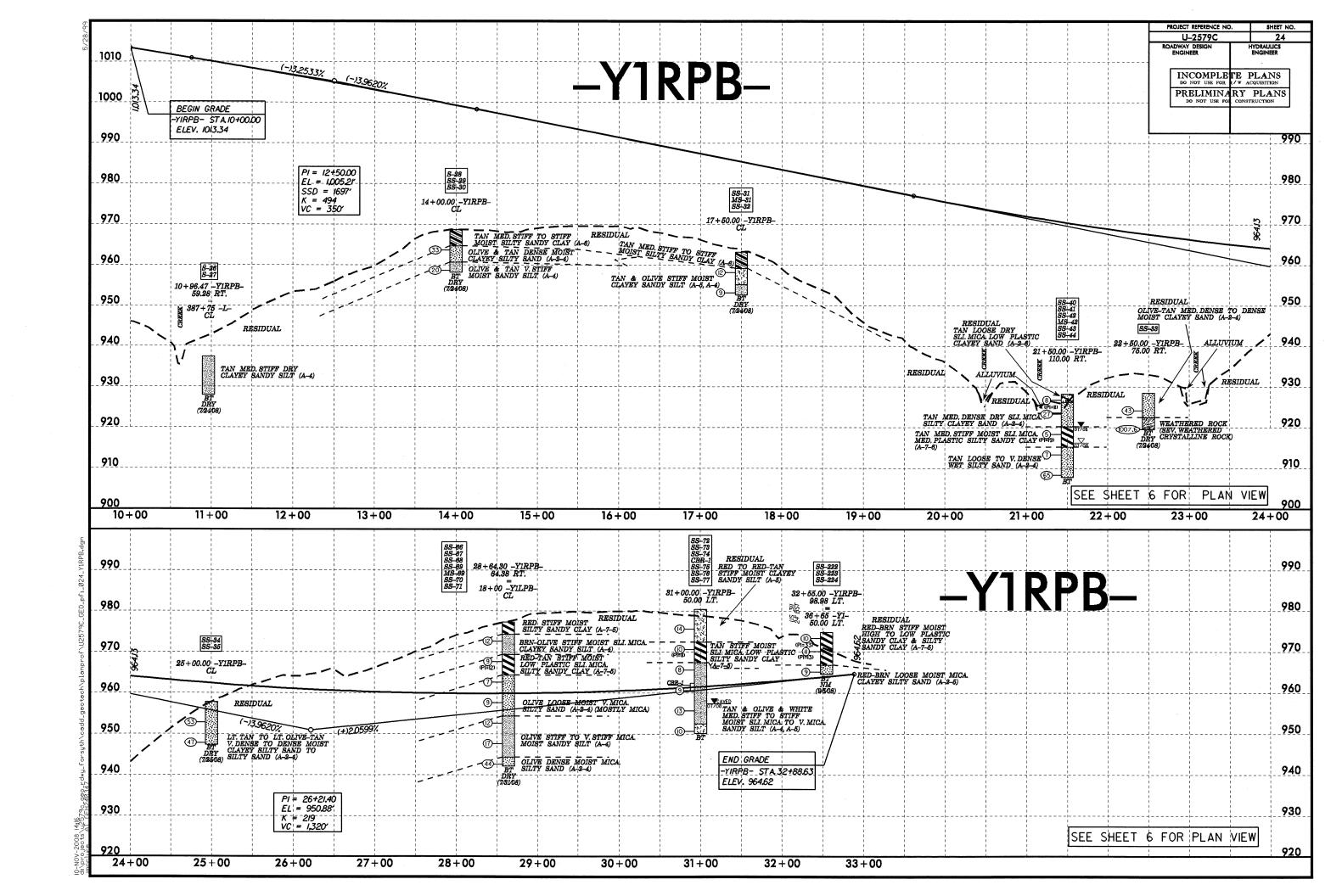


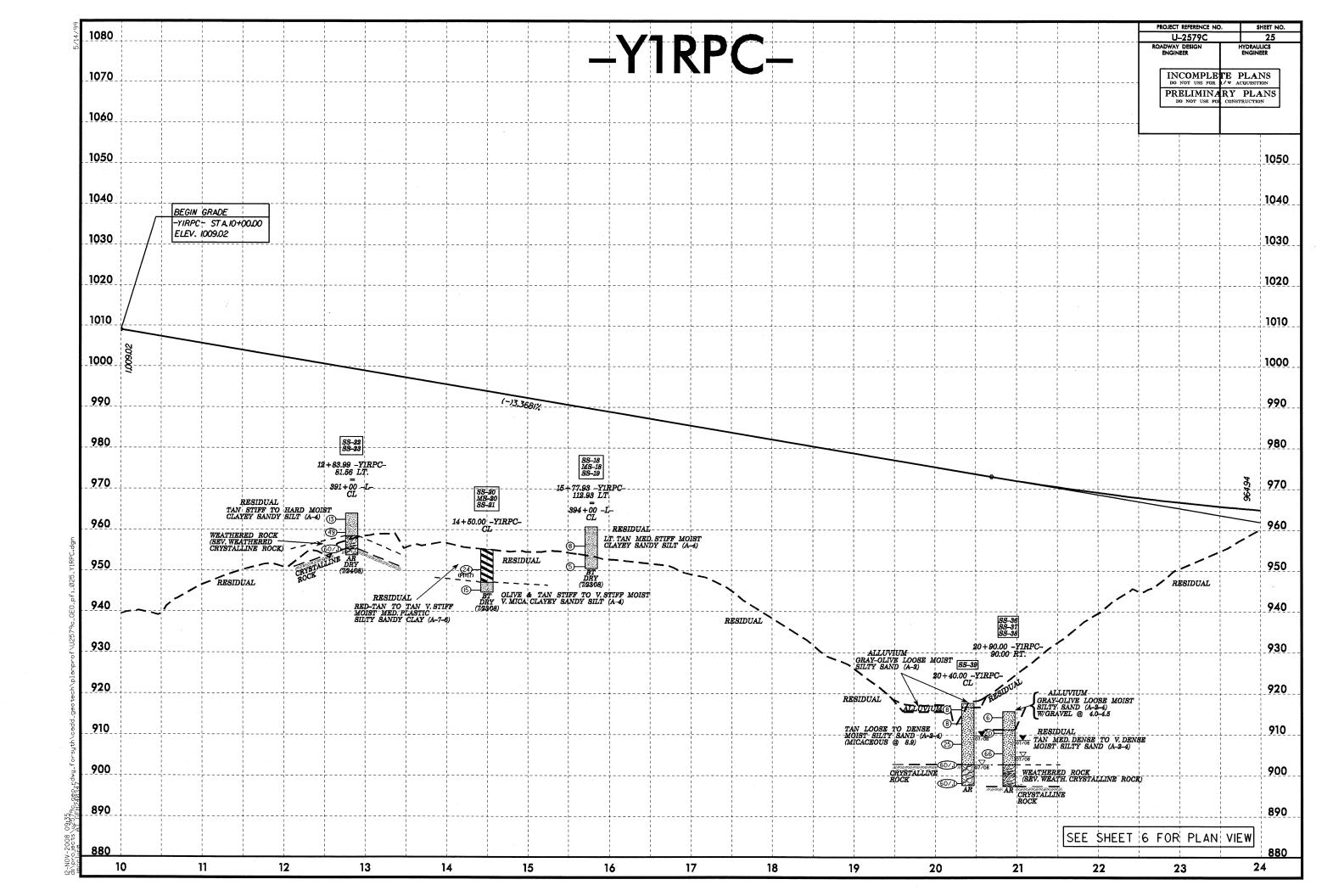


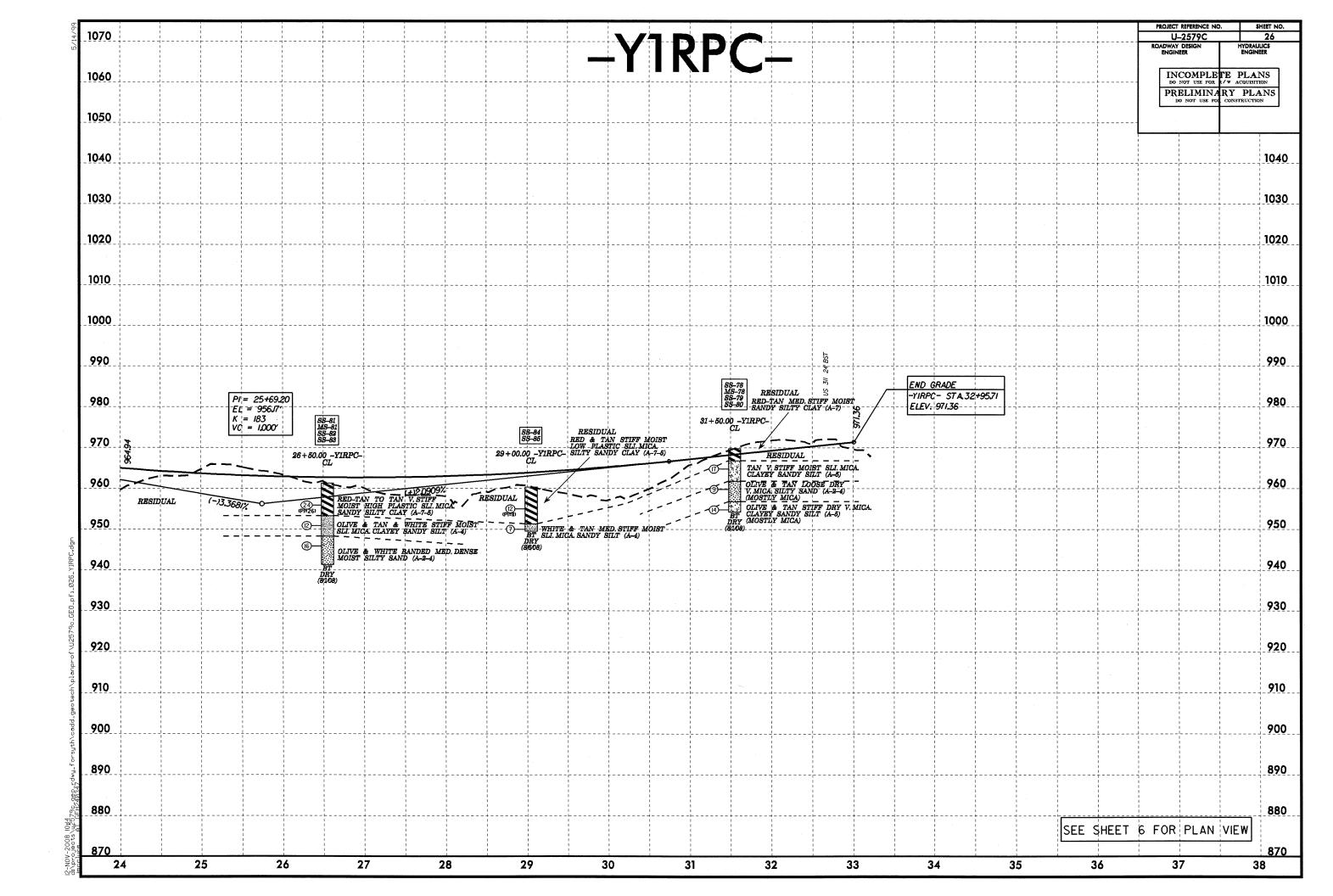


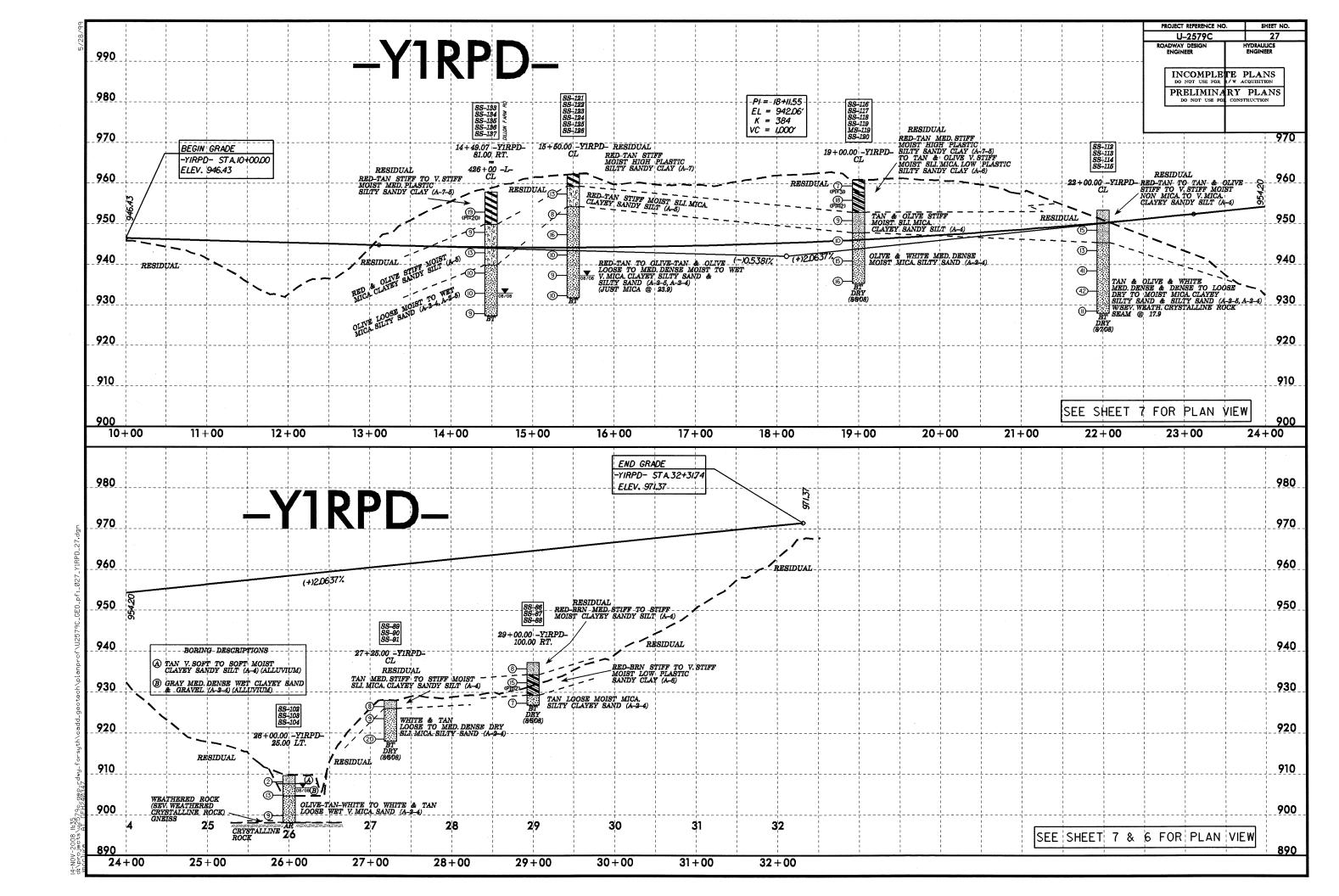




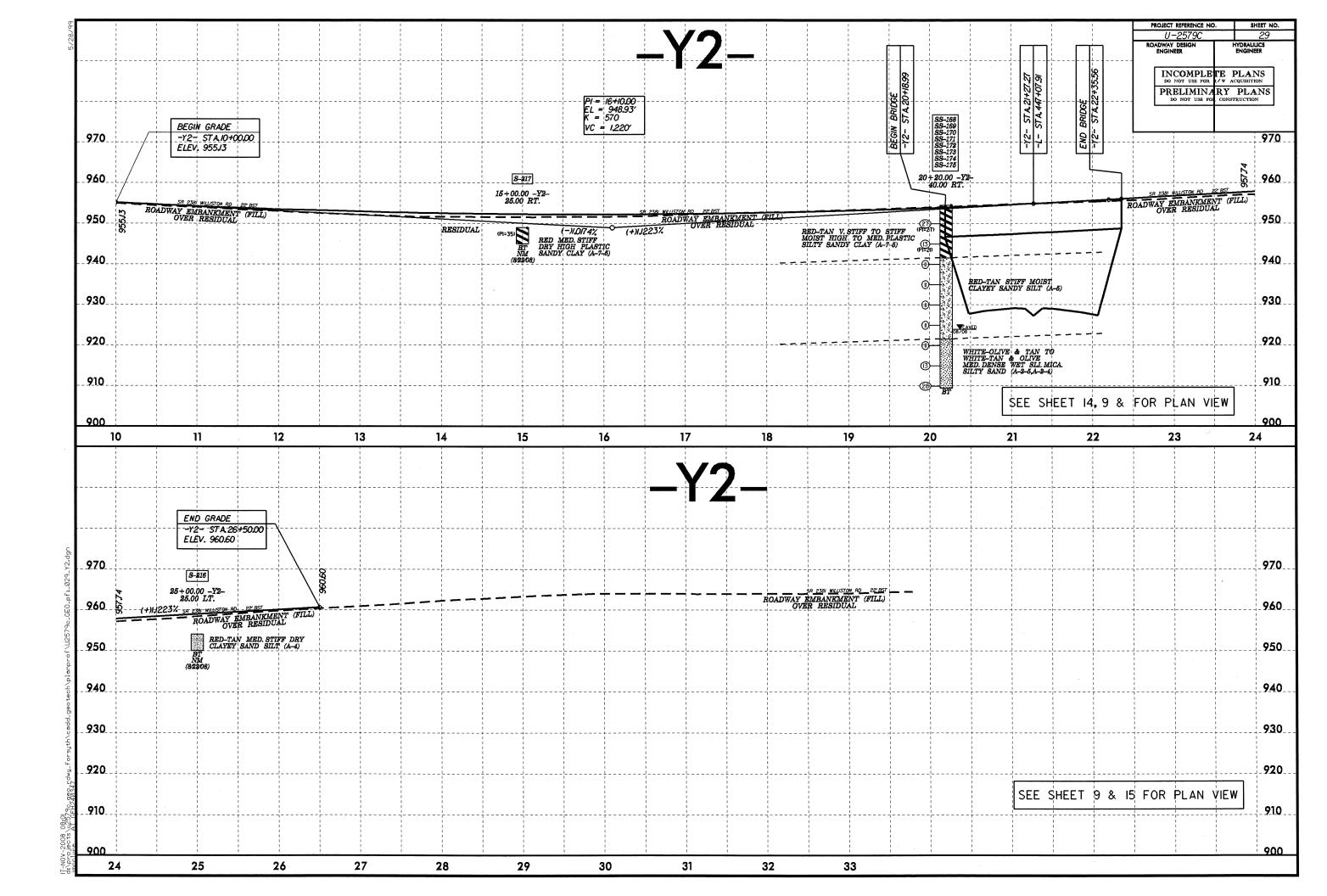


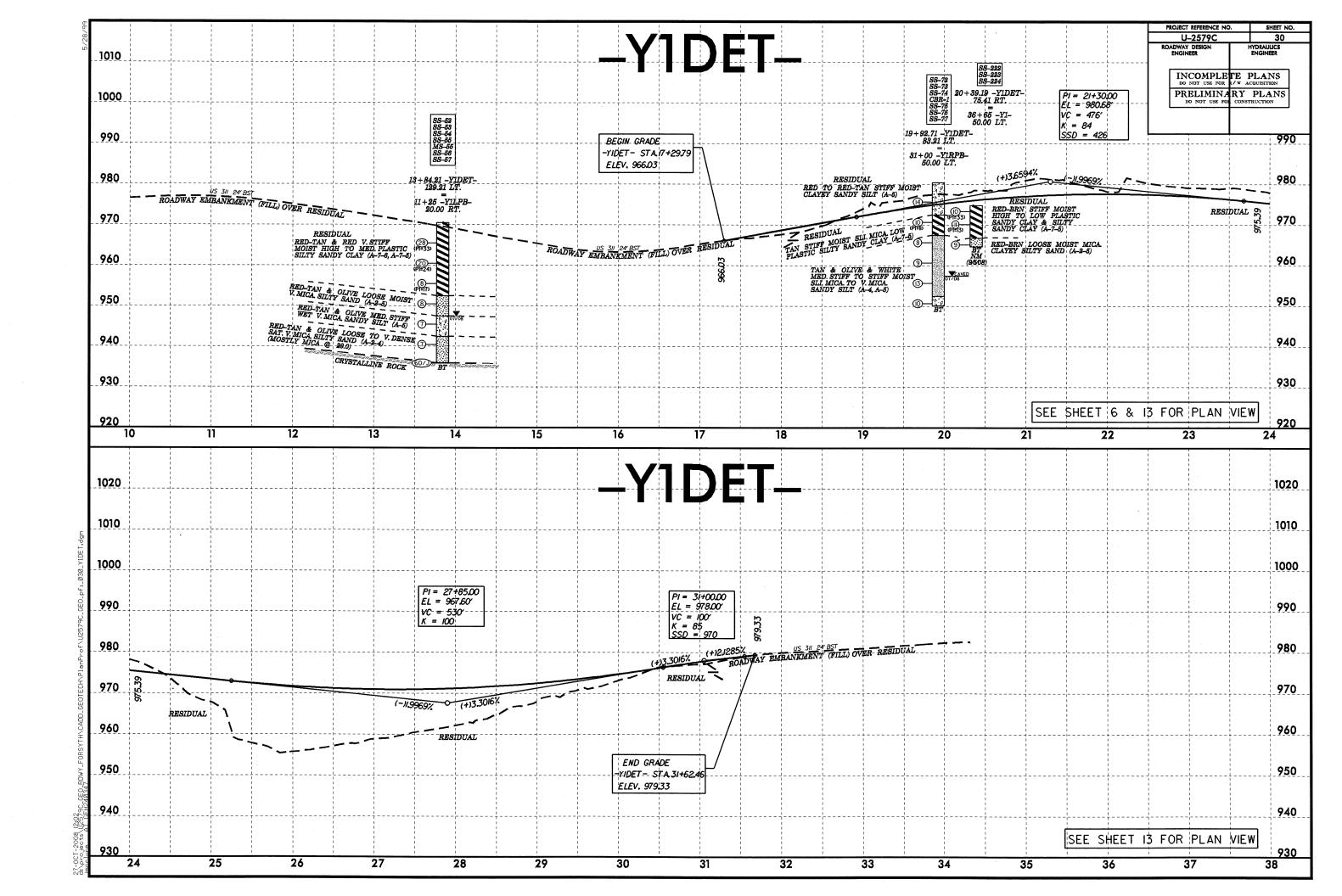


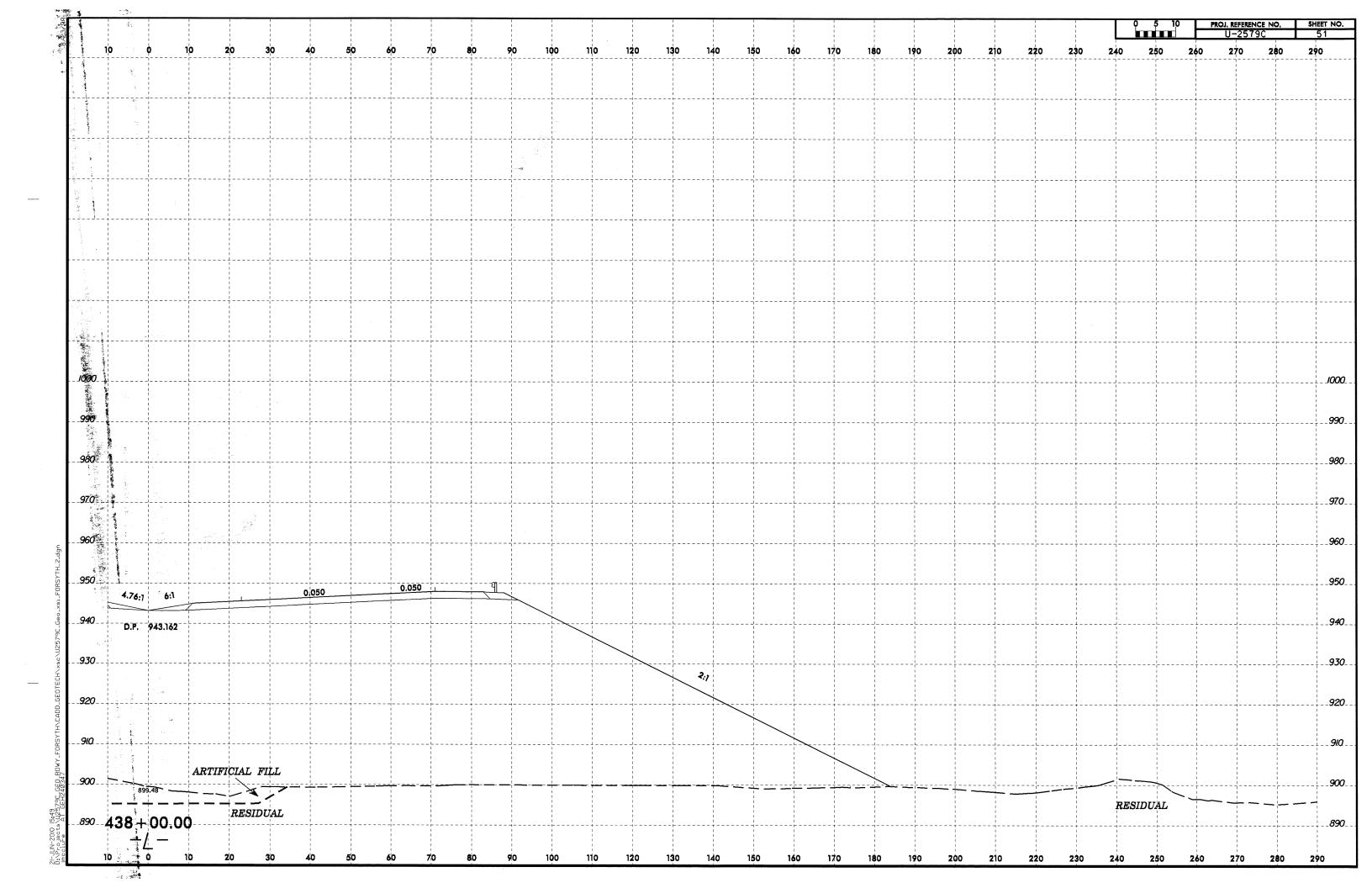




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SOIL TEST RESULTS																
SAMPLE			DEPTH	AASHTO				% BY V	VEIGHT		% PAS	SING (S	SIEVES)	%	%	Line o
NO.	OFFSET	STATION	INTERVAL	CLASS.	L.L.	P.I.	C.SAND	F.SAND	SILT	CLAY	10	40	200	MOISTURE	ORGANIC	Boring I
SS-1	150 LT	372+00	4.00-5.50	A-7-6(11)	51	23	16.4	32.2	19.1	32.4	100	93	56	20.8	•	L
SS-2	150 LT	372+00	9.00-10.50	A-5(2)	53	8	13.8	51.0	21.1	14.2	100	96	44	•	•	L
SS-3	150 LT	376+00	3.90-5.40	A-7-5(5)	52	12	12.9	42.3	20.5	24.3	100	95	52	23.0		L
SS-4	150 LT	376+00	8.90-10.40	A-4(0)	38	NP	13.5	53.0	21.3	12.1	99	94	41		•	L
SS-5	80 RT	377+75	0.50-2.00	A-7-5(9)	56	15	10.7	35.8	21.1	32.4	99	95	59		•	L
SS-6	80 RT	377+75	4.00-5.50	A-5(0)	53	NP	18.6	51.6	19.7	10.1	100	93	37	<u> </u>	•	L
SS-7	80 RT	377+75	9.00-10.50	A-2-5(0)	45	NP	18.2	59.0	14.7	8.1	100	94	31			L
SS-8	CL	377+85	3.70-5.20	A-6(4)	40	15	19.6	36.0	14.1	30.3	98	90	48	<u> </u>	•	L
SS-9	CL	377+85	8.70-10.20	A-2-4(0)	32	10	38.4	39.2	10.2	12.1	73	56	20		•	L
SS-10	CL	380+50	4.50-6.00	A-7-6(5)	46	22	23.1	37.6	5.0	34.4	98	87	43	19.8	•	<u> </u>
SS-11	CL	380+50	9.50-11.00	A-5(0)	45	4	18.4	47.3	18.1	16.2	98	91	40	· ·	<u> </u>	L.
SS-12 SS-13	225 RT	382+50 382+50	0.50-2.00	A-4(4)	39 30	9	6.9	41.5	27.4	24.3	100	97	60	<u> </u>	<u> </u>	<u> </u>
SS-13	225 RT 225 RT	382+50	4.40-5.90 7.00-8.50	A-4(2)	31	10 6	20.8	34.6	14.3	30.3	98	87	48	<u> </u>	<u> </u>	<u> </u>
SS-14 SS-15	225 RT	382+50	9.40-10.90	A-2-4(0) A-4(0)	38	NP	33.0 21.4	40.8 42.1	10.0 24.4	16.2 12.1	87 96	70	28 41	ļ ·	•	L
SS-16	50 LT	382+65	4.00-5.50	A-4(0) A-5(5)	56	8	13.8	34.8	19.1	32.4	98	86 91	56	25.8		L
SS-17	50 LT	382+65	9.00-10.50	A-7-5(6)	47	14	15.6	38.2	24.0	22.2	98	89	53	23.6	•	L L
SS-18	CL	394+00	3.70-5.20	A-4(1)	37	8	15.4	47.1	17.3	20.2	97	93	42	18.9	-:	L
SS-19	CL	394+00	8.70-10.20	A-4(0)	33	NP	14.4	55.0	18.5	12.1	96	92	37	10.9	- :	
SS-20	CL	14+50	3.90-5.40	A-7-6(9)	46	17	11.9	30.5	21.1	36.4	96	91	60	22.7		YIRPO
SS-21	CL	14+50	8.90-10.40	A-4(1)	38	9	11.1	54.8	17.9	16.2	100	97	43			YIRPO
SS-22	CL	391+00	0.50-10.40	A-4(1)	27	5	16.3	46.9	14.3	22.4	95	90	43			I
SS-23	CL	391+00	3.70-5.20	A-4(0)	31	9	23.9	43.9	18.0	14.3	91	79	37		-	l i
S-24	CL	385+00	0.00-2.00	A-7-5(22)	65	32	12.2	18.8	9.8	59.2	95	89	68		- :	 -
S-25	CL	385+00	2.00-6.00	A-7-5(22)	76	35	4.7	11.8	8.0	75.5	100	98	86	 		1
S-26	CL	387+75	0.00-4.00	A-4(1)	29	9	12.9	45.7	16.9	24.5	98	93	47	-		
S-27	CL	387+75	4.00-8.00	A-4(0)	23	6	17.6	45.3	14.7	22.4	92	86	40			l i
S-28	CL	14+00	0.00-4.00	A-6(3)	32	11	14.1	43.9	19.6	22.4	97	92	49	-		Y1RP
SS-29	CL	14+00	4.00-5.50	A-2-4(0)	28	4	15.9	57.8	16.1	10.2	95	90	34			Y1RP
SS-30	CL	14+00	9.00-10.50	A-4(0)	35	3	10.0	54.5	27.3	8.2	98	96	46			Y1RP(
SS-31	CL	17+50	4.00-5.50	A-5(4)	41	7	11.4	38.4	25.7	24.5	100	97	60	20.2		Y1RPE
SS-32	CL	17+50	9.00-10.50	A-4(0)	36	2	14.9	47.8	12.9	24.5	99	94	46			Y1RPE
SS-33	75 RT	22+50	3.30-4.80	A-2-4(0)	29	NP	25.1	51.2	9.4	14.3	72	64	22			Y1RP0
SS-34	CL	25+00	4.00-5.50	A-2-4(0)	26	4	33.9	43.9	12.0	10.2	89	76	25			Y1RPE
SS-35	CL	25+00	9.00-10.50	A-2-4(0)	25	NP	20.8	54.9	16.1	8.2	99	94	32			Y1RPI
SS-36	90 RT	20+90	0.50-2.00	A-2-4(0)	23	NP	18.8	54.5	18.6	8.2	98	91	33			Y1RP0
SS-37	90 RT	20+90	4.00-4.50	A-2-4(0)	31	NP	40.4	42.2	13.3	4.1	96	76	22			Y1RP0
SS-38	90 RT	20+90	9.30-10.80	A-2-4(0)	23	NP	34.7	48.6	12.7	4.1	96	81	22			Y1RP0
SS-39	CL	20+40	8.90-10.40	A-2-4(0)	32	NP	26.9	46.6	18.4	8.1	97	86	34			Y1RP0
SS-40	110 RT	21+50	0.50-2.00	A-2-6(0)	27	11	24.9	42.1	6.7	26.3	91	79	34	-		Y1RPE
SS-41	110 RT	21+50	3.90-5.40	A-2-4(0)	24	6	25.5	44.7	11.5	18.2	84	72	30			Y1RPE
SS-42	110 RT	21+50	8.90-10.40	A-7-6(8)	44	19	14.6	37.1	26.0	22.3	99	93	54	30.8		Y1RPE
SS-43	110 RT	21+50	13.90-15.40	A-2-4(0)	33	3	32.7	35.3	23.9	8.1	88	71	34	•	•	Y1RPE
SS-44	110 RT	21+50	18.90-20.40	A-2-4(0)	34	4	24.9	42.6	24.3	8.1	86	75	34		•	Y1RPE
SS-45	CL	398+35	3.50-5.00	A-4(0)	27	8	25.2	38.3	18.3	18.3	95	82	41	•		L
SS-46	CL	398+35	8.50-10.00	A-2-4(0)	26	7	32.0	35.3	22.5	10.1	87	70	34	•		L
SS-47	CL	398+35	13.50-15.00	A-2-4(0)	24	NP	26.4	46.5	21.1	6.1	97	86	35		-	L
SS-48	CL	398+35	18.50-20.00	A-2-4(0)	25	NP	23.9	50.5	19.5	6.1	98	87	34	•	-	L
SS-49	CL	401+50	3.80-5.30	A-4(0)	35	6	19.9	48.7	23.3	8.1	100	97	38	13.9	-	L
SS-50	CL	401+50	8.80-10.30	A-2-4(0)	30	6	20.3	52.5	19.1	8.1	98	91	35		•	L
SS-51	CL	401+50	13.80-15.30	A-4(0)	33	NP	21.1	50.9	21.9	6.1	100	94	36	•		L
SS-52	20 RT	11+25	4.00-5.50	A-7-6(14)	60	33	23.1	26.1	10.2	40.5	99	85	53		-	Y1LPE
SS-53	20 RT	11+25	9.00-10.50	A-7-5(13)	57	24	15.8	29.8	13.9	40.5	99	90	58	•	•	Y1LPE
SS-54	20 RT	11+25	14.00-15.50	A-7-5(9)	65	17	16.4	37.1	30.3	16.2	100	92	55	•	•	Y1LPE
SS-55	20 RT	11+25	19.00-20.50	A-2-5(0)	45	NP	18.0	62.0	13.9	6.1	100	92	30		-	Y1LPE
SS-56	20 RT	11+25	24.00-25.50	A-5(0)	47	NP	14.2	58.6	21.2	6.1	100	94	37	27.0	•	Y1LPE
SS-57	20 RT	11+25	34.00-35.50	A-2-4(0)	39	NP	22.5	61.0	14.5	2.0	100	90	25		-	Y1LPE
SS-58	25 RT	14+00	4.00-5.50	A-7-5(16)	63	33	22.5	23.1	9.8	44.6	97	83	56	<u> </u>	•	Y1LPE
SS-59	25 RT	14+00	9.00-10.50	A-2-5(0)	48	NP	23.3	51.1	17.5	8.1	95	82	32	<u> </u>	-	Y1LPI
SS-60 SS-61	25 RT	14+00	14.00-15.50	A-2-4(0)	40	NP 45	26.3	57.5	12.1	4.1	97	83	25	20.0	•	Y1LPE
SS-61	50 RT	16+00	3.90-5.40	A-7-5(10)	55	15	17.8	25.4	22.3	34.5	97	85	62	32.3	•	Y1LPE
SS-62	50 RT	16+00	8.90-10.40	A-5(4)	47	6	17.8	28.8	39.1	14.2	100	91	61		-	Y1LPE
SS-63 SS-64	50 RT 50 RT	16+00 16+00	13.90-15.40	A-5(0)	49	NP	25.8	44.2	26.0	4.1	100	87	40	32.4	•	Y1LPE
		16+00	18.90-20.40	A-2-4(0)	38	NP	28.0	46.5	19.5	6.1	98	85	33	-	-	Y1LPE
SS-65	50 RT	16+00	23.90-25.40	A-2-4(0)	24	NP	12.8	67.7	15.4	4.1	100	92	29		-	Y1LPE
SS-66	CL	18+00	3.70-5.20	A-4(0)	40	NP 42	15.4	50.7	19.7	14.2	98	91	42	•	-	Y1LPE
SS-67	CL	18+00	8.70-10.20	A-7-5(10)	52	12	4.9	35.1	31.6	28.4	100	98	69		•	Y1LPI
SS-68	CL	18+00	13.70-15.20	A-2-4(0)	31	NP	16.0	60.0	19.9	4.1	100	93	35	•	•	Y1LPE
SS-69	CL	18+00	23.70-25.20	A-4(0)	35	5	21.9	46.9	27.2	4.1	99	90	41	28.1	•	Y1LPE
SS-70	CL	18+00	28.70-30.20	A-4(0)	33	NP	23.9	44.0	28.0	4.1	99	88	42			Y1LPE
SS-71	CL	18+00	33.70-35.20	A-2-4(0)	27	NP	19.5	61.3	17.2	2.0	98	91	28		•	Y1LPE
SS-72	50 LT	36+00	3.80-5.30	A-5(6)	48	10	13.8	35.3	30.6	20.3	100	94	60		•	Y1RPI
SS-73	50 LT	36+00	8.80-10.30	A-7-5(5)	44	11	10.8	47.3	27.8	14.2	100	97	55		-	Y1RPI

			S	SOIL '	TES	T R	ES	ULT	S	***						
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	C.SAND	% BY W	VEIGHT	CLAY	% PAS	SING (S	IEVES)	% MOISTURE	% ORGANIC	Line or Boring ID
SS-75	50 LT	36+00	18.80-20.30	A-4(0)	38	NP	10.8	56.2	24.9	8.1	100	95	44	WOSTORE	ONGANIC	Y1RPB
SS-76	50 LT	36+00	23.80-25.30	A-4(0)	36	NP	27.8	44.6	19.5	8.1	98	82	36		-	Y1RPB
SS-77	50 LT	36+00	28.80-30.30	A-5(4)	46	9	9.9	46.9	35.1	8.1	96	92	54		•	Y1RPB
SS-78	CL	31+50	4.00-5.50	A-5(4)	51	10	15.6	41.0	19.1	24.3	100	93	51	9.90		Y1RPC
SS-79 SS-80	CL CL	31+50 31+50	9.00-10.50 14.00-15.50	A-2-5(0) A-5(2)	48 44	NP 8	15.2 18.5	60.2 44.0	16.4 23.3	14.2	100	96 91	34 47	•		Y1RPC Y1RPC
SS-81	CL	26+50	4.40-5.90	A-7-5(23)	64	26	8.3	19.3	23.7	48.7	100	96	77	25.0	-	Y1RPC
SS-82	CL	26+50	9.40-10.90	A-4(0)	38	3	23.3	42.2	20.3	14.2	99	88	42	•		Y1RPC
SS-83	CL	26+50	14.40-19.90	A-2-4(0)	30	NP	29.2	47.9	18.9	4.1	99	92	31	-		Y1RPC
SS-84	CL	29+00	4.30-5.80	A-7-5(6)	57	11	12.7	40.8	18.1	28.3	100	94	53	-	•	YIRPC
SS-85 SS-86	CL 100 RT	29+00 29+00	9.30-10.80 0.50-2.00	A-4(0)	36 23	5 8	27.9 25.9	42.7 36.8	21.3	8.1 28.3	100	85	37	-	-	YIRPC
SS-87	100 RT	29+00	3.90-5.40	A-4(0) A-6(2)	32	12	26.3	31.7	9.0	32.4	100	90	40 45		•	YIRPD YIRPD
SS-88	100 RT	29+00	8.90-10.40	A-2-4(0)	33	6	34.6	40.8	10.4	14.2	100	85	29	-		YIRPD
SS-89	CL	27+25	0.50-2.00	A-4(0)	36	3	25.3	42.3	14.3	18.2	99	88	39			YIRPD
SS-90	CL	27+25	3.50-5.00	A-2-4(0)	35	NP	31.5	50.4	14.1	4.0	99	85	25			Y1RPD
SS-91	CL	27+25	8.50-10.00	A-2-4(0)	36	NP	31.3	54.0	12.7	2.0	99	85	22	•	-	Y1RPD
SS-92 SS-93	CL CL	30+35 30+35	3.30-4.80 8.30-9.80	A-7-5(11)	52 41	21 NP	17.1	27.8 56.9	18.8	36.3 14.1	99	90 96	59	•	•	Y1 Y1
SS-93 SS-94	CL	30+35	13.30-14.80	A-2-5(0) A-2-5(0)	41	NP NP	14.9	63.7	14.1	6.0	100	95	35 34	•	•	Y1 Y1
SS-95	CL	30+35	18.30-19.80	A-2-3(0) A-2-4(0)	36	NP	22.2	58.9	14.9	4.0	100	91	28			Y1
SS-96	CL	30+35	23.30-24.80	A-2-5(0)	43	NP	15.7	59.1	19.2	6.0	99	93	35	-	-	Y1
SS-97	CL	30+35	28.30-29.80	A-5(0)	44	NP	16.1	56.0	21.8	6.0	100	94	36	-	•	Y1
SS-98	CL	30+35	33.30-34.80	A-2-4(0)	33	NP	32.9	41.3	21.8	4.0	98	79	33	•	-	Y1
SS-99 SS-100	140 RT 140 RT	414+40 414+40	1.00-2.50 3.90-5.40	A-2-4(0) A-2-4(0)	25 21	NP NP	44.8 34.5	42.6 50.5	4.4	8.1 10.1	96 93	71 78	16 17			<u> </u>
SS-100	140 RT	414+40	8.90-10.40	A-2-4(0) A-2-4(0)	27	NP NP	37.6	51.1	7.3	4.0	96	84	15		-	L
SS-102	25 LT	26+00	0.50-2.00	A-4(0)	34	6	22.8	43.6	15.4	18.2	97	87	37	-	-	YIRPD
SS-103	25 LT	26+00	2.00-3.50	A-2-4(0)	22	NP	27.3	53.9	6.7	12.1	98	87	23	-	-	YIRPD
SS-104	25 LT	26+00	8.80-10.30	A-2-4(0)	33	NP	33.9	54.3	7.7	4.0	96	85	16	-	-	YIRPD
SS-105	125 LT	416+50	3.40-4.90	A-7-5(4)	58	11	15.4	44.8	11.5	28.3	98	89	47		•	L
SS-106 SS-107	125 LT 125 LT	416+50 416+50	8.40-9.90 13.40-14.90	A-5(0) A-2-4(0)	49 37	NP NP	18.4 28.3	49.3 54.9	18.2 10.7	14.1 6.1	99 98	93 85	40	32.8		L
SS-107 SS-108	CL	419+00	3.40-4.90	A-2-4(0) A-2-4(0)	34	NP NP	35.2	45.5	7.3	12.1	94	78	23	-		
SS-109	CL	419+00	13.40-14.90	A-2-4(0)	39	NP	41.4	48.1	4.4	6.1	88	70	14		-	L
SS-110	CL	419+00	18.40-19.90	A-2-5(0)	52	NP	32.7	48.9	12.3	6.1	98	82	24	27.5	-	L
SS-111	CL	419+00	23.40-24.90	A-5(0)	43	NP	28.5	39.8	21.6	10.1	100	83	40			L
SS-112	CL	22+00	3.90-5.40	A-4(1)	40	10	30.5	36.6	14.7	18.2	100	82	39		•	YIRPD
SS-113 SS-114	CL CL	22+00 22+00	8.90-10.40 13.90-15.40	A-2-5(0) A-2-4(0)	42 34	NP NP	35.8 38.8	38.6 36.8	13.5	12.1	100 97	80 73	32			YIRPD YIRPD
SS-115	CL	22+00	18.90-20.40	A-2-4(0) A-2-4(0)	33	NP NP	46.9	40.7	9.4	3.0	81	57	14			YIRPD
SS-116	CL	19+00	0.50-2.00	A-7-5(22)	62	31	17.3	16.9	19.4	46.4	100	90	69			Y1RPD
SS-117	CL	19+00	4.00-5.50	A-6(3)	40	12	22.2	36.9	14.7	26.2	100	89	48	-	-	Y1RPD
SS-118	CL	19+00	9.00-10.50	A-4(0)	34	3	23.2	46.4	16.3	14.1	100	90	40	-	-	Y1RPD
SS-119	CL	19+00	14.00-15.50	A-2-4(0)	32	NP	27.6	49.6	16.7	6.0	100	86	32	12.2	•	Y1RPD
SS-120 SS-121	CL CL	19+00 15+50	19.00-20.50 3.90-5.40	A-2-4(0) A-5(1)	36 51	NP 10	34.1	40.9 32.5	19.0	6.0 20.2	99 99	79	33		-	Y1RPD
SS-121	CL	15+50	8.90-10.40	A-2-5(0)	50	NP	37.3	32.3	13.7 18.3	12.1	100	79 79	39 35	-:-		Y1RPD Y1RPD
SS-123	CL	15+50	13.90-15.40	A-2-5(0)	42	NP	42.9	40.1	14.9	2.0	99	76	21	-		Y1RPD
SS-124	CL	15+50	18.90-20.40	A-2-4(0)	40	NP	30.2	49.0	14.7	6.0	100	85	31		-	Y1RPD
SS-125	CL	15+50	23.90-25.40	A-2-4(0)	30	NP	29.0	49.8	15.1	6.0	99	85	30	•	-	Y1RPD
SS-126	CL	15+50	28.90-30.40	A-2-5(0)	48	NP	22.6	52.4	19.0	6.0	99	90	35	•	· -	Y1RPD
SS-127 SS-128	CL CL	422+00 422+00	3.60-5.10 8.60-10.10	A-7-6(15)	53 36	25 5	17.7 25.8	20.4 32.1	17.5 24.0	44.4 18.1	97 100	89 87	63 50	<u> </u>	-	<u> </u>
SS-120 SS-129	CL	422+00	13.60-15.10	A-4(1) A-4(0)	36	3	28.0	41.1	22.8	8.1	99	85	40		-	L
SS-130	CL	422+00	18.60-20.10	A-2-4(0)	33	3	33.7	37.5	20.8	8.1	93	74	35	-	-	L
SS-131	CL	422+00	23.60-25.10	A-2-4(0)	31	NP	50.4	26.8	16.7	6.0	81	52	23	-	-	Ē
SS-132	CL	422+00	28.60-30.10	A-4(1)	40	4	22.0	39.9	26.0	12.1	99	88	48	-		L
SS-133	CL	426+00	4.00-5.50	A-7-5(10)	57	20	20.2	27.2	18.3	34.3	99	87	57		•	L
SS-134 SS-135	CL CL	426+00 426+00	9.00-10.50	A-5(1)	52	7	25.8	42.9	21.2	10.1	99	85	40	-		L
SS-135 SS-136	CL	426+00	14.00-15.50 19.00-20.50	A-5(0) A-2-4(0)	47 30	4 NP	31.9 31.5	37.5 49.8	20.6 14.7	10.1 4.0	99 100	80 86	38 26			L
SS-137	CL	426+00	24.00-25.50	A-2-4(0)	41	NP	40.5	35.7	17.7	6.0	96	70	29			L
SS-138	75 LT	427+75	0.50-2.00	A-4(0)	23	6	36.4	29.3	12.0	22.2	97	78	36	-	-	
SS-139	75 LT	427+75	4.00-5.50	A-5(2)	42	9	29.9	27.7	18.1	24.3	99	82	47	-		L
SS-140	75 LT	427+75	9.00-10.50	A-4(0)	37	5	34.4	36.4	17.1	12.1	95	75	36	-	•	L
SS-141 SS-142	75 RT	431+00	4.00-5.50	A-7-5(11)	53	15	7.7	31.7	26.2	34.4	100	97	68	- 26.0	•	<u> </u>
SS-142 SS-143	75 RT 75 RT	431+00 431+00	9.00-10.50 14.00-15.50	A-5(1) A-5(2)	54 57	5	15.4 11.3	50.2 47.7	18.3 24.8	16.2 16.2	100	95 97	43	26.0		L
SS-144	75 RT	431+00	19.00-20.50	A-5(2)	54	4	11.9	48.3	25.6	14.2	100	96	47	 	.	
SS-145	50 LT	434+00	4.00-5.50	A-5(3)	48	10	23.1	34.6	14.1	28.3	100	87	48	23.4		
SS-146	50 LT	434+00	9.00-10.50	A-2-4(0)	40	NP	29.3	47.9	14.7	8.1	100	88	29		-	L
SS-147	40 RT	436+50	0.00-1.50	A-7-6(6)	45	16	23.3	26.5	9.8	40.4	99	87	53	-	-	L
SS-148	100 RT	437+20	4.00-5.50	A-4(1)	31	9	27.7	30.3	13.7	28.3	96	82	43	<u> </u>	<u> </u>	L

	SOIL TEST RESULTS															
SAMPLE	OFFSET	STATION	DEPTH	AASHTO		P.I.			VEIGHT		ı	SING (S		%	%	Line or
NO. SS-149	100 RT	437+20	9.00-10.50	CLASS. A-7-6(6)	L.L. 42	15	C.SAND 21.8	F.SAND 23.9	SILT 9.8	44.5	10 98	40 87	200 56	MOISTURE 22.5	ORGANIC	Boring ID L
SS-150	100 RT	437+20	11.50-13.00	A-7-0(0) A-6(1)	28	11	29.5	33.6	8.6	28.3	97	83	39	18.9	 	
SS-151	100 RT	437+20	14.00-15.50	A-6(3)	37	15	26.7	29.5	11.4	32.4	97	84	45	10.5		
SS-152	100 RT	437+20	16.50-18.00	A-5(2)	45	5	21.0	32.4	32.5	14.2	98	87	53	81.2	-	Ī
SS-153	100 RT	437+20	19.00-20.50	A-7-5(32)	66	31	4.7	15.8	47.2	32.4	100	98	86		-	L
SS-154	180 RT	436+90	3.50-5.00	A-7-6(7)	44	18	25.1	23.9	14.7	36.4	97	83	53			L
SS-155	60 LT	437+50	8.90-10.40	A-6(3)	38	13	24.9	29.3	17.5	28.3	98	86	48	•	-	L
SS-156	60 LT	437+50	13.90-15.40	A-7-5(16)	58	25	18.6	18.8	14.1	48.5	99	89	64	•	•	L
SS-157	60 LT	437+50	18.90-20.40	A-7-6(8)	52	25	25.7	27.5	12.4	34.4	95	81	48		•	L
SS-158	130 LT	437+50	0.00-1.50	A-5(1)	43	8	27.9	36.2	19.7	16.2	99	83	42		•	L
SS-159 SS-160	130 LT	437+50 437+50	4.20-5.70 9.20-10.70	A-5(0) A-5(0)	46 55	NP NP	31.8 27.3	41.5 46.0	20.6 18.6	6.1 8.1	98	80	36	<u> </u>		L
SS-160	120 RT	436+50	3.80-5.30	A-6(3)	36	14	29.1	30.0	12.6	28.3	99	84	44	-	-	
SS-163	120 RT	436+50	8.80-10.30	A-7-5(10)	56	20	21.5	26.9	13.2	38.5	100	90	56			
SS-164	90 RT	439+60	3.70-5.20	A-2-6(1)	36	16	31.4	36.0	6.3	26.3	88	73	32			Ī
SS-165	90 RT	439+60	8.70-10.20	A-4(0)	36	8	24.7	45.5	15.6	14.2	97	85	38	-		L
SS-166	100 RT	444+00	4.00-5.50	A-7-5(12)	57	12	7.5	26.7	27.3	38.5	99	96	72			L
SS-167	100 RT	444+00	9.00-10.50	A-7-5(12)	57	12	8.1	28.1	33.4	30.4	100	96	72	-		L
SS-168	40 RT	20+20	3.60-5.10	A-7-5(26)	68	27	6.3	19.2	21.9	52.6	100	97	79		•	Y2
SS-169	40 RT	20+20	8.60-10.10	A-7-5(15)	61	21	8.1	30.4	23.1	38.5	100	96	67	-	•	Y2
SS-170	40 RT	20+20	13.60-15.10	A-5(4)	56	8 ND	9.7	45.1	26.9	18.2	98	93	53	<u> </u>	•	Y2
SS-171 SS-172	40 RT 40 RT	20+20 20+20	18.60-20.10 23.60-25.10	A-5(0) A-5(0)	52 51	NP NP	12.1	57.1 58.3	16.6 16.6	14.2 12.1	100 99	97	40 38	-	•	Y2 Y2
SS-172 SS-173	40 RT	20+20	28.60-25.10	A-5(0)	43	4 4	26.3	36.6	24.9	12.1	99	82	38 42	-		Y2 Y2
SS-173	40 RT	20+20	33.60-35.10	A-2-5(0)	41	NP	37.0	36.2	18.6	8.1	96	72	33	 		Y2
SS-175	40 RT	20+20	38.60-40.10	A-2-4(0)	35	NP	22.3	56.1	13.6	8.1	98	87	30	 	- : -	Y2
SS-176	110 RT	451+50	4.00-5.50	A-5(0)	44	NP	25.3	42.5	11.9	20.2	98	85	38	 -	-	L
SS-177	110 RT	451+50	9.00-10.50	A-2-5(0)	46	NP	32.4	44.9	12.6	10.1	98	82	28		-	L
SS-178	110 RT	451+50	14.00-15.50	A-2-5(0)	60	NP	35.4	42.5	14.0	8.1	99	90	27	34.4	•	L
SS-179	110 RT	451+50	19.00-21.50	A-2-5(0)	42	NP	34.2	43.3	16.4	6.1	63	52	18			L
SS-180	CL	453+50	3.30-4.80	A-7-5(5)	53	13	19.8	33.5	18.4	28.3	99	88	51			L
SS-181	CL	453+50	8.30-9.80	A-5(1)	58	8	17.6	47.7	18.6	16.2	100	92	41	<u> </u>		L.
SS-182	CL	453+50	13.30-14.80	A-2-5(0)	45	NP	23.2	52.5	18.2	6.1	100	87	35	· ·		L
SS-183 SS-184	CL CL	453+50 453+50	18.30-19.80 28.30-29.80	A-2-4(0) A-2-5(0)	33 42	NP NP	23.4	58.4 54.1	12.1 15.4	6.1 6.1	98 99	87 88	25 28	47.4	-	L L
SS-185	CL	453+50	33.30-34.80	A-2-3(0) A-2-4(0)	23	NP	44.6	40.6	10.7	4.0	83	67	17	47.1		L
SS-186	CL	456+50	3.60-5.10	A-2-4(0)	33	NP	27.5	46.9	9.5	16.2	100	91	23	 		
SS-187	CL	456+50	13.60-15.10	A-2-4(0)	24	NP	26.3	52.1	11.5	10.1	77	68	22	 	<u> </u>	
SS-188	CL	456+50	18.60-20.10	A-2-4(0)	26	NP	39.6	45.5	8.9	6.1	65	52	13			Ī
SS-189	CL	456+50	33.60-35.10	A-2-5(0)	41	NP	36.8	51.3	7.9	4.0	99	85	17	29.1		L
SS-190	CL	459+50	3.80-5.30	A-2-4(0)	38	9	43.0	28.3	8.5	20.2	97	72	31			L
SS-191	CL	459+50	8.80-10.30	A-7-5(2)	52	13	35.8	28.5	13.5	22.2	98	73	40	•	•	L
SS-192	CL	459+50	18.80-20.30	A-4(0)	39	4	30.3	32.9	26.7	10.1	96	77	43			L
SS-193	CL	459+50	28.80-30.30	A-2-4(0)	38	NP	37.4	34.5	18.0	10.1	94	72	32	14.3	•	L
SS-194	50 RT	462+75	3.50-5.00	A-7-5(15)	57	22	18.8	17.8	21.0	42.4	99	87	67		•	L L
SS-195	50 RT	462+75	8.50-10.00	A-5(0)	43	6	32.1	35.6	24.2	8.1	94	74	40	<u> </u>	•	L
SS-196 SS-197	50 RT 50 RT	462+75 462+75	18.50-20.00 28.50-30.00	A-5(0)	41	NP NP	24.8 33.1	40.6 35.6	26.5 23.2	8.1	100	87	44	- 22.2	<u> </u>	L
SS-197	50 KT	466+00	4.00-5.50	A-5(0) A-2-5(0)	43	NP NP	33.1	39.8	16.2	8.1 10.1	98	76 79	39 32	23.2		L
SS-190	50 LT	466+00	9.00-10.50	A-2-5(0) A-5(1)	44	5	25.3	37.4	21.2	16.2	99	84	46			
SS-200	50 LT	466+00	19.00-20.50	A-5(1)	44	6	25.9	37.0	23.0	14.1	99	83	45	-	-	L
SS-201	50 LT	466+00	29.00-30.50	A-2-4(0)	39	NP	26.9	53.9	11.1	8.1	98	87	26	-		L
SS-202	CL	469+00	3.90-5.40	A-2-4(0)	40	5	37.8	30.3	17.8	14.1	89	65	34	-	-	ī
SS-203	CL	469+00	8.90-10.40	A-2-4(0)	30	NP	41.2	43.4	13.3	2.0	93	73	20	10.9		L
SS-204	CL	469+00	13.90-15.40	A-2-4(0)	32	NP	48.5	35.6	9.9	6.1	88	60	19	9.1	•	L
SS-205	CL	469+00	18.90-20.40	A-2-5(0)	42	NP	44.4	40.0	9.5	6.1	88	63	18	•	•	L
SS-206	15 LT	471+85	4.00-5.50	A-7-5(15)	57	21	18.4	16.4	10.7	54.5	99	88	67			L
SS-207	15 LT	471+85	9.00-10.50	A-7-6(10)	53	25	27.1	20.4	10.1	42.4	96	79	53		· .	L
SS-208	15 LT	471+85	14.00-15.50	A-7-6(7)	51	23	31.3	22.4	11.9	34.3	92	72	46			L
SS-209 SS-210	15 LT 15 LT	471+85 471+85	19.00-20.50	A-2-5(0)	58 46	NP NP	38.7	48.5	6.7	6.1	100	86	17	<u> </u>	<u> </u>	L
SS-210 SS-211	CL	4/1+85 475+50	29.00-30.50 0.50-2.00	A-2-5(0) A-7-5(17)	54	17	40.6 10.9	44.0 11.5	9.3	6.1 38.4	98	78 93	21 80	-	-	L
SS-211	CL	475+50	2.00-3.50	A-7-5(17)	51	27	5.9	19.0	22.6	52.5	100	98	78		-	L
SS-212	CL	475+50	3.70-5.20	A-7-0(22) A-2-4(0)	26	7	22.4	48.7	12.7	16.2	100	93	34	 	 	1
SS-214	CL	475+50	6.20-7.70	A-2-4(0)	22	NP	60.2	26.3	5.5	8.1	98	64	15	 	-	l i
SS-215	CL	475+50	8.70-10.20	A-7-5(9)	51	15	17.4	28.5	31.9	22.2	99	91	60		-	
S-216	25 LT	25+00	0.00-4.00	A-4(0)	29	10	23.6	32.9	15.2	28.3	76	66	36			Y2
SS-216	25 RT	20+25	0.50-2.00	A-6(3)	33	16	25.4	34.7	9.4	30.5	97	84	42	20.0	-,	ΥI
S-217	25 RT	15+00	0.00-4.00	A-7-5(33)	83	35	9.9	14.3	3.0	72.7	99	93	77			Y2
SS-217	25 RT	20+25	4.30-5.80	A-7-5(17)	65	22	8.5	29.0	15.7	46.7	100	96	68	20.2		ΥI
SS-218	25 RT	20+25	9.30-10.80	A-5(0)	51	5	14.2	56.2	11.3	18.3	99	92	40			ΥI
SS-219	25 RT	18+00	0.50-2.00	A-7-6(20)	62	34	15.6	24.2	7.4	52.8	100	92	63	27.9		ΥI
00 000	25 RT	18+00	4.10-5.60	A-7-5(16)	70	27	13.4	32.3	15.7	38.6	99	93	60	24.4	•	ΥI
SS-220 SS-221	25 RT	18+00	9.10-10.60	A-5(0)	47	5	11.8	59.1	17.0	12.2	100	96	42			Υl

	SOIL TEST RESULTS															
SAMPLE			DEPTH	AASHTO				% BY W	/EIGHT		% PAS	SING (S	IEVES)	%	%	Line or
NO.	OFFSET	STATION	INTERVAL	CLASS.	L.L.	P.I.	C.SAND	F.SAND	SILT	CLAY	10	40	200	MOISTURE	ORGANIC	Boring ID
SS-222	50 LT	36+65	0.50-2.00	A-7-5(20)	63	33	14.0	24.6	8.6	52.8	100	93	64	38.7	•	ΥI
SS-223	50 LT	36+65	3.70-5.20	A-7-5(6)	55	13	15.6	37.2	14.7	32.5	99	92	52	26.5	•	ΥI
SS-224	50 LT	36+65	8.70-10.20	A-2-5(0)	48	6	15.8	59.5	14.5	10.2	100	95	34		•	ΥI
CBR-1	50 LT	36+00	18.00-20.00	A-4(0)	40	5	16.2	51.1	20.6	12.1	98	90	40		-	Y1RPB