

NOTE: SEE SHEET 1A FOR PLAN SHEET LAYOUT AT TIME OF INVESTIGATION

STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-2707C	1	277
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
34497.1.4	NHF-74(14)	P.E.	
		RW & UTIL.	

CONTENTS

LINE	STATION	PLAN	PROFILE	XSECT
-L-	353+22.84-635+00.00	4-28	47-64	97-255
RAMP A @ -Y1-	0+00.00-21+11.85	5-6	65	256-258
RAMP D @ -Y1-	0+00.00-23+72.31	5-6	66	
LOOP A @ -Y1-	0+00.00-11+20.63	5	67	259-263
LOOP D @ -Y1-	0+00.00-11+72.36	5	67	264
RAMP A @ -Y9-	0+00.00-20+93.98	19-20	68	
RAMP B @ -Y9-	0+00.00-19+96.30	18-19	69	
RAMP C @ -Y9-	0+00.00-16+26.54	18-19	70	
RAMP D @ -Y9-	0+00.00-16+16.51	19-20	71	
LOOP B @ -Y9-	0+00.00-12+88.76	19	72	
RAMP A @ -Y14-	0+00.00-18+05.44	25-26	73	
RAMP A1 @ -Y14-	2+01.97-5+95.56	25	74	
RAMP B @ -Y14-	0+00.00-12+78.33	24-25	75	
RAMP B1 @ -Y14-	1+09.68-6+69.55	25	75	
RAMP C @ -Y14-	0+00.00-12+89.44	24-25	76	
RAMP C1 @ -Y14-	0+00.00-3+45.69	25	77	
RAMP D @ -Y14-	0+00.00-16+87.22	25-26	78	
RAMP D1 @ -Y14-	1+47.61-3+98.6	25	79	
-Y1-	11+90.00-42+40.00	5, 28-29	80-81	
-Y2-	23+85.00-33+25.00	7, 30	82	
-Y3-	17+90.00-25+54.02	12, 31-32	82	
-Y4-	15+02.00-34+76.31	14, 33-34	83	
-Y6A-	10+00.00-19+41.19	17, 46	84	
-Y8A-	33+00.00-35+96.71	38	86	
-Y8- REV	10+32.02-36+00.00	36-38	85	
-Y9-	10+70.00-36+00.00	19, 35-36	87	
-Y11-	26+00.00-69+75.00	23-24, 41, 43-44	88-89	
-Y14-	12+50.00-56+76.76	25, 39-42	90-91	
-Y16- REV	10+00.00-20+09.90	40, 45	92	
-Y16A-	13+50.00-15+00.65	45	93	
-Y17-	10+20.47-38+40.15	5-6, 29	94-95	
-Y18-	12+00.00-16+56.58	14, 34	96	
-Y1- DETOUR	12+64.08-27+35.00	5, 28		
-Y9- DETOUR	11+98.88-23+44.80	19		
SAMPLE RESULTS		265-267		
CORE PHOTOS		268-277		

ROADWAY  
SUBSURFACE INVESTIGATION

PROJ. REFERENCE NO. 34497.1.2 (R-2707C) F.A. PROJ. NHF-74(14)  
COUNTY CLEVELAND  
PROJECT DESCRIPTION US 74 SHELBY BYPASS FROM WEST OF NC 226 TO EAST OF NC 150

INVENTORY

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING, AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES, AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 250-4088. NEITHER THE SUBSURFACE PLANS AND REPORTS, NOR THE FIELD BORING LOGS, ROCK CORES, OR SOIL TEST DATA ARE PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION, AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THIS PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

PERSONNEL

R. W. TODD

J. P. ROGERS

M. L. SMITH

C. E. BURRIS

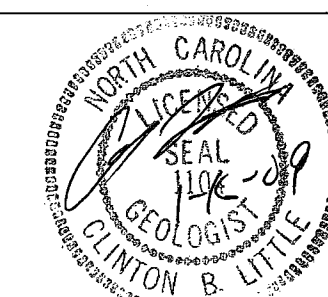
A. C. SMITH

INVESTIGATED BY J. P. ROGERS

CHECKED BY C. B. LITTLE

SUBMITTED BY C. B. LITTLE

DATE NOVEMBER 2008



DRAWN BY: J. P. ROGERS & C. E. BURRIS

NOTE - THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS BEING ACCURATE NOR IS IT CONSIDERED TO BE PART OF THE PLANS, SPECIFICATIONS, OR CONTRACT FOR THE PROJECT.

NOTE - BY HAVING REQUESTED THIS INFORMATION THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

ID: R-2707C

CONTRACT:

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

PROJECT REFERENCE NO.  
R-2707C

SHEET NO.  
2

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION	GRADATION	ROCK DESCRIPTION	TERMS AND DEFINITIONS
SOIL IS CONSIDERED TO BE THE UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER, AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO STANDARD PENETRATION TEST (ASTM D-1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY SHALL INCLUDE: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. EXAMPLE: <i>VERY STIFF, BRN. SCLY CLAY, MOST WITH INTERBEDDED FINE SAND LAYERS, HIGH PLASTIC, A-7-6</i>	WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORM - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. (ALSO POORLY GRADED) GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLES OF TWO OR MORE SIZES.  ANGULARITY OF GRAINS THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.  MINERALOGICAL COMPOSITION MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHENEVER THEY ARE CONSIDERED OF SIGNIFICANCE.  COMPRESSIBILITY SLIGHTLY COMPRESSIBLE LIQUID LIMIT LESS THAN 31 MODERATELY COMPRESSIBLE LIQUID LIMIT EQUAL TO 31-50 HIGHLY COMPRESSIBLE LIQUID LIMIT GREATER THAN 50  PERCENTAGE OF MATERIAL ORGANIC MATERIAL GRANULAR SILT - CLAY OTHER MATERIAL TRACE OF ORGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10% LITTLE ORGANIC MATTER 3 - 5% 5 - 12% LITTLE 10 - 20% MODERATELY ORGANIC 5 - 10% 12 - 20% SOME 20 - 35% HIGHLY ORGANIC >10% >20% HIGHLY 35% AND ABOVE  GROUND WATER ▽ WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING ▽ PW STATIC WATER LEVEL AFTER 24 HOURS ▽ PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA ○ SPRING OR SEEP  MISCELLANEOUS SYMBOLS ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION SOIL SYMBOL ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT INFERRED SOIL BOUNDARY INFERRED ROCK LINE ALLUVIAL SOIL BOUNDARY DIP & DIP DIRECTION OF ROCK STRUCTURES SOUNDING ROD SPT TEST BORING AUGER BORING CORE BORING MONITORING WELL PIEZOMETER INSTALLATION SLOPE INDICATOR INSTALLATION SPT N-VALUE SPT REFUSAL	HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT IF TESTED, WOULD YIELD SPT REFUSAL, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:  WEATHERED ROCK (WR) CRYSTALLINE ROCK (CR) NON-CRYSTALLINE ROCK (NCR) COASTAL PLAIN SEDIMENTARY ROCK (CP)  WEATHERING FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE. VERY SLIGHT (V SL.) ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN, CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE. SLIGHT (SL.) ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE OULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS. MODERATE (MOD.) SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE OULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS OULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK. MODERATELY SEVERE (MOD. SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS OULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. IF TESTED, WOULD YIELD SPT REFUSAL. SEVERE (SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. IF TESTED, YIELDS SPT N VALUES > 100 BPF. VERY SEVERE (V SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT THE MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE SUCH THAT ONLY MINOR VESTIGES OF THE ORIGINAL ROCK FABRIC REMAIN. IF TESTED, YIELDS SPT N VALUES < 100 BPF. COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.  ROCK HARDNESS VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK. HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN. MODERATELY HARD CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES DR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS. MEDIUM HARD CAN BE GROVED OR GOUGED 0.25 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PEICES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK. SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE. VERY SOFT CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH DR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.  ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARGILLACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. 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STRATA ROCK QUALITY DESIGNATION (SRQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.	
<b>SOIL LEGEND AND AASHTO CLASSIFICATION</b> GENERAL CLASS. GRANULAR MATERIALS (<= 35% PASSING #200) SILT-CLAY MATERIALS (> 35% PASSING #200) ORGANIC MATERIALS GROUP CLASS. A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5 A-6, A-7 SYMBOL [Diagrams showing soil patterns for A-1, A-3, A-2, A-4, A-5, A-6, A-7, A-1, A-2, A-4, A-5, A-6, A-7] % PASSING: 10, 40, 200 (mm) [Diagrams showing sieve analysis patterns] LIQUID LIMIT PLASTIC INDEX [Diagrams showing LL and PI patterns] GROUP INDEX [Diagrams showing GI patterns] USUAL TYPES OF MAJOR MATERIALS: STONE FRAGS, GRAVEL AND SAND, FINE SAND, SILTY OR CLAYEY GRAVEL AND SAND, SILTY SOILS, CLAYEY SOILS GENERATING AS A SUBGRADE: EXCELLENT TO GOOD, FAIR TO POOR, POOR, UNSUITABLE PI OF A-7-5 SUBGROUP IS ≤ LL - 30; PI OF A-7-6 SUBGROUP IS > LL - 30	<b>TEXTURE OR GRAIN SIZE</b> U.S. STD. SIEVE SIZE OPENING (MM): 4, 10, 40, 60, 200, 270 COEFFICIENTS: 4.76, 2.00, 0.42, 0.25, 0.075, 0.053 BOULDER (BLDR.), COBBLE (COB.), GRAVEL (GR.), COARSE SAND (CS. SD.), FINE SAND (F. SD.), SILT (SL.), CLAY (CL.) GRAIN SIZE: MM 305, 75, 2.0, 0.25, 0.05, 0.005; IN. 12, 3, 0.075, 0.01, 0.002, 0.0002	<b>WEATHERED ROCK (WR)</b> CRYSTALLINE ROCK (CR) NON-CRYSTALLINE ROCK (NCR) COASTAL PLAIN SEDIMENTARY ROCK (CP) <b>WEATHERING</b> FRESH VERY SLIGHT (V SL.) SLIGHT (SL.) MODERATE (MOD.) MODERATELY SEVERE (MOD. SEV.) SEVERE (SEV.) VERY SEVERE (V SEV.) COMPLETE <b>ROCK HARDNESS</b> VERY HARD HARD MODERATELY HARD MEDIUM HARD SOFT VERY SOFT	<b>TERMS AND DEFINITIONS</b> ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARGILLACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SREC) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SRQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
<b>CONSISTENCY OR DENSENESS</b> PRIMARY SOIL TYPE COMPACTNESS OR CONSISTENCY RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE) RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> ) GENERALLY GRANULAR MATERIAL (NON-COHESIVE) VERY LOOSE, LOOSE, MEDIUM DENSE, DENSE, VERY DENSE 4 TO 10, 10 TO 30, 30 TO 50, >50 N/A GENERALLY SILT-CLAY MATERIAL (COHESIVE) VERY SOFT, MEDIUM STIFF, STIFF, VERY STIFF, HARD <2, 2 TO 4, 4 TO 8, 8 TO 15, 15 TO 30, >30 0.25 TO 0.50, 0.5 TO 1.0, 1 TO 2, 2 TO 4, >4	<b>ABBREVIATIONS</b> AR - AUGER REFUSAL BT - BORING TERMINATED CL - CLAY CPT - CONE PENETRATION TEST CSE - COARSE DHT - DILATOMETER TEST DPT - DYNAMIC PENETRATION TEST F - FINE FOSS. - FOSSILIFEROUS FRAC. - FRACTURED, FRACTURES FRAGS. - FRAGMENTS HL - HIGHLY MED. - MEDIUM MICA - MICACEOUS MOD. - MODERATELY NP - NON PLASTIC ORG. - ORGANIC PMT - PRESSUREMETER TEST SAP. - SAPROLITIC SD. - SAND, SANDY SL. - SILT, SILTY SLI. - SLIGHTLY TCR - TRICONE REFUSAL # - MOISTURE CONTENT V - VERY VST - VANE SHEAR TEST WEA. - WEATHERED W - UNIT WEIGHT W <sub>d</sub> - DRY UNIT WEIGHT	<b>FRACATURE SPACING</b> TERM SPACING VERY WIDE MORE THAN 10 FEET WIDE 3 TO 10 FEET MODERATELY CLOSE 1 TO 3 FEET CLOSE 0.75 TO 1 FEET VERY CLOSE LESS THAN 0.75 FEET <b>BEDDING</b> TERM THICKNESS VERY THICKLY BEDDED > 4 FEET THICKLY BEDDED 1.5 - 4 FEET THINLY BEDDED 0.16 - 1.5 FEET VERY THINLY BEDDED 0.03 - 0.16 FEET THICKLY LAMINATED 0.008 - 0.03 FEET THINLY LAMINATED < 0.008 FEET <b>INDURATION</b> FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF THE MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC. FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE. MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER. INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER. EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.	<b>EQUIPMENT USED ON SUBJECT PROJECT</b> DRILL UNITS: [X] MOBILE B-57, BK-51, CME-45C, [X] CME-550, PORTABLE HOIST ADVANCING TOOLS: [X] CLAY BITS, [X] 6" CONTINUOUS FLIGHT AUGER, [X] 8" HOLLOW AUGERS, [X] HARD FACED FINGER BITS, [X] TUNG-CARBIDE INSERTS, [X] CASING [X] W/ ADVANCER, [X] TRICONE * STEEL TEETH, [X] TRICONE * TUNG-CARB., [X] CORE BIT HAMMER TYPE: [X] AUTOMATIC [ ] MANUAL CORE SIZE: [ ] B, [X] N-0, [ ] H HAND TOOLS: [X] POST HOLE DIGGER, [X] HAND AUGER, [X] SOUNDING ROD, [ ] VANE SHEAR TEST
<b>PLASTICITY</b> NONPLASTIC LOW PLASTICITY MED. PLASTICITY HIGH PLASTICITY PLASTICITY INDEX (PI) DRY STRENGTH VERY LOW SLIGHT MEDIUM HIGH 0-5, 6-15, 16-25, 26 OR MORE	<b>COLOR</b> DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.	<b>NOTES:</b> BENCH MARK: _____ ELEVATION: _____ FT. _____	



STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION

MICHAEL F. EASLEY  
GOVERNOR

LYNDO TIPPETT  
SECRETARY

November 20, 2008

STATE PROJECT: 34497.1.2 (R-2707C)  
FEDERAL PROJECT: NHF-74(14)  
COUNTY: Cleveland  
DESCRIPTION: US 74 Shelby Bypass from West of NC 226 to East of NC 150

SUBJECT: Geotechnical Report - Inventory

**PROJECT DESCRIPTION**

This project is located in south central Cleveland County, approximately six miles north of the city of Shelby. The -L- line is on new location for the entire project. Typical sections for the proposed -L- line call for a four-lane roadway with paved shoulders. Median width is 34'. There are three proposed interchanges that will connect the -L- alignment with existing NC 226, existing NC 18, and existing NC 150. A total of seven bridges are included in the scope of this project. Four of these bridges will be required for grade separations at -Y2-, -Y3-, -Y4-, and -Y9- over -L-. A dual structure water crossing is proposed at -L- line over the Broad River. The last two bridges will be required for railroad separation (-L- and -Y11- over -Y13-, CSX RR). The -L- alignment runs generally west to east. The following alignments were investigated:

<u>Line</u>	<u>Station(s)</u>
-L-	351+75.00 to 635+00.00 (5.38 miles)
Ramp A (RP A1) at NC 226	0+00.00 to 21+11.85 (0.40 miles)
Ramp D (RP D1) at NC 226	0+00.00 to 23+72.31 (0.45 miles)
Loop A (LP A1) at NC 226	0+00.00 to 11+20.63 (0.21 miles)
Loop D (LP D1) at NC 226	0+00.00 to 11+72.36 (0.22 miles)
Ramp A (RP A2) at NC 18	0+00.00 to 20+93.98 (0.40 miles)
Ramp B (RP B2) at NC 18	0+00.00 to 19+96.30 (0.38 miles)

MAILING ADDRESS:  
NC DEPARTMENT OF TRANSPORTATION  
GEOTECHNICAL ENGINEERING UNIT  
1589 MAIL SERVICE CENTER  
RALEIGH NC 27699-1589

TELEPHONE: 919-250-4088  
FAX: 919-250-4237

WEBSITE: WWW.DOH.DOT.STATE.NC.US

LOCATION:  
CENTURY CENTER COMPLEX  
ENTRANCE B-2  
1020 BIRCH RIDGE DRIVE  
RALEIGH NC

Ramp C (RP C2) at NC 18	0+00 to 16+26.54 (0.31 miles)
Ramp D (RP D2) at NC 18	0+00 to 16+16.61 (0.31 miles)
Loop B (LP B2) at NC 18	0+00 to 12+88.76 (0.24 miles)
Ramp A (RP A3) at NC 150	0+00 to 13+93.46 (0.26 miles)
Ramp B (RP B3) at NC 150	0+00 to 14+14.00 (0.27 miles)
Ramp C (RP C3) at NC 150	0+00 to 13+94.92 (0.26 miles)
Loop C (LP C3) at NC 150	0+00 to 8+66.03 (0.16 miles)
-Y1-	11+90.00 to 42+40.00 (0.58 miles)
-Y2-	23+85.00 to 33+25.00 (0.18 miles)
-Y3-	17+90.00 to 25+54.02 (0.14 miles)
-Y4-	15+02.00 to 34+76.31 (0.37 miles)
-Y8-	10+32.02 to 36+00.00 (0.49 miles)
-Y9-	10+70.00 to 36+00.00 (0.48 miles)
-Y11-	26+00.00 to 69+75.00 (0.83 miles)
-Y14-	22+00.00 to 49+00.00 (0.51 miles)
-Y15-	17+65.30 to 26+96.37 (0.18 miles)
-Y17- at SR 1	10+20.47 to 38+40.15 (0.53 miles)

The total length of lines investigated is 13.54 miles.

The initial field investigation was conducted between October 2005 and April 2006. Borings were conducted with a CME-550 drill machine with an automatic hammer. Standard Penetration Tests were conducted at selected locations utilizing hollow stem augers and additional borings were advanced with 6" continuous flight augers. Various hand tools (hand auger, drive rods) and visual reconnaissance completed the investigation. Numerous soil samples were submitted to the Materials and Tests Unit for laboratory analysis.

**AREAS OF SPECIAL GEOTECHNICAL INTEREST**

**Crystalline Rock:** There is a considerable amount of hard rock on the project. Rock was encountered above or within 10' of the proposed grade at the following locations:

<u>Line</u>	<u>Station(s)</u>
-L-	355+00 to 358+00
-L-	360+50 to 362+50
-L-	377+00 to 379+00
-L-	388+00 to 402+50
-L-	412+50 to 413+00
-L-	417+00 to 421+50
-L-	423+00 to 424+00
-L-	428+50 to 438+50
-L-	439+50 to 446+50
-L-	447+50 to 450+00
-Loop A1-	1+50 to 4+50
-Ramp A1-	14+00 to 16+00
-Loop D1-	0+25 to 2+75

2 3A

The rock lines depicted on the attached cross-sections and profiles are interpolated between borings and based primarily on 8" hollow stem auger and 6" standard auger refusal. Four core borings were performed in the rock cut encountered between Stations 388+00 to 402+50 -L-. The Mica Gneiss encountered in those borings had RQD's between 21% and 100%. These borings also confirmed what the Geologic map of North Carolina had indicated would be present in the area.

In addition, there are zones of weathered rock and/or layers with alternating very hard residual soils and weathered rock that occur above the depicted rock lines. According to the Geologic map of North Carolina and our core borings, the most likely rock type within the project corridor is Biotite/Mica Gneiss metamorphic rock (CZms & CZbg). These rocks are likely to become more schistose on the western end of the project near NC 226. The rock is described on the cross-sections and profiles as *Hard Crystalline Rock - Biotite/Mica Gneiss*. As stated previously, the hardness was determined on 8" hollow stem auger refusal, 6" standard auger refusal, and core borings. In addition, the pull down pressure on the feed cylinders on the CME-550 was observed to be 800 - 1000 psi in the areas of Hollow Stem/Standard Auger refusal.

**Alluvial Soils;** Areas with significant alluvial deposits are discussed below.

**Station 365+65 to 366+35 -L-, Left;** Alluvial soils present in this location are associated with a topographical low area that serves as a drainage feature for the surrounding pasture. The deposit is approximately eight feet thick and contains very soft to medium stiff sandy silt (A-4) and very loose coarse sand (A-1-b). At the time of our investigation, groundwater was not encountered in the two borings performed in this area.

**Station 382+90 to 386+05 -L-;** The alluvial deposits in this segment are associated with the Broad River Floodplain. A dual four-lane structure has been proposed for this water crossing. No borings were performed in this interval during our Roadway investigation. These alluvial soils will be addressed in detail during the subsequent structure investigation.

**Station 503+20 to 509+00 -L-, Left;** Alluvial soils present in this location are associated with a small stream that intersects the -Y5- alignment near Station 17+00. The stream continues in an easterly direction running parallel to the -L- line at an offset of 50' - 120'. The deposit is eight to 10' thick and contains primarily very loose to loose, silty, coarse and fine sand (A-2-4). At the time of our investigation, groundwater was encountered in this area between elevations 840' and 845'.

**Station 538+15 to 539+15 -L- and 6+70 to 7+40 -Ramp D2-;** Alluvial soils present in this location are associated with a small stream that drains the area north of existing Carter Road. The stream moves in a southerly direction while bisecting the proposed -L- line and -Ramp D2-. The deposit is six to seven feet thick and contains medium stiff sandy silt (A-4), loose to medium dense silty sand (A-2-4), and soft sandy clay (A-6). At the time of our investigation, groundwater was encountered in this area between elevation 875' and 890'.

A 3B

**563+90 to 566+20 -L-;** This pond is formed by an earthen dam located right of -L- centerline and fed by surface drainage from the northeast. It is also possible that a spring located outside the construction limits could be feeding the pond as well. Please refer to plan sheet 21 of the attached inventory plans for a graphical depiction of this area. The residual soils encountered in the immediate area around the pond consist of moderate to highly plastic, medium stiff to stiff sandy clays (A-7). No alluvial soils were encountered around the pond. Based on the residual soils immediately adjacent to the pond, we estimate up to three feet of wet plastic soils in the bottom of the pond.

**Wells:** Wells were encountered within 100' of the project corridor at the following locations:

Line	Station(s)	Offset
-L-	584+00	155' Rt.
-L-	584+75	115 Lt.
-L-	599+70	120 Rt.
-L-	608+90	55' Lt.

**Plastic Clays:** Highly Plastic clays ( $PI \geq 26$ ) were encountered with six feet of proposed grade at the following locations:

Line	Station(s)	P.I.
-L-	559+50 to 561+00	38
-L-	569+00 to 573+40	36
-L-	459+25 to 460+75	31-39
-L-	497+50 to 501+00	29-35
-L-	582+30 to 583+40	33
-Y4-	21+50 to 25+50	27
-RPA2-	15+35 to 17+35	34
-Y8REV-	10+75 to 14+15	31
-Y8REV-	18+50 to 26+10	26-43
-RPA3-	7+20 to 8+55	30
-RPC3-	11+50 to 14+00	36
-LPC3-	6+00 to 8+66	36
-Y11REV-	49+15 to 50+50	30

Highly Plastic cap clays ( $PI \geq 26$ ) were encountered in the following cut sections:

Line	Station(s)	P.I.
-LPA1-	5+50,60' Lt.	29
-RPA1-	7+50 to 9+00	26
-L-	396+50 to 401+50	29
-L-	418+00 to 420+00	39
-L-	525+00 to 532+00	35
-L-	468+25 to 469+50	28
-L-	479+25 to 480+30	26
-L-	483+50 to 487+25	40

## PHYSIOLOGRAPHY AND GEOLOGY

The project is located in the southwestern piedmont region of North Carolina. The terrain is rolling hills and steep valleys with generally narrow floodplains at stream crossings. Elevation relief (from highest point to lowest point) within the entire project corridor is approximately 245'. The majority of the project is open land but there are areas where homes and businesses will be affected. Most of the wooded areas encountered in our investigation had not been logged. The entire project is within the southwestern Inner Piedmont Geological Belt. Please refer to the section above entitled "Crystalline Rock" for a more detailed description of anticipated rock types within the project corridor.

## SOIL PROPERTIES

### Residual Soils

All residual soils on the project are derived from the Biotite/Mica Gneiss rocks previously discussed. The dominant soil types encountered are silty and sandy clay (A-6, A-7), silty sand (A-2-4, A-1-b) and sandy silts (A-4, A-5). In areas where rock above grade was encountered, the clays tended to be cap clays extending up to 10' below the ground surface. It is in these areas of hard rock that the predominant soil is silty sand (A-2-4) with alternating zones of dense residual soil and weathered rock. A large majority of the residual silty sands encountered on this project were observed to be micaceous.

## CULVERTS

### Station 453+03 -L-

The proposed structure is a 2 @ 7' x 7" RCBC, Overall length = 3247. Five test borings were conducted in the vicinity of the proposed structure. The floor elevation, moving left to right, varies from 768.40' to 772.30'. The borings indicate that sandy residual soils are present near the proposed floor elevation. Weathered rock was encountered between elevation 761' - 766' in the three closest borings to the structure. Floodplain soils in the area consist of clayey and silty sands approximately ten feet or less in thickness.

### Station 553+29 -L-

The proposed structure is a 2 @ 8' x 7' RCBC, Overall length = 330'. Two borings conducted in the vicinity indicate the top of residual soil between elevation 861' - 866'. The proposed culvert has an inlet elevation = 864.8' and an outlet elevation = 861.0'. Three to nine feet of alluvial silts were present across this location. The culvert will be founded primarily on residual soil consisting of soft -to medium stiff sandy silt and very loose silty sand. We estimate very soft to soft alluvial silts extending down to elevation 860.50' at Station 553+50 -L-, 55' Lt. Neither weathered nor hard rock was encountered at this location.

**Groundwater:** Groundwater can occur at or very near the ground surface in floodplain areas. Groundwater will also be present in some of the cut sections. The profiles and cross-sections in the areas of rock above grade could be misleading because most of the auger borings did not penetrate deep enough to reach proposed grade. We anticipate that groundwater could occur above proposed grade in the following intervals:

Line	Station(s)
-L-	358+00 to 361+00
-L-	421+50 to 422+50
-L-	467+50 to 471+00
-L-	481+00 to 485+00
-L-	525+00 to 531+00
-Ramp A1-	1+00 to 8+00
-Loop A1-	4+00 to 8+00

### Artificial Fill/Roadway Fill:

Station 613+15 to 616+75 —L-: This interval falls within the proposed interchange of alignment -L- and NC 150 at the easternmost portion of the project. The artificial fill soils encountered in this segment are approximately three to 11' thick and consist primarily of stiff to very stiff sandy clay (A-7, A-6). Please refer to Plan Sheet 25 of the attached Inventory Plans to view the extent of these soils left and right of centerline -L-. All other soils encountered in the immediate vicinity of these fill materials were residual clays. In addition, this area is currently being used by the NCDOT as a place to stockpile soil for use in road building activities. Due to the extremely dynamic nature of the materials that are either being taken out or brought in, none of the stockpiles we observed at the time of our investigation were mapped.

Due to the presence of utilities and high traffic volumes, none of the existing roadway fill soils along any of the proposed alignments were investigated by drilling. However, visual reconnaissance of side slopes and existing pavement was performed. No problems were observed with the existing roadway soils except for some minor erosion on the steeper side slopes.

**Ponds:** Three ponds were encountered within the project corridor at the following locations:

439+00 -L-, 160' right. This pond is approximately 60' south of the slope stake line at this location. The drainage outlet for this pond bisects the -L- line at Station 438+90 -L-. Alluvial soils associated with this drainage path are estimated to be five feet thick. Based on the rock line in the two cuts adjacent to this stream, we estimate that hard rock will be encountered below the stream between elevation 780' and 785'.

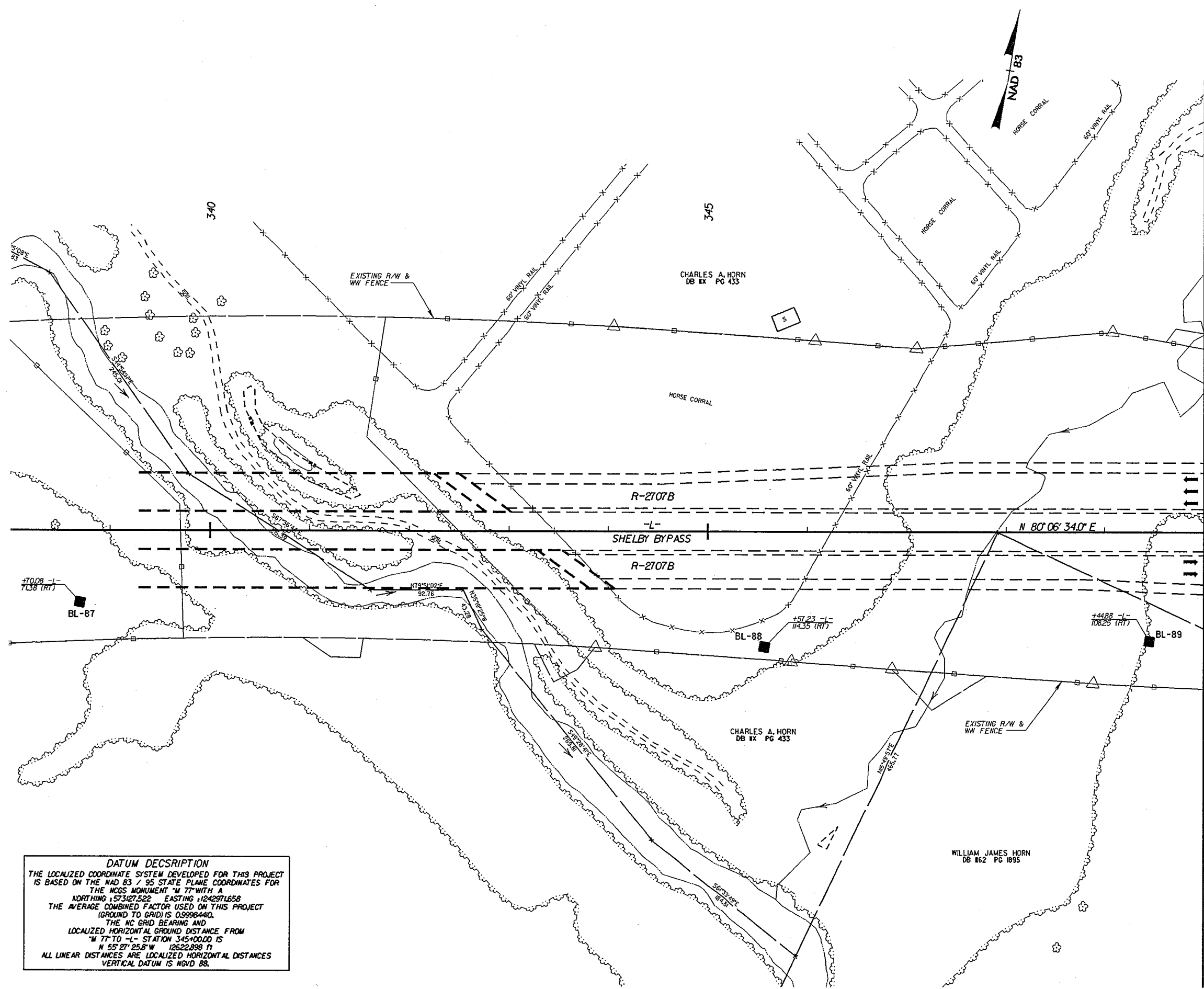
503+50 -L-, 100' right. At the time of our investigation, this pond had been drained. The water feeding into the pond appears to be coming primarily from surface drainage. It is also possible that a spring located outside the construction limits could be feeding the pond as well. Three to 11' of alluvial materials were encountered at the edge of the pond and downstream of the outlet, respectively. These materials consist of very loose silty sands (A-2-4) and very soft silt clays (A-7). Please refer to the attached profiles and cross-sections for a detailed, graphical depiction of this area.

Respectfully submitted,

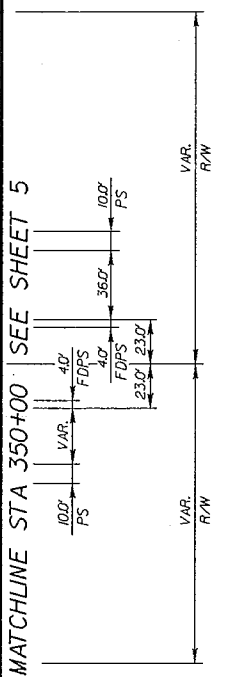


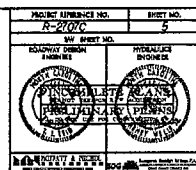
John P. Rogers  
Project Geological Engineer

PROJECT REFERENCE NO. R-2707C	SHEET NO. 4
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
PRELIMINARY PLANS NOT TO BE USED FOR CONSTRUCTION	
HOFFATT & NICHOL 14 N. EAST HILLSIDE ROAD, SUITE 100 RALEIGH, NORTH CAROLINA 27605 919.871.4525 FAX 919.871.4525	SDG Sungate Design Group, P.A. 100 S. JONES FREDERICK BL. RANDOLPH, NORTH CAROLINA 28134 704.781.7300



**DATUM DESCRIPTION**  
 THE LOCALIZED COORDINATE SYSTEM DEVELOPED FOR THIS PROJECT IS BASED ON THE NAD 83 / 95 STATE PLANE COORDINATES FOR THE NCGS MONUMENT "M 77" WITH A NORTHING: 1573127.522 EASTING: 1242971.658 THE AVERAGE COMBINED FACTOR USED ON THIS PROJECT (GROUND TO GRID) IS 0.99984410.  
 THE NC GRID BEARING AND LOCALIZED HORIZONTAL GROUND DISTANCE FROM "M 77" TO -L- STATION 345+00.00 IS N 55° 27' 25.8" W 12622.898 FT  
 ALL LINEAR DISTANCES ARE LOCALIZED HORIZONTAL DISTANCES VERTICAL DATUM IS NGVD 88.





PROJECT APPROVAL NO.	R-2707C
PROJECT NAME	INTERCHANGE AT I-74 BYPASS AND -YI- NC 226
DATE	5/29/02

RAMP -A-			
PI STA 3400.00	PI STA 3400.00	PI STA 3400.00	PI STA 3400.00
Δ = 30.00	Δ = 30.00	Δ = 30.00	Δ = 30.00
L = 300.00	L = 300.00	L = 300.00	L = 300.00
E = 1.00	E = 1.00	E = 1.00	E = 1.00
SE = 28	SE = 28	SE = 28	SE = 28

LOOP -A-			
PI STA 3400.00	PI STA 3400.00	PI STA 3400.00	PI STA 3400.00
Δ = 30.00	Δ = 30.00	Δ = 30.00	Δ = 30.00
L = 300.00	L = 300.00	L = 300.00	L = 300.00
E = 1.00	E = 1.00	E = 1.00	E = 1.00
SE = 28	SE = 28	SE = 28	SE = 28

RAMP -B-			
PI STA 3400.00	PI STA 3400.00	PI STA 3400.00	PI STA 3400.00
Δ = 30.00	Δ = 30.00	Δ = 30.00	Δ = 30.00
L = 300.00	L = 300.00	L = 300.00	L = 300.00
E = 1.00	E = 1.00	E = 1.00	E = 1.00
SE = 28	SE = 28	SE = 28	SE = 28

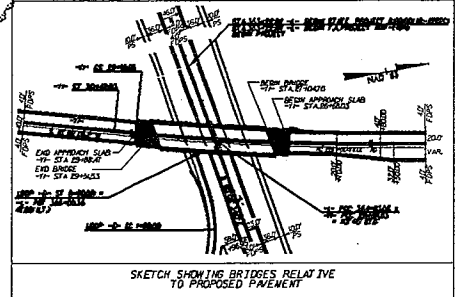
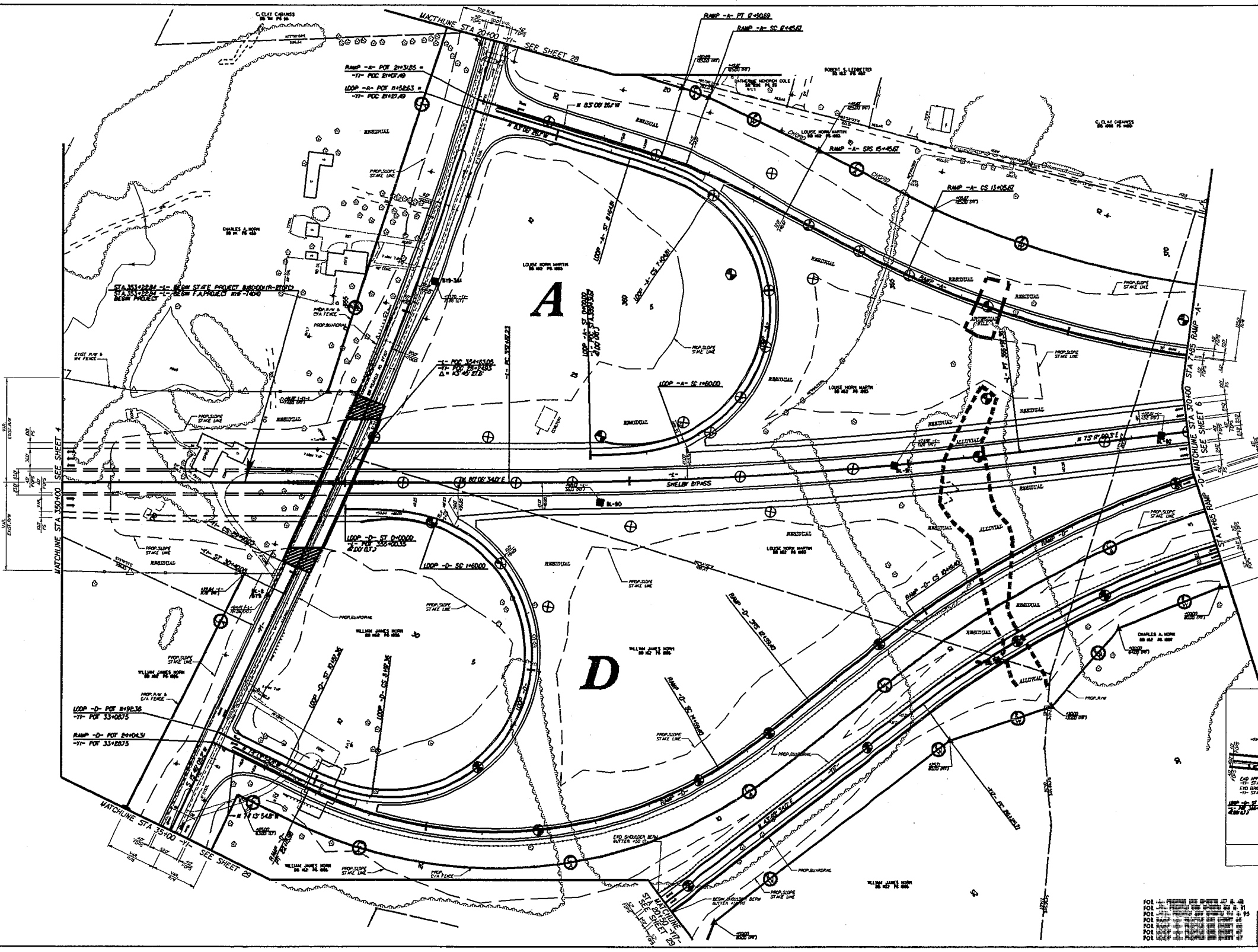
LOOP -B-			
PI STA 3400.00	PI STA 3400.00	PI STA 3400.00	PI STA 3400.00
Δ = 30.00	Δ = 30.00	Δ = 30.00	Δ = 30.00
L = 300.00	L = 300.00	L = 300.00	L = 300.00
E = 1.00	E = 1.00	E = 1.00	E = 1.00
SE = 28	SE = 28	SE = 28	SE = 28

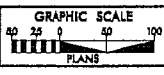
RAMP -C-			
PI STA 3400.00	PI STA 3400.00	PI STA 3400.00	PI STA 3400.00
Δ = 30.00	Δ = 30.00	Δ = 30.00	Δ = 30.00
L = 300.00	L = 300.00	L = 300.00	L = 300.00
E = 1.00	E = 1.00	E = 1.00	E = 1.00
SE = 28	SE = 28	SE = 28	SE = 28

LOOP -C-			
PI STA 3400.00	PI STA 3400.00	PI STA 3400.00	PI STA 3400.00
Δ = 30.00	Δ = 30.00	Δ = 30.00	Δ = 30.00
L = 300.00	L = 300.00	L = 300.00	L = 300.00
E = 1.00	E = 1.00	E = 1.00	E = 1.00
SE = 28	SE = 28	SE = 28	SE = 28

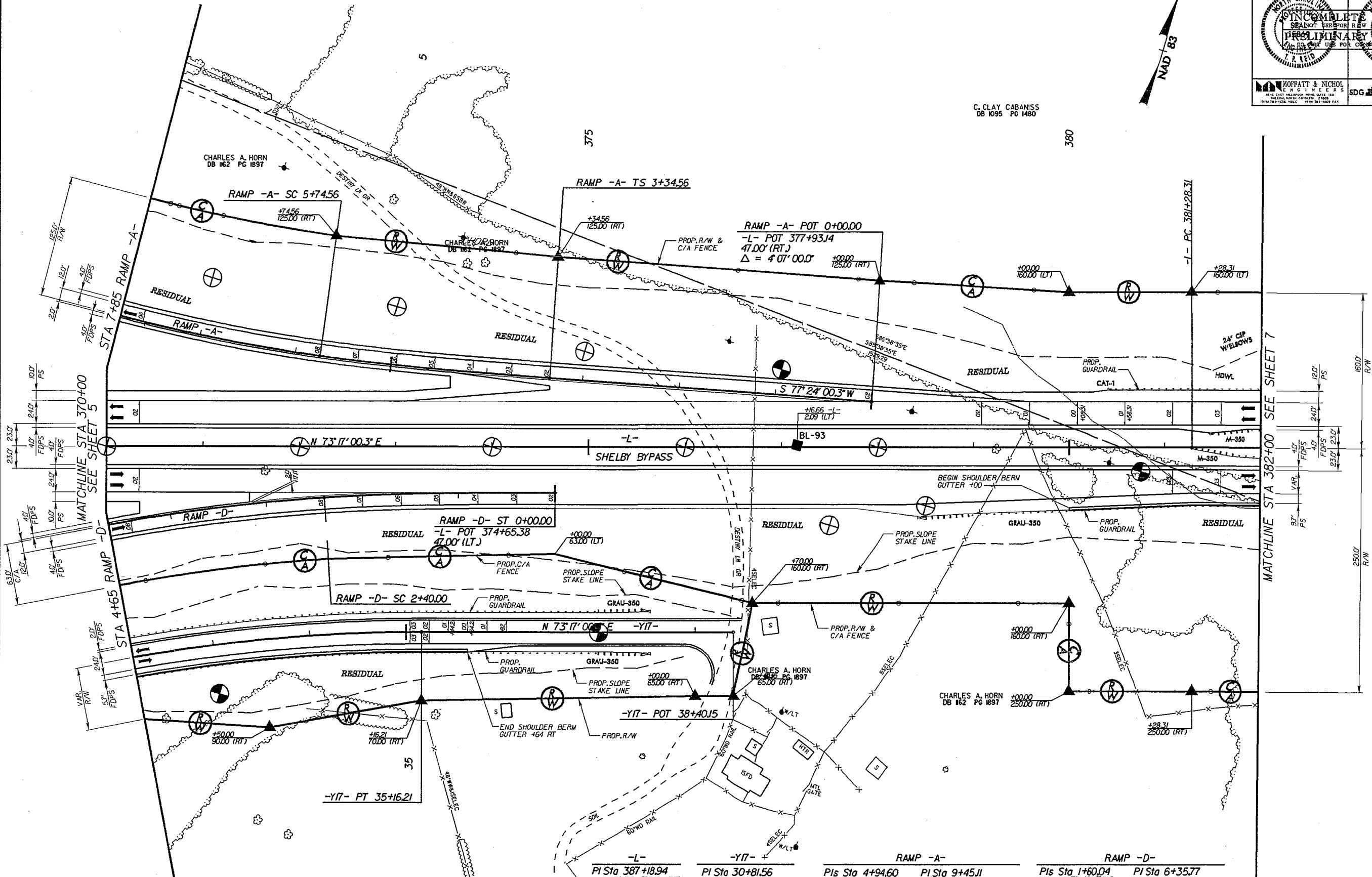


PROJECT APPROVAL NO.	R-2707C	COUNTY	CLEVELAND
PROJECT NAME	INTERCHANGE AT I-74 BYPASS AND -YI- NC 226		
DESIGNED BY	T. HUFFMAN		
CHECKED BY	T. REID	DATE	5/29/02



REVISIONS
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C. CLAY CABANISS  
DB 1095 PG 1480



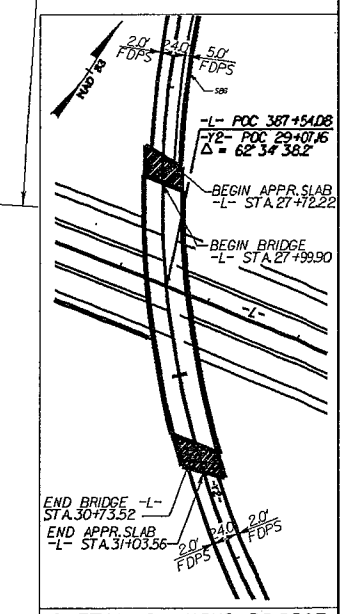
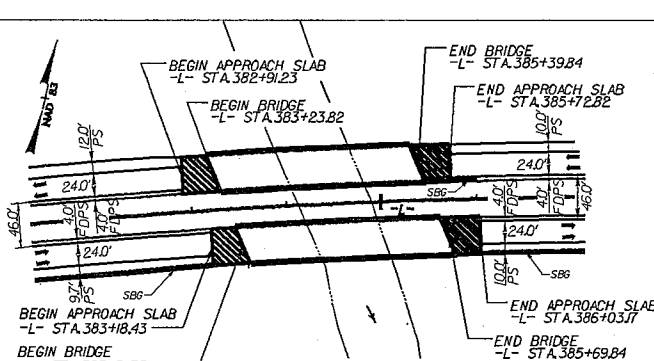
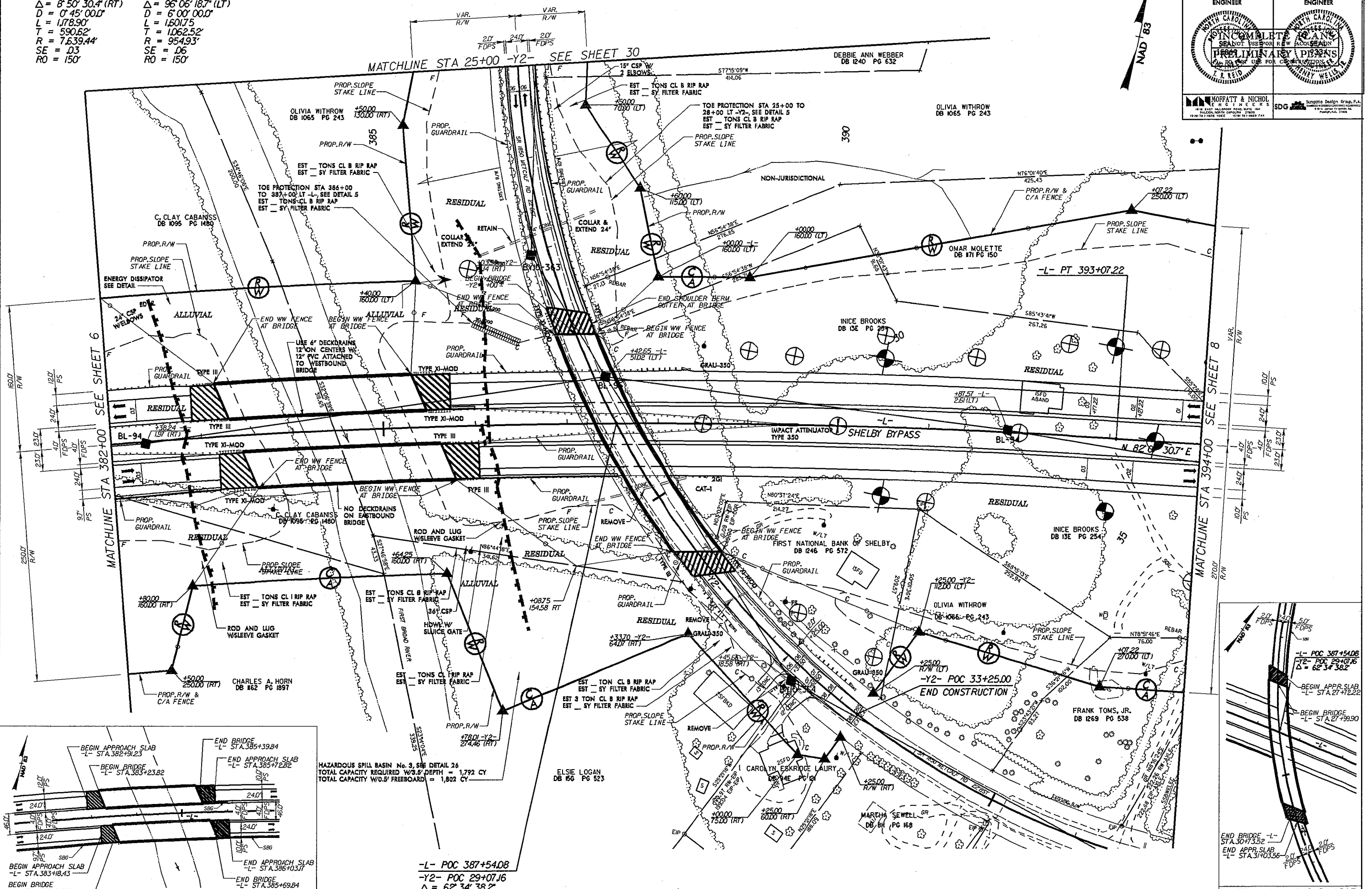
-L-		-Y17-		RAMP -A-		RAMP -D-	
PI Sta 387+18.94	PI Sta 30+81.56	PIs Sta 4+94.60	PI Sta 9+45.11	PIs Sta 1+60.04	PI Sta 6+35.77		
$\Delta = 8^{\circ} 50' 30.4'' (RT)$	$\Delta = 30^{\circ} 11' 26.3'' (RT)$	$\Theta s = 3^{\circ} 46' 39.9''$	$\Delta = 23^{\circ} 00' 57.7'' (RT)$	$\Theta s = 3^{\circ} 46' 39.9''$	$\Delta = 24^{\circ} 32' 11.4'' (LT)$		
$D = 0^{\circ} 45' 00.0''$	$D = 3^{\circ} 23' 25.0''$	$D = 240.00'$	$D = 3^{\circ} 08' 53.2''$	$D = 240.00'$	$D = 3^{\circ} 08' 53.2''$		
$L = 1,178.90'$	$L = 890.51'$	$LT = 160.04'$	$L = 731.10'$	$LT = 160.04'$	$L = 779.40'$		
$T = 590.62'$	$T = 455.85'$	$ST = 80.03'$	$T = 370.55'$	$T = 395.77'$	$T = 1,820.00'$		
$R = 7,639.44'$	$R = 1,690.00'$		$R = 1,820.00'$	$SE = .08$	$R = 1,820.00'$		
$SE = .03$	$SE = .03$		$SE = .08$	$RO = 240'$	$RO = 240'$		
$RO = 150'$	$RO = 60'$						

FOR -L- PROFILE SEE SHEET 48  
 FOR RAMP -A- PROFILE SEE SHEET 65  
 FOR RAMP -D- PROFILE SEE SHEET 66  
 FOR -Y17- PROFILE SEE SHEETS 94 & 95



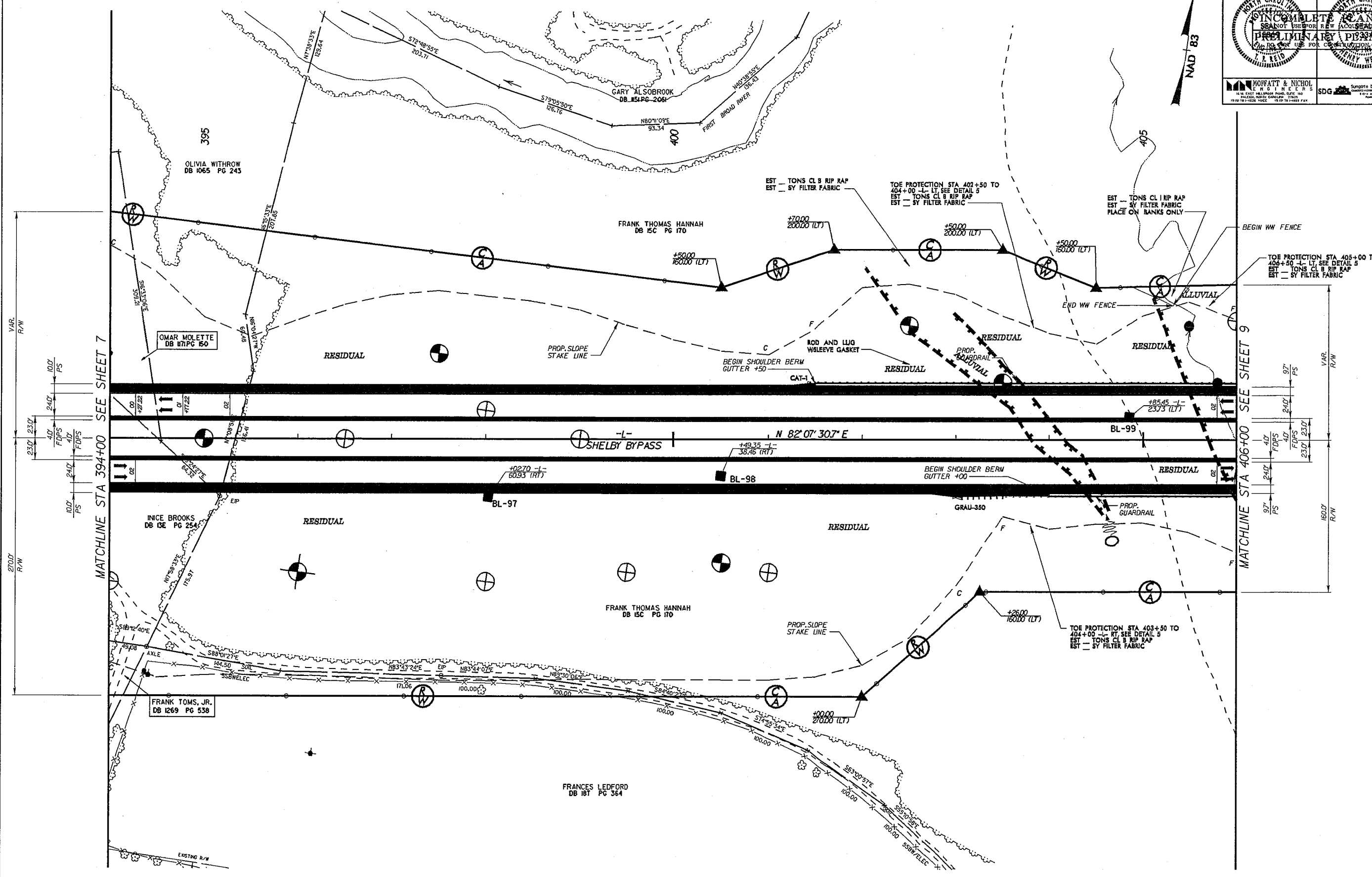
**-L-**  
 PI Sta 387+18.94  
 $\Delta = 8^\circ 50' 30.4''$  (RT)  
 $D = 0' 45' 00.0''$   
 $L = 1,178.90'$   
 $T = 590.62'$   
 $R = 7,639.44'$   
 $SE = .03$   
 $RO = 150'$

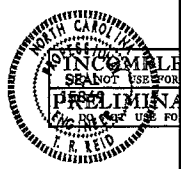
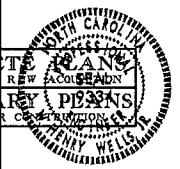


**-Y2-**  
 PI Sta 31+27.15  
 $\Delta = 96^\circ 06' 18.7''$  (LT)  
 $D = 6' 00' 00.0''$   
 $L = 1,601.75'$   
 $T = 1,062.52'$   
 $R = 954.93'$   
 $SE = .06$   
 $RO = 150'$

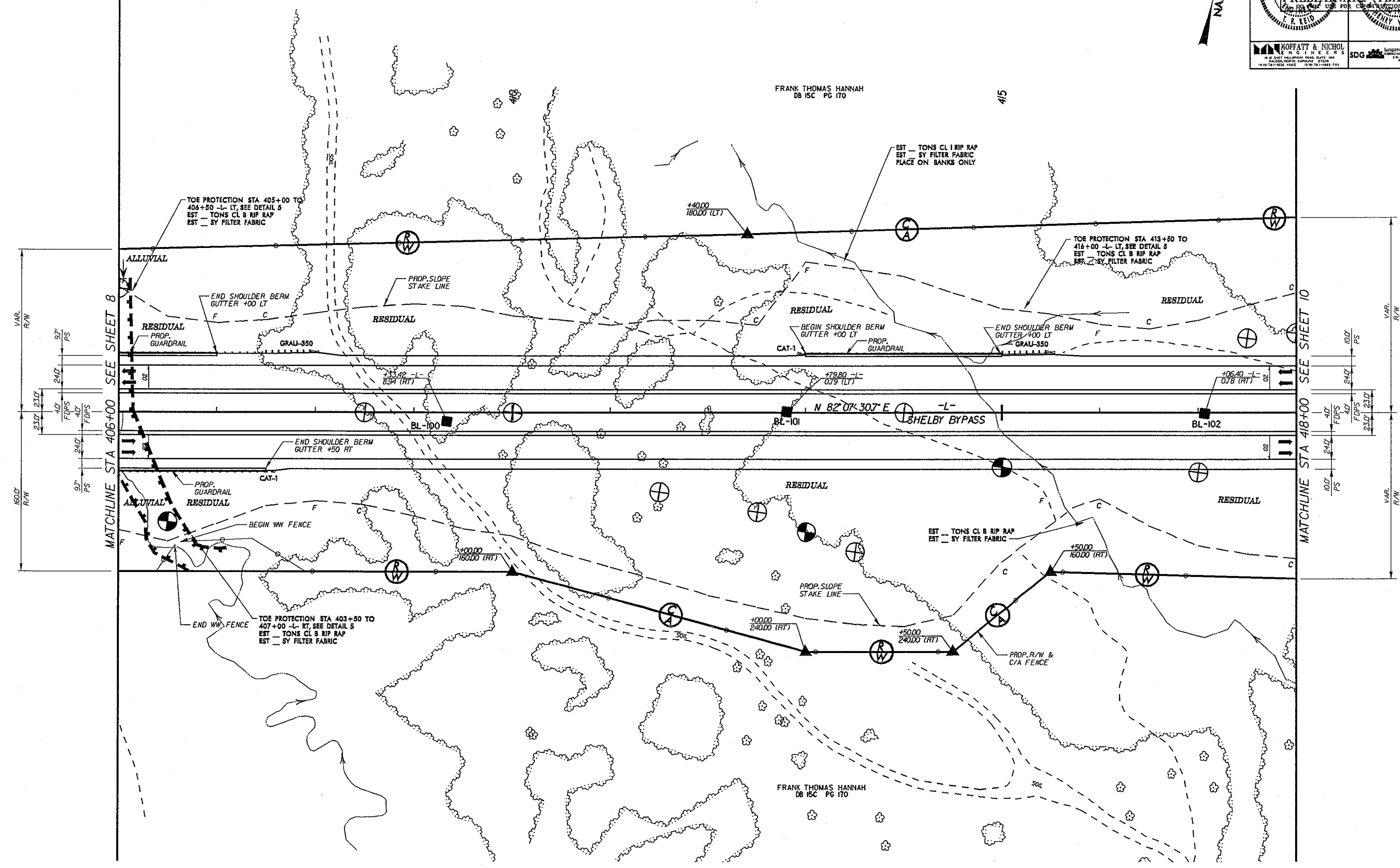


FOR -L- PROFILE SEE SHEETS 48 & 49  
 FOR -Y2- PROFILE SEE SHEET 82

PROJECT REFERENCE NO. R-2707C	SHEET NO. 8
RAW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



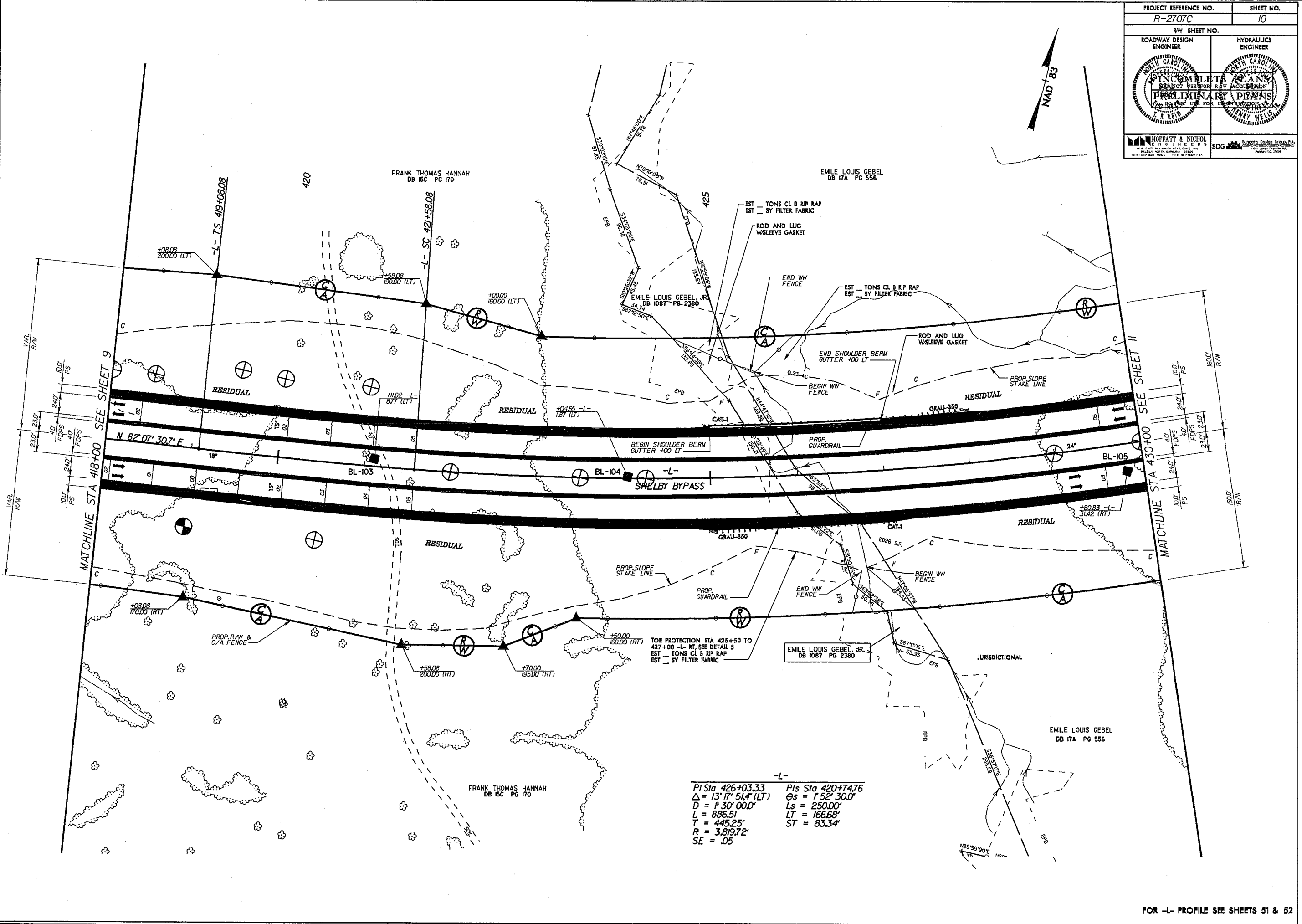
PROJECT REFERENCE NO. R-2707C		SHEET NO. 9	
RW SHEET NO.			
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
			
			



8/17/99

2-MAY-2008 14:11  
c:\pco\lects\27075(rev)\_geo\_rdwj.cleveland\cadd\geotech\p1\mproj\AR2707c(REV).GEO.in\010\_010.psh  
c:\pco\lects\27075(rev)\_geo\_rdwj.cleveland\cadd\geotech\p1\mproj\AR2707c(REV).GEO.in\010\_010.psh

PROJECT REFERENCE NO. R-2707C	SHEET NO. 10
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

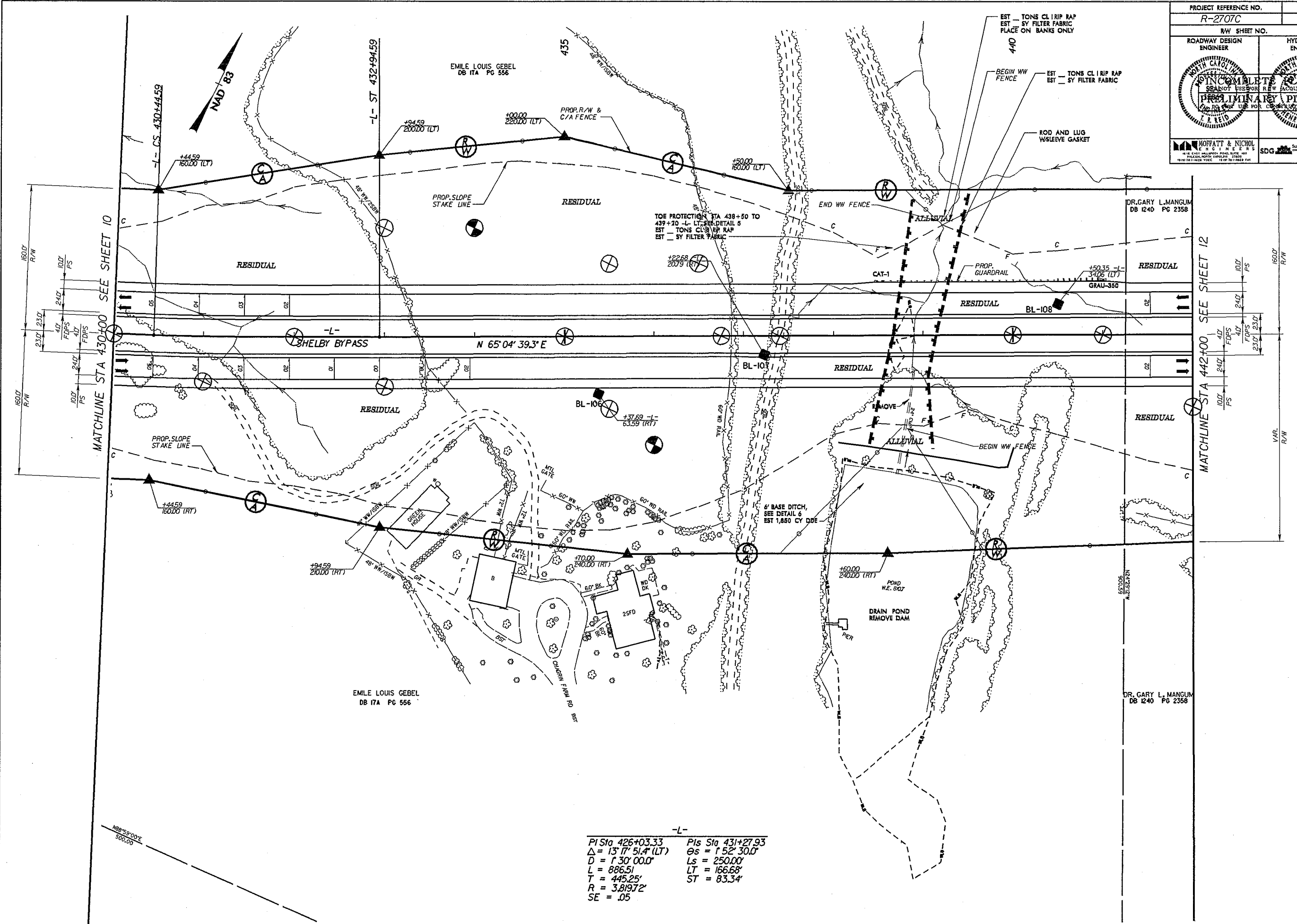


-L-

PI Sta 426+03.33	PIs Sta 420+74.76
$\Delta = 13^{\circ} 17' 51.4" (LT)$	$\Theta_s = 1^{\circ} 52' 30.0"$
$D = 1^{\circ} 30' 00.0"$	$L_s = 250.00'$
$L = 886.51'$	$LT = 166.68'$
$T = 445.25'$	$ST = 83.34'$
$R = 3,819.72'$	
$SE = .05$	

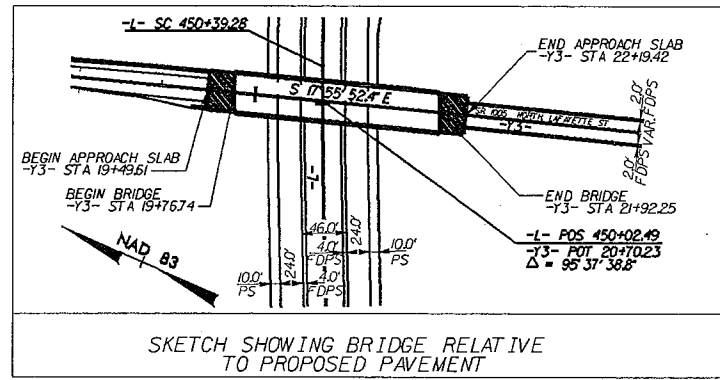
FOR -L- PROFILE SEE SHEETS 51 & 52

PROJECT REFERENCE NO. R-2707C		SHEET NO. 11	
RW SHEET NO.			
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> SHALL NOT BE USED FOR CONSTRUCTION OF ANY WORK <b>PRELIMINARY PLANS</b> NO PART OF THESE PLANS SHALL BE USED FOR CONSTRUCTION OF ANY WORK			

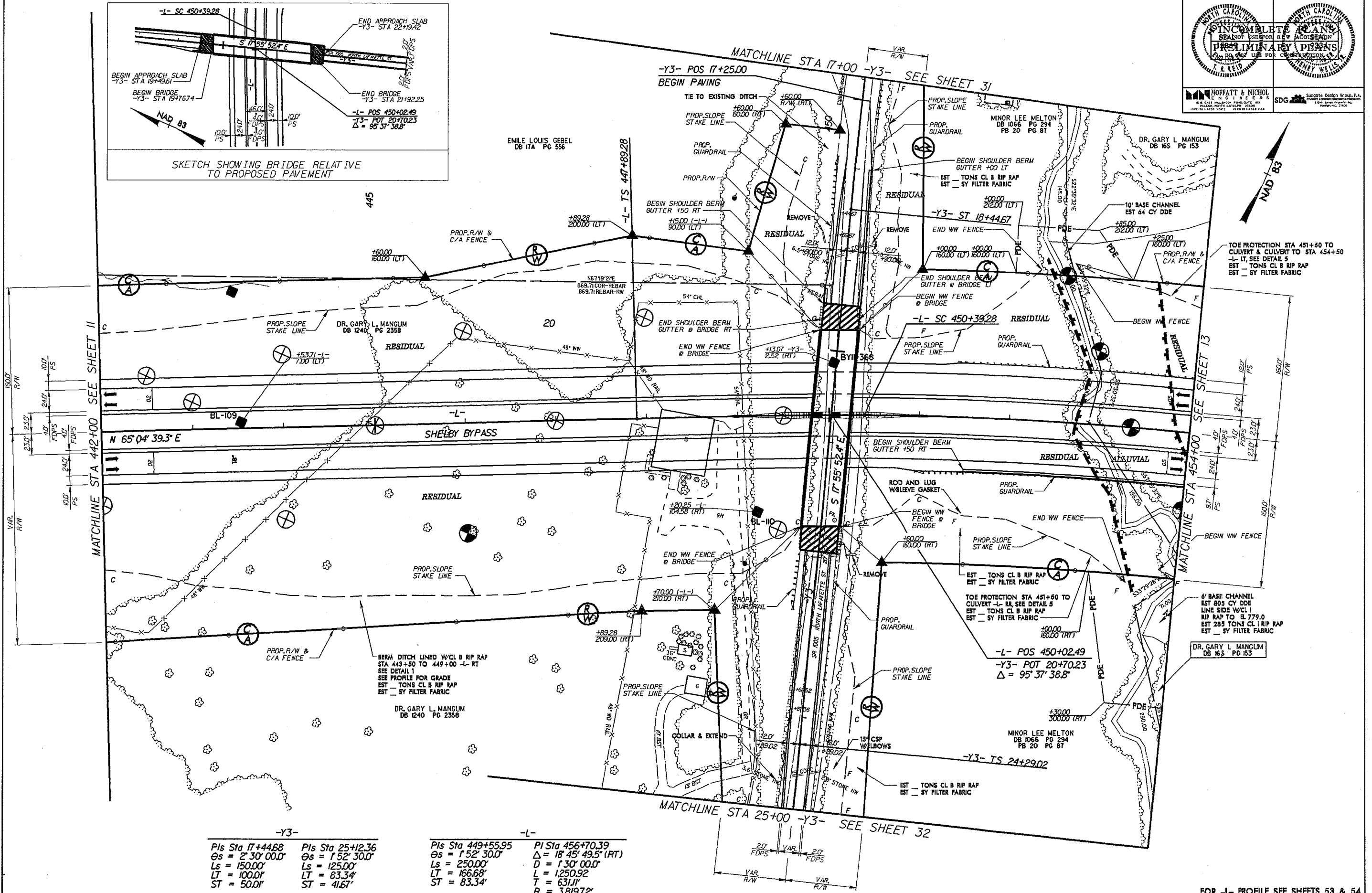


-L-

PI Sta 426+03.33	PIs Sta 431+27.93
$\Delta = 13^{\circ}17' 51.4" (LT)$	$\Theta_s = 1^{\circ}52' 30.0"$
$D = 1^{\circ}30' 00.0"$	$L_s = 250.00'$
$L = 886.51'$	$LT = 166.68'$
$T = 445.25'$	$ST = 83.34'$
$R = 3,819.72'$	
$SE = .05$	

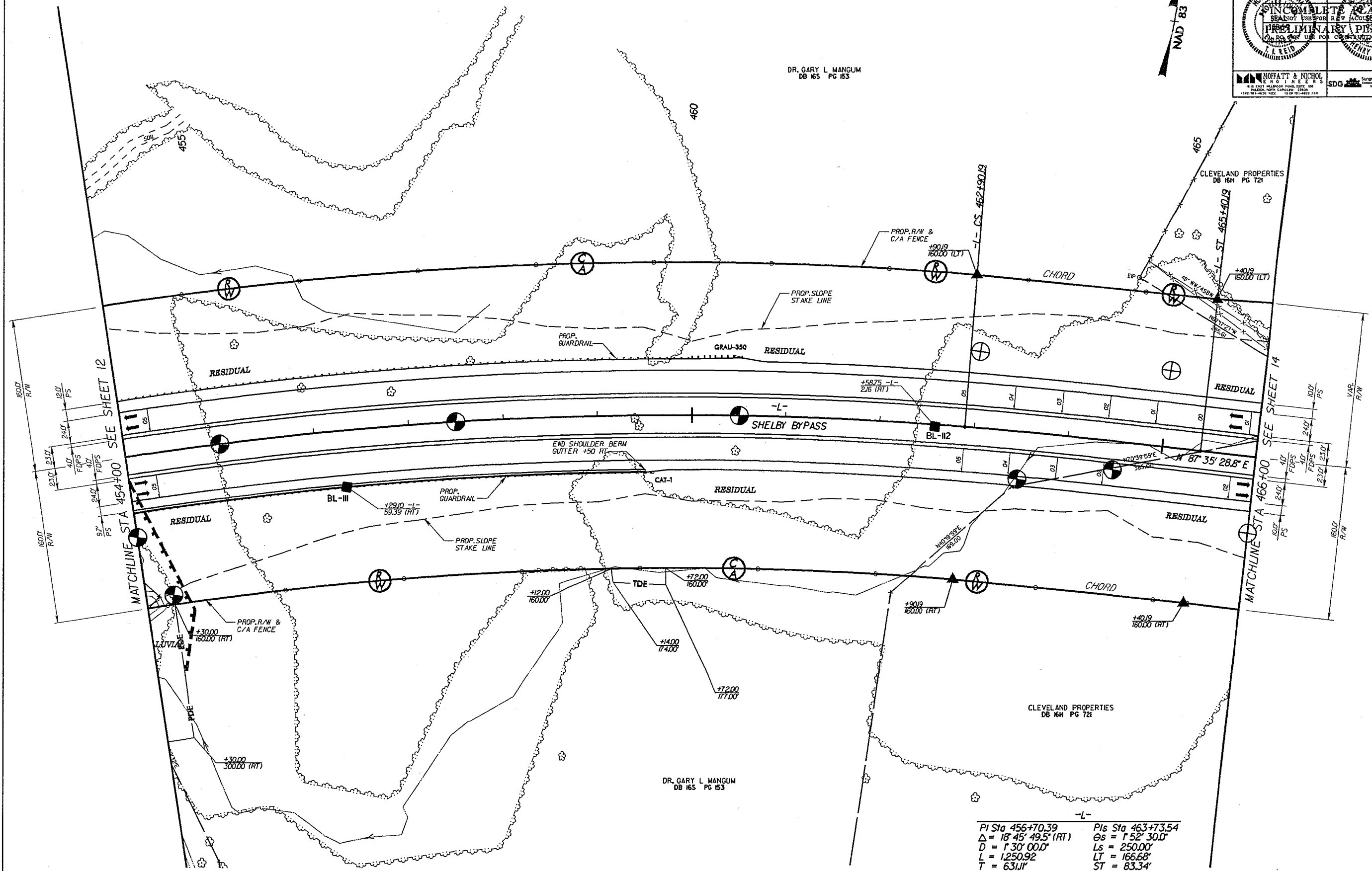


SKETCH SHOWING BRIDGE RELATIVE TO PROPOSED PAVEMENT



-Y3-	
Pls Sta 17+44.68	Pls Sta 25+12.36
Os = 2° 30' 00.0"	Os = 1° 52' 30.0"
Ls = 150.00'	Ls = 125.00'
LT = 100.01'	LT = 83.34'
ST = 50.01'	ST = 41.67'

-L-	
Pls Sta 449+55.95	Pls Sta 456+70.39
Os = 1° 52' 30.0"	Os = 1° 45' 49.5" (RT)
Ls = 250.00'	D = 1° 30' 00.0"
LT = 166.68'	L = 1,250.92'
ST = 83.34'	T = 631.11'
	R = 3,819.72'
	SE = .05

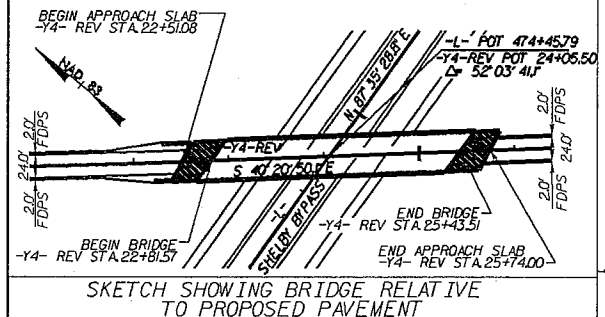


DR. GARY L. MANGUM  
DB 165 PG 153

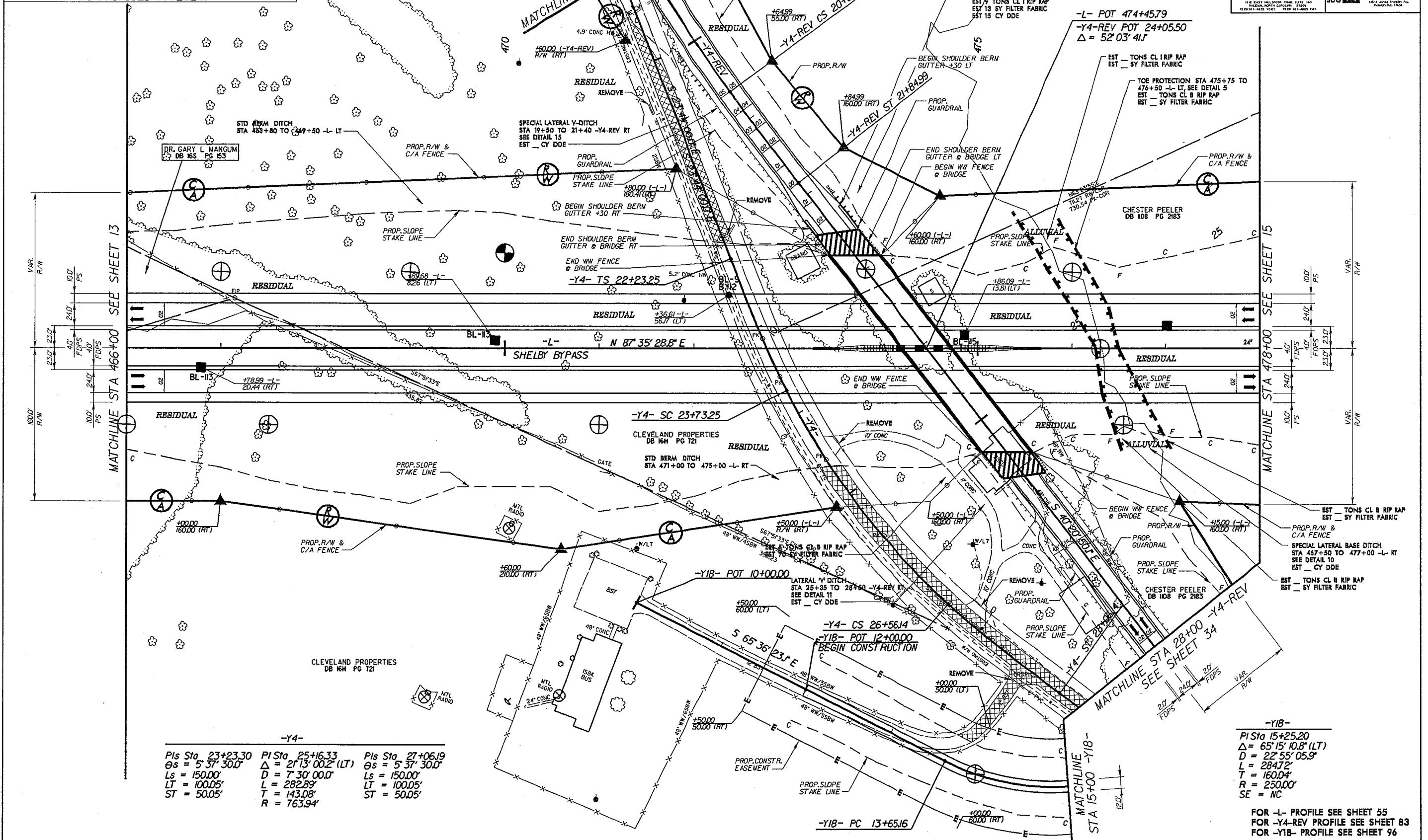
DR. GARY L. MANGUM  
DB 165 PG 153

-L-  
 PI Sta 456+70.39      PIs Sta 463+73.54  
 $\Delta = 18^\circ 45' 49.5" (RT)$        $\Theta_s = 1^\circ 52' 30.0"$   
 $D = 1^\circ 30' 00.0"$        $L_s = 250.00'$   
 $L = 1,250.92$        $LT = 166.68'$   
 $T = 63.11'$        $ST = 83.34'$   
 $R = 3,819.72'$   
 $SE = .05$

PROJECT REFERENCE NO. R-2707C	SHEET NO. 14
RAW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



**-Y4-REV**  
 PI Sta 18+44.49    PIs Sta 21+04.99  
 $\Delta = 13' 17'' 22.9''$  (LT)     $\Theta s = 1' 48'' 00.0''$   
 $D = 3' 00'' 00.0''$      $Ls = 120.00'$   
 $L = 442.99'$      $LT = 80.00'$   
 $T = 222.49'$      $ST = 40.00'$   
 $R = 1,909.86'$   
 $SE = .05$



**-Y4-**

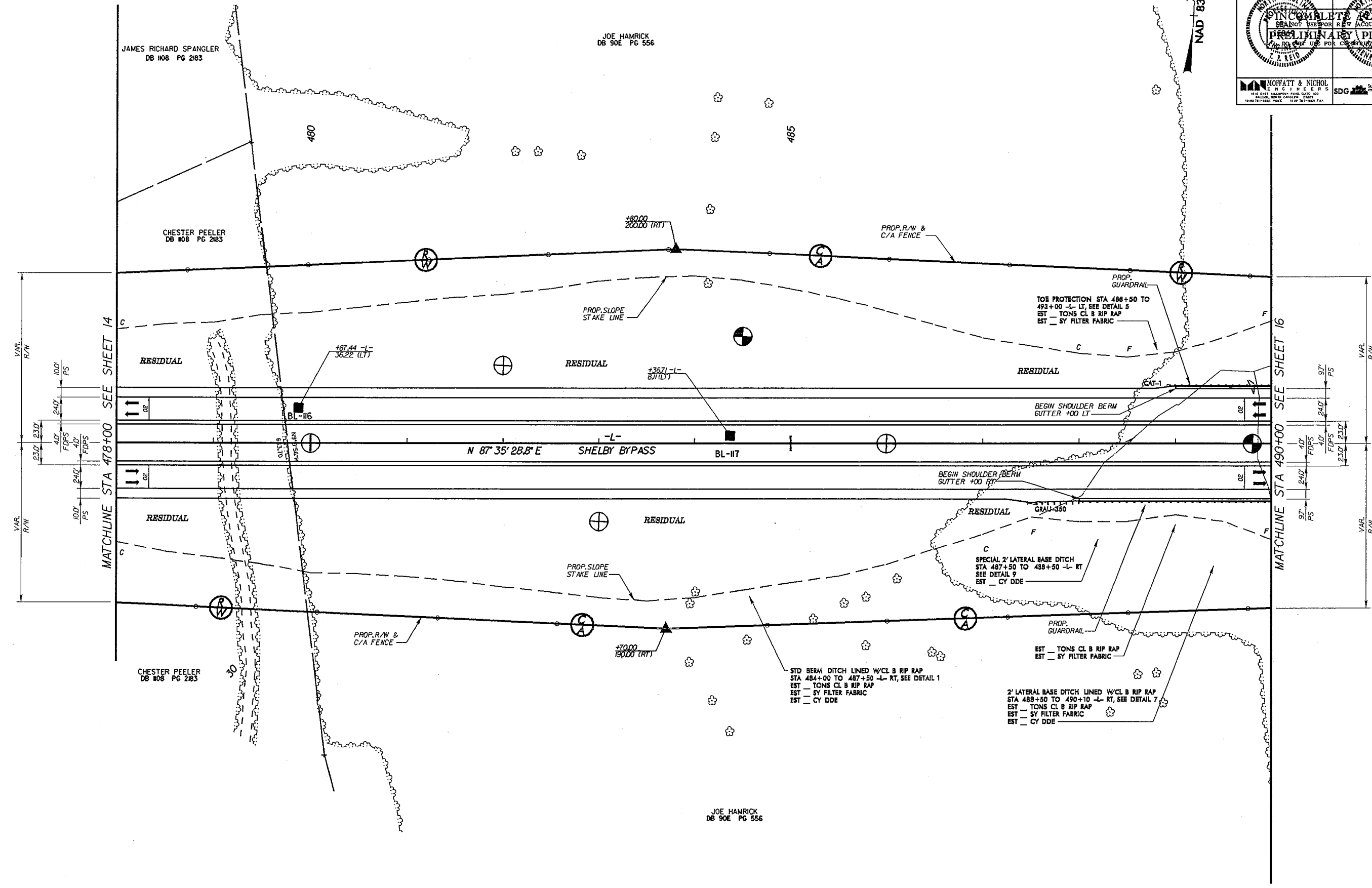
PIs Sta. 23+23.30	PIs Sta. 25+16.33	PIs Sta. 27+06.19
$\Theta s = 5' 37'' 30.0''$	$\Delta = 2' 13'' 00.2''$ (LT)	$\Theta s = 5' 37'' 30.0''$
$Ls = 150.00'$	$L = 282.89'$	$Ls = 150.00'$
$LT = 100.05'$	$T = 143.08'$	$LT = 100.05'$
$ST = 50.05'$	$R = 763.94'$	$ST = 50.05'$

**-Y18-**

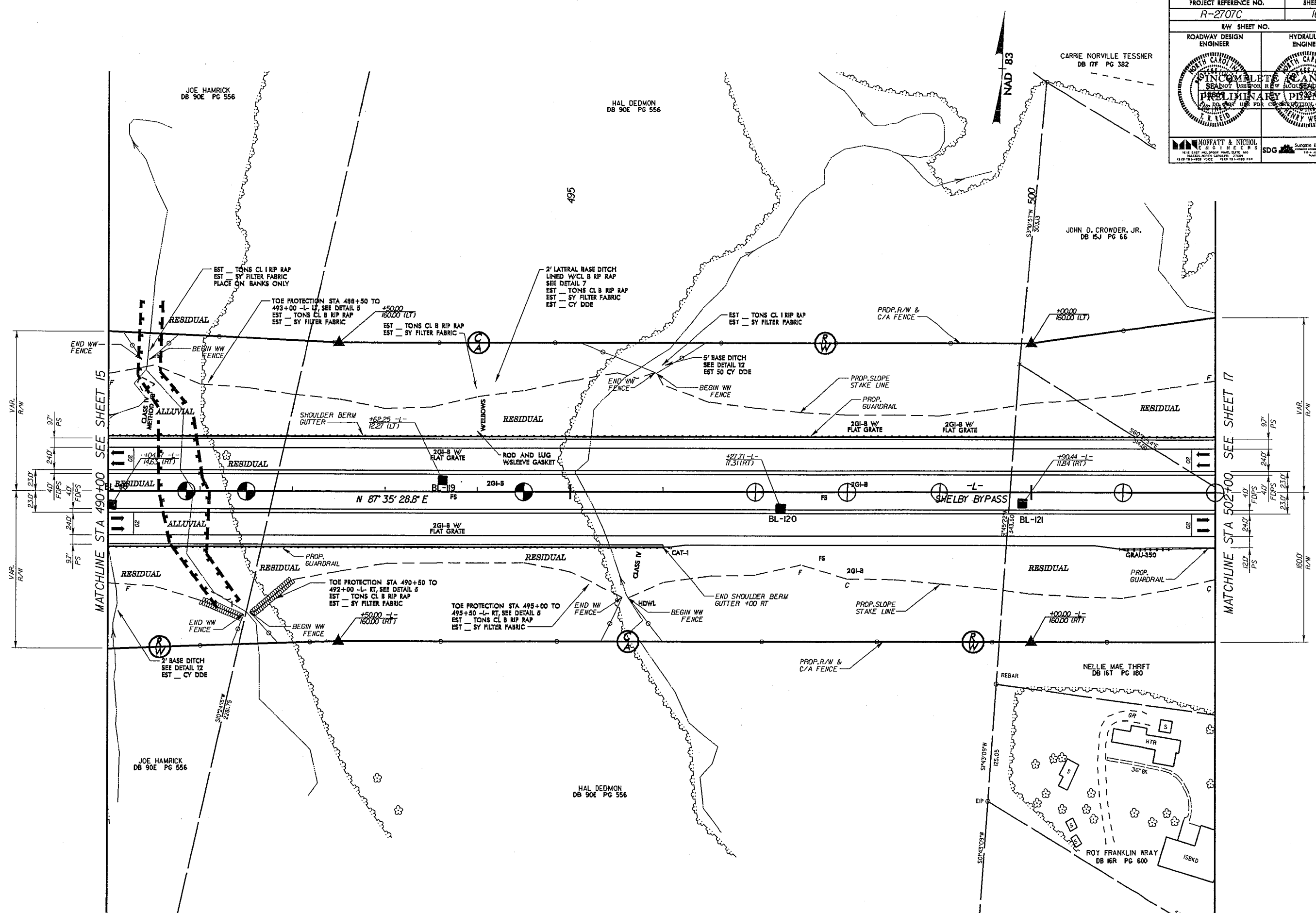
PIs Sta 15+25.20
$\Delta = 65' 15'' 10.8''$ (LT)
$D = 22' 55'' 05.9''$
$L = 284.72'$
$T = 150.04'$
$R = 250.00'$
$SE = NC$

FOR -L- PROFILE SEE SHEET 55  
 FOR -Y4-REV PROFILE SEE SHEET 83  
 FOR -Y18- PROFILE SEE SHEET 96

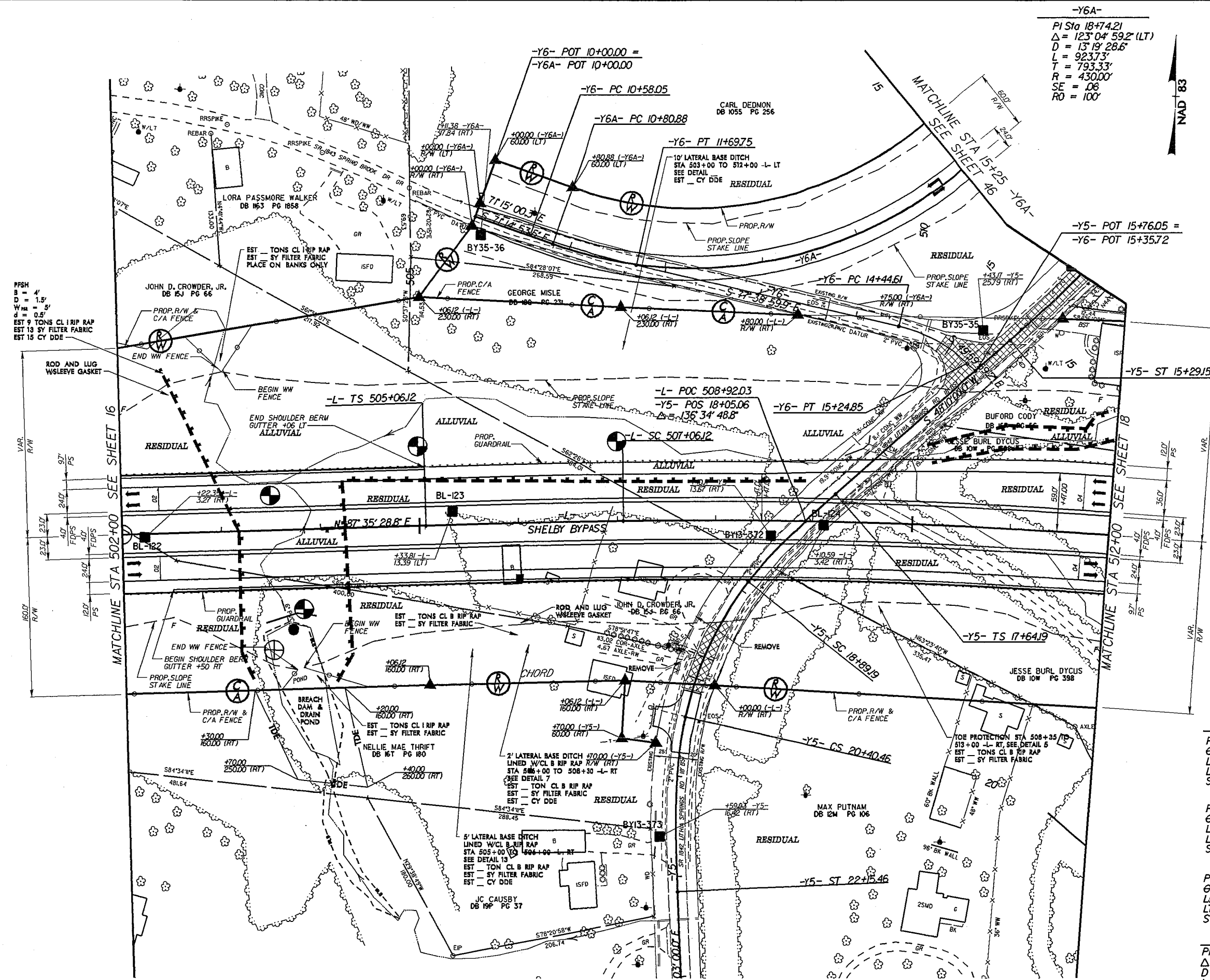




PROJECT REFERENCE NO. R-2707C	SHEET NO. 16
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



PROJECT REFERENCE NO. R-2707C		SHEET NO. 17	
RW SHEET NO.			
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
PRELIMINARY PLANS FOR CONSTRUCTION OF SHELBY BYPASS L. E. REID J. W. WELLS			
MOFFATT & NICHOL ENGINEERS 1400 W. HARRIS ROAD, SUITE 101 FAYETTEVILLE, NORTH CAROLINA 28404 910-441-1100 FAX 910-441-1101		Surgis Design Group, P.A. 114 W. HARRIS ROAD, SUITE 101 FAYETTEVILLE, NORTH CAROLINA 28404 910-441-1100 FAX 910-441-1101	



-Y6A-  
 PI Sta 18+74.21  
 $\Delta = 123^{\circ} 04' 59.2''$  (LT)  
 $D = 13' 19' 28.6''$   
 $L = 923.73'$   
 $T = 793.33'$   
 $R = 430.00'$   
 $SE = .06$   
 $RO = 100'$

-L-  
 PIs Sta 506+39.45 PIs Sta 520+51.16  
 $\Theta_s = 1^{\circ} 00' 00.0''$   $\Delta = 26^{\circ} 25' 21.1''$  (RT)  
 $L_s = 200.00'$   $D = 1^{\circ} 00' 00.0''$   
 $LT = 133.34'$   $L = 2,642.25'$   
 $ST = 66.67'$   $T = 1,345.05'$   
 $R = 57,295.8'$   
 $SE = .04$

-Y5-  
 PIs Sta 13+96.72 PIs Sta 14+85.71  
 $\Theta_s = 2^{\circ} 30' 00.0''$   $\Delta = 30^{\circ} 39' 00.8''$  (RT)  
 $L_s = 200.00'$   $D = 38' 11' 49.9''$   
 $LT = 134.33'$   $L = 80.24'$   
 $ST = 67.57'$   $T = 411'$   
 $R = 150.00'$

PIs Sta 18+47.67 PIs Sta 19+66.12  
 $\Theta_s = 10^{\circ} 37' 30.0''$   $\Delta = 25^{\circ} 43' 00.0''$  (LT)  
 $L_s = 125.00'$   $D = 17^{\circ} 00' 00.0''$   
 $LT = 83.48'$   $L = 151.27'$   
 $ST = 41.80'$   $T = 76.93'$   
 $R = 337.03'$

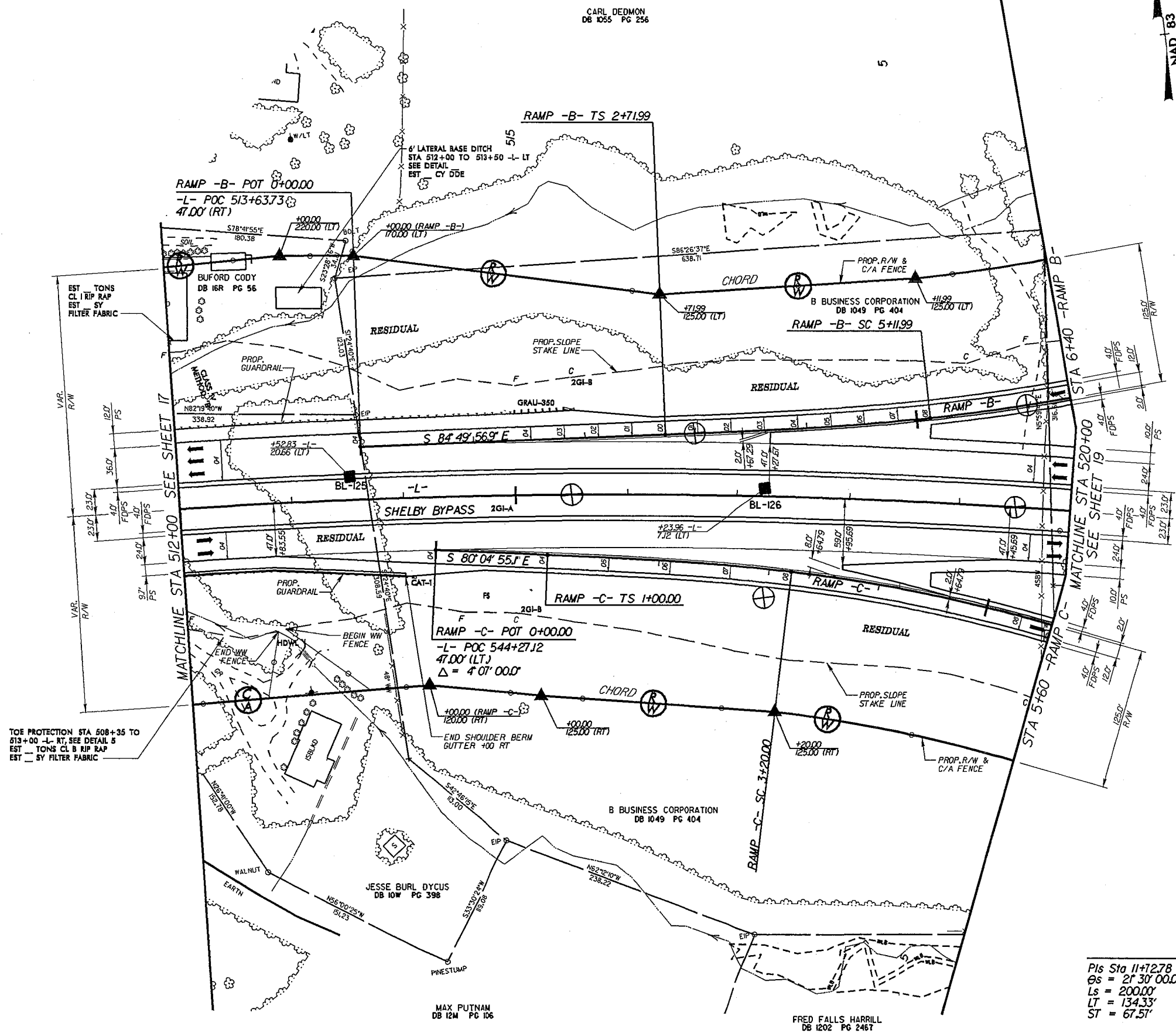
PIs Sta 20+99.17  
 $\Theta_s = 14^{\circ} 52' 30.0''$   
 $L_s = 175.00'$   
 $LT = 117.08'$   
 $ST = 58.71'$

-Y6-  
 PIs Sta 11+13.95 PIs Sta 14+85.71  
 $\Delta = 6^{\circ} 23' 59.7''$  (LT)  $\Delta = 30^{\circ} 39' 00.8''$  (RT)  
 $D = 5' 43' 46.5''$   $D = 38' 11' 49.9''$   
 $L = 111.70'$   $L = 80.24'$   
 $T = 55.9'$   $T = 411'$   
 $R = 1,000.00'$   $R = 150.00'$

FOR -L- PROFILE SEE SHEETS 57 & 58  
 FOR -Y6A- PROFILE SEE SHEET 84

PFSS  
 $B = 4'$   
 $D = 1.5'$   
 $W = 0.5'$   
 $d = 0.5'$   
 EST 9 TONS CL RIP RAP  
 EST 13 SY FILTER FABRIC  
 EST 15 CY DDE

ROY FRANKLIN WRAY  
 DB 16R PG 600



-L-

PI Sta 520+51.6	$\Delta = 26' 25' 21''$ (RT)
D = 1' 00' 00"	L = 2,642.25'
T = 1,345.05'	R = 5,729.58'
SE = .04	

RAMP -B-

PIs Sta 4+32.03	PI Sta 7+59.93
$\Theta_s = 3' 46' 39''$	$\Delta = 15' 30' 56.3''$ (LT)
Ls = 240.00'	D = 3' 08' 53.2"
LT = 160.04'	L = 492.85'
ST = 80.03'	T = 247.94'
	R = 1,820.00'
	SE = .08

RAMP -C-

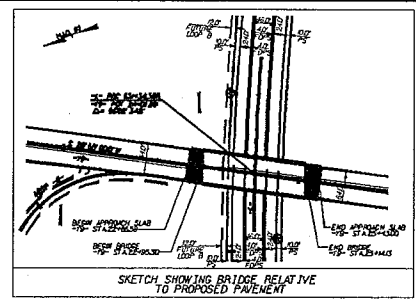
PIs Sta 2+46.71	PI Sta 6+42.46
$\Theta_s = 4' 14' 38.5''$	$\Delta = 24' 30' 08.9''$ (RT)
Ls = 220.00'	D = 3' 51' 29.9"
LT = 146.71'	L = 635.06'
ST = 73.37'	T = 322.46'
	R = 1,485.00'
	SE = .08

-Y5-

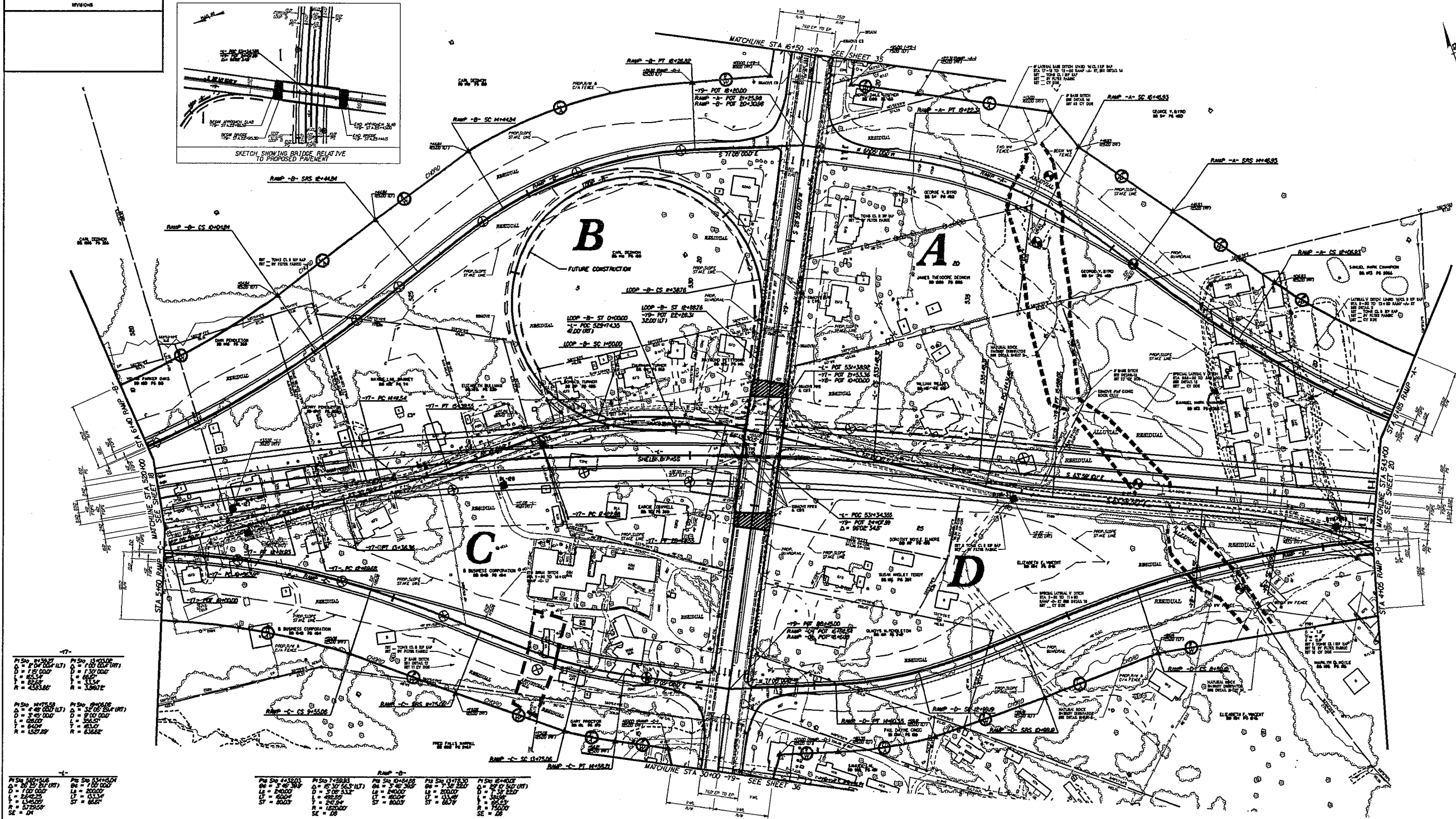
PIs Sta 11+72.78	PI Sta 12+84.24	PIs Sta 13+96.72
$\Theta_s = 2' 30' 00.0''$	$\Delta = 19' 29' 59.5''$ (RT)	$\Theta_s = 2' 30' 00.0''$
Ls = 200.00'	D = 2' 30' 00.0"	Ls = 200.00'
LT = 134.33'	L = 90.70'	LT = 134.33'
ST = 67.57'	T = 45.79'	ST = 67.57'
	R = 266.49'	

FOR -L- PROFILE SEE SHEETS 58 & 59  
 FOR RAMP -B- PROFILE SEE SHEET 69  
 FOR RAMP -C- PROFILE SEE SHEET 70  
 FOR -Y6A- PROFILE SEE SHEET 84



BYWAYS

1	2	3	4
5	6	7	8
9	10	11	12
13	14	15	16
17	18	19	20
21	22	23	24
25	26	27	28
29	30	31	32
33	34	35	36
37	38	39	40
41	42	43	44
45	46	47	48
49	50	51	52
53	54	55	56
57	58	59	60
61	62	63	64
65	66	67	68
69	70	71	72
73	74	75	76
77	78	79	80
81	82	83	84
85	86	87	88
89	90	91	92
93	94	95	96
97	98	99	100



-17-

PI Stn 8130.27	PI Stn 13403.02
Δ = 5' 00" (15')	Δ = 5' 00" (15')
L = 150.00'	L = 150.00'
ST = 800.00'	ST = 800.00'
R = 1500.00'	R = 1500.00'
SE = 26	SE = 26

RAMP -A-

PI Stn 8130.27	PI Stn 13403.02	PI Stn 13403.02	PI Stn 13403.02
Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')
L = 150.00'	L = 150.00'	L = 150.00'	L = 150.00'
ST = 800.00'	ST = 800.00'	ST = 800.00'	ST = 800.00'
R = 1500.00'	R = 1500.00'	R = 1500.00'	R = 1500.00'
SE = 26	SE = 26	SE = 26	SE = 26

RAMP -B-

PI Stn 8130.27	PI Stn 13403.02	PI Stn 13403.02	PI Stn 13403.02
Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')
L = 150.00'	L = 150.00'	L = 150.00'	L = 150.00'
ST = 800.00'	ST = 800.00'	ST = 800.00'	ST = 800.00'
R = 1500.00'	R = 1500.00'	R = 1500.00'	R = 1500.00'
SE = 26	SE = 26	SE = 26	SE = 26

RAMP -C-

PI Stn 8130.27	PI Stn 13403.02	PI Stn 13403.02	PI Stn 13403.02
Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')
L = 150.00'	L = 150.00'	L = 150.00'	L = 150.00'
ST = 800.00'	ST = 800.00'	ST = 800.00'	ST = 800.00'
R = 1500.00'	R = 1500.00'	R = 1500.00'	R = 1500.00'
SE = 26	SE = 26	SE = 26	SE = 26

RAMP -D-

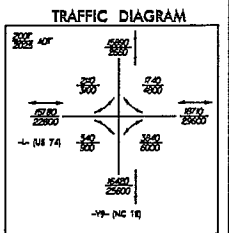
PI Stn 8130.27	PI Stn 13403.02	PI Stn 13403.02	PI Stn 13403.02
Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')
L = 150.00'	L = 150.00'	L = 150.00'	L = 150.00'
ST = 800.00'	ST = 800.00'	ST = 800.00'	ST = 800.00'
R = 1500.00'	R = 1500.00'	R = 1500.00'	R = 1500.00'
SE = 26	SE = 26	SE = 26	SE = 26

FUTURE LOOP -B-

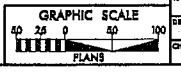
PI Stn 8130.27	PI Stn 13403.02	PI Stn 13403.02	PI Stn 13403.02
Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')
L = 150.00'	L = 150.00'	L = 150.00'	L = 150.00'
ST = 800.00'	ST = 800.00'	ST = 800.00'	ST = 800.00'
R = 1500.00'	R = 1500.00'	R = 1500.00'	R = 1500.00'
SE = 26	SE = 26	SE = 26	SE = 26

-18-

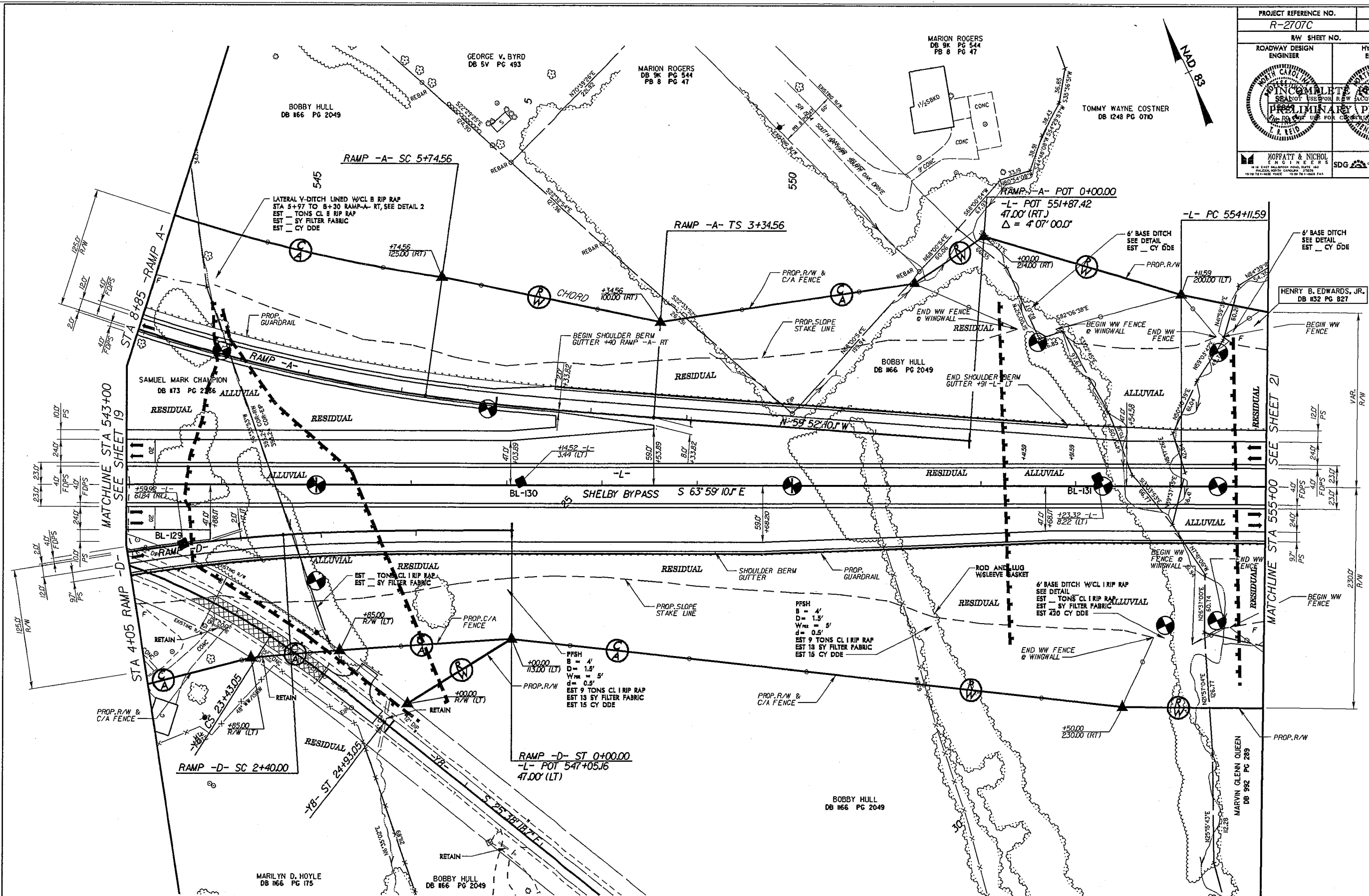
PI Stn 8130.27	PI Stn 13403.02	PI Stn 13403.02	PI Stn 13403.02
Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')	Δ = 5' 00" (15')
L = 150.00'	L = 150.00'	L = 150.00'	L = 150.00'
ST = 800.00'	ST = 800.00'	ST = 800.00'	ST = 800.00'
R = 1500.00'	R = 1500.00'	R = 1500.00'	R = 1500.00'
SE = 26	SE = 26	SE = 26	SE = 26



FOR -1- PROFILE SEE SHEET 57  
 FOR RAMP -A- PROFILE SEE SHEET 68  
 FOR RAMP -B- PROFILE SEE SHEET 69  
 FOR RAMP -C- PROFILE SEE SHEET 70  
 FOR RAMP -D- PROFILE SEE SHEET 71  
 FOR LOOP -B- PROFILE SEE SHEET 72



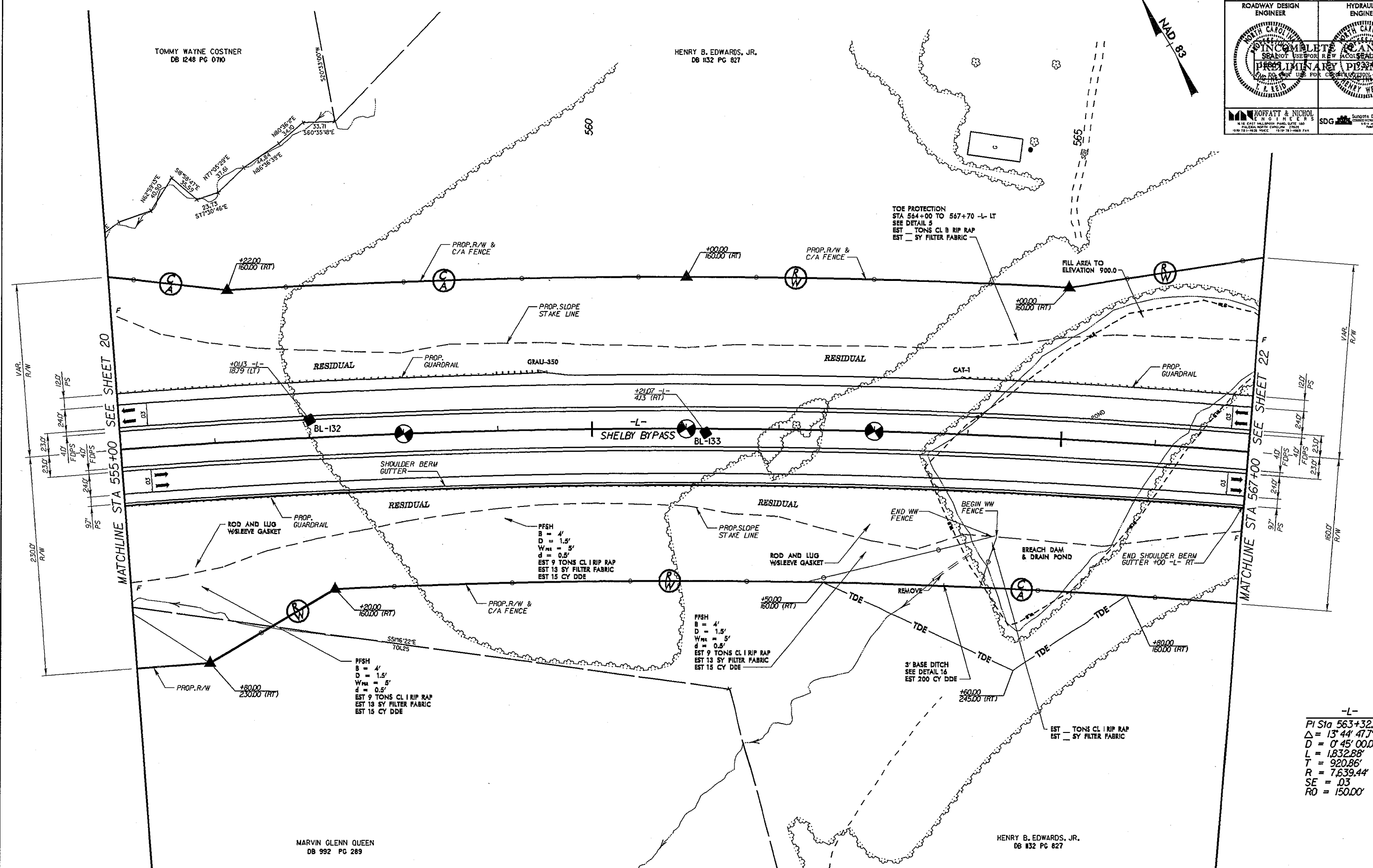
LOCATION: INTERCHANGE AT  
 -1- LIS 74 BYPASS  
 AND -19- NC 18  
 COUNTY: CLEVELAND  
 ENGINEER: T. HUFFMAN  
 CHECKED BY: T. REID  
 DATE: 5/19/62



-L-	RAMP -A-	RAMP -D-	-Y8-
PI Sta 563+32.45	PI Sta 4+94.60	PI Sta 1+60.04	PI Sta 21+71.57
$\Delta = 13' 44" 47.7" (RT)$	$\Delta = 19' 54" 27.3" (RT)$	$\Delta = 3' 46' 39.9"$	$\Delta = 26' 47' 34.0" (RT)$
$D = 0' 45' 00.0"$	$D = 3' 08' 53.2"$	$D = 240.00'$	$D = 7' 40' 00.0"$
$L = 1,832.88'$	$L = 632.36'$	$L = 160.04'$	$L = 349.47'$
$T = 920.86'$	$T = 319.40'$	$T = 312.62'$	$T = 177.99'$
$R = 7,639.44'$	$R = 1,820.00'$	$R = 1,820.00'$	$R = 747.34'$
$SE = .03$	$SE = .08$	$SE = .08$	
$RO = 150.00'$			

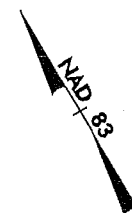
FOR -L- PROFILE SEE SHEETS 59 & 60  
 FOR RAMP -A- PROFILE SEE SHEET 68  
 FOR RAMP -D- PROFILE SEE SHEET 71

PROJECT REFERENCE NO. R-2707C	SHEET NO. 21
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



MATCHLINE STA 555+00 SEE SHEET 20

MATCHLINE STA 567+00 SEE SHEET 22



TOMMY WAYNE COSTNER  
DB 1248 PG 070

HENRY B. EDWARDS, JR.  
DB 1132 PG 827

MARVIN GLENN QUEEN  
DB 992 PG 289

HENRY B. EDWARDS, JR.  
DB 1132 PG 827

TOE PROTECTION  
STA 564+00 TO 567+70 -L- LT  
SEE DETAIL 5  
EST TONS CL 1 RIP RAP  
EST 5Y FILTER FABRIC

PFSH  
B = 4'  
D = 1.5'  
W<sub>HA</sub> = 5'  
d = 0.5'  
EST 9 TONS CL 1 RIP RAP  
EST 13 SY FILTER FABRIC  
EST 15 CY DDE

PFSH  
B = 4'  
D = 1.5'  
W<sub>HA</sub> = 5'  
d = 0.5'  
EST 9 TONS CL 1 RIP RAP  
EST 13 SY FILTER FABRIC  
EST 15 CY DDE

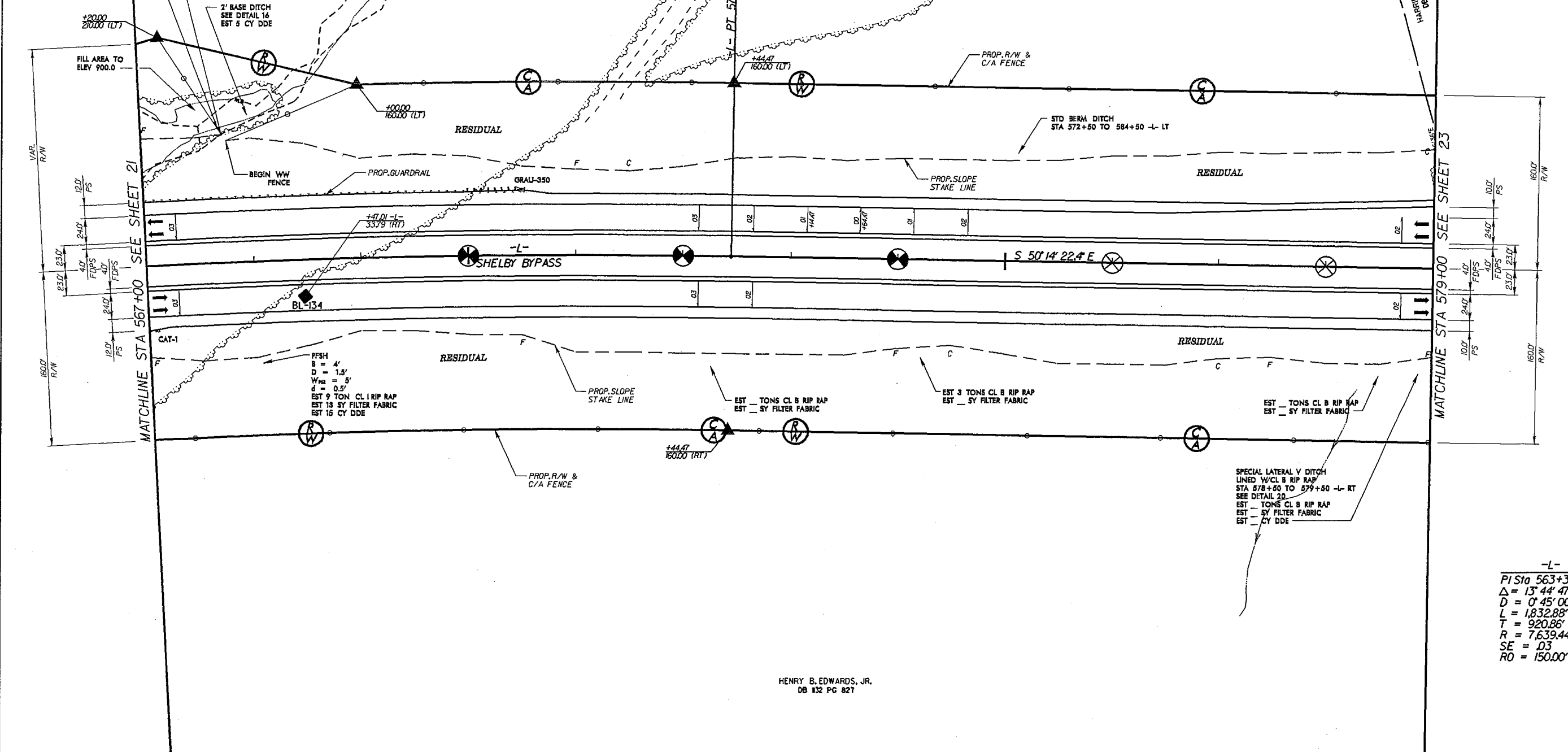
PFSH  
B = 4'  
D = 1.5'  
W<sub>HA</sub> = 5'  
d = 0.5'  
EST 9 TONS CL 1 RIP RAP  
EST 13 SY FILTER FABRIC  
EST 15 CY DDE

3' BASE DITCH  
SEE DETAIL 16  
EST 200 CY DDE

-L-  
PI Sta 563+32.45  
Δ = 13° 44' 47.7" (RT)  
D = 0' 45' 00.0"  
L = 1,832.88'  
T = 920.86'  
R = 7,639.44'  
SE = .03  
RO = 150.00'

PROJECT REFERENCE NO. R-2707C	SHEET NO. 22
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
 MOFFATT & NICHOL ENGINEERS 1401 W. GARDNER AVE. SUITE 101 RALEIGH, NORTH CAROLINA 27606 919-879-6200 FAX 919-879-6200	
 SDG Suncoast Design Group, P.A. 1101 W. GARDNER AVE. SUITE 101 RALEIGH, NORTH CAROLINA 27606 919-879-6200 FAX 919-879-6200	

TDE PROTECTION  
STA 564+00 TO 567+70 -L- LT  
SEE DETAIL 5  
EST \_ TONS CL B RIP RAP  
EST \_ SY FILTER FABRIC



PFSH  
B = 4'  
D = 1.5'  
W<sub>FL</sub> = 5'  
d = 0.5'

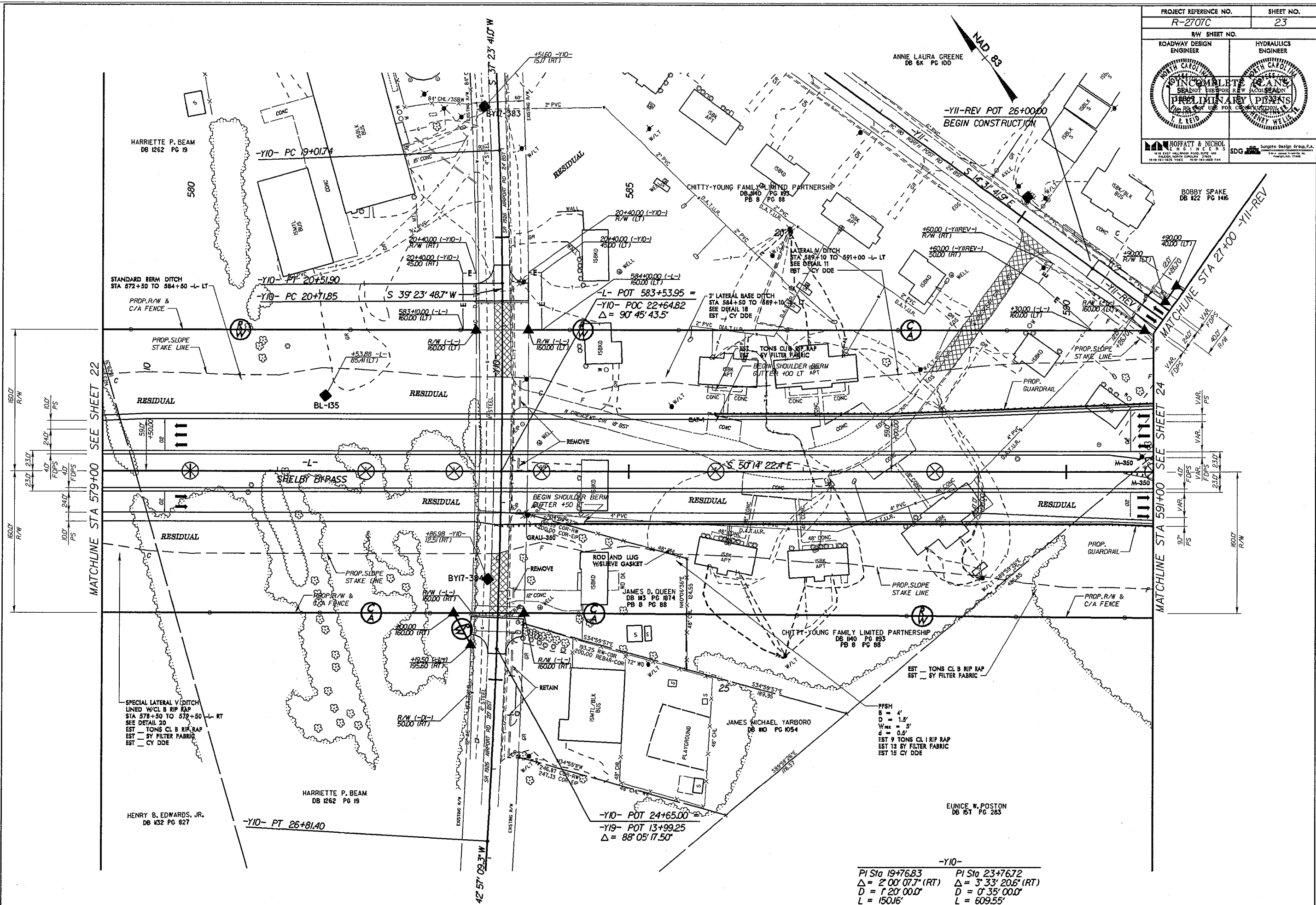
EST 9 TON CL B RIP RAP  
EST 18 SY FILTER FABRIC  
EST 15 CY DDE

SPECIAL LATERAL V DITCH  
LINED W/CL B RIP RAP  
STA 578+50 TO 579+50 -L- RT  
SEE DETAIL 20  
EST \_ TONS CL B RIP RAP  
EST \_ SY FILTER FABRIC  
EST \_ CY DDE

-L-  
PI Sta 563+32.45  
 $\Delta = 13^{\circ} 44' 47.7" (RT)$   
D = 0' 45' 00.0"  
L = 1,832.88'  
T = 920.86'  
R = 7,639.44'  
SE = .03  
RO = 150.00'

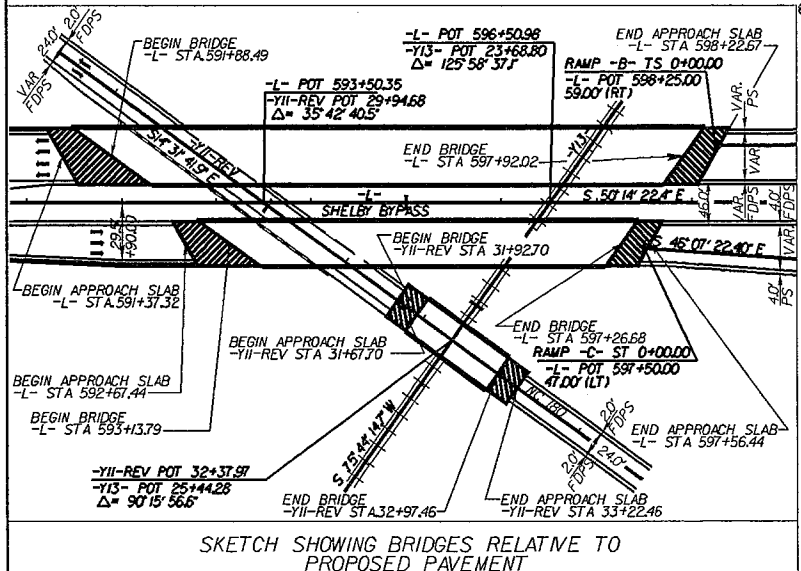
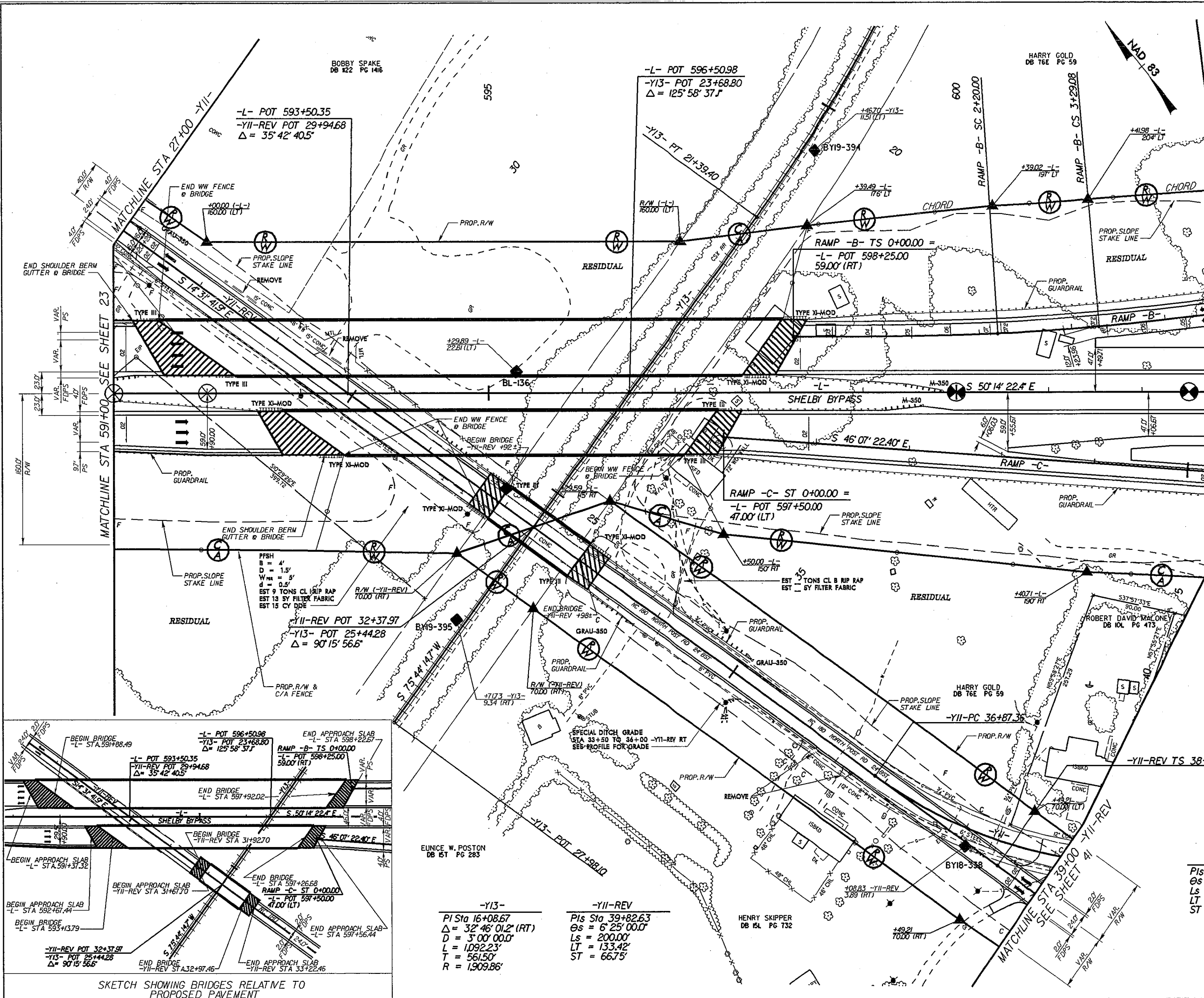
HENRY B. EDWARDS, JR.  
DB #32 PG 827





-Y10-	
PI Sta 19+76.83	PI Sta 23+76.72
$\Delta = 2^{\circ} 00' 07.7''$ (RT)	$\Delta = 3^{\circ} 33' 20.6''$ (RT)
$D = 1^{\circ} 20' 00.0''$	$D = 0^{\circ} 35' 00.0''$
$L = 150.16'$	$L = 609.55'$
$T = 75.09'$	$T = 304.87'$
$R = 4,297.18'$	$R = 9,822.13'$

FOR -L- PROFILE SEE SHEET 62  
FOR -Y11-REV PROFILE SEE SHEETS 88 & 89



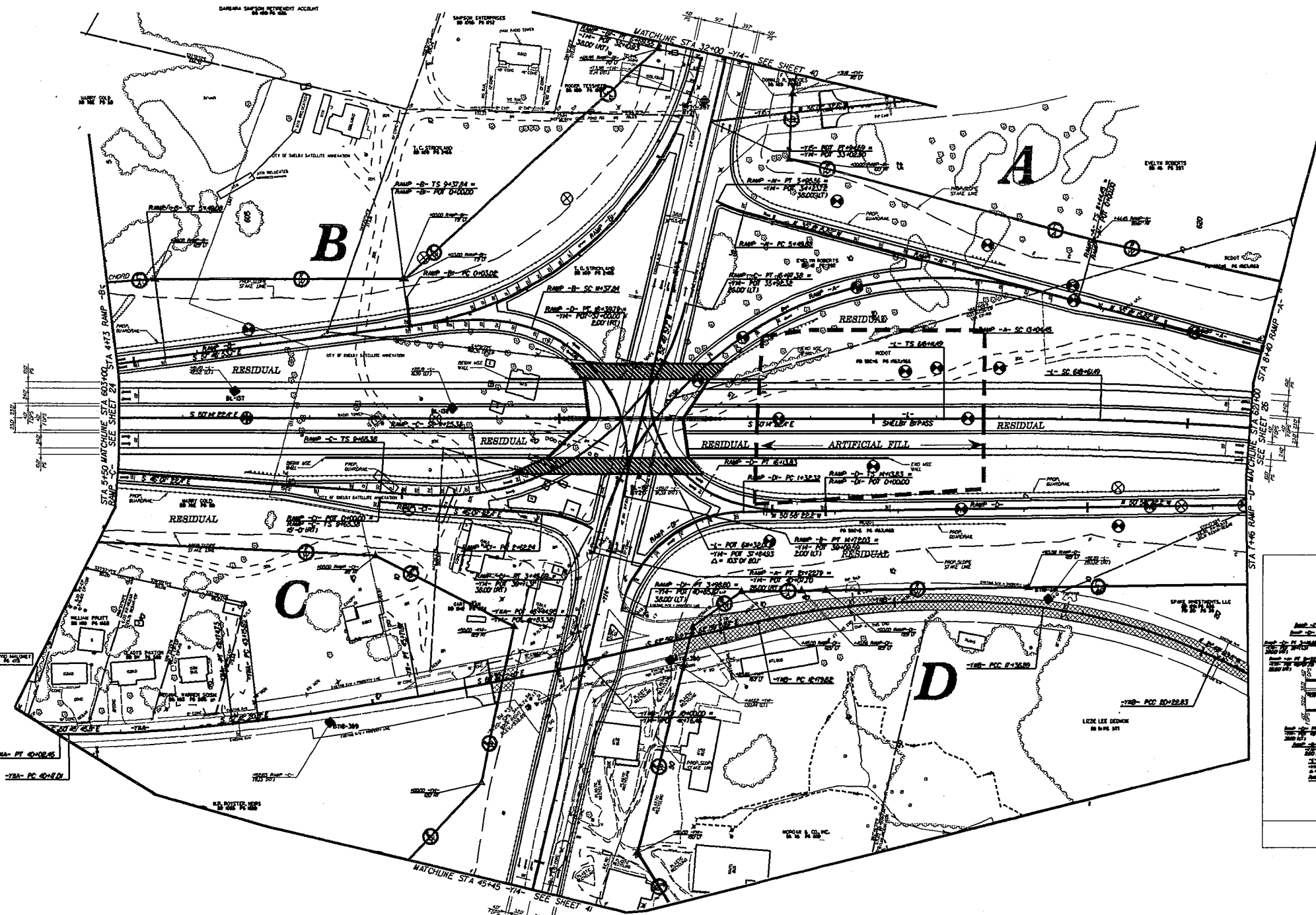
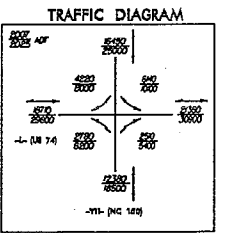
-Y13-	-Y11-REV
PI Sta 16+08.67	PI Sta 39+82.63
$\Delta = 32' 46" 01.2" (RT)$	$\Delta = 6' 25" 00.0" (L)$
D = 3' 00' 00.0'	Ls = 200.00'
L = 1092.23'	LT = 133.42'
T = 561.50'	ST = 66.75'
R = 1909.86'	

-Y11-	RAMP -B-
PI Sta 38+50.38	PI Sta 1+46.68
$\Delta = 36' 14" 03.9" (LT)$	$\Delta = 2' 31" 15.7" (L)$
D = 11' 30' 00.0"	Ls = 220.00'
L = 315.08'	LT = 146.68'
T = 163.01'	T = 54.55'
R = 498.22'	R = 2,500.00'
	SE = 08

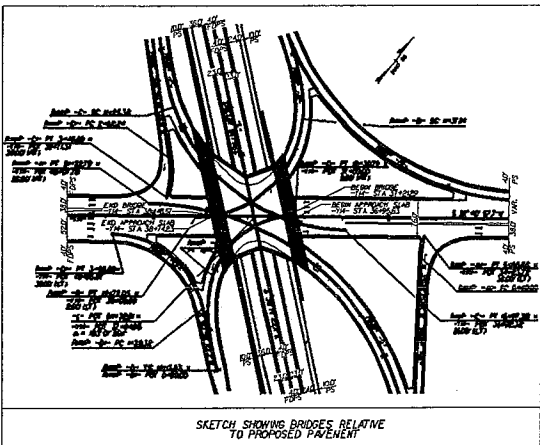
FOR -L- PROFILE SEE SHEETS 62 & 63  
 FOR RAMP B PROFILE SEE SHEET 75  
 FOR RAMP C PROFILE SEE SHEET 76  
 FOR -Y11-REV PROFILE SEE SHEETS 88 & 89

BYFORD

PROJECT NUMBER: R-2707C  
 SHEET NO.: 25  
 DATE: 5/29/02



<p>RAMP -A-</p> <p>PI Stn 4145.00          BE = 8.15          LE = 82.00          LT = 82.00          ST = 82.00          SE = 26</p>	<p>RAMP -B-</p> <p>PI Stn 4175.00          BE = 8.15          LE = 82.00          LT = 82.00          ST = 82.00          SE = 26</p>	<p>RAMP -C-</p> <p>PI Stn 4205.00          BE = 8.15          LE = 82.00          LT = 82.00          ST = 82.00          SE = 26</p>	<p>RAMP -D-</p> <p>PI Stn 4235.00          BE = 8.15          LE = 82.00          LT = 82.00          ST = 82.00          SE = 26</p>
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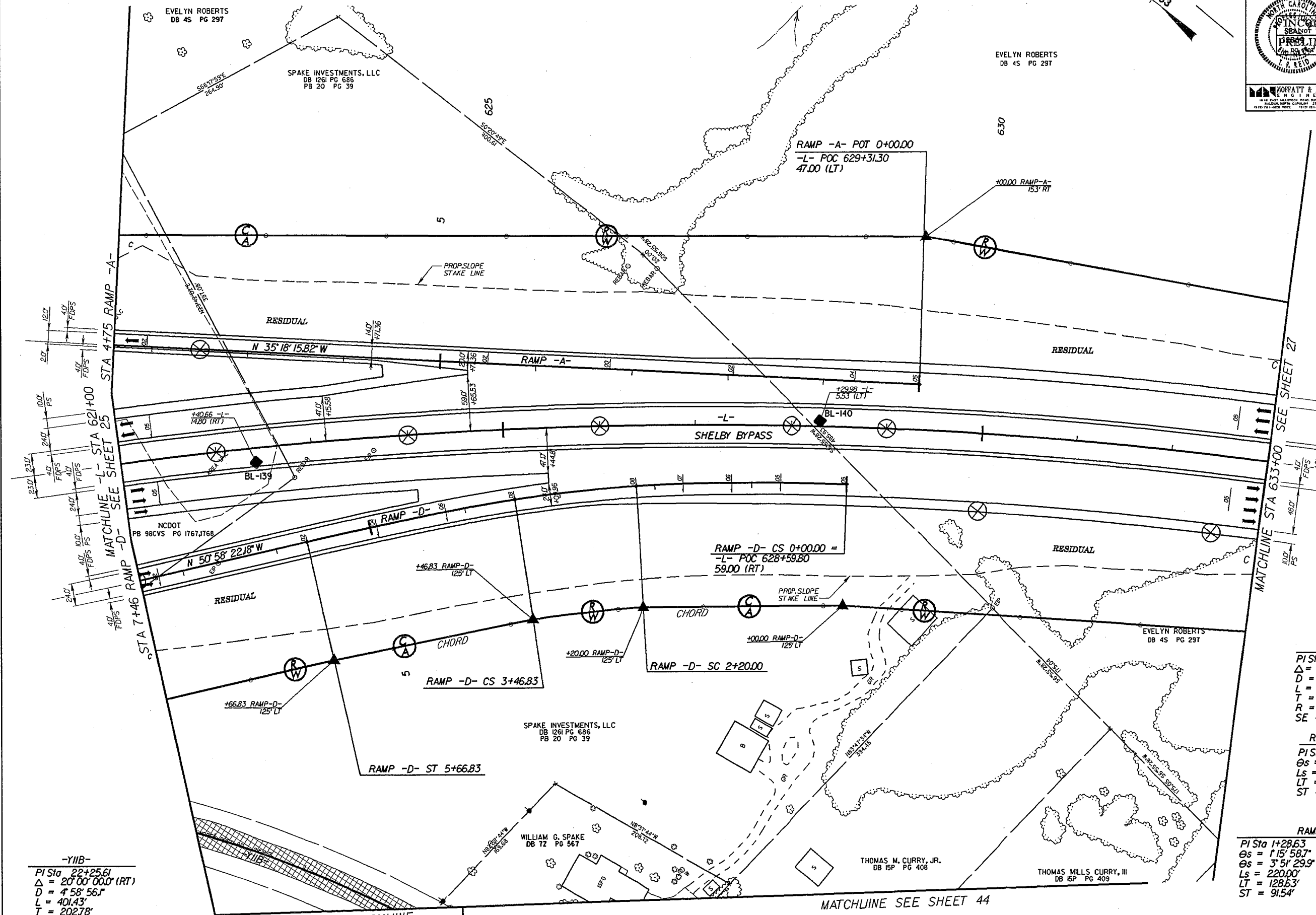
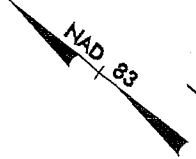


FOR -L- PROFILE SEE SHEET 23  
 FOR -T- PROFILE SEE SHEETS 20 & 21  
 FOR RAMP -A- PROFILE SEE SHEET 74  
 FOR RAMP -B- PROFILE SEE SHEET 74  
 FOR RAMP -C- PROFILE SEE SHEET 75  
 FOR RAMP -D- PROFILE SEE SHEET 75  
 FOR RAMP -E- PROFILE SEE SHEET 76  
 FOR RAMP -F- PROFILE SEE SHEET 76  
 FOR RAMP -G- PROFILE SEE SHEET 77  
 FOR RAMP -H- PROFILE SEE SHEET 77

INTERCHANGE AT  
 -L- US 74 BYPASS  
 AND -Y- NC 150

PROJECT NO. R-2707C CLEVELAND  
 DRAWN BY T. HUFFMAN  
 CHECKED BY T. REID DATE 5/29/02

GRAPHIC SCALE  
 0 20 40 80 100  
 FEET  
 PLANS



**-Y11B-**  
 PI Sta 22+25.61  
 $\Delta = 20'00''00.0''$  (RT)  
 $D = 4'58''56.1''$   
 $L = 401.43'$   
 $T = 202.78'$   
 $R = 1150.00'$

MATCHLINE  
SEE SHEET 43

MATCHLINE SEE SHEET 44

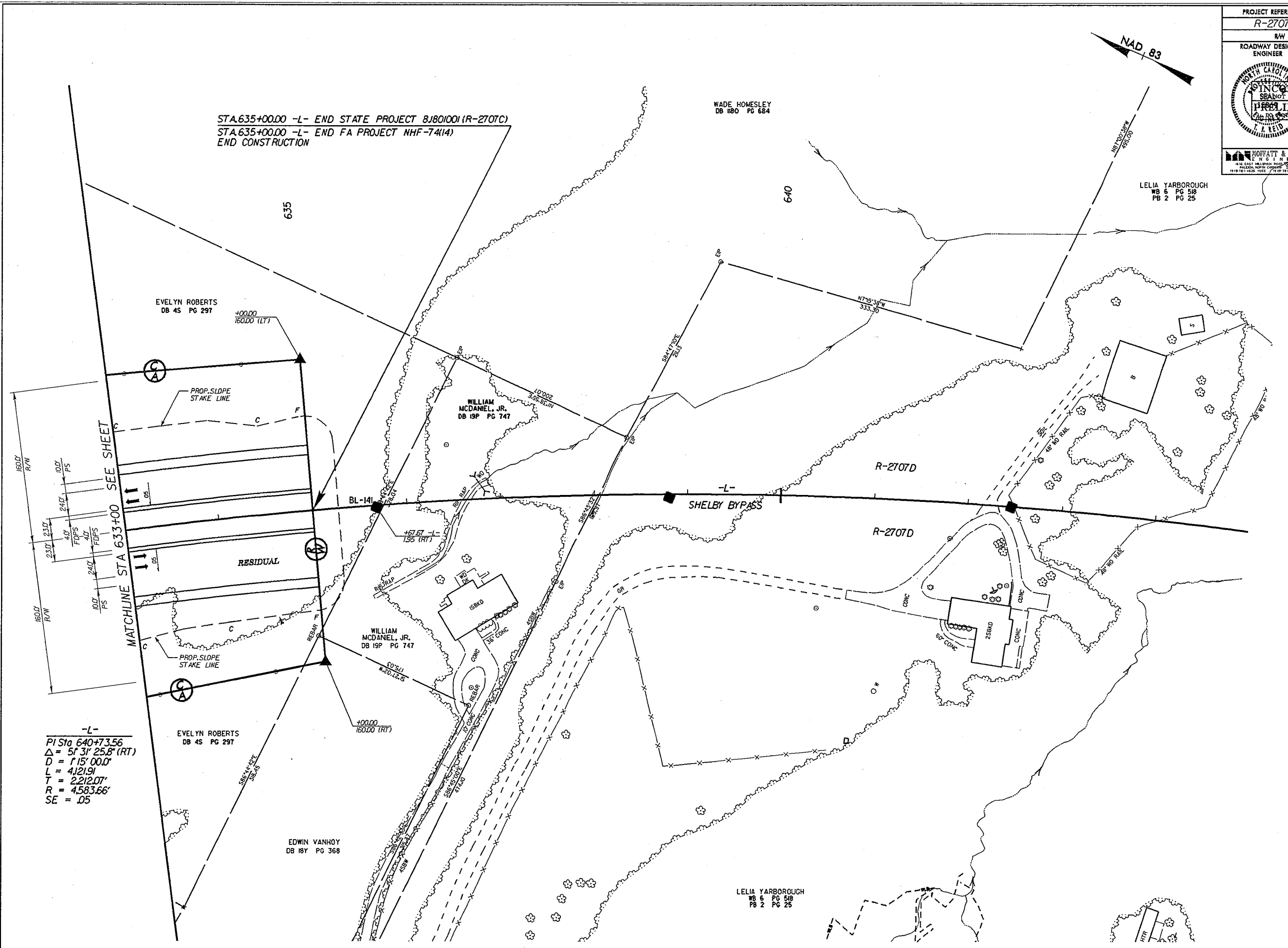
**-L-**  
 PI Sta 640+73.56  
 $\Delta = 5'31''25.8''$  (RT)  
 $D = 1'15''00.0''$   
 $L = 4121.91'$   
 $T = 2212.07'$   
 $R = 4583.66'$   
 $SE = .05$

**RAMP -D-**  
 PI Sta 4+20.20  
 $\Theta_s = 4'14''38.9''$   
 $L_s = 220.00'$   
 $LT = 146.71'$   
 $ST = 73.37'$

<b>RAMP -D-</b>	<b>PI Sta 1+28.63</b>	<b>PI Sta 2+83.45</b>
$\Theta_s = 1'15''58.7''$	$\Delta = 4'53''36.5''$ (LT)	$D = 3'51''29.9''$
$L_s = 220.00'$	$L = 126.83'$	$T = 63.45'$
$LT = 128.63'$	$R = 1,485.00'$	$SE = .05$
$ST = 91.54'$		

FOR -L- PROFILE SEE SHEETS 63 & 64  
 FOR RAMP -A- PROFILE SEE SHEET 73  
 FOR RAMP -D- PROFILE SEE SHEET 78

PROJECT REFERENCE NO. R-2707C	SHEET NO. 27
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>PRELIMINARY PLANS</b> <small>FOR REVIEW ONLY - NOT TO BE USED FOR CONSTRUCTION</small>	
HOFFATT & NICHOL ENGINEERS <small>114 EAST MAIN STREET, SUITE 100, WELLSVILLE, NORTH CAROLINA 28691</small> TEL: 704-738-1100 FAX: 704-738-1101	
SDG  Suncoast Design Group, P.A. <small>11401 W. BAYVIEW BLVD., SUITE 100, BOCA RATON, FLORIDA 33433</small> TEL: 561-993-1100 FAX: 561-993-1101	



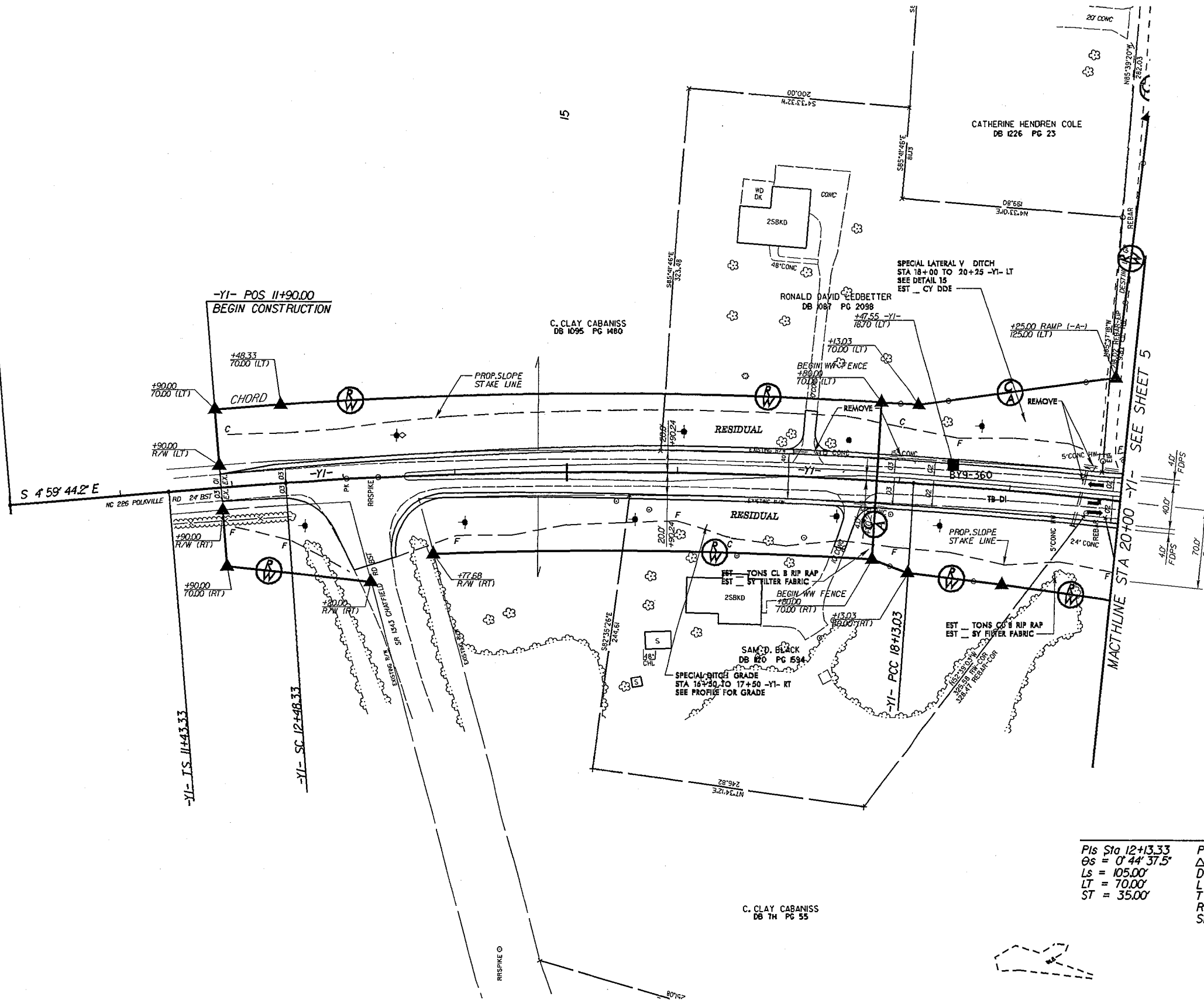
STA.635+00.00 -L- END STATE PROJECT 8J801001(R-2707C)  
 STA.635+00.00 -L- END FA PROJECT NHF-74(14)  
 END CONSTRUCTION

-L-  
 P1 Sta 640+73.56  
 $\Delta = 51' 31" 25.8" (RT)$   
 $D = 1' 15" 00.0"$   
 $L = 4121.91$   
 $T = 2212.07'$   
 $R = 4583.66'$   
 $SE = .05$

10

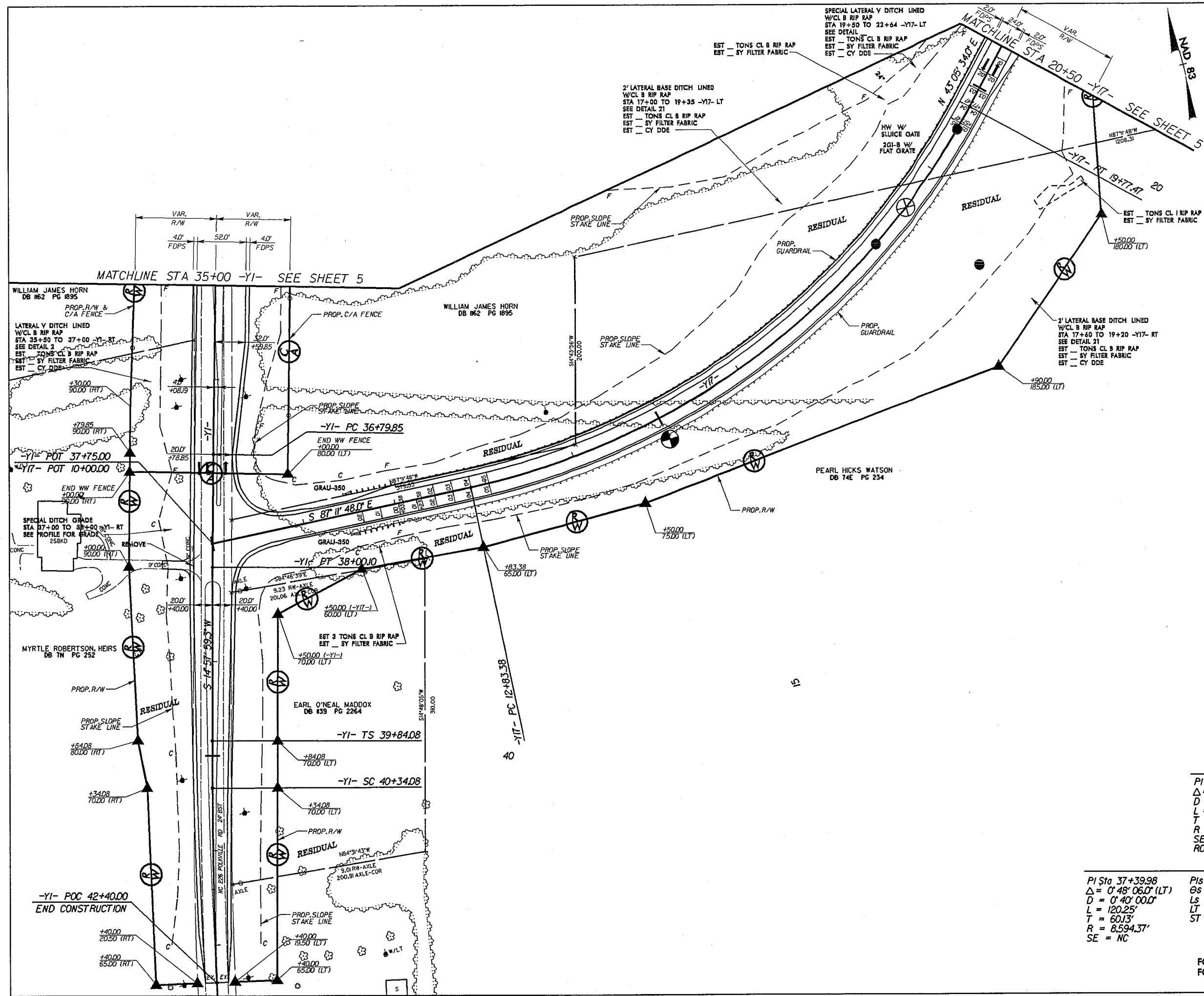
-YI- POT 10+00.00

NAD 83



-YI-		
PI Sta 12+13.33	PI Sta 15+31.4	PI Sta 24+03.61
Os = 0' 44' 37.5"	Δ = 8' 00' 00.0" (RT)	Δ = 11' 46' 11.9" (RT)
Ls = 105.00'	D = 1' 25' 00.0"	D = 1' 00' 00.0"
LT = 70.00'	L = 564.71'	L = 1,177.00'
ST = 35.00'	T = 282.81'	T = 590.58'
	R = 4044.41'	R = 5729.58'
	SE = .03	SE = .02
		RO = 72'

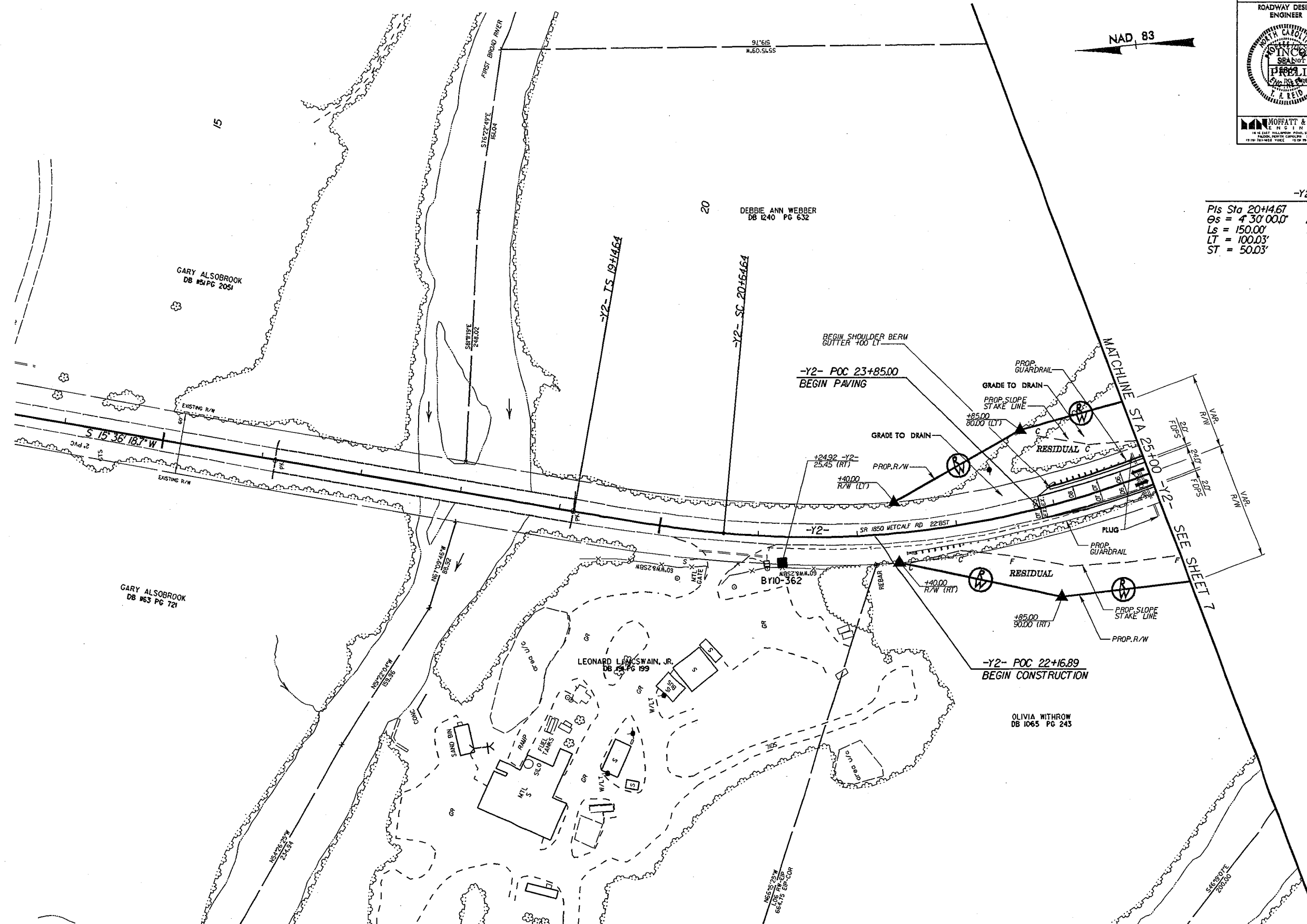
PROJECT REFERENCE NO. R-2707C	SHEET NO. 29
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



-Y17-  
 PI Sta 16+53.97  
 $\Delta = 49^\circ 42' 38.0''$  (LT)  
 $D = 7' 09' 43.1''$   
 $L = 694.09'$   
 $T = 370.59'$   
 $R = 800.00'$   
 $SE = .05$   
 $RO = 100'$

-Y1-	-Y1-	-Y1-
PI Sta 37+39.98	PI Sta 40+17.41	PI Sta 42+29.87
$\Delta = 0^\circ 48' 06.0''$ (LT)	$\Delta = 0^\circ 15' 00.0''$	$\Delta = 3^\circ 54' 51.5''$ (LT)
$D = 0' 40' 00.0''$	$Ls = 50.00'$	$D = 1' 00' 00.0''$
$L = 120.25'$	$LT = 33.33'$	$L = 391.43'$
$T = 60.13'$	$ST = 16.67'$	$T = 195.79'$
$R = 8,594.37'$		$R = 5,729.58'$
$SE = NC$		$SE = NC$

FOR -Y1- PROFILE SEE SHEETS 80 & 81  
 FOR -Y17- PROFILE SEE SHEETS 94 & 95



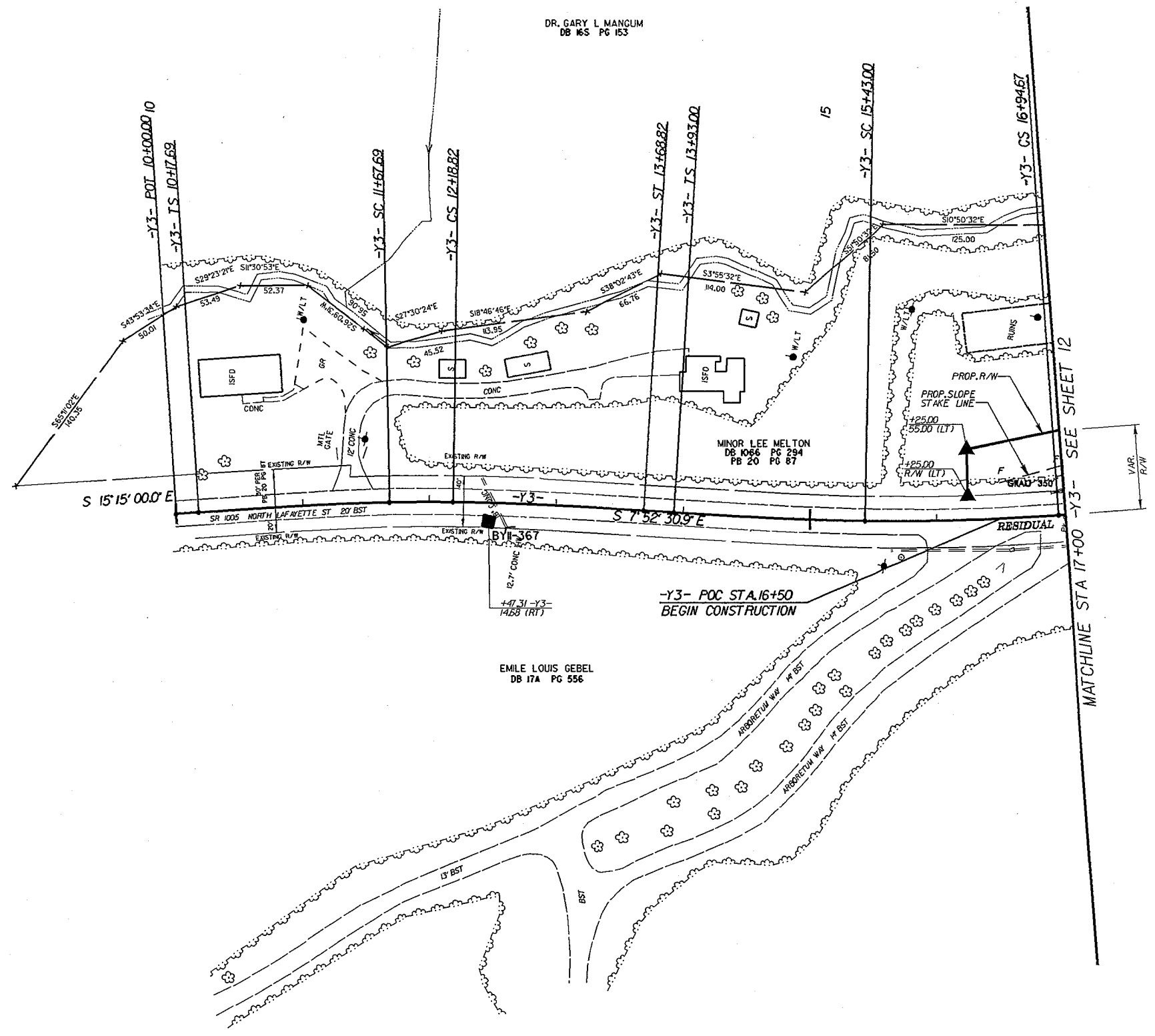
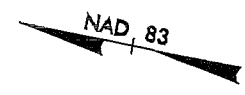
NAD 83

-Y2-

PI Sta 20+46.7	PI Sta 31+27.15
θs = 4° 30' 00.0"	Δ = 96° 06' 18.7" (LT)
Ls = 150.00'	D = 6' 00' 00.0"
LT = 100.03'	L = 1,601.75'
ST = 50.03'	T = 1,062.52'
	R = 954.93'
	SE = .06
	RO = 150'

SEE SHEET 7





DR. GARY L. MANCUM  
DB 16S PG 153

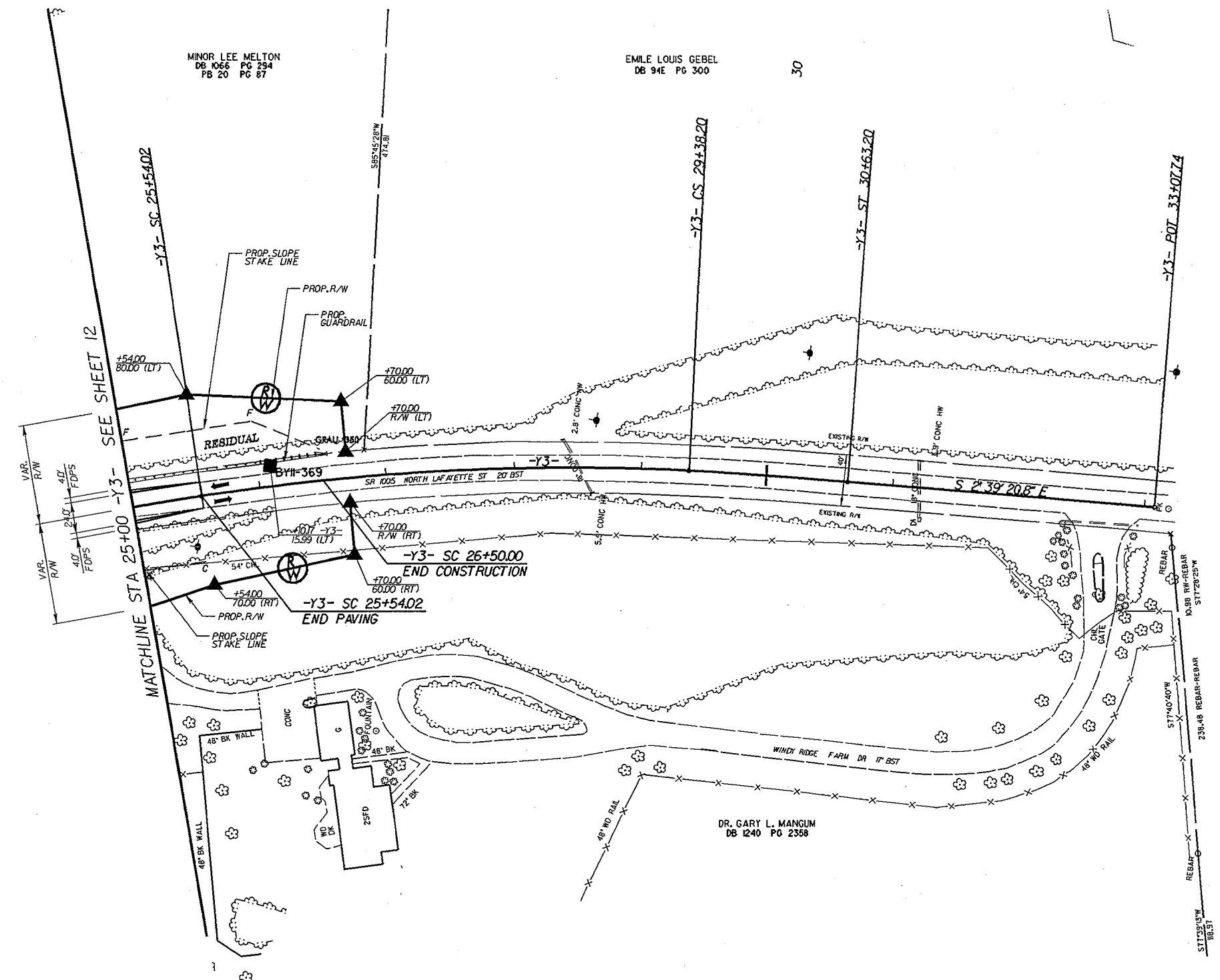
MINOR LEE MELTON  
DB 1066 PG 294  
PB 20 PG 87

EMILE LOUIS GEBEL  
DB 17A PG 556

-Y3-

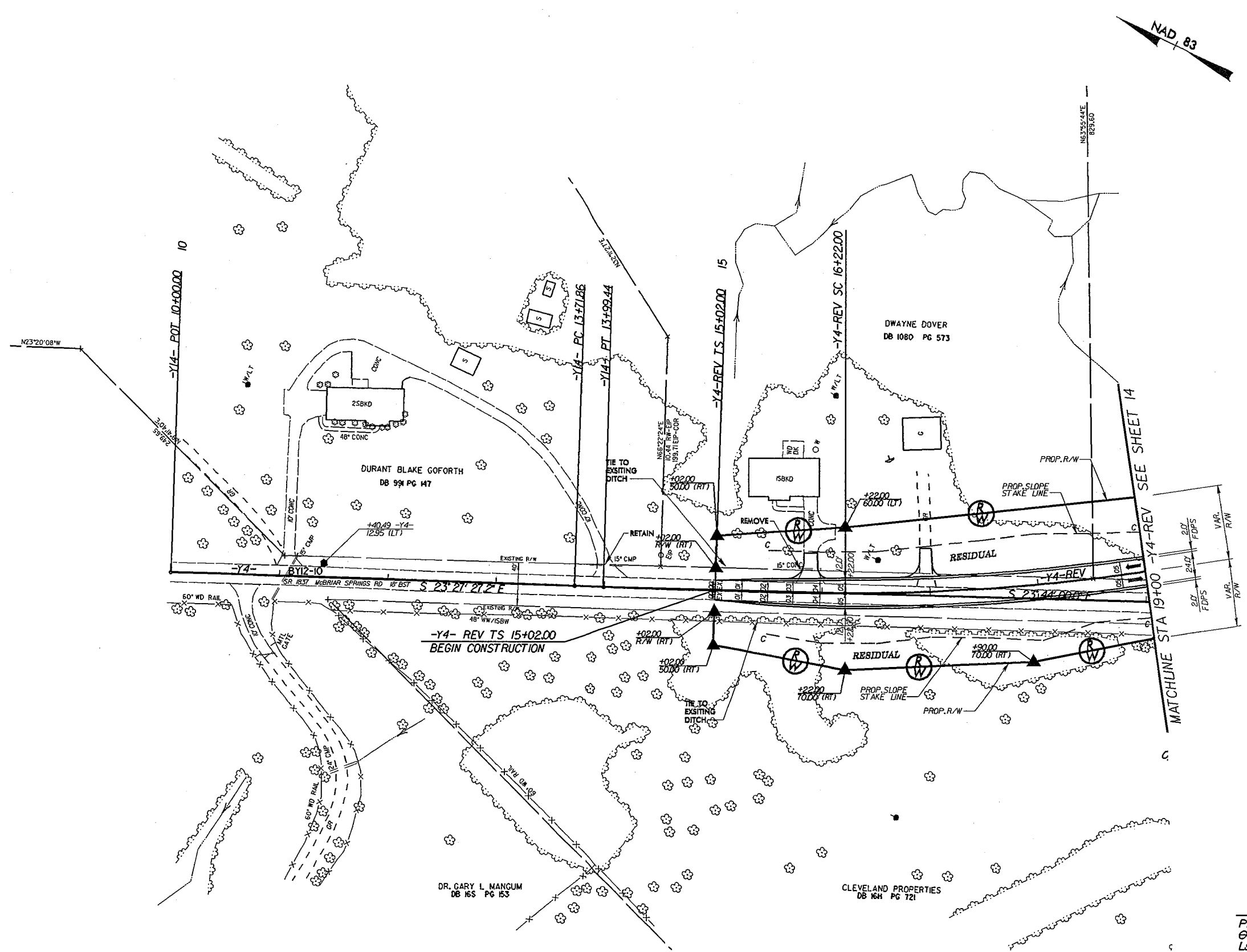
Pls Sta 11+17.70 Cs = 2° 45' 00.0" Ls = 150.00' LT = 100.01' ST = 50.01'	PI Sta 11+93.28 Δ = 1° 52' 29.1" (RT) D = 3° 40' 00.0" L = 5113 T = 25.57' R = 1562.61'	Pls Sta 12+68.83 Cs = 2° 45' 00.0" Ls = 150.00' LT = 100.01' ST = 50.01'
Pls Sta 14+93.01 Cs = 2° 30' 00.0" Ls = 150.00' LT = 100.01' ST = 50.01'	Pls Sta 17+44.68 Cs = 2° 30' 00.0" Ls = 150.00' LT = 100.01' ST = 50.01'	PI Sta 16+18.88 Δ = 5° 03' 21.5" (LT) D = 3° 20' 00.0" L = 151.68 T = 75.89' R = 1,718.87'

PROJECT REFERENCE NO. R-2707C	SHEET NO. 32
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



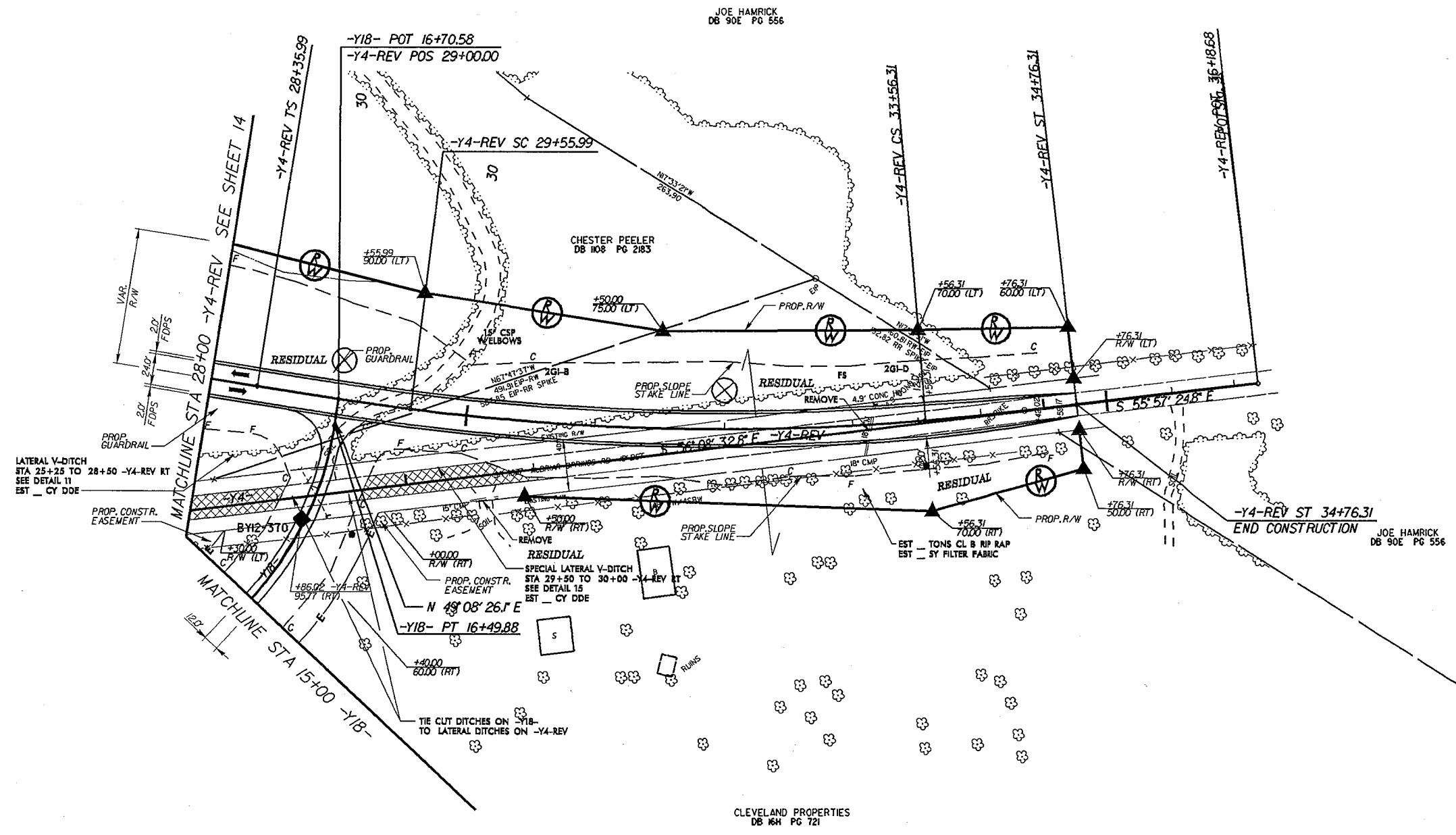
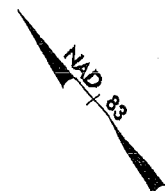
-Y3-

Pls Sta 25+12.36	Pls Sta 27+46.76	Pls Sta 29+79.88
Es = 1'52' 30.0"	Δ = 11' 31' 31.6" (RT)	Es = 1'52' 30.0"
Ls = 125.00'	D = 3' 00' 00.0"	Ls = 125.00'
LT = 83.34'	L = 384.18	LT = 83.34'
ST = 41.67'	T = 192.74'	ST = 41.67'
	R = 1,909.86'	
	SE = .08	



-Y4-  
 PI Sta 13+85.65  
 $\Delta = 0' 16' 32.7''$  (LT)  
 $D = 1' 00' 00.0''$   
 $L = 27.58'$   
 $T = 13.79'$   
 $R = 5729.58'$

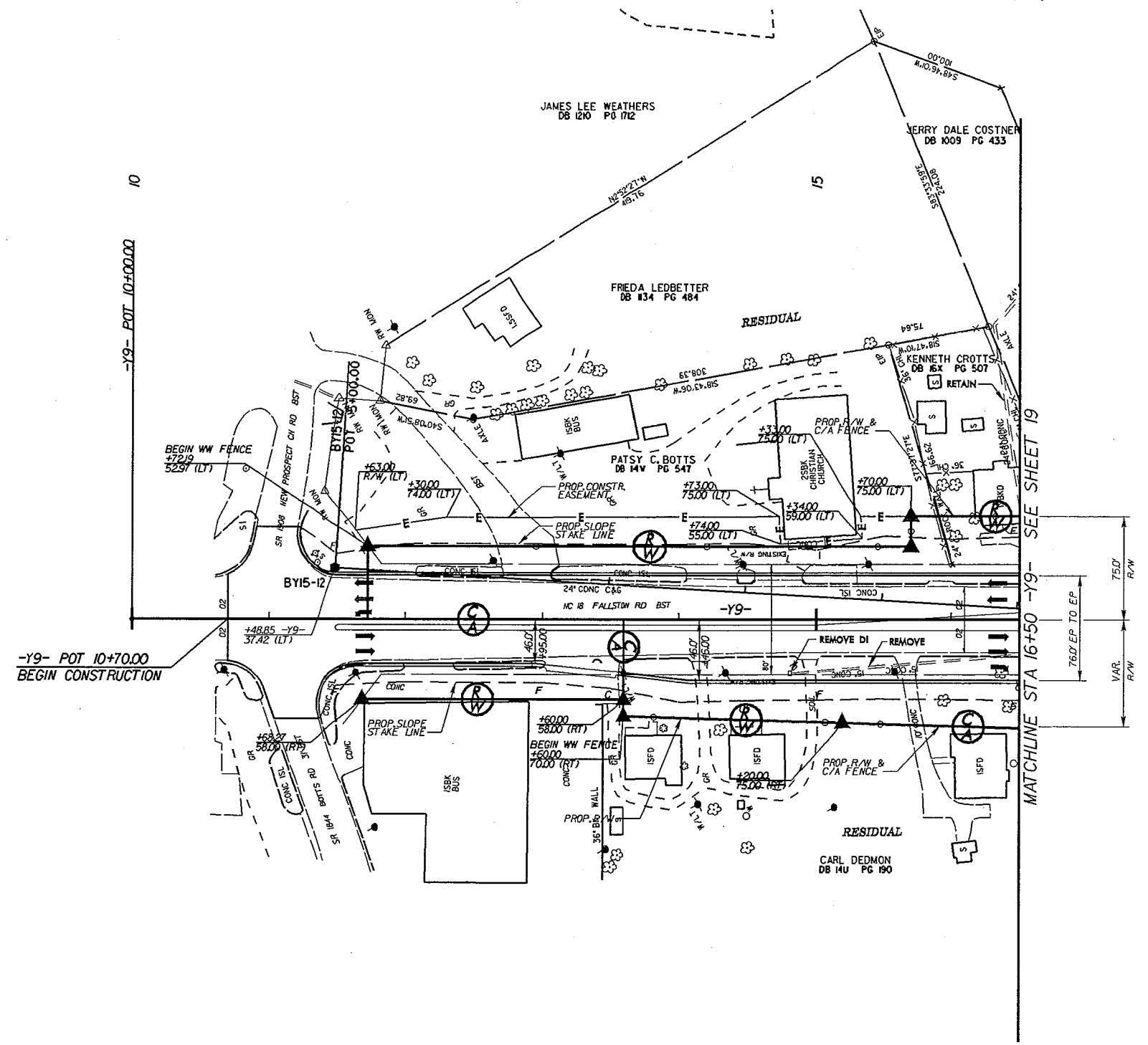
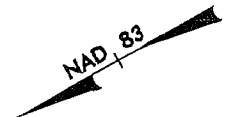
-Y4-REV  
 PIs Sta 15+82.00    PI Sta 18+44.49  
 $\Theta s = 1' 48' 00.0''$      $\Delta = 13' 17' 22.9''$  (LT)  
 $L s = 120.00'$      $D = 3' 00' 00.0''$   
 $LT = 80.00'$      $L = 442.99'$   
 $ST = 40.00'$      $T = 222.49'$   
                           $R = 1,909.86'$   
                           $SE = .05$



-Y4-REV		-Y1B-	
PIs Sta 29+15.99	PI Sta 31+56.89	PIs Sta 33+96.31	PI Sta 15+25.20
Es = 1' 48" 00.0'	Δ = 12' 00" 34.7' (LT)	Es = 1' 48" 00.0'	Δ = 65' 15" 10.8' (LT)
Ls = 120.00'	D = 3' 00" 00.0'	Ls = 120.00'	D = 22' 55" 05.9'
LT = 80.00'	L = 400.32	LT = 80.00'	L = 284.72'
ST = 40.00'	T = 200.90'	ST = 40.00'	T = 160.04'
	R = 1909.86'		R = 250.00'
	SE = .05		

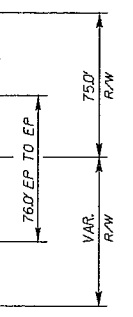
FOR -Y4-REV PROFILE SEE SHEET 83  
 FOR -Y1B- PROFILE SEE SHEET 96

PROJECT REFERENCE NO. R-2707C	SHEET NO. 35
RAW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

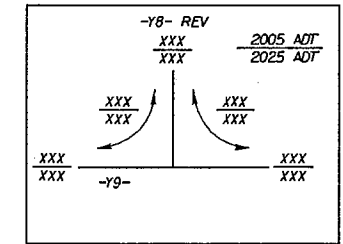
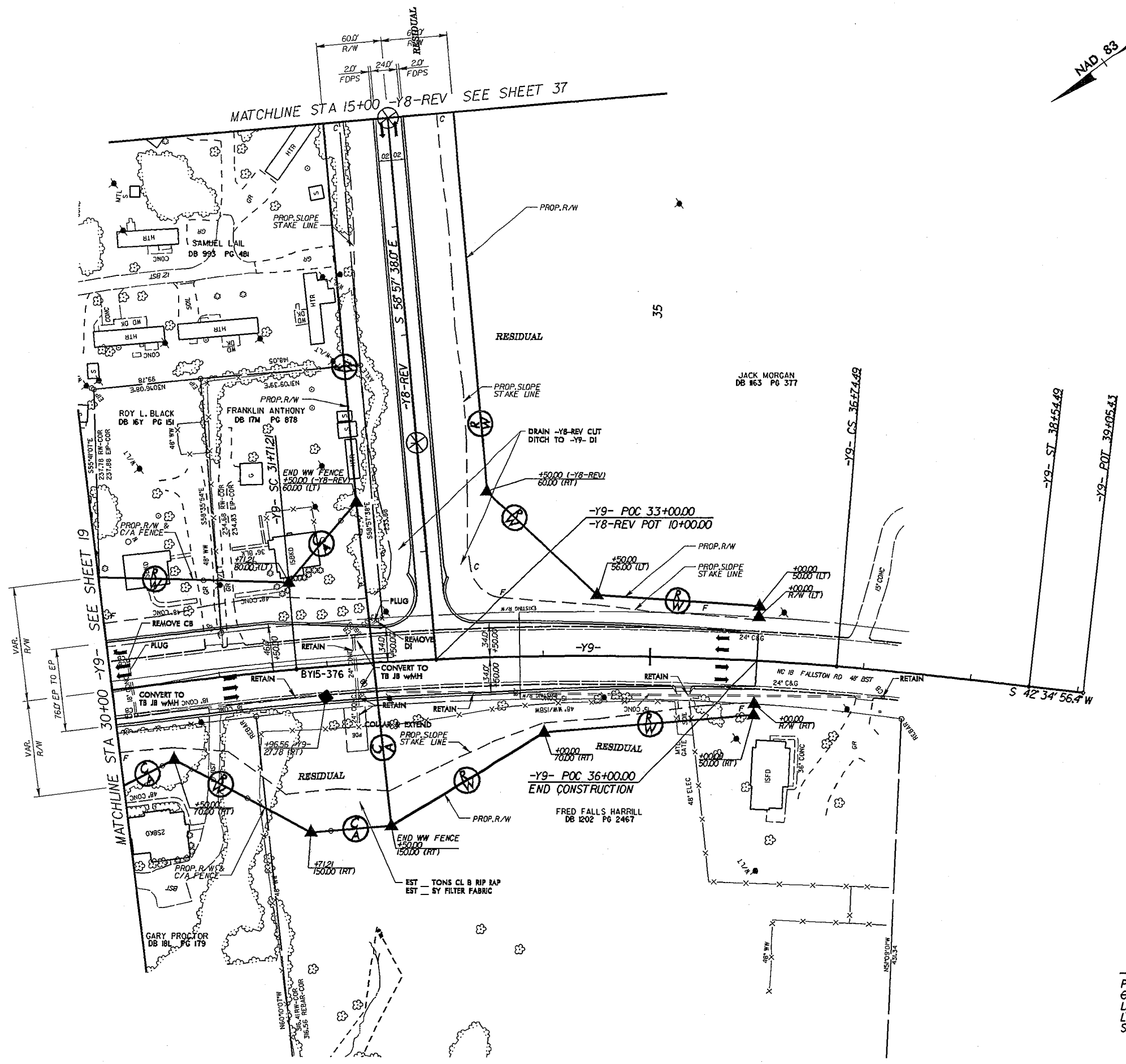
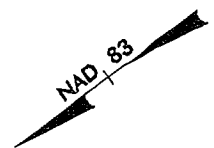


-Y9- POT 10+70.00  
BEGIN CONSTRUCTION

MATCHLINE STA 16+50 -Y9- SEE SHEET 19



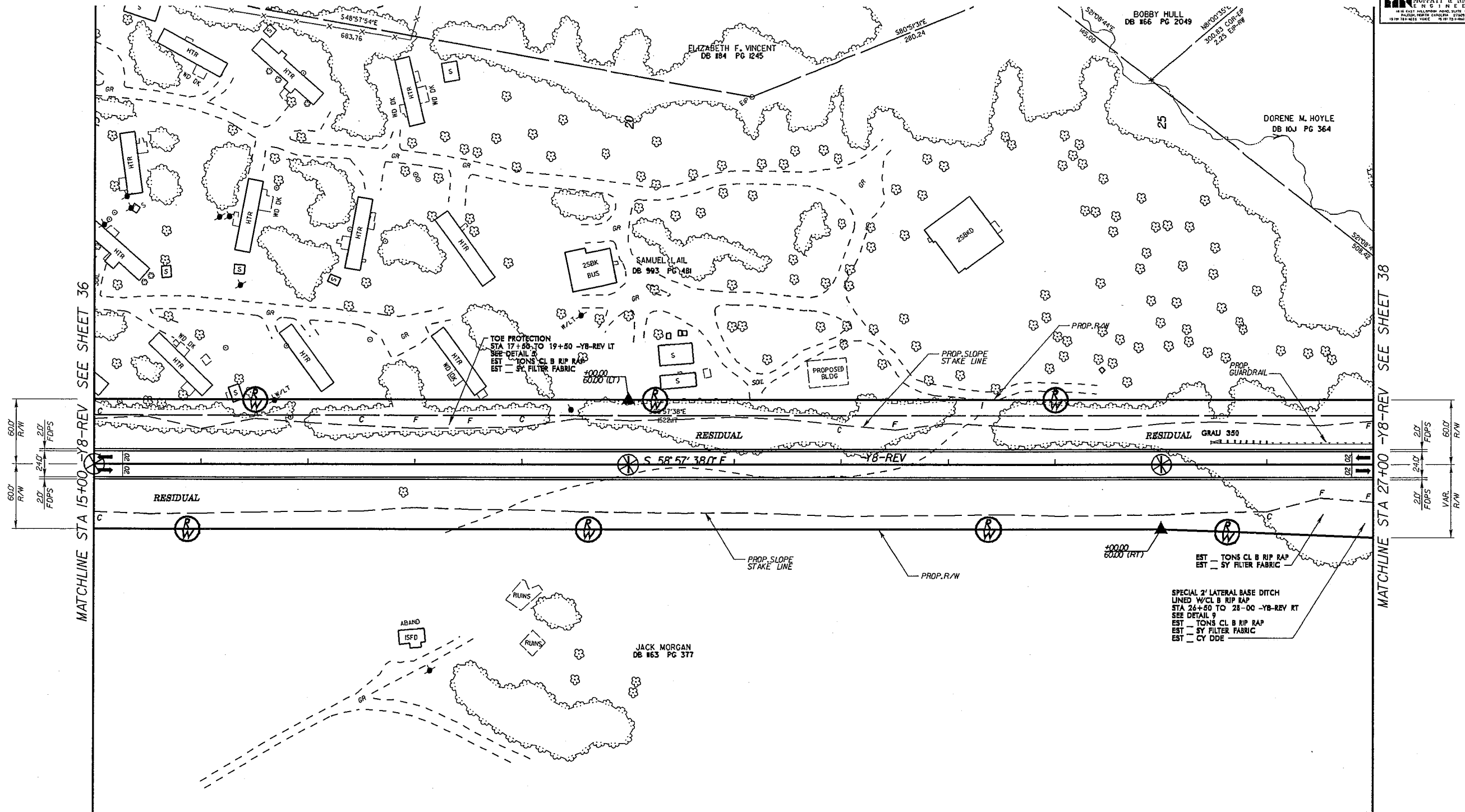
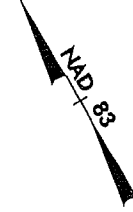
PROJECT REFERENCE NO. R-2707C	SHEET NO. 36
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



-Y9-		
Pis Sta 31+11.21	Pi Sta 34+23.50	Pis Sta 37+34.50
Es = 1'48" 00.0"	Δ = 10'03" 56.4" (RT)	Es = 1'48" 00.0"
Ls = 180.00'	D = 2'00" 00.0"	Ls = 180.00'
LT = 120.01'	L = 503.28'	LT = 120.01'
ST = 60.01'	T = 252.29'	ST = 60.01'
	R = 2,864.79'	
	SE = .04	

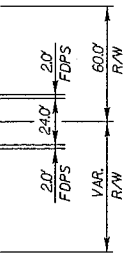
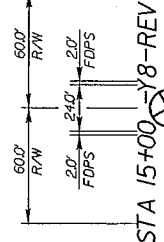
FOR -Y9- PROFILE SEE SHEET 87  
FOR -Y8-REV PROFILE SEE SHEET 85

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>37</b>
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

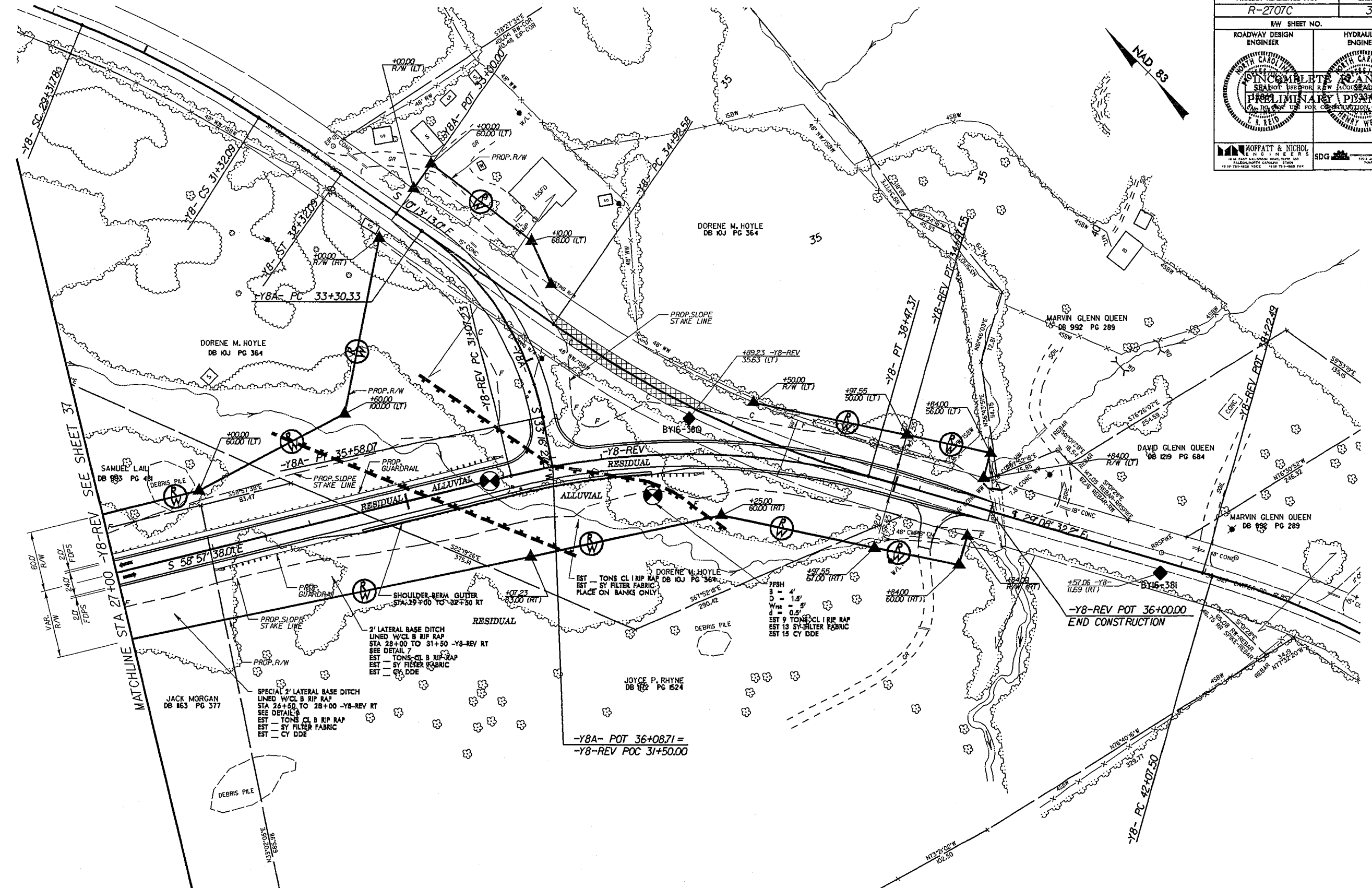


MATCHLINE STA 15+00 -Y8-REV SEE SHEET 36

MATCHLINE STA 27+00 -Y8-REV SEE SHEET 38



SPECIAL 2' LATERAL BASE DITCH  
LINED W/CL B RIP RAP  
STA 26+50 TO 28-00 -Y8-REV RT  
SEE DETAIL 9  
EST - TONS CL B RIP RAP  
EST - SY FILTER FABRIC  
EST - CY DDE

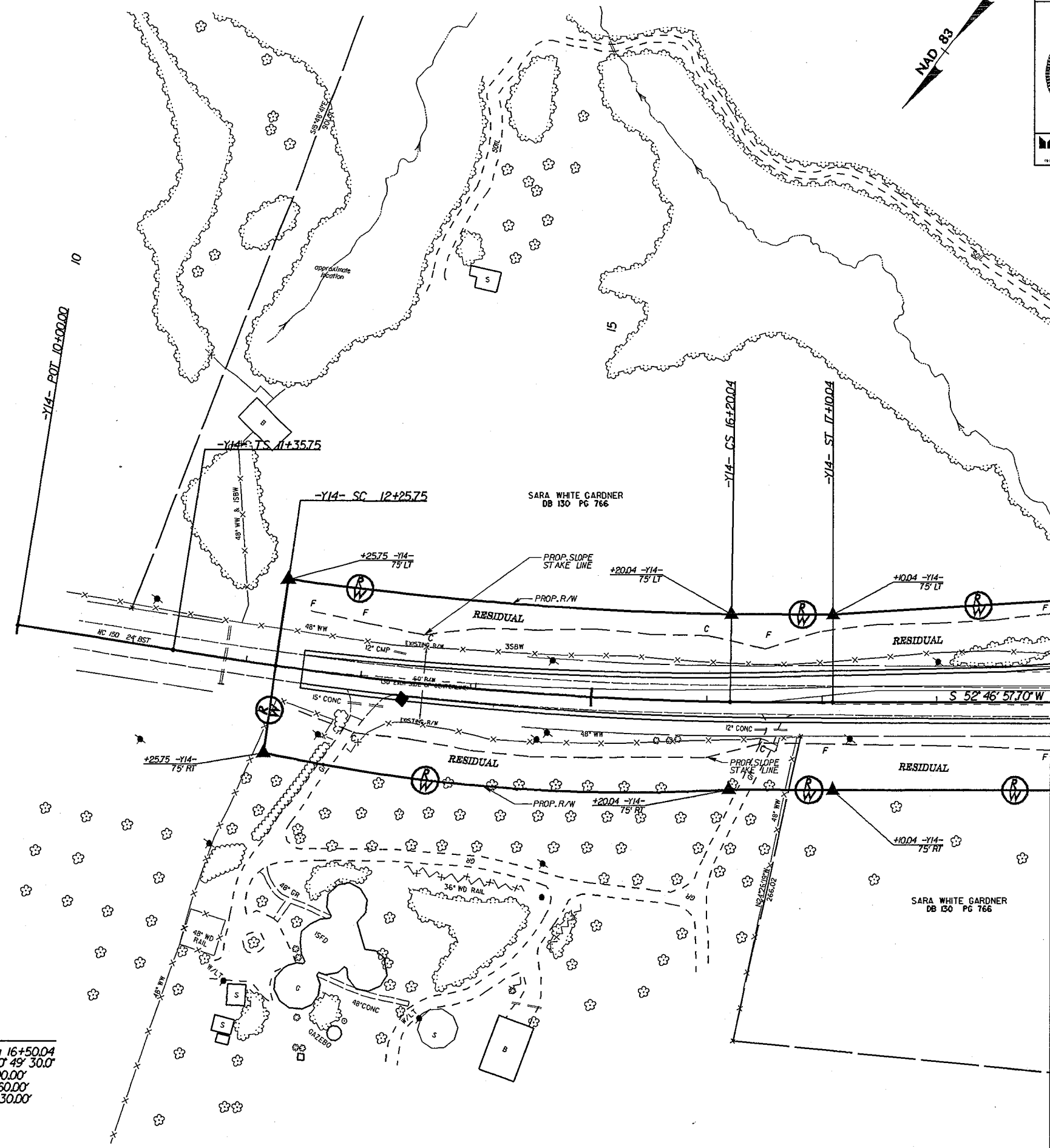
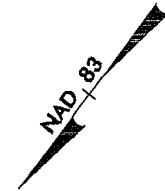


-Y8-			-Y8-			-Y8-		
PI Sta 28+98.45	PI Sta 30+32.20	PI Sta 31+65.43	PI Sta 36+71.61	PI Sta 43+89.21				
$\Delta s = 2^{\circ} 34' 01.3''$	$\Delta = 10^{\circ} 17' 03.1''$ (RT)	$\Delta s = 2^{\circ} 34' 01.3''$	$\Delta = 18^{\circ} 55' 19.2''$ (LT)	$\Delta = 23^{\circ} 17' 46.6''$ (RT)				
Ls = 100.00'	D = 5^{\circ} 08' 02.5''	Ls = 100.00'	D = 5^{\circ} 20' 00.0''	D = 6^{\circ} 30' 00.0''				
LT = 66.67'	L = 200.31'	LT = 66.67'	L = 354.79'	L = 358.40'				
ST = 33.34'	T = 100.43'	ST = 33.34'	T = 179.02'	T = 181.71'				
	R = 1116.00'		R = 1074.30'	R = 881.47'				

-Y8A-		-Y8-REV	
PI Sta 34+50.00	PI Sta 33+06.92	PI Sta 34+50.00	PI Sta 33+06.92
$\Delta = 43^{\circ} 29' 40.5''$ (RT)	$\Delta = 29^{\circ} 49' 05.8''$ (RT)	$\Delta = 43^{\circ} 29' 40.5''$ (RT)	$\Delta = 29^{\circ} 49' 05.8''$ (RT)
D = 19^{\circ} 05' 54.9''	D = 7^{\circ} 38' 22.0''	D = 19^{\circ} 05' 54.9''	D = 7^{\circ} 38' 22.0''
L = 227.74'	L = 390.32'	L = 227.74'	L = 390.32'
T = 119.67'	T = 199.69'	T = 119.67'	T = 199.69'
R = 300.00'	R = 750.00'	R = 300.00'	R = 750.00'
SE = .08	SE = .08	SE = .08	RO = 200'

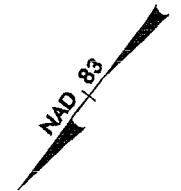
FOR -Y8A- PROFILE SEE SHEET 86  
FOR -Y8-REV PROFILE SEE SHEET 85



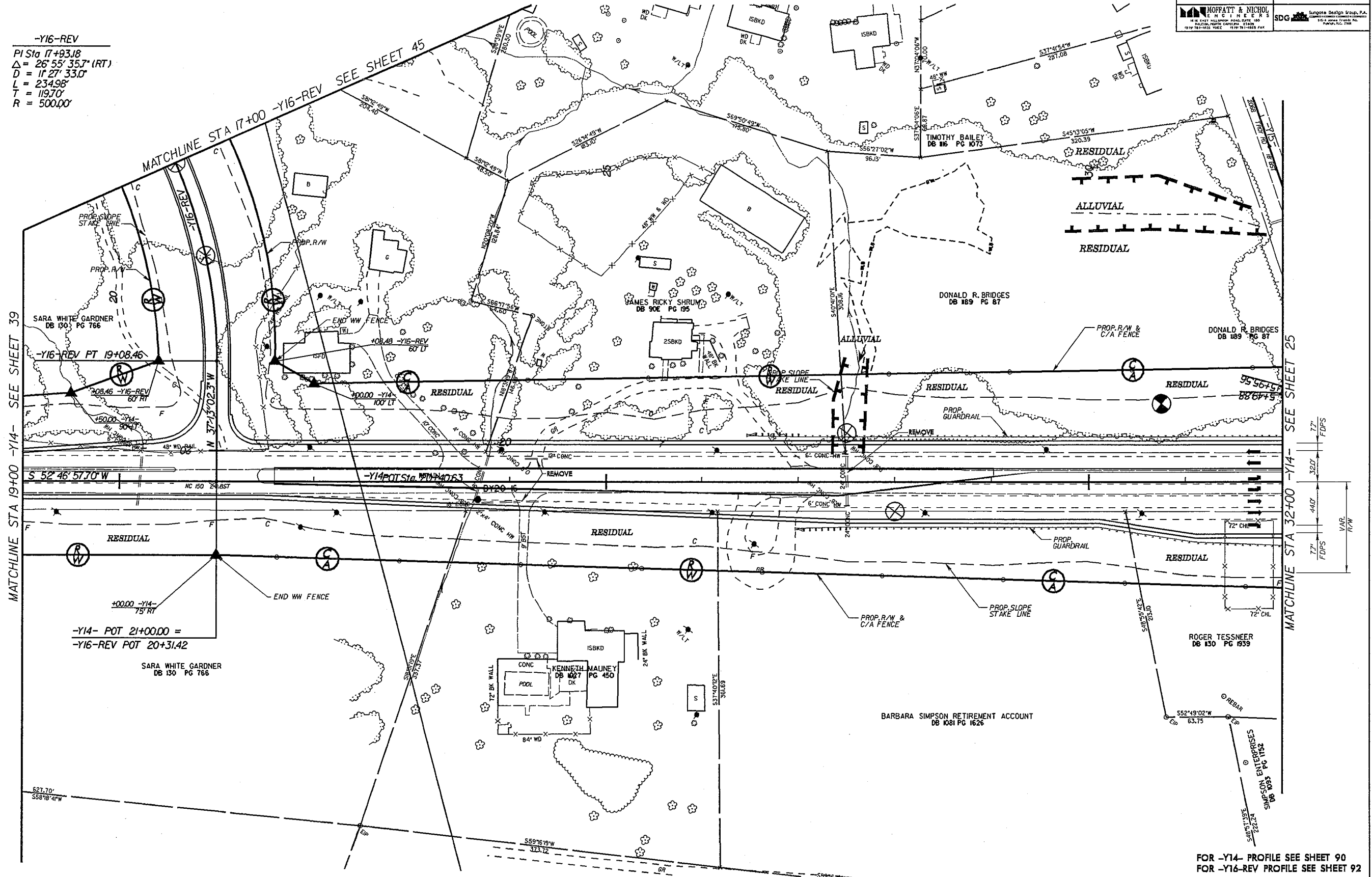


-Y14-		
Pls Sta 11+9575	PI Sta 14+2315	Pls Sta 16+5004
Os = 0° 49' 30.0"	Δ = 7° 13' 43.1" (LT)	Os = 0° 49' 30.0"
Ls = 90.00'	D = 1,50' 00.0"	Ls = 90.00'
LT = 60.00'	L = 394.29	LT = 60.00'
ST = 30.00'	T = 197.41'	ST = 30.00'
	R = 3,125.22'	

MATCHLINE STA 19+00 -Y14- SEE SHEET 40



-Y16-REV  
 PI Sta 17+93.8  
 $\Delta = 26^{\circ} 55' 35.7''$  (RT)  
 $D = 11^{\circ} 27' 33.0''$   
 $L = 234.98'$   
 $T = 119.70'$   
 $R = 500.00'$

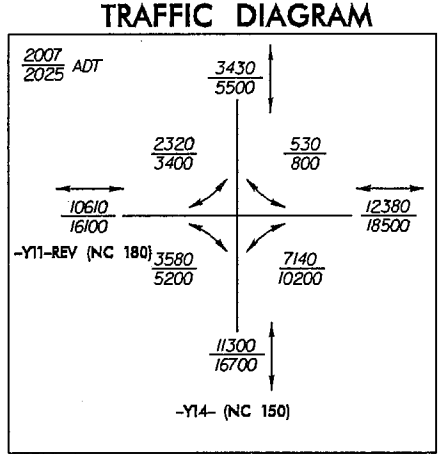
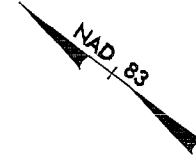
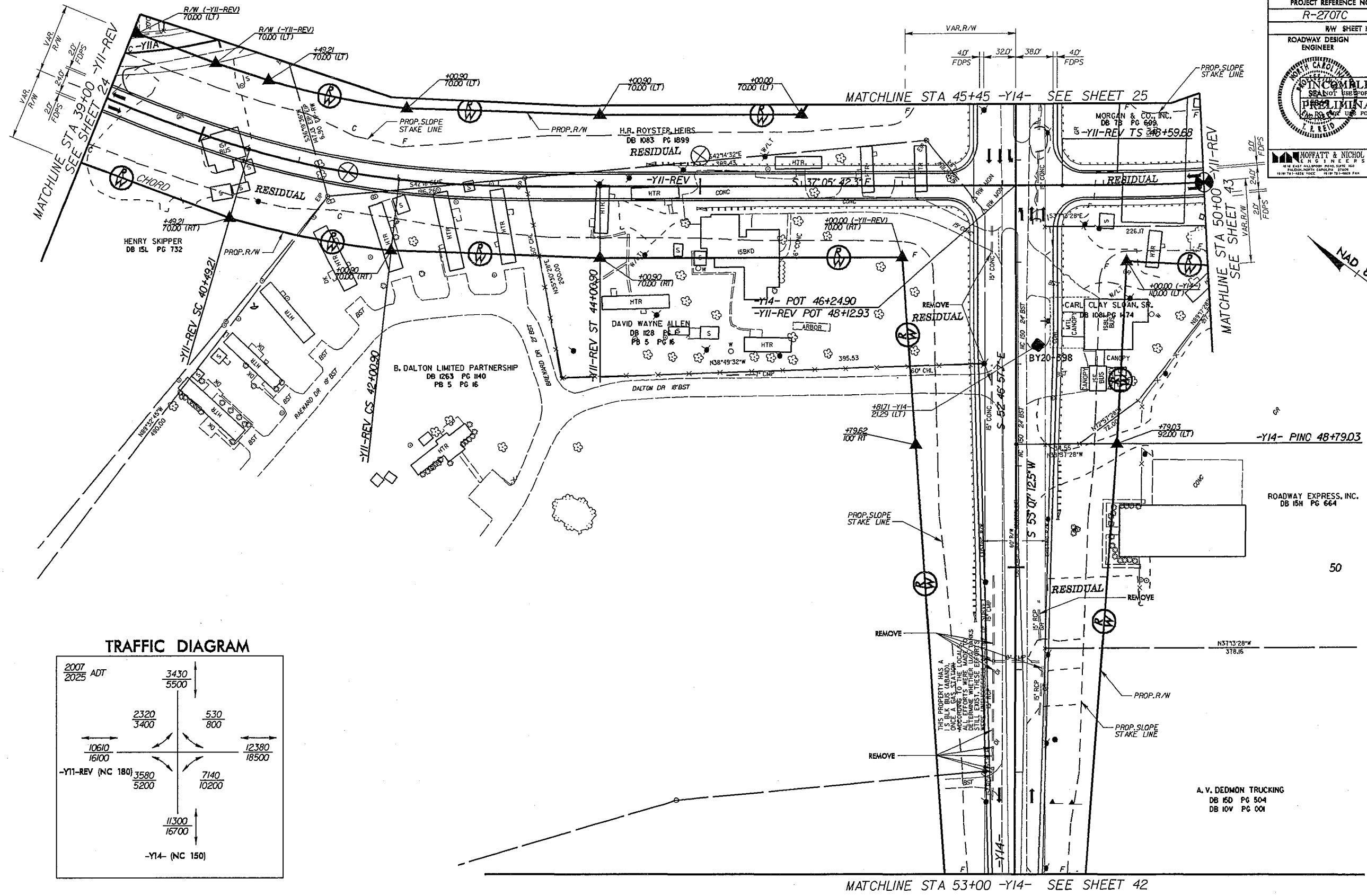


MATCHLINE STA 19+00 -Y14- SEE SHEET 39

MATCHLINE STA 32+00 -Y14- SEE SHEET 25

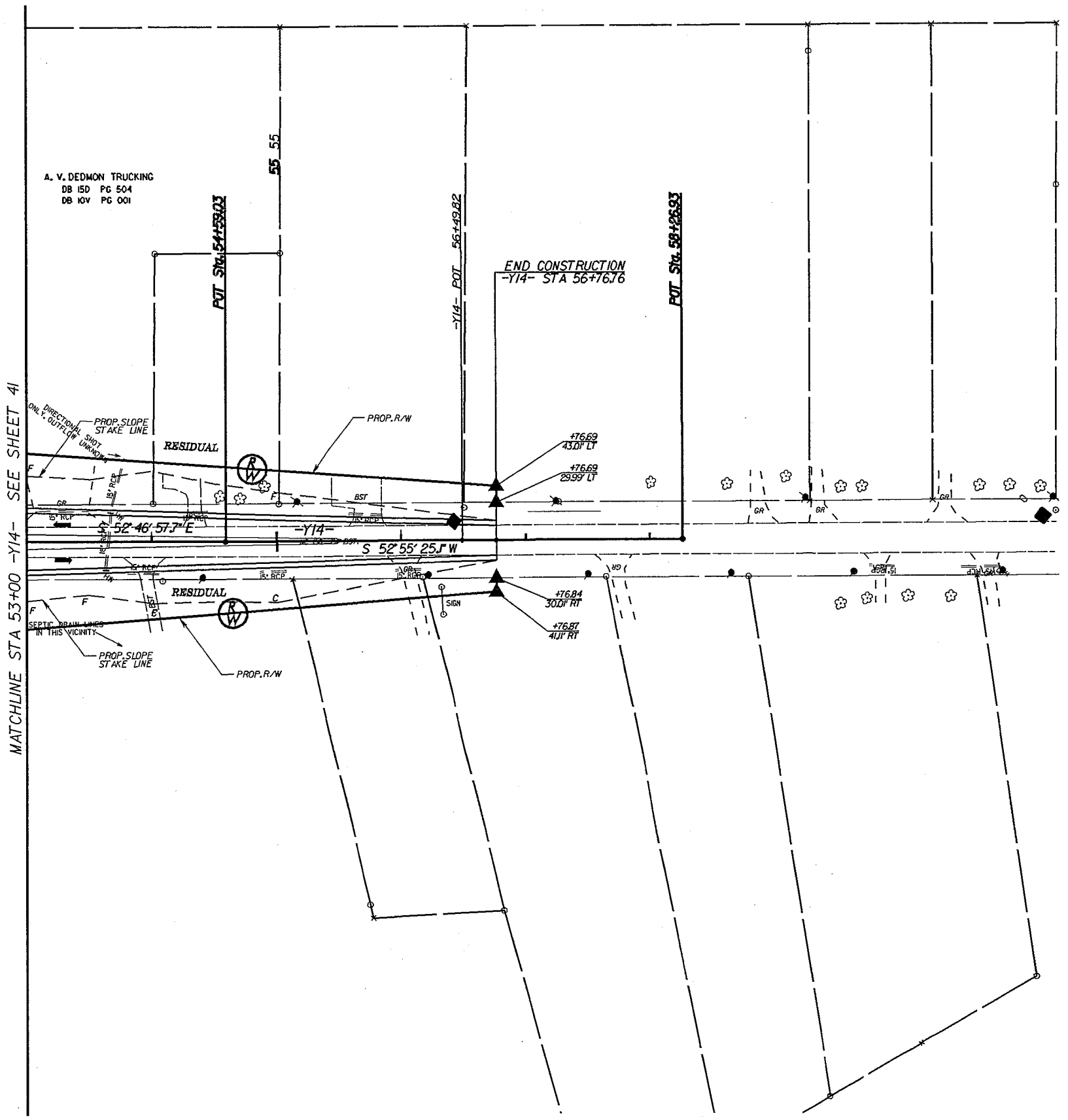
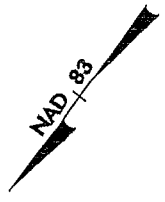
-Y14- POT 21+00.00 =  
 -Y16-REV POT 20+31.42

FOR -Y14- PROFILE SEE SHEET 90  
 FOR -Y16-REV PROFILE SEE SHEET 92







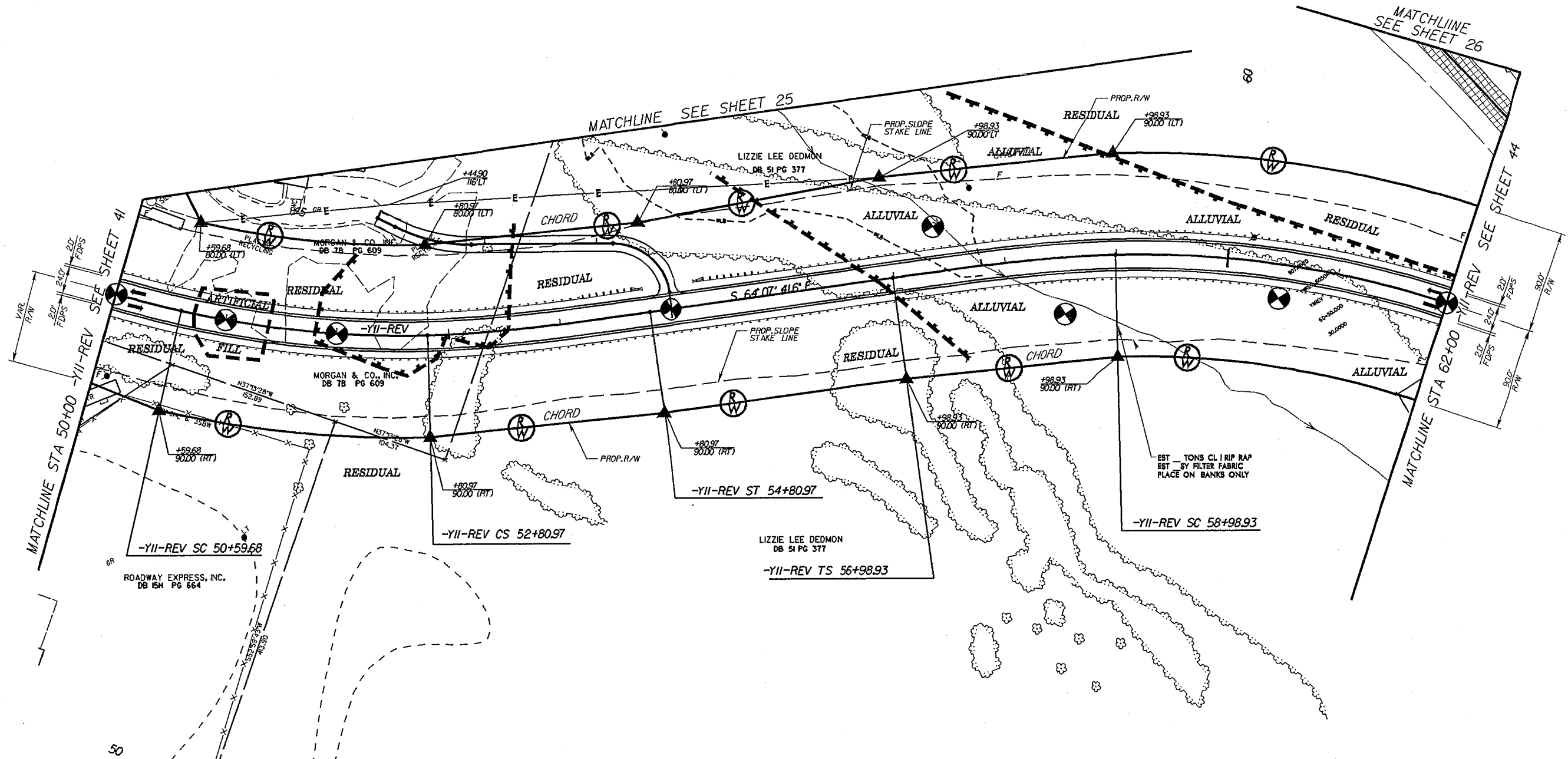
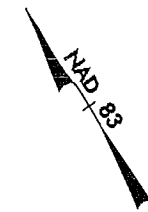
-YII-REV			
Pis Sta 39+82.63	PI Sta 41+25.24	Pis Sta 42+67.65	Pis Sta 49+93.10
Os = 6' 25' 00.0"	Δ = 9' 44' 00.4" (LT)	Os = 6' 25' 00.0"	Os = 6' 25' 00.0"
Ls = 200.00'	D = 6' 25' 00.0"	Ls = 200.00'	Ls = 200.00'
LT = 133.42'	L = 151.69'	LT = 133.42'	LT = 133.42'
ST = 66.75'	T = 76.03'	ST = 66.75'	ST = 66.75'
	R = 892.92'		
	SE = .08		

PROJECT REFERENCE NO. R-2707C		SHEET NO. 42	
RW SHEET NO.			
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION			
 MOFFATT & NICHOL ENGINEERS 18 EAST WASHINGTON STREET, SUITE 400 RALEIGH, NORTH CAROLINA 27601 919.974.4626 VOICE 919.974.7549 FAX		 SDG Suncoast Design Group, P.A. 317 S. JONES STREET, SUITE 200 PORTLAND, OREGON 97204 503.251.1234	



MATCHLINE STA 53+00 -Y14- SEE SHEET 41

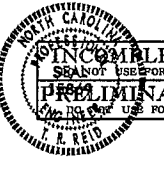

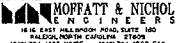

PROJECT REFERENCE NO. R-2707C		SHEET NO. 43	
RW SHEET NO.			
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
			
			

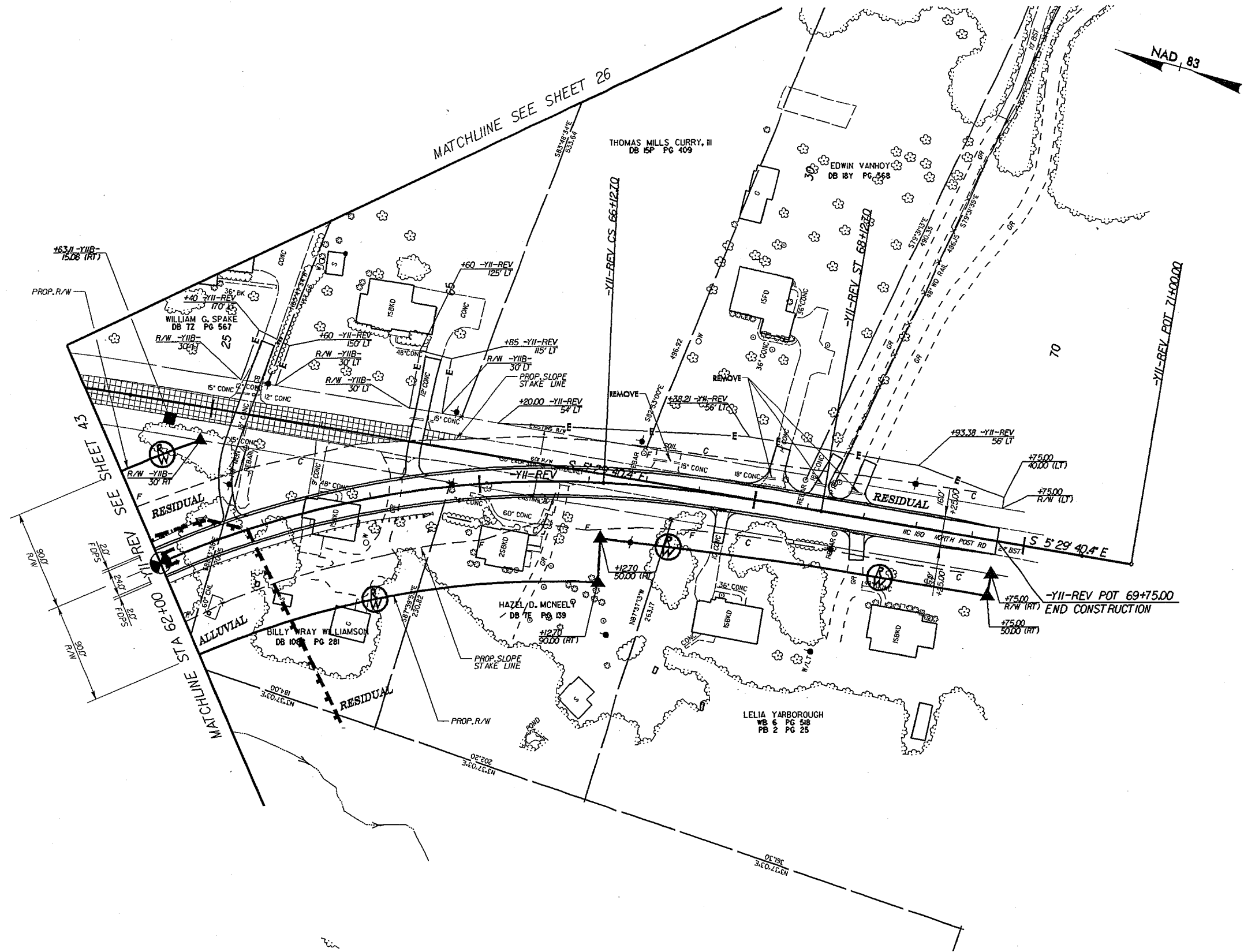


-YII-REV				
PI Sta 49+93.10	PI Sta 51+70.89	PI Sta 53+47.72	PI Sta 58+32.35	PI Sta 62+76.12
Os = 6' 25' 00.0"	Δ = 14' 11' 59.3" (LT)	Os = 6' 25' 00.0"	Os = 6' 25' 00.0"	Δ = 45' 48' 01.2" (RT)
Ls = 200.00'	D = 6' 25' 00.0"	Ls = 200.00'	Ls = 200.00'	D = 6' 25' 00.0"
LT = 133.42'	L = 221.30'	LT = 133.42'	LT = 133.42'	L = 713.77'
ST = 66.75'	T = 111.22'	ST = 66.75'	ST = 66.75'	T = 377.19'
	R = 892.92'			R = 892.92'
	SE = .08			SE = .08

8/17/99

22-MAY-2008 09:55  
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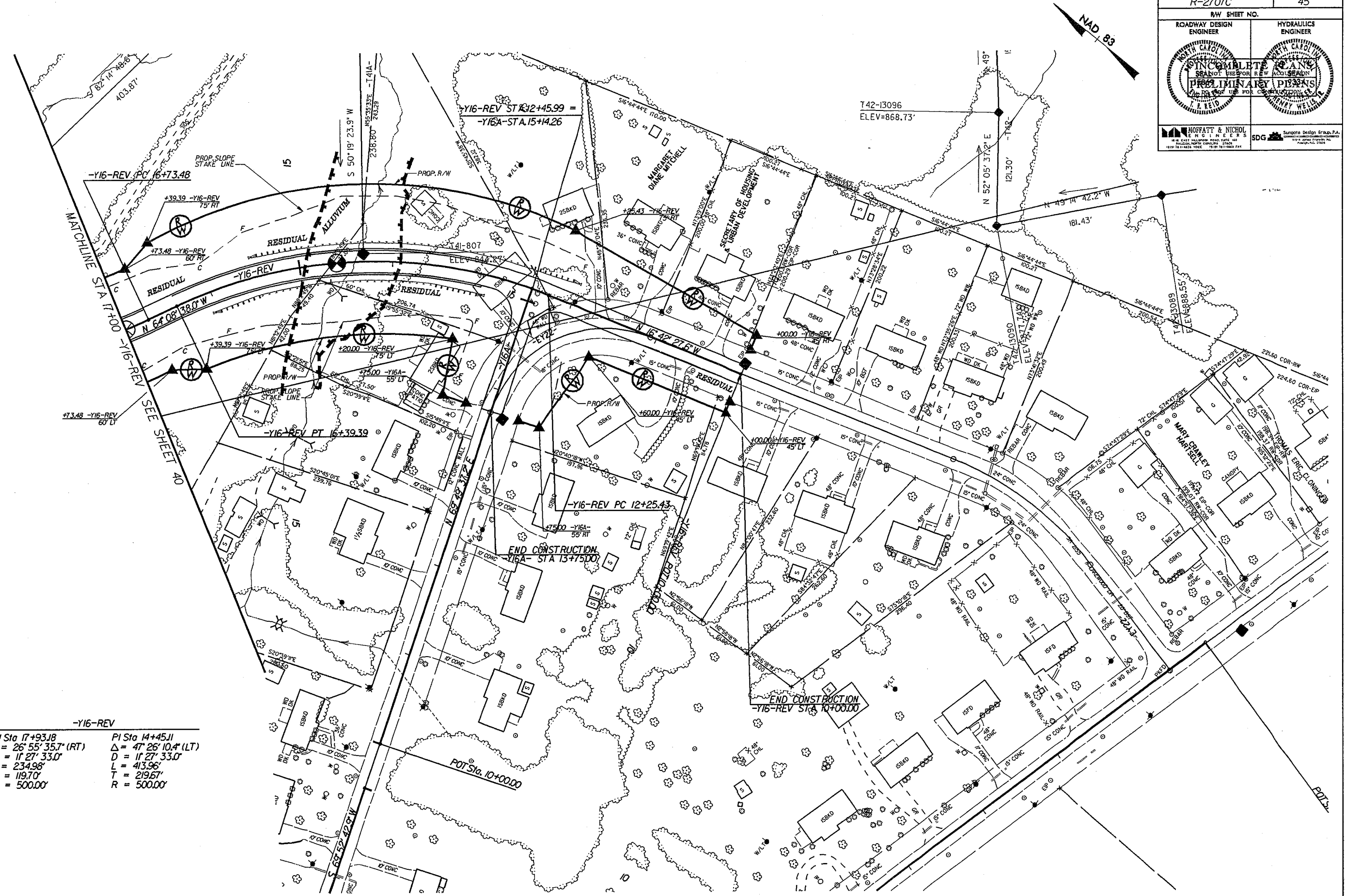
PROJECT REFERENCE NO. R-2707C		SHEET NO. 44	
RW SHEET NO.			
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
			
			



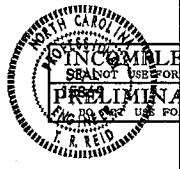
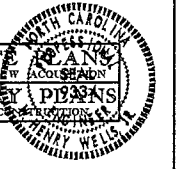


-Y11-REV

PI Sta 62+76.12	PIs Sta 66+79.45
$\Delta = 45^\circ 48' 01.2\" (RT)$	$\Theta s = 6' 25' 00.0\"$
$D = 6' 25' 00.0\"$	$Ls = 200.00'$
$L = 713.77'$	$LT = 133.42'$
$T = 377.19'$	$ST = 66.75'$
$R = 892.92'$	
$SE = .08$	

FOR -Y11-REV PROFILE SEE SHEET 89

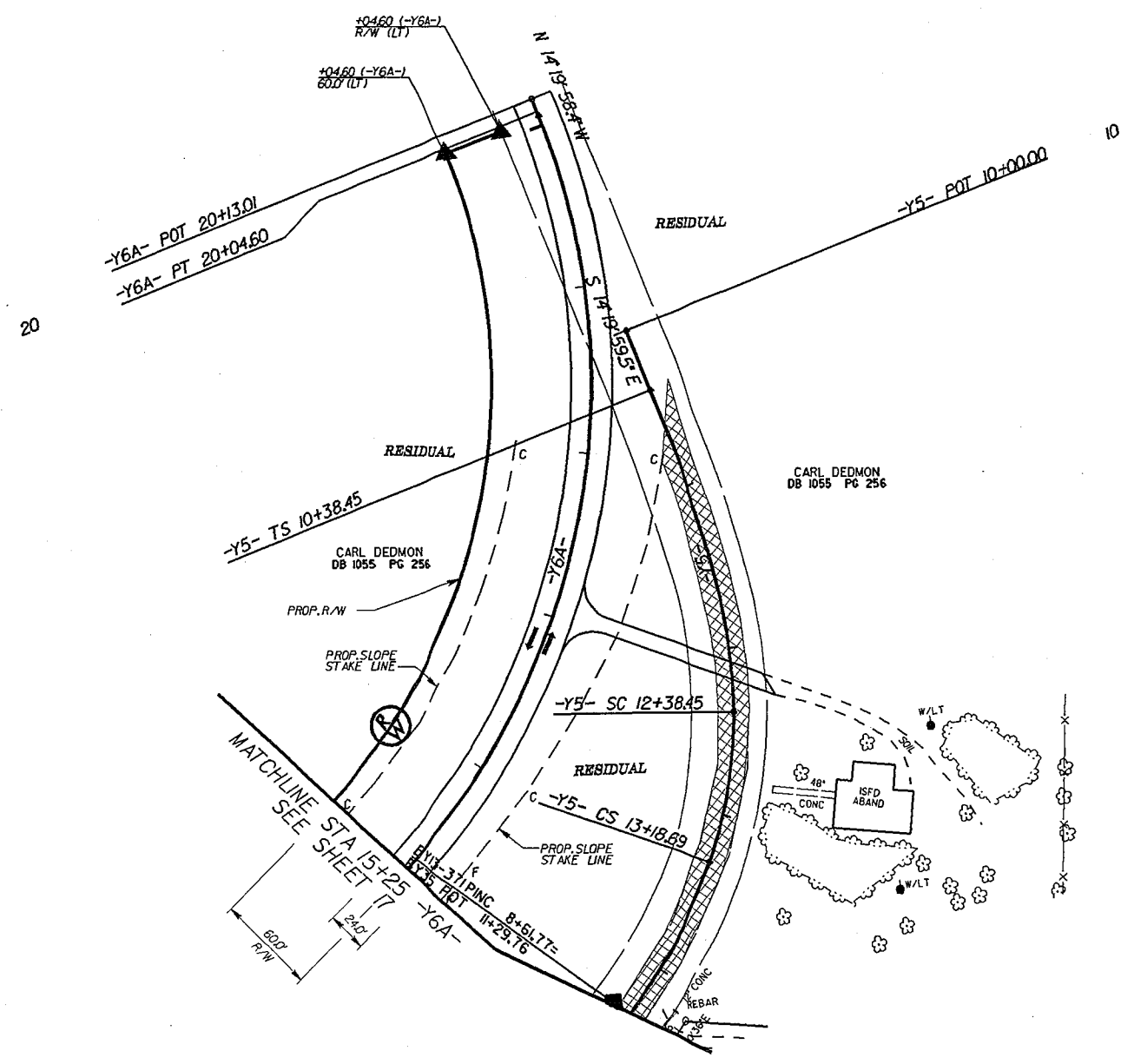


-Y16-REV	
PI Sta 17+93.18	PI Sta 14+45.11
$\Delta = 26^{\circ} 55' 35.7''$ (RT)	$\Delta = 47^{\circ} 26' 10.4''$ (LT)
D = 11' 27' 33.0"	D = 11' 27' 33.0"
L = 234.98'	L = 413.96'
T = 119.70'	T = 219.67'
R = 500.00'	R = 500.00'

PROJECT REFERENCE NO. R-2707C		SHEET NO. 46	
RW SHEET NO.			
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
			
			



# ADDITIONAL TOPO AND DTM COVERAGE REQUIRED

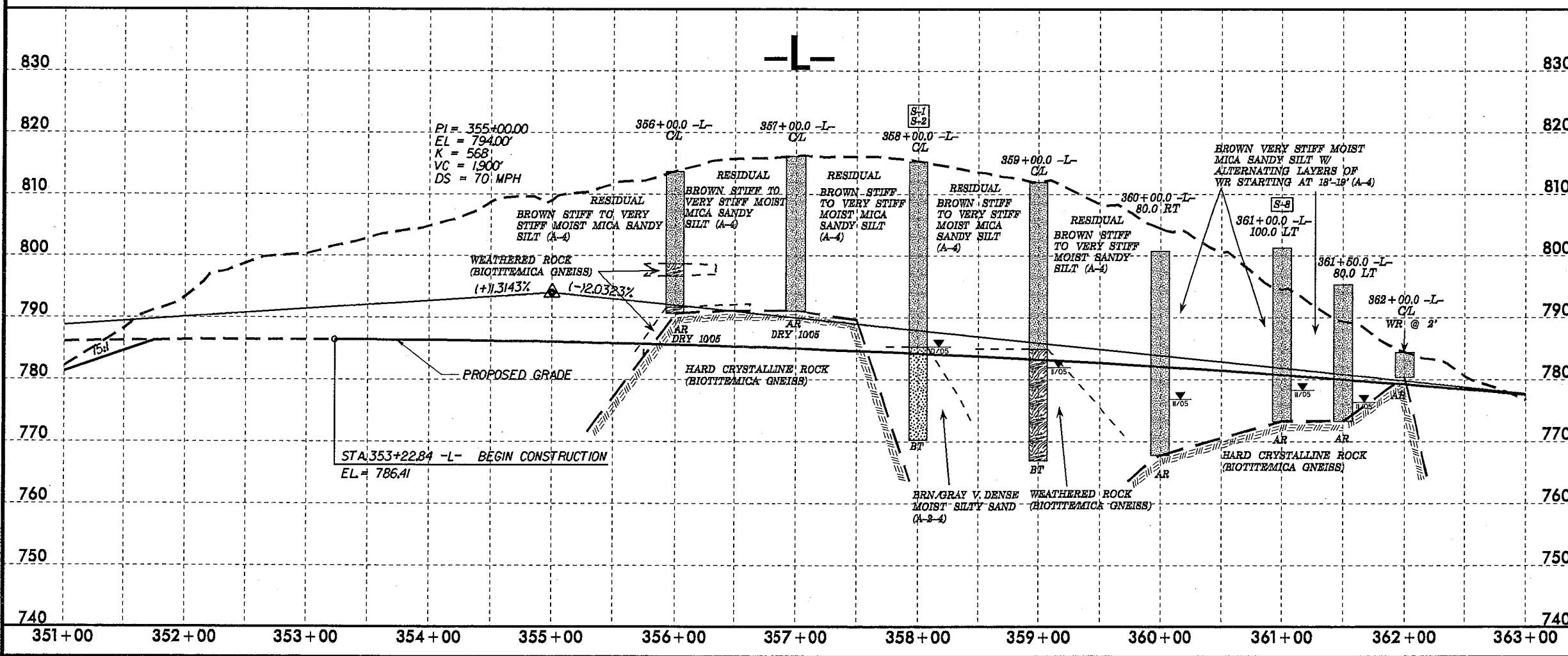
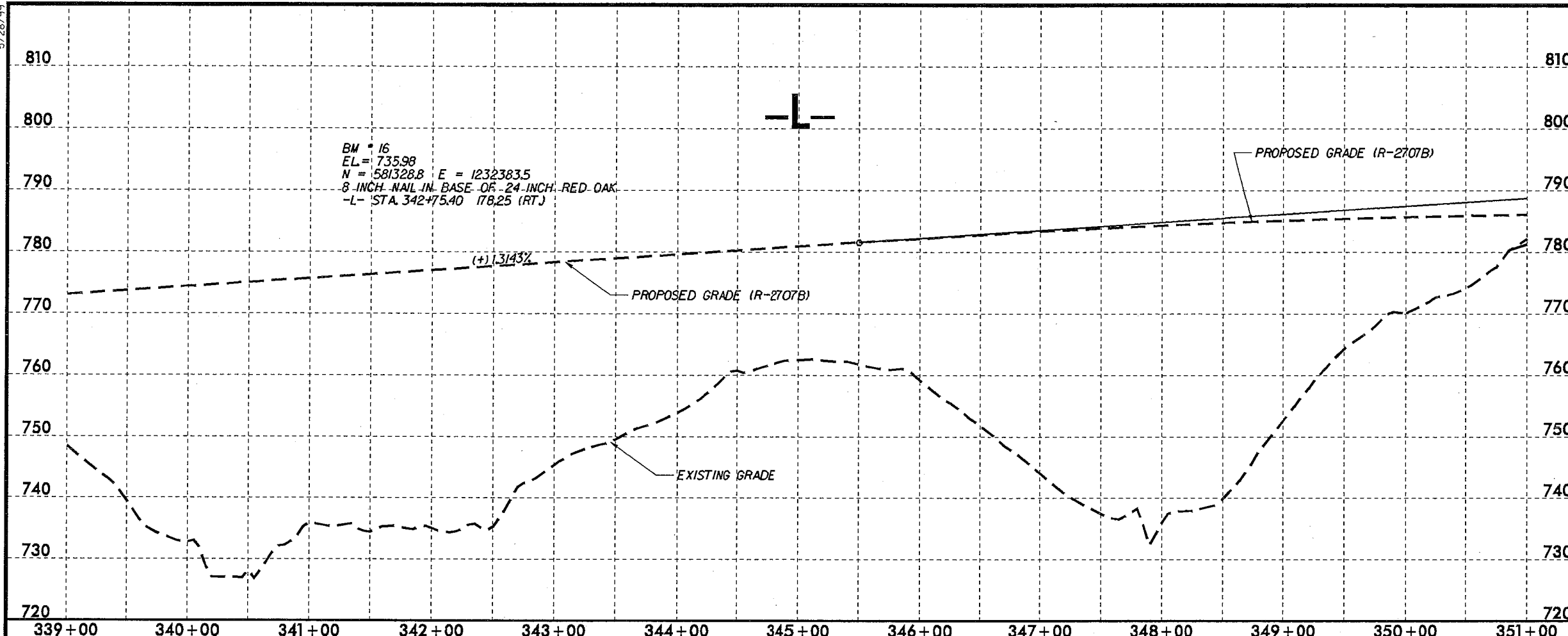


-Y6A-  
 PI Sta 18+74.21  
 $\Delta = 123^{\circ} 04' 59.2''$  (LT)  
 $D = 13^{\circ} 19' 28.6''$   
 $L = 923.73'$   
 $T = 793.33'$   
 $R = 430.00'$

-Y5-  
 Pls Sta 13+96.72      PI Sta 14+85.71  
 $E_s = 2^{\circ} 30' 00.0''$        $\Delta = 30^{\circ} 39' 00.8''$  (RT)  
 $L_s = 200.00'$        $D = 38^{\circ} 11' 49.9''$   
 $LT = 134.33'$        $L = 80.24'$   
 $ST = 67.57'$        $T = 41.11'$   
 $R = 150.00'$

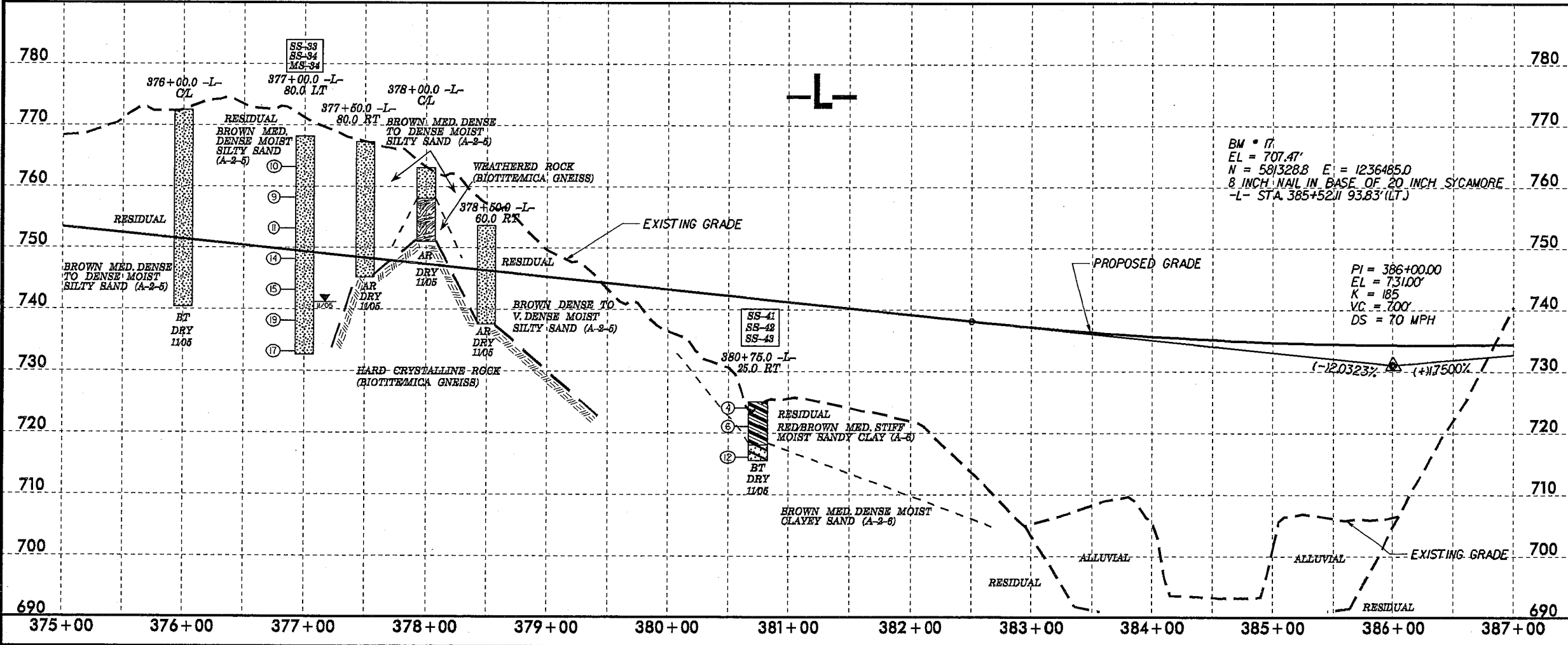
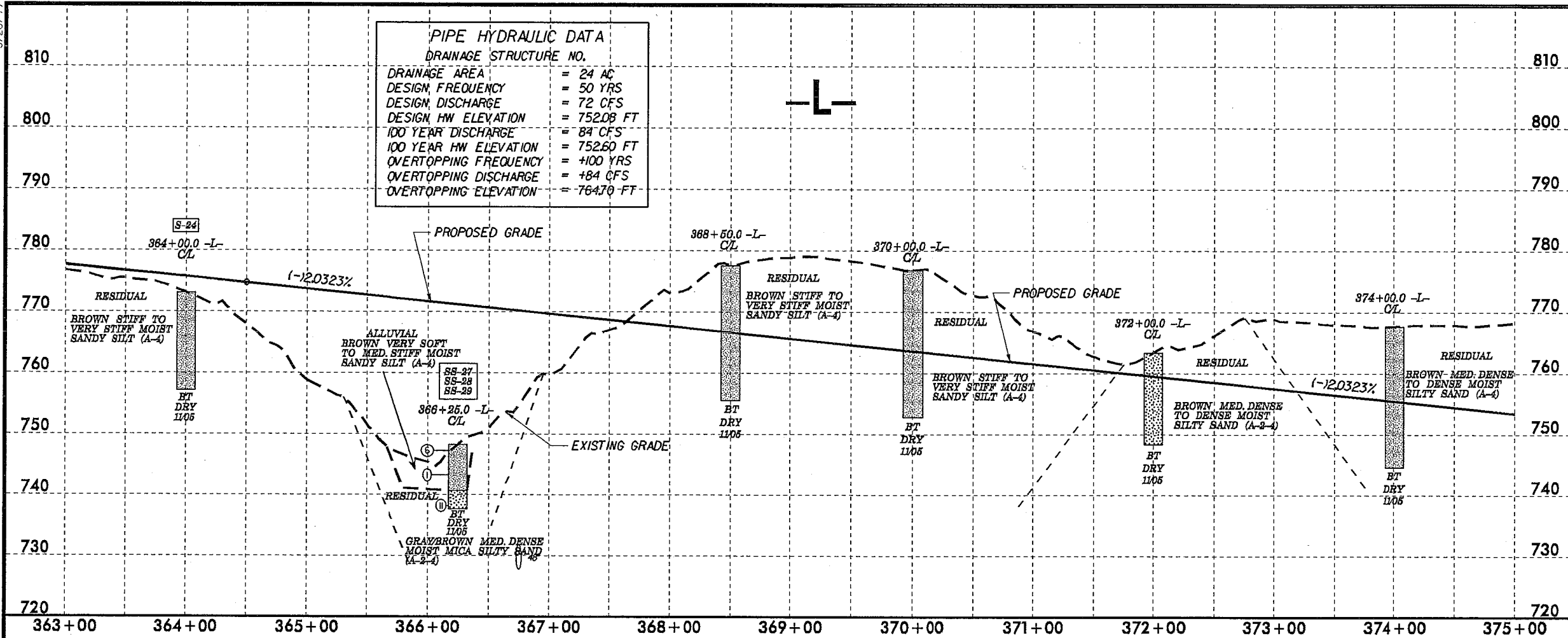


PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>47</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR A/W ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	



28-MAY-2008 15:19  
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PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 24 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 72 CFS
DESIGN HW ELEVATION	= 752.08 FT
100 YEAR DISCHARGE	= 84 CFS
100 YEAR HW ELEVATION	= 752.60 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +84 CFS
OVERTOPPING ELEVATION	= 764.70 FT

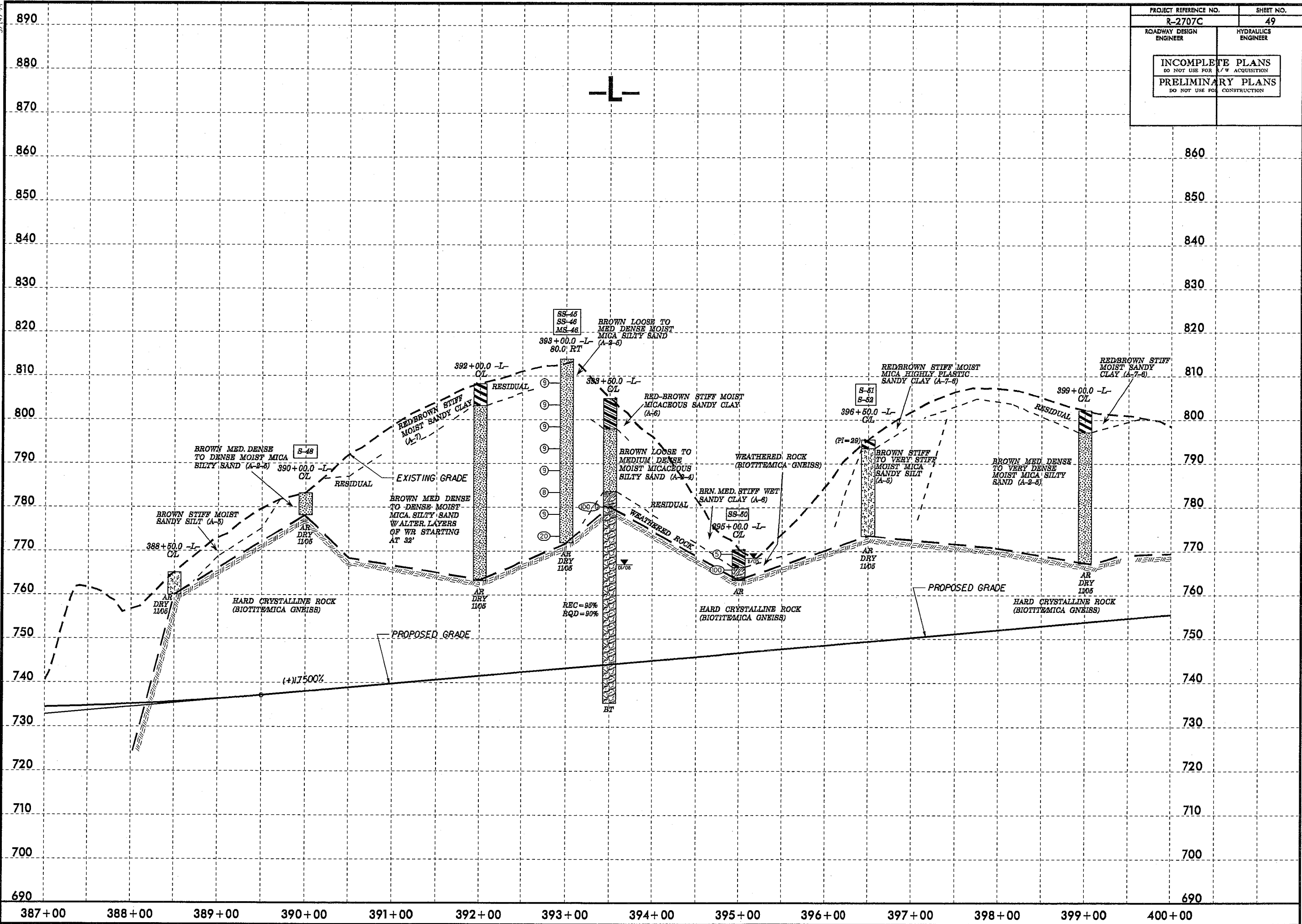


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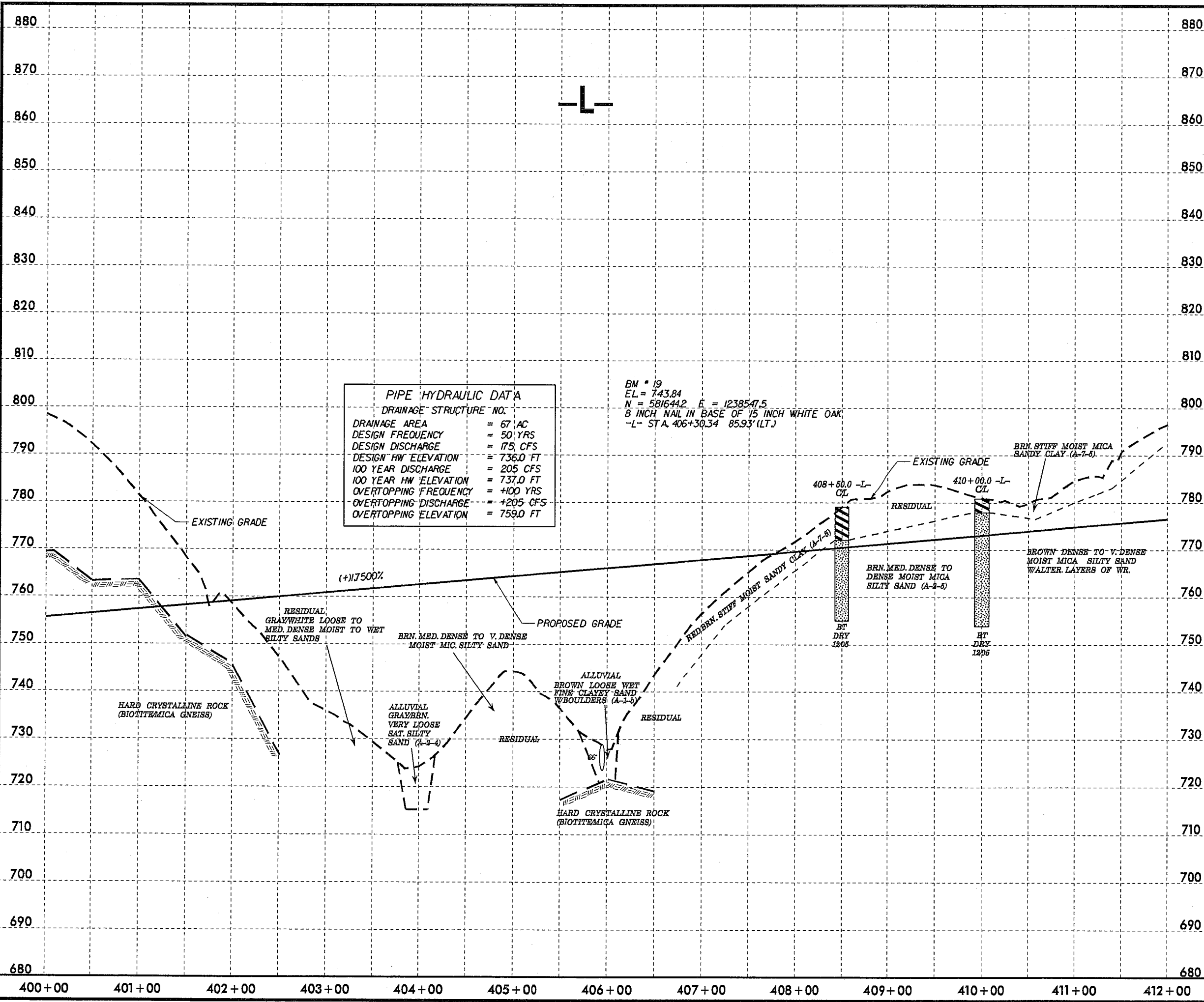
5/14/99

PROJECT REFERENCE NO.	SHEET NO.
R-2707C	49
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

29-MAY-2008 08:46  
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5/14/99  
 01MAY-2008 14:30  
 C:\Users\joseph\Documents\Projects\2707\2707.dwg



PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 67 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 179 CFS
DESIGN HW ELEVATION	= 736.0 FT
100 YEAR DISCHARGE	= 205 CFS
100 YEAR HW ELEVATION	= 737.0 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +205 CFS
OVERTOPPING ELEVATION	= 759.0 FT

BM # 19  
 EL = 743.84  
 N = 581644.2 E = 1238547.5  
 8 INCH NAIL IN BASE OF 15 INCH WHITE OAK  
 -L- STA. 406+30.34 85.93' (LTJ)

RESIDUAL GRAY/WHITE LOOSE TO MED. DENSE MOIST TO WET SILTY SANDS

BRN. MED. DENSE TO V. DENSE MOIST MIC. SILTY SAND

ALLUVIAL GRAY/BRN. VERY LOOSE SAT. SILTY SAND (A-2-4)

ALLUVIAL BROWN LOOSE WET FINE CLAYEY SAND W/BOULDERS (A-1-5)

BRN. MED. DENSE TO DENSE MOIST MICA SILTY SAND (A-2-5)

BRN. STIFF MOIST MICA SANDY CLAY (A-7-8)

BROWN DENSE TO V. DENSE MOIST MICA SILTY SAND W/ALTER. LAYERS OF WR.

BT DRY 1206

BT DRY 1206

HARD CRYSTALLINE ROCK (BIOTITE/MICA GNEISS)

HARD CRYSTALLINE ROCK (BIOTITE/MICA GNEISS)

(+)17500%

PROPOSED GRADE

EXISTING GRADE

EXISTING GRADE

RESIDUAL

RESIDUAL

RESIDUAL

408+50.0 -L- CL

410+00.0 -L- CL

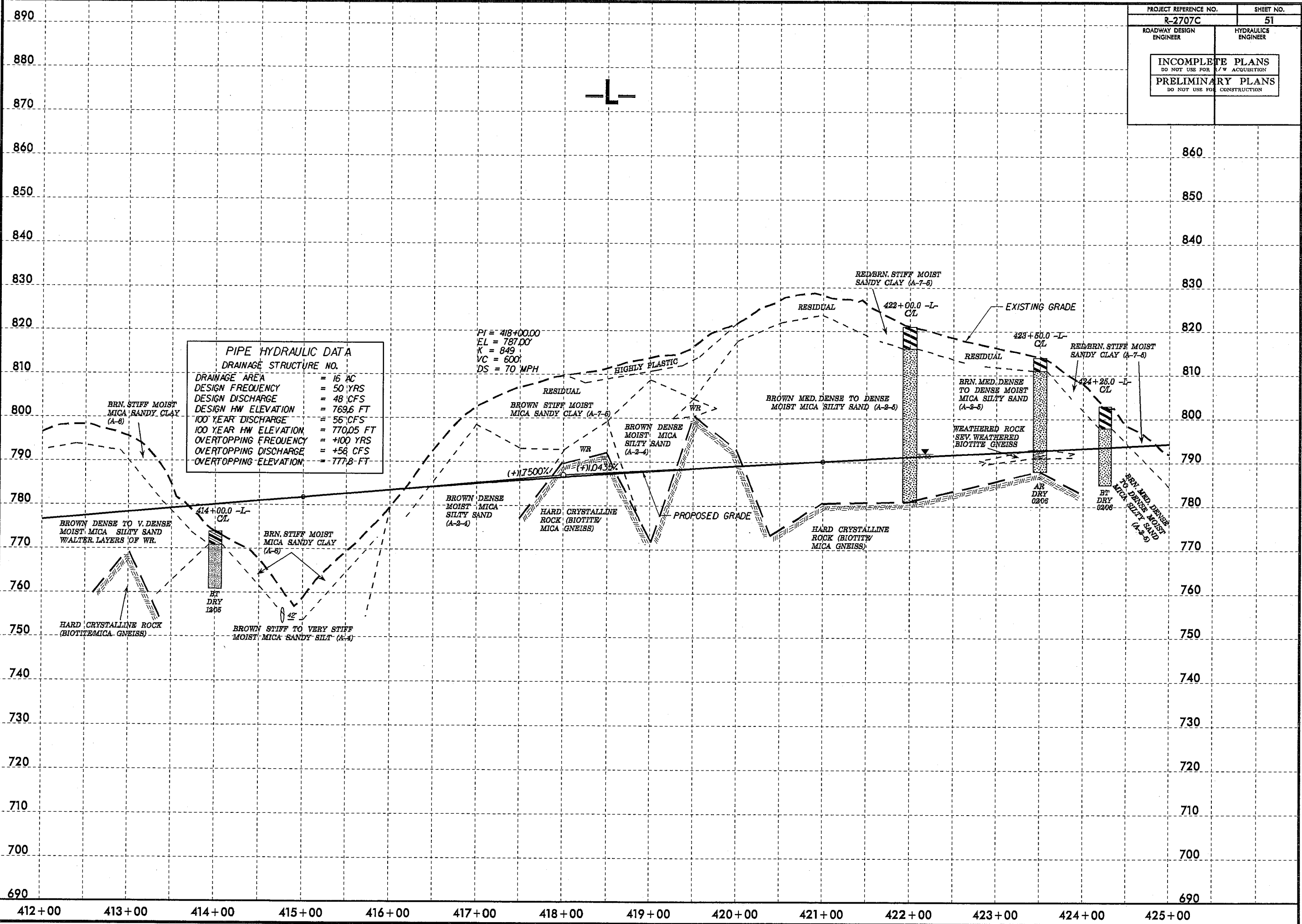
880  
870  
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730  
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710  
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680

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710  
700  
690  
680

400+00 401+00 402+00 403+00 404+00 405+00 406+00 407+00 408+00 409+00 410+00 411+00 412+00

5/14/99  
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PROJECT REFERENCE NO.		SHEET NO.	
R-2707C		51	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER		
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION <b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION			

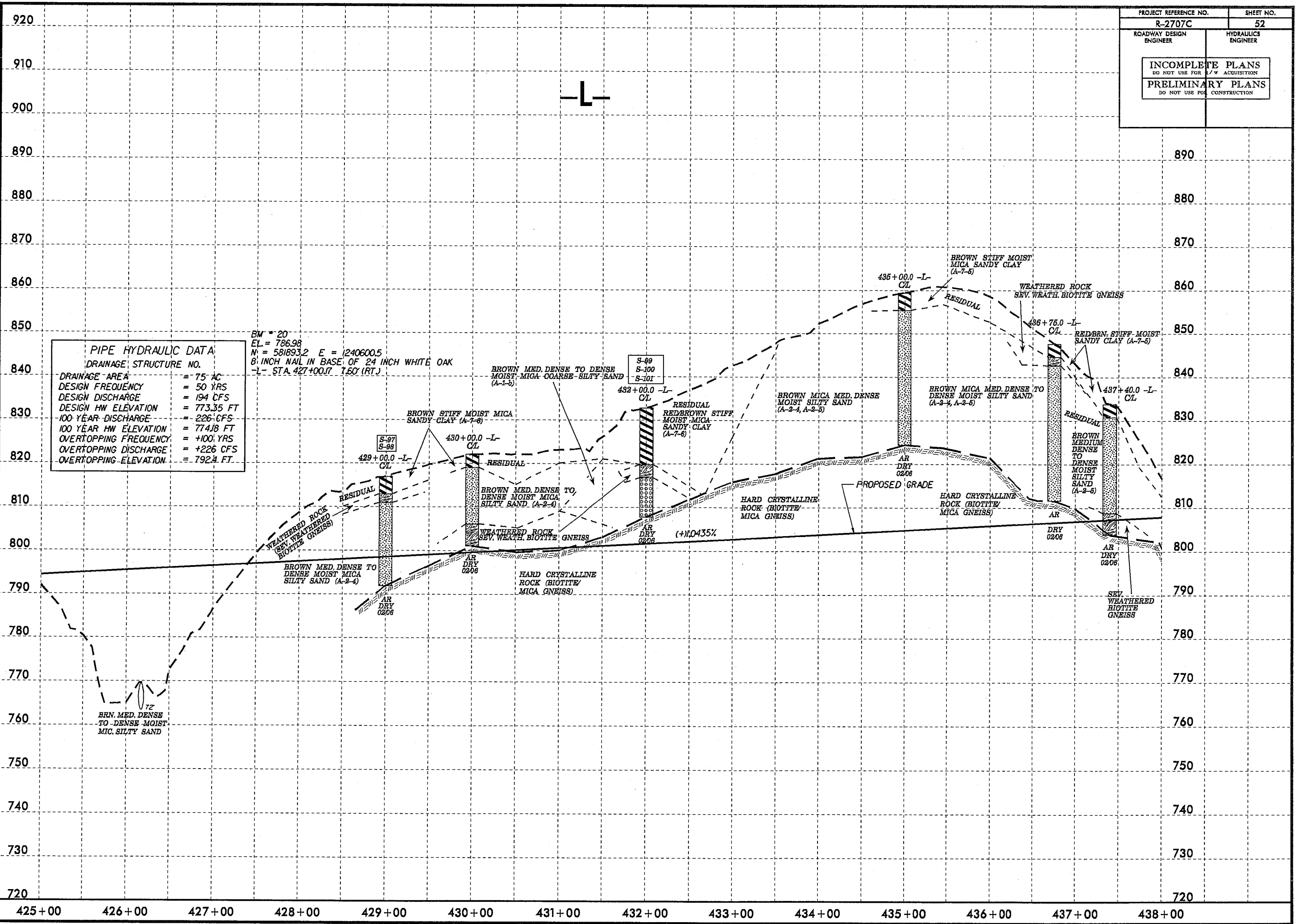


PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 16 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 48 CFS
DESIGN HW ELEVATION	= 769.6 FT
100 YEAR DISCHARGE	= 56 CFS
100 YEAR HW ELEVATION	= 770.05 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +58 CFS
OVERTOPPING ELEVATION	= 777.8 FT

PI = 418+00.00  
 EL = 787.00'  
 K = 849  
 VC = 600'  
 DS = 70 MPH

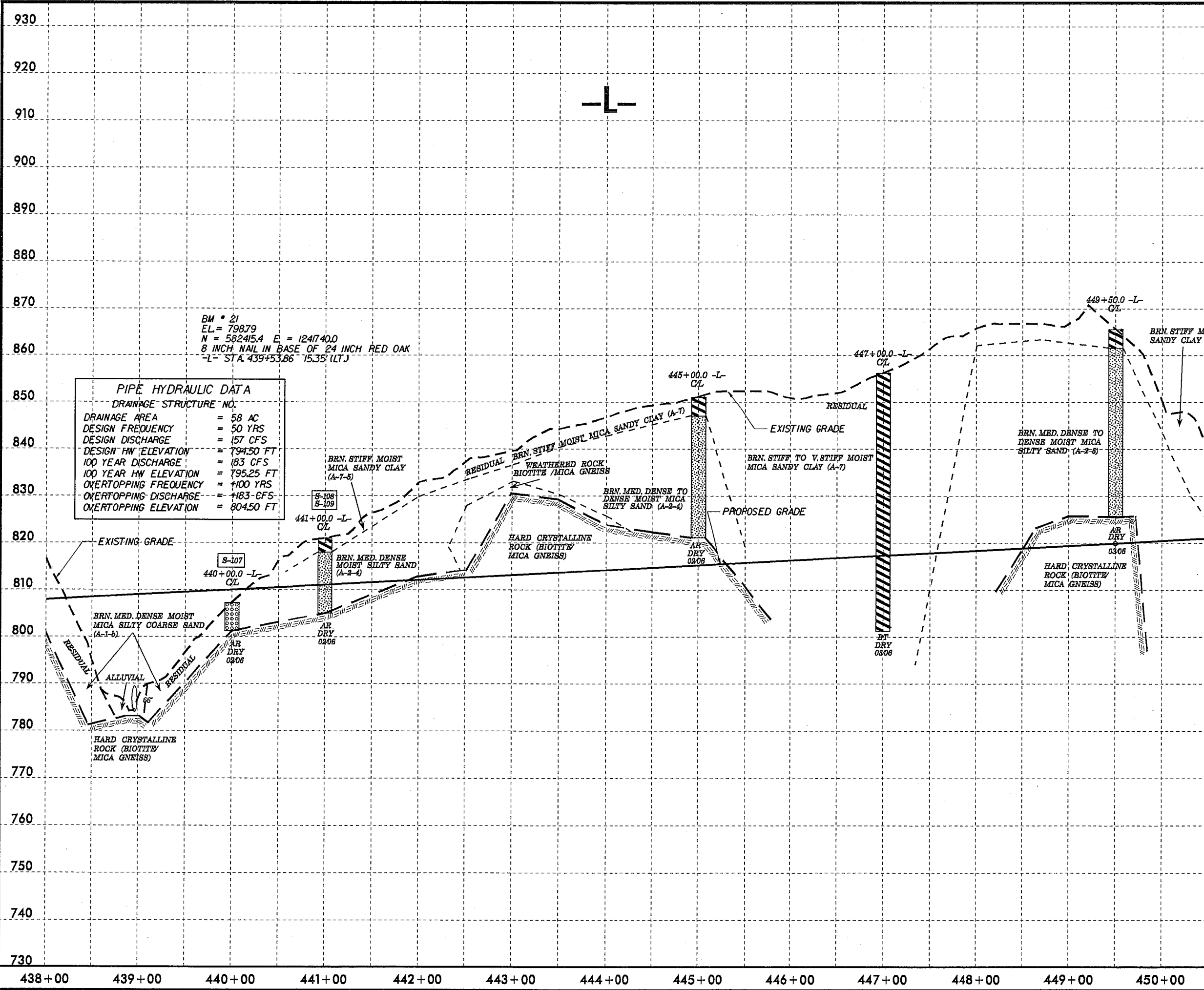
5/14/99  
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PROJECT REFERENCE NO. R-2707C	SHEET NO. 52
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION <b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	



5/14/99  
27-MAY-2008 09:53:23  
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PROJECT REFERENCE NO.	SHEET NO.
R-2707C	53
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	



**PIPE HYDRAULIC DATA**

DRAINAGE STRUCTURE NO. _____	
DRAINAGE AREA	= 58 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 157 CFS
DESIGN HW ELEVATION	= 794.50 FT
100 YEAR DISCHARGE	= 183 CFS
100 YEAR HW ELEVATION	= 795.25 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +183 CFS
OVERTOPPING ELEVATION	= 804.50 FT

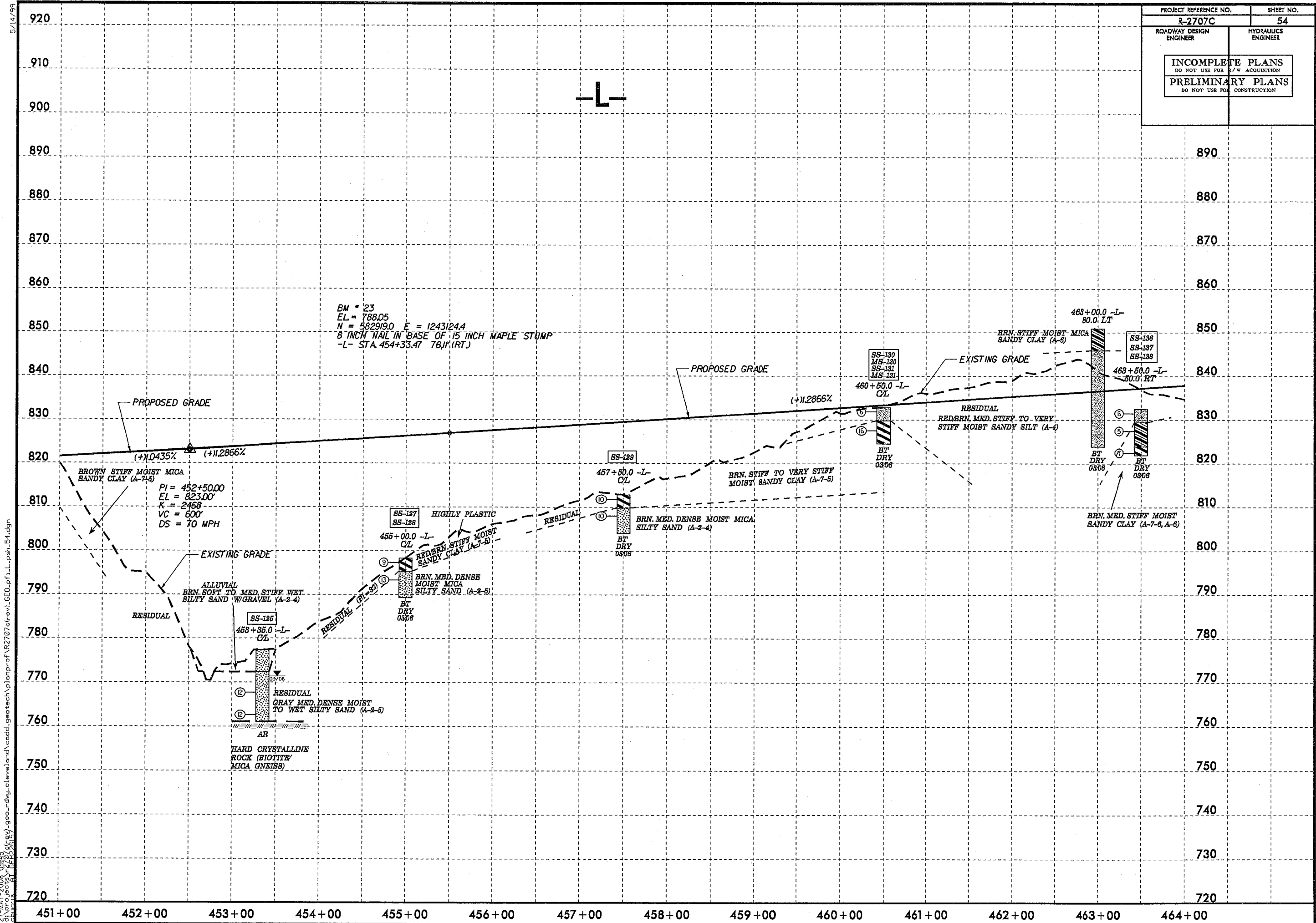
BM \* 21  
EL = 798.79  
N = 582415.4 E = 1241740.0  
8 INCH NAIL IN BASE OF 24 INCH RED OAK  
-L- STA. 439+53.86 15.35 (LT.)

-L-

438+00 439+00 440+00 441+00 442+00 443+00 444+00 445+00 446+00 447+00 448+00 449+00 450+00 451+00

930  
920  
910  
900  
890  
880  
870  
860  
850  
840  
830  
820  
810  
800  
790  
780  
770  
760  
750  
740  
730

PROJECT REFERENCE NO. R-2707C		SHEET NO. 54	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION <b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION			



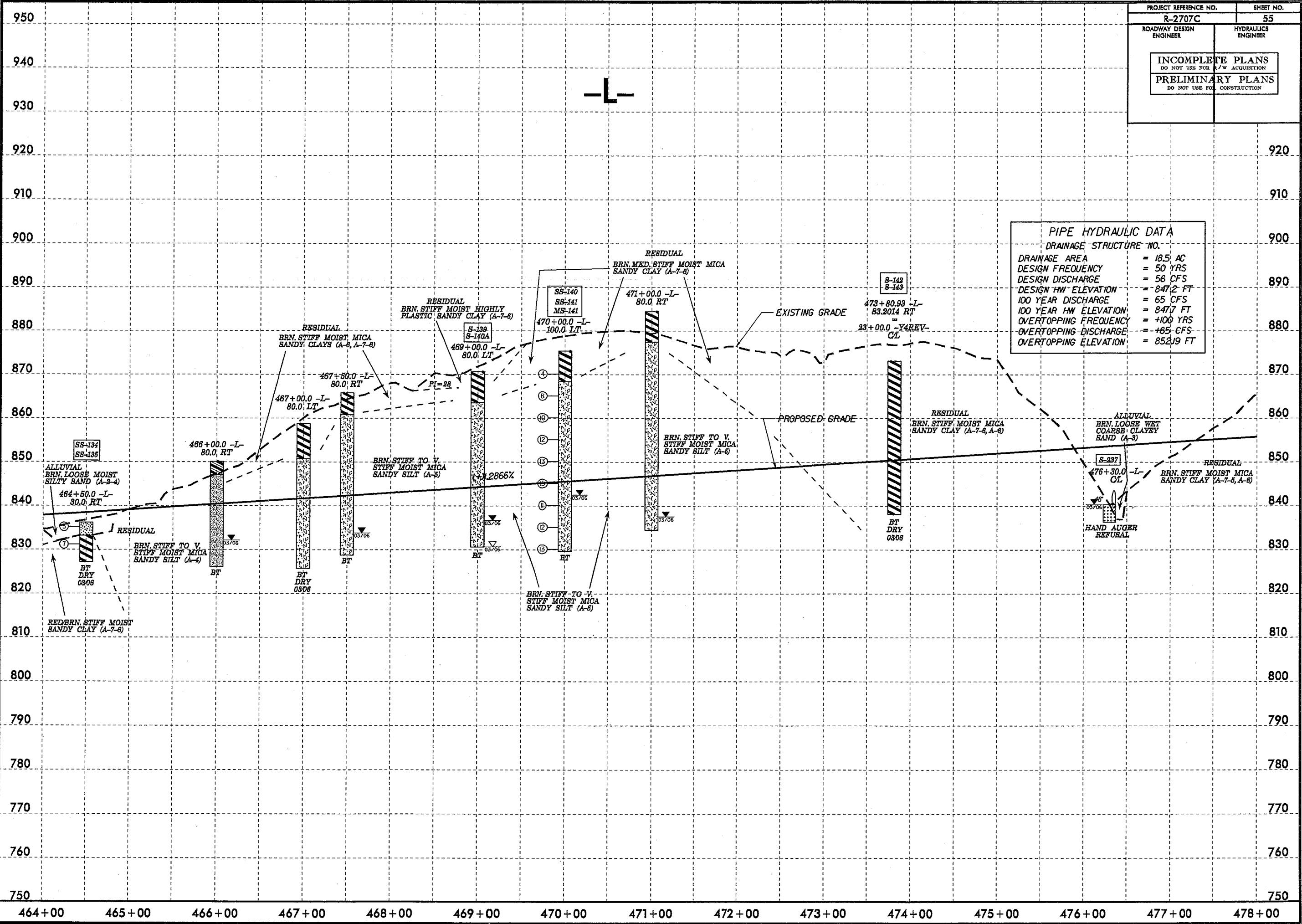
5/14/99  
 27-MAY-2008 09:45  
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27 MAY 2008 11:56 AM  
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PROJECT REFERENCE NO. R-2707C	SHEET NO. 55
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR A/W ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

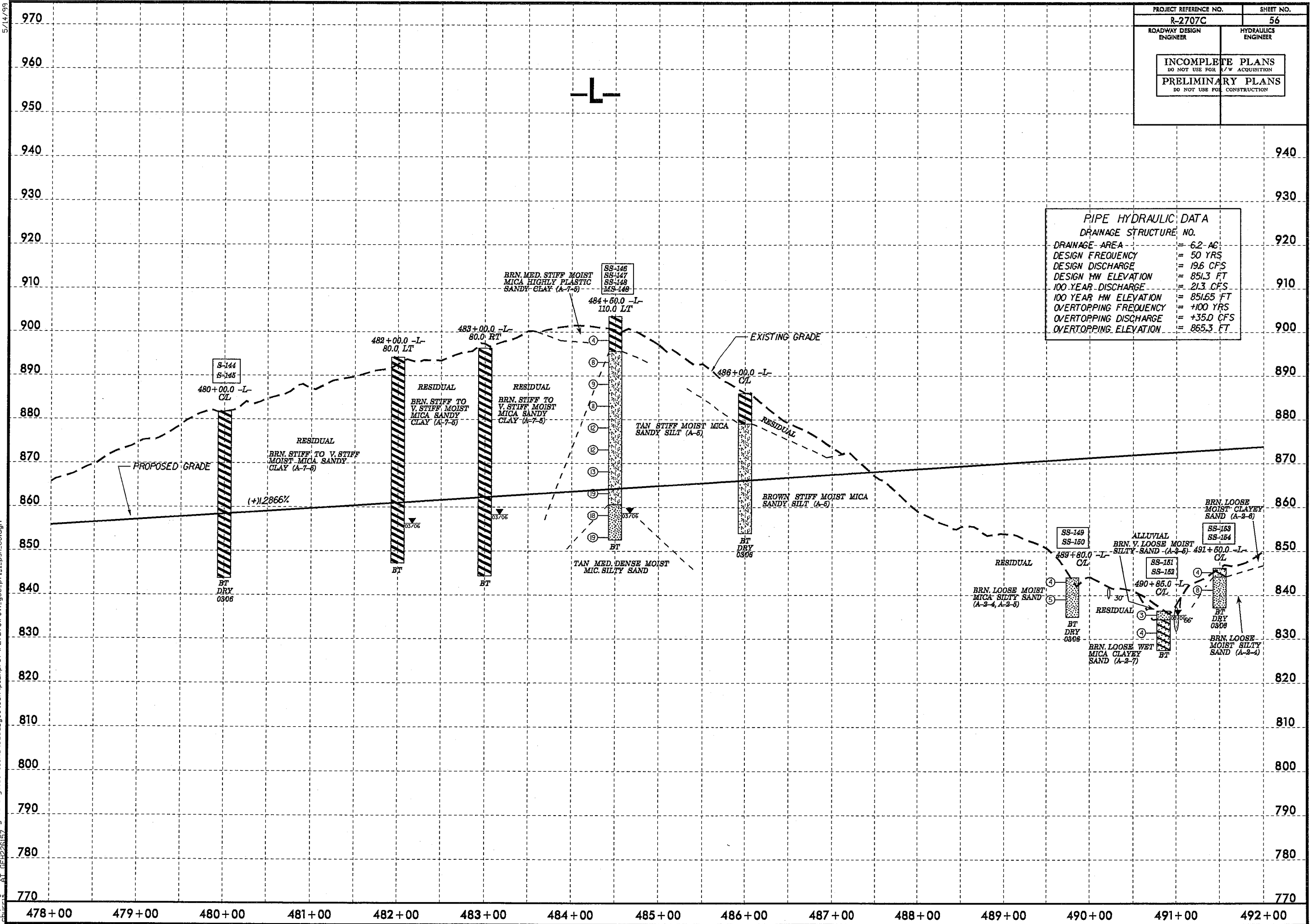


PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 18.5 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 58 CFS
DESIGN HW ELEVATION	= 847.2 FT
100 YEAR DISCHARGE	= 65 CFS
100 YEAR HW ELEVATION	= 847.7 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +65 CFS
OVERTOPPING ELEVATION	= 852.19 FT

464+00    465+00    466+00    467+00    468+00    469+00    470+00    471+00    472+00    473+00    474+00    475+00    476+00    477+00    478+00

PROJECT REFERENCE NO. R-2707C	SHEET NO. 56
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR P/W ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 6.2 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 19.6 CFS
DESIGN HW ELEVATION	= 851.3 FT
100 YEAR DISCHARGE	= 21.3 CFS
100 YEAR HW ELEVATION	= 851.65 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +35.0 CFS
OVERTOPPING ELEVATION	= 865.3 FT



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PROJECT REFERENCE NO. R-2707C	SHEET NO. 57
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

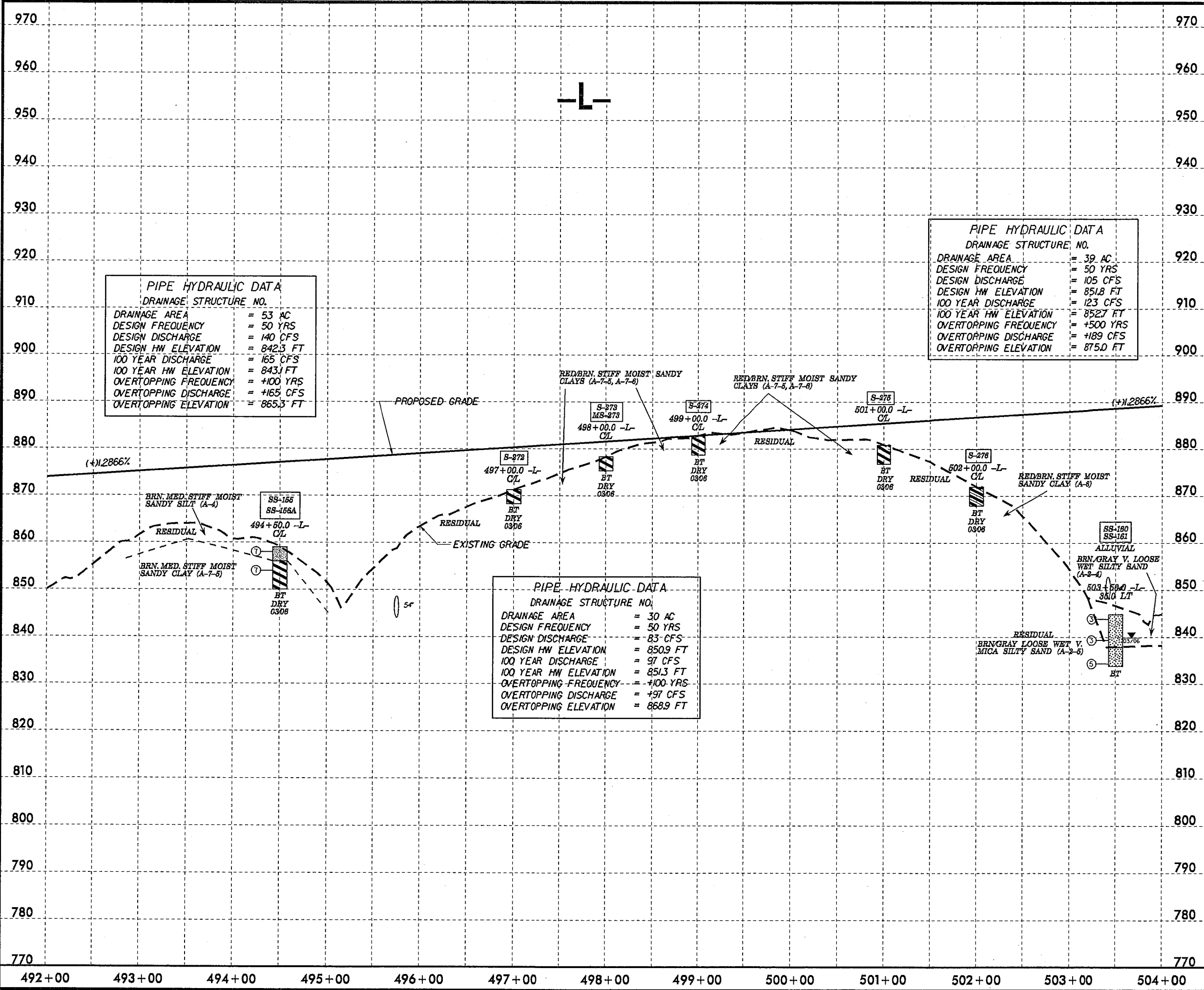
PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 53 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 140 CFS
DESIGN HW ELEVATION	= 842.3 FT
100 YEAR DISCHARGE	= 165 CFS
100 YEAR HW ELEVATION	= 843.1 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +165 CFS
OVERTOPPING ELEVATION	= 865.3 FT

PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 39 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 105 CFS
DESIGN HW ELEVATION	= 851.8 FT
100 YEAR DISCHARGE	= 123 CFS
100 YEAR HW ELEVATION	= 852.7 FT
OVERTOPPING FREQUENCY	= +500 YRS
OVERTOPPING DISCHARGE	= +189 CFS
OVERTOPPING ELEVATION	= 875.0 FT

PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 30 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 83 CFS
DESIGN HW ELEVATION	= 850.9 FT
100 YEAR DISCHARGE	= 97 CFS
100 YEAR HW ELEVATION	= 851.3 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +97 CFS
OVERTOPPING ELEVATION	= 868.9 FT

5/14/99

28-MAY-2008 09:20  
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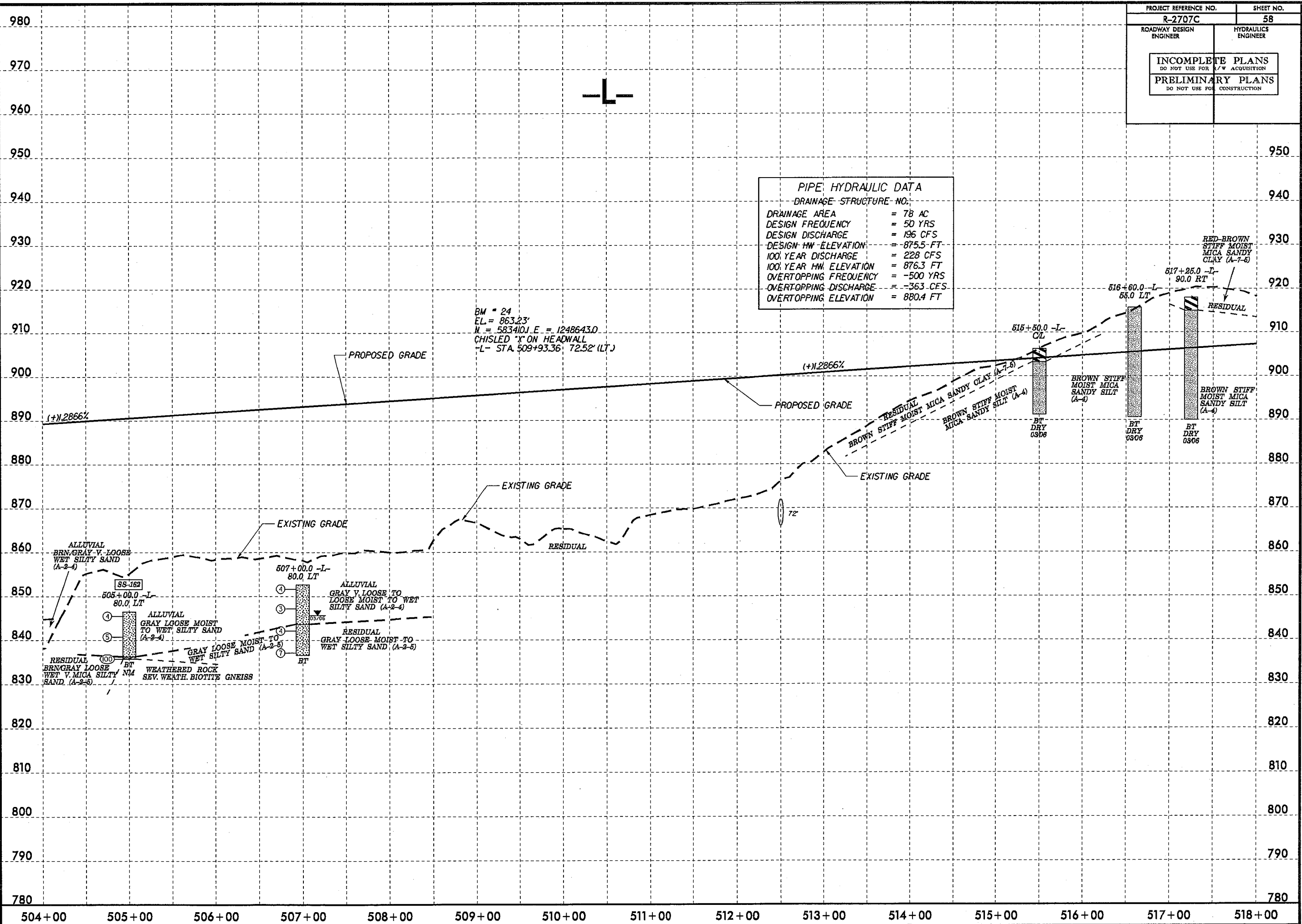


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PROJECT REFERENCE NO. R-2707C	SHEET NO. 58
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

DRAINAGE STRUCTURE NO:	
DRAINAGE AREA	= 78 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 196 CFS
DESIGN HW ELEVATION	= 875.5 FT
100 YEAR DISCHARGE	= 228 CFS
100 YEAR HW ELEVATION	= 876.3 FT
OVERTOPPING FREQUENCY	= 500 YRS
OVERTOPPING DISCHARGE	= 363 CFS
OVERTOPPING ELEVATION	= 880.4 FT

BM = 24  
EL = 863.23'  
N = 583410.1 E = 1248643.0  
CHISLED 'X' ON HEADWALL  
-L- STA. 509+93.36 72.52' (LT.)



(+1.2866%)

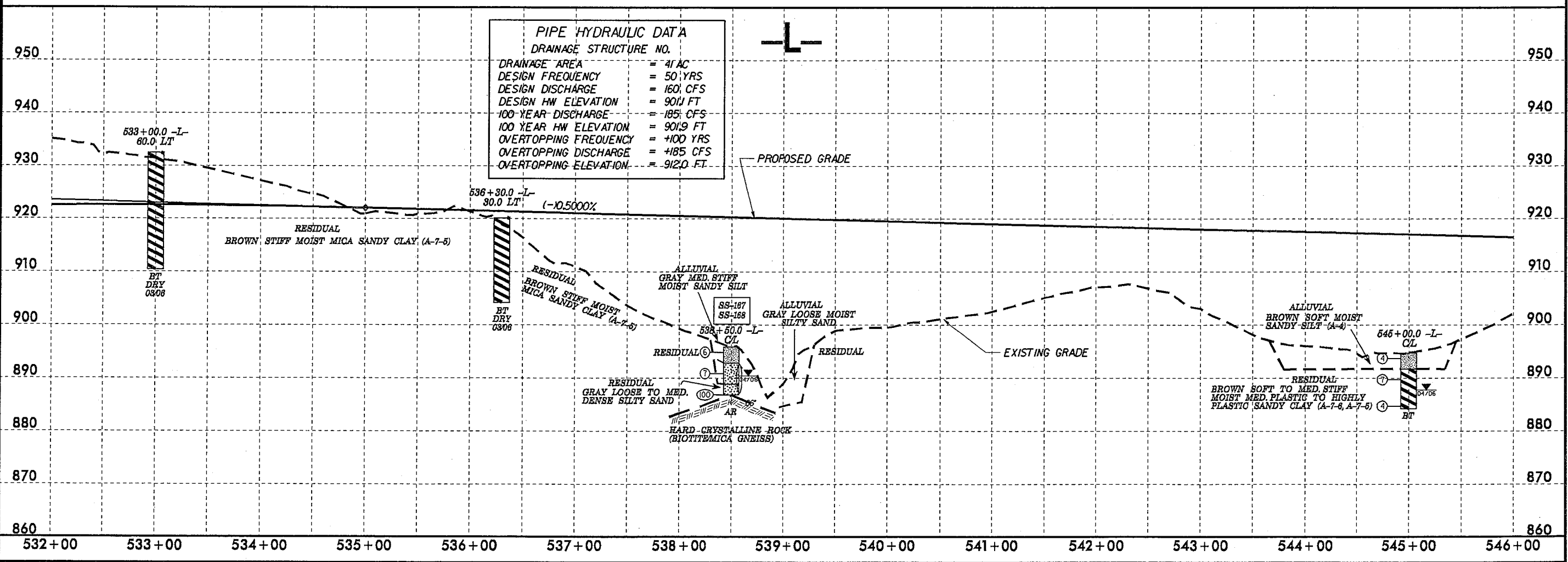
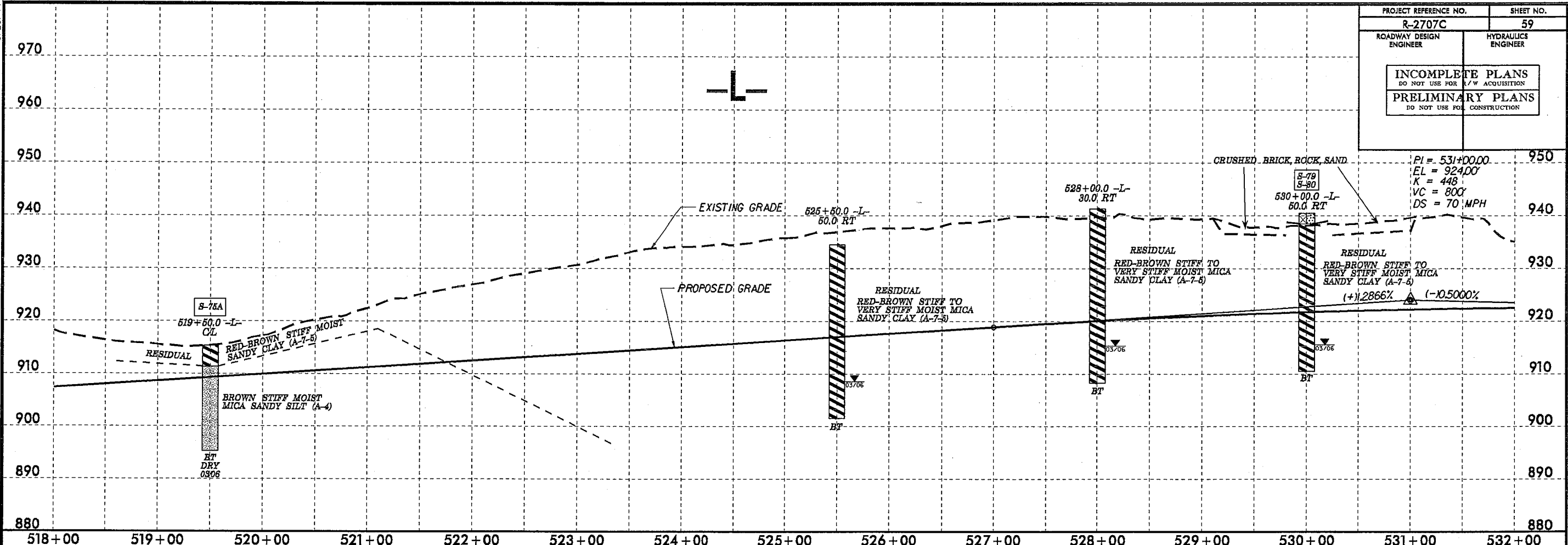
(+1.2866%)

72'

504+00 505+00 506+00 507+00 508+00 509+00 510+00 511+00 512+00 513+00 514+00 515+00 516+00 517+00 518+00

5/28/99

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>59</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR A/C ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	



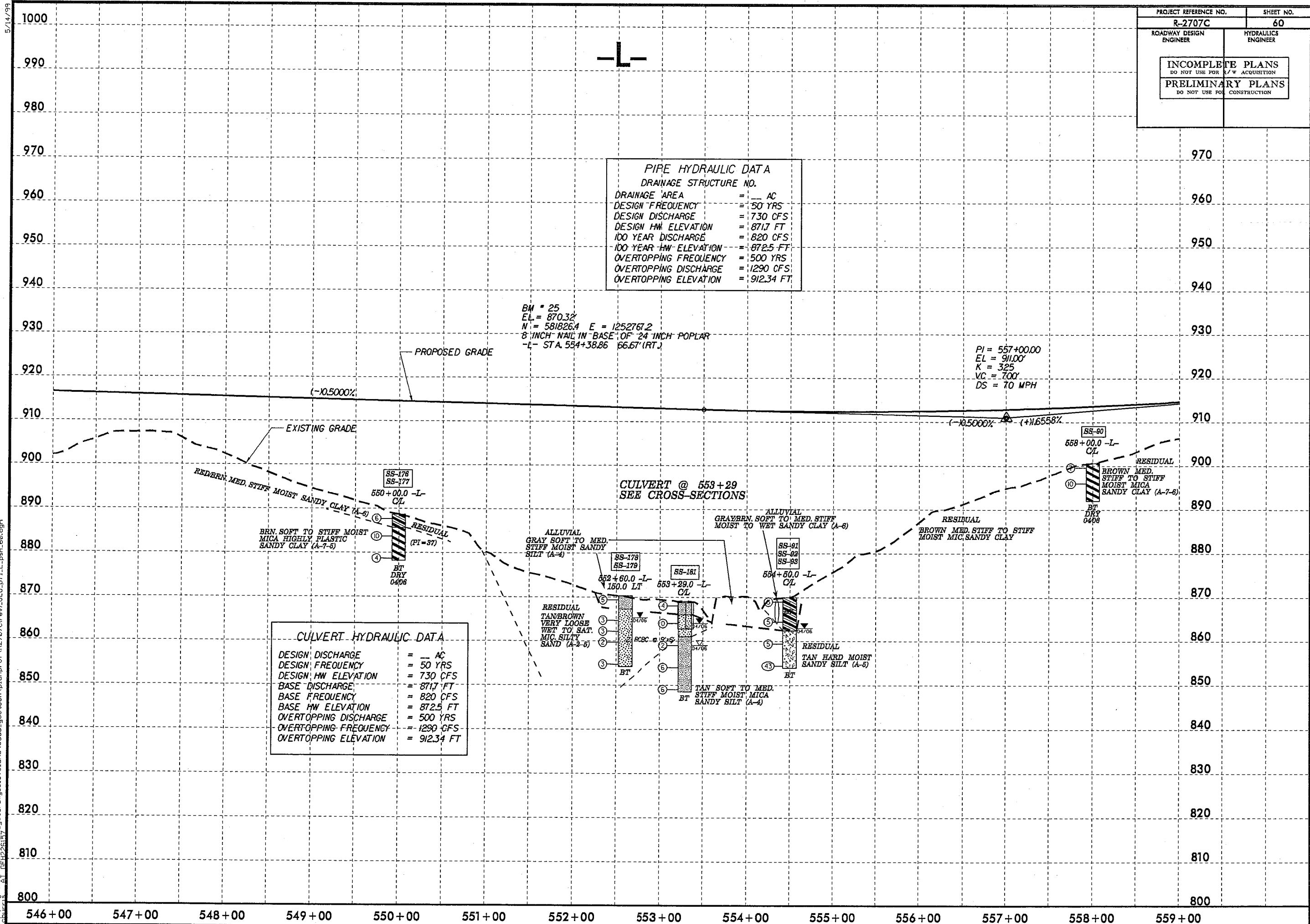
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PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 1 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 730 CFS
DESIGN HW ELEVATION	= 871.7 FT
100 YEAR DISCHARGE	= 820 CFS
100 YEAR HW ELEVATION	= 872.5 FT
OVERTOPPING FREQUENCY	= 500 YRS
OVERTOPPING DISCHARGE	= 1290 CFS
OVERTOPPING ELEVATION	= 912.34 FT

BM \* 25  
 EL = 870.32  
 N = 581826.4 E = 1252767.2  
 8" INCH NAIL IN BASE OF 24" INCH POPLAR  
 -L- STA. 554+38.86 66.67' (RT)

PI = 557+00.00  
 EL = 911.00'  
 K = 325  
 VC = 700'  
 DS = 70 MPH

CULVERT HYDRAULIC DATA	
DESIGN DISCHARGE	= 1 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN HW ELEVATION	= 730 CFS
BASE DISCHARGE	= 871.7 FT
BASE FREQUENCY	= 820 CFS
BASE HW ELEVATION	= 872.5 FT
OVERTOPPING DISCHARGE	= 500 YRS
OVERTOPPING FREQUENCY	= 1290 CFS
OVERTOPPING ELEVATION	= 912.34 FT

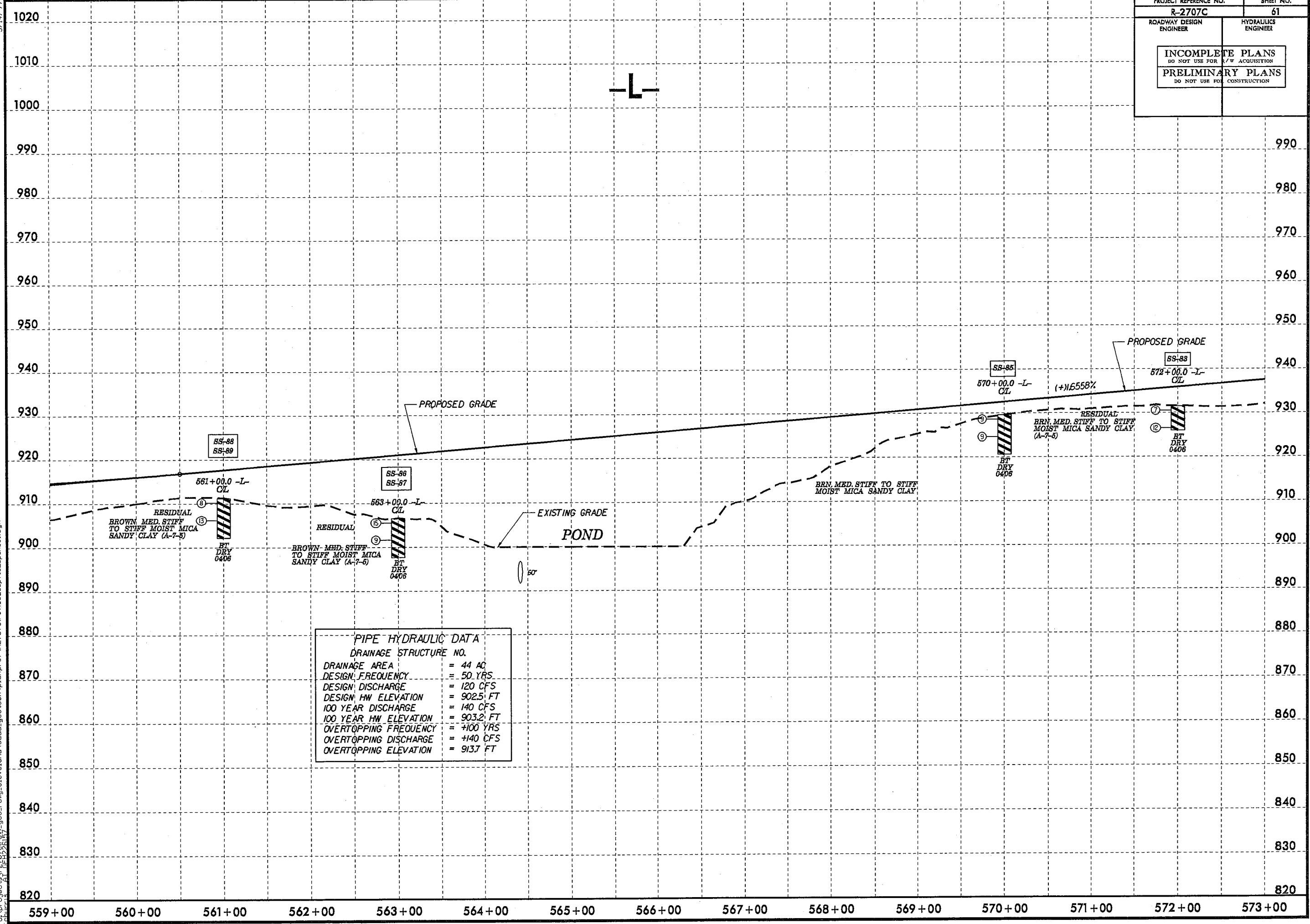


13-MAY-2008 09:28  
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5/14/99

03-APR-2008 10:46  
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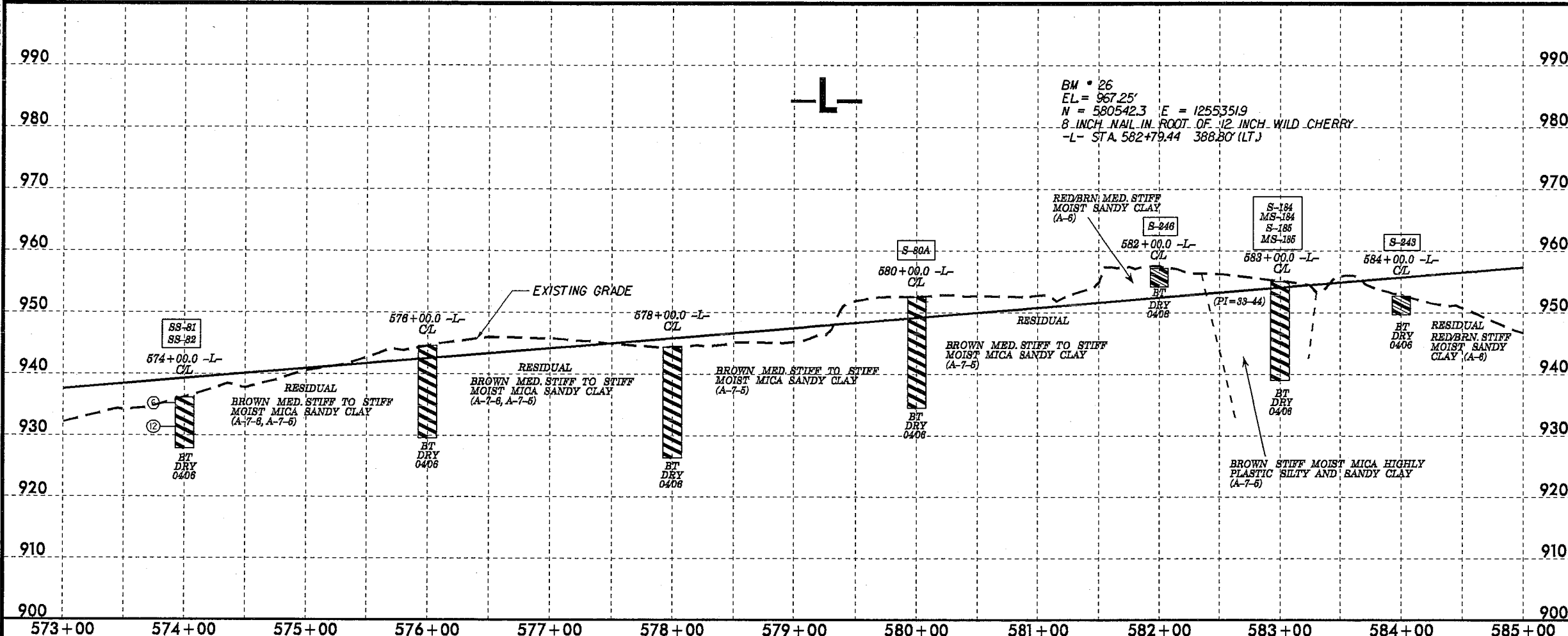
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ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR A/W ACQUISITION <b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	



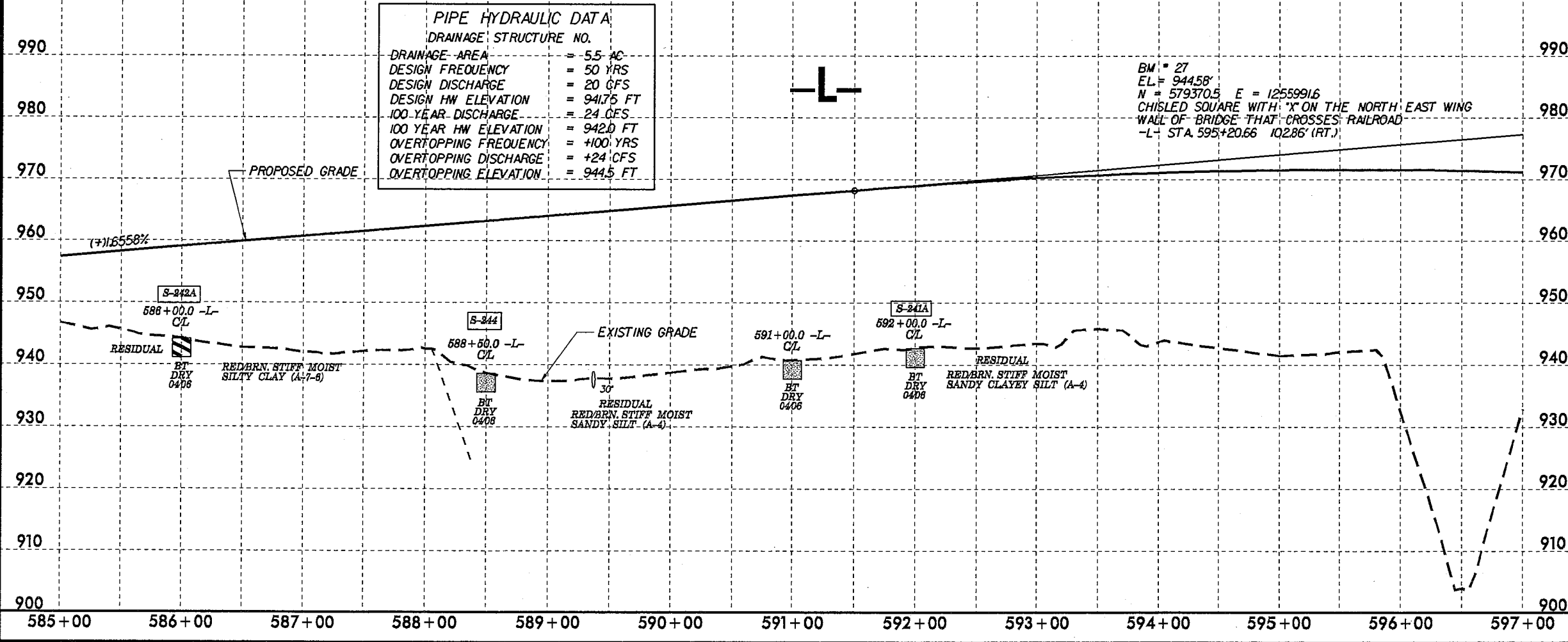
PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 44 AC
DESIGN FREQUENCY	= 50 YRS.
DESIGN DISCHARGE	= 120 CFS
DESIGN HW ELEVATION	= 902.5 FT
100 YEAR DISCHARGE	= 140 CFS
100 YEAR HW ELEVATION	= 903.2 FT
OVERTOPPING FREQUENCY	= 100 YRS
OVERTOPPING DISCHARGE	= 110 CFS
OVERTOPPING ELEVATION	= 913.7 FT

5/28/99

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>62</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR $E/W$ ACQUISITION <b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	



DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 5.5 AC
DESIGN FREQUENCY	= 50 YRS
DESIGN DISCHARGE	= 20 CFS
DESIGN HW ELEVATION	= 941.75 FT
100-YEAR DISCHARGE	= 24 CFS
100 YEAR HW ELEVATION	= 942.0 FT
OVERTOPPING FREQUENCY	= 100 YRS
OVERTOPPING DISCHARGE	= 24 CFS
OVERTOPPING ELEVATION	= 944.5 FT

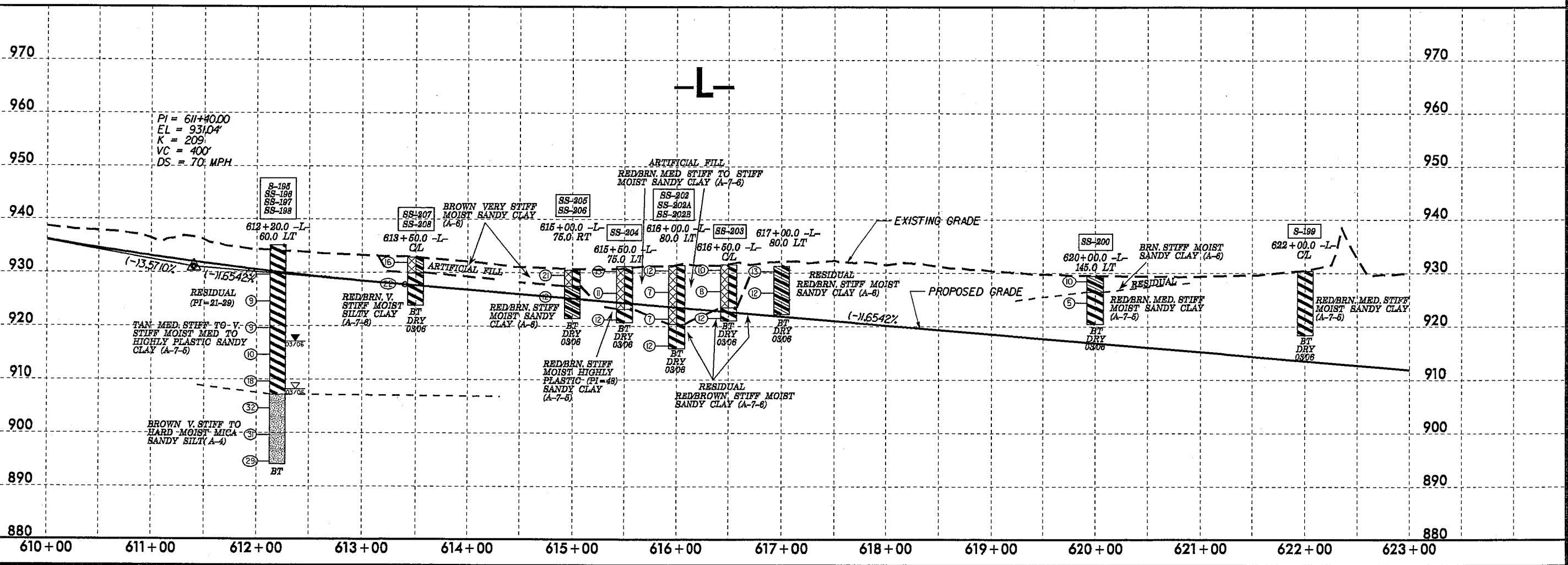
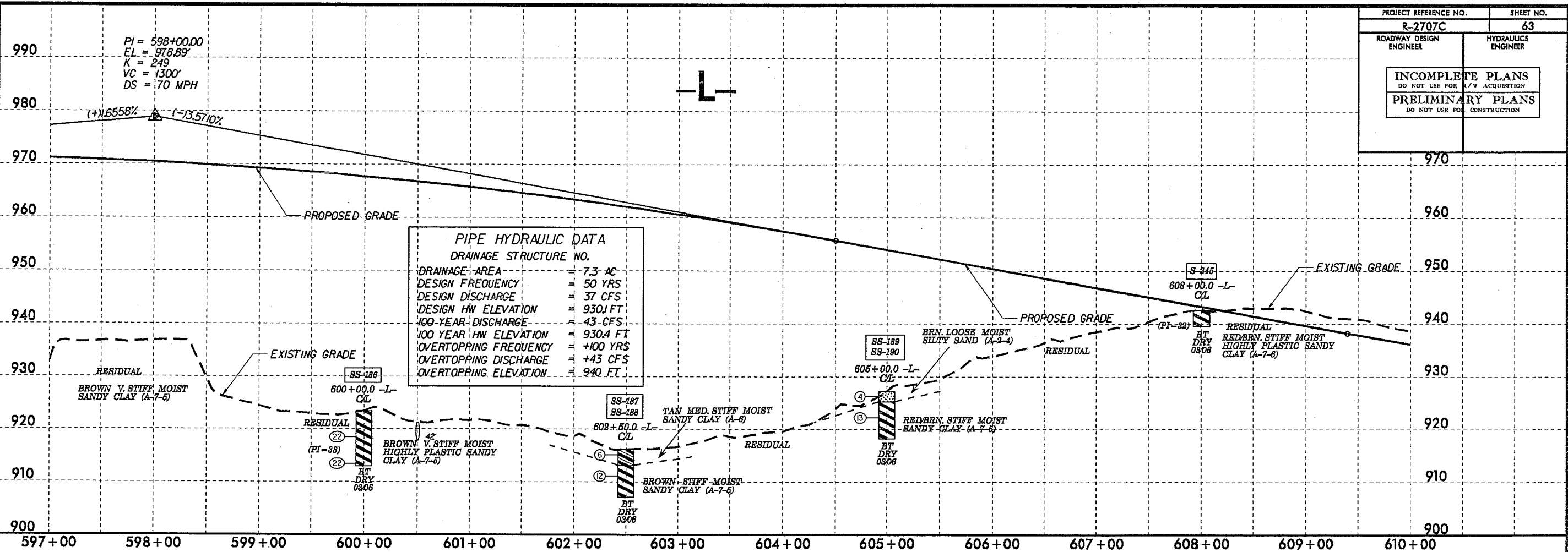


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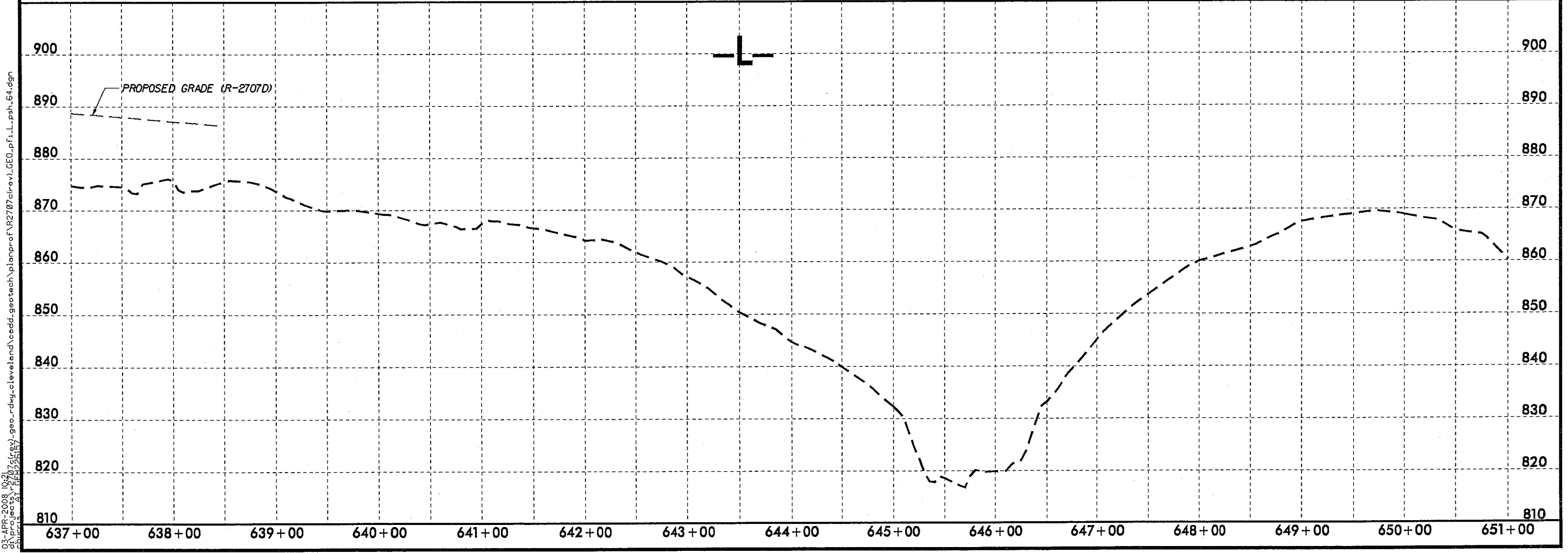
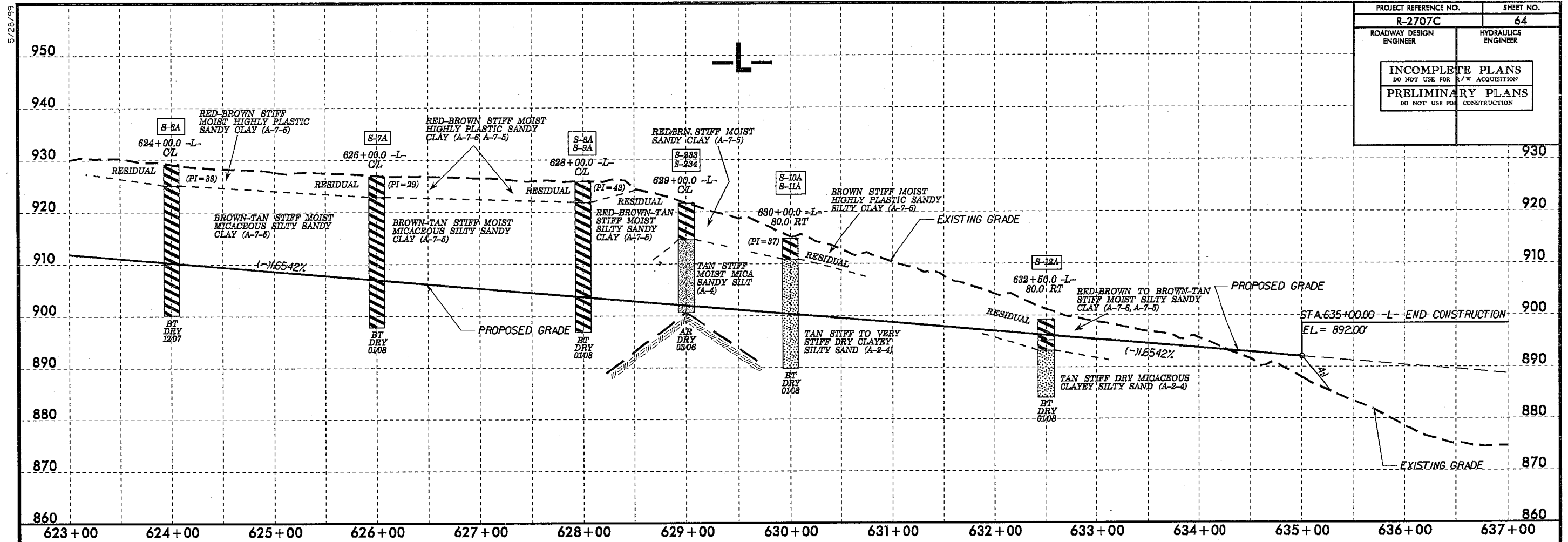
5/28/99

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>63</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	



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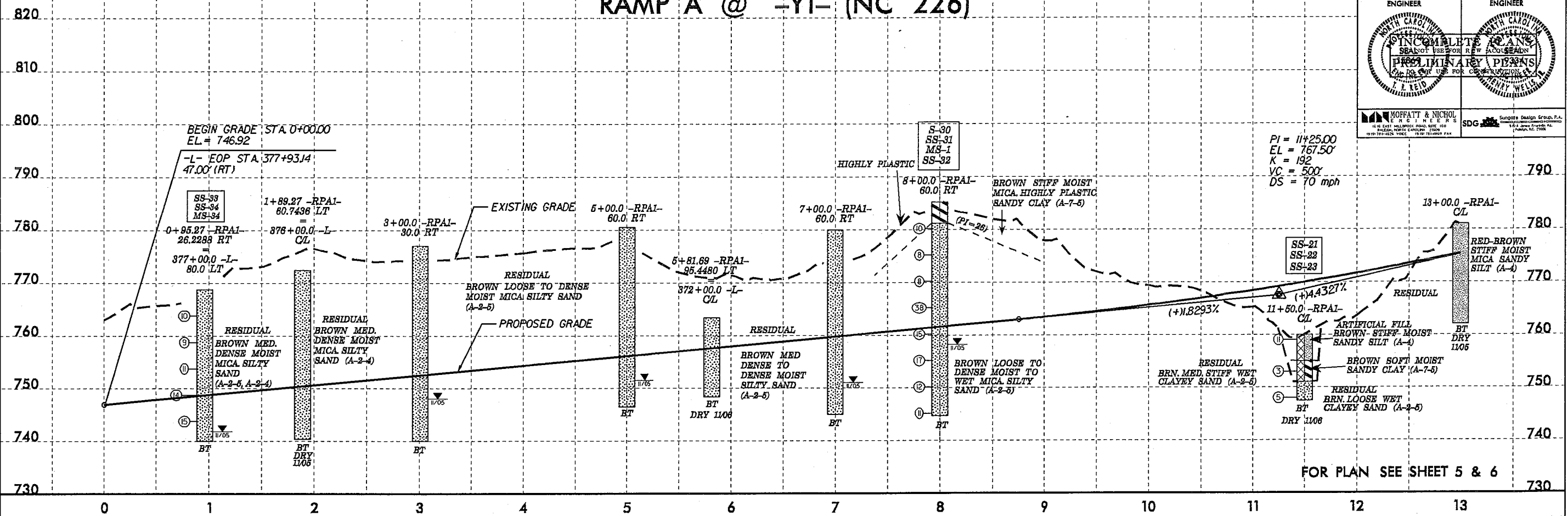
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ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	



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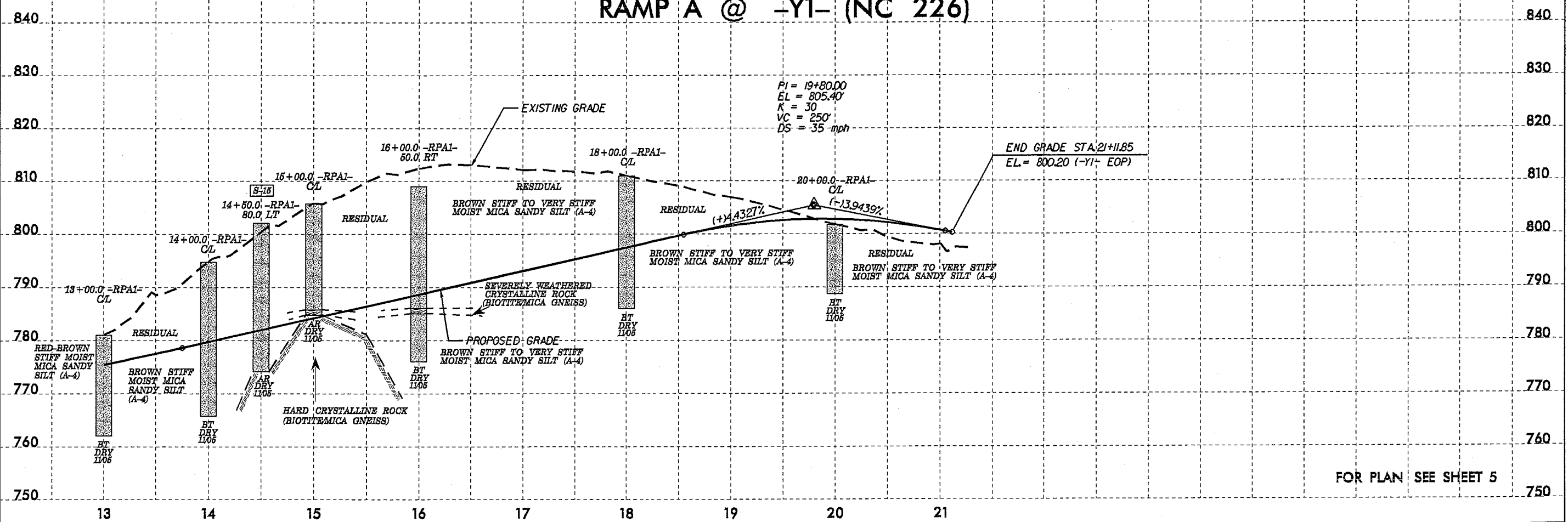
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PROJECT REFERENCE NO. R-2707C	SHEET NO. 65
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
MOFFATT & NICHOL 1414 East Independence Blvd., Suite 100 Raleigh, North Carolina 27601 Phone: 919-482-1000 Fax: 919-482-1001	
SDG Sumpston Design Group, P.A. 11111 North Carolina Highway 101 Raleigh, North Carolina 27615 Phone: 919-482-1000	



FOR PLAN SEE SHEET 5 & 6

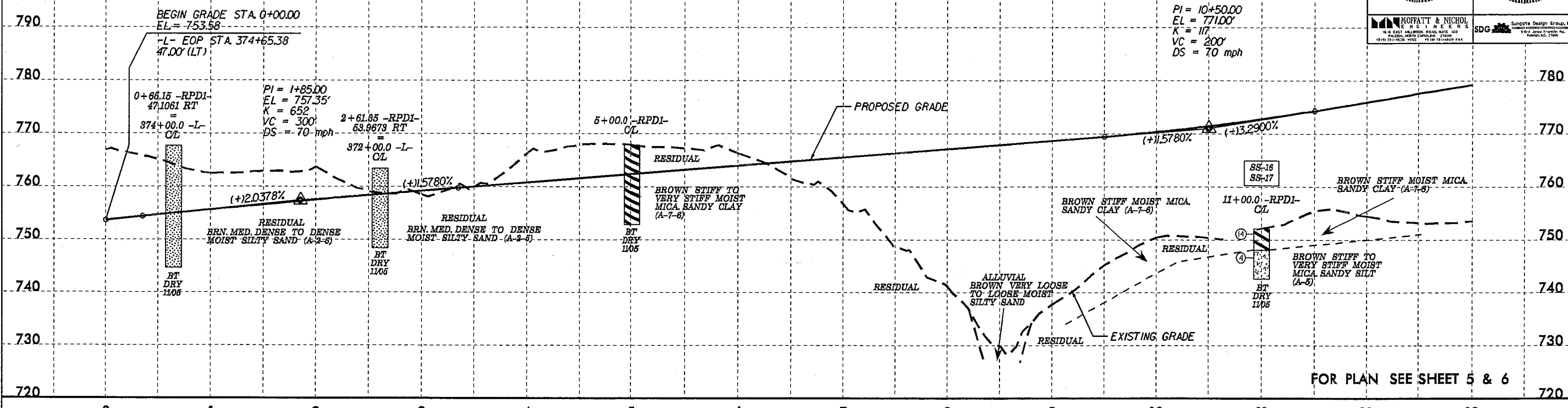
# RAMP A @ -Y1- (NC 226)



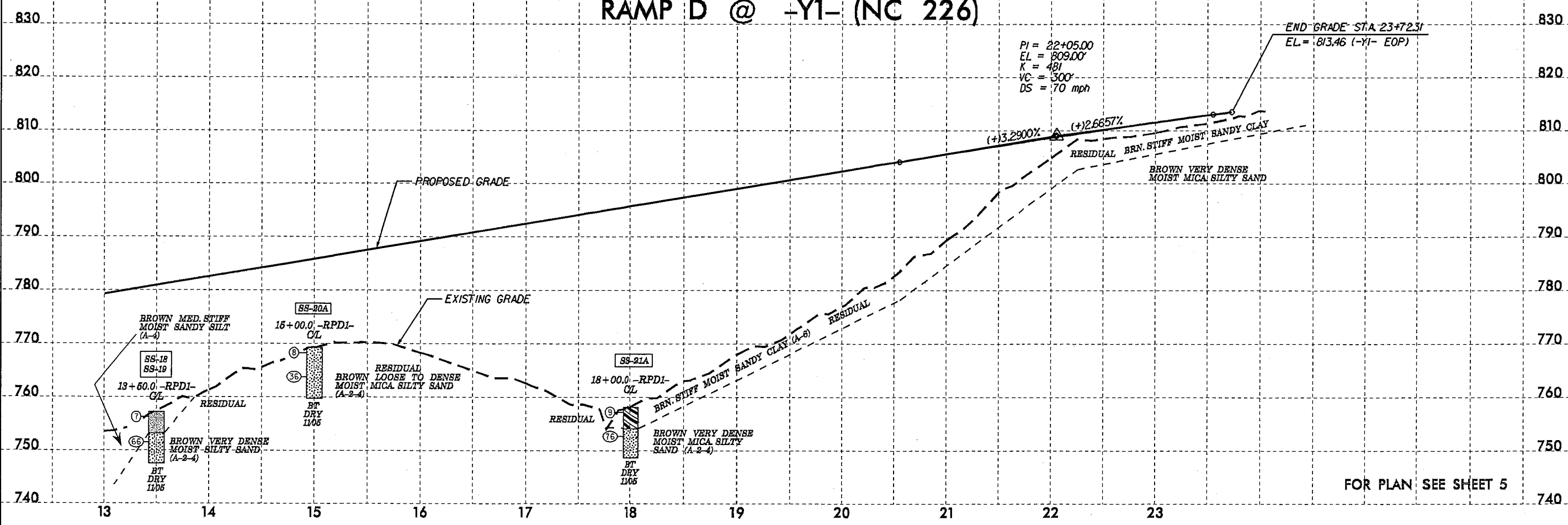
FOR PLAN SEE SHEET 5

# RAMP D @ -Y1- (NC 226)

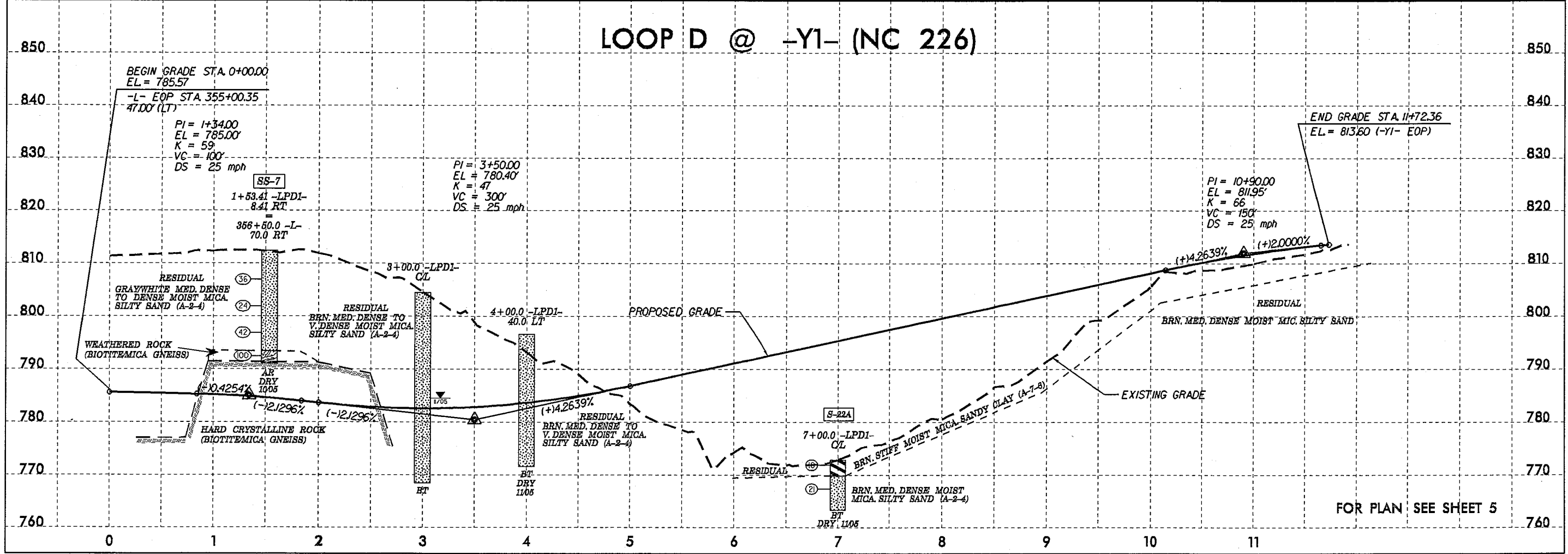
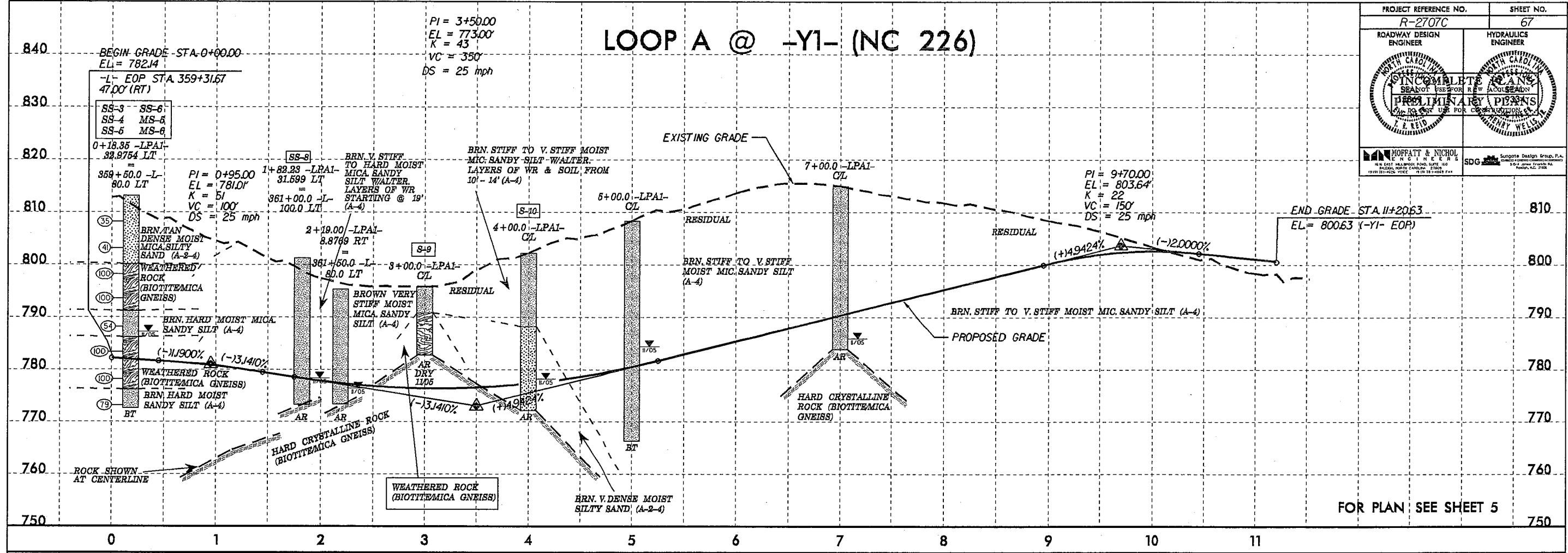
PROJECT REFERENCE NO. R-2707C	SHEET NO. 66
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



# RAMP D @ -Y1- (NC 226)

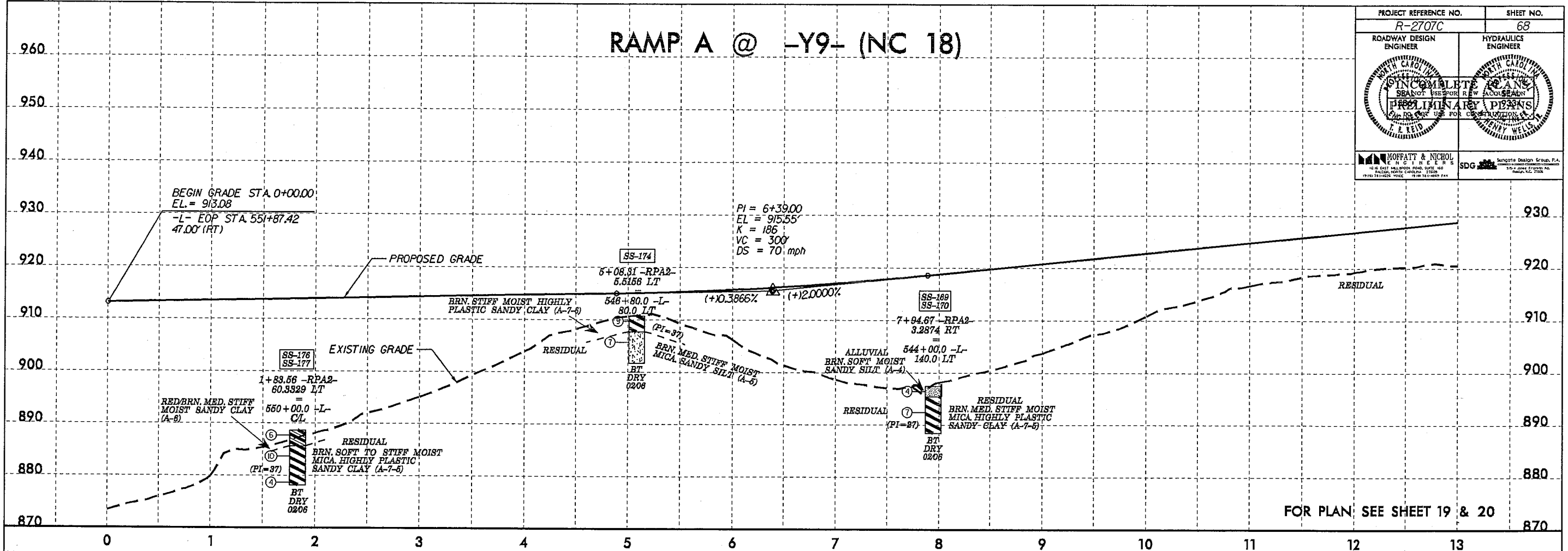


PROJECT REFERENCE NO. R-2707C	SHEET NO. 67
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



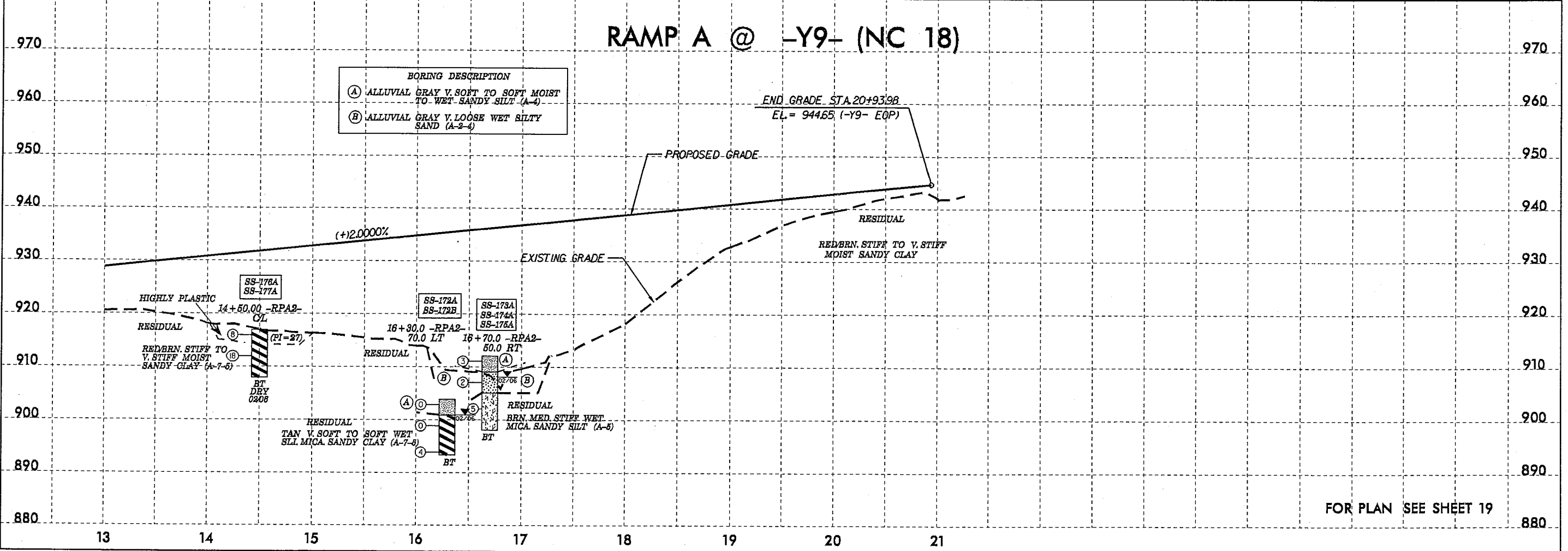
# RAMP A @ -Y9- (NC 18)

PROJECT REFERENCE NO. R-2707C	SHEET NO. 68
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
MOFFATT & NICHOL ENGINEERS & ARCHITECTS 100 EAST HARRIS ROAD, SUITE 400 RALEIGH, NORTH CAROLINA 27601 919-781-8222 VOICE 919-781-4444 FAX	



FOR PLAN SEE SHEET 19 & 20

# RAMP A @ -Y9- (NC 18)



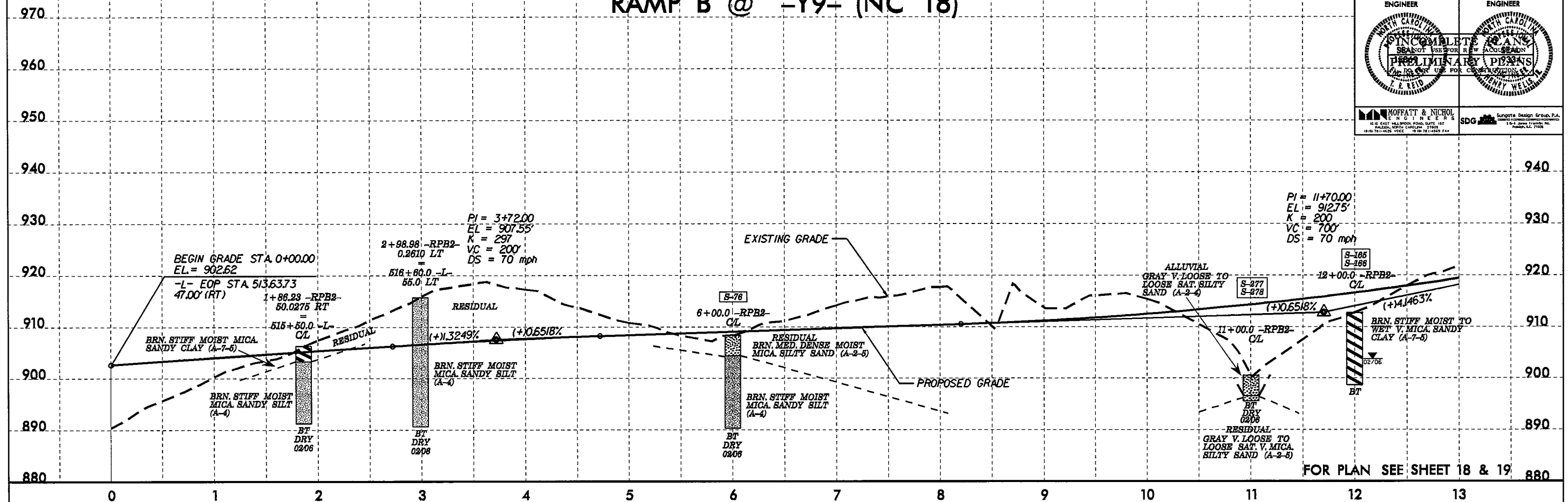
**BORING DESCRIPTION**

- (A) ALLUVIAL GRAY V. SOFT TO SOFT MOIST TO WET SANDY SILT (A-4)
- (B) ALLUVIAL GRAY V. LOOSE WET SILTY SAND (A-2-4)

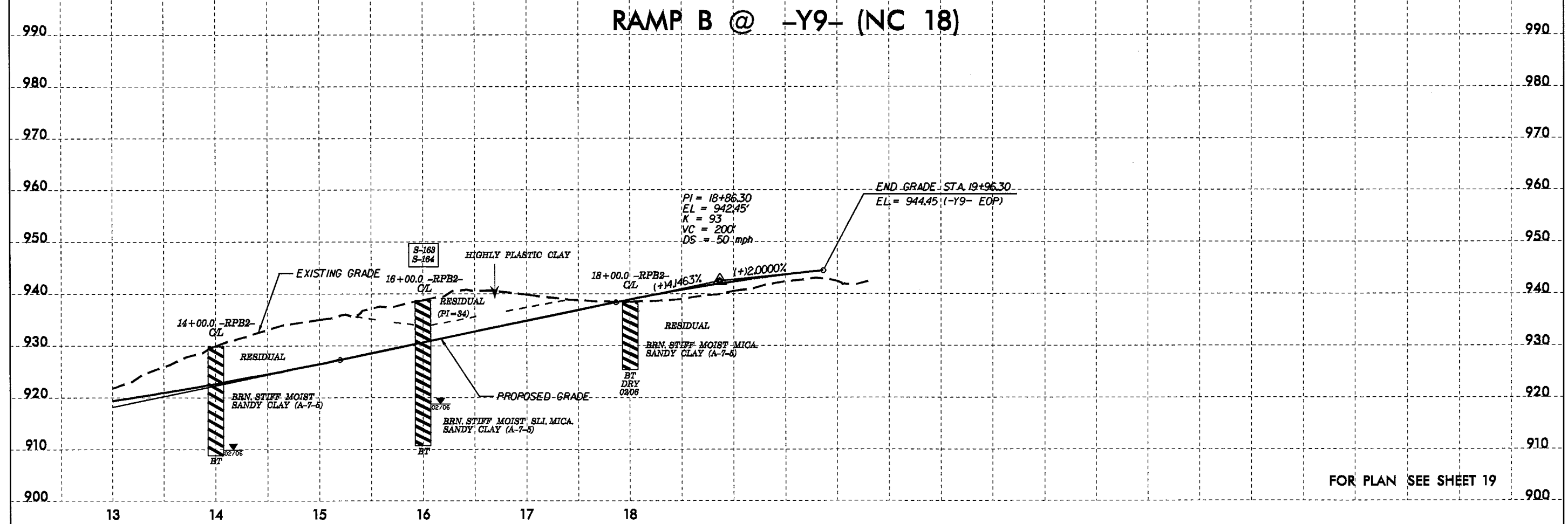
FOR PLAN SEE SHEET 19

# RAMP B @ -Y9- (NC 18)

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>69</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>MOFFATT &amp; NICHOL</b> 1410 EAST WALKER ROAD, SUITE 100 RALEIGH, NORTH CAROLINA 27609 919 781-4425 VOIC 919 781-4425 FAX	<b>SDG</b> SUPPORTS DESIGN GROUP, P.L.L.C. 1501 JAMES STREET, SUITE 100 RALEIGH, NC 27601 919 781-7100

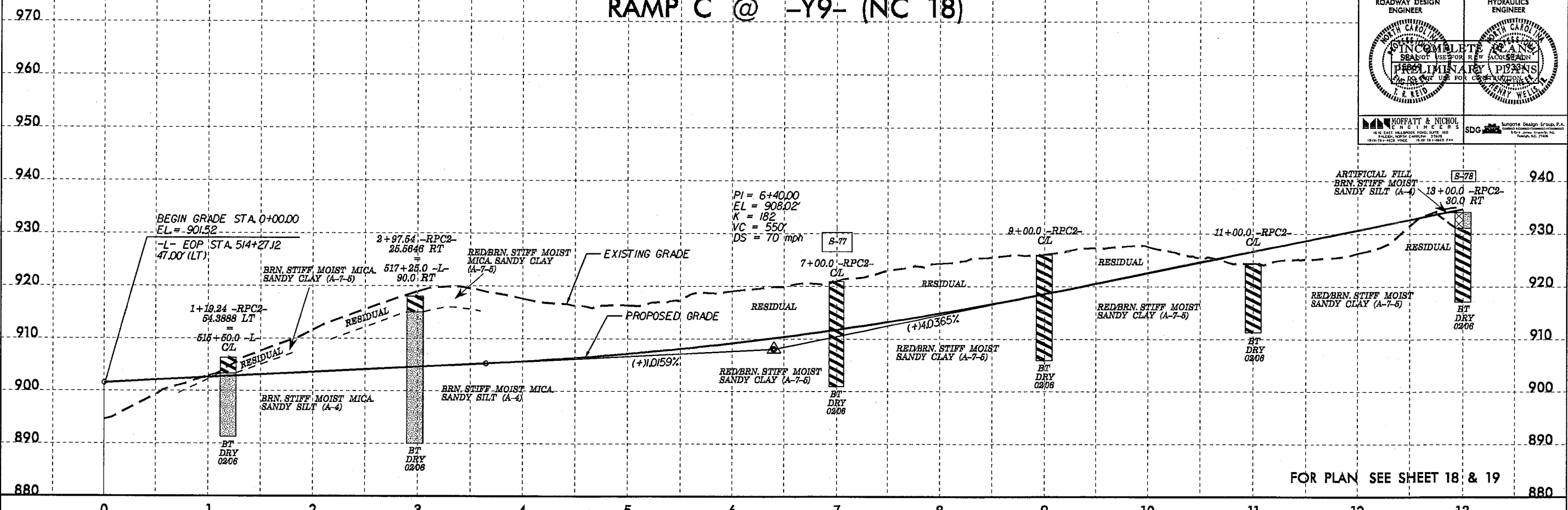


# RAMP B @ -Y9- (NC 18)

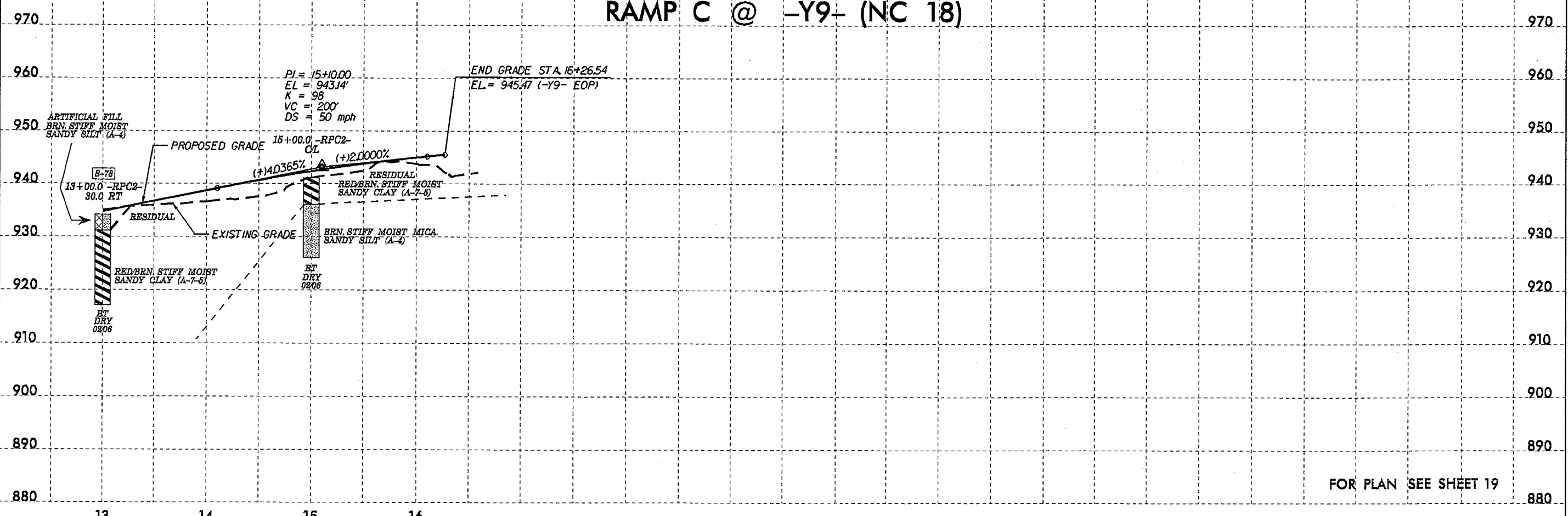


# RAMP C @ -Y9- (NC 18)

PROJECT REFERENCE NO. R-2707C	SHEET NO. 70
ROADWAY DESIGN ENGINEER HOFFATT & NICHOLS	HYDRAULICS ENGINEER HOFFATT & NICHOLS



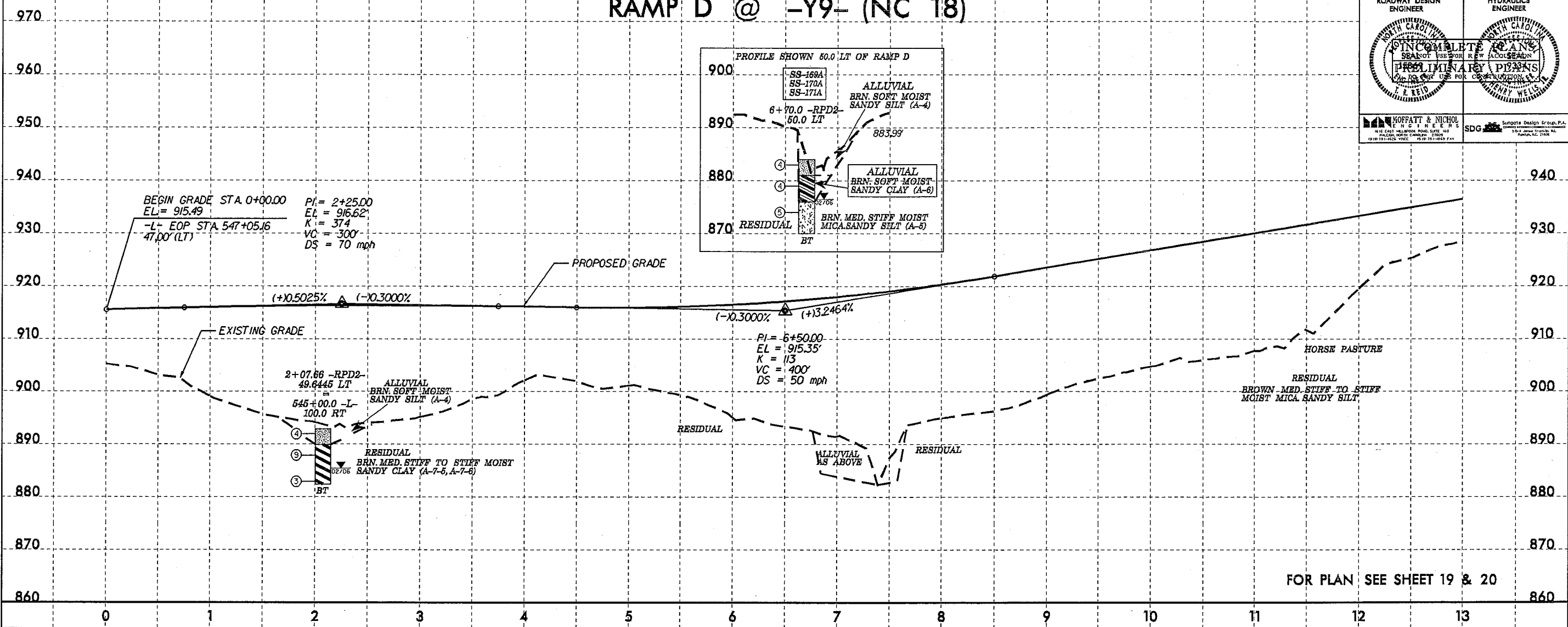
# RAMP C @ -Y9- (NC 18)



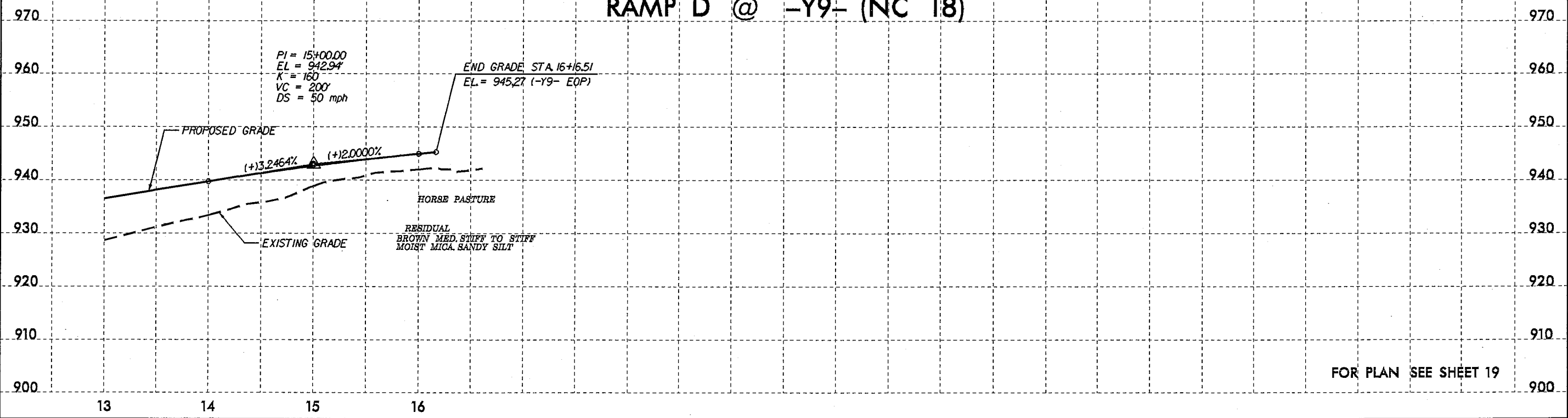


# RAMP D @ -Y9- (NC 18)

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>71</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
MOFFATT & NICHOL ENGINEERS 115 EAST HARRISON ROAD, SUITE 110 WALTON, NORTH CAROLINA 27087 919 781-1000 FAX 919 781-1000	SDG SOUTHWEST DESIGN GROUP, P.A. 1100 WEST 10TH AVENUE, SUITE 100 DENVER, COLORADO 80202 303 733-1100 FAX 303 733-1100

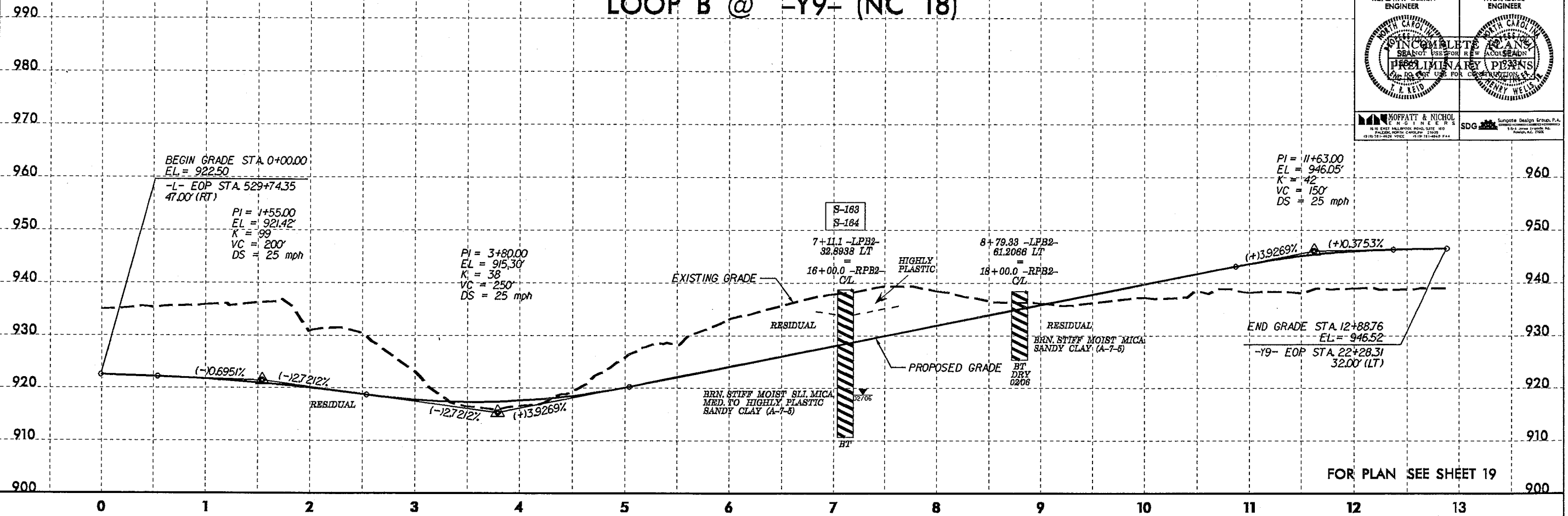


# RAMP D @ -Y9- (NC 18)



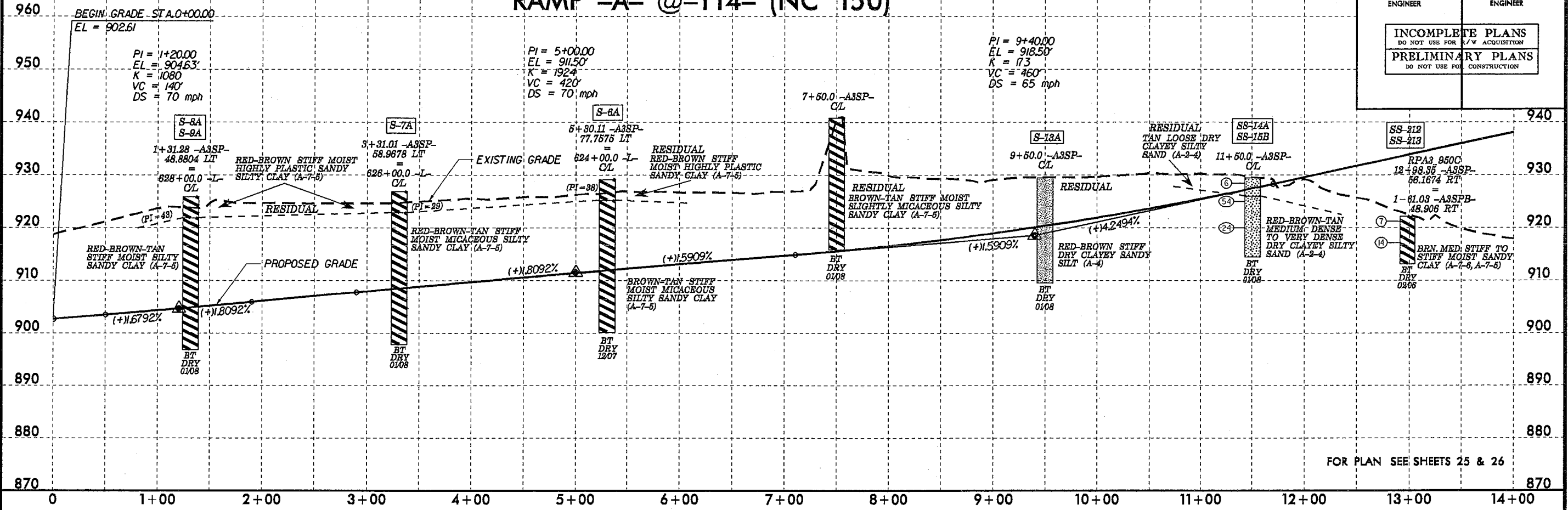
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PROJECT REFERENCE NO. R-2707C	SHEET NO. 72
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

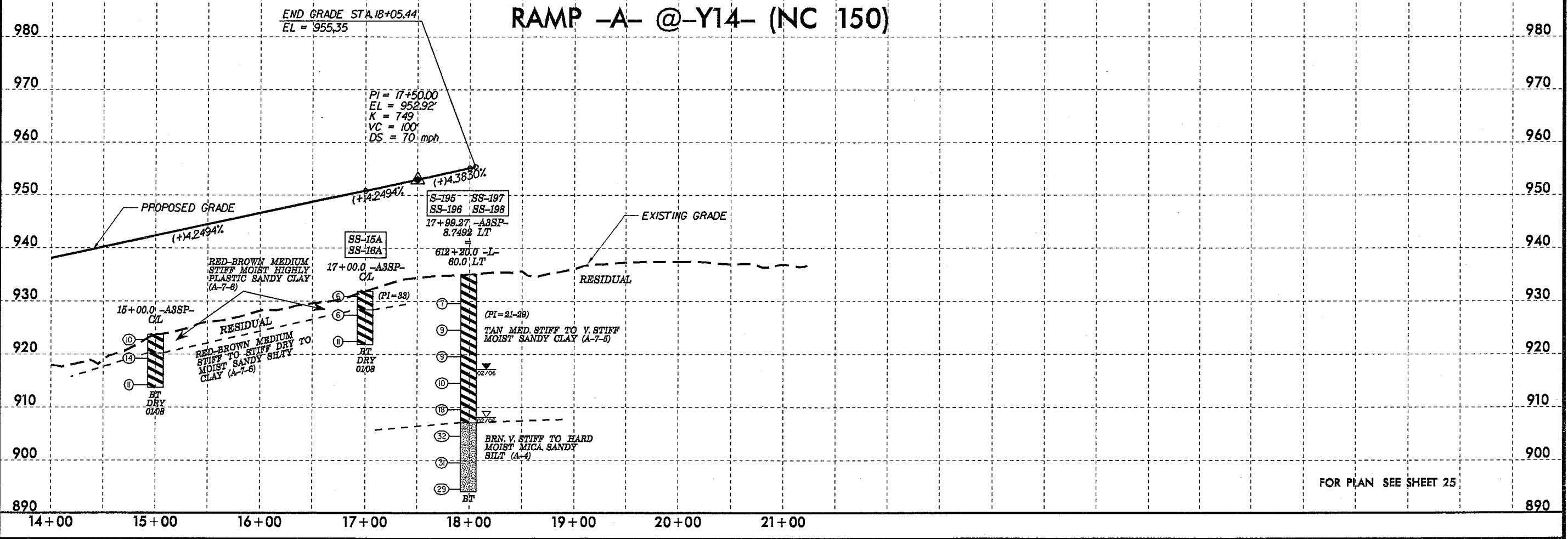


PROJECT REFERENCE NO.	SHEET NO.
R-2707C	73
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR A/W ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

## RAMP -A- @-Y14- (NC 150)



## RAMP -A- @-Y14- (NC 150)



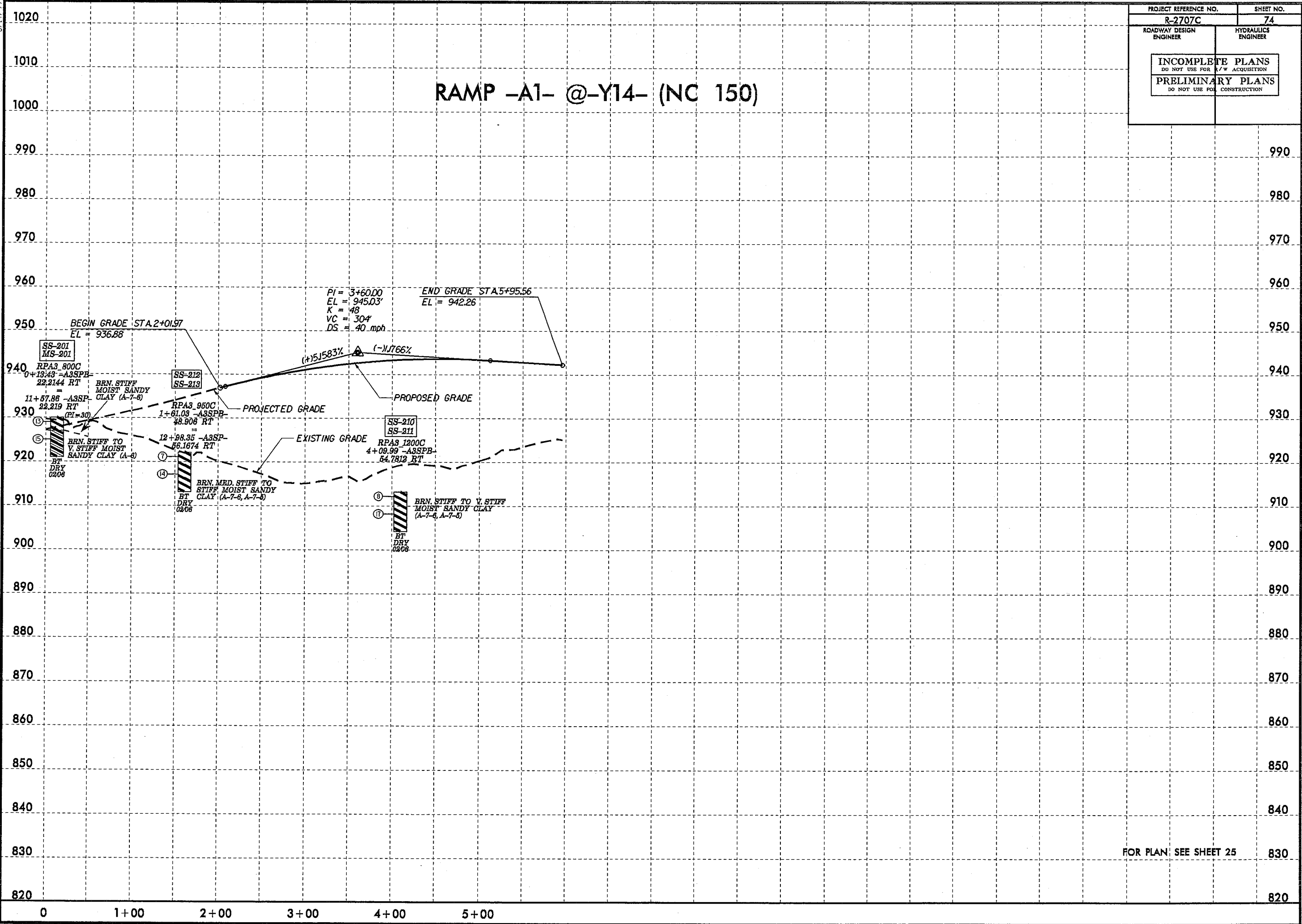
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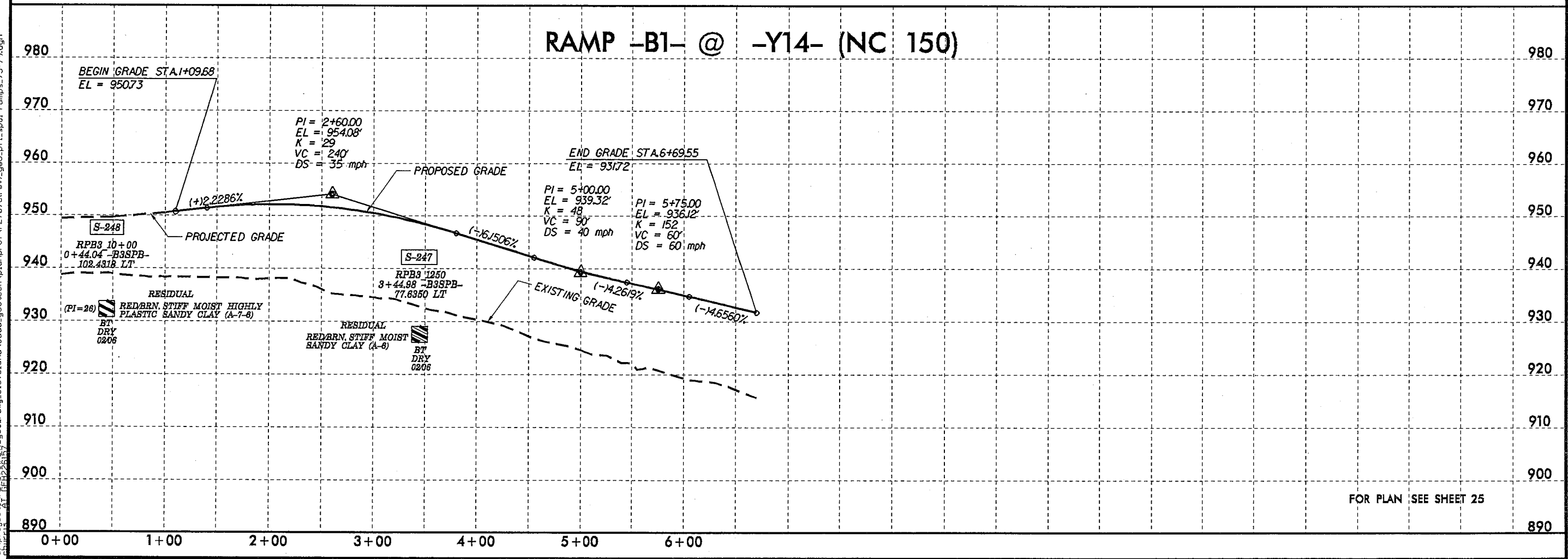
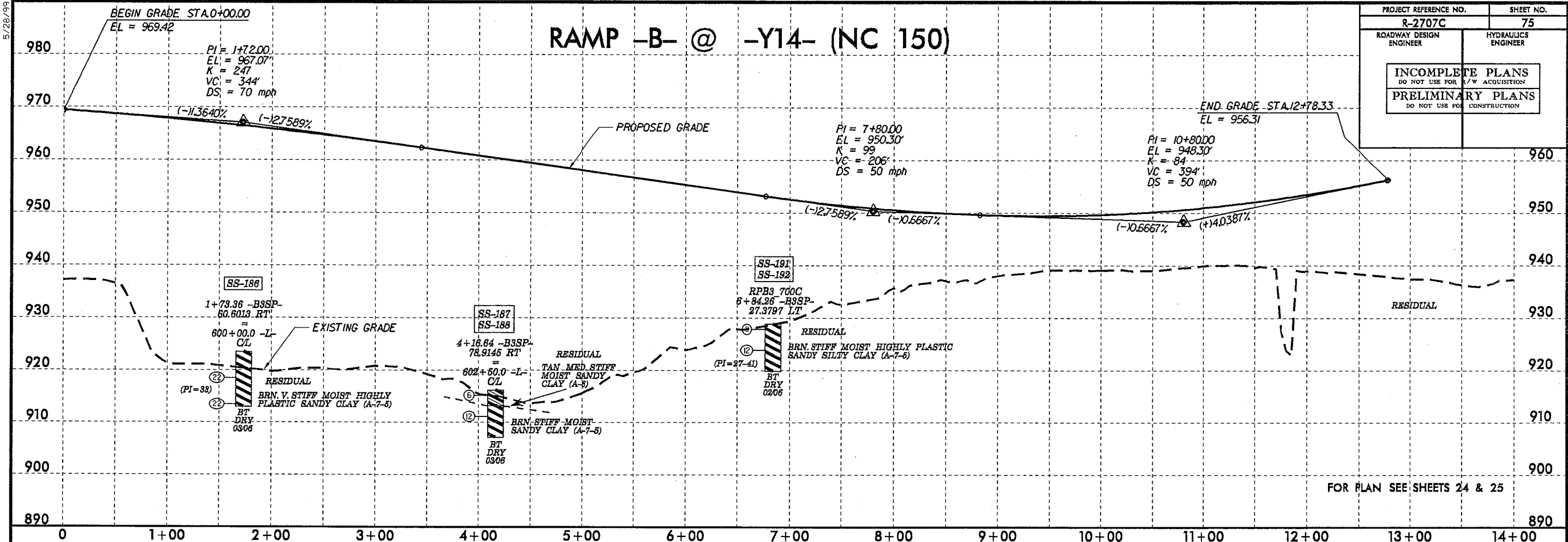
PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>74</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR A/W ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

# RAMP -A1- @-Y14- (NC 150)



FOR PLAN SEE SHEET 25

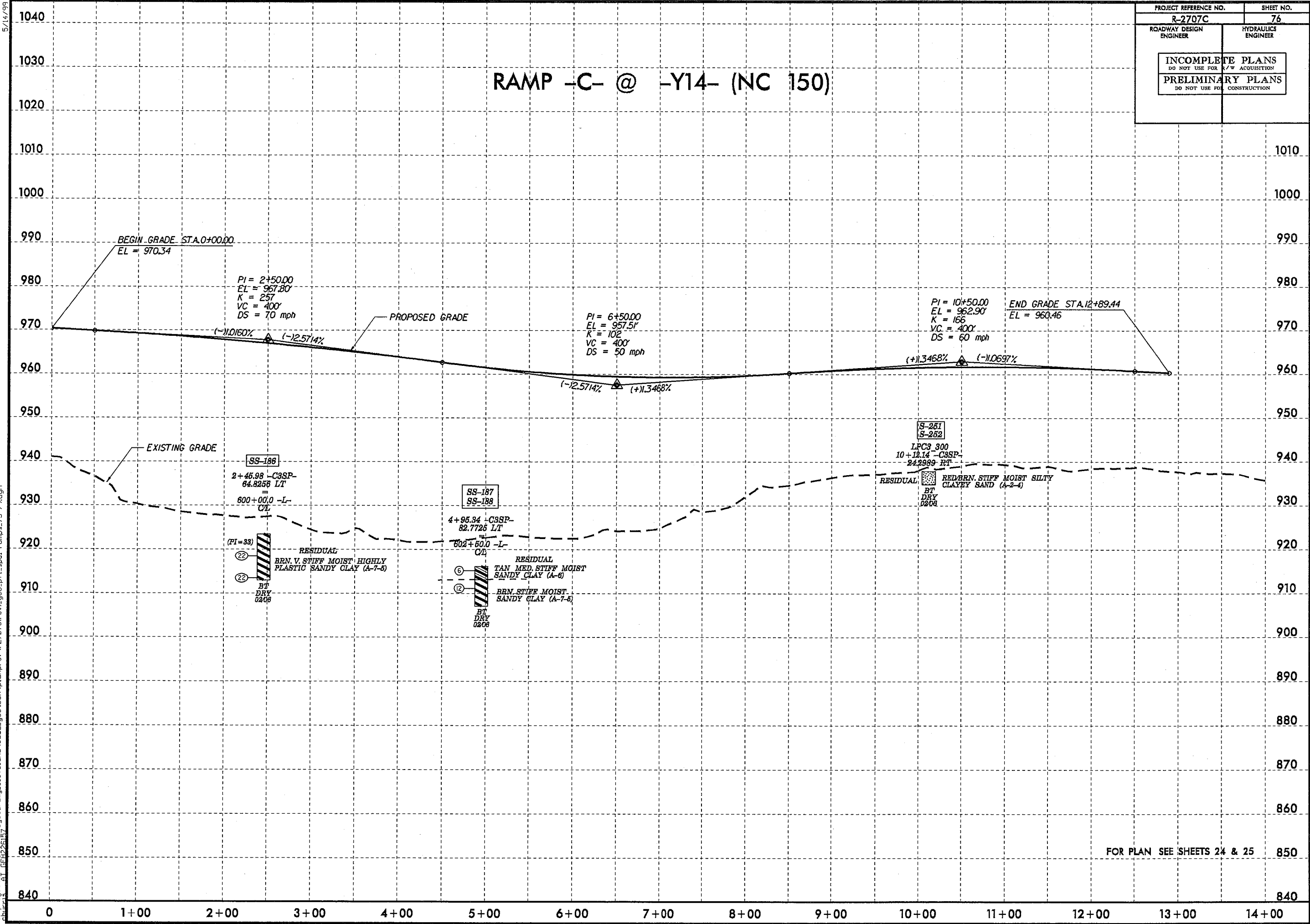
PROJECT REFERENCE NO. R-2707C	SHEET NO. 75
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	



5/28/99  
 28 MAY 2008 09:10  
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PROJECT REFERENCE NO. R-2707C	SHEET NO. 76
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

# RAMP -C- @ -Y14- (NC 150)

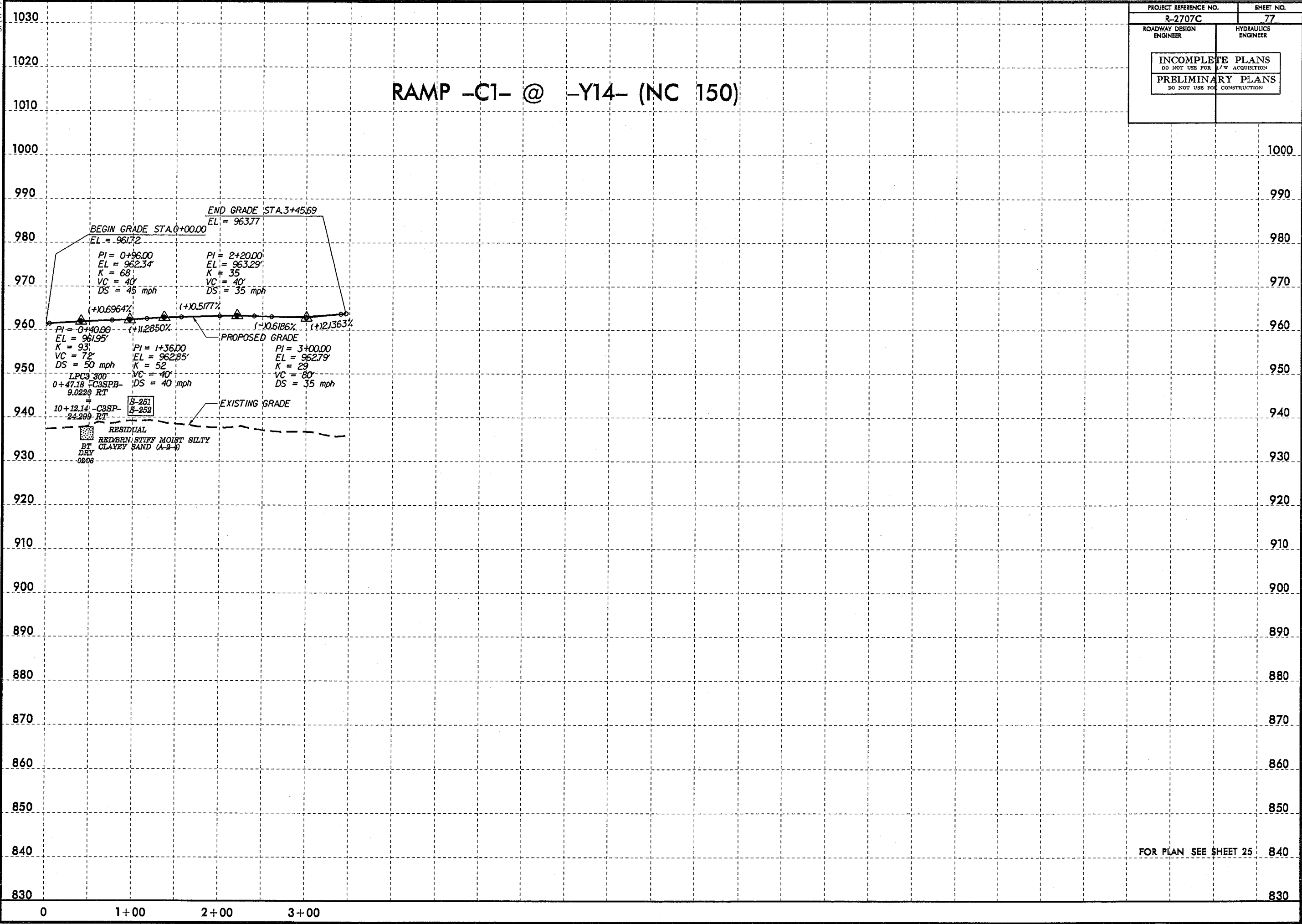


FOR PLAN SEE SHEETS 24 & 25

5/14/99  
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PROJECT REFERENCE NO. R-2707C	SHEET NO. 77
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

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5/14/99  
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FOR PLAN SEE SHEET 25



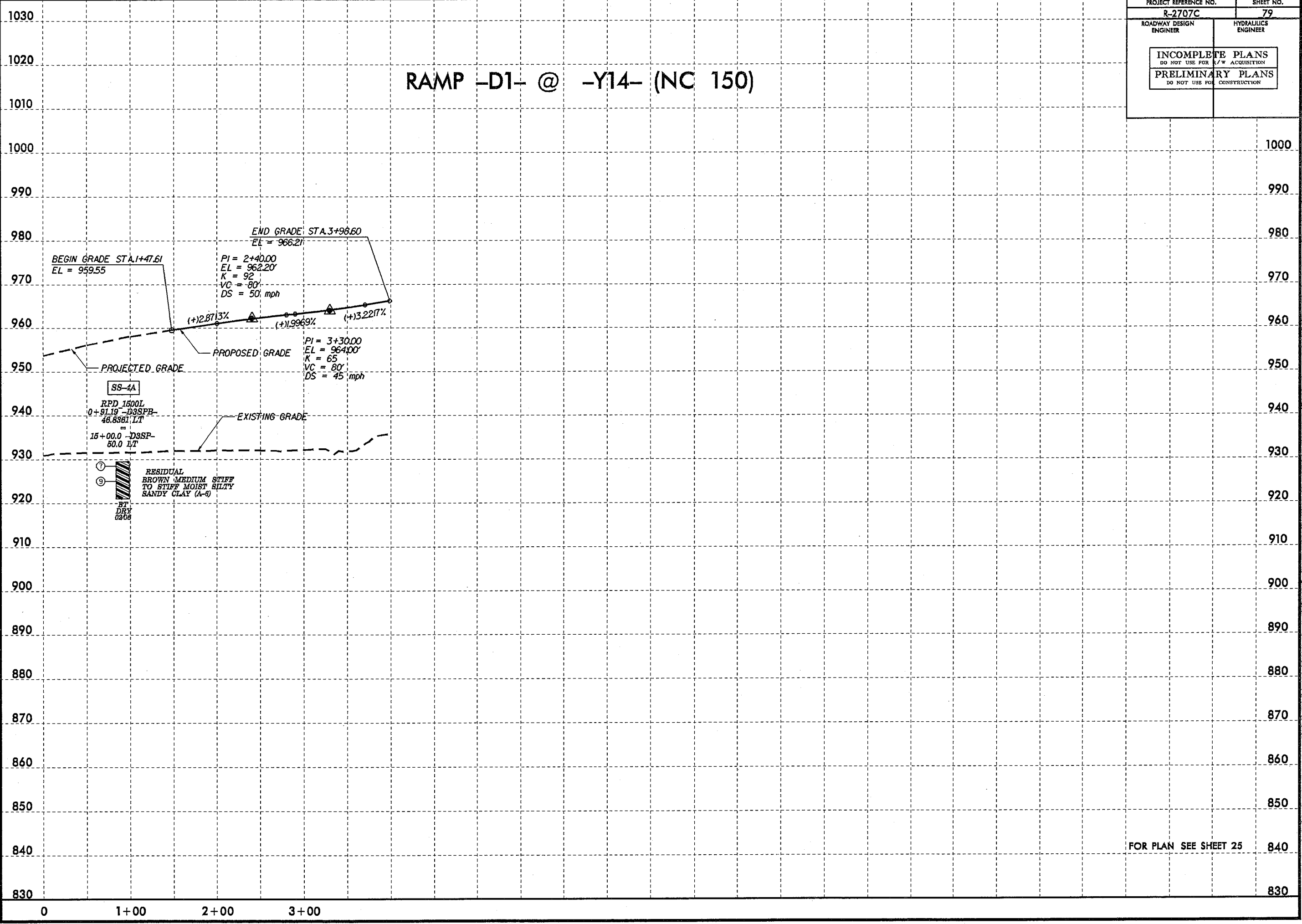


5/14/99

22-MAY-2008 13:45  
d:\projects\2707c\rev\geo-rdwy-cleveland\cadd-geotech\planprof\2707c(rev).geo.plt\spurramps\_73-79.dgn

PROJECT REFERENCE NO. R-2707C	SHEET NO. 79
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

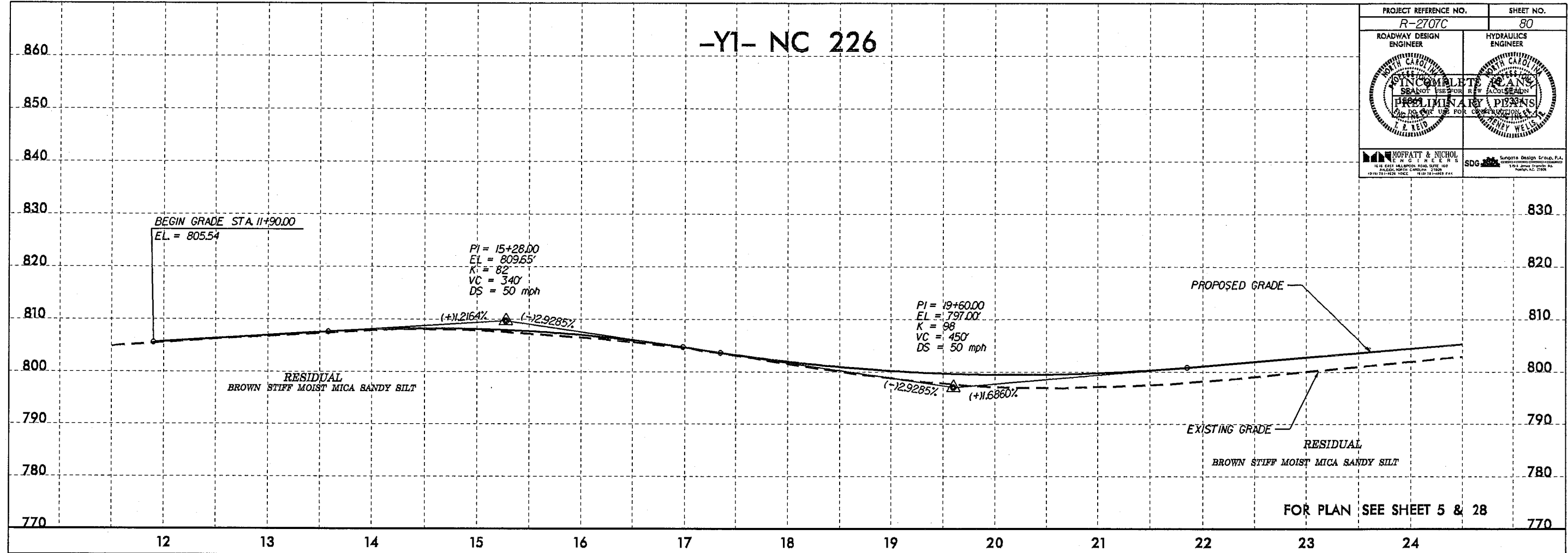
# RAMP -D1- @ -Y14- (NC 150)



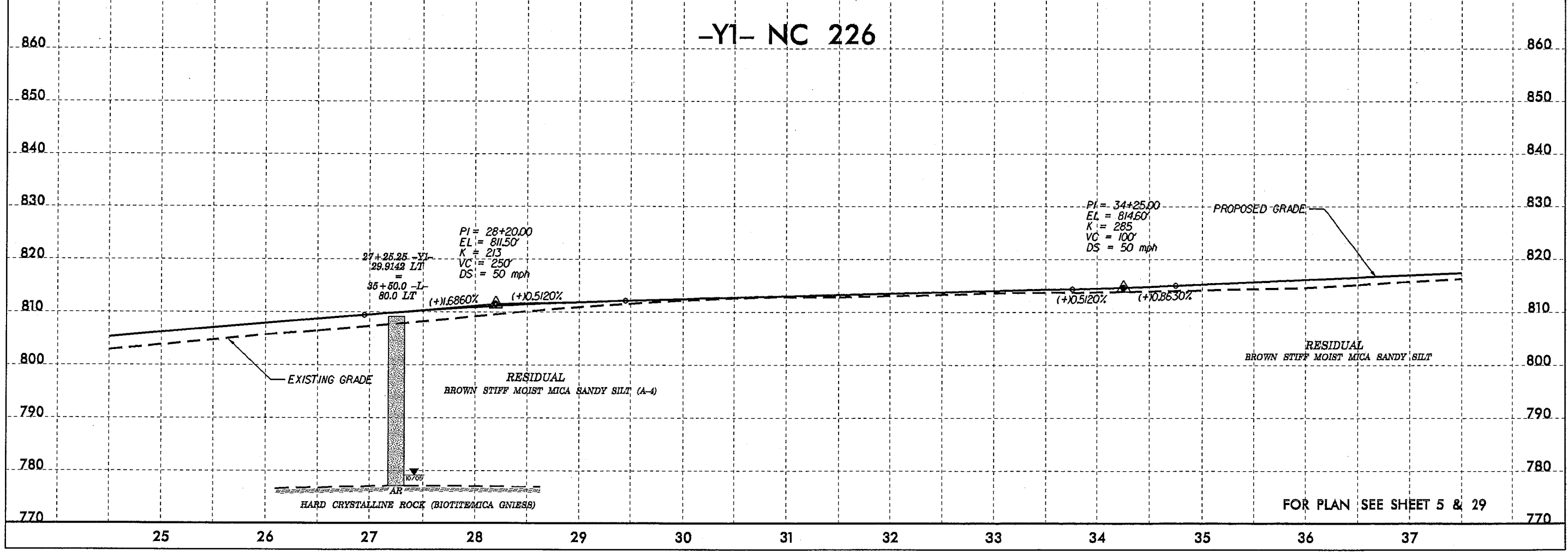
FOR PLAN SEE SHEET 25

# -YI- NC 226

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>80</b>
ROADWAY DESIGN ENGINEER 	HYDRAULICS ENGINEER 
<b>PRELIMINARY PLANS</b>	
<b>MOFFATT &amp; NICHOL</b> ENGINEERS 1400 WEST HALESBROOK ROAD, SUITE 100 FALCON, NORTH CAROLINA 27829 PHONE: 703-221-1100 FAX: 703-221-1101	
<b>SDG</b> <small>Support Design Group, P.A.</small> 1100 WEST HALESBROOK ROAD, SUITE 100 FALCON, NORTH CAROLINA 27829 PHONE: 703-221-1100 FAX: 703-221-1101	

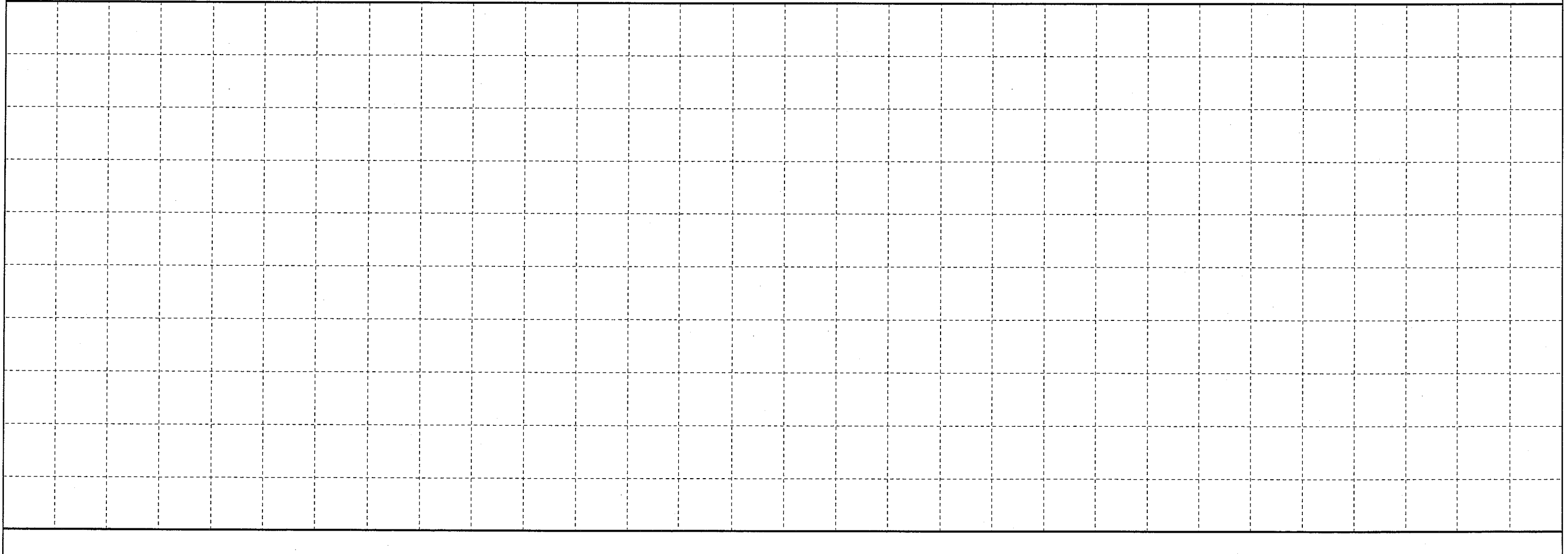
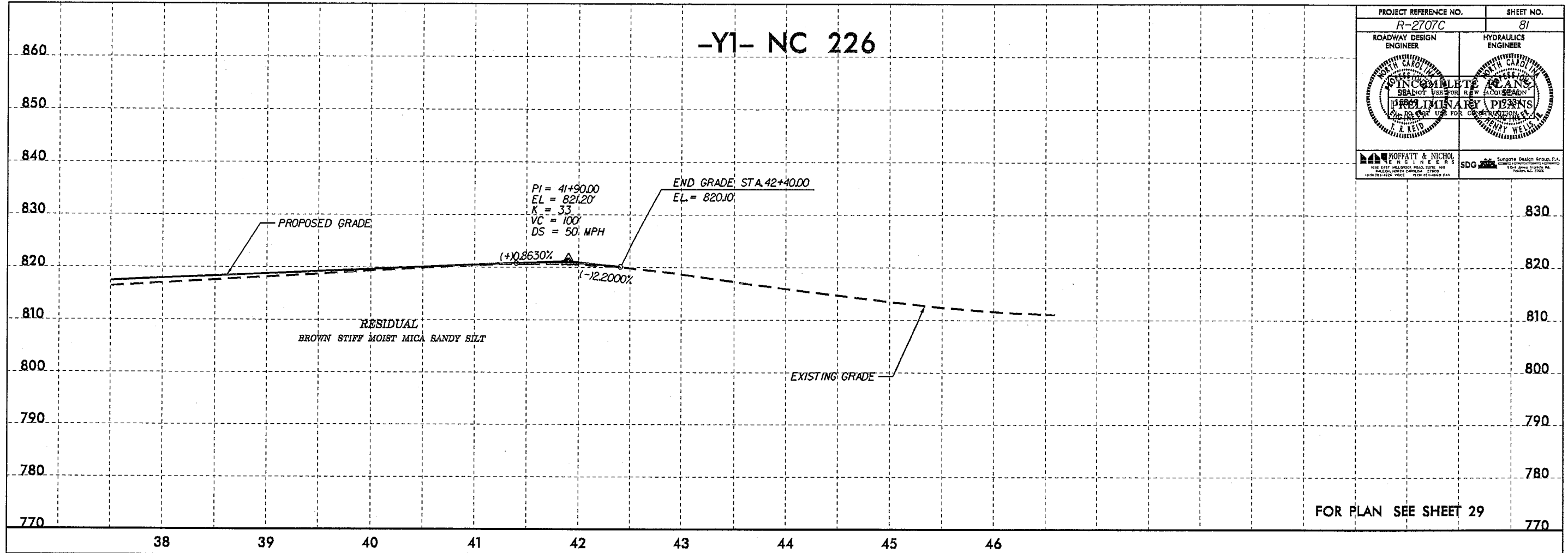


# -YI- NC 226

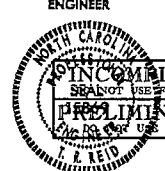
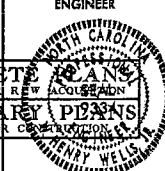

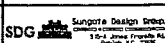


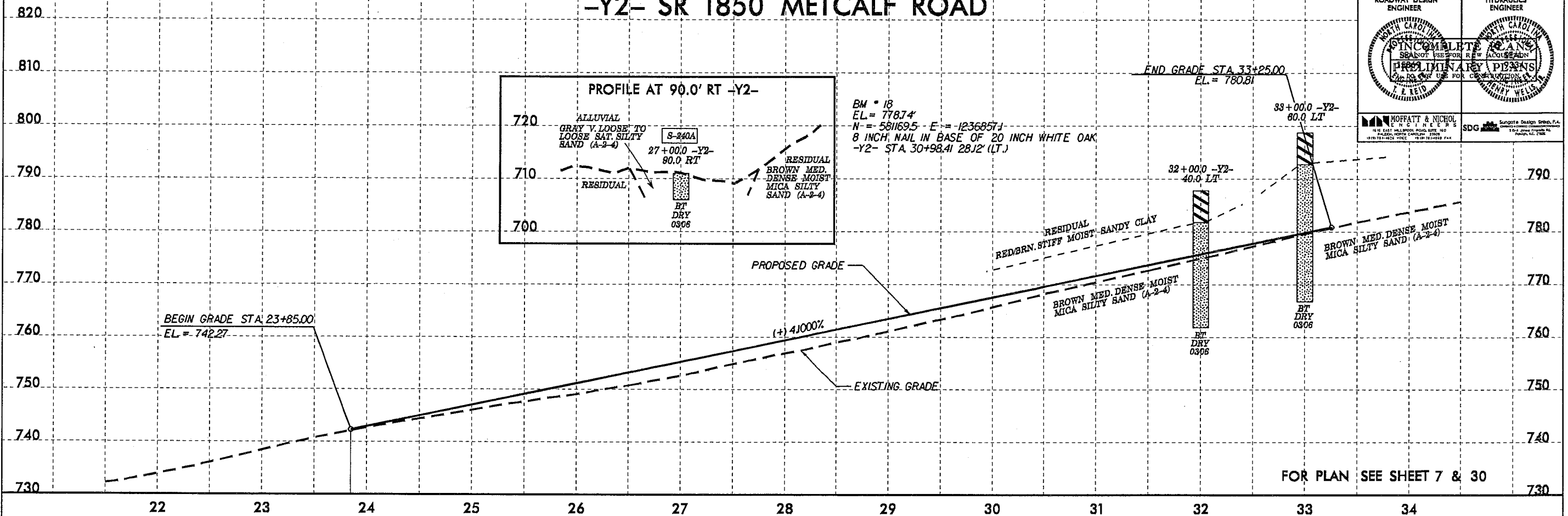
# -Y1- NC 226

PROJECT REFERENCE NO. <i>R-2707C</i>	SHEET NO. <i>81</i>
ROADWAY DESIGN ENGINEER <i>[Signature]</i>	HYDRAULICS ENGINEER <i>[Signature]</i>
INCOMPLETE DO NOT USE FOR CONSTRUCTION	PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION
<b>HOPPATT &amp; NICHOL</b> ENGINEERS 140 WEST HILLSBORO ROAD, SUITE 100 RALEIGH, NORTH CAROLINA 27601 1987-1988 LICENSE # 1987-1988	<b>SDG</b> Sungate Design Group, P.A. 1504 JONES CREEK ROAD RALEIGH, NC 27601 1987-1988 LICENSE # 1987-1988

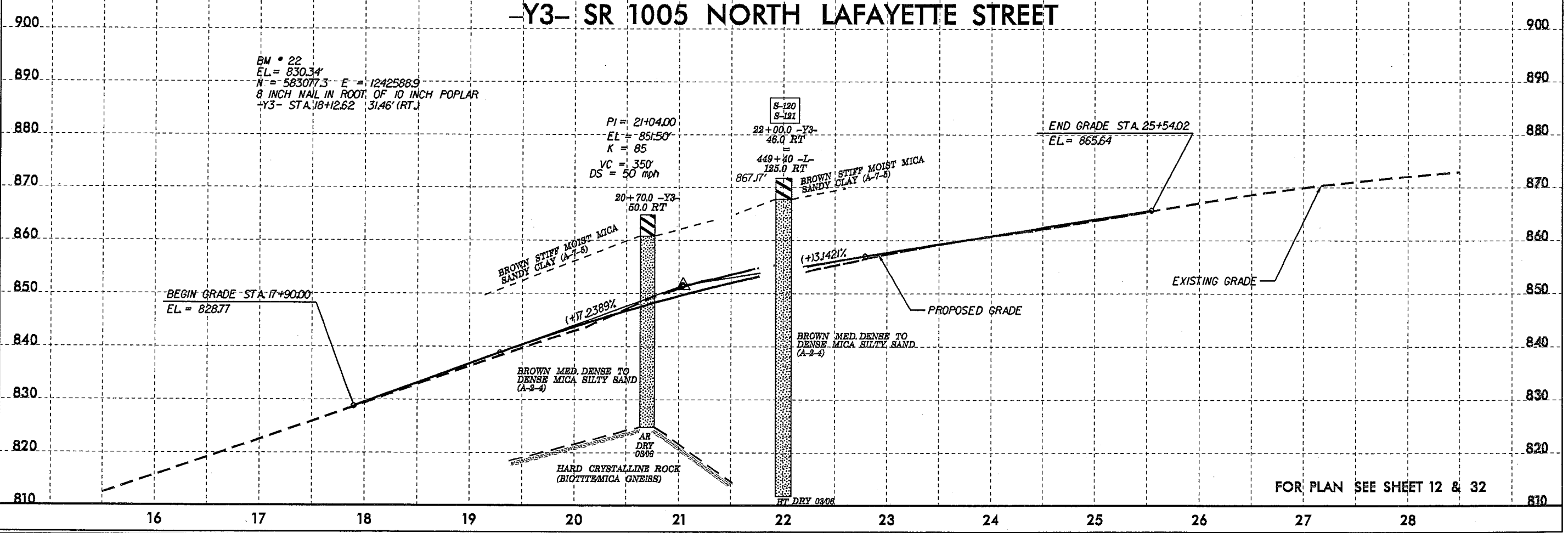


# -Y2- SR 1850 METCALF ROAD





PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>82</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
	
	

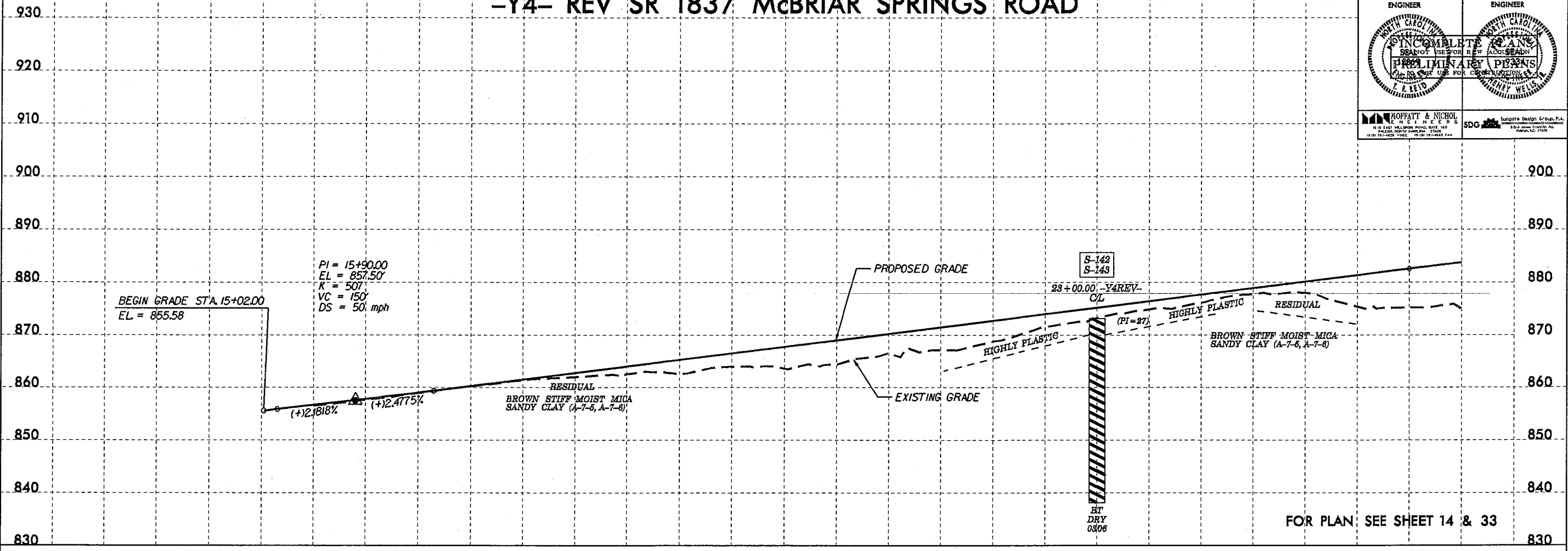


# -Y3- SR 1005 NORTH LAFAYETTE STREET

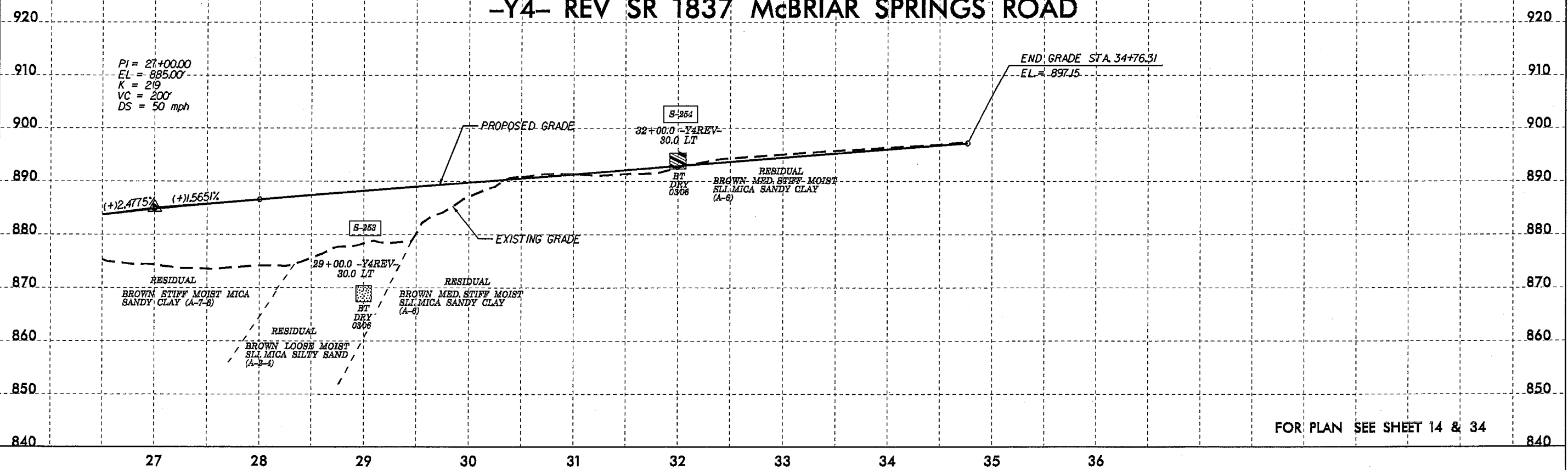


# -Y4- REV SR 1837 McBRIAR SPRINGS ROAD

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>83</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
	
 	

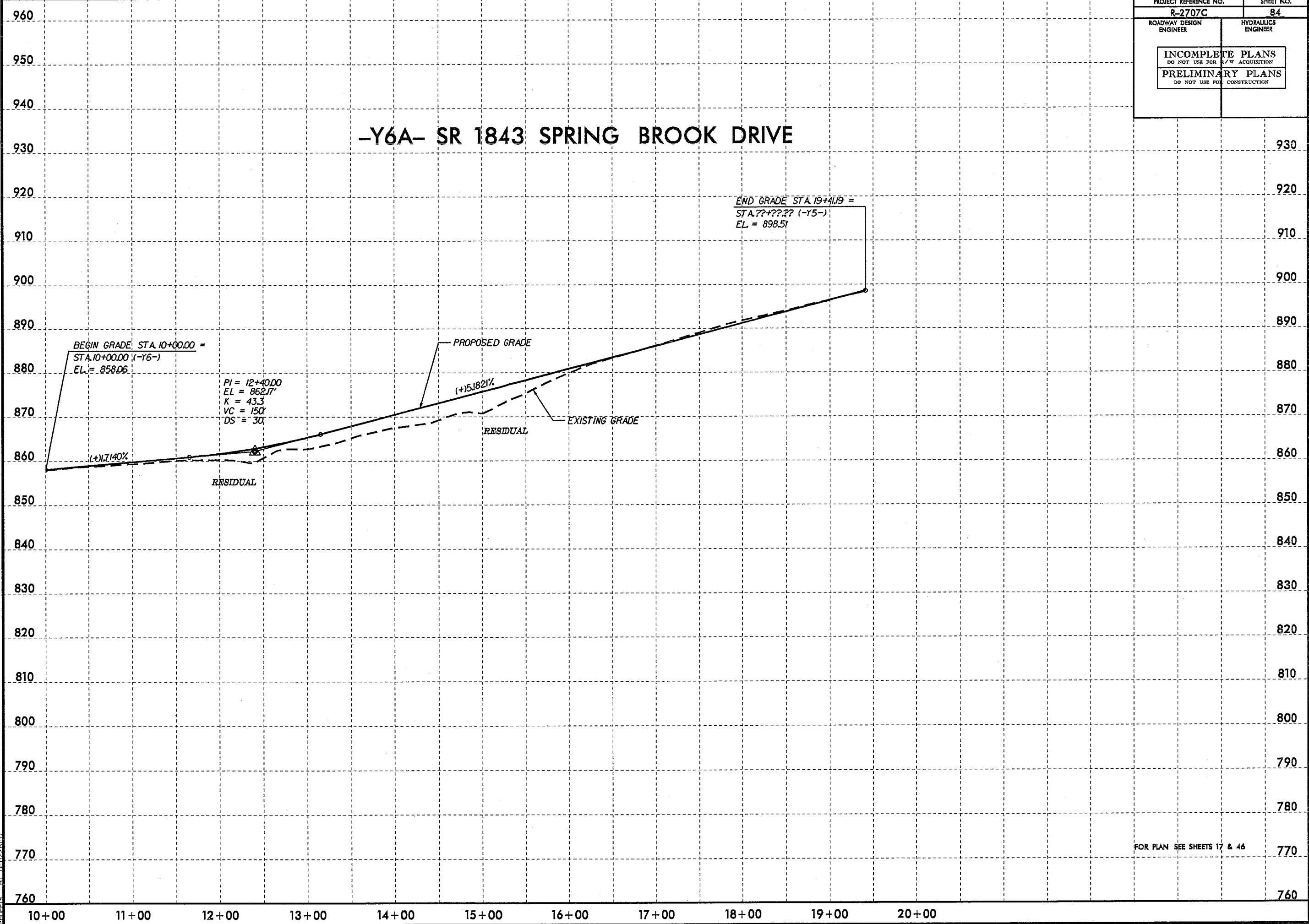


# -Y4- REV SR 1837 McBRIAR SPRINGS ROAD



PROJECT REFERENCE NO. R-2707C	SHEET NO. 84
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

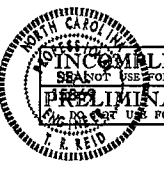
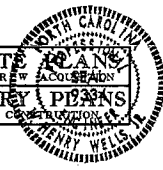

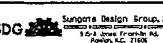

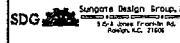
# -Y6A- SR 1843 SPRING BROOK DRIVE

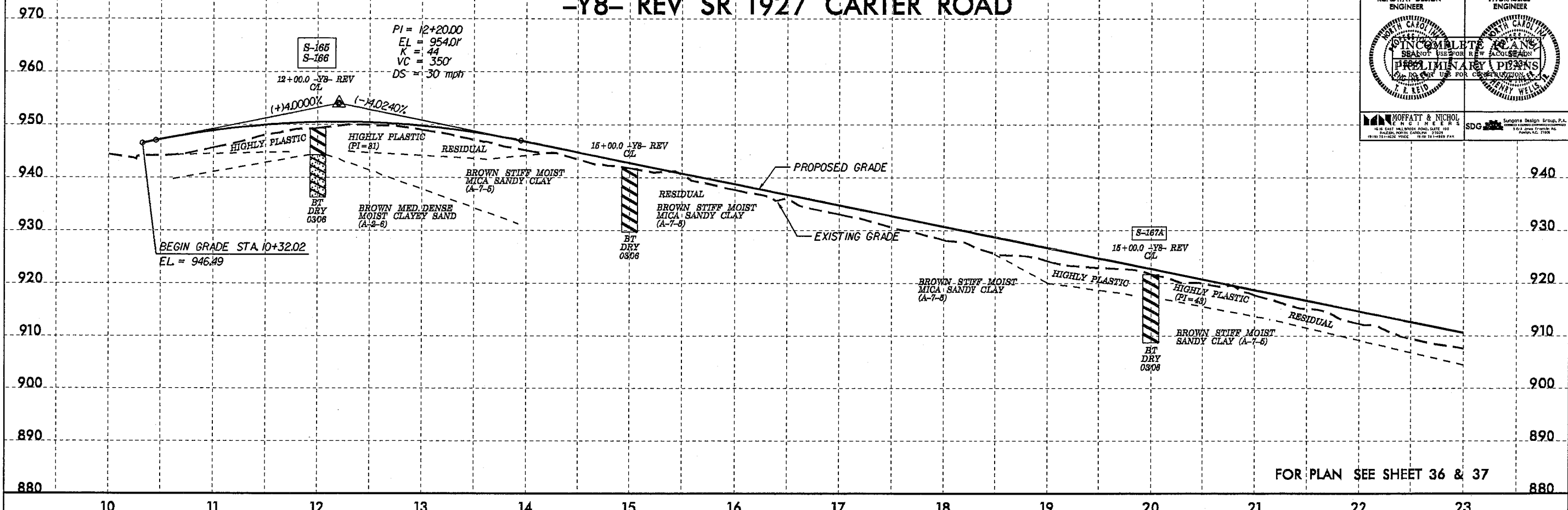


FOR PLAN SEE SHEETS 17 & 46

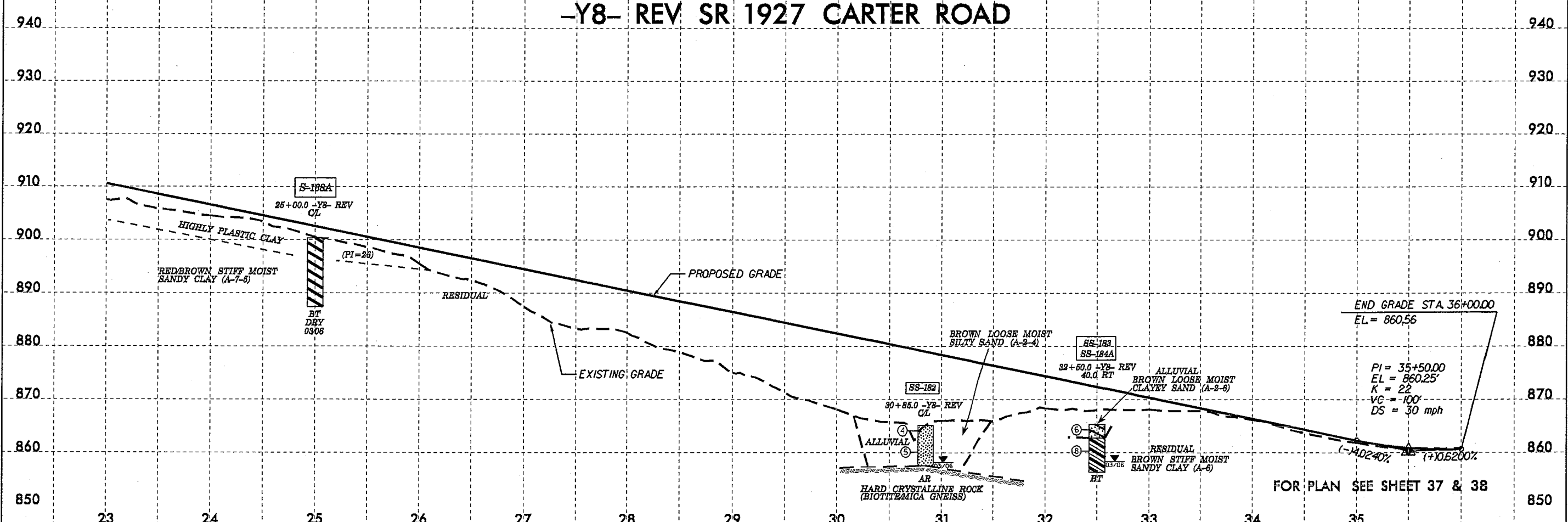
5/14/99  
 22-MAY-2008 14:15  
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# -Y8- REV SR 1927 CARTER ROAD

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>85</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
	
	
	



# -Y8- REV SR 1927 CARTER ROAD

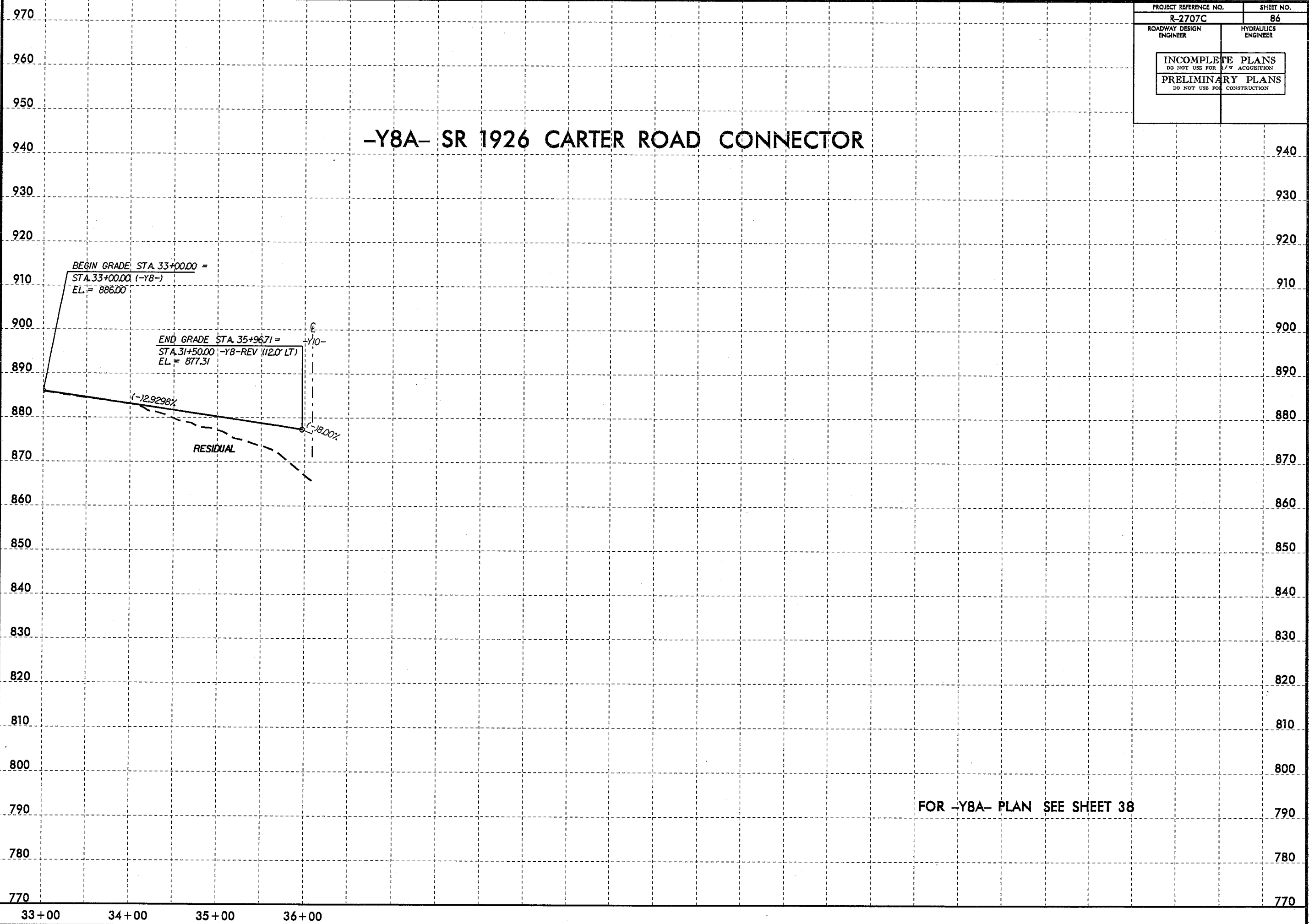


5/14/99

B:\APR-2008\1577\1577.dwg; c:\leveland\cadd\geotech\planpro\v2707c(rev).geo.pf...y8a\_86.dgn

PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>86</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

# -Y8A- SR 1926 CARTER ROAD CONNECTOR



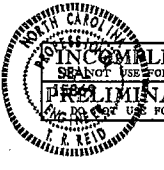
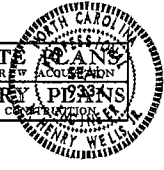


FOR -Y8A- PLAN SEE SHEET 38

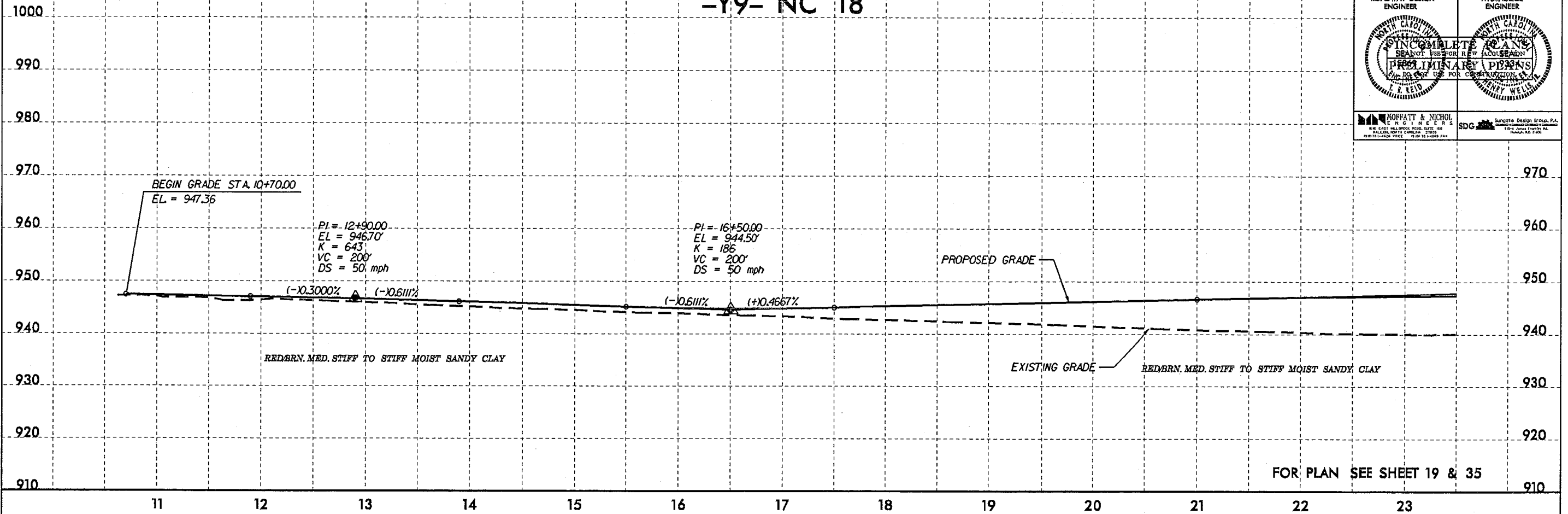
33+00    34+00    35+00    36+00

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770

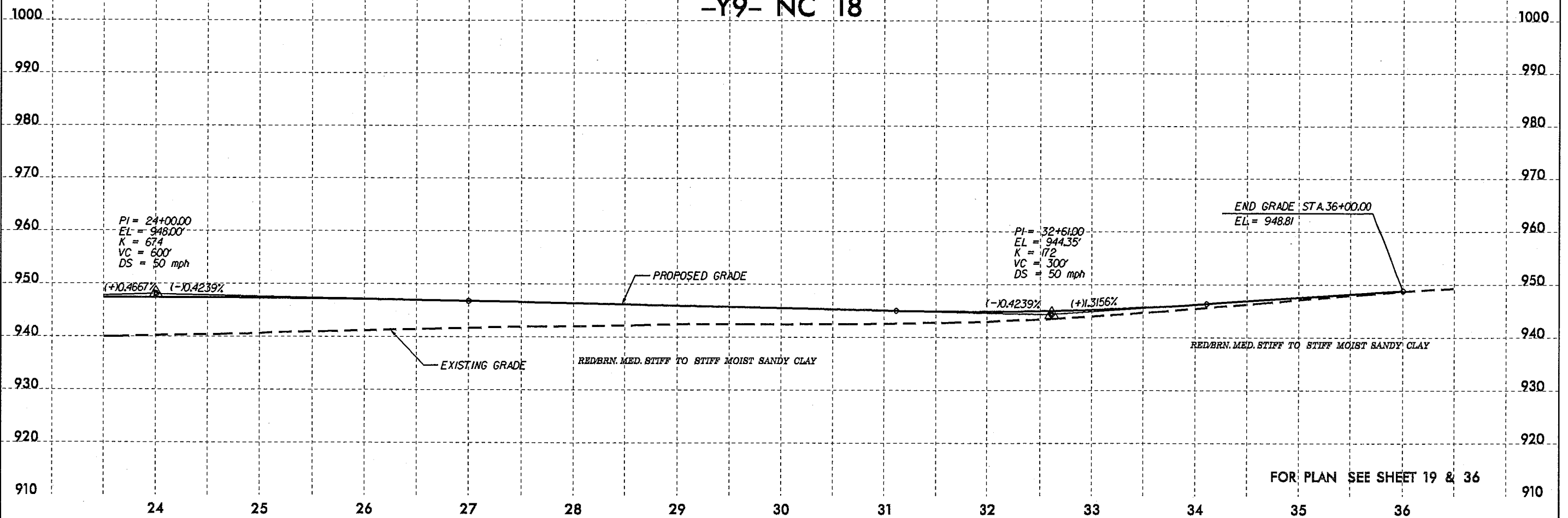


# -Y9- NC 18

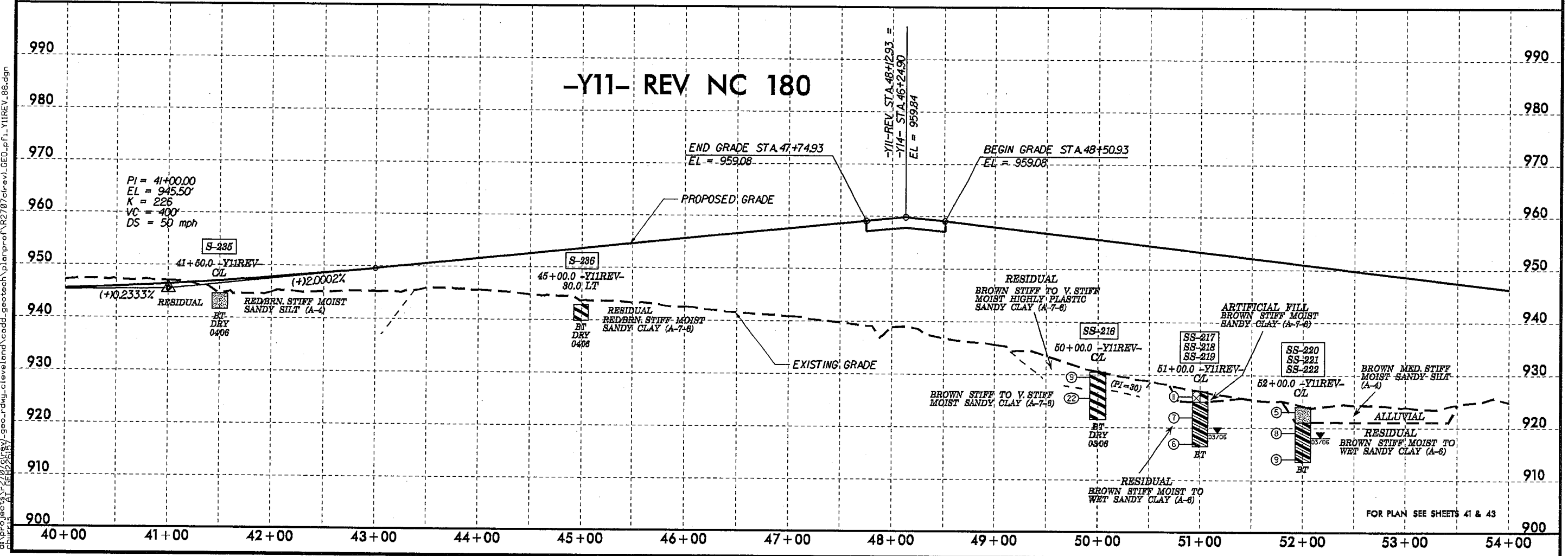
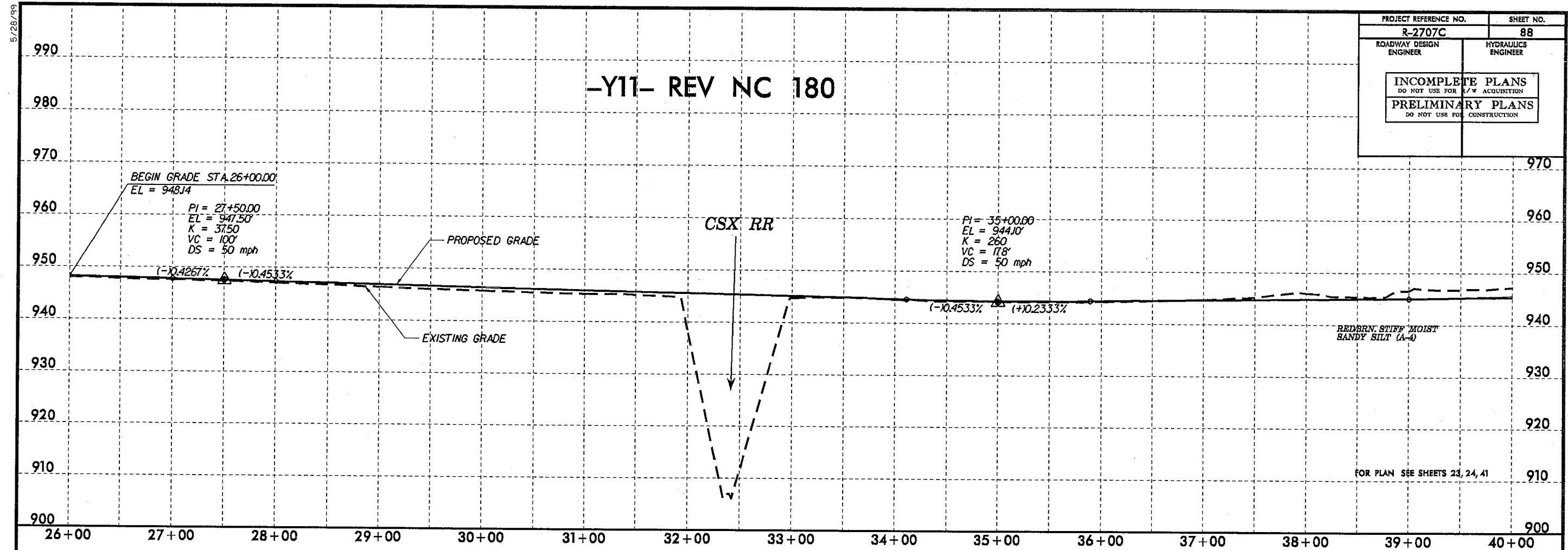
PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>87</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
	
 	



# -Y9- NC 18



PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>88</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION <b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

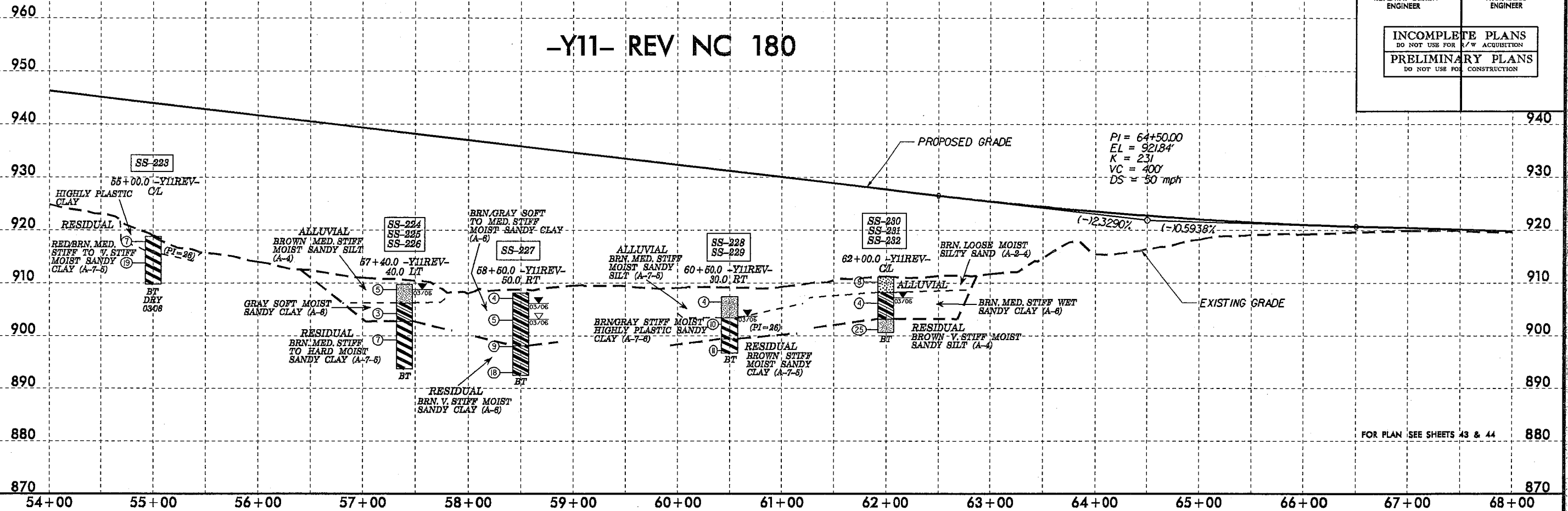


5/28/99  
 27-MAY-2008 10:25  
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PROJECT REFERENCE NO.	SHEET NO.
R-2707C	89
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS	
DO NOT USE FOR A/W ACQUISITION	
PRELIMINARY PLANS	
DO NOT USE FOR CONSTRUCTION	

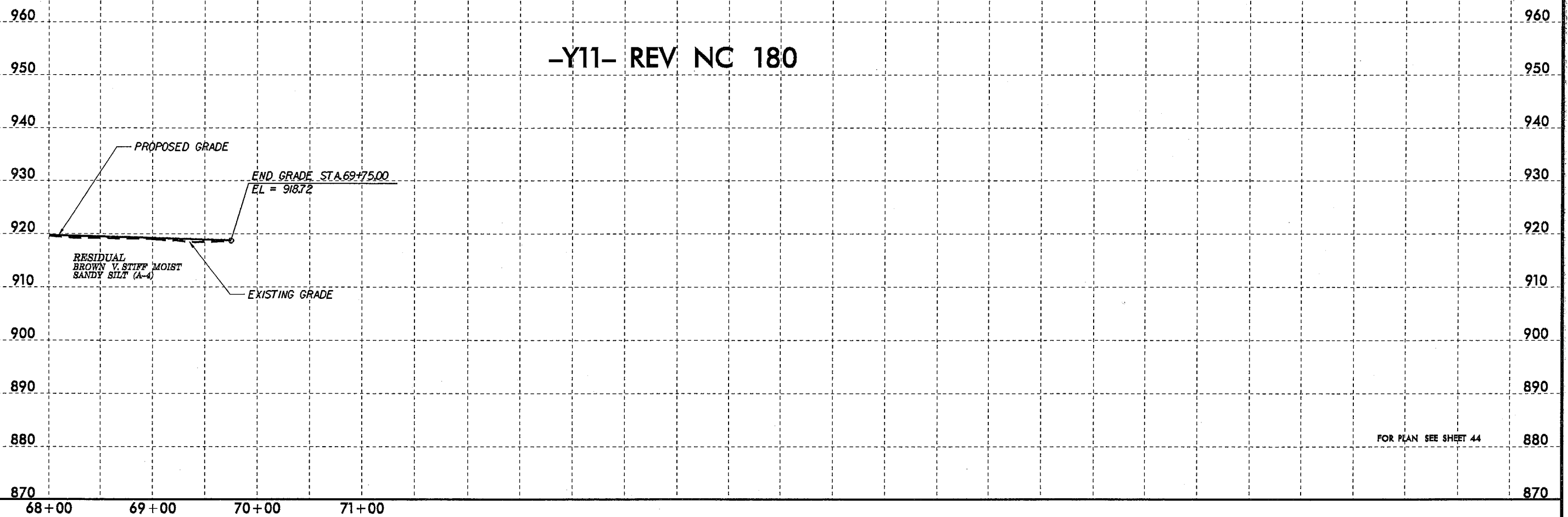
5/28/99

# -Y11- REV NC 180



FOR PLAN SEE SHEETS 43 & 44

# -Y11- REV NC 180

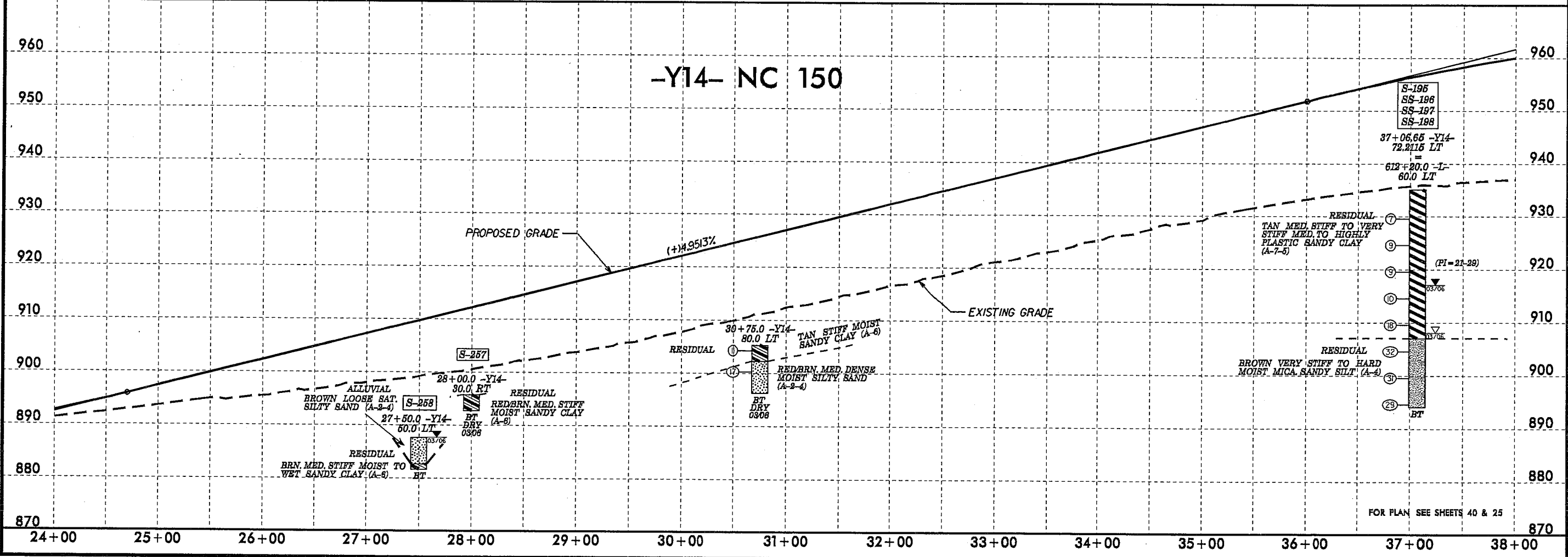
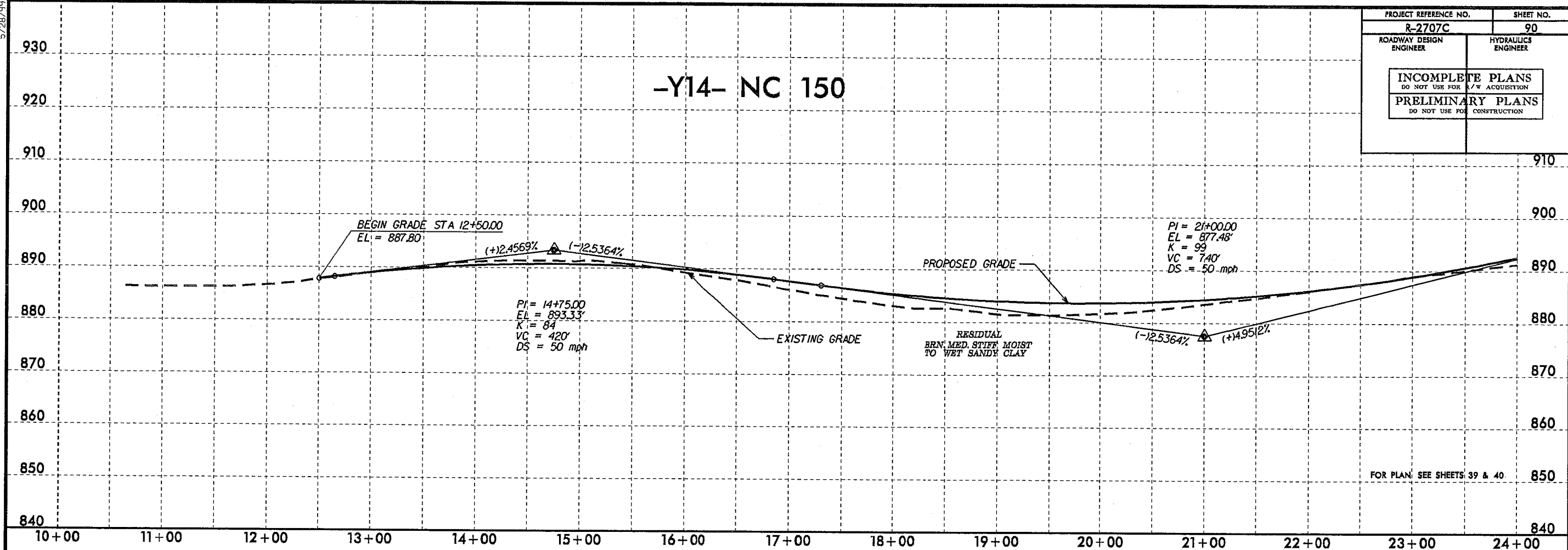


FOR PLAN SEE SHEET 44

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5/28/99

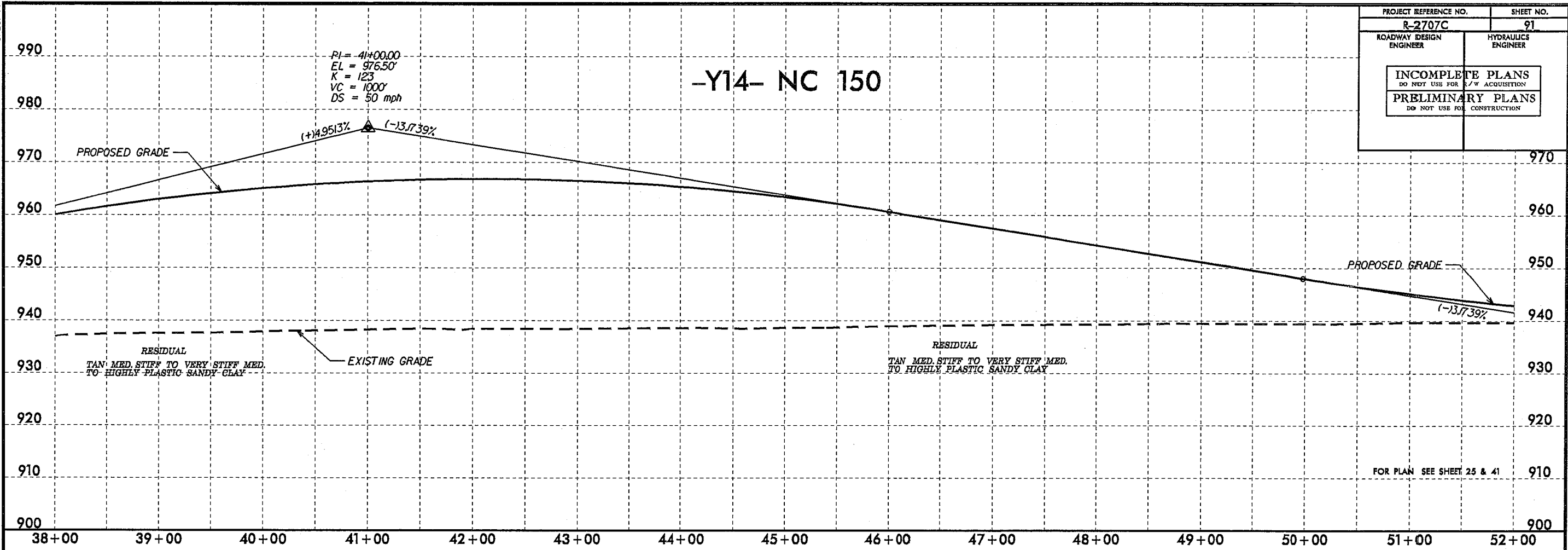
PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>90</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	



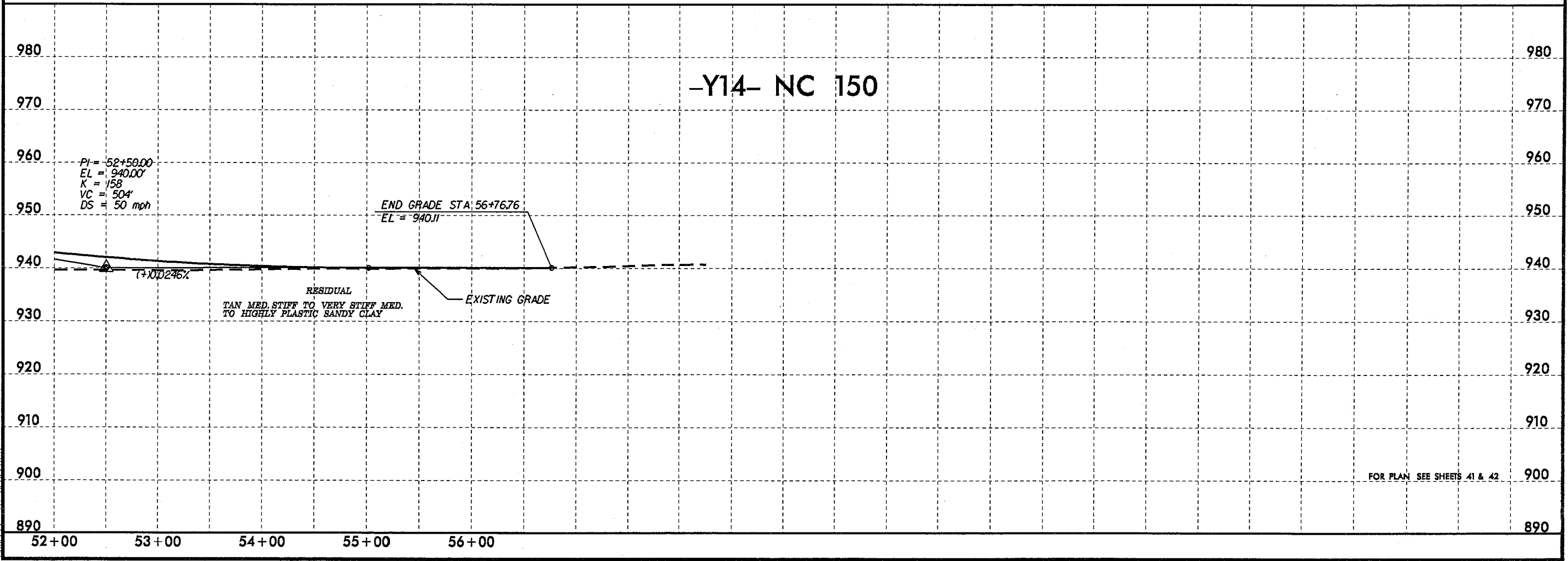
28-MAY-2008 15:07  
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PROJECT REFERENCE NO. R-2707C	SHEET NO. 91
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

5/28/99



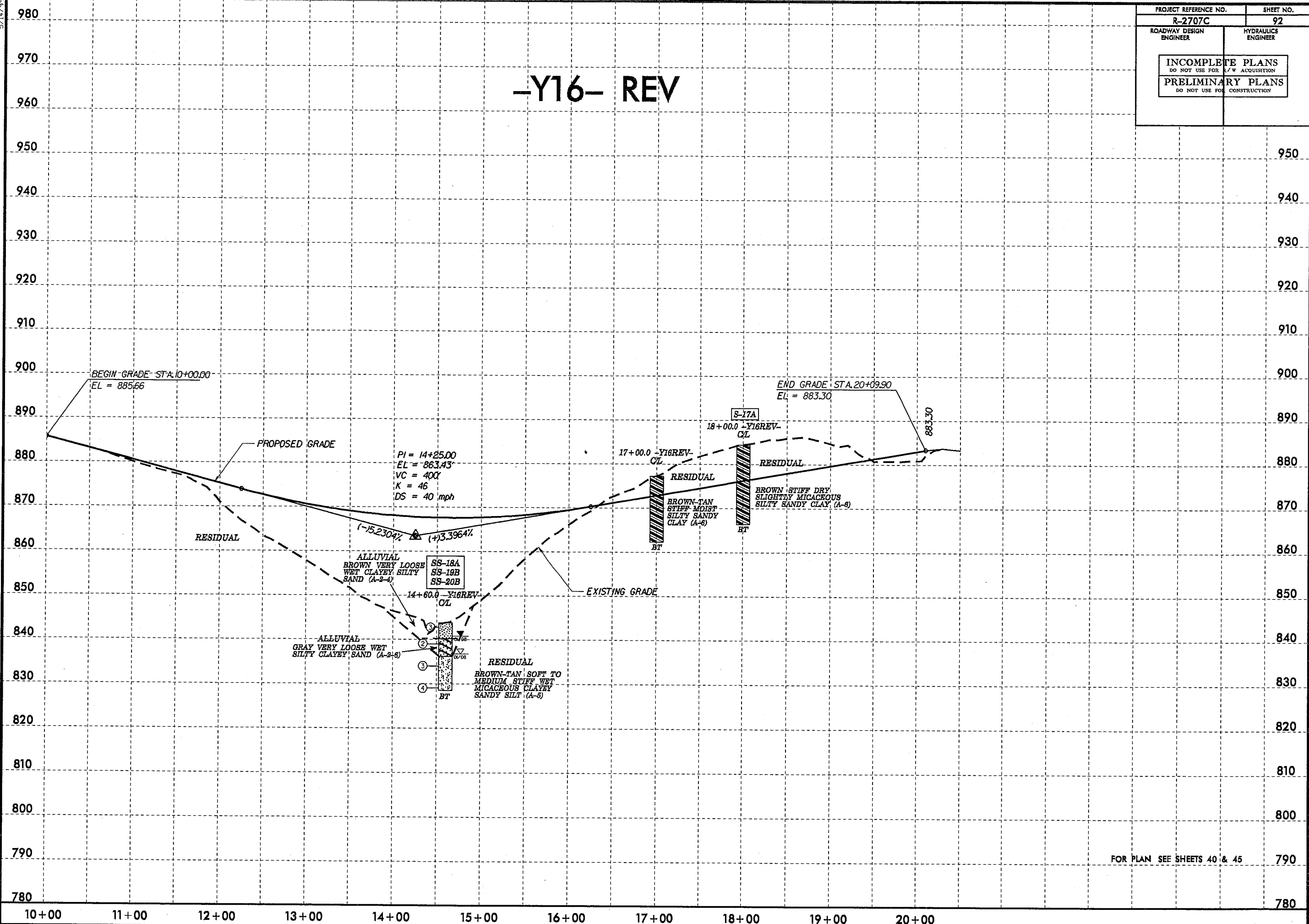
22-MAY-2008 14:49  
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5/14/99  
 23-MAY-2008 11:44  
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PROJECT REFERENCE NO. <b>R-2707C</b>	SHEET NO. <b>92</b>
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR ACQUISITION	
<b>PRELIMINARY PLANS</b> DO NOT USE FOR CONSTRUCTION	

# -Y16- REV



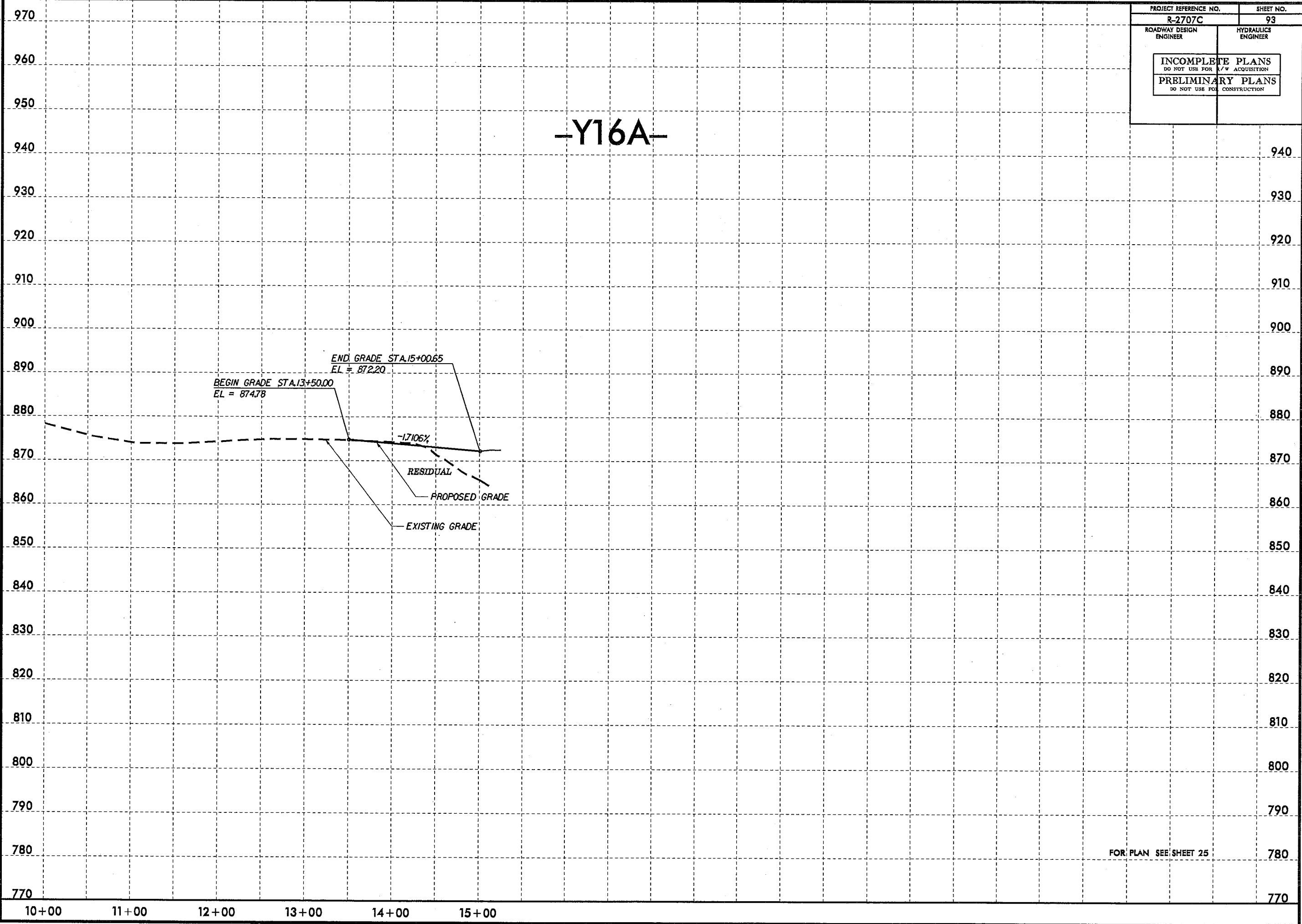
FOR PLAN SEE SHEETS 40 & 45

5/14/99

22-MAY-2008 15:06  
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PROJECT REFERENCE NO. R-2707C	SHEET NO. 93
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

# -Y16A-



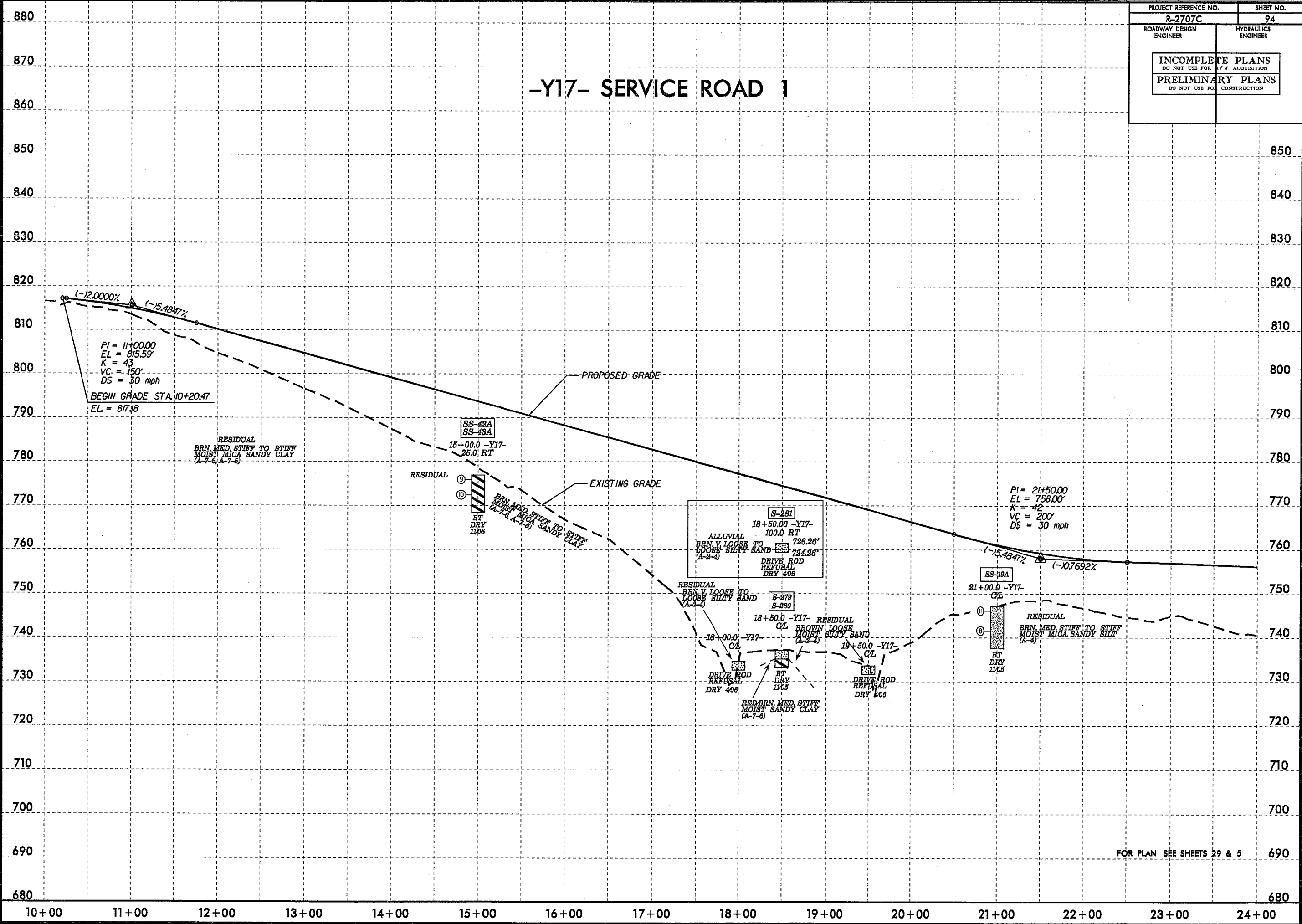
FOR PLAN SEE SHEET 25

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770

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PROJECT REFERENCE NO. R-2707C	SHEET NO. 94
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION	
PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

# -Y17- SERVICE ROAD 1

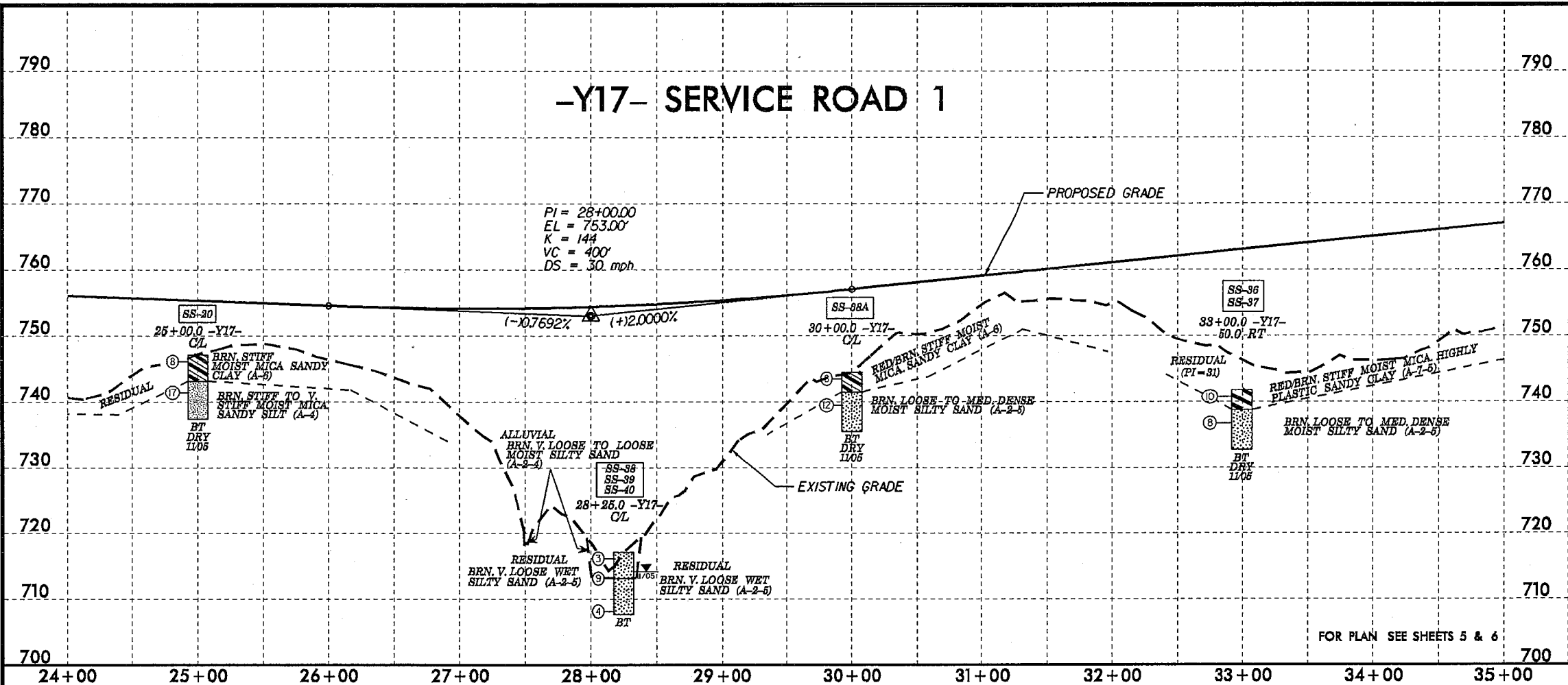


FOR PLAN SEE SHEETS 29 & 5

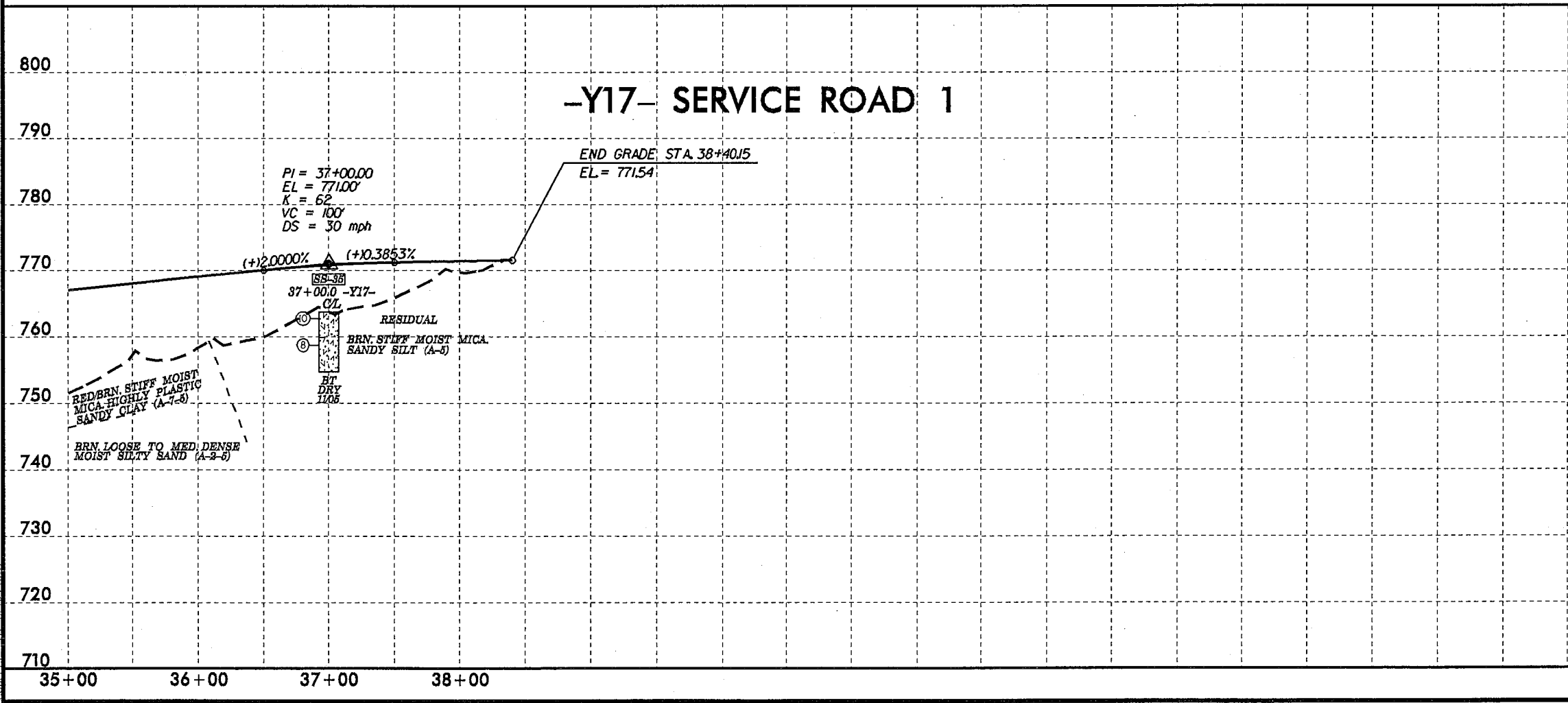
22-MAY-2008 15:40  
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 5/14/99



5/28/99

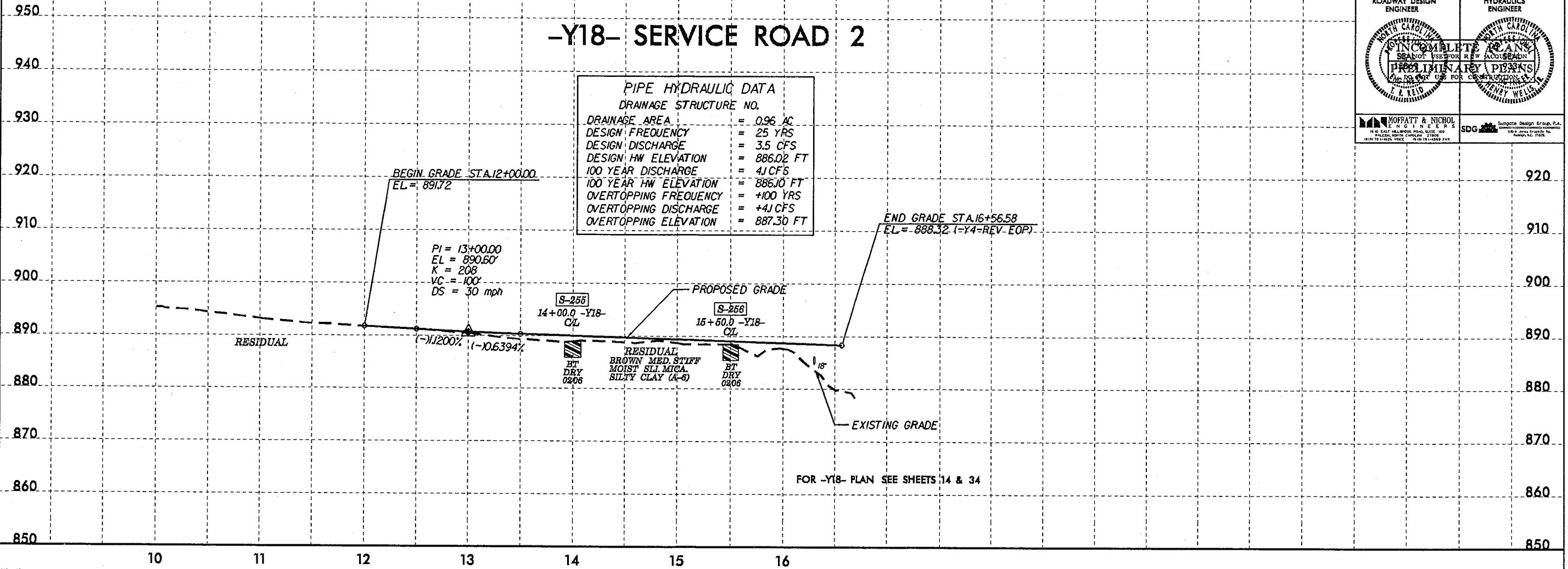


22-MAY-2008 15:20  
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# -Y18- SERVICE ROAD 2

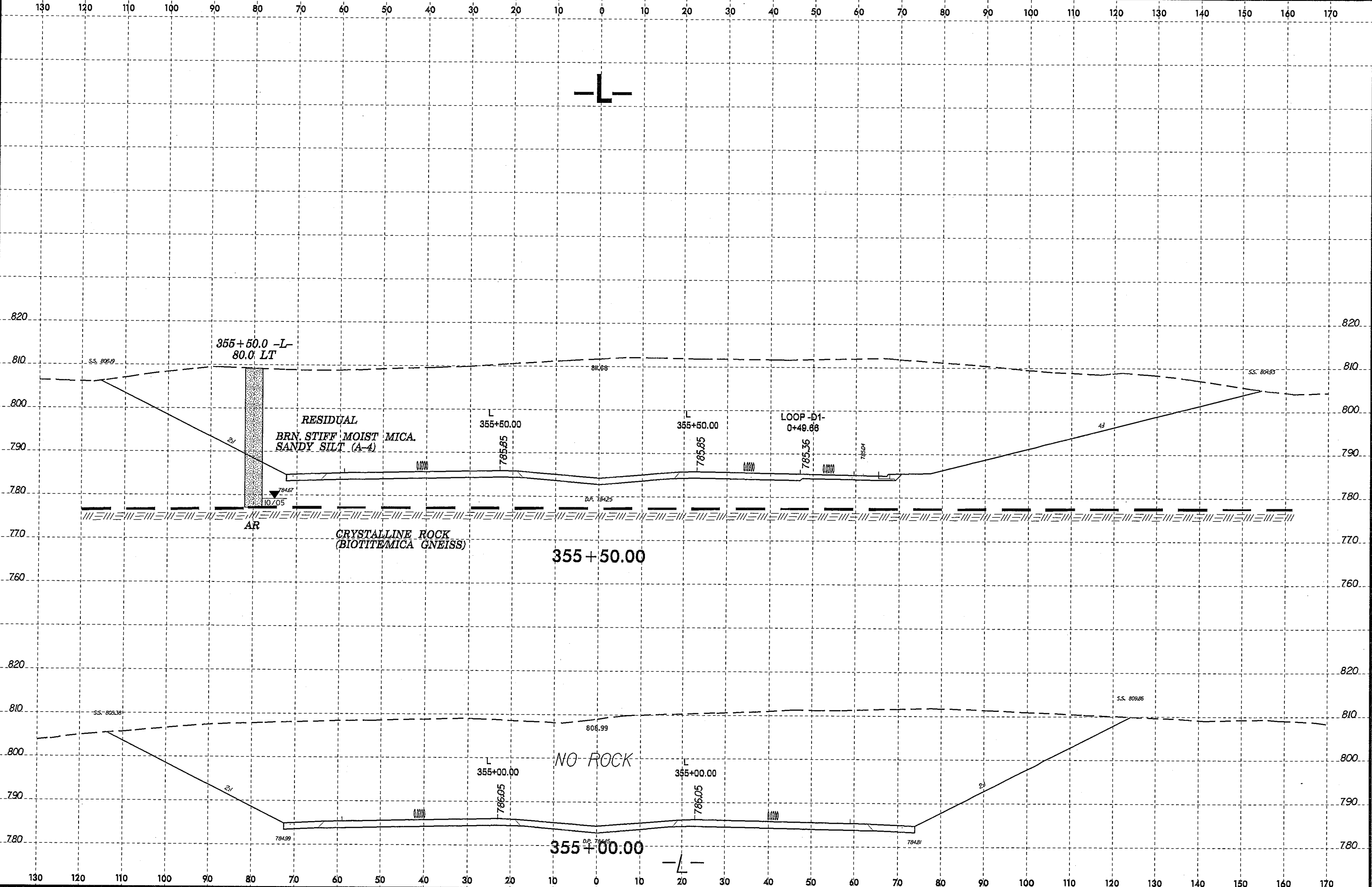
PIPE HYDRAULIC DATA	
DRAINAGE STRUCTURE NO.	
DRAINAGE AREA	= 0.96 AC
DESIGN FREQUENCY	= 25 YRS
DESIGN DISCHARGE	= 3.5 CFS
DESIGN HW ELEVATION	= 886.02 FT
100 YEAR DISCHARGE	= 4.1 CFS
100 YEAR HW ELEVATION	= 886.10 FT
OVERTOPPING FREQUENCY	= +100 YRS
OVERTOPPING DISCHARGE	= +4.1 CFS
OVERTOPPING ELEVATION	= 887.30 FT



10      11      12      13      14      15      16

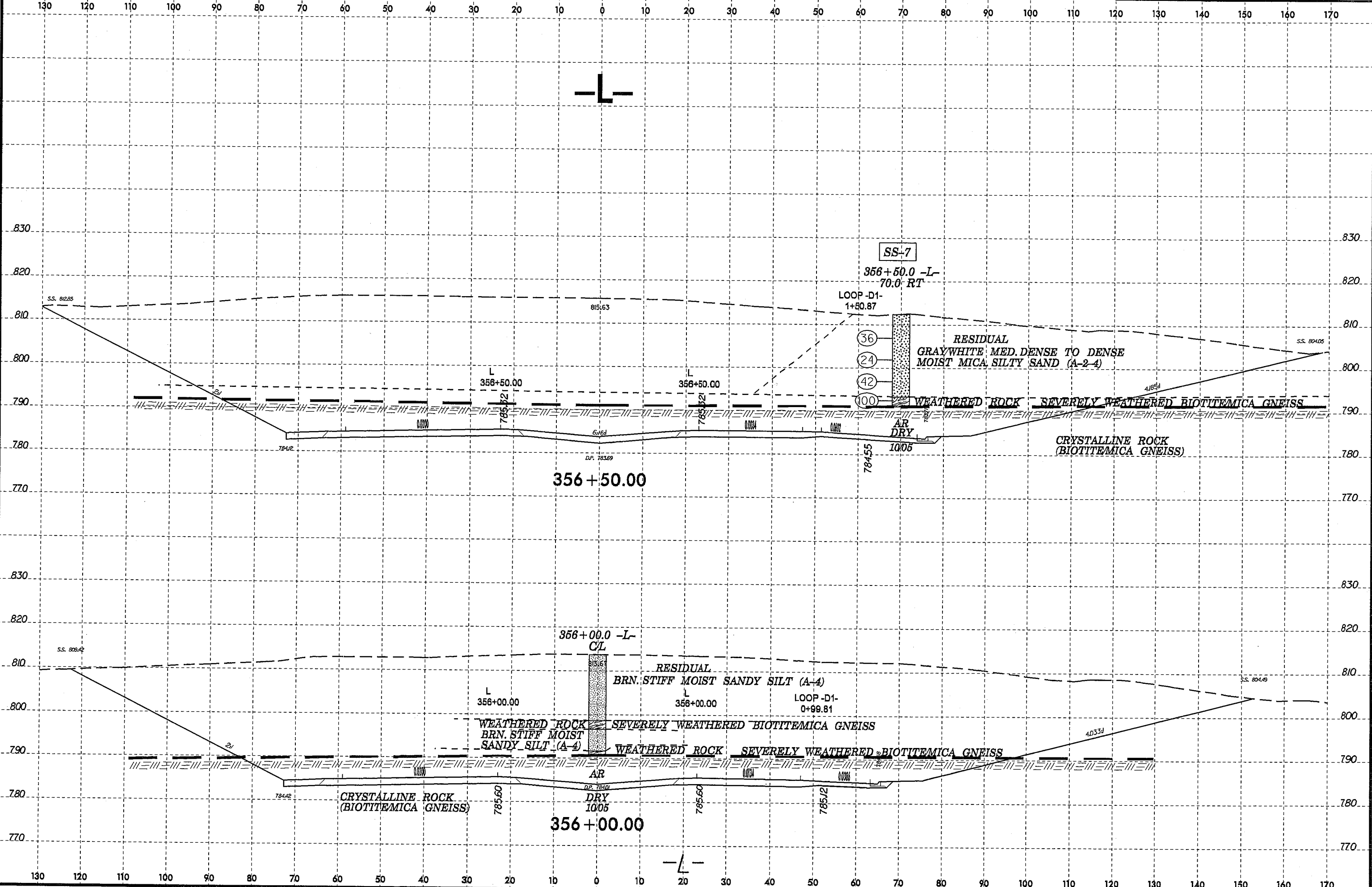
8/23/99

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	77



14-MAY-2008 13:10  
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 AT 08:25:15

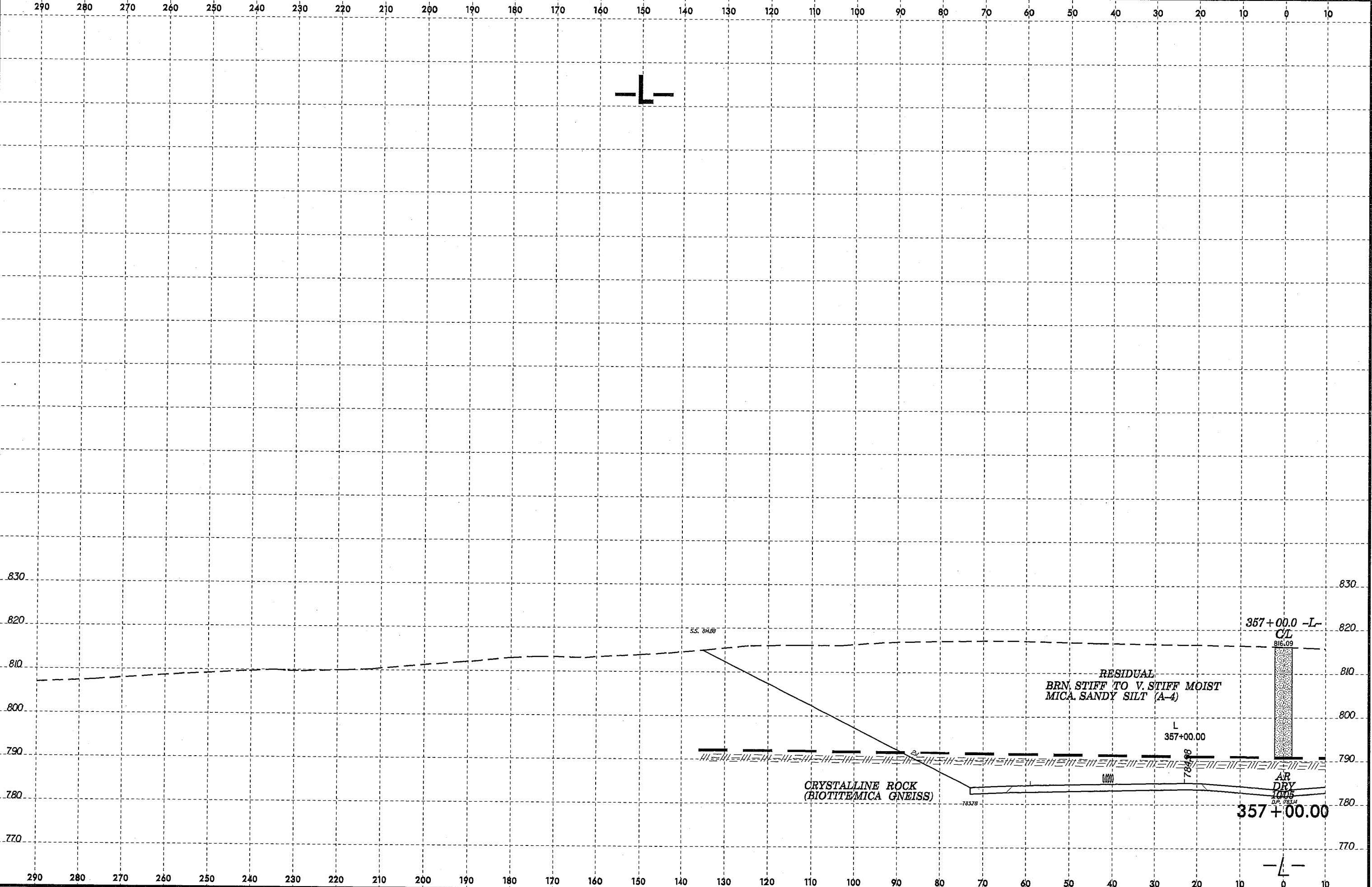
8/23/99



I5-MAY-2008 14:16  
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 cburris AT 06/26/07

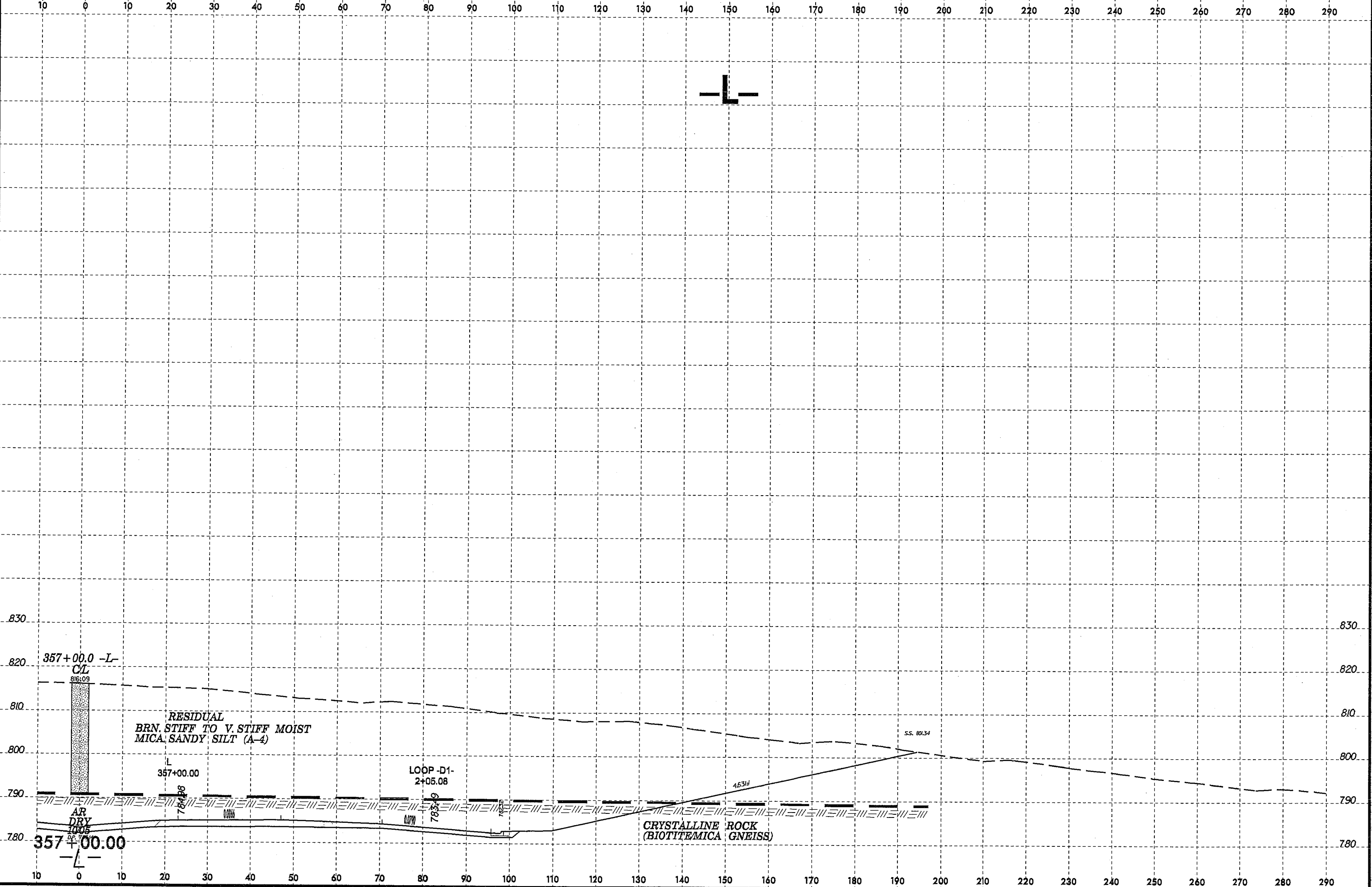
8/23/99

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	79



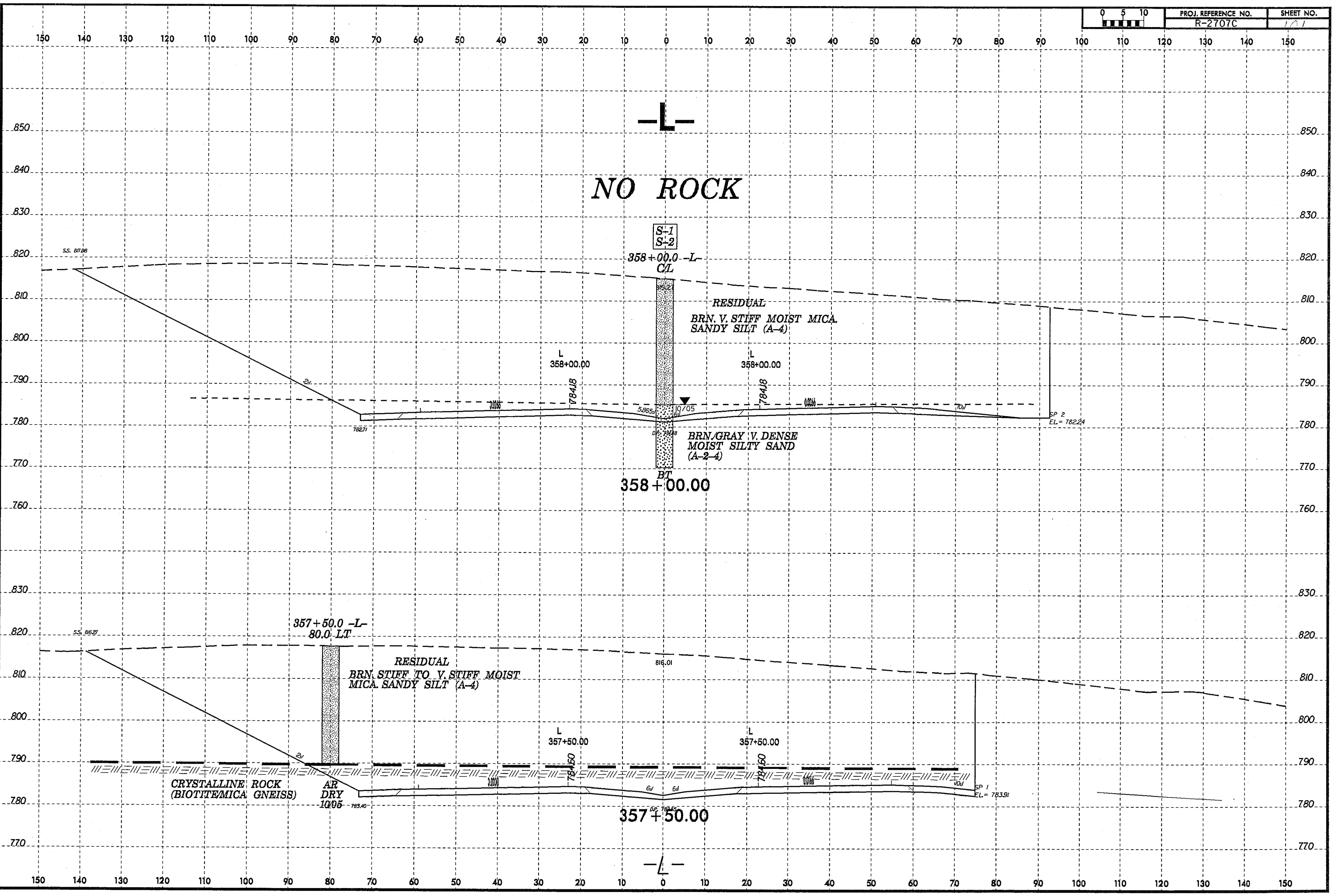
15-MAY-2008 14:18  
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 geotech - AT GEN25137

8/23/99



15-MAY-2008 14:19  
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 sburris AT 05/22/2008

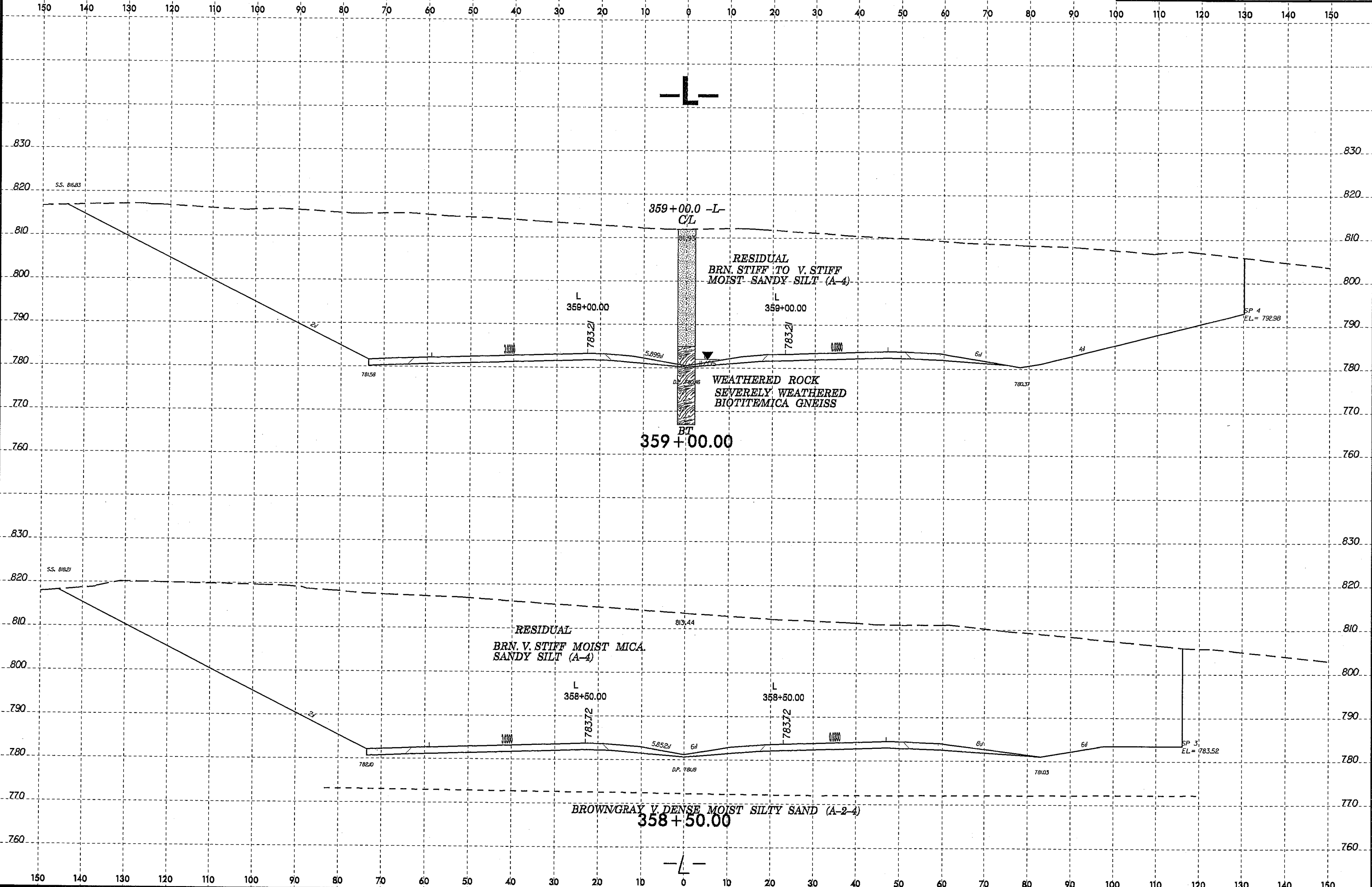
8/23/99  
28-MAY-2008 15:22  
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8/23/99



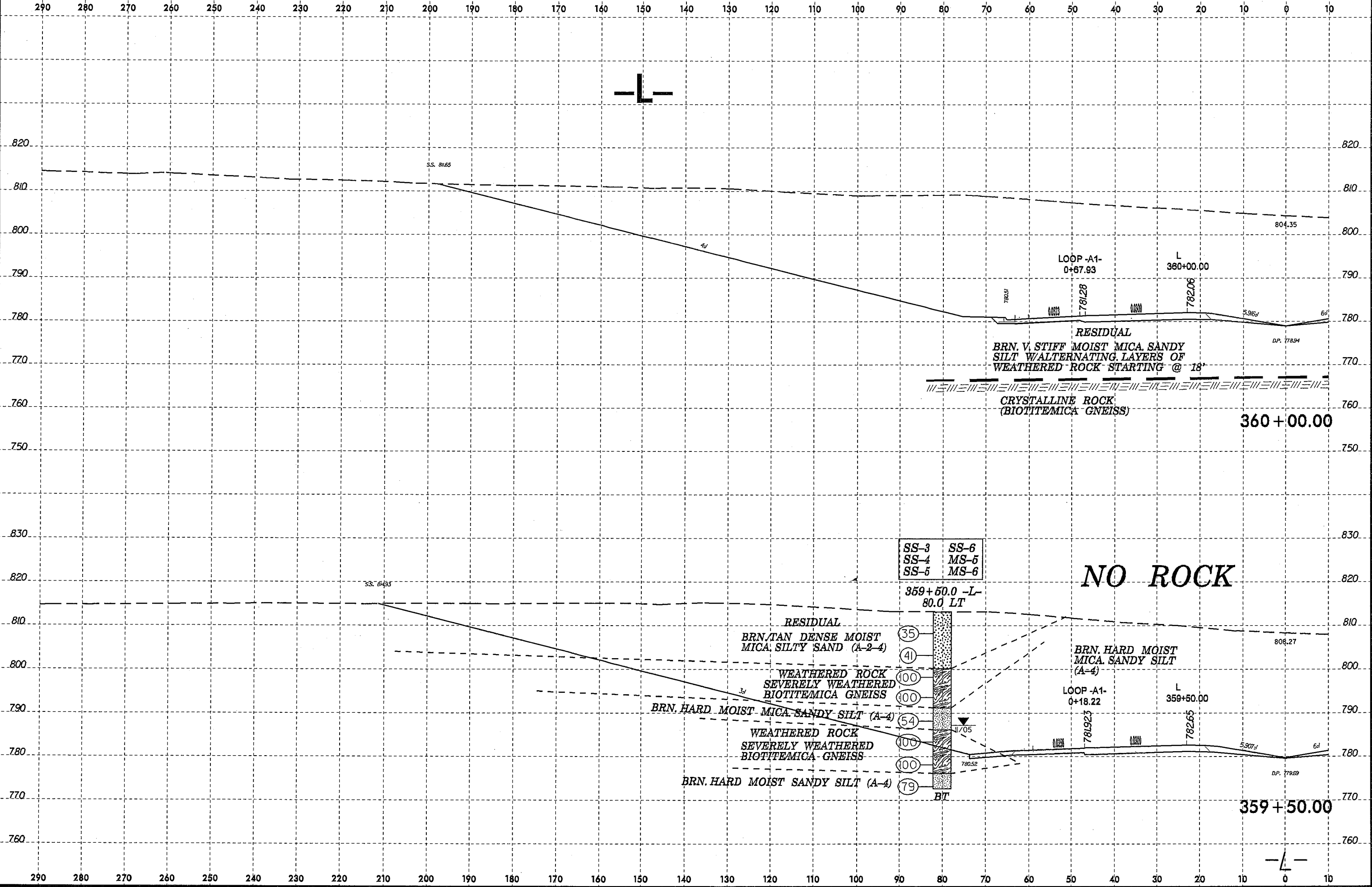
PROJ. REFERENCE NO.	SHEET NO.
R-2707C	102



14-MAY-2008 13:32  
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 gburris AT 06/26/07

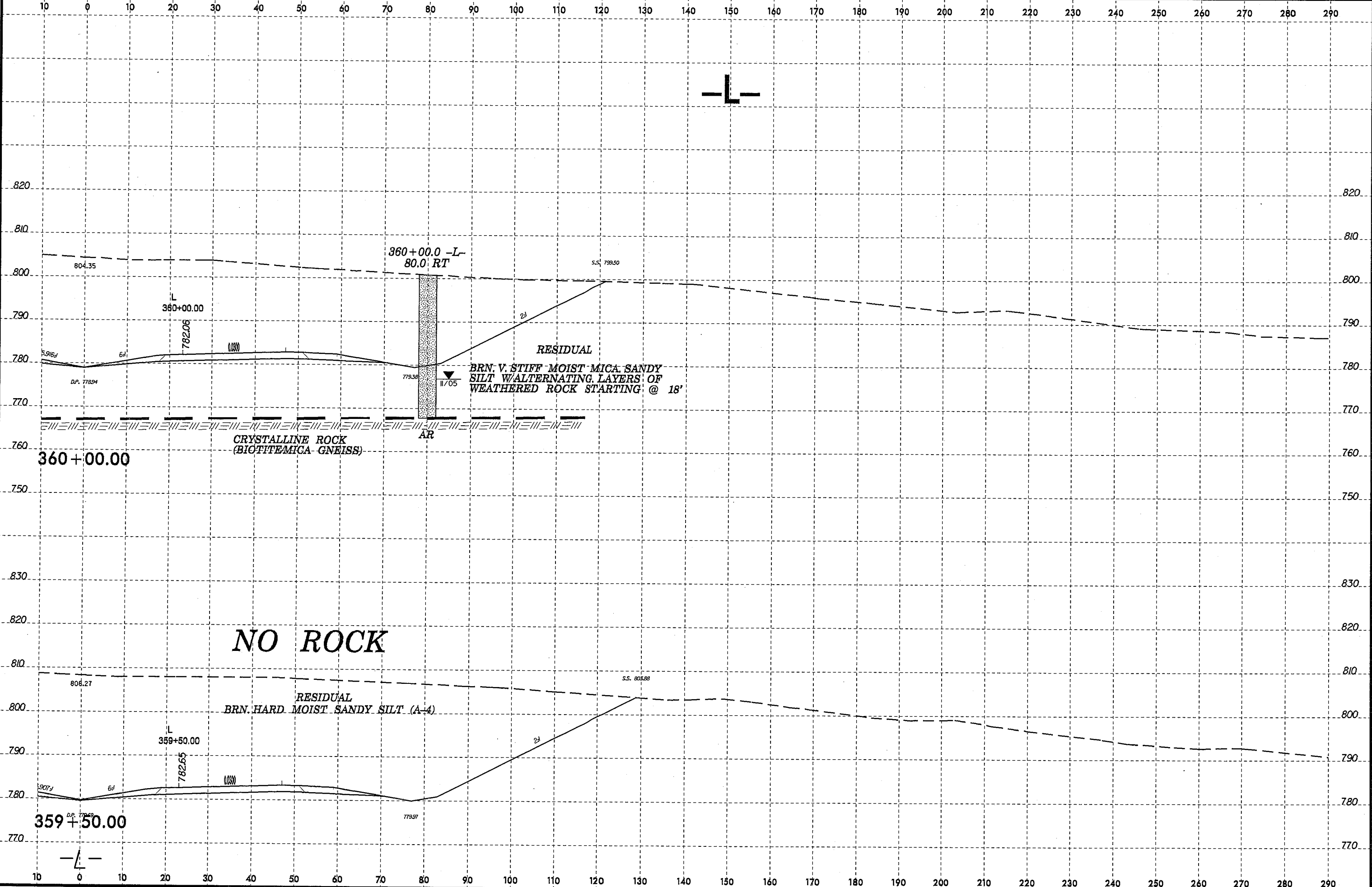


8/23/99



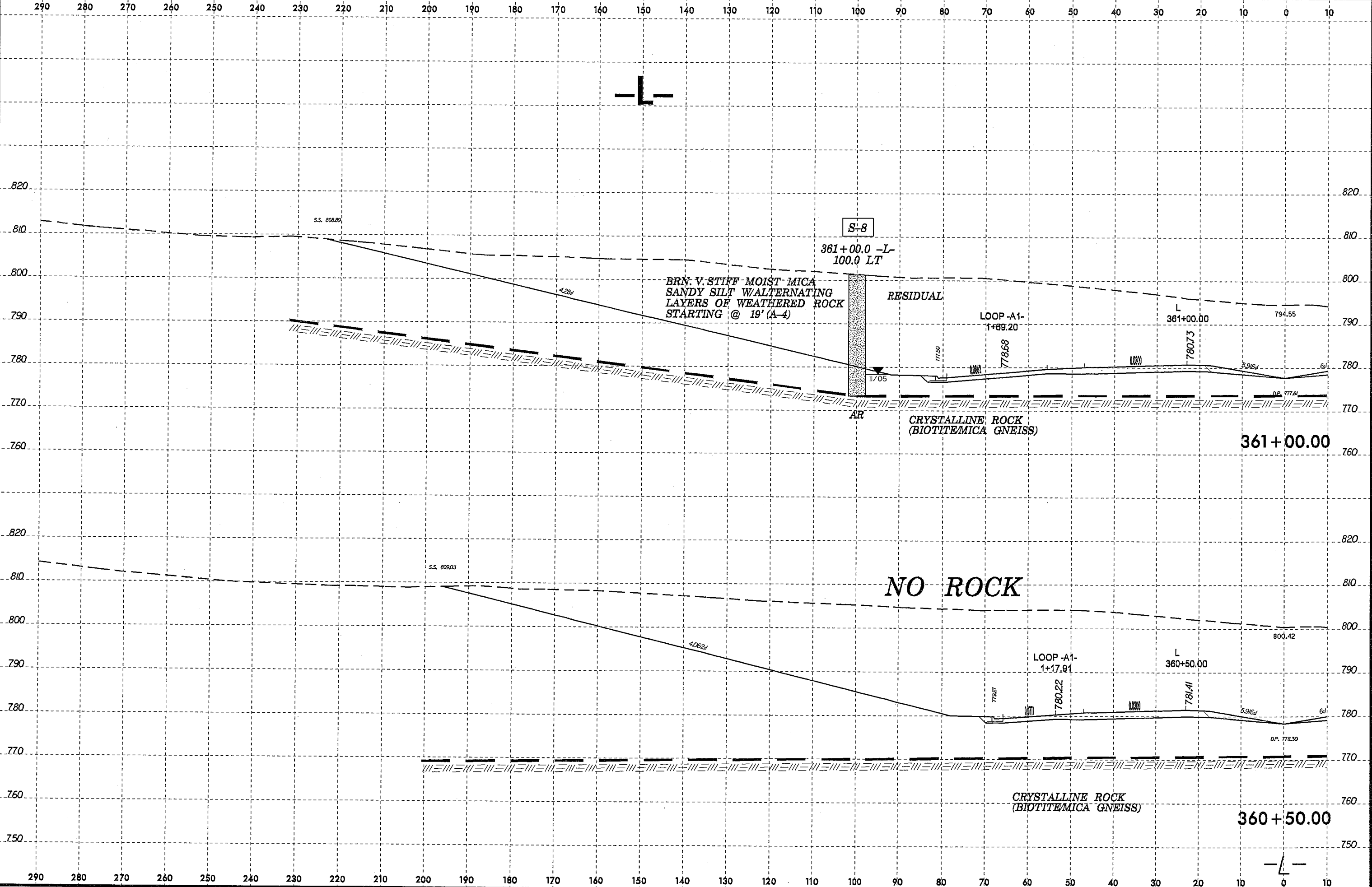
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 gburris AT 6E22615

8/23/99



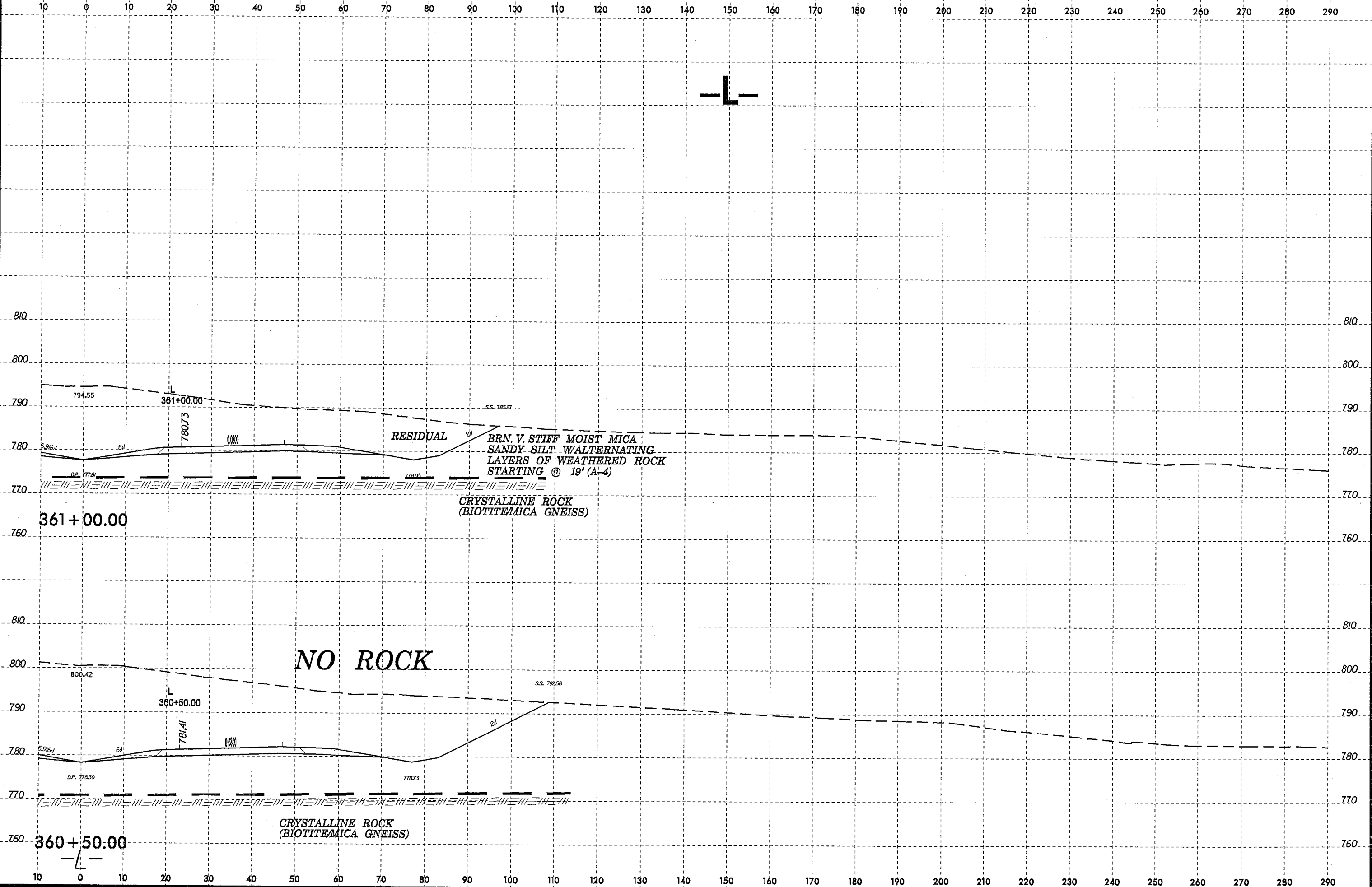
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gburris AT 06/22/07

8/23/99



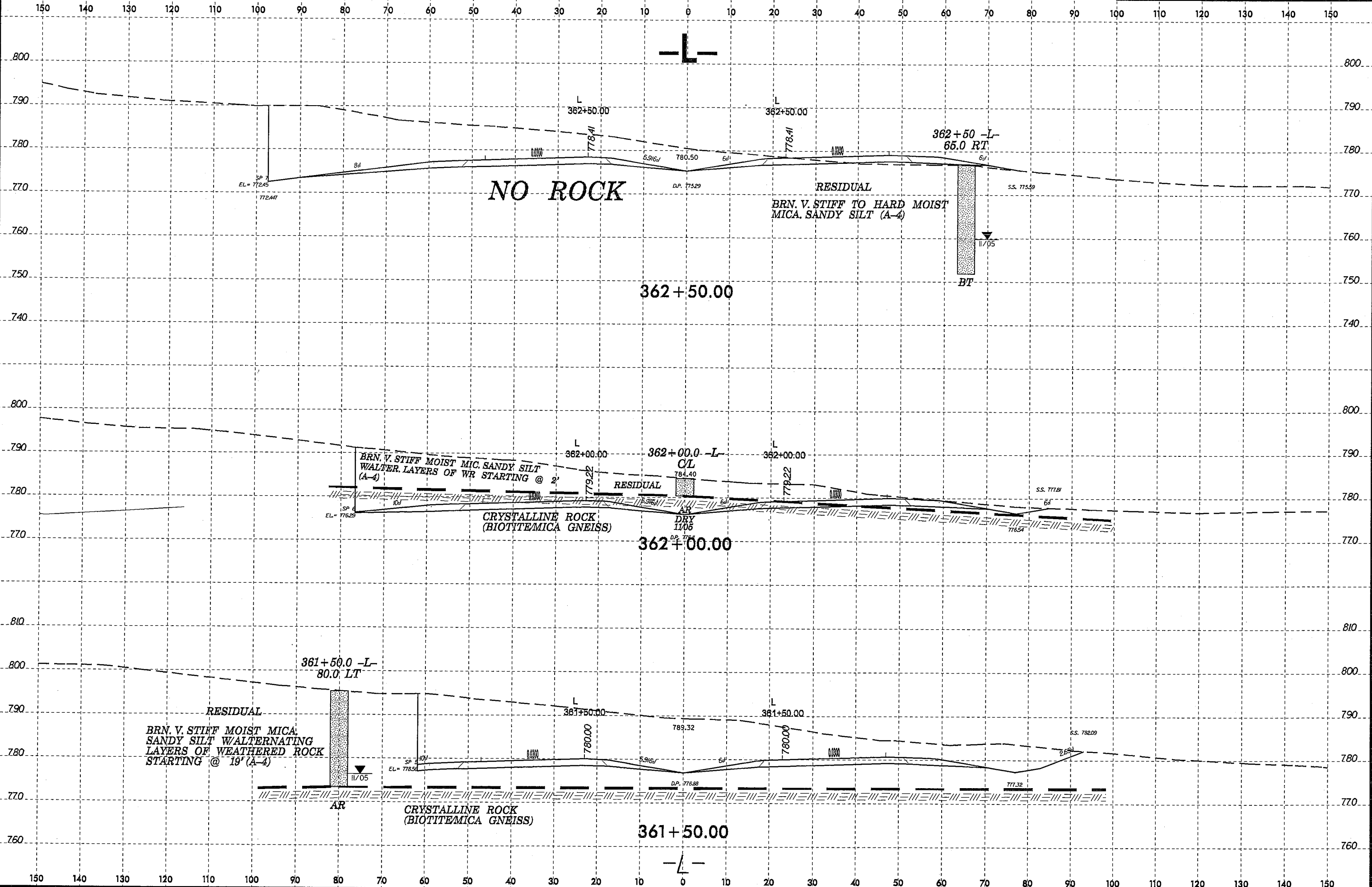
14-MAY-2008 13:34  
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 gburris AT DEN28137

8/23/99



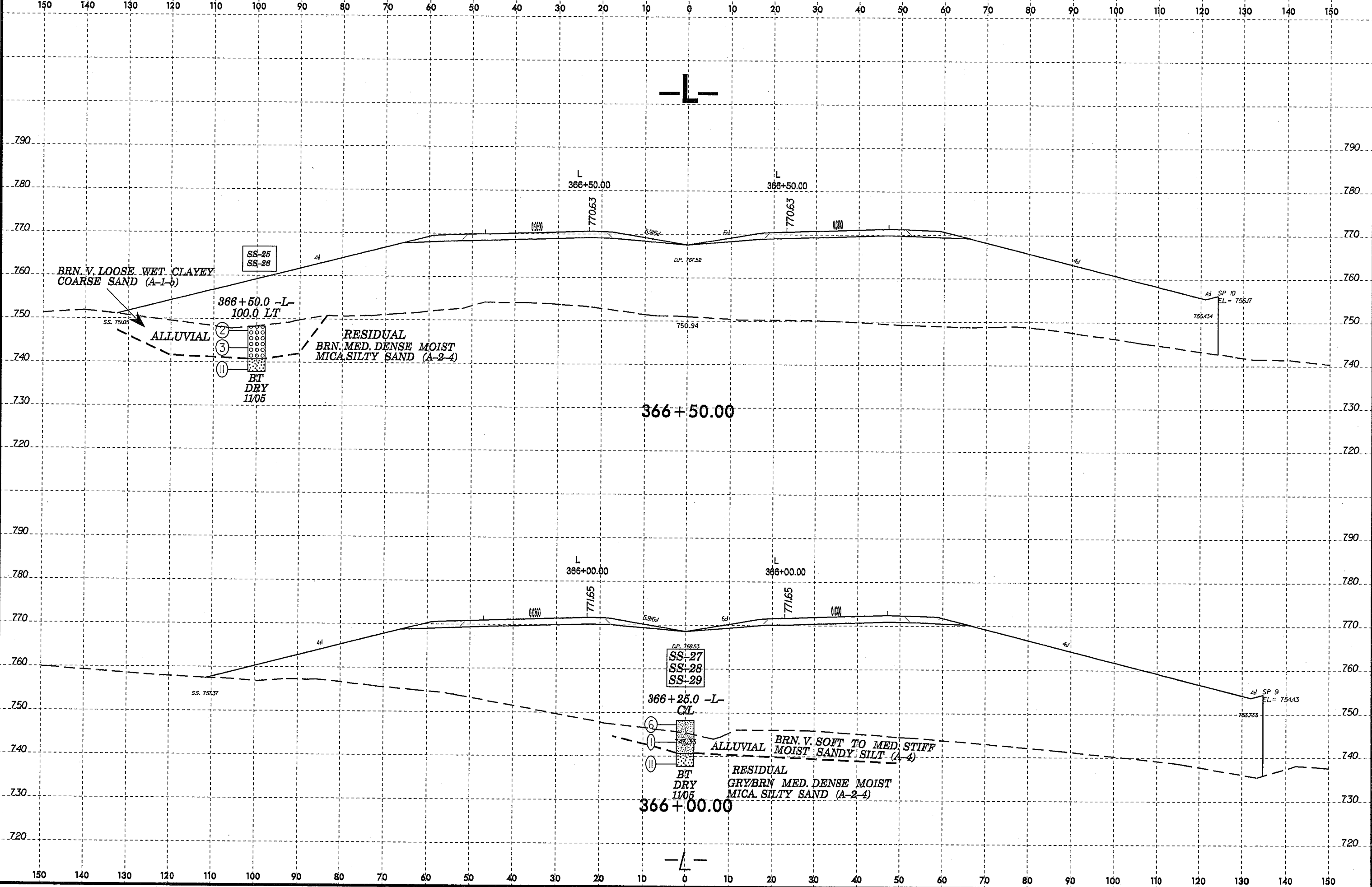
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 gburris AT GE226157

8/23/99



14-MAY-2008 13:37  
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 burnis AT 6E125615

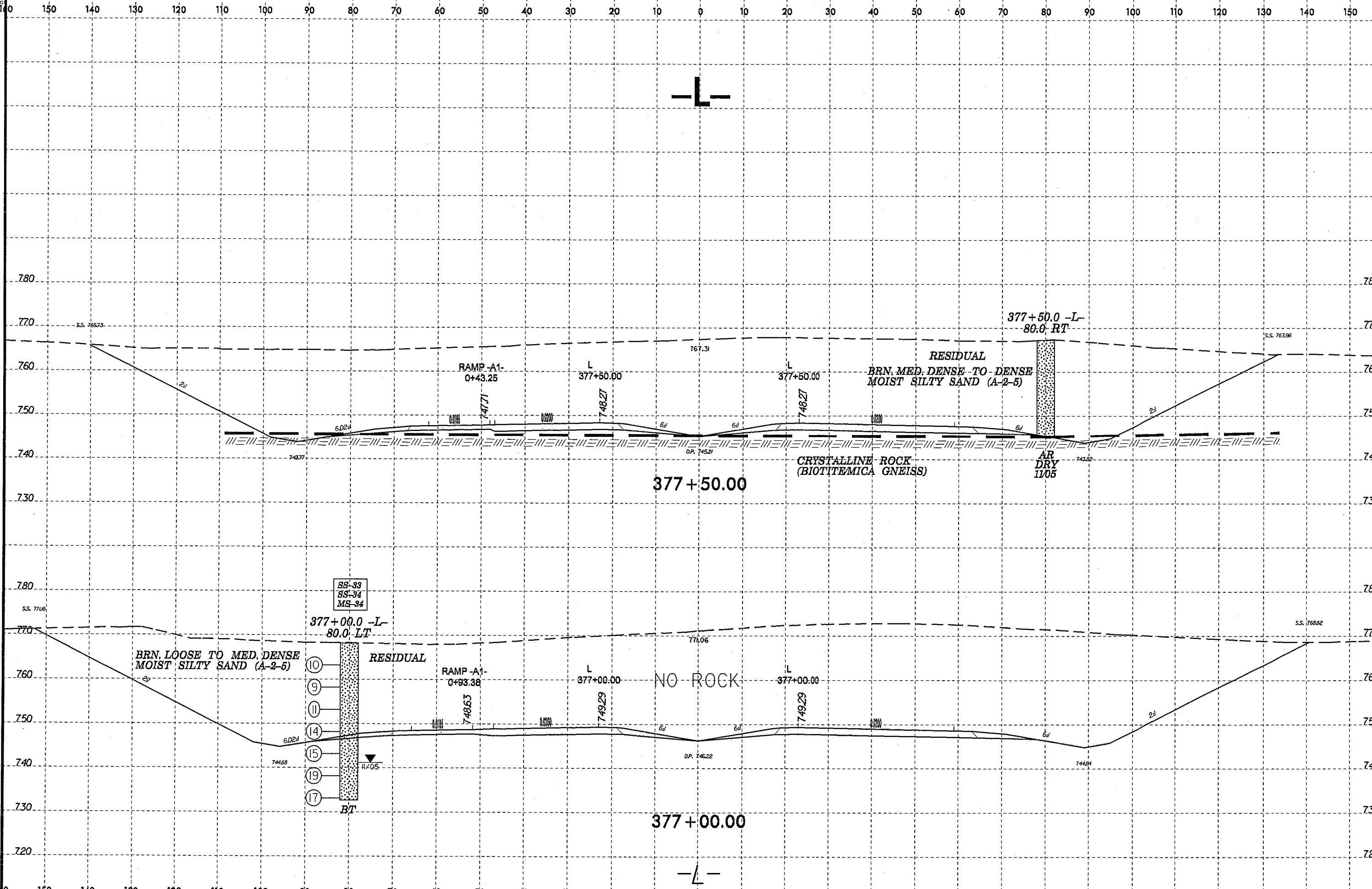
8/23/99



28-MAY-2008 15:35  
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 64226187  
 64226187



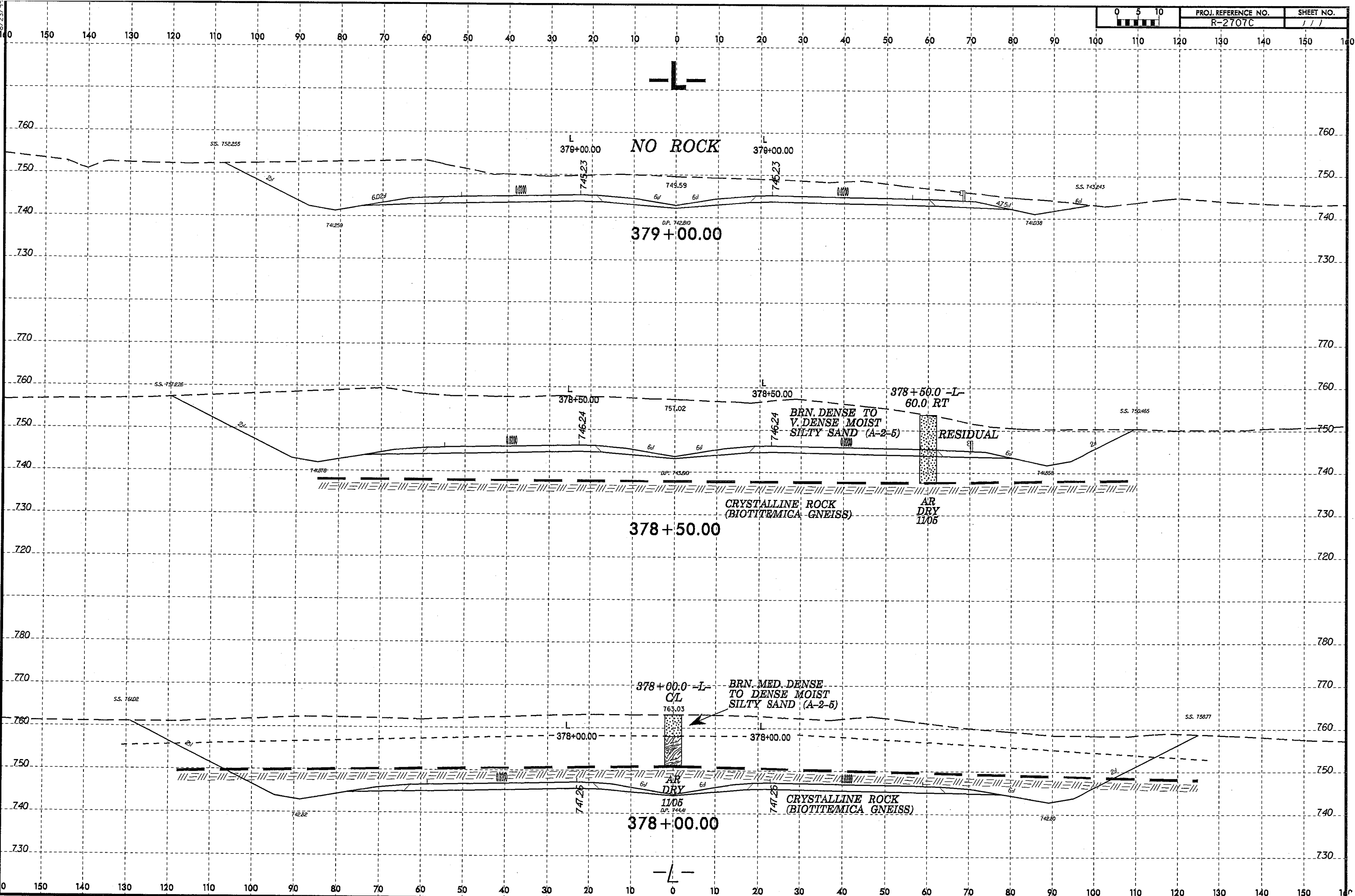
27-MAY-2008 12:38  
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Sheet 110



- SS-33
- SS-34
- MS-34
- BT



14-MAY-2008 13:40  
c:\p\proj\2707\geo\rd\w-c\leveland\cadd\geotech\2707\c\rev\geo\_xsl.L.dgn



NO ROCK

BRN. DENSE TO V. DENSE MOIST SILTY SAND (A-2-5)

RESIDUAL

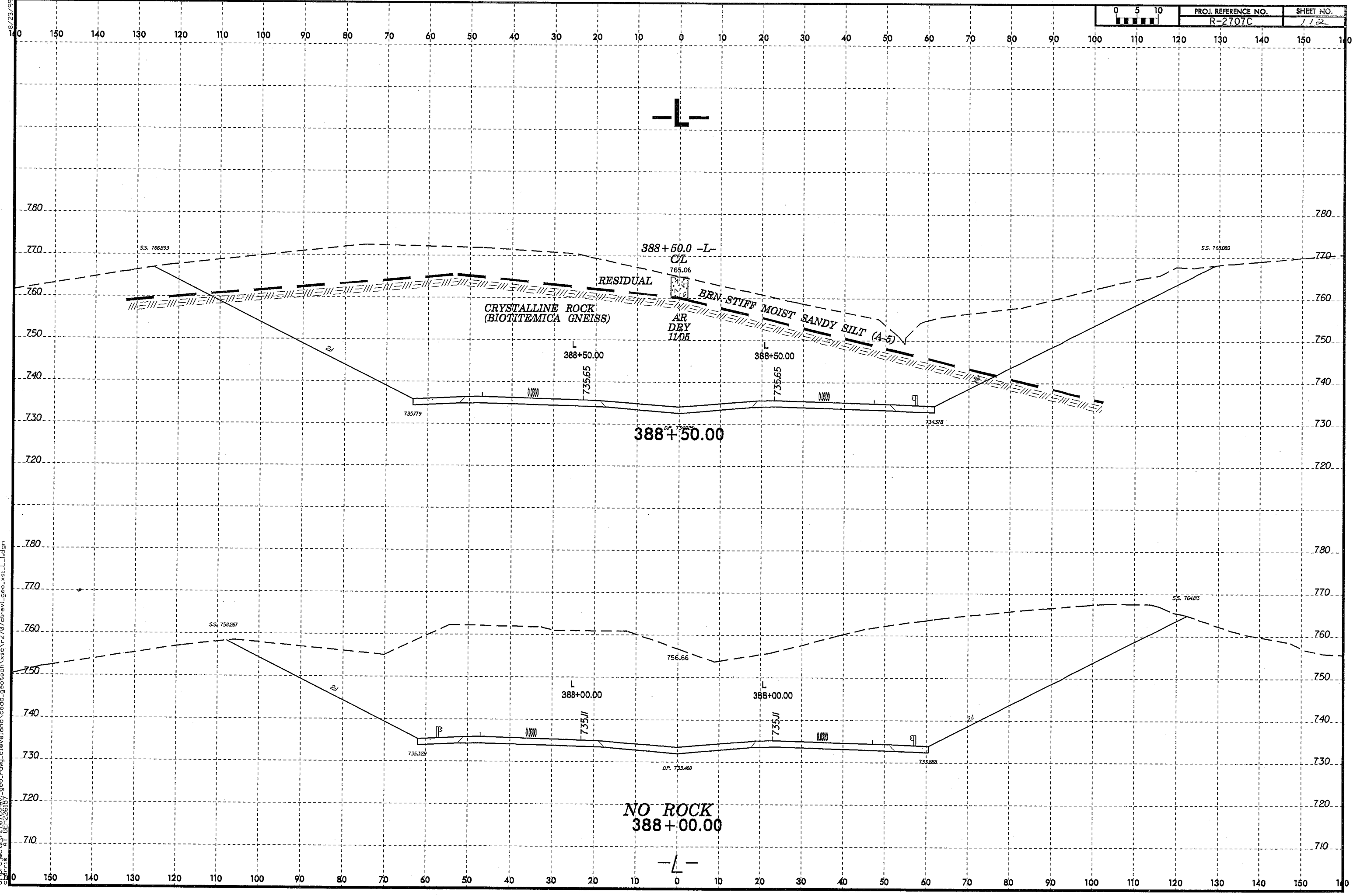
CRYSTALLINE ROCK (BIOTITEMICA GNEISS)

AR DRY 1105

BRN. MED. DENSE TO DENSE MOIST SILTY SAND (A-2-5)

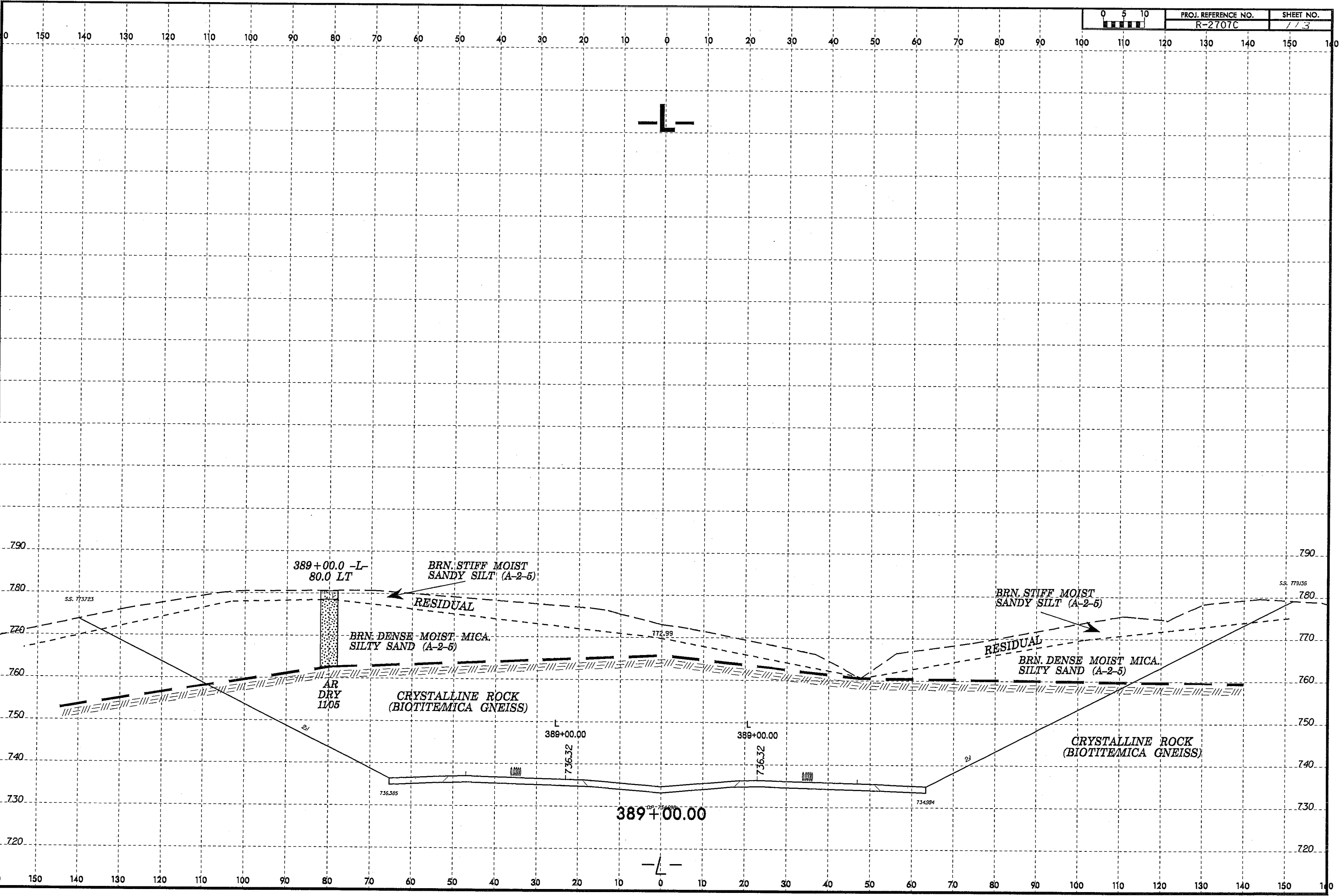
CRYSTALLINE ROCK (BIOTITEMICA GNEISS)

378+00.00



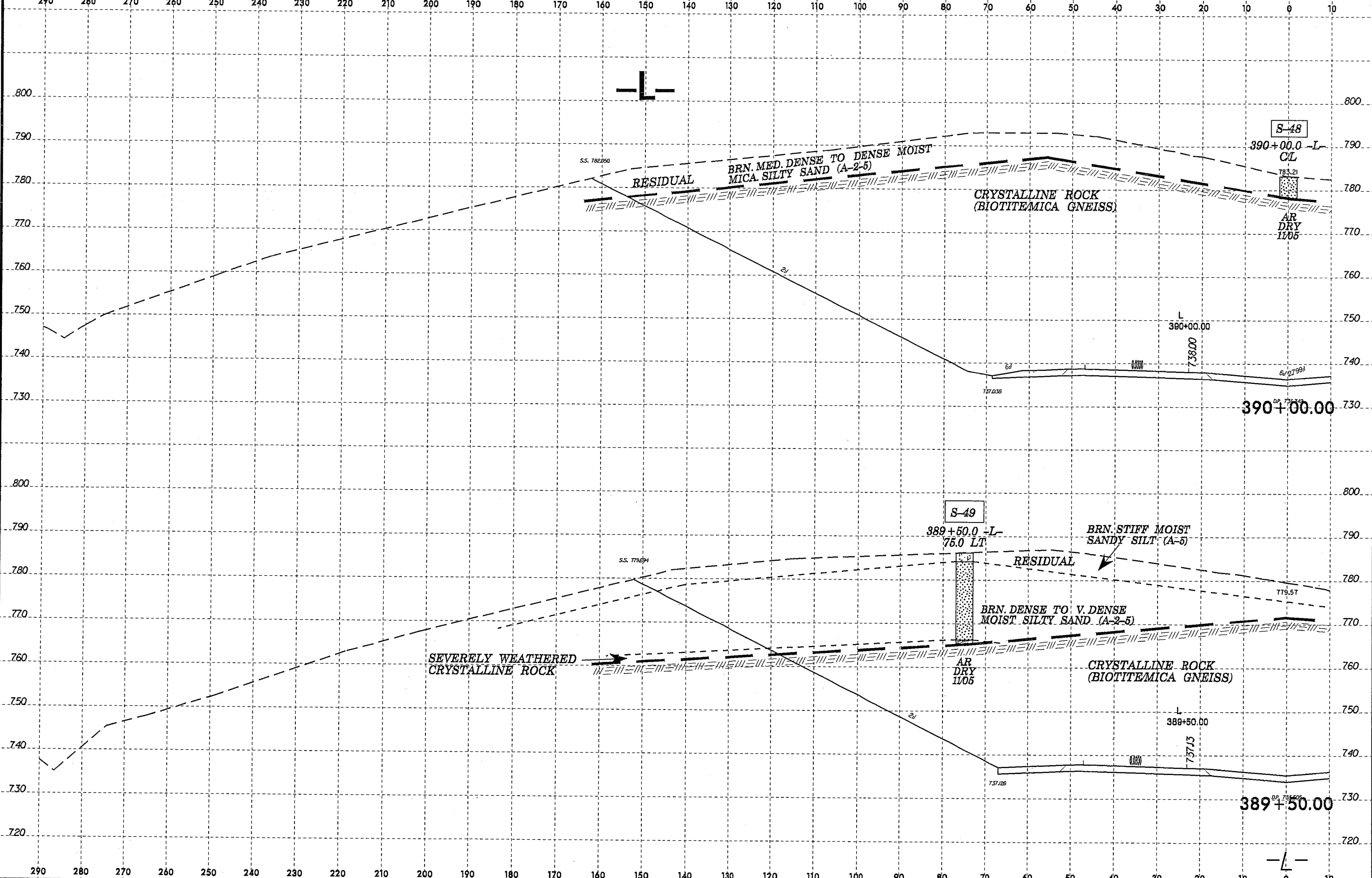
14-MAY-2008 13:41  
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14-MAY-2008 13:42  
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AT: 6826157

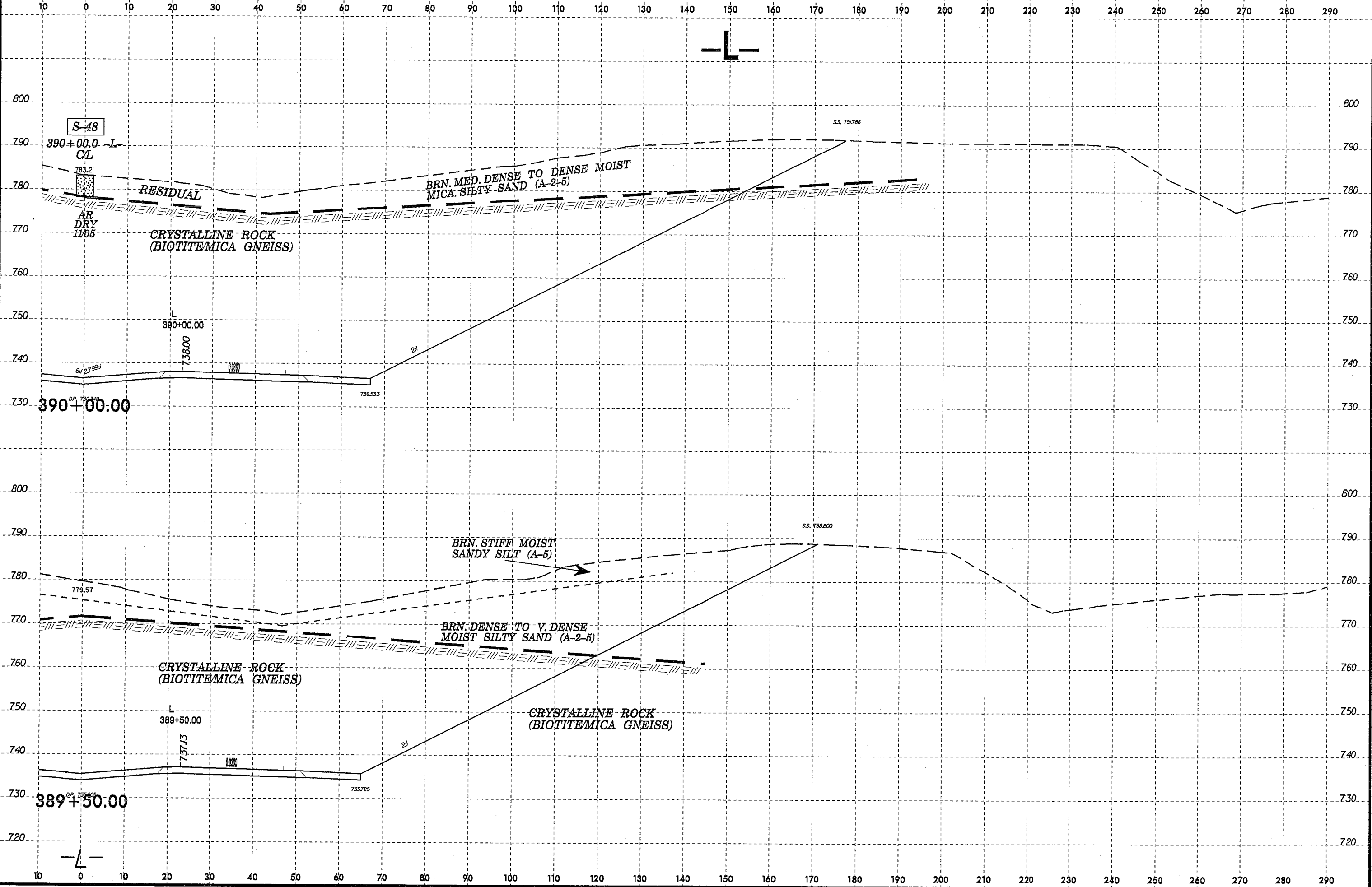


29-MAY-2008 07:52  
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	11

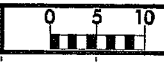


8/23/99

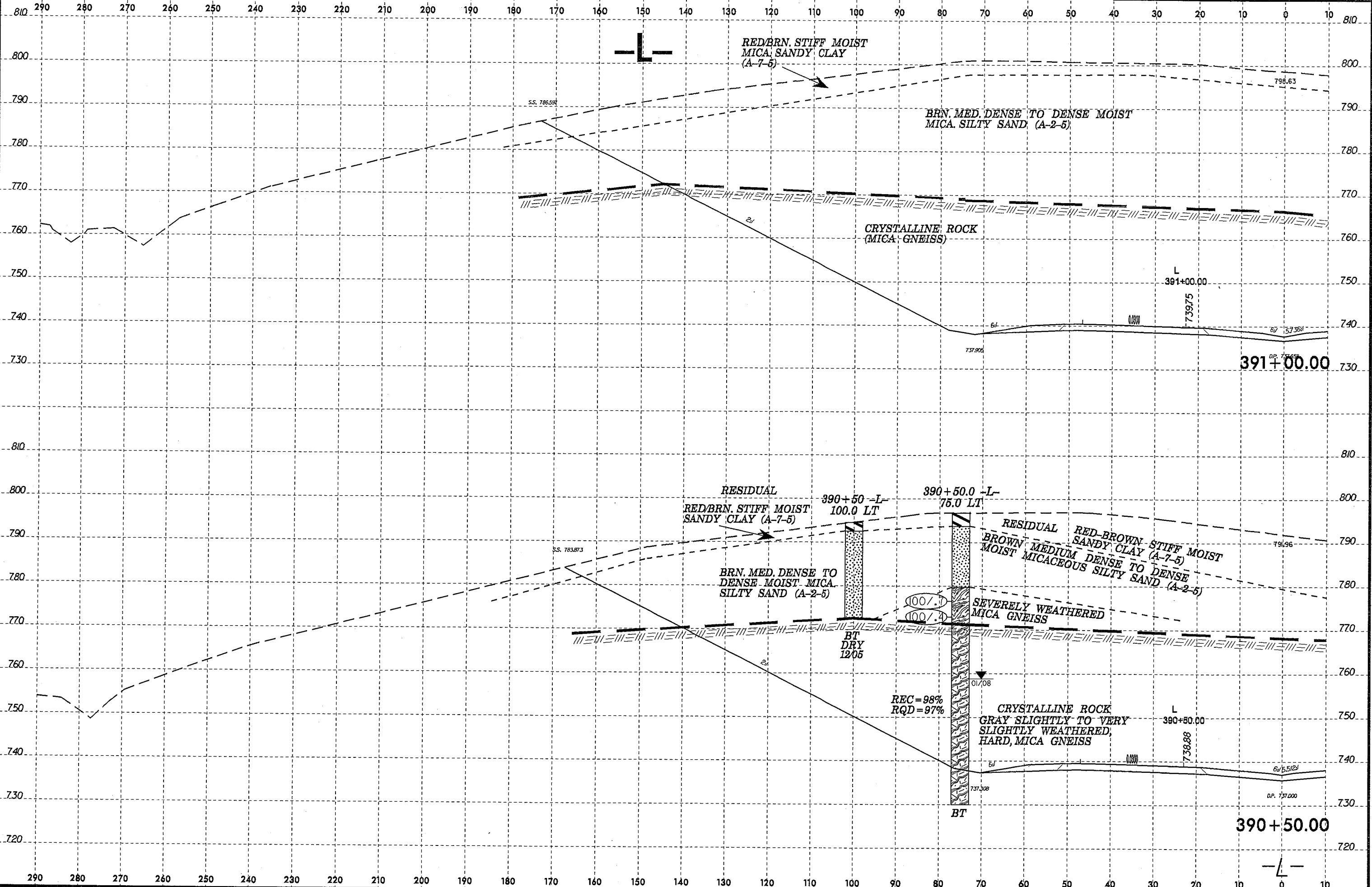


29-MAY-2008 07:55  
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 cburns AT 6/22/07

8/23/98

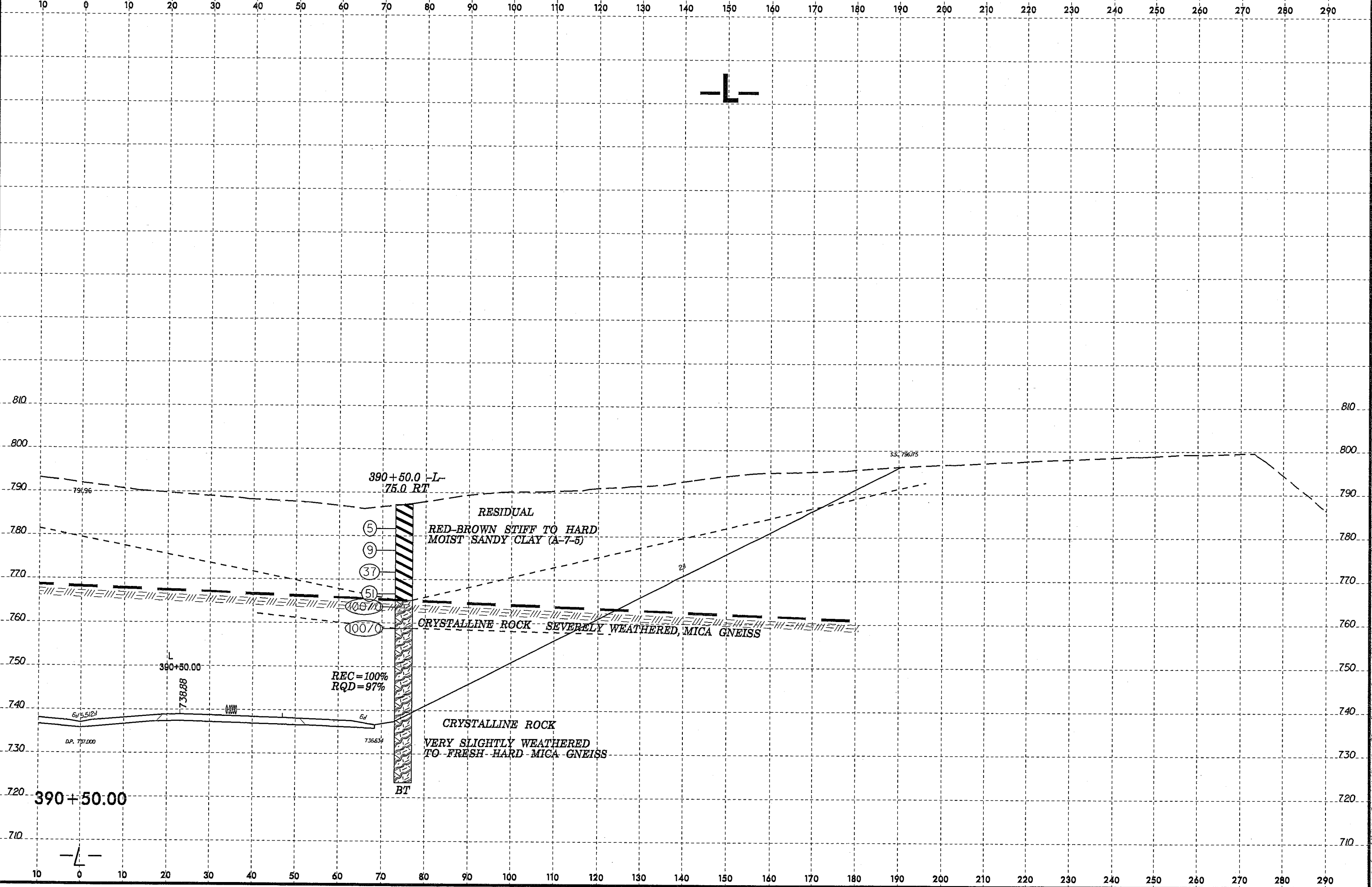


PROJ. REFERENCE NO.	SHEET NO.
R-2707C	116

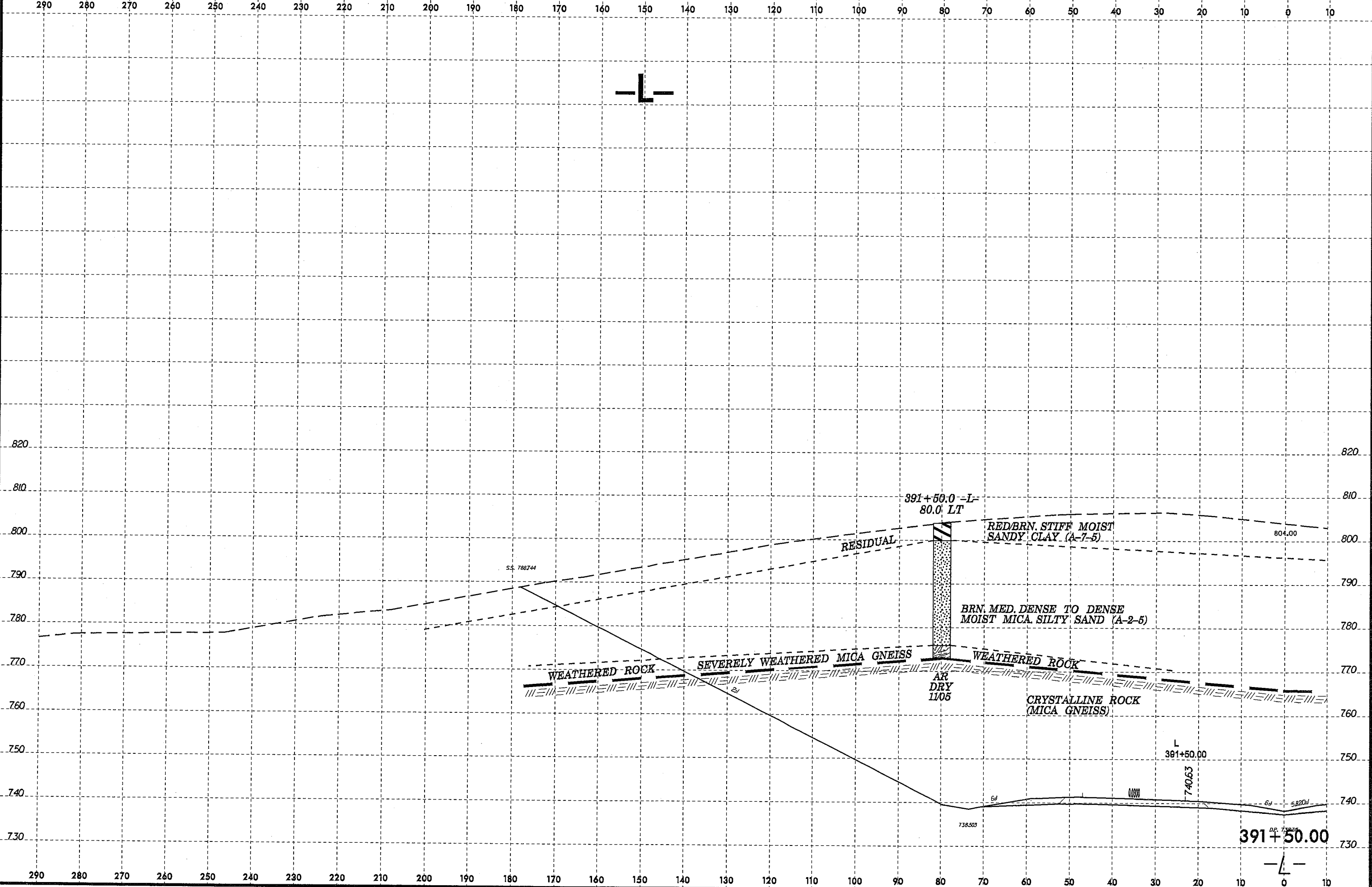


14-MAY-2008 13:44  
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 gburris AT 08/23/98

8/23/99  
29-MAY-2008 08:20  
c:\projects\2707\2707\rev\geo\_rdw\cleveland\cadd\geotech\sec\2707\rev\geo\_xsi.L.L.dgn  
sburns AT 08:22:57



8/23/95



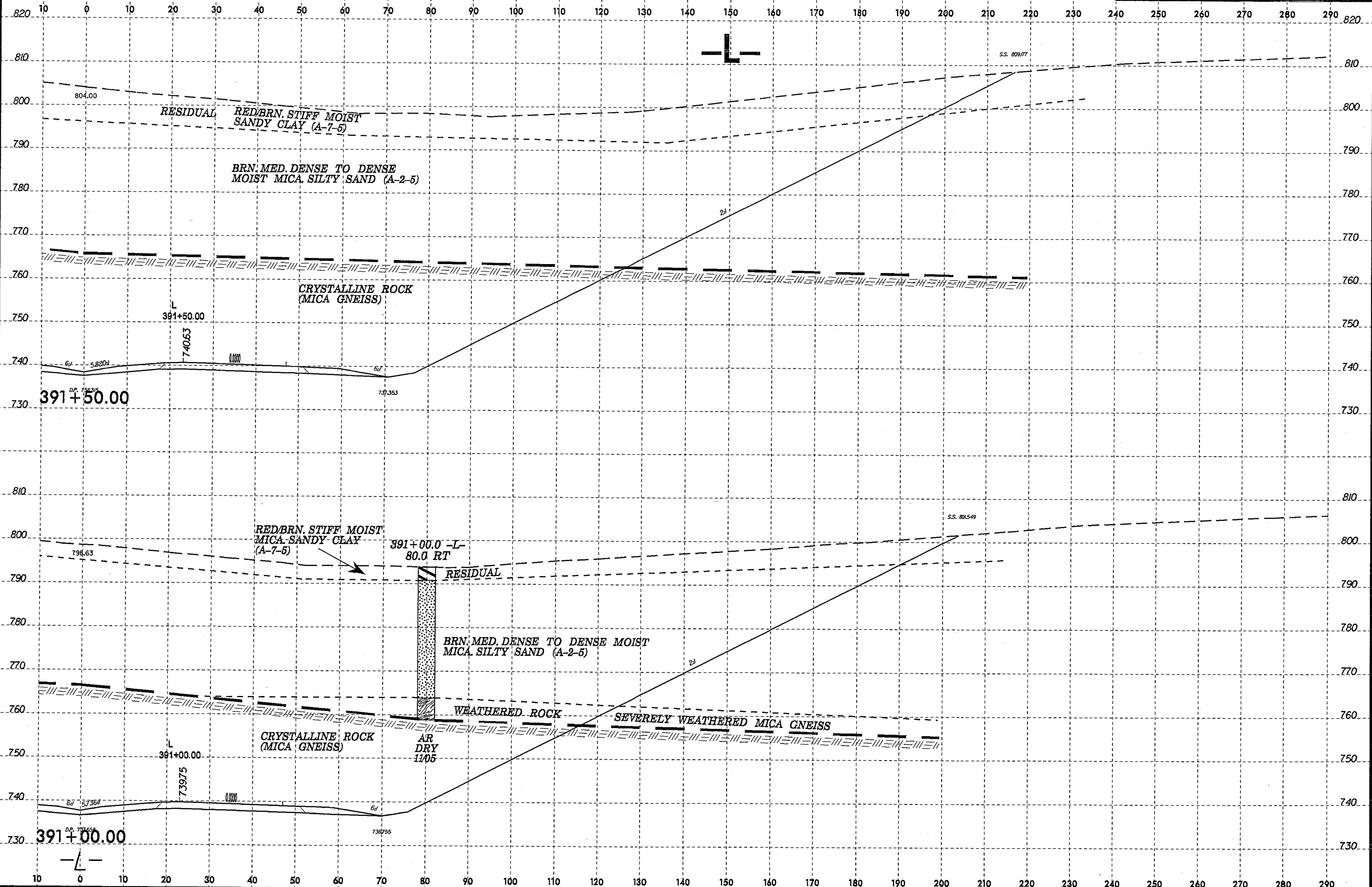
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 cburns AT BEH226187



8/23/99



PROJ. REFERENCE NO.	SHEET NO.
R-2707C	119



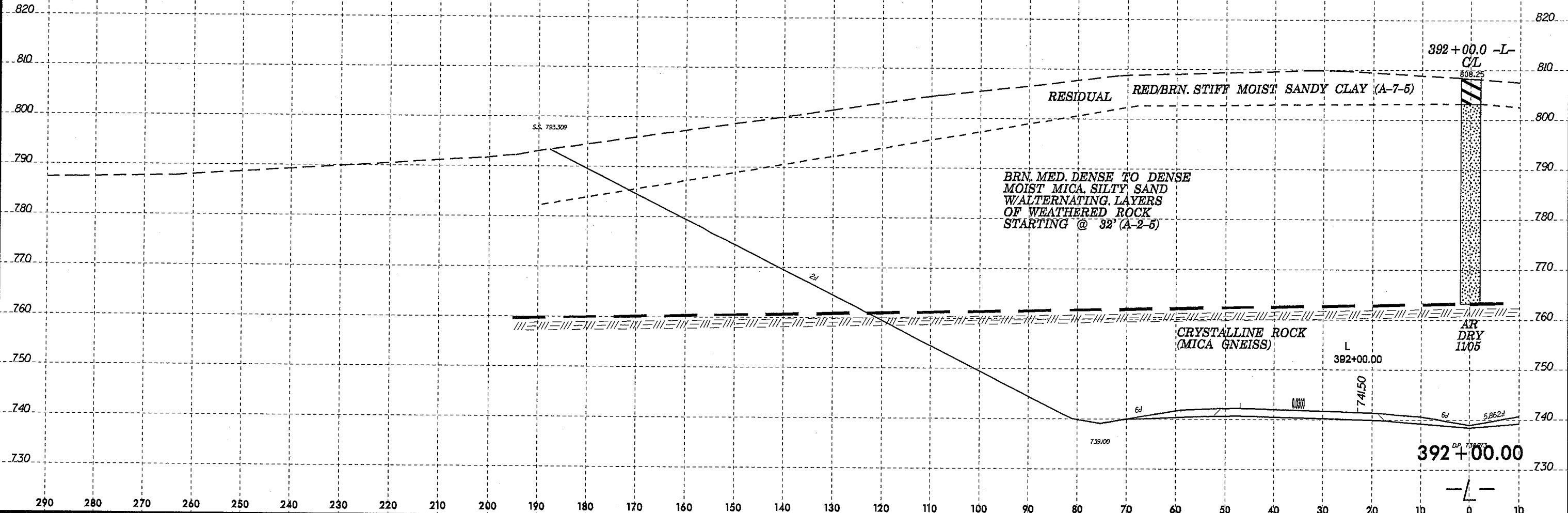
15-MAY-2008 14:47  
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 cburns AT BEH26157

8/23/99



PROJ. REFERENCE NO.	SHEET NO.
R-2707C	120

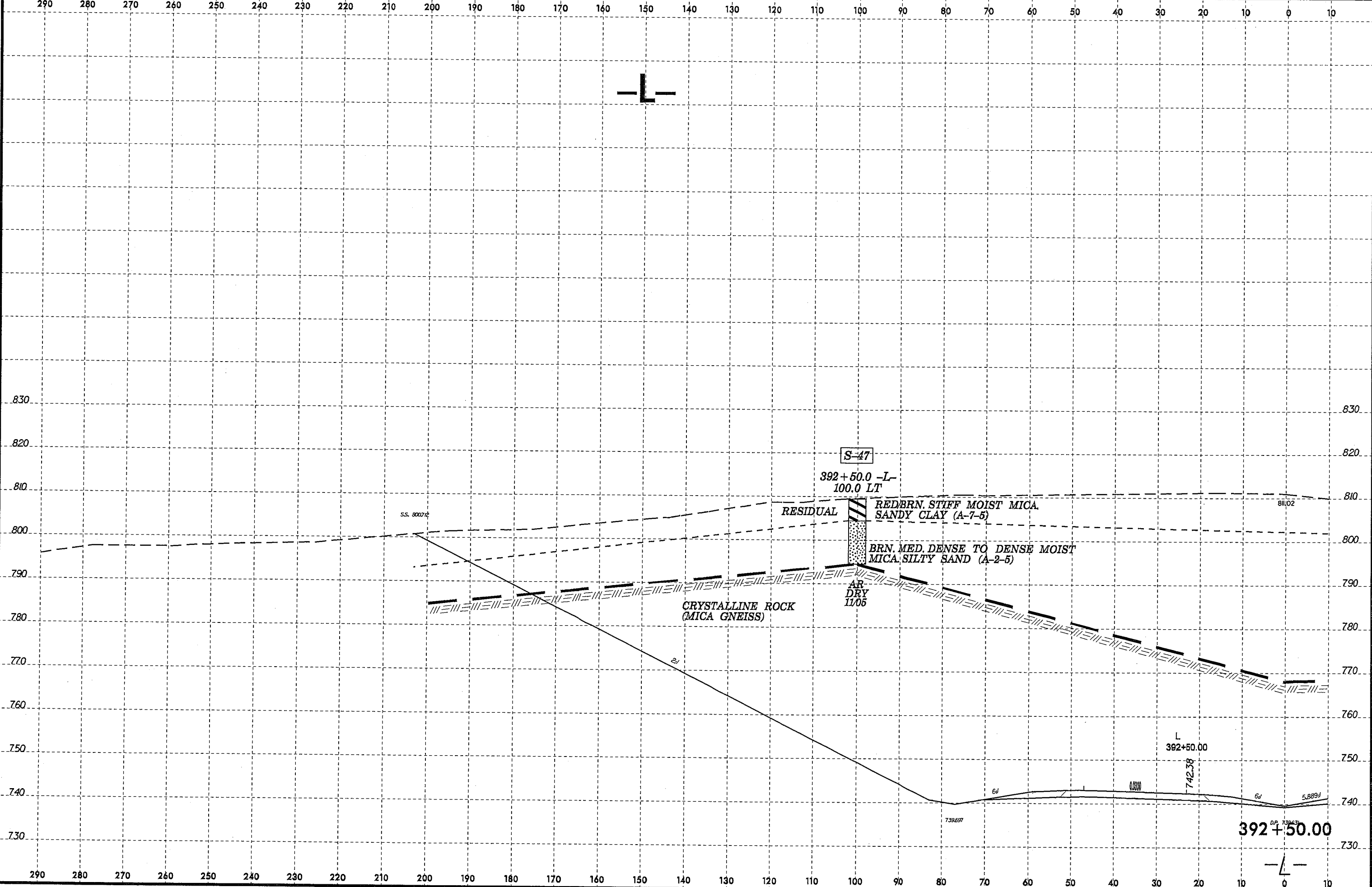
290 280 270 260 250 240 230 220 210 200 190 180 170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10



I:\MAY-2008\BAC  
 di\projects\2707\geo\_rdy\cleveland\cadd\geotech\ssc\2707\c(rev).geo\_xsl.L\dgn  
 c:\projects\2707\geo\_rdy\cleveland\cadd\geotech\ssc\2707\c(rev).geo\_xsl.L\dgn  
 AT 6/23/99

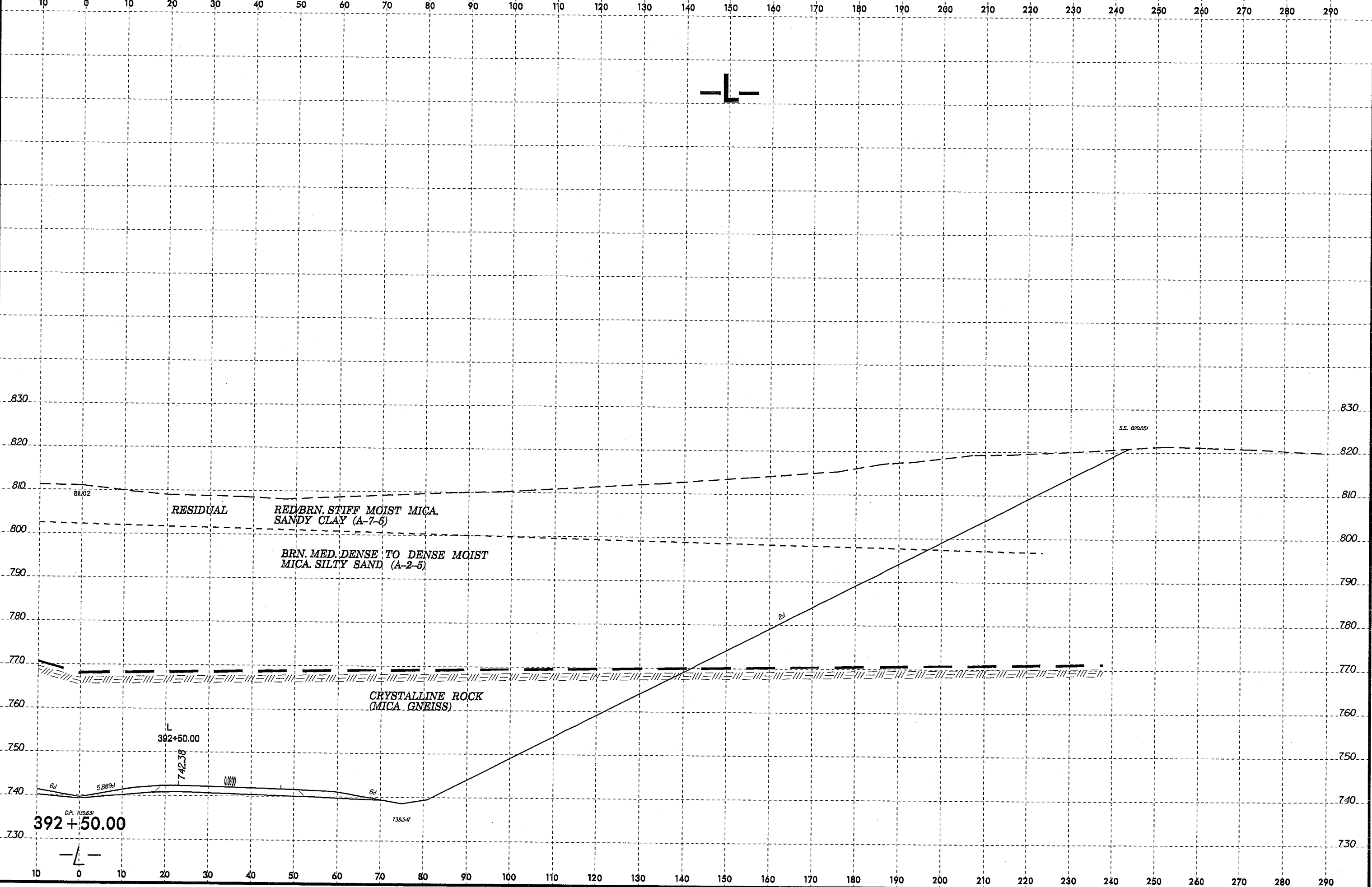


8/23/99



I4-MAY-2008 13:47  
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8/23/98

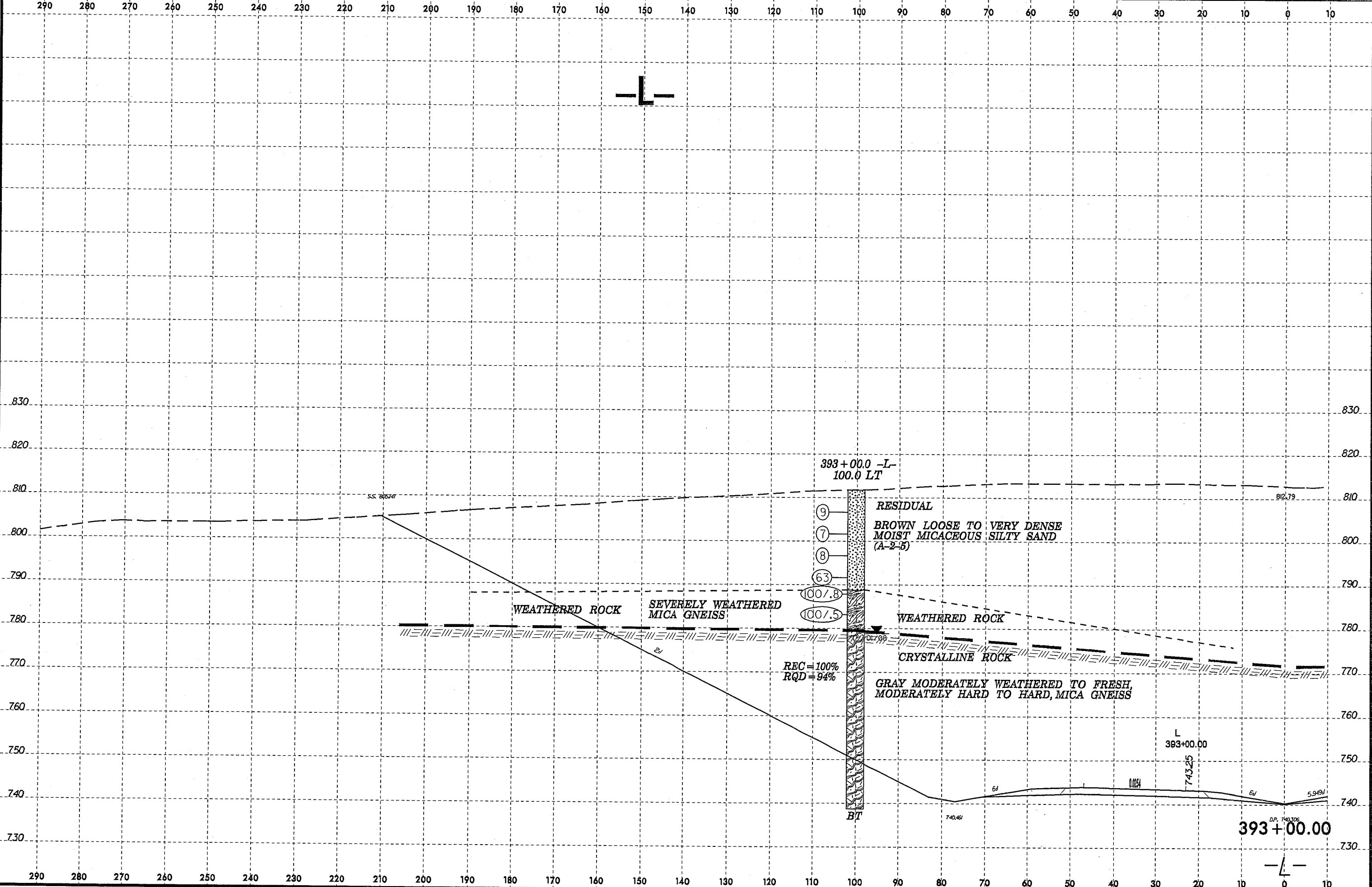


14-MAY-2008 14:10  
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 08:00:33 AT 65H2615

392+50.00



8/23/99



15-MAY-2008 14:38  
d:\projects\27075\rev1\geo\_rdw\cleveland\cadd\geotech\2707c\rev1\geo\_xst.l.l.dgn  
gburris AT 06/22/05

393+00.0 -L-  
100.0 LT

- 9
- 7
- 8
- 63
- 100/8
- 100/5

RESIDUAL  
BROWN LOOSE TO VERY DENSE  
MOIST MICACEOUS SILTY SAND  
(A-2-5)

WEATHERED ROCK

SEVERELY WEATHERED  
MICA GNEISS

WEATHERED ROCK

CRYSTALLINE ROCK

GRAY MODERATELY WEATHERED TO FRESH,  
MODERATELY HARD TO HARD, MICA GNEISS

REC = 100%  
RQD = 94%

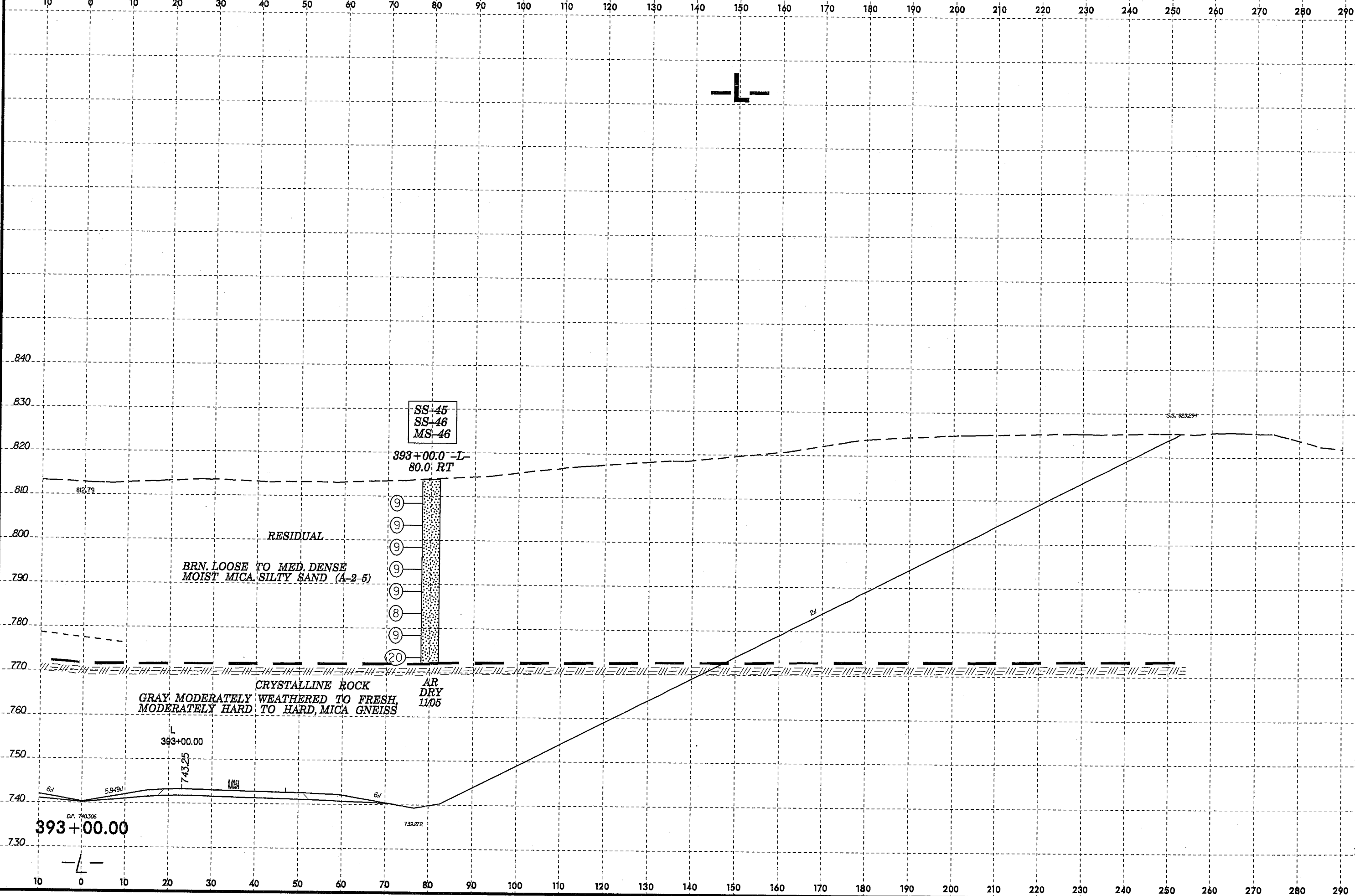
BT

L  
393+00.00

393+00.00

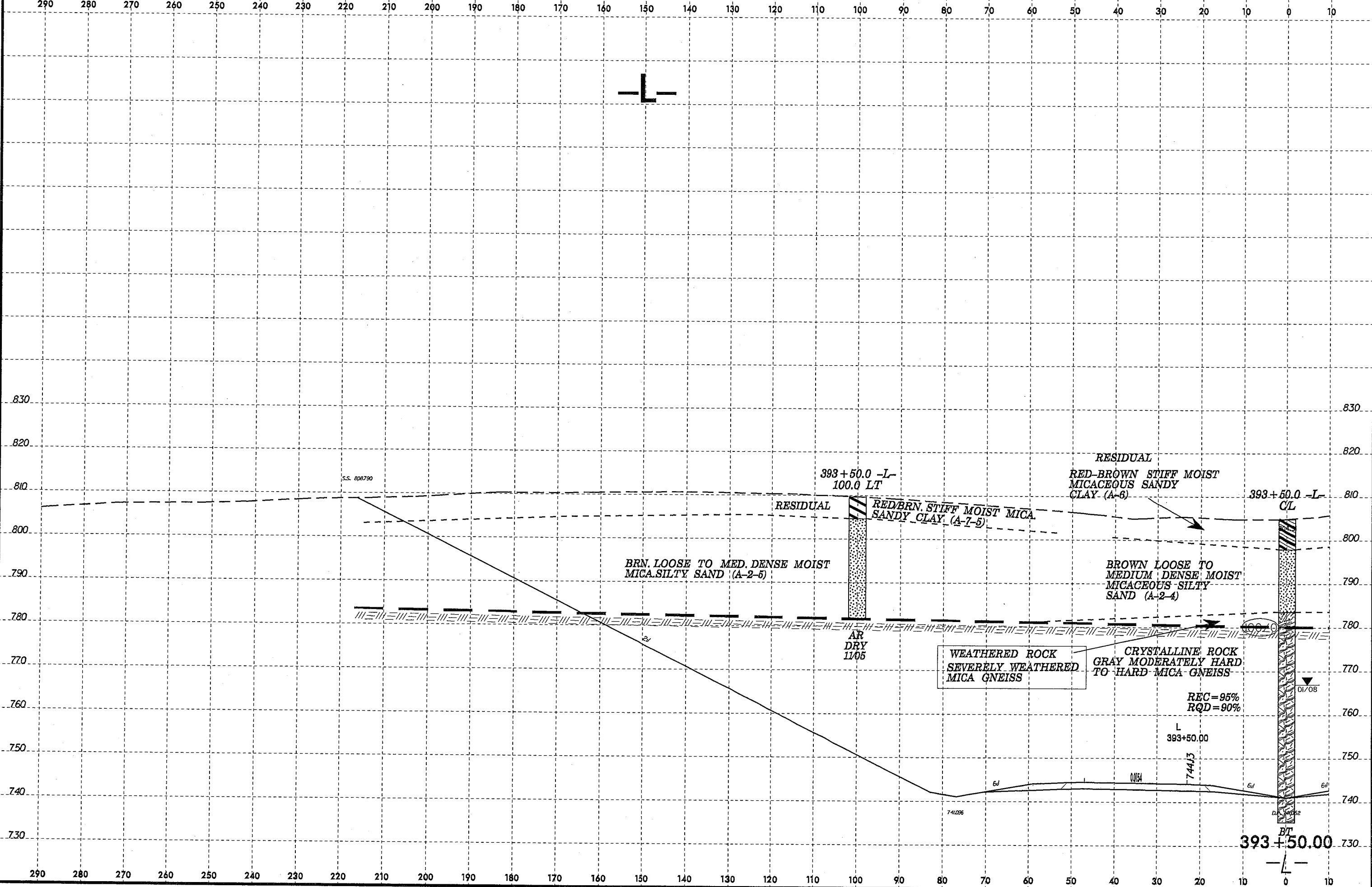
-L-

8/23/98



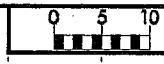
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 cburris AT GEH22617

8/23/99  
23-MAY-2008 08:36  
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cburris AT BEH22618

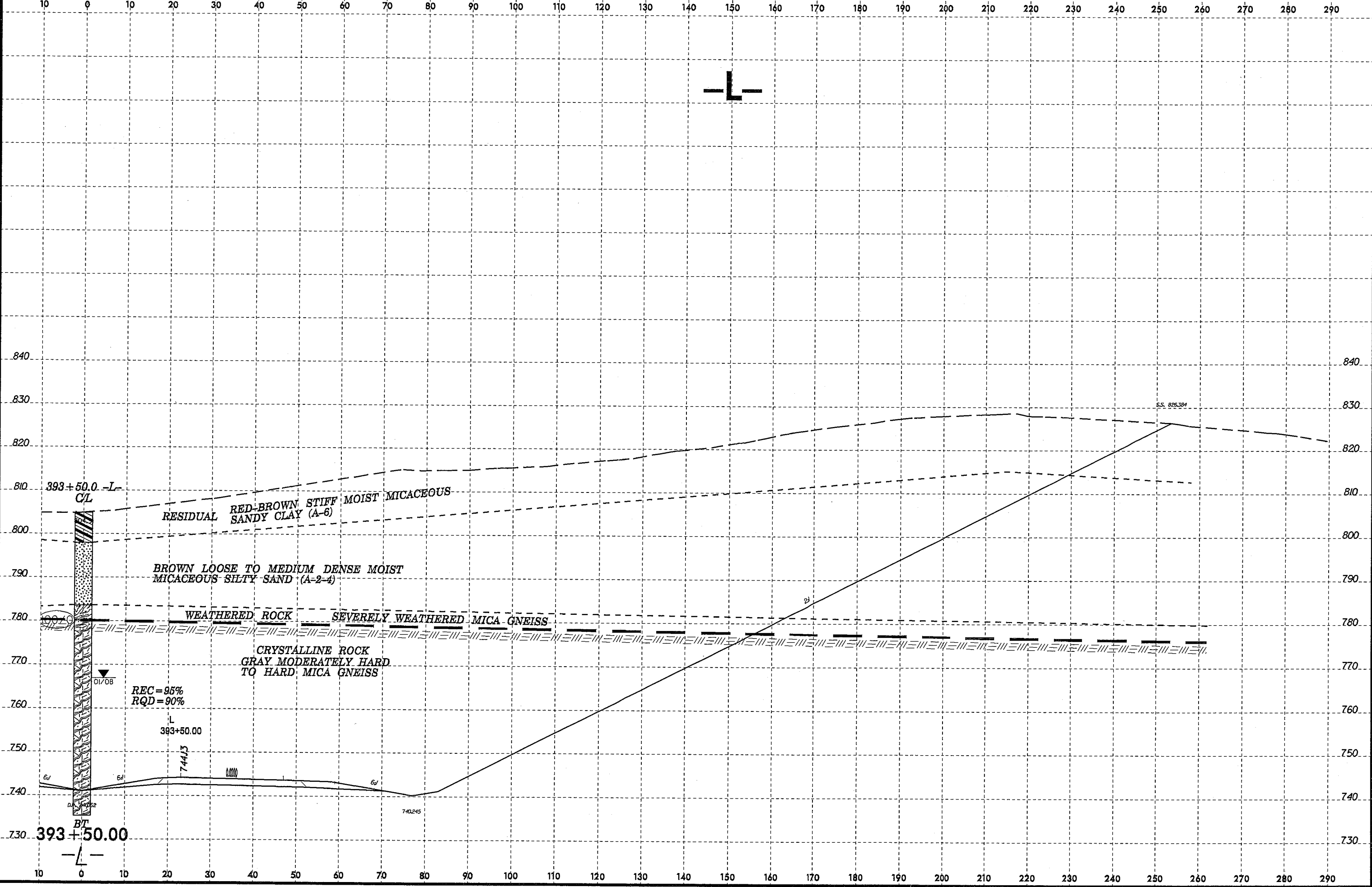




8/23/95



PROJ. REFERENCE NO.	SHEET NO.
R-2707C	757



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 cburr:rs AT BEH226157

393+50.0 -L-  
C/L

RESIDUAL RED-BROWN STIFF MOIST MICACEOUS SANDY CLAY (A-6)

BROWN LOOSE TO MEDIUM DENSE MOIST MICACEOUS SILTY SAND (A-2-4)

WEATHERED ROCK SEVERELY WEATHERED MICA GNEISS

CRYSTALLINE ROCK GRAY MODERATELY HARD TO HARD MICA GNEISS

REC = 95%  
RQD = 90%

L  
393+50.00

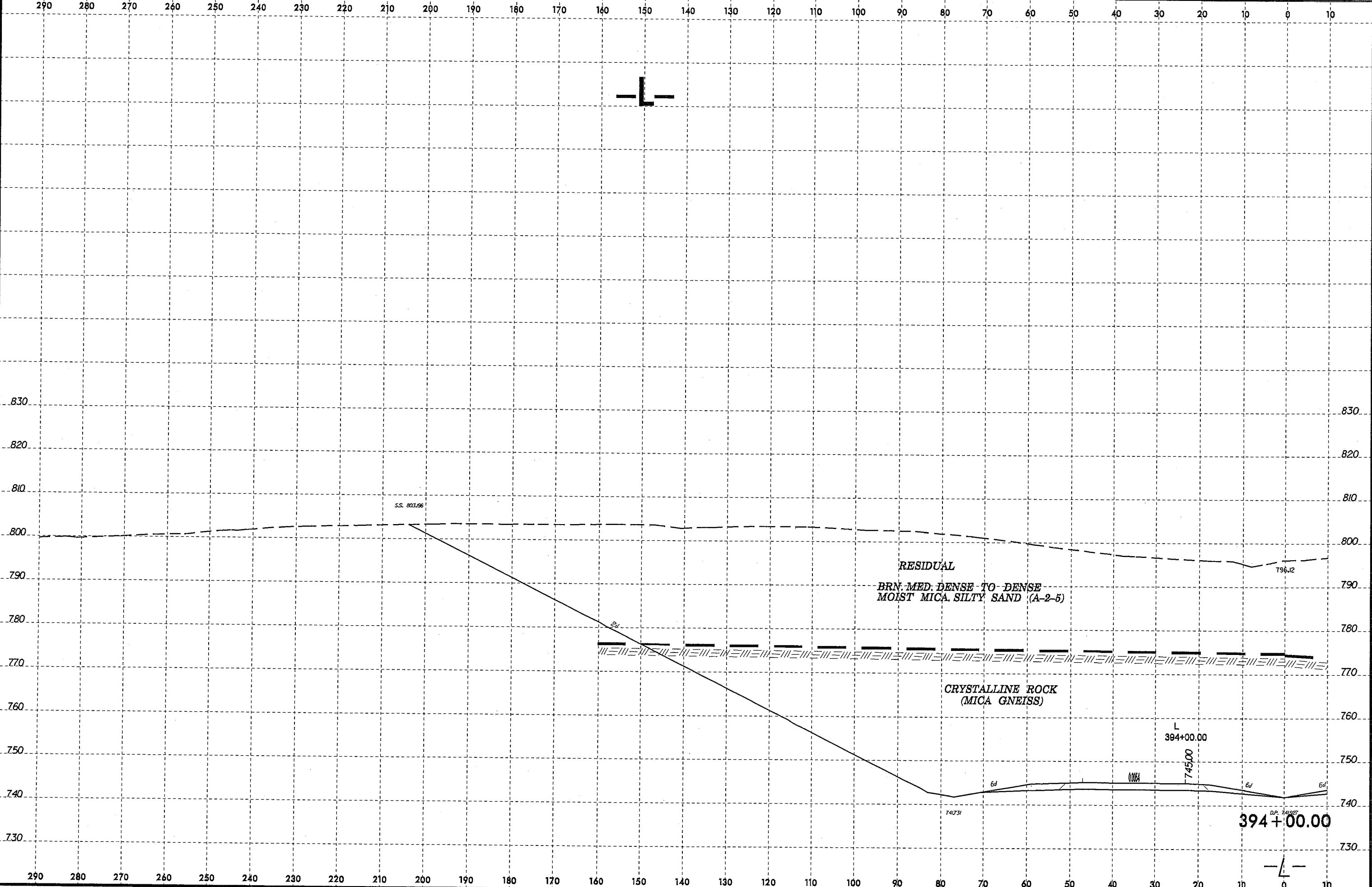
744.13

740.245

BT  
393+50.00

8/23/99

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	129



14-MAY-2008 13:49  
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 burris AT DEN28137

RESIDUAL  
 BRN. MED. DENSE TO DENSE  
 MOIST MICA SILTY SAND (A-2-5)

CRYSTALLINE ROCK  
 (MICA GNEISS)

394+00.00

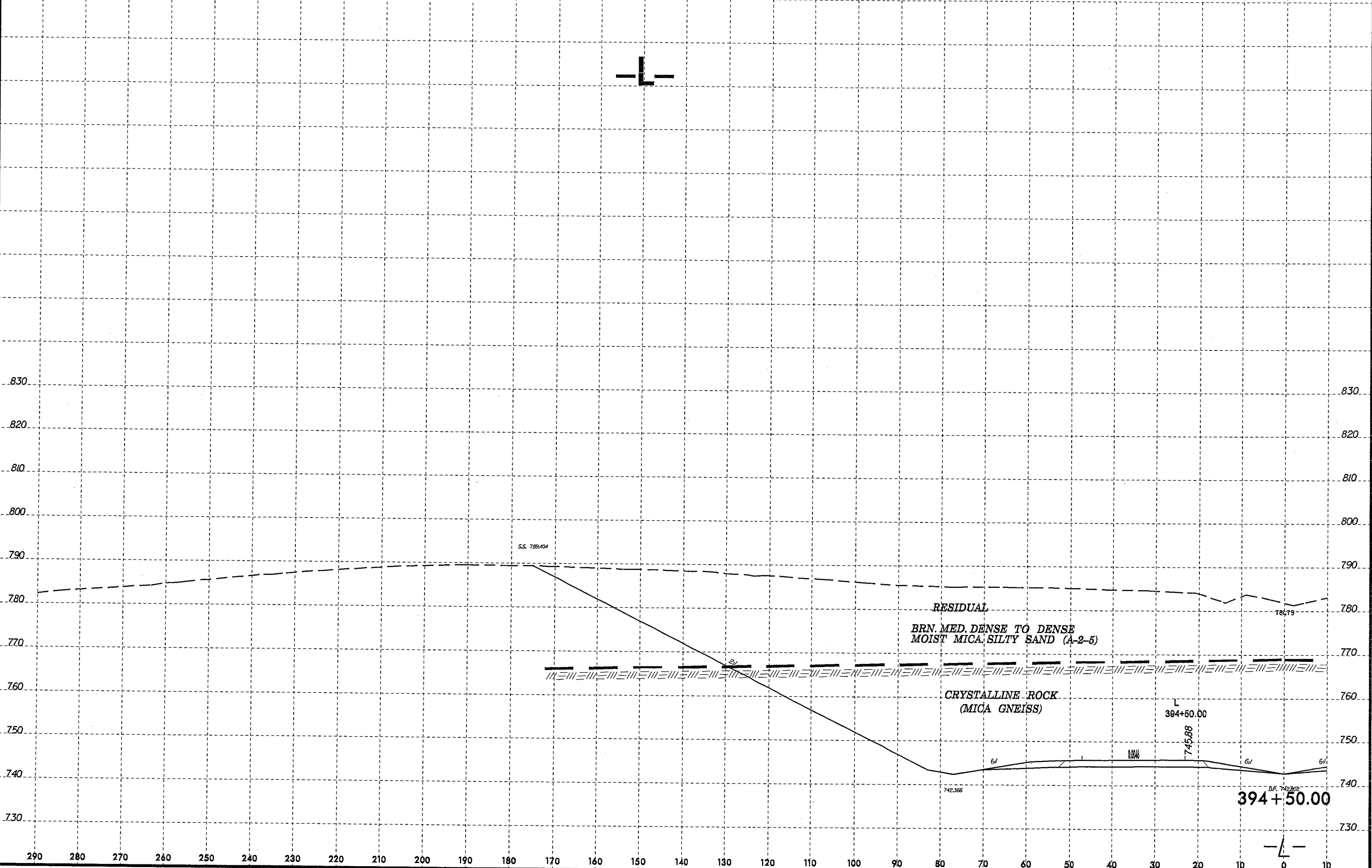
14-MAY-2008 13:49



8/23/99

290 280 270 260 250 240 230 220 210 200 190 180 170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 10
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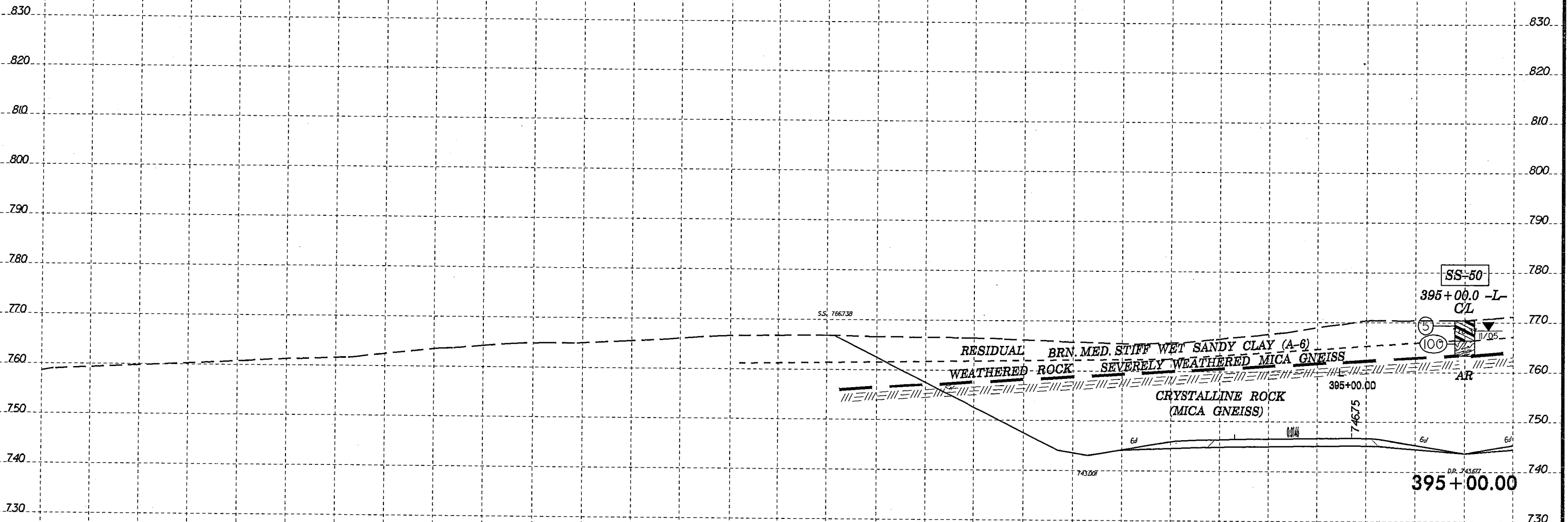
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saurzj

290 280 270 260 250 240 230 220 210 200 190 180 170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10



8/23/99

290 280 270 260 250 240 230 220 210 200 190 180 170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10

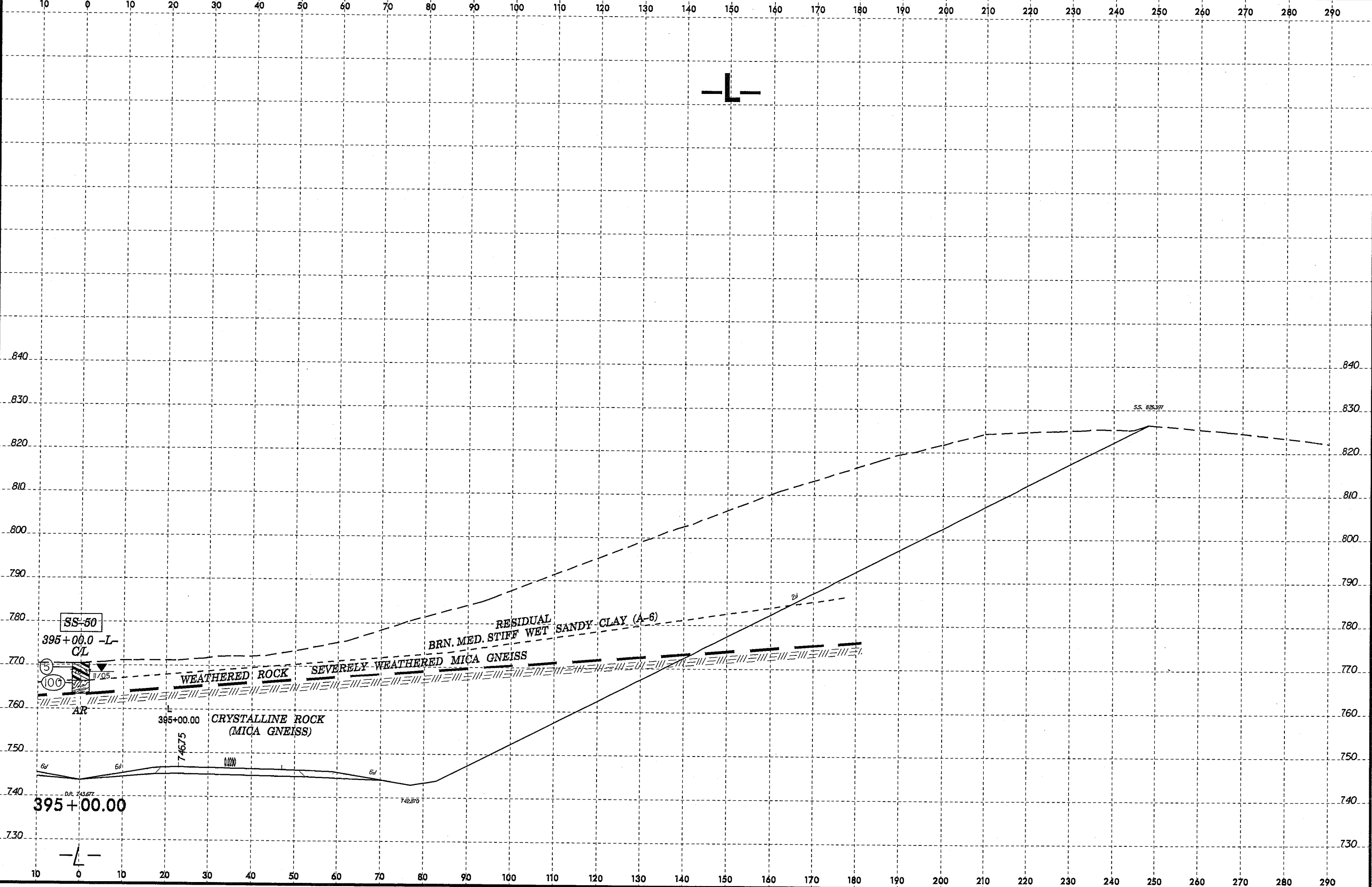


290 280 270 260 250 240 230 220 210 200 190 180 170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10

15-MAY-2008 14:55  
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 A1 BEH26187

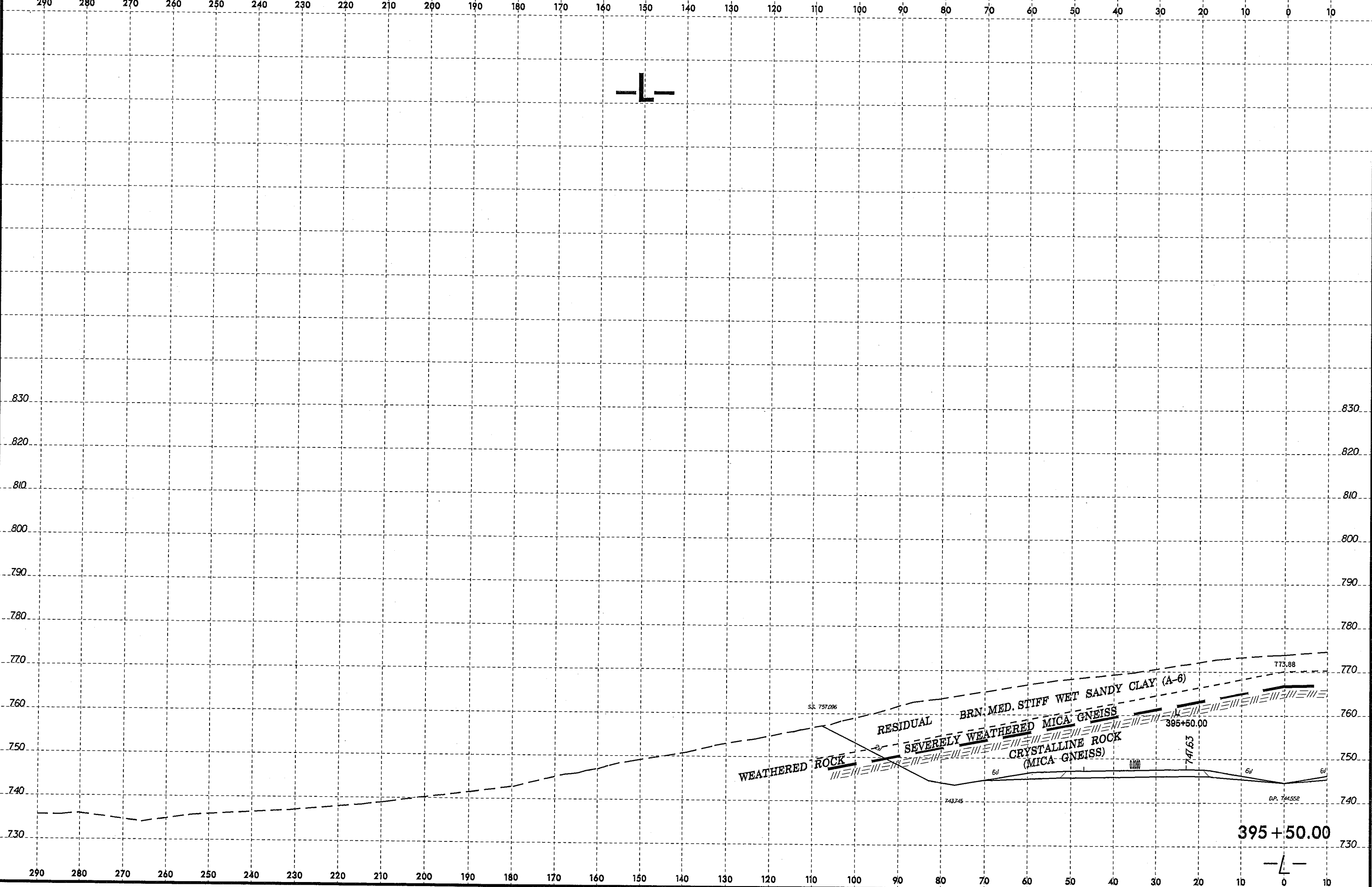
-L-

8/23/95  
15-MAY-2008 14:56  
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dburris AT DEHZ26157



8/23/95

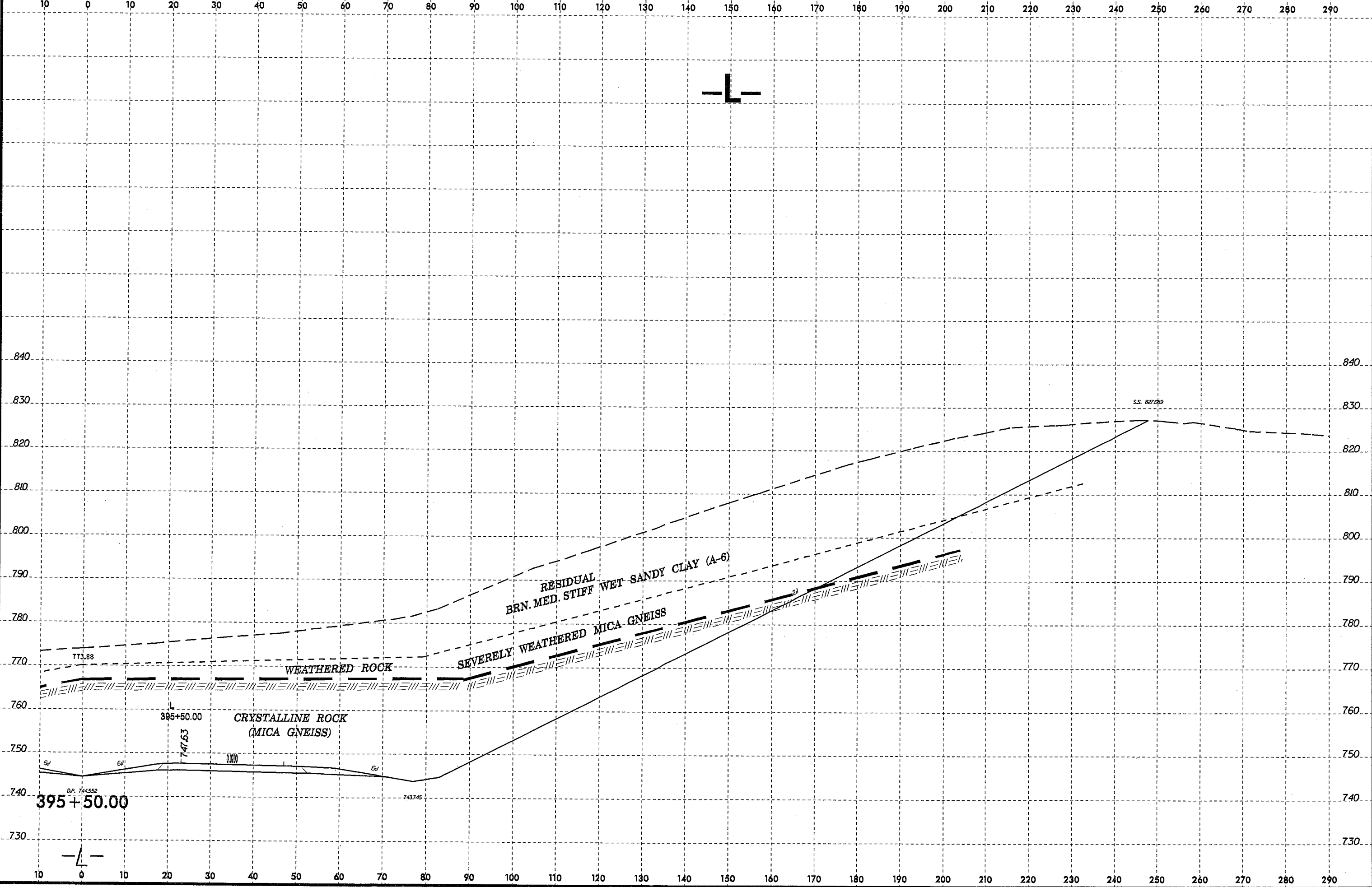
0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 134
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15-MAY-2008 14:57  
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cburris AT BEH226157



8/23/95  
15-MAY-2009 14:58  
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cburris



840  
830  
820  
810  
800  
790  
780  
770  
760  
750  
740  
730

10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290

CRYSTALLINE ROCK  
(MICA GNEISS)

WEATHERED ROCK

SEVERELY WEATHERED MICA GNEISS

RESIDUAL  
BRN. MED. STIFF WET SANDY CLAY (A-6)

773.88

395+50.00  
747.63

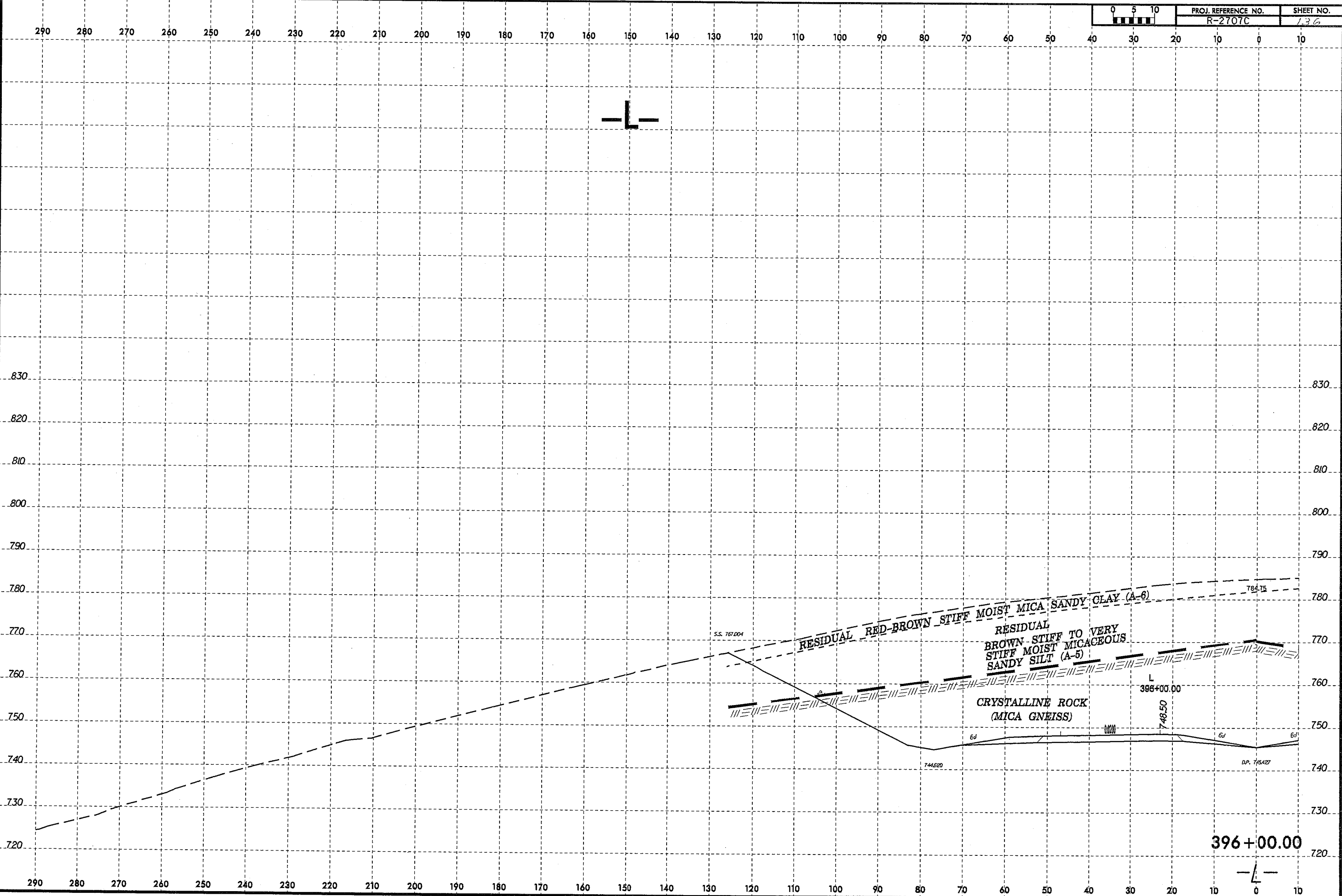
D.P. 745.52

743.45

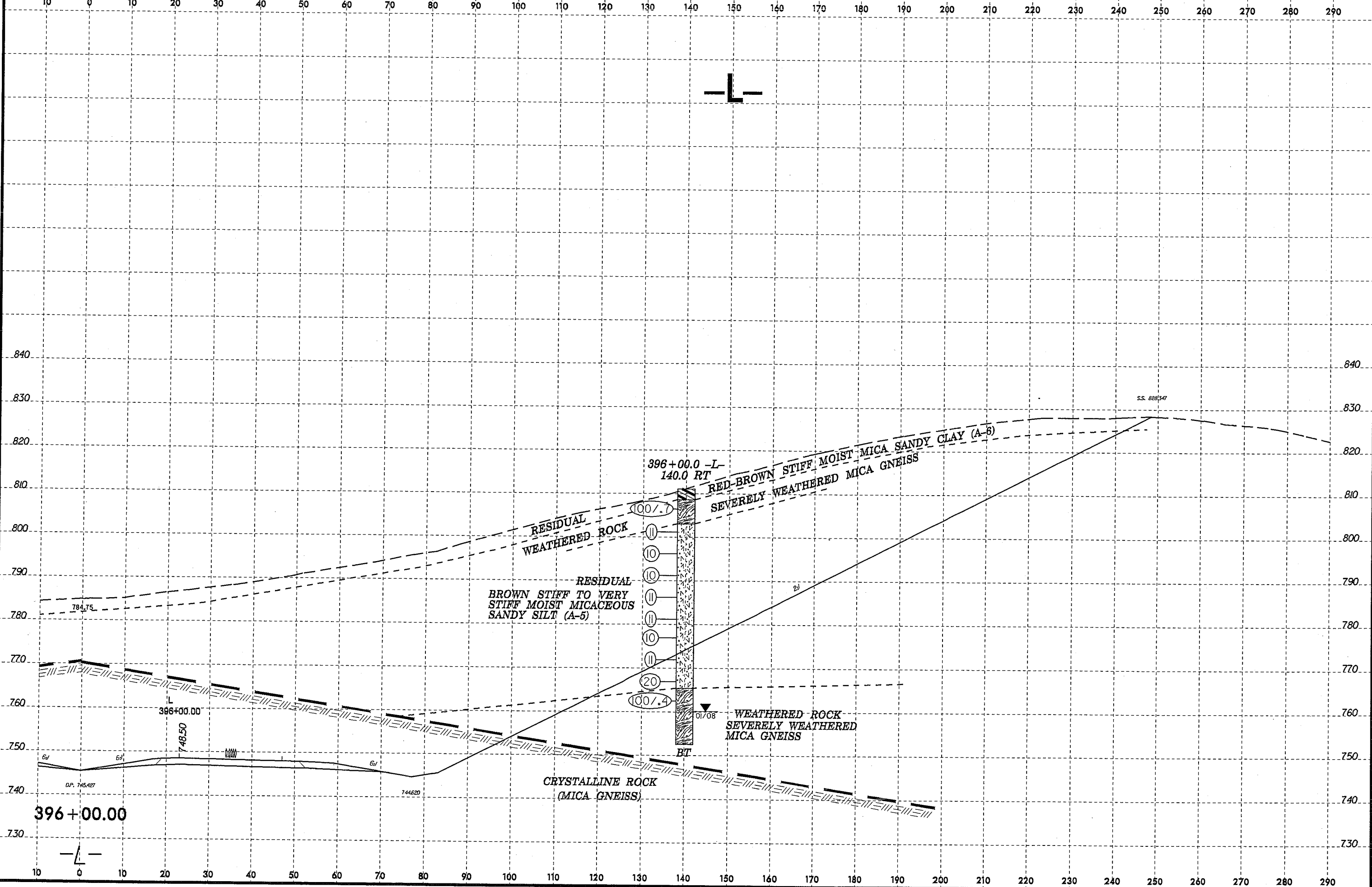
S.S. 827.09

6' 6' 6'

16-MAY-2008 14:35  
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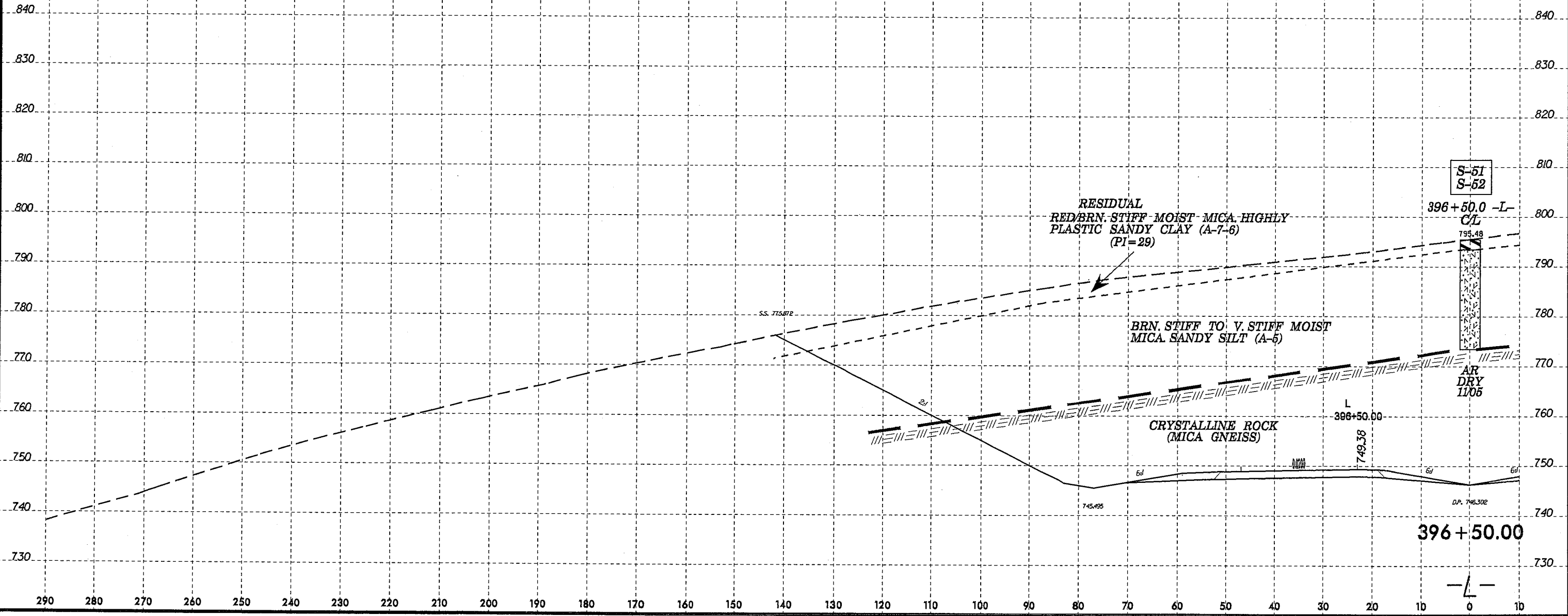
8/23/98



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 cburris AT BEH226157

8/23/99

290 280 270 260 250 240 230 220 210 200 190 180 170 160 150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10



RESIDUAL  
RED/BRN. STIFF MOIST MICA HIGHLY  
PLASTIC SANDY CLAY (A-7-6)  
(PI=29)

BRN. STIFF TO V. STIFF MOIST  
MICA SANDY SILT (A-5)

CRYSTALLINE ROCK  
(MICA GNEISS)

S-51  
S-52

396+50.0 -L-  
CL

795.48

AR  
DRY  
1105

L  
396+50.00

749.58

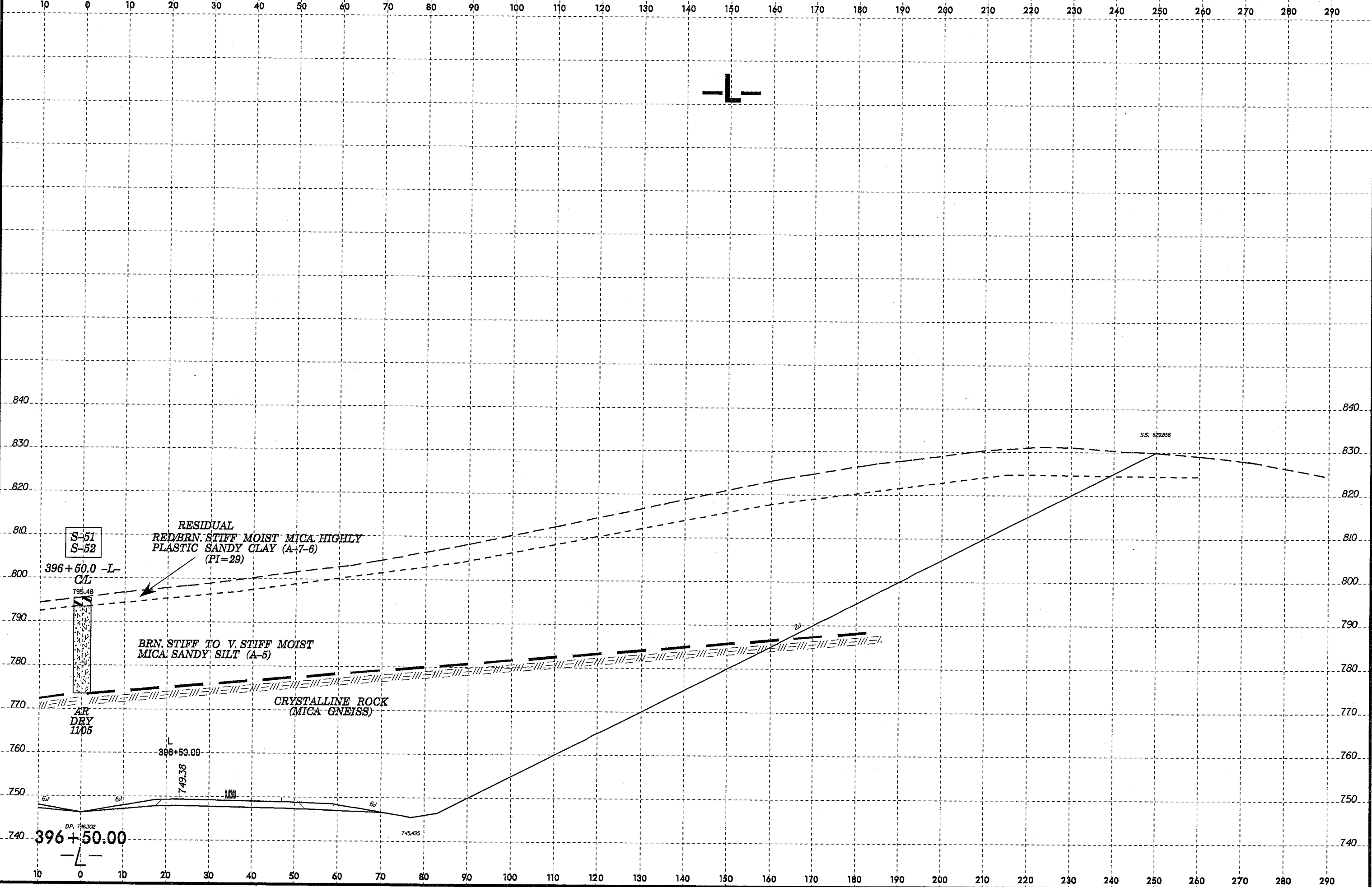
745.495

D.P. 746.302

396+50.00

29-MAY-2008 09:01  
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8/23/99

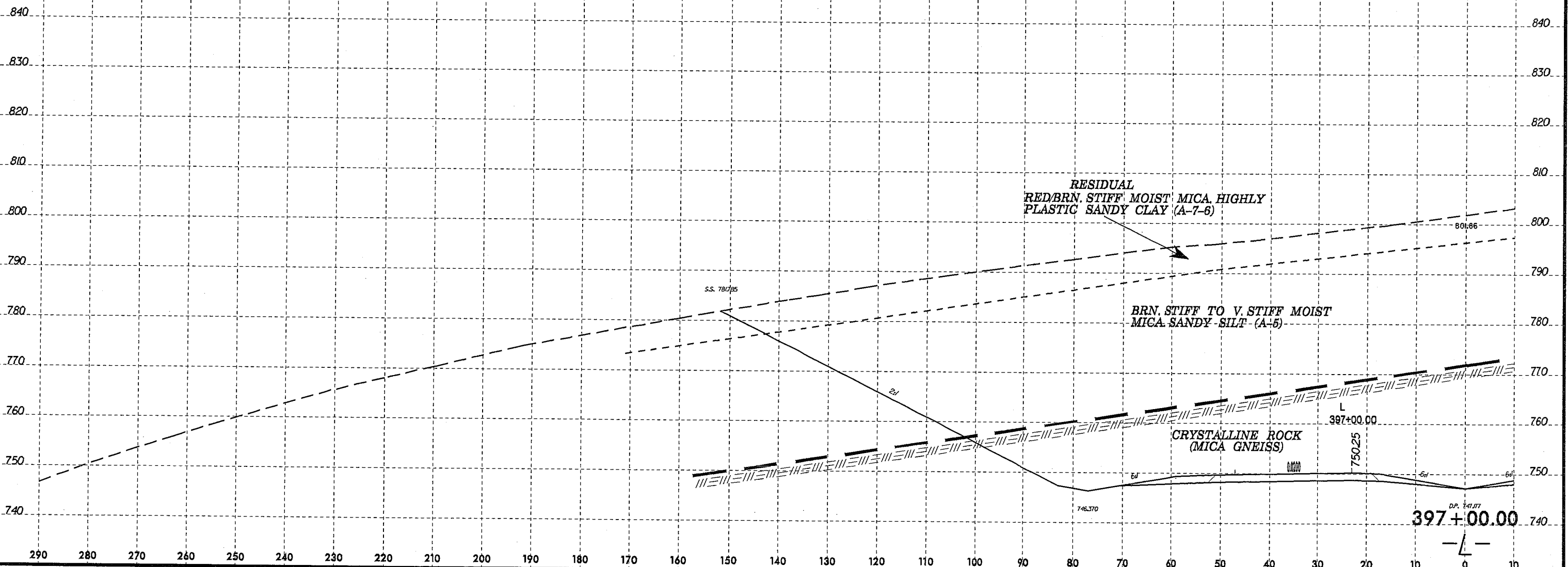


29-MAY-2008 09:02  
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 cburr AT 08H2517

8/23/99

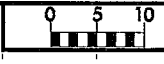
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0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 10
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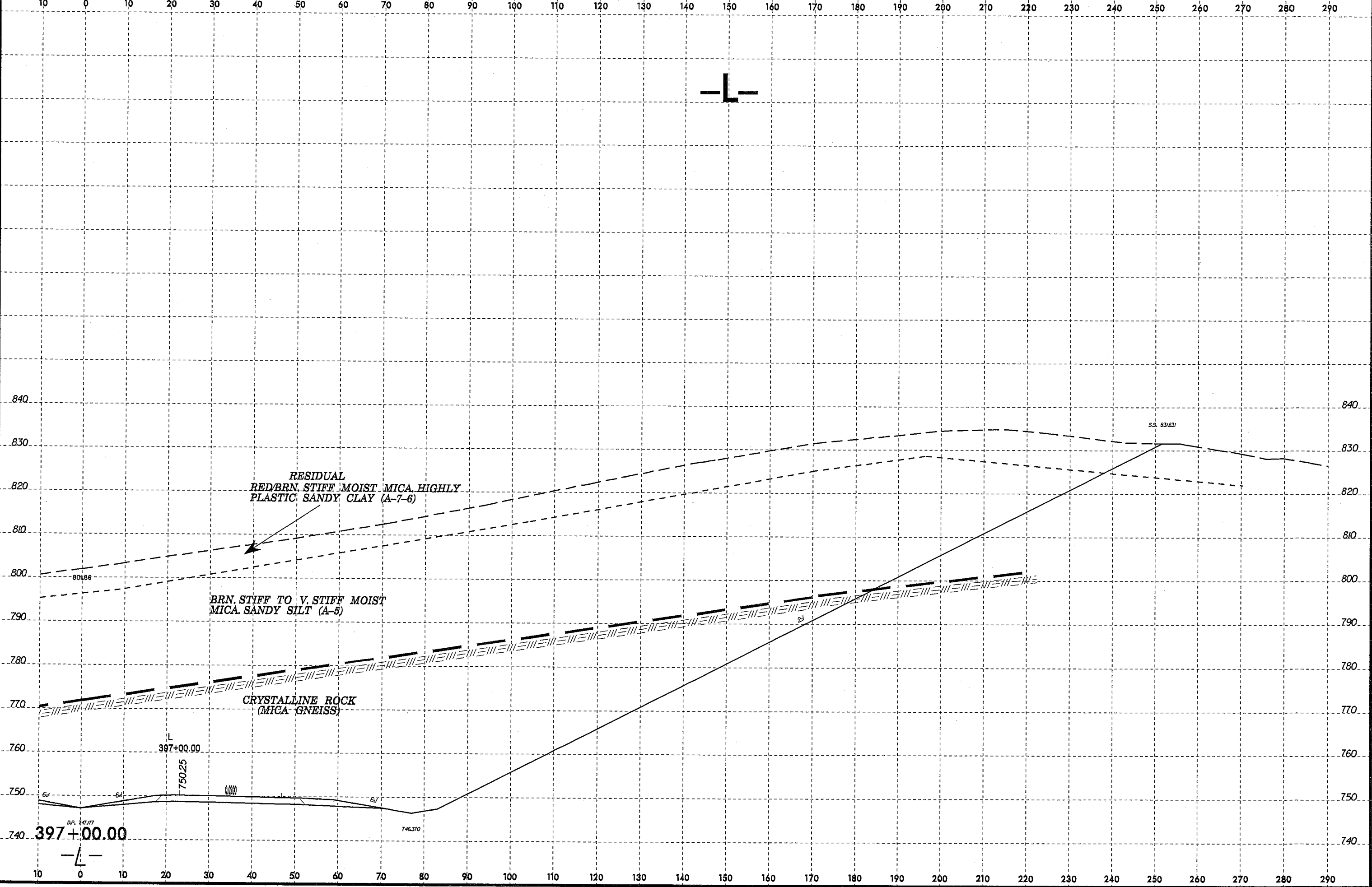


14-MAY-2008 13:54  
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8/23/99

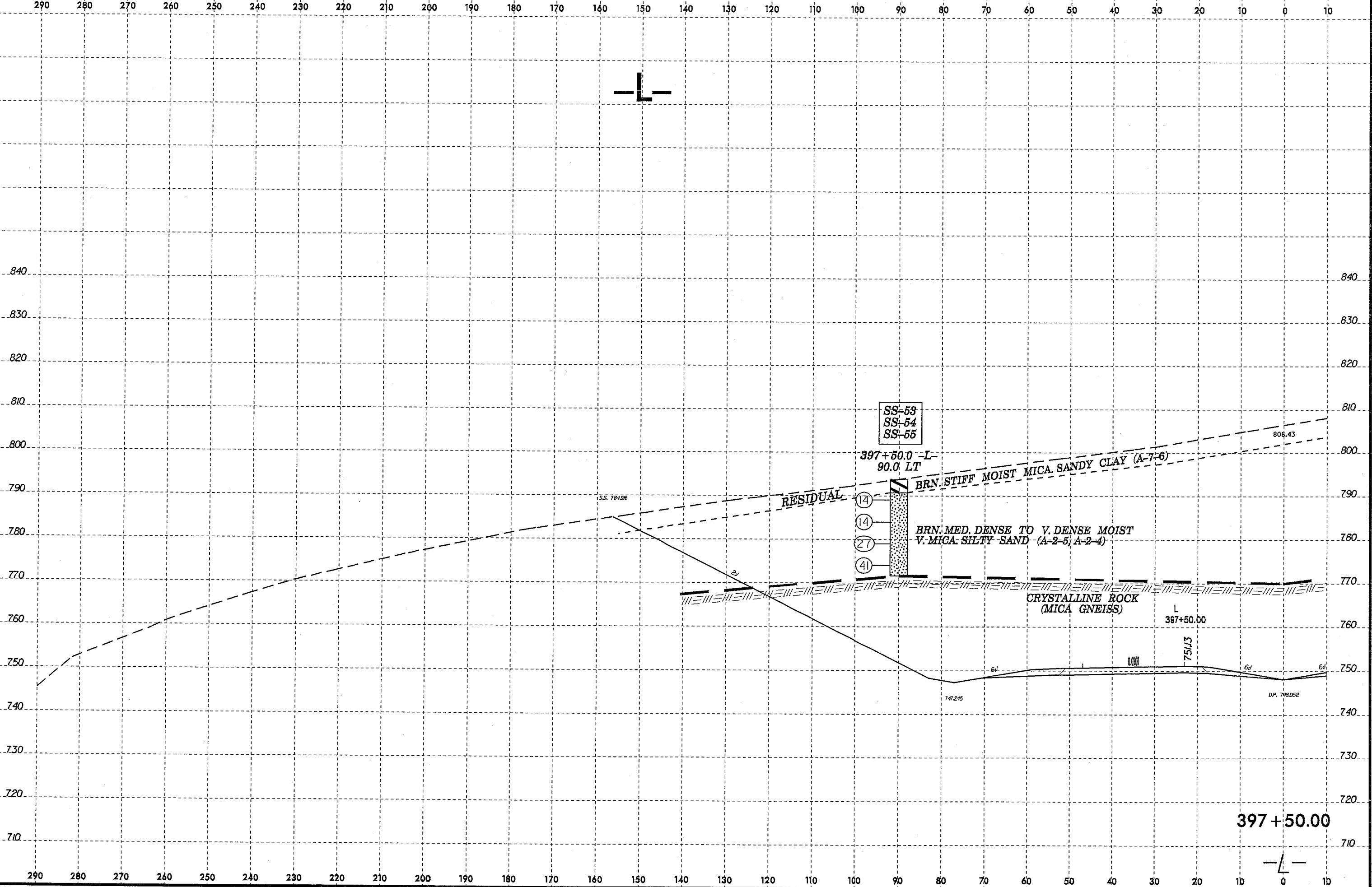


PROJ. REFERENCE NO.	SHEET NO.
R-2707C	14/1



14-MAY-2008 14:21  
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 cburns AT BEH226157

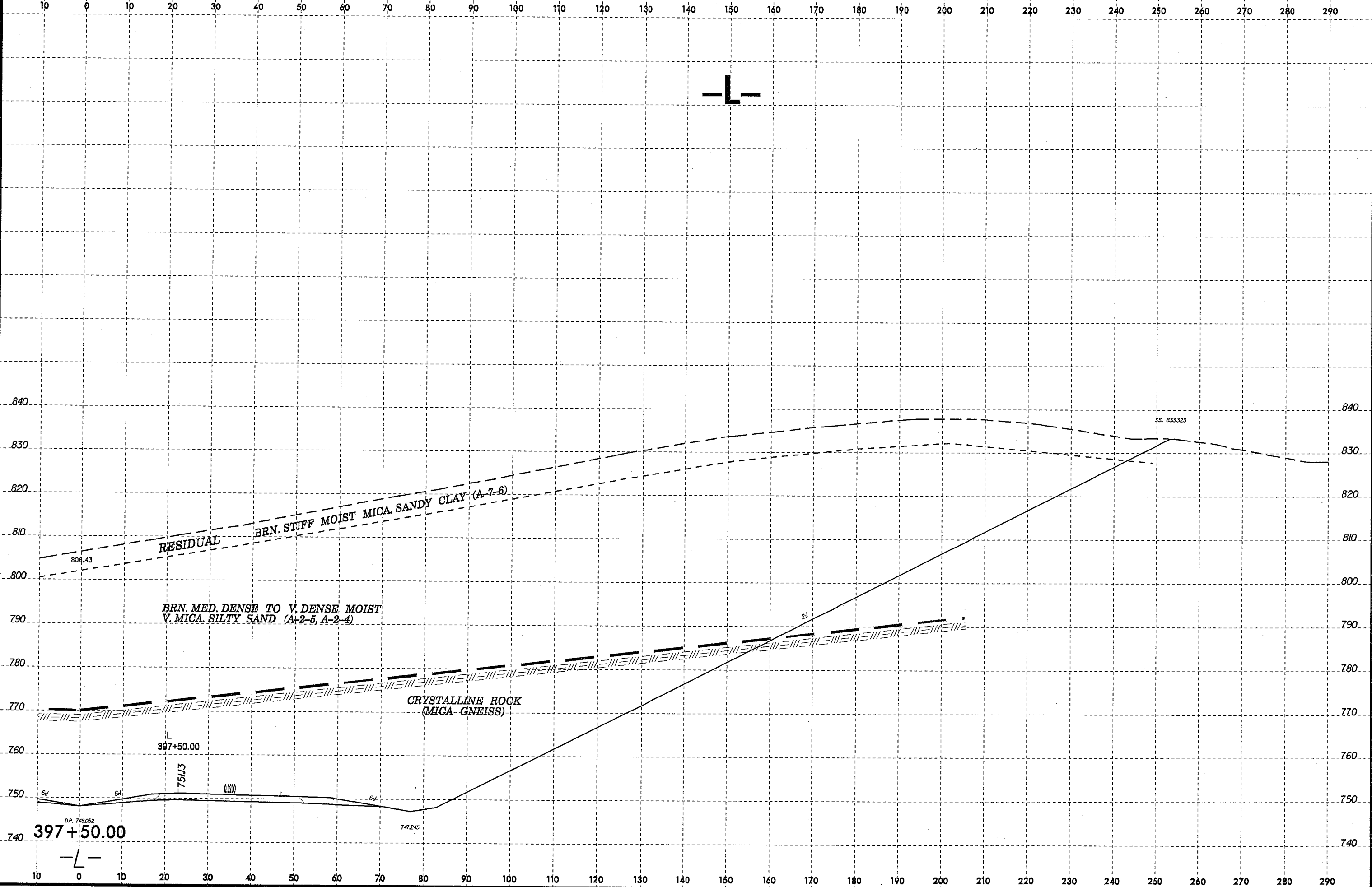
8/23/99



14-MAY-2008 13:55  
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14-MAY-2008 14:22  
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gburr13 AT 08/22/07



10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290

840 830 820 810 800 790 780 770 760 750 740

RESIDUAL BRN. STIFF MOIST MICA SANDY CLAY (A-7-6)

BRN. MED. DENSE TO V. DENSE MOIST V. MICA SILTY SAND (A-2-5, A-2-4)

CRYSTALLINE ROCK (MICA-GNEISS)

806.43

397+50.00

751.13

741.245

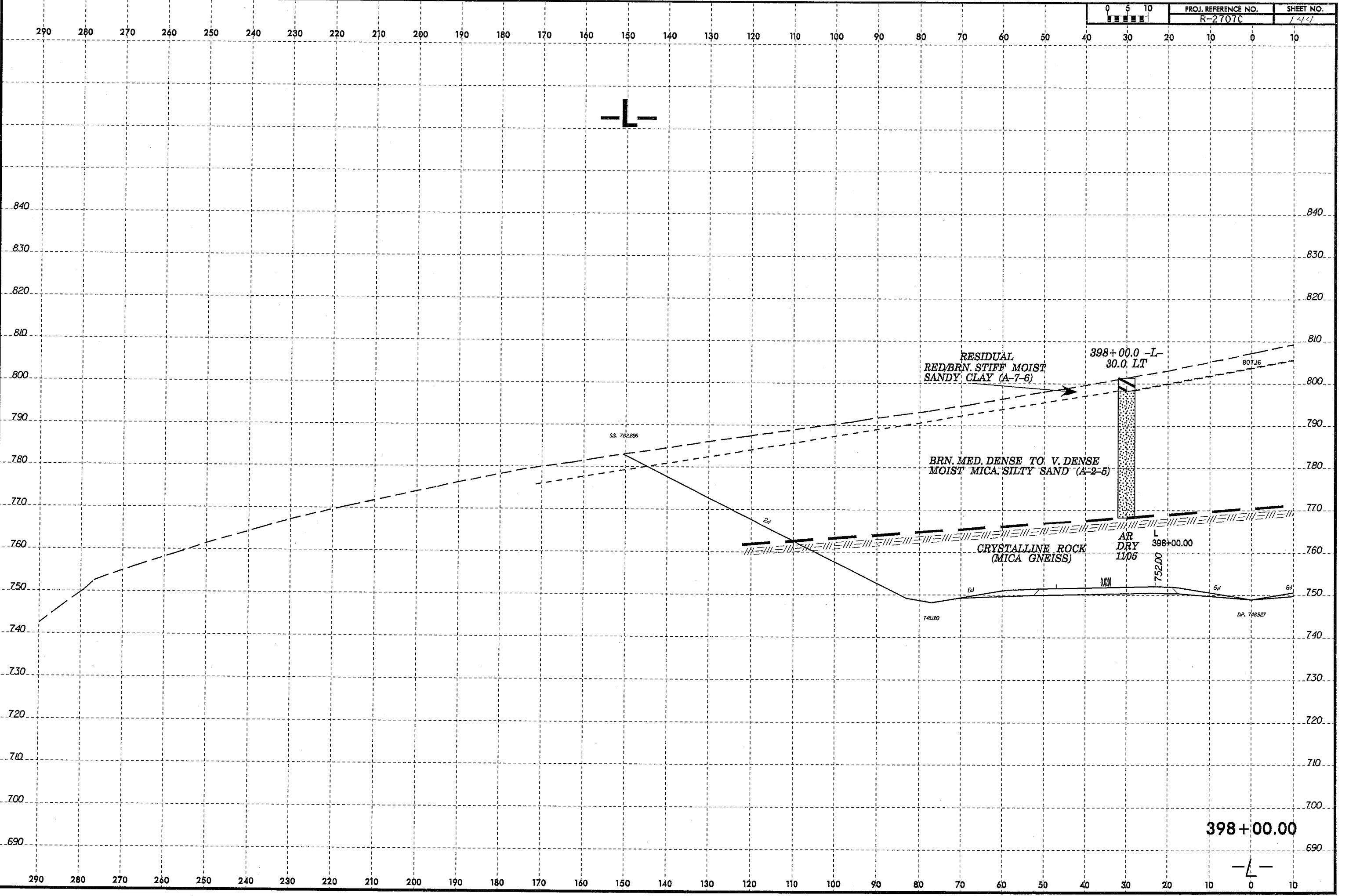
833.323

10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290

14-MAY-2008 13:56  
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cburns AL BEH26187

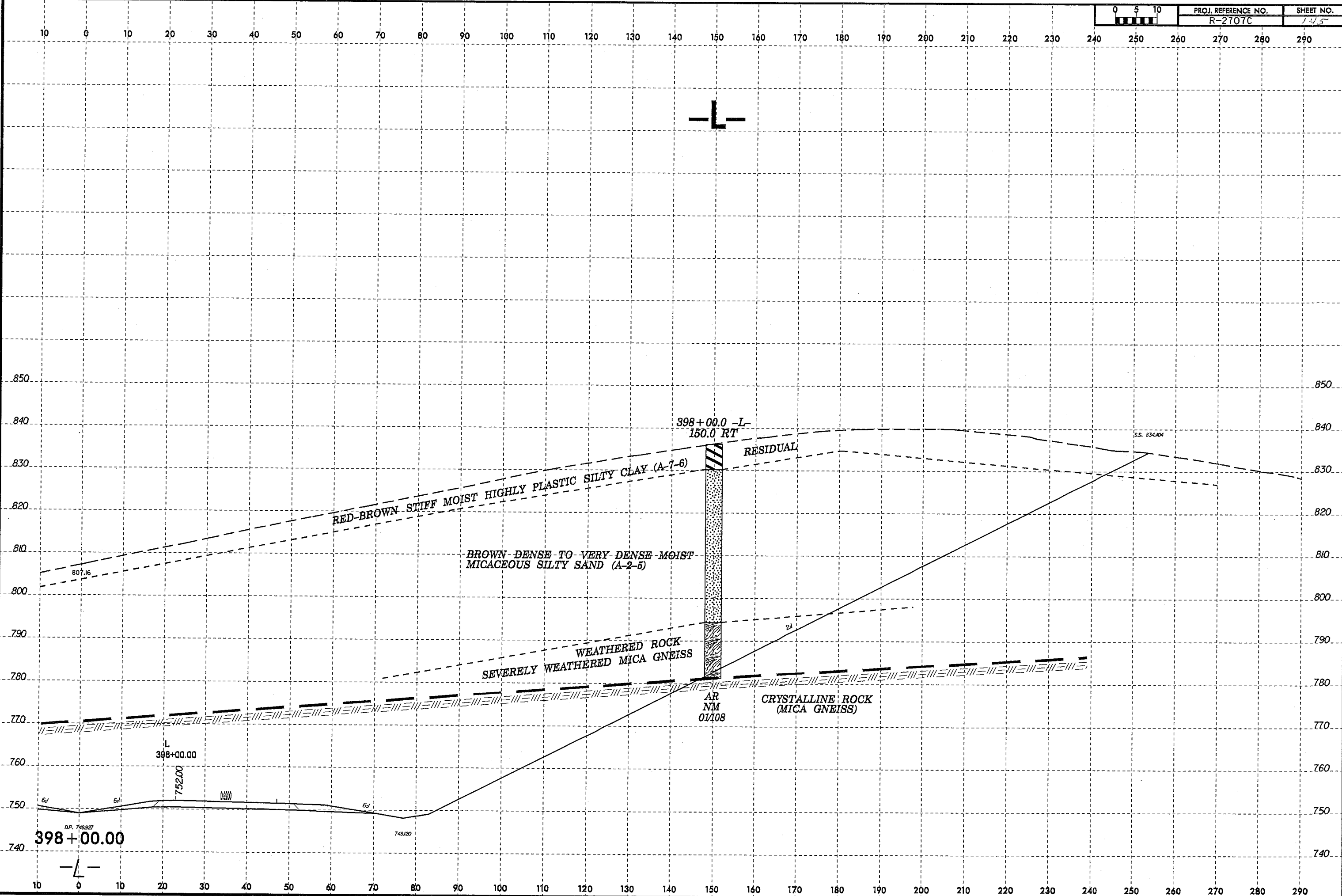
0 5 10

PROJ. REFERENCE NO. R-2707C	SHEET NO. 144
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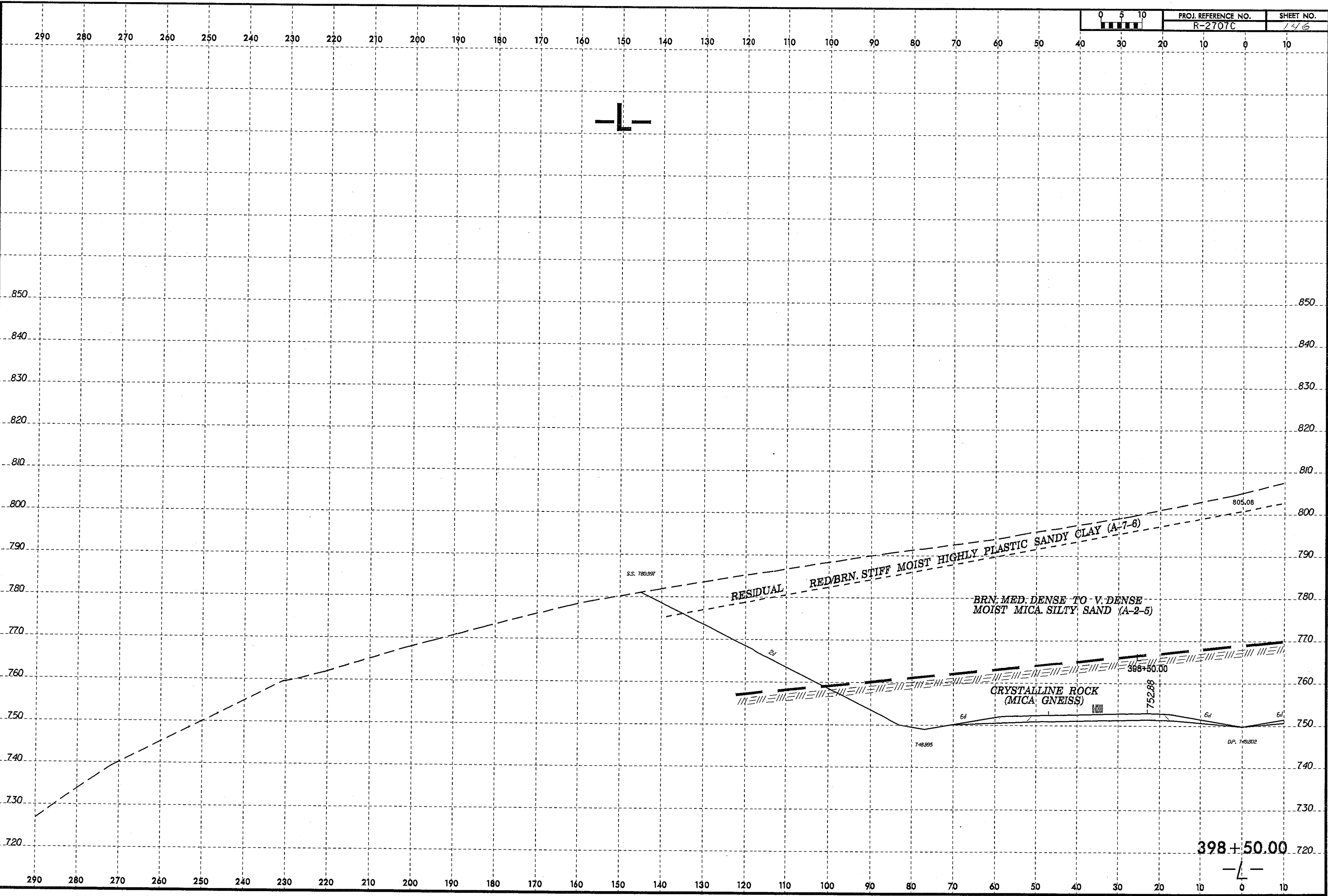


398+00.00

-L-

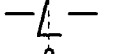


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 8/23/09

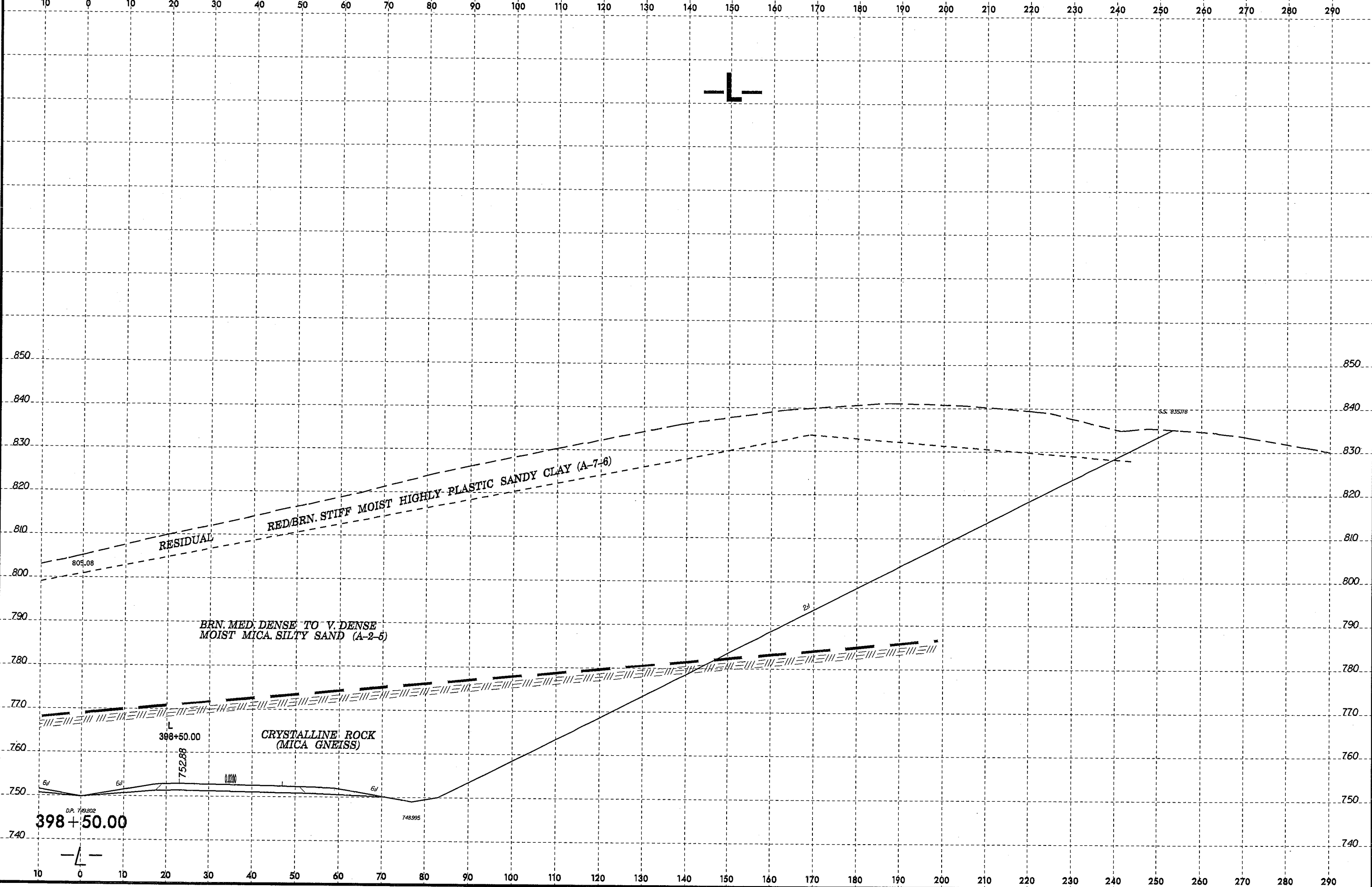


I:\4-MAY-2008 13:57  
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Author: AL BENZONIS

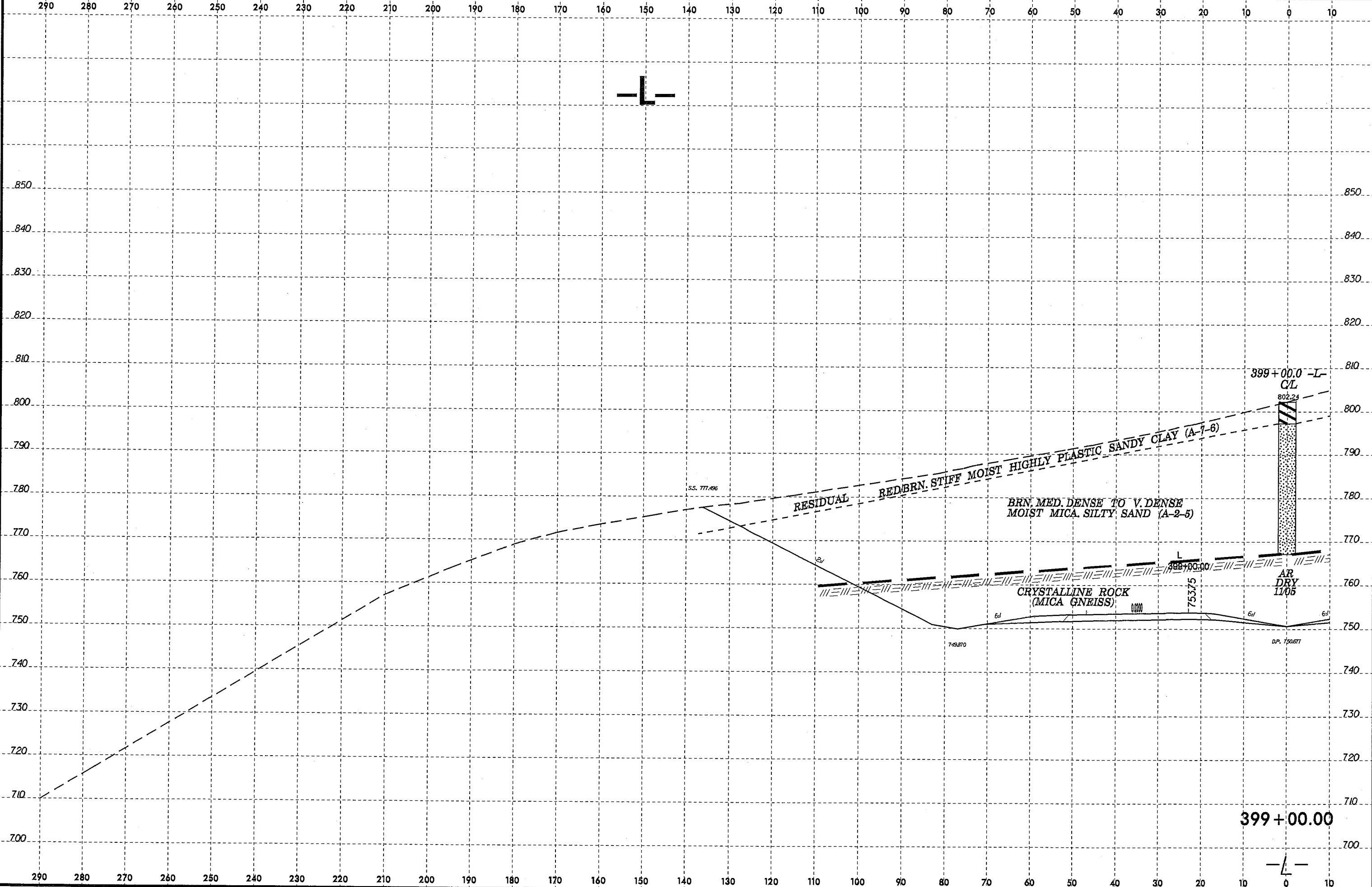
398+50.00



8/23/99  
14-MAY-2008 14:24  
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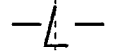


8/23/99

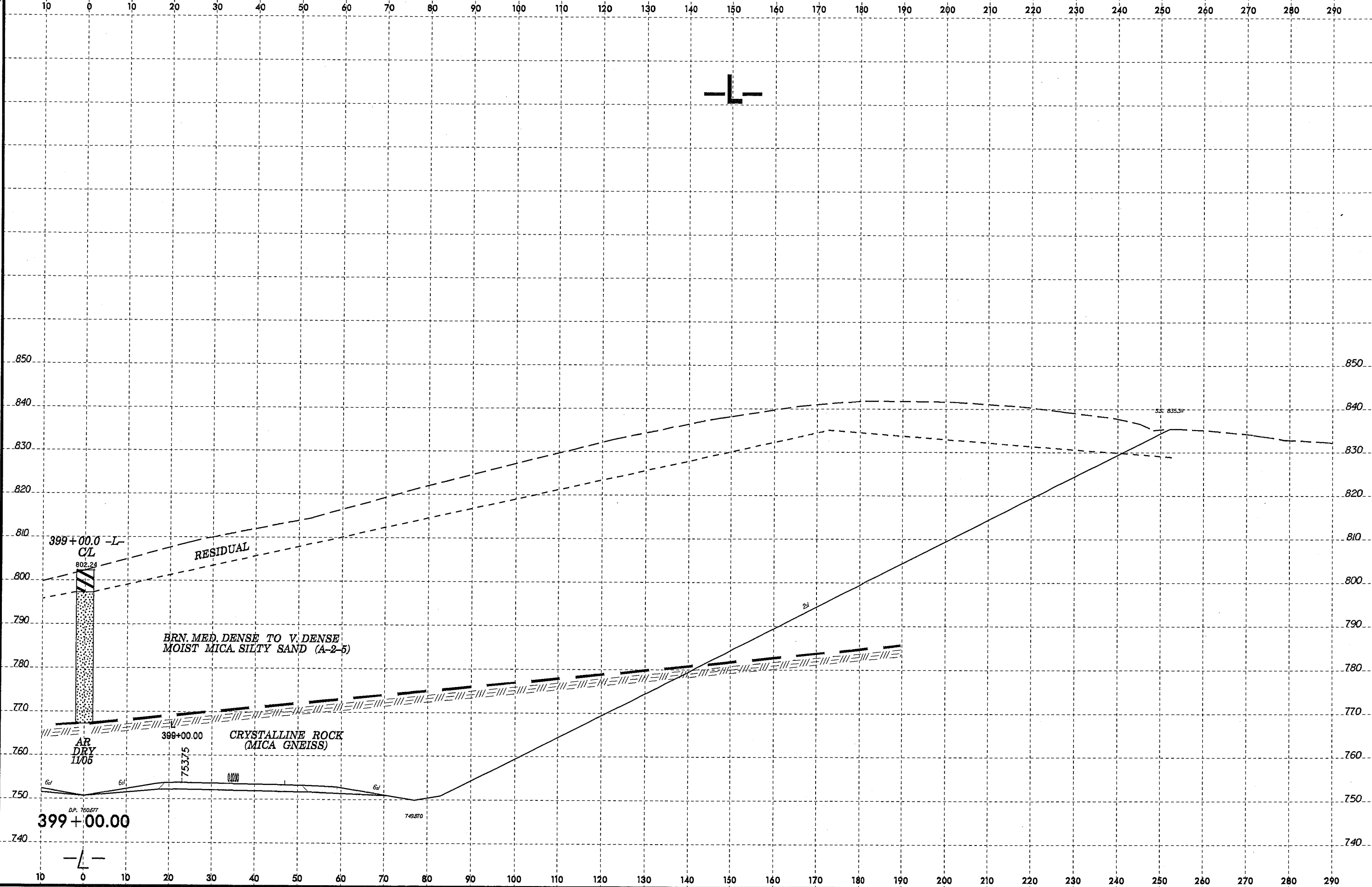


I:\MAY-2008\1547  
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 dburris AT 6/22/05

399+00.00

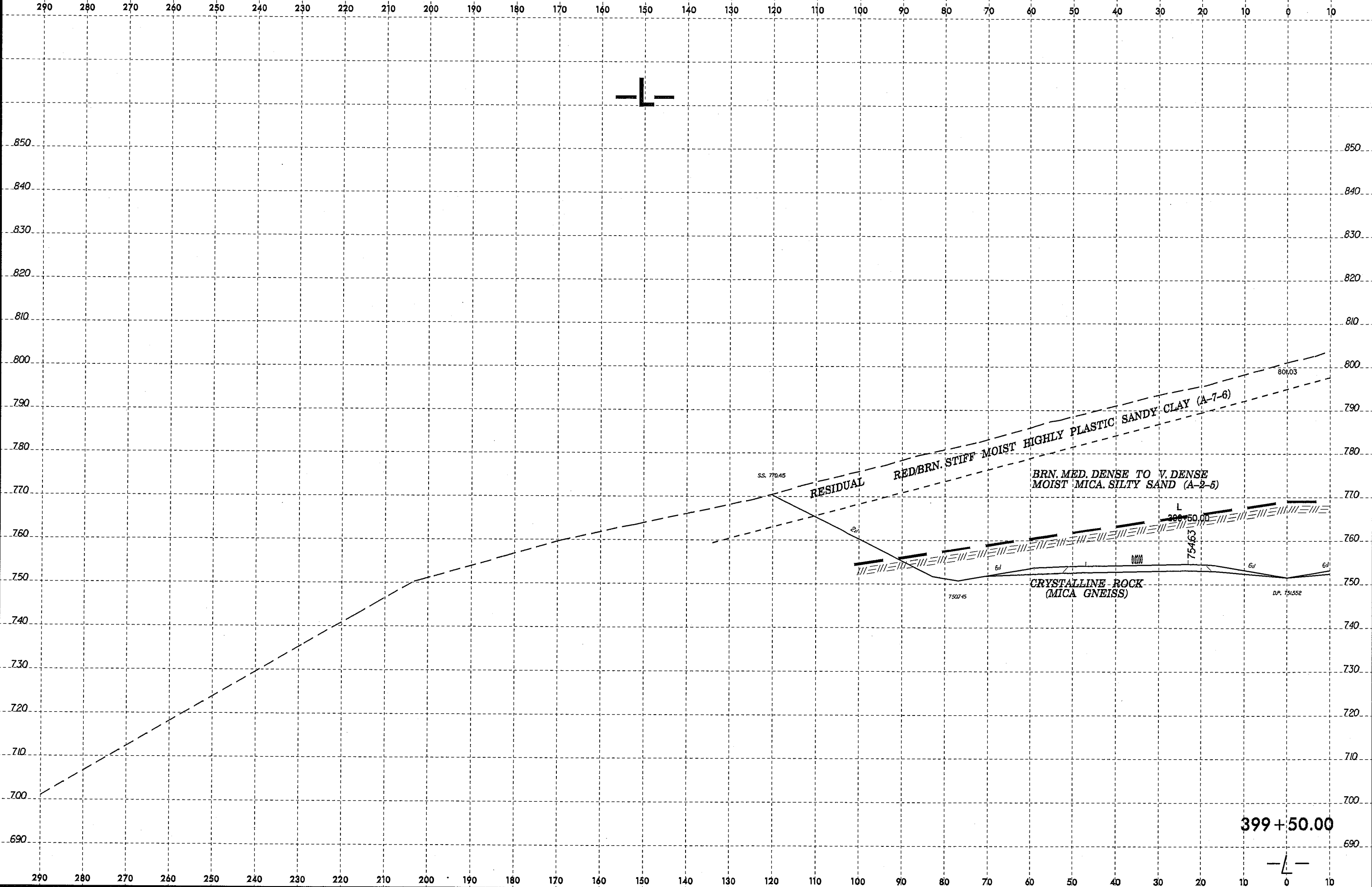


8/23/99



14-MAY-2008 14:55  
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 6423687

8/23/99

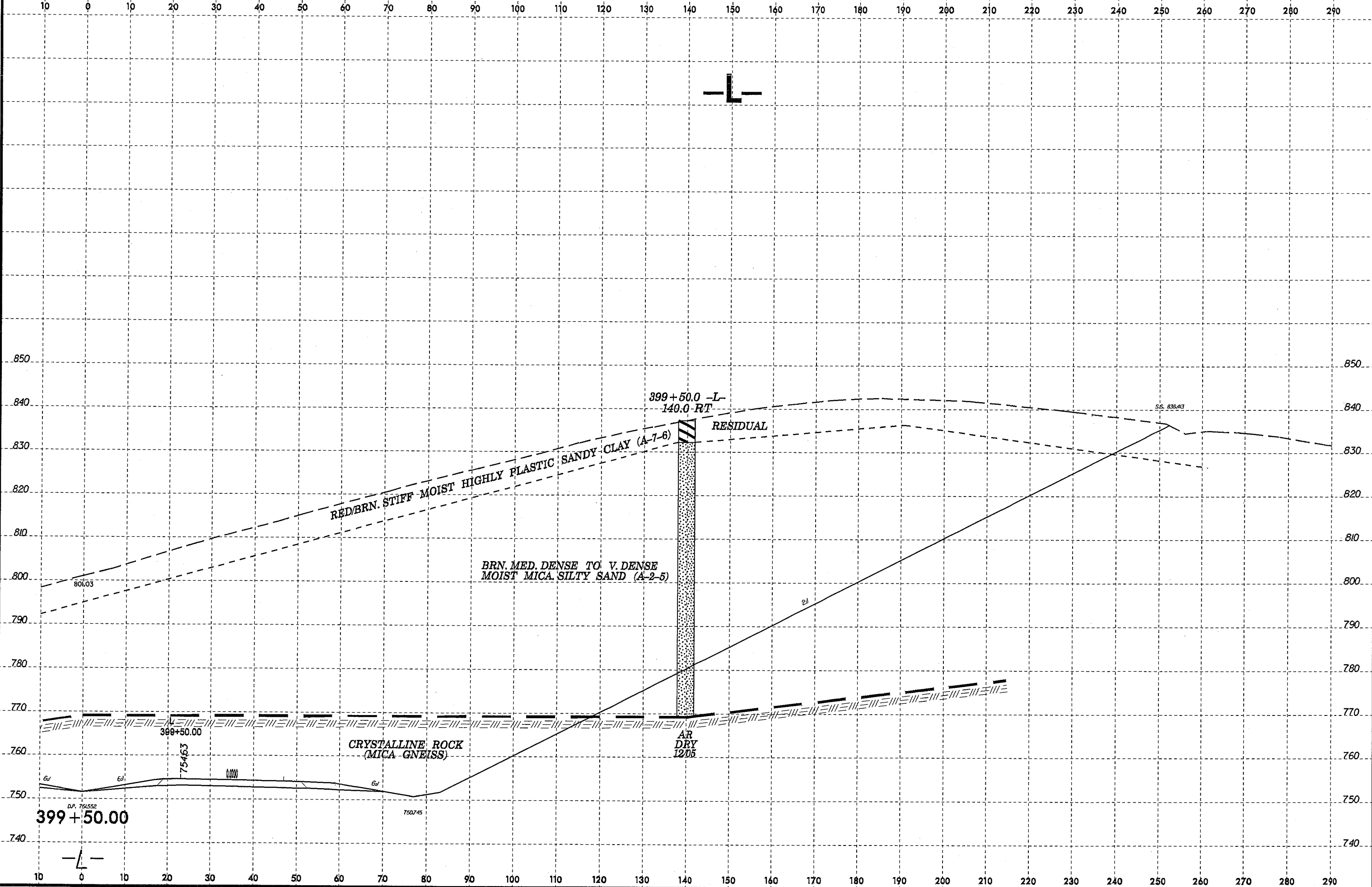


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 cburr13 AT 6/26/05

399+50.00

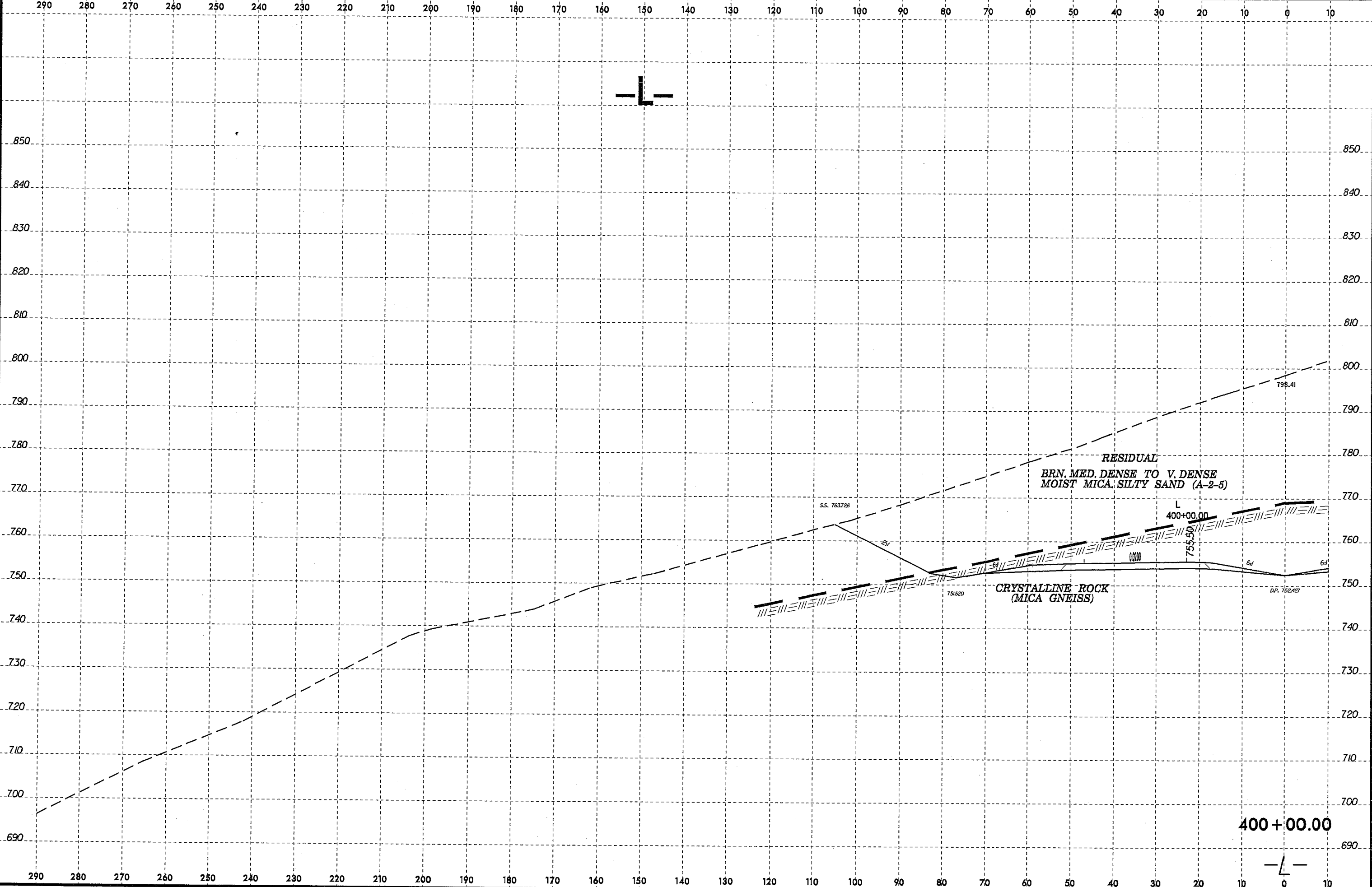


8/23/99



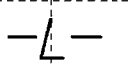
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8/23/99

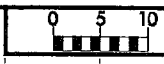


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8/23/99

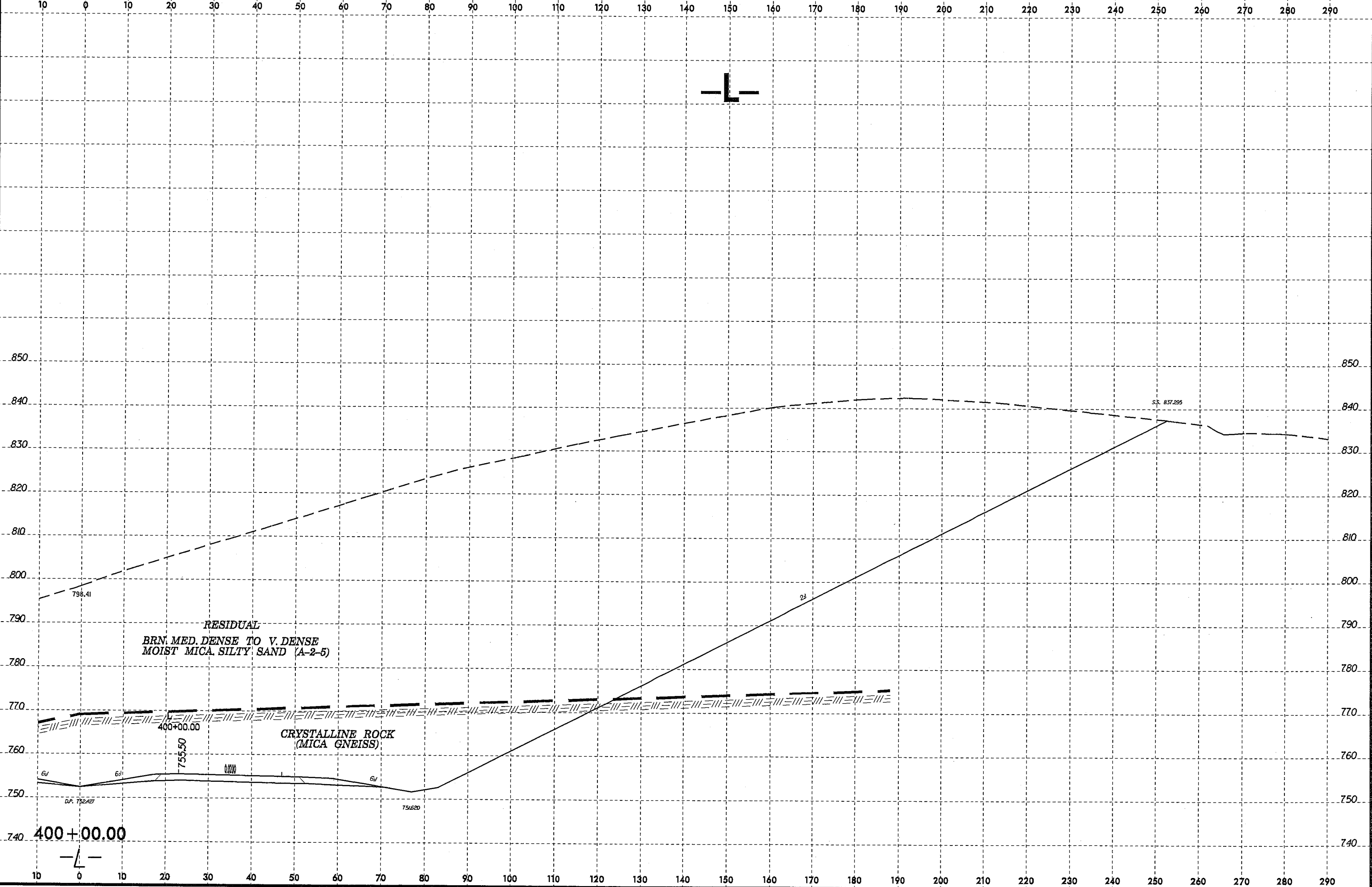
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8/23/99

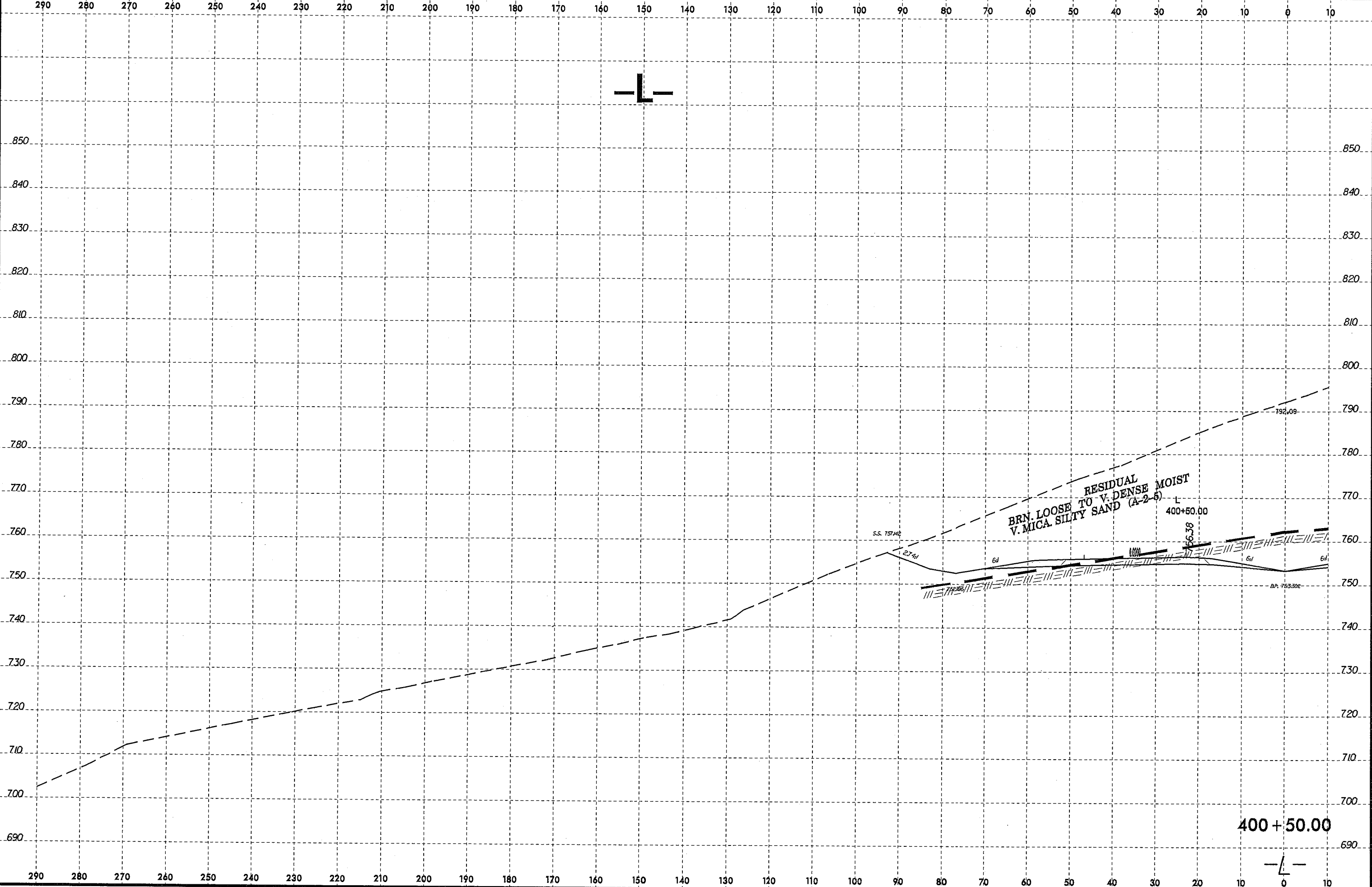


PROJ. REFERENCE NO. R-2707C	SHEET NO. 153
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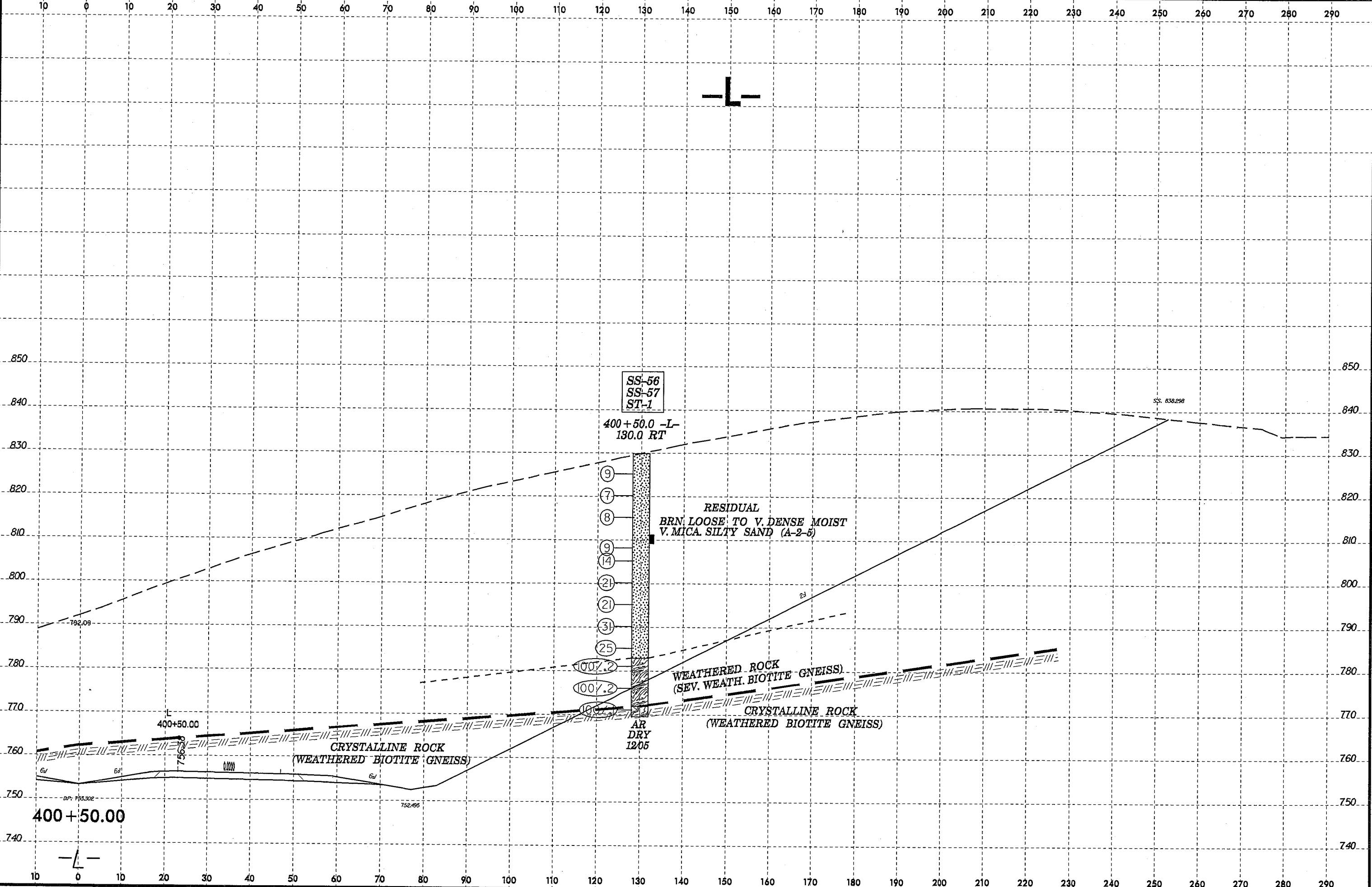
I:\MAY-2008 1427  
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 8/23/99 11:05:13 AM

8/23/99



14-MAY-2008 13:59  
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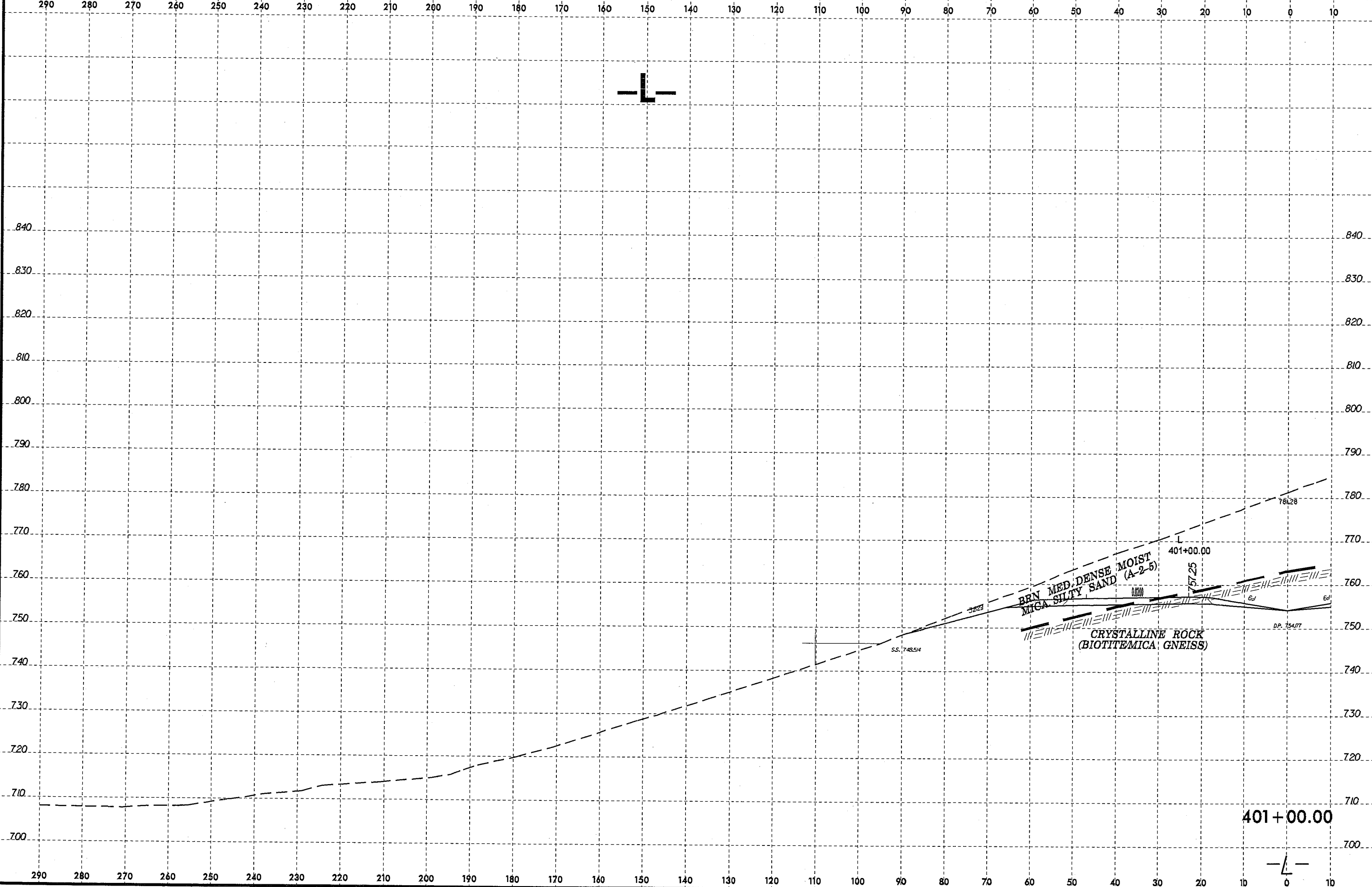
8/23/95



14-MAY-2008 14:28  
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 burris AT DENVER157

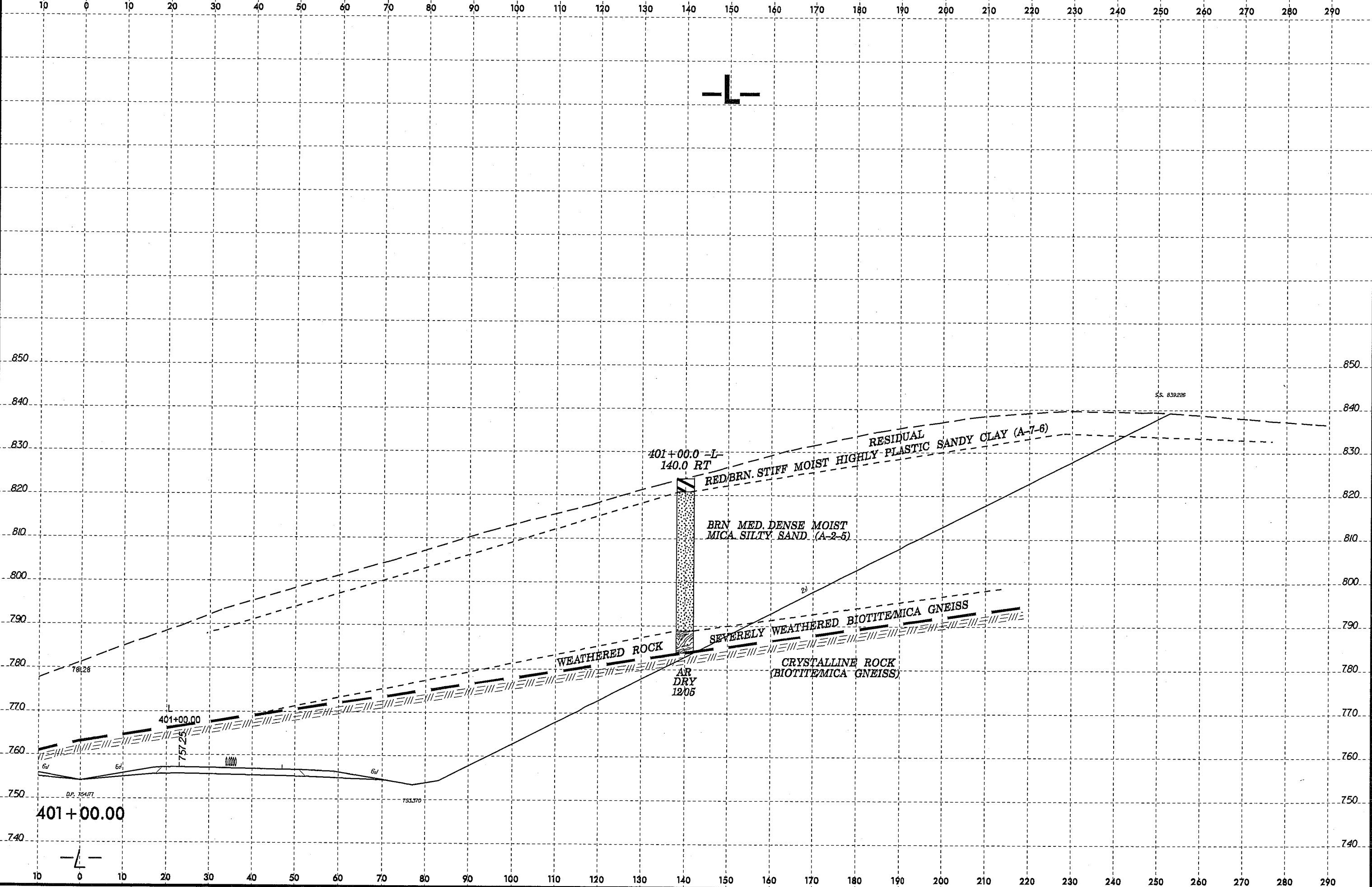
8/23/99

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 156
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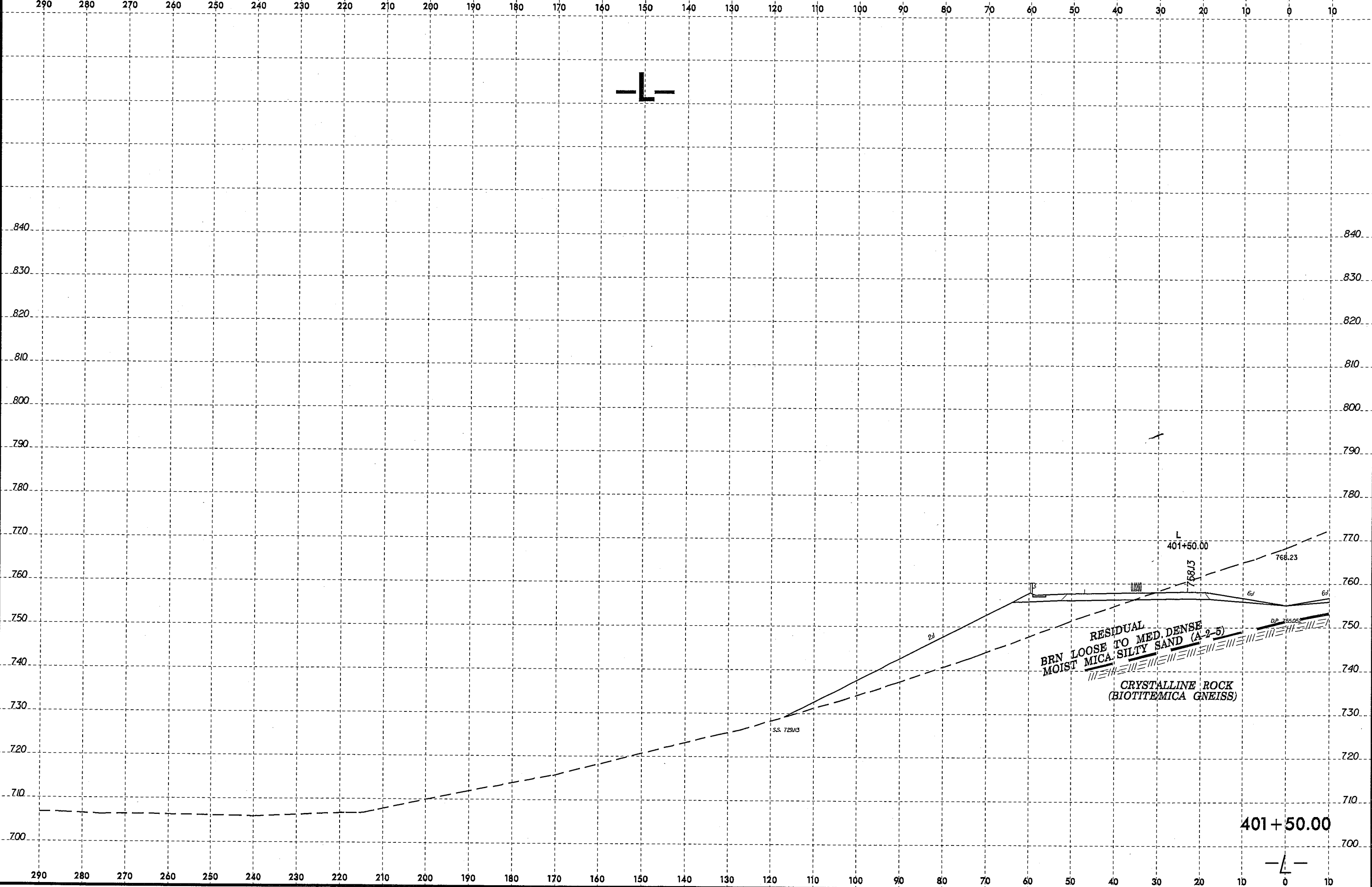
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 cburns AT 06/22/07

8/23/99



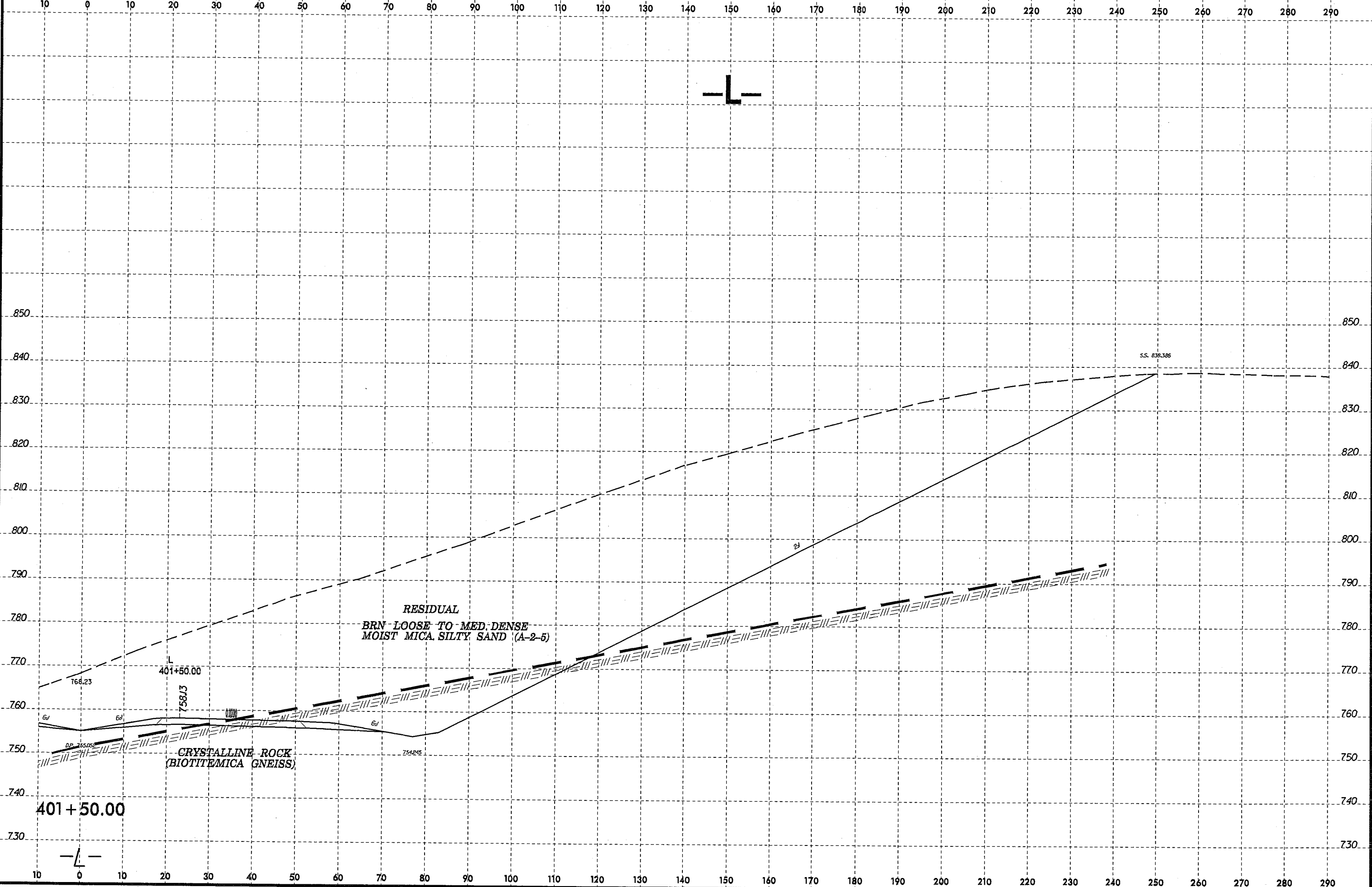
I:\MAY-2008 14:29  
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8/23/99  
14-MAY-2008 14:01  
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cburr3



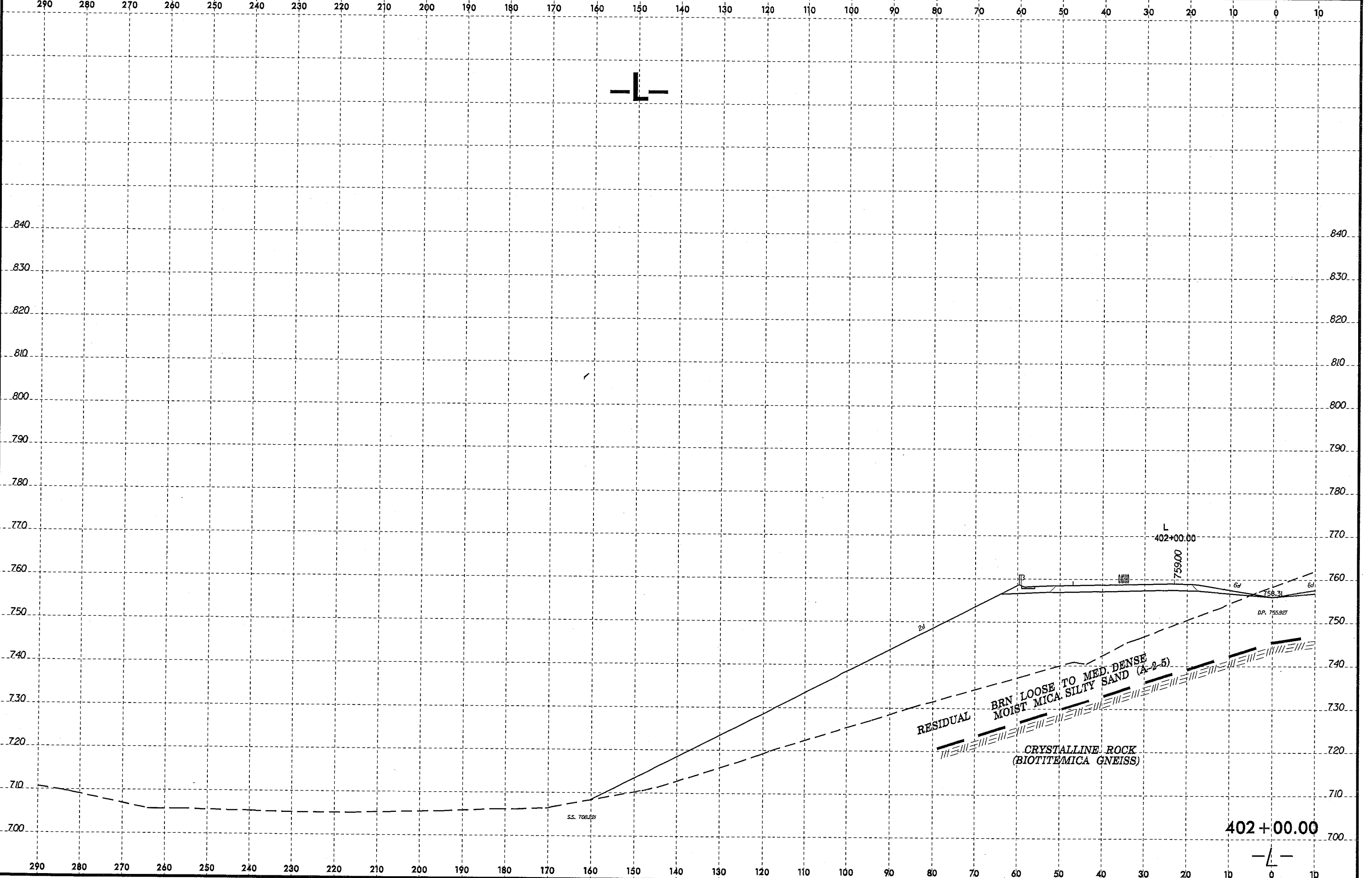


8/23/99



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 gburris AT BEH226187

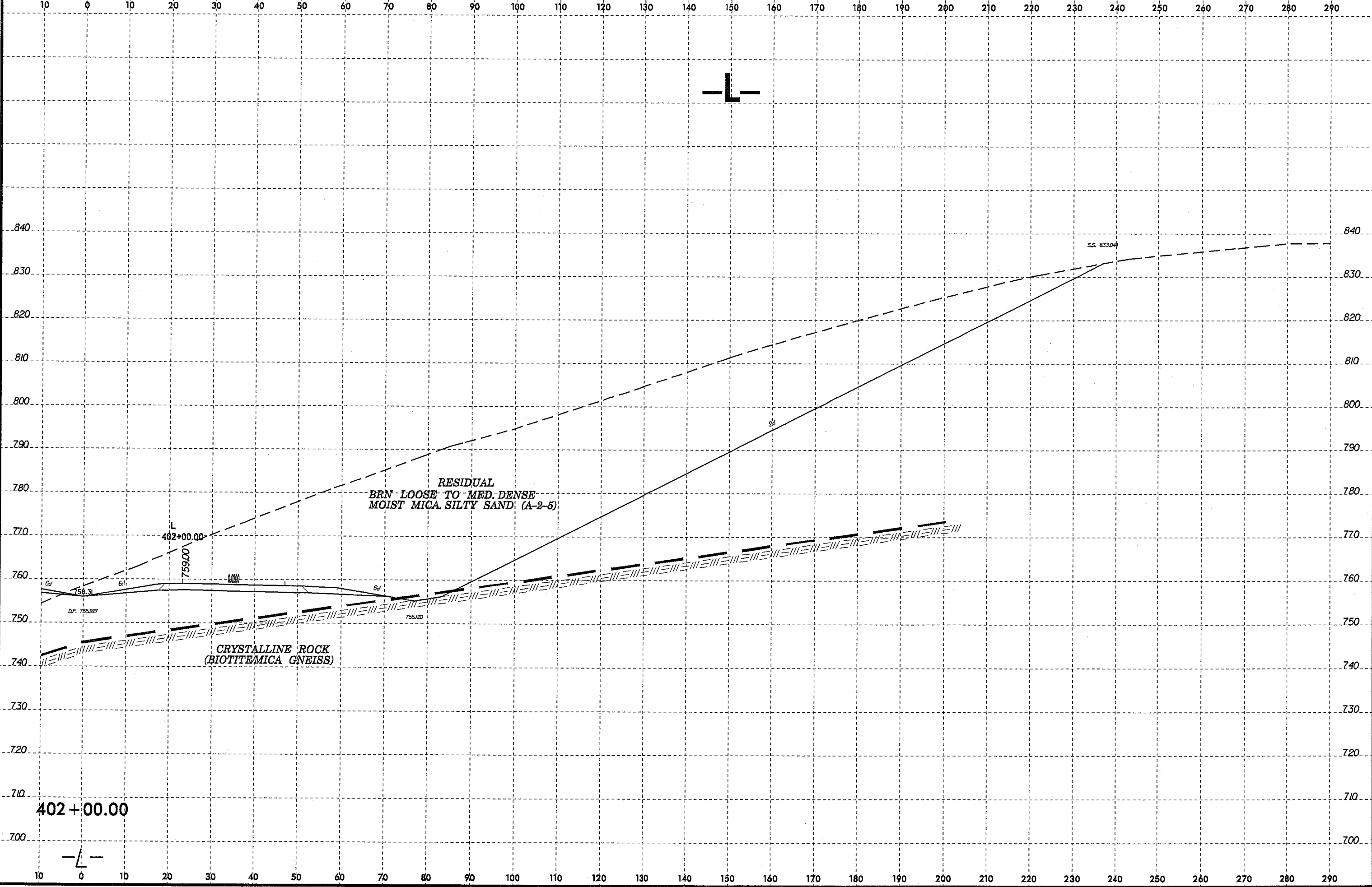
8/23/95



14-MAY-2008 14:02  
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 cburns AT 08/22/95

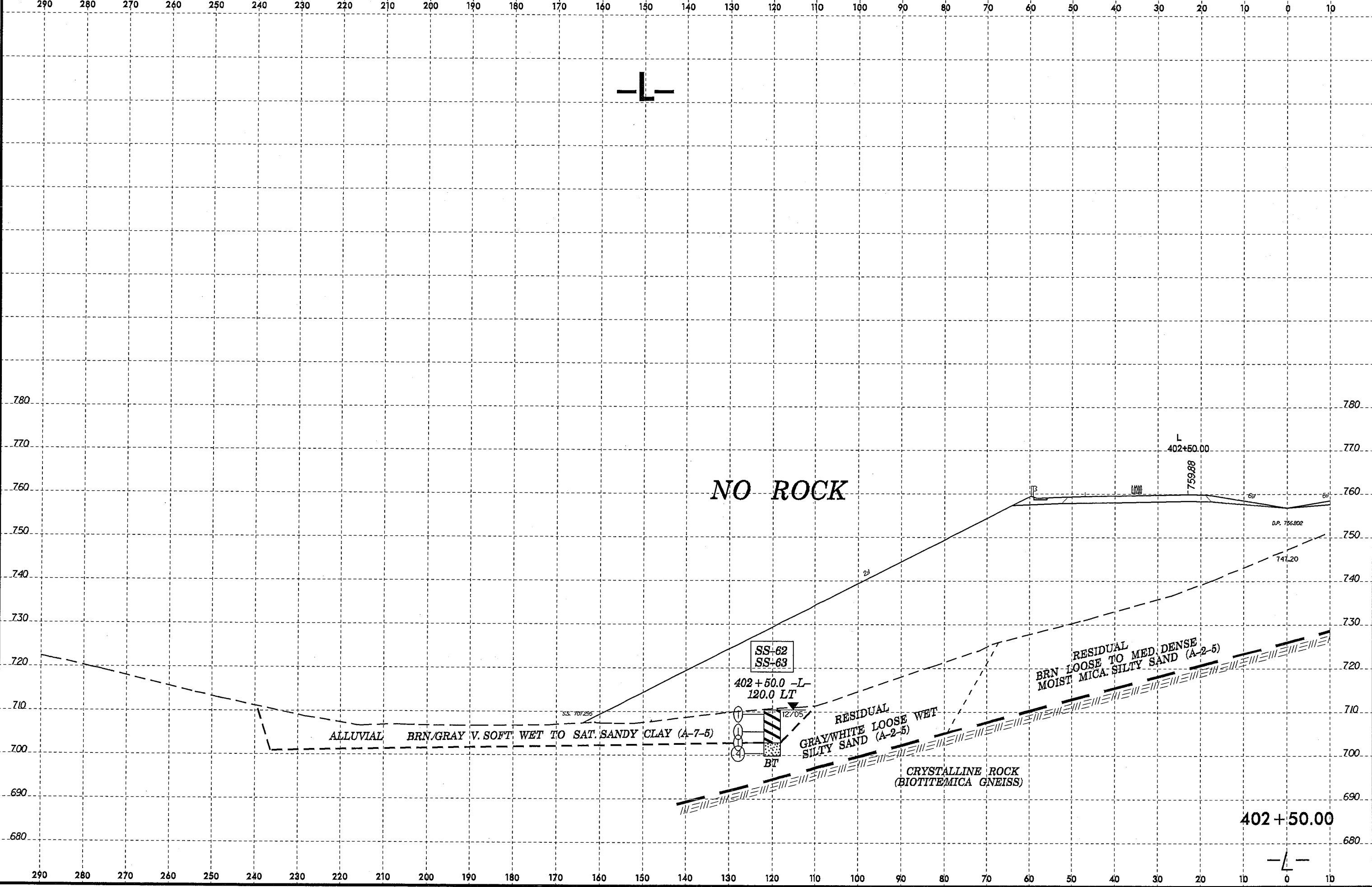
402+00.00

8/23/99



I:\MAY-2008 (43) \div\projects\2707\c\c\g\geo\_rdwj\_cleveland\oaddd\geotech\csc\2707\c\c\g\geo\_xsl.L.dgn

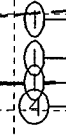
8/23/95  
14-MAY-2008 14:02  
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c:\proj\cleveland\voadd\geotech\ss\2707\rev\geo\_xst\_L.dgn



NO ROCK

SS-62  
SS-63

402+50.0 -L  
120.0 LT



ALLUVIAL BRN/GRAY V. SOFT WET TO SAT. SANDY CLAY (A-7-5)

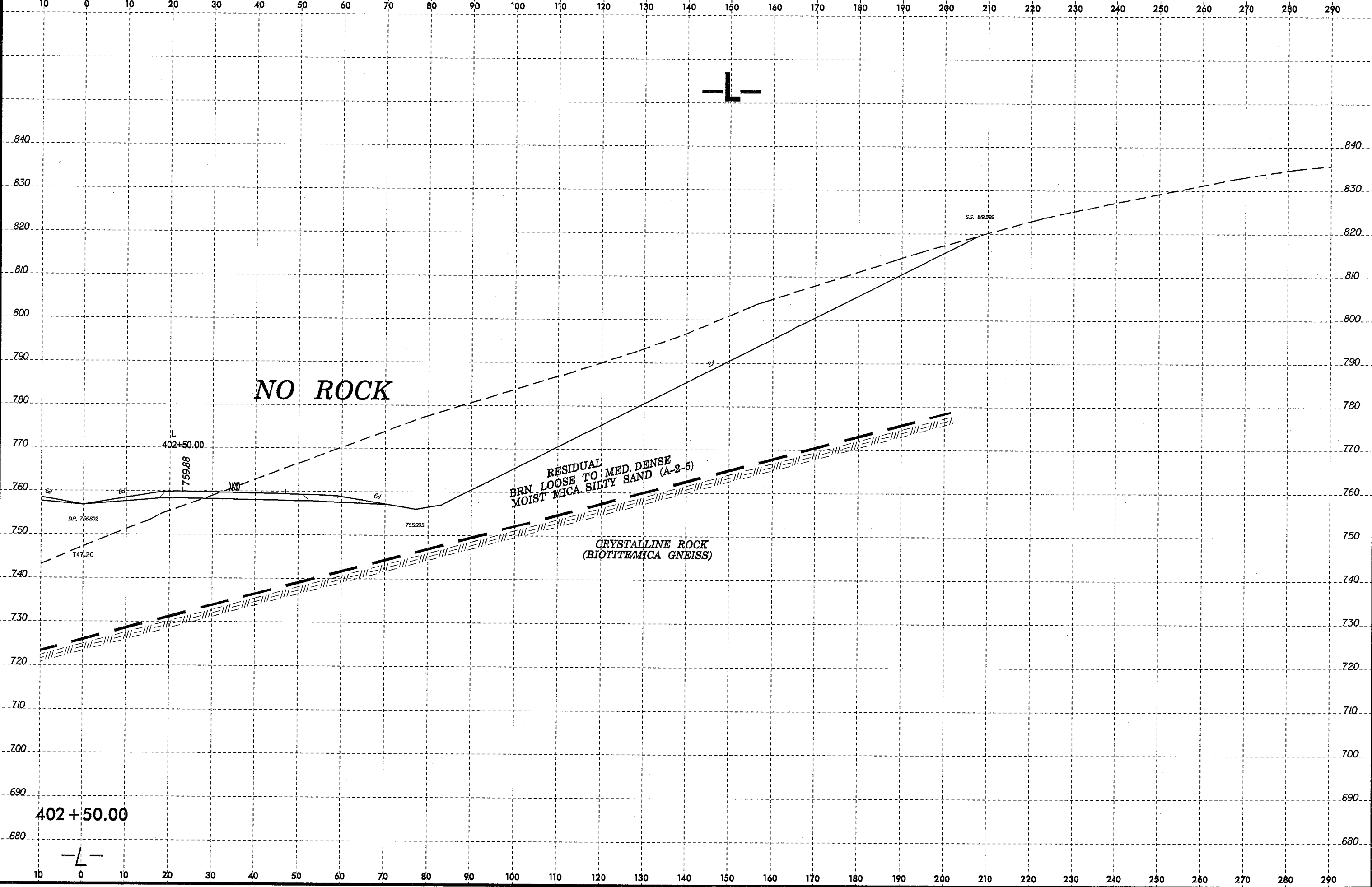
RESIDUAL GRAY/WHITE LOOSE WET SILTY SAND (A-2-5)

RESIDUAL BRN LOOSE TO MED. DENSE MOIST MICA SILTY SAND (A-2-5)

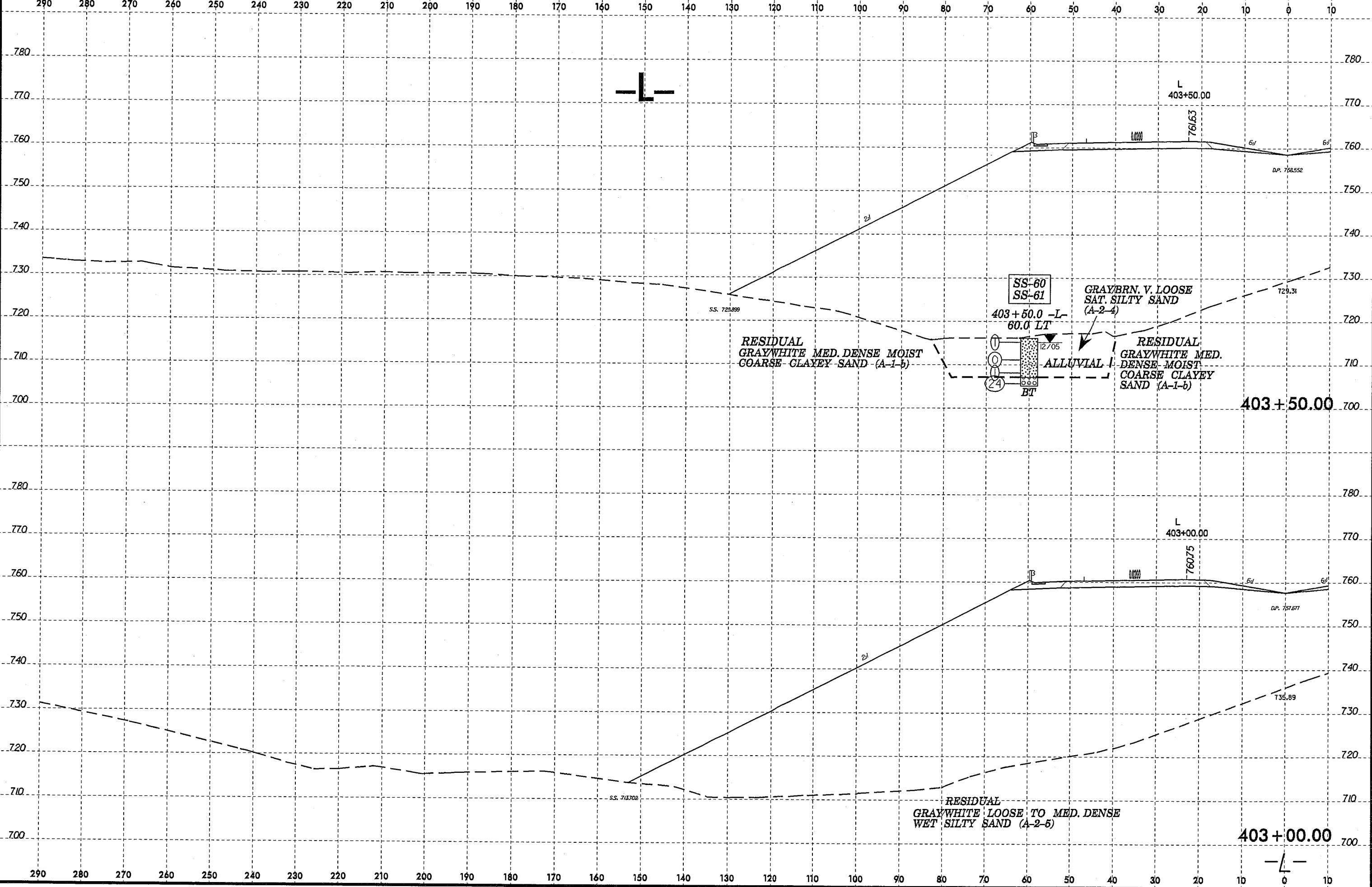
CRYSTALLINE ROCK (BIOTITE/MICA GNEISS)

402+50.00

8/23/95  
14-MAY-2008 14:33  
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c:\projects\2707c\rev\at\622517

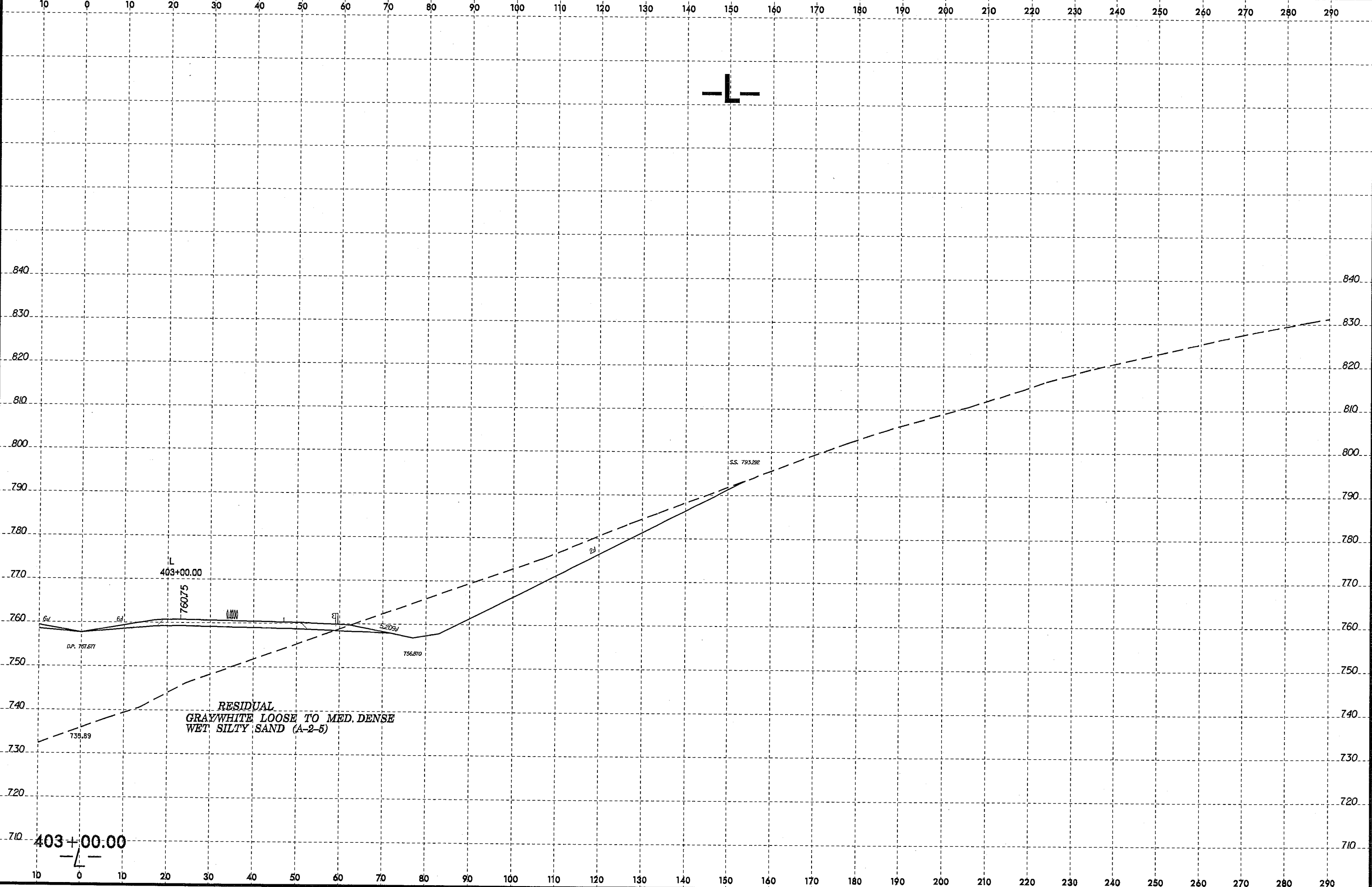


8/23/99



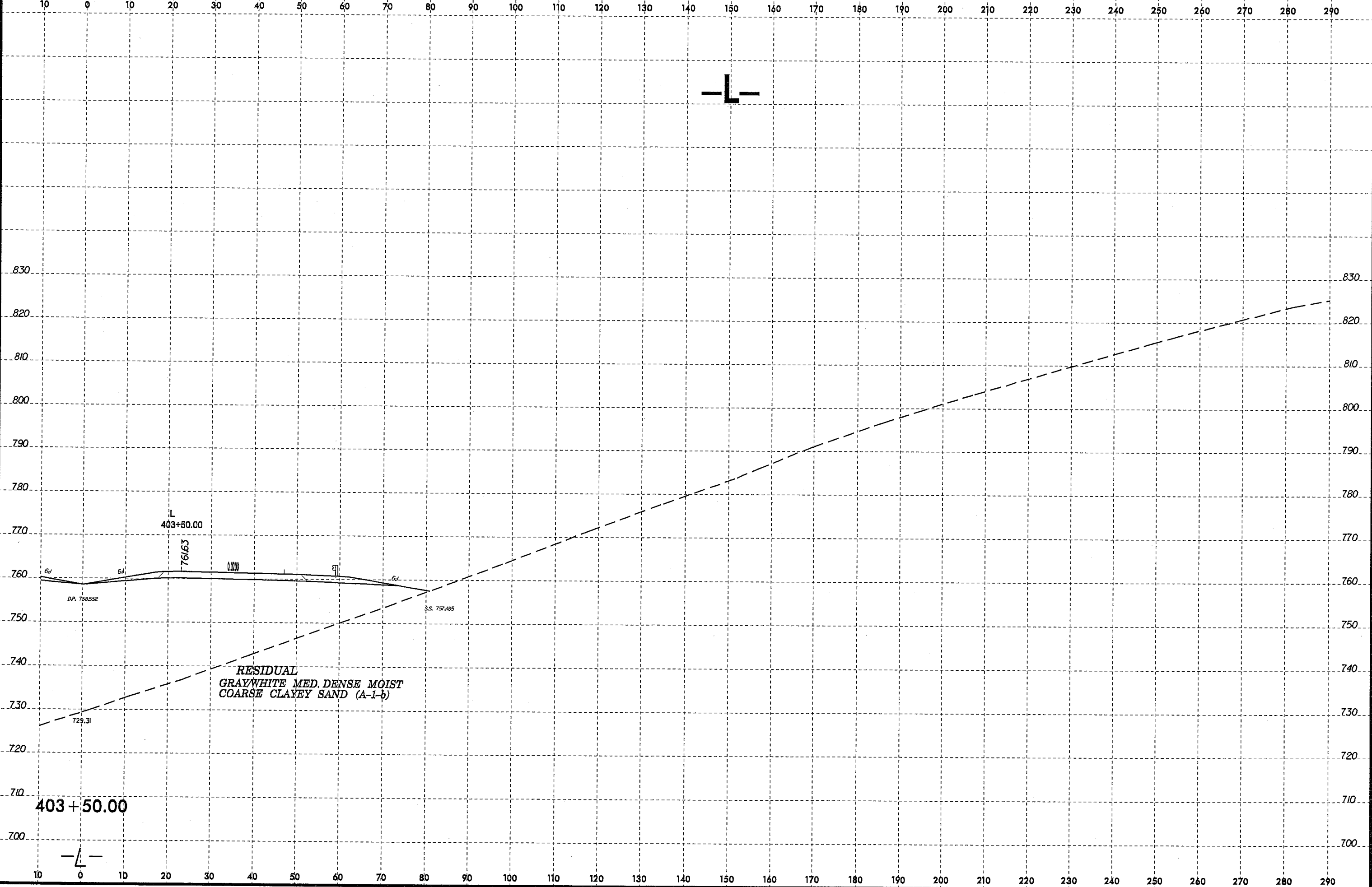
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 cburris AT GEH226187

8/23/99



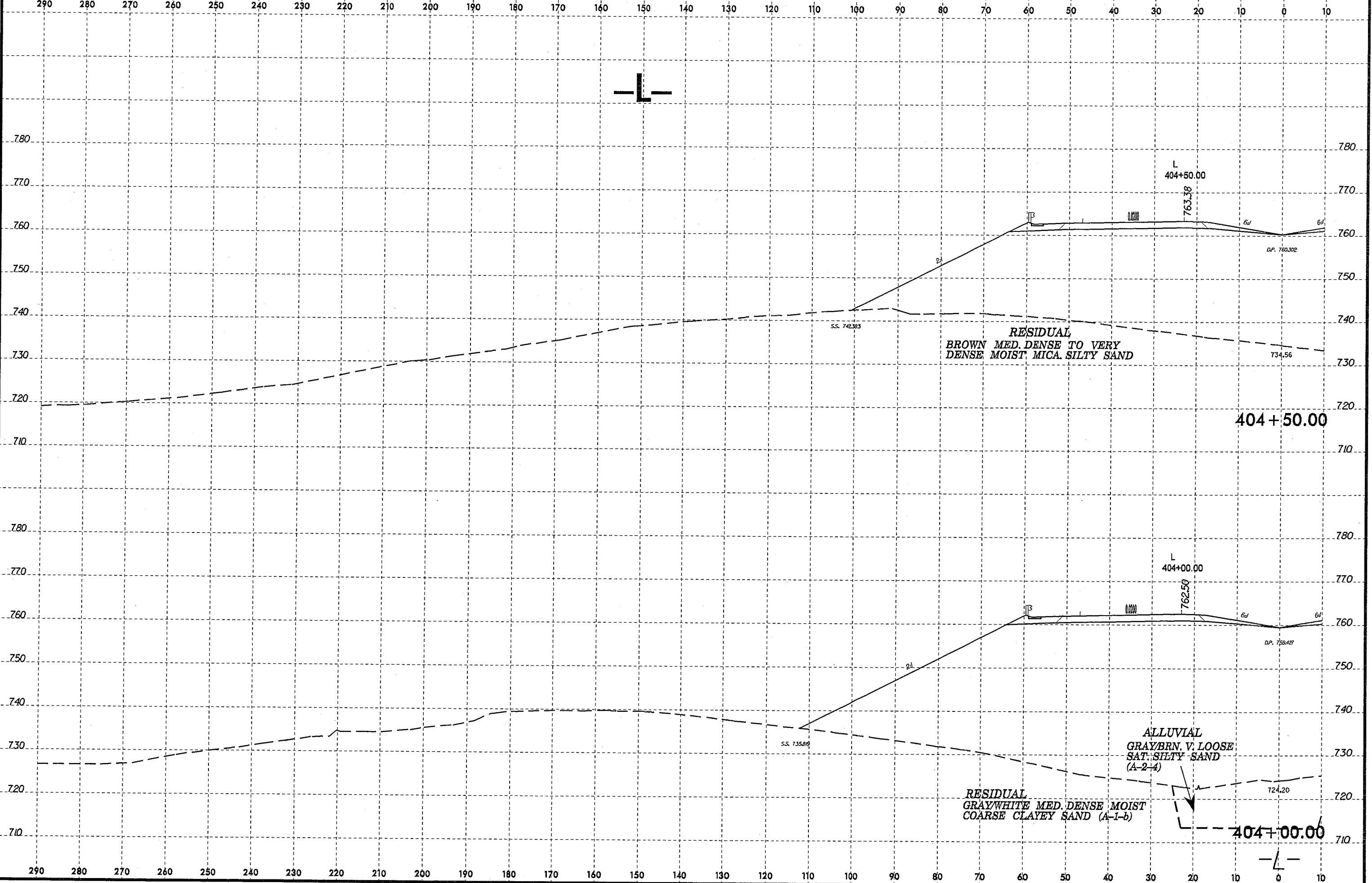
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8/23/95  
15-MAY-2008 15:14  
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AT: BEH226157





8/23/99

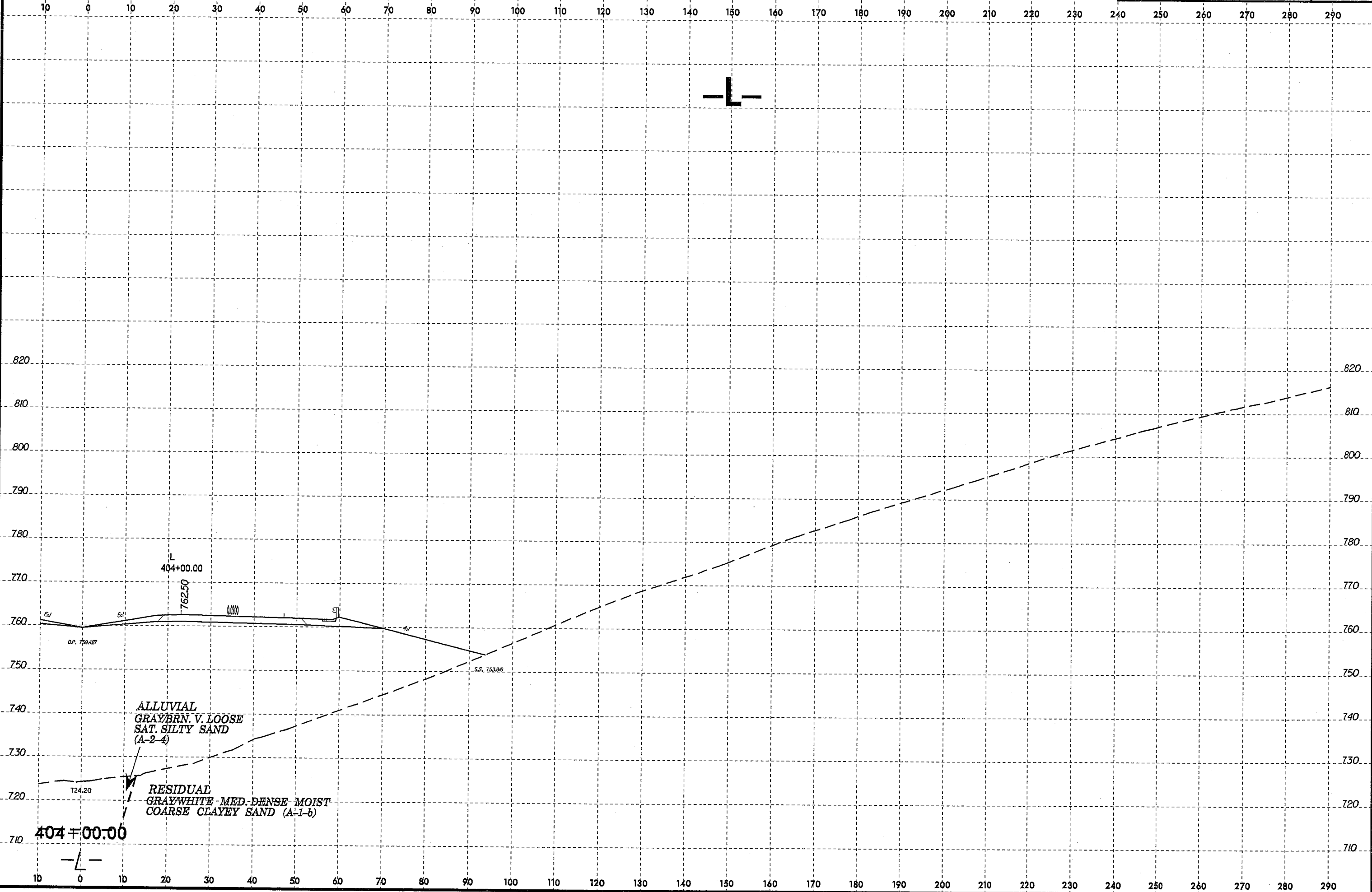


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cburns AL BEH28187

8/23/99



PROJ. REFERENCE NO. R-2707C	SHEET NO. 168
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14-MAY-2008 14:35  
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 dburris AT 08H26B7

404+00.00

ALLUVIAL  
 GRAY/BRN. V. LOOSE  
 SAT. SILTY SAND  
 (A-2-4)

RESIDUAL  
 GRAY/WHITE MED-DENSE MOIST  
 COARSE CLAYEY SAND (A-1-b)

404+00.00

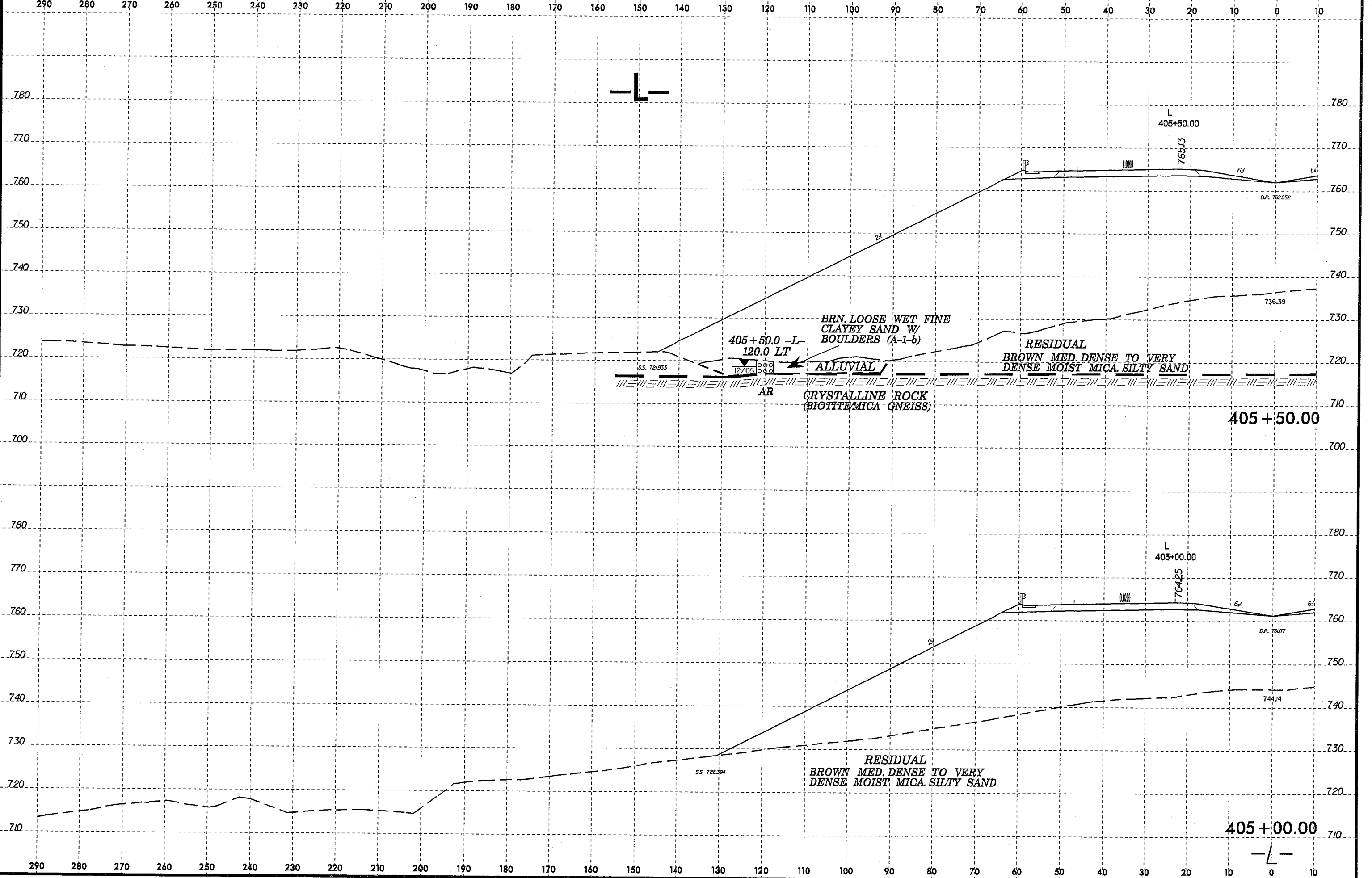
762.50

DP, 759.427

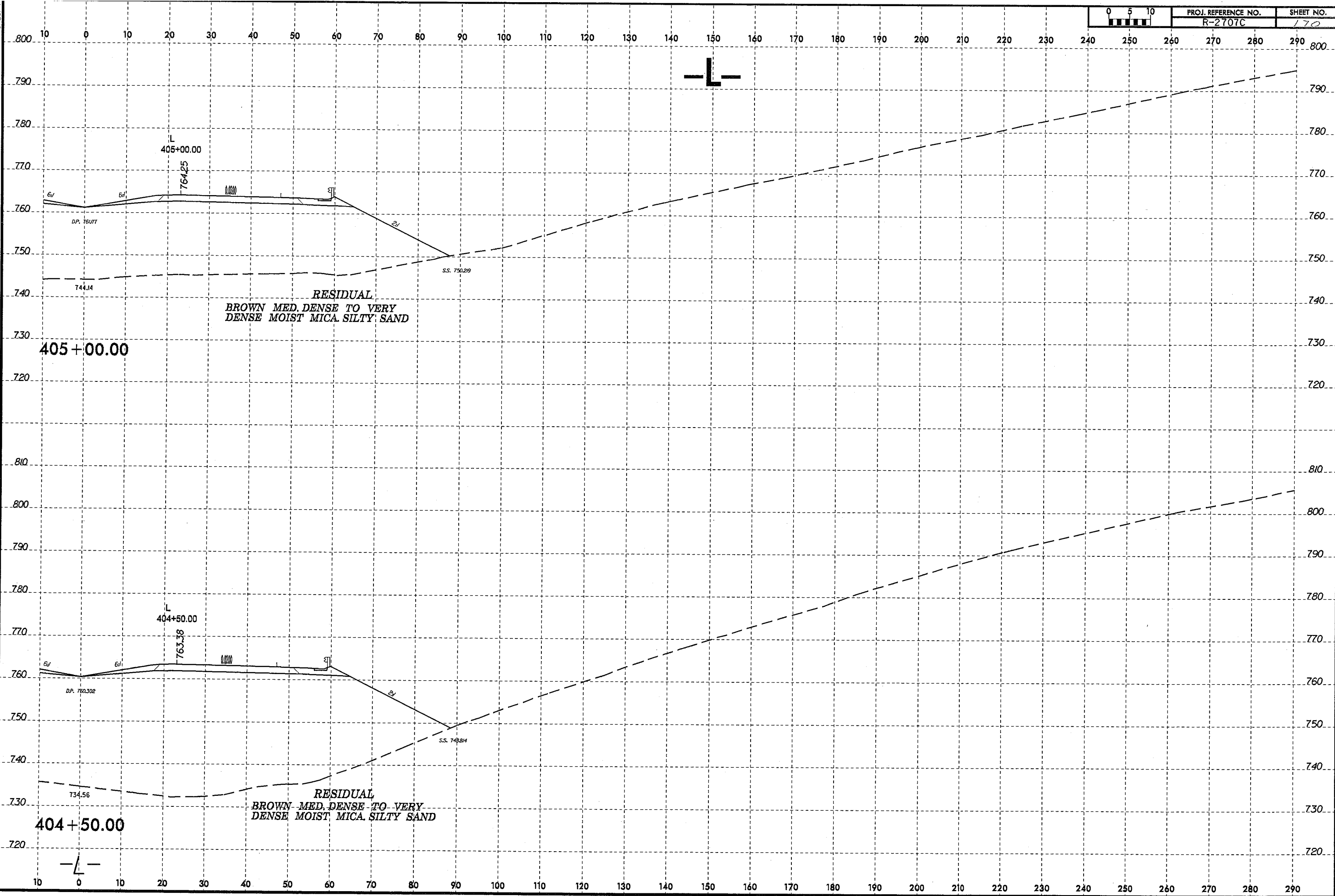
S.S. 75326

724.20

8/23/99

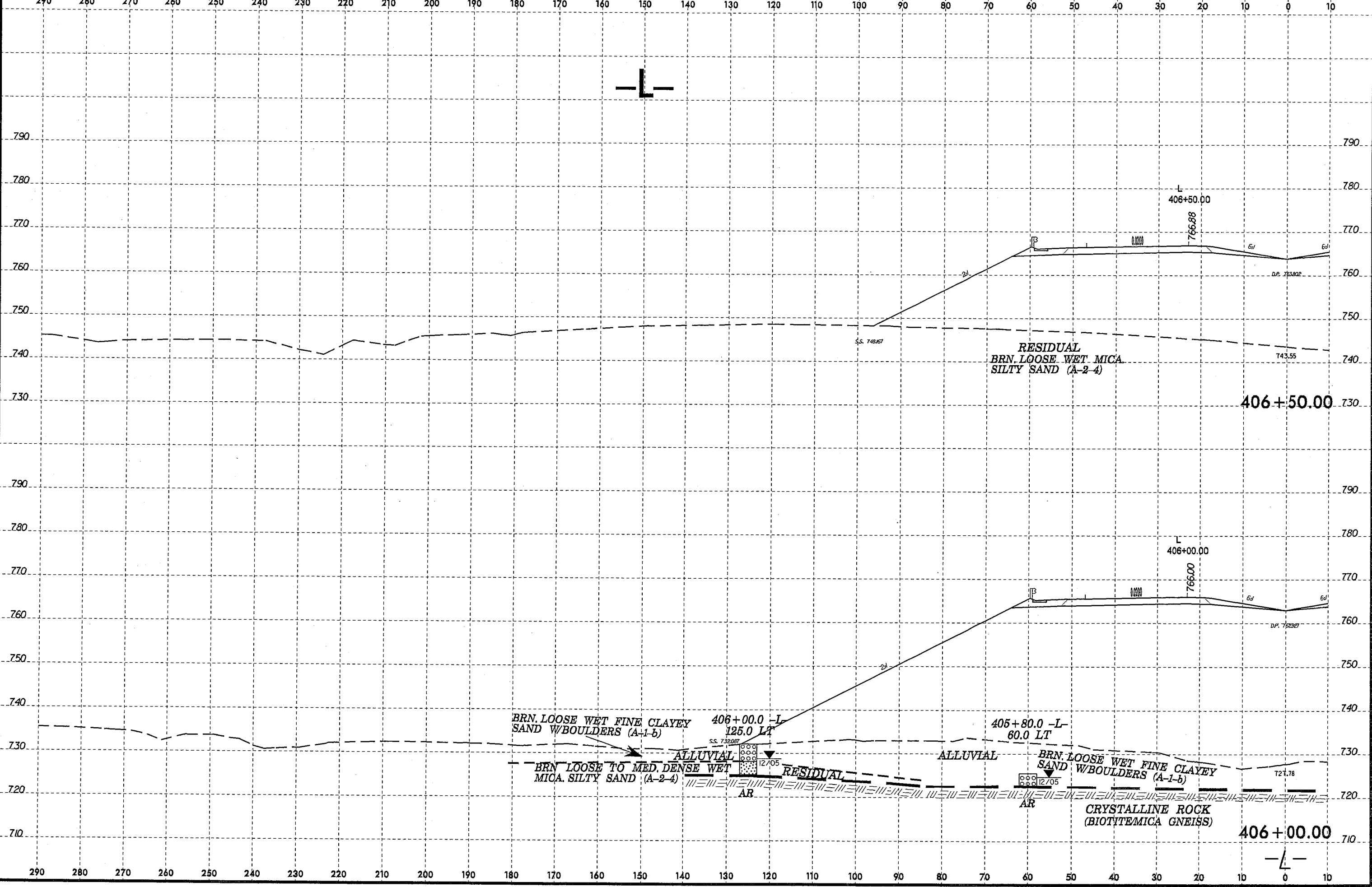


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sburns AL BEH226157



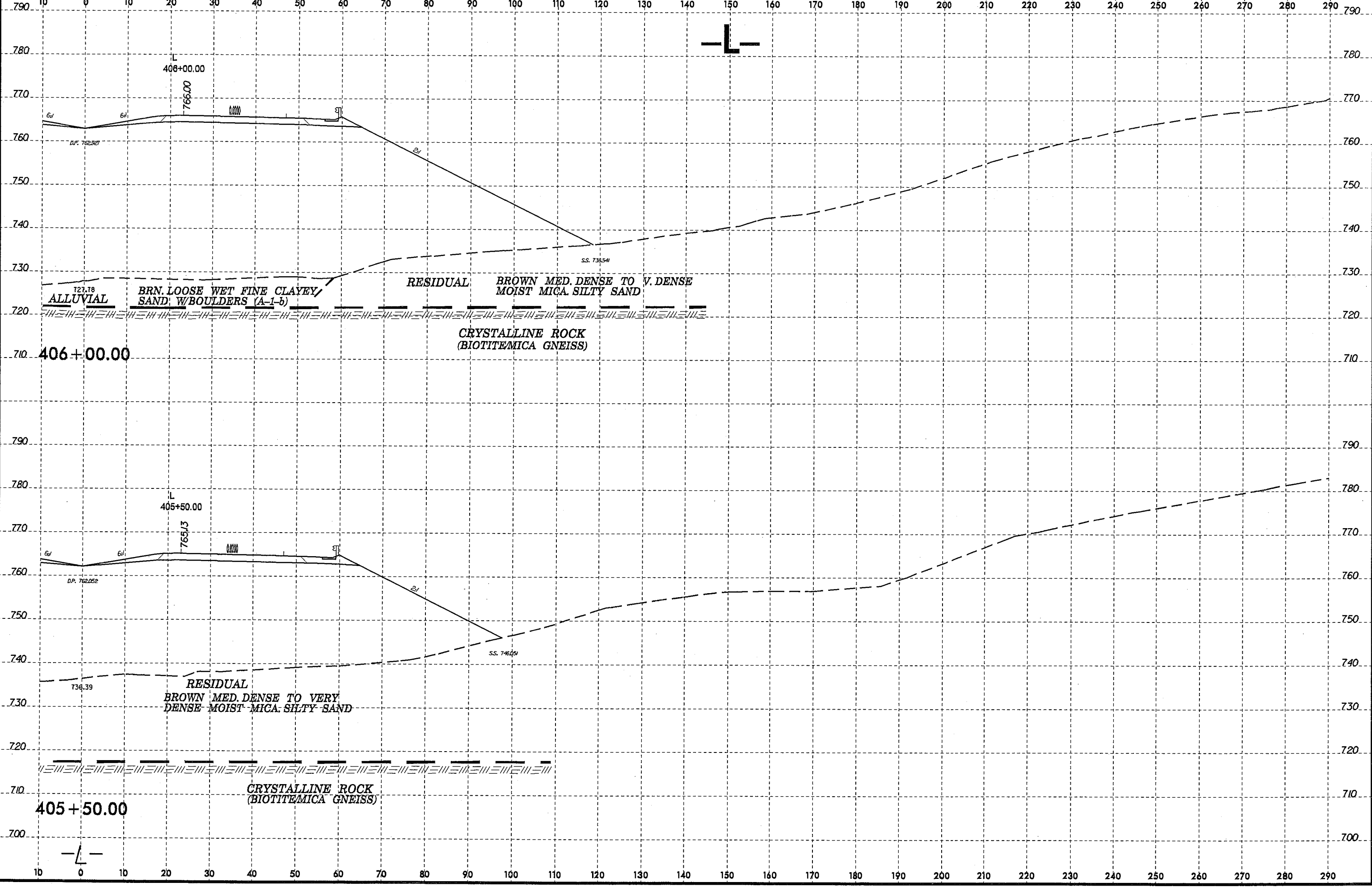
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8/23/06



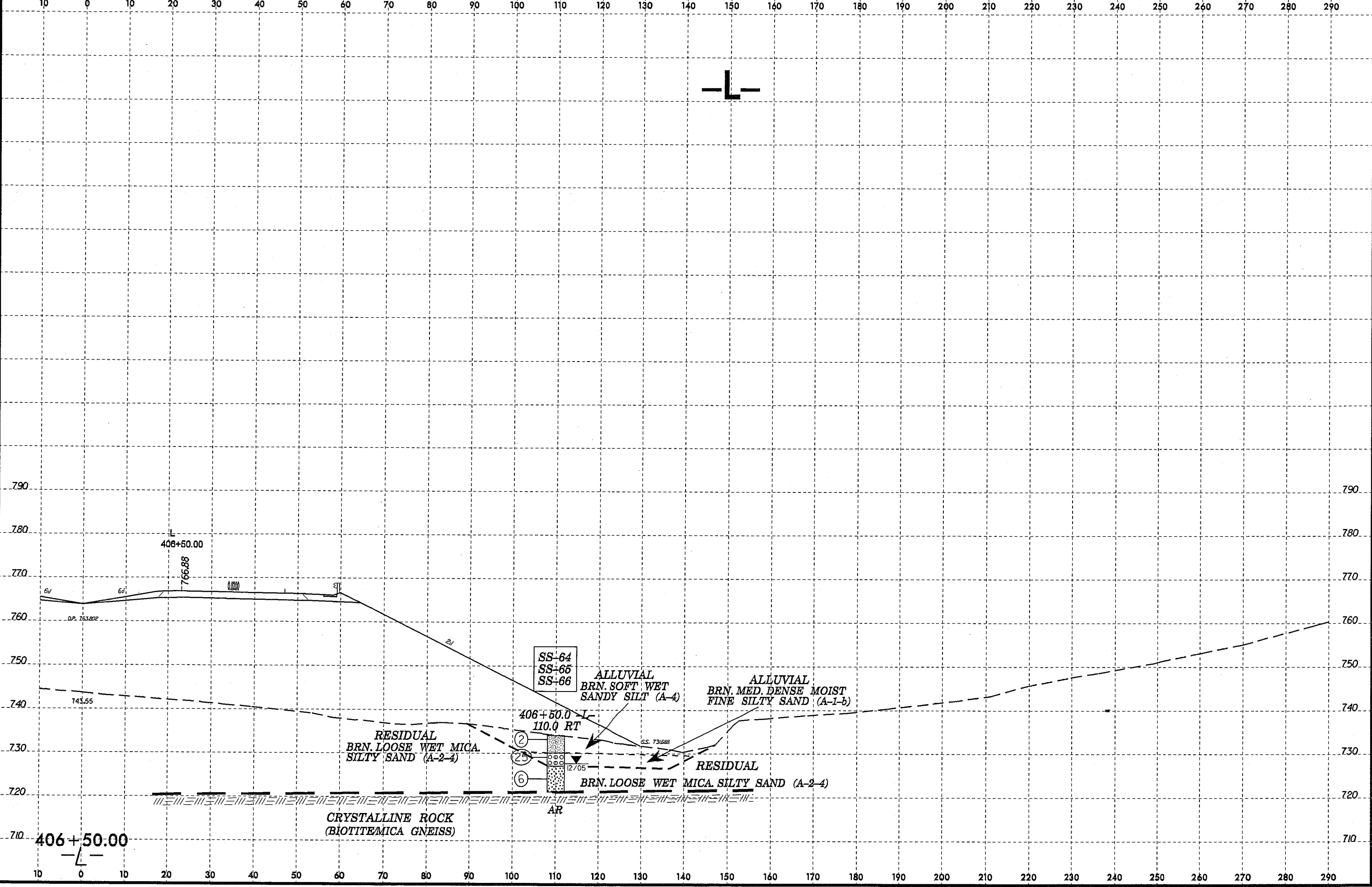
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8/23/98

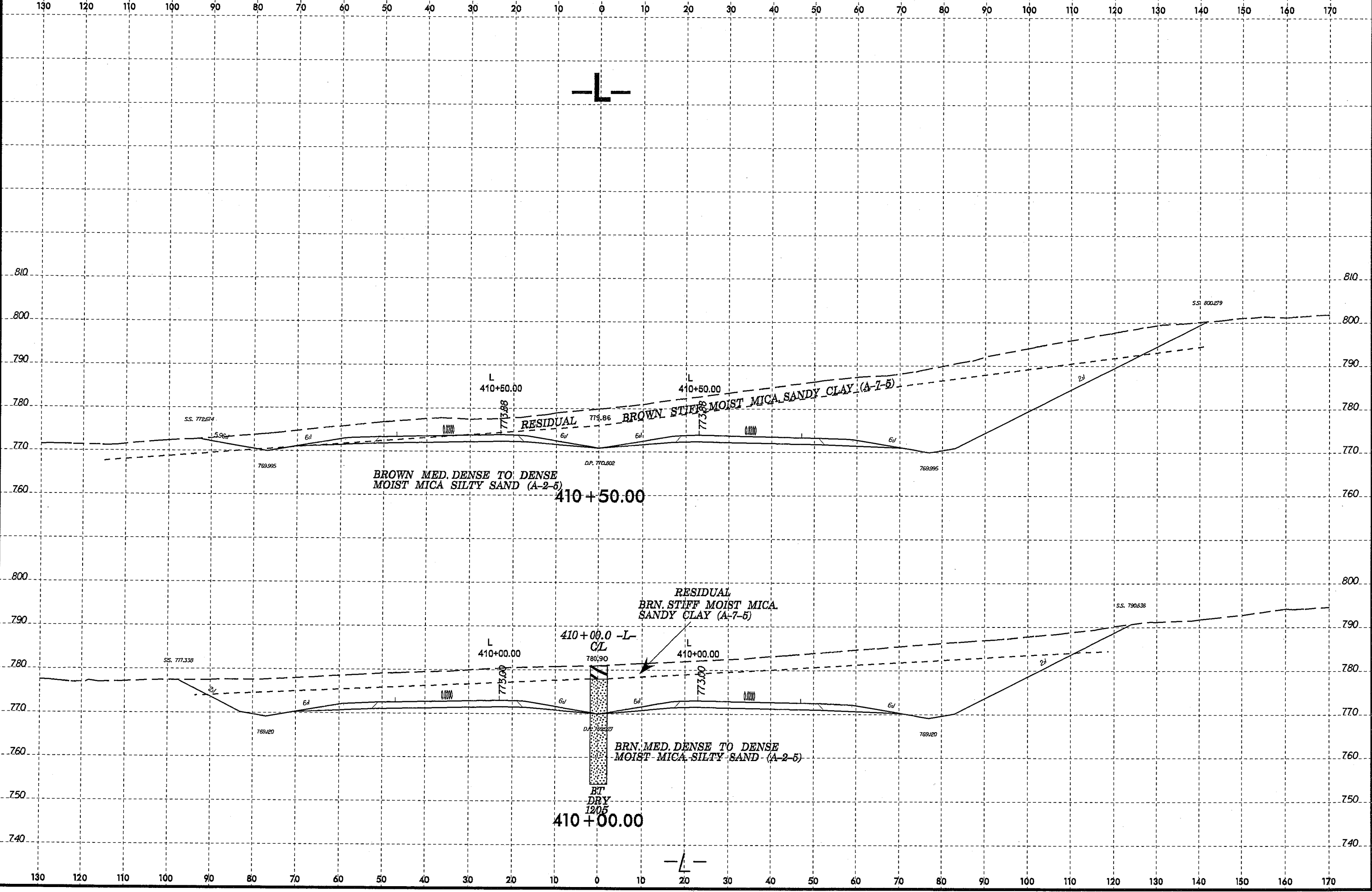


15-MAY-2008 15:28  
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cburris AT BEH226157

8/23/95  
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c:\projects\2707\rev\geo\_rdw\cleveland\cadd\geotech\sec\2707\rev\geo\_xsl.l.dgn



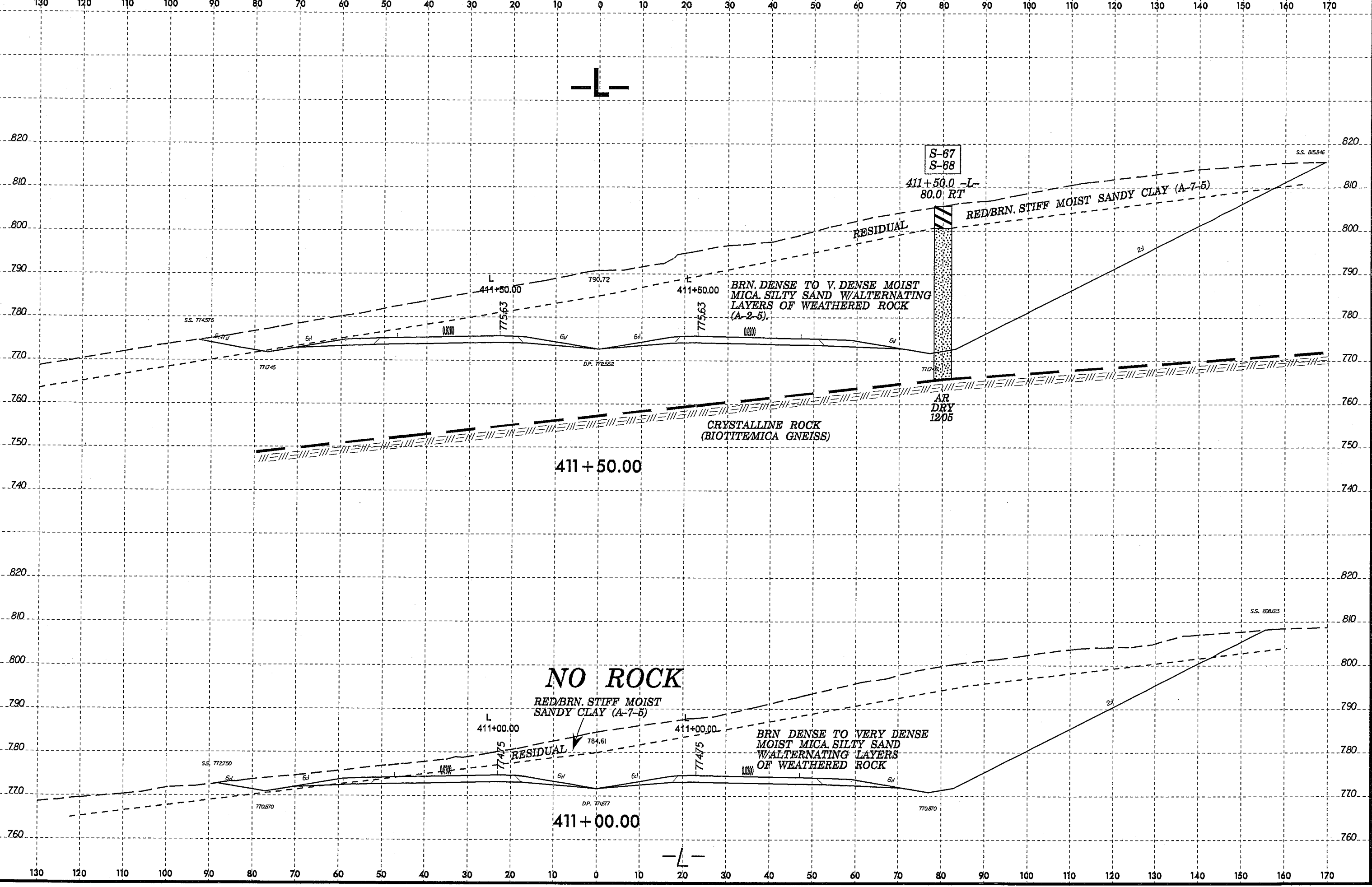
8/23/05



14-MAY-2008 14:41  
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 cburris AT BEH226157

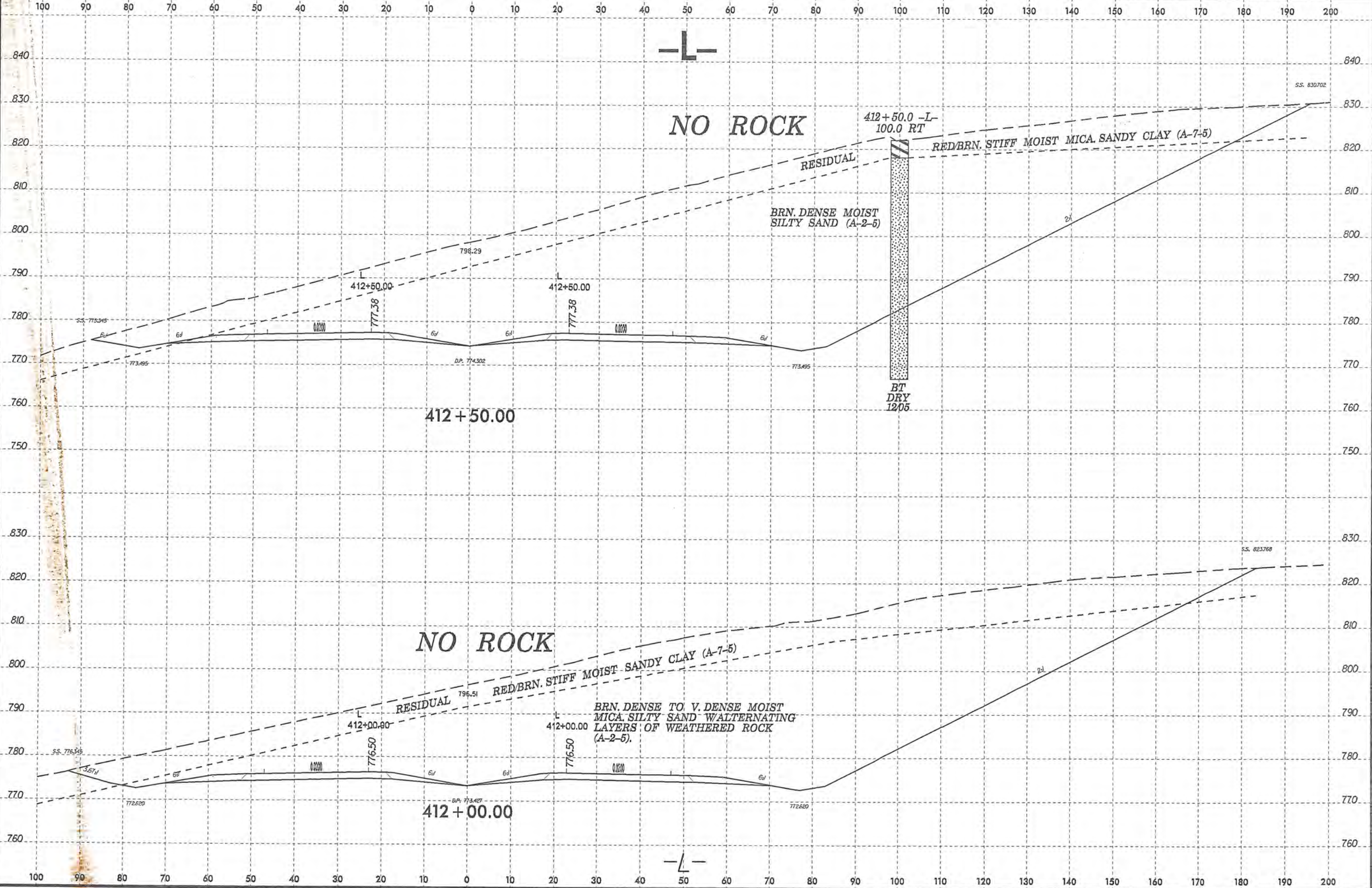


8/23/99



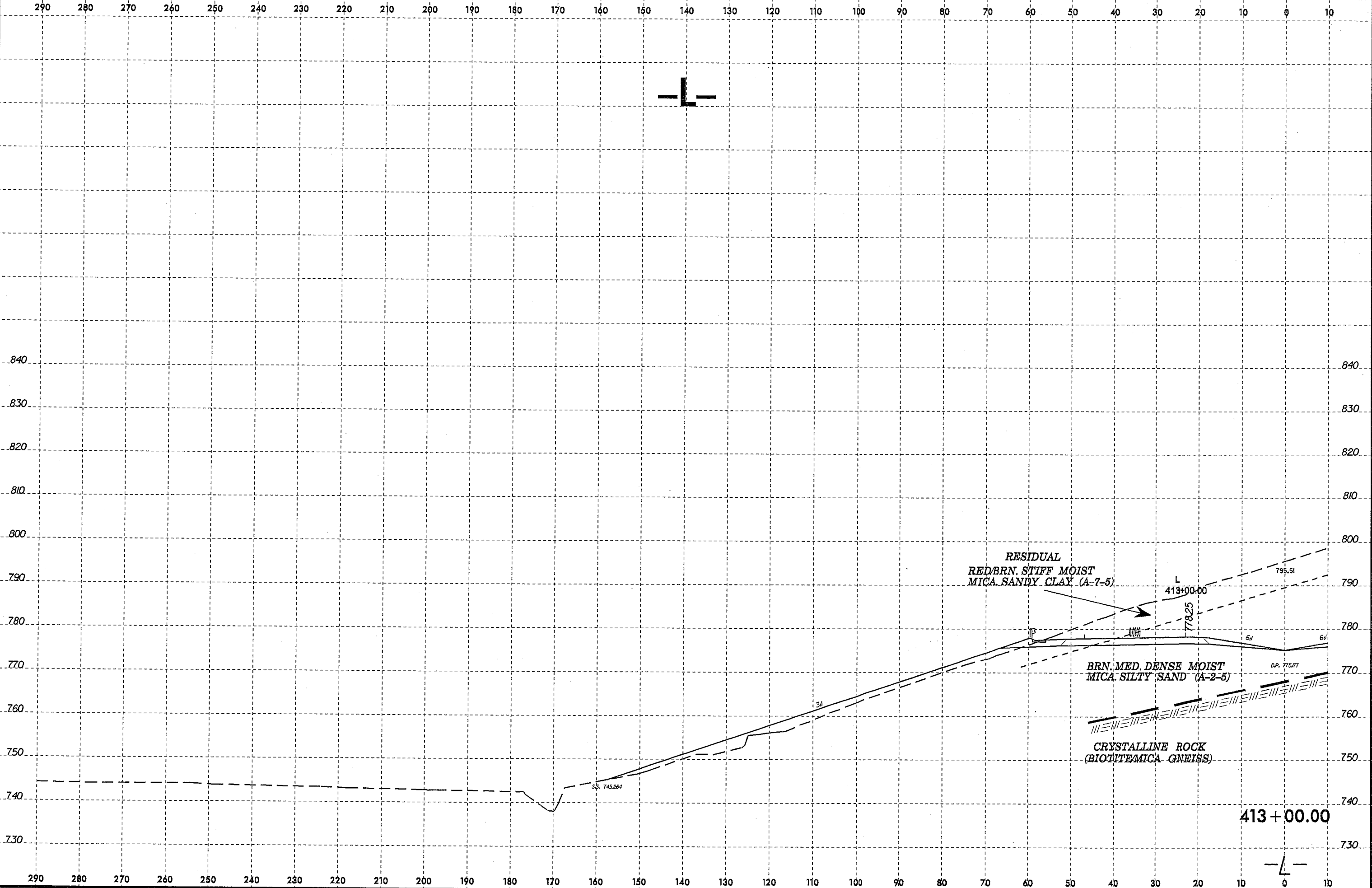
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 2707  
 2707  
 2707

8/23/98  
16-MAY-2008 08:35  
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8/23/99

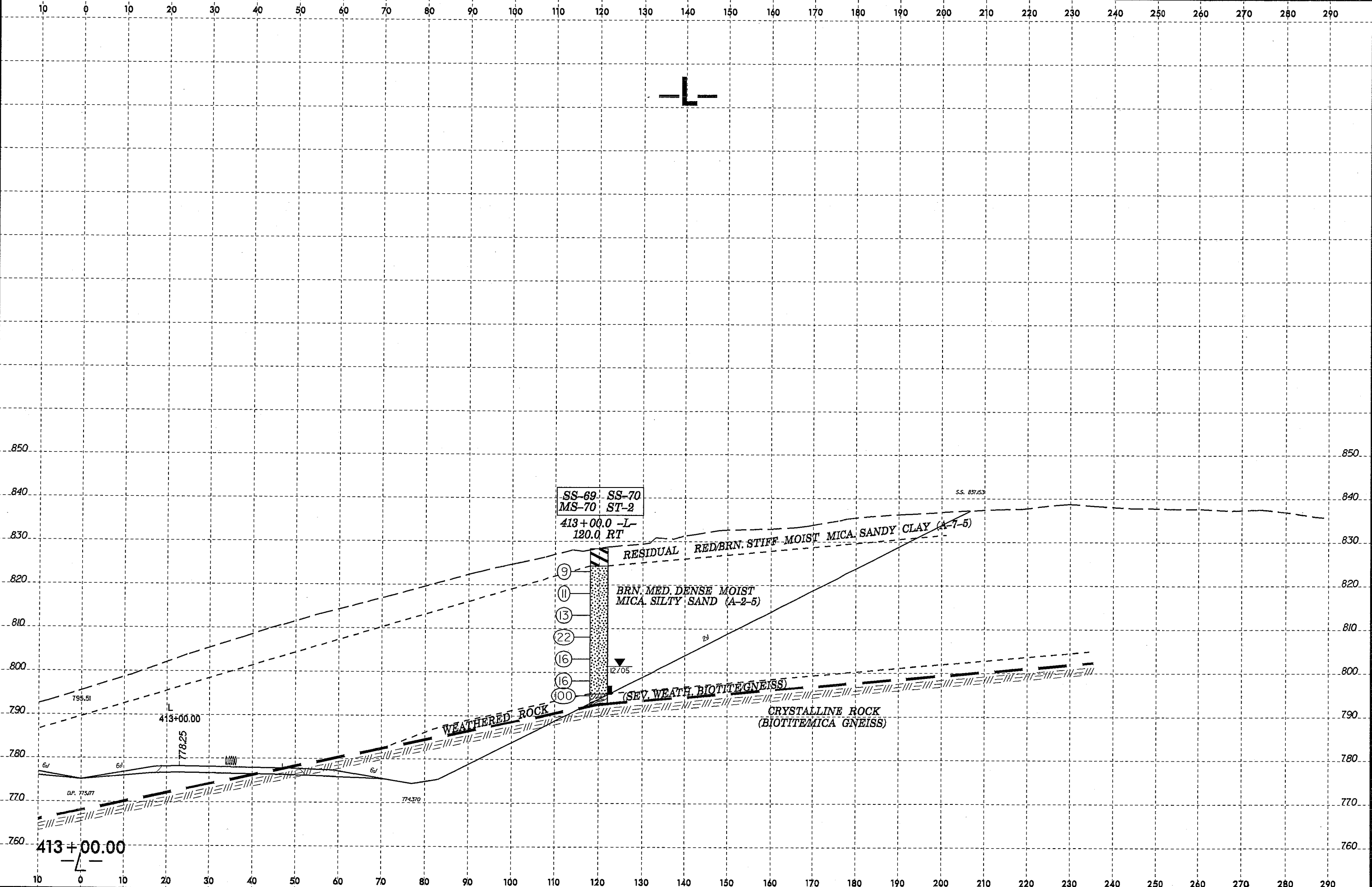
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	177



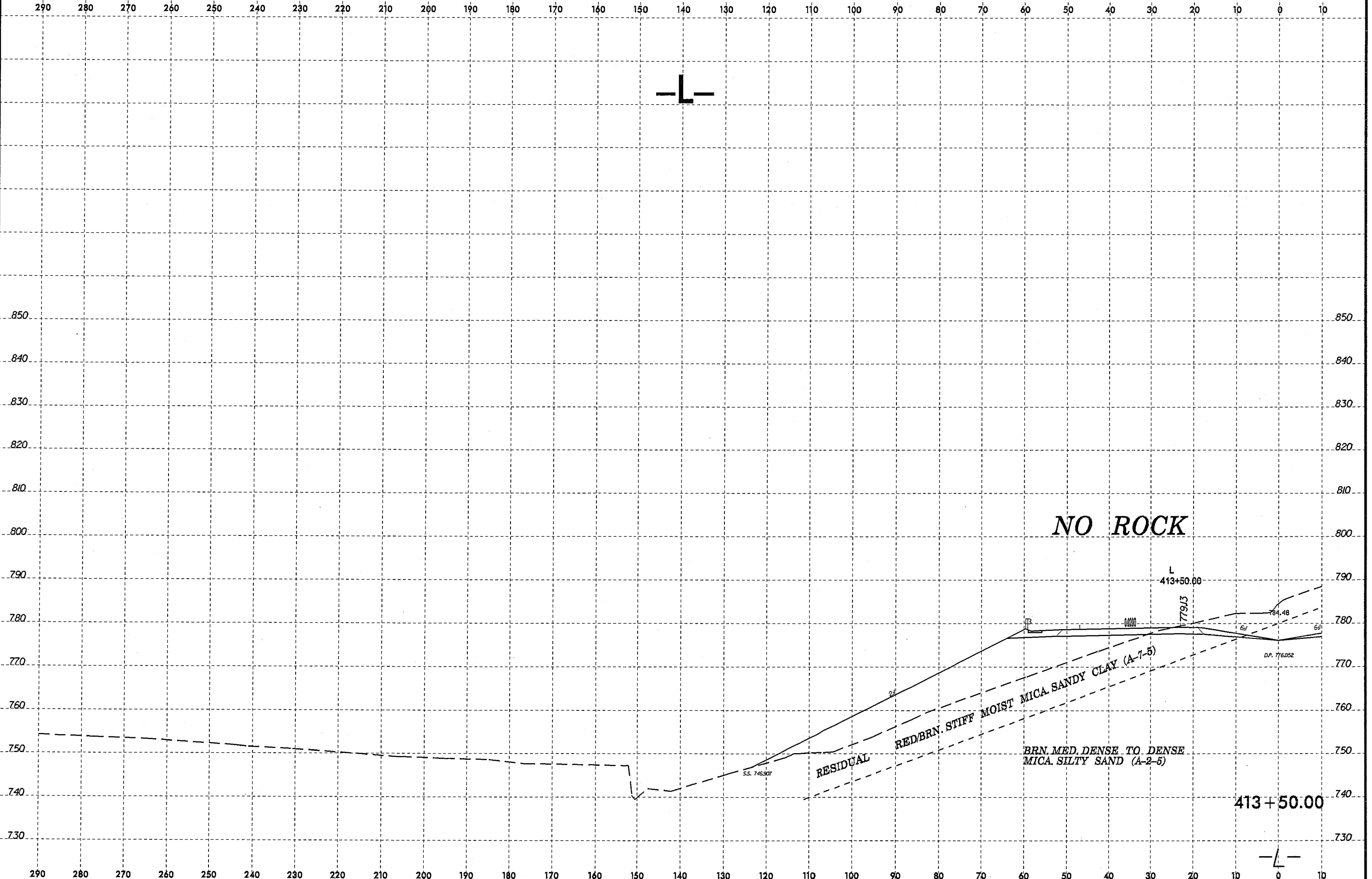
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 2707C\proj\joe\2707C\proj\2707C\geo\rdw\cleveland\cadd\geotech\p\2707C\rev\geo\_xsl.1.2.dgn

413 + 00.00

8/23/09  
27-MAY-2008 15:34  
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cburris AT GEH26157



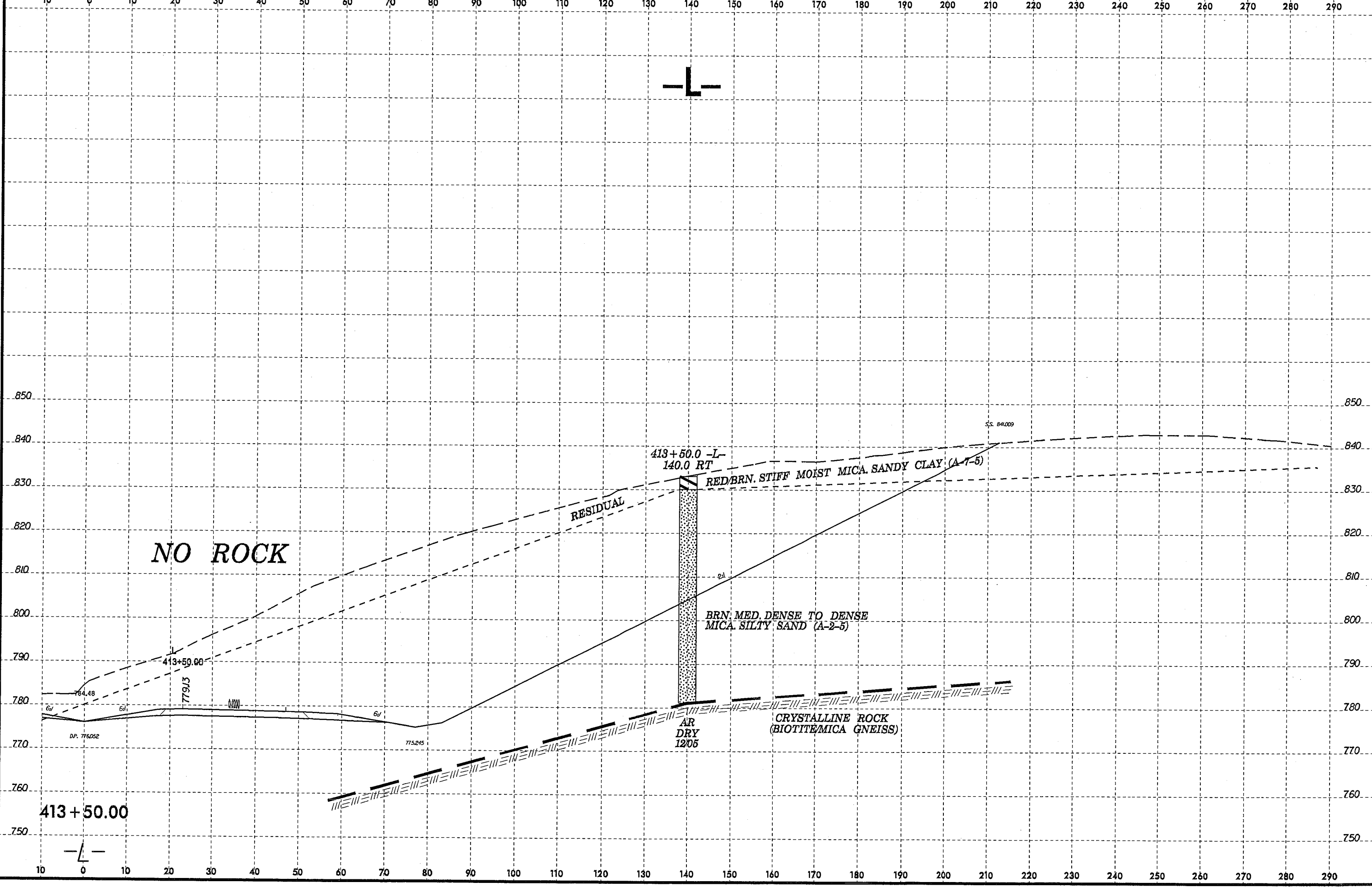
8/23/99



16-MAY-2008 08:39  
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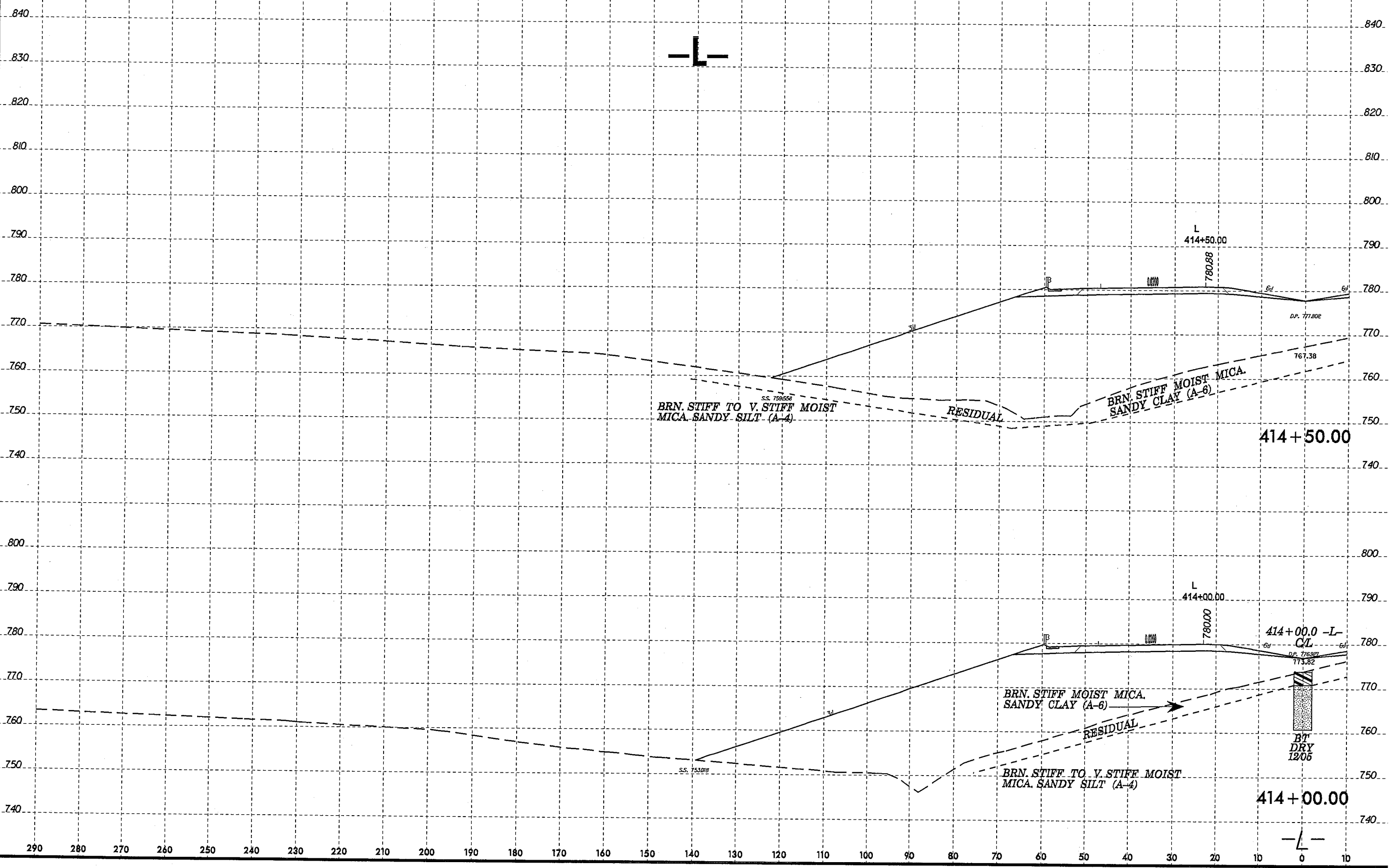
413 + 50.00

8/23/91



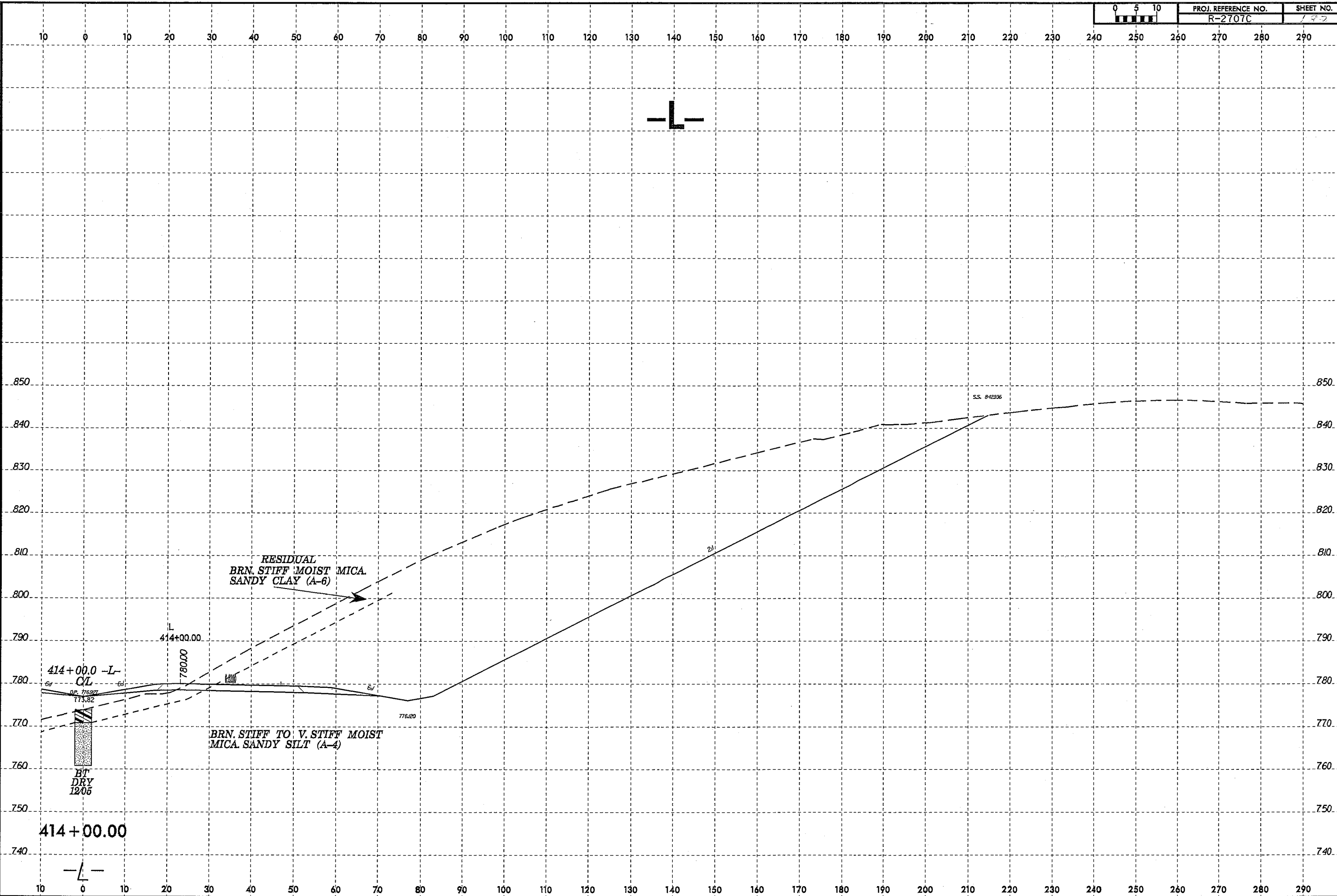
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8/23/99



16-MAY-2008 08:49  
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 borris AT DEPT26157

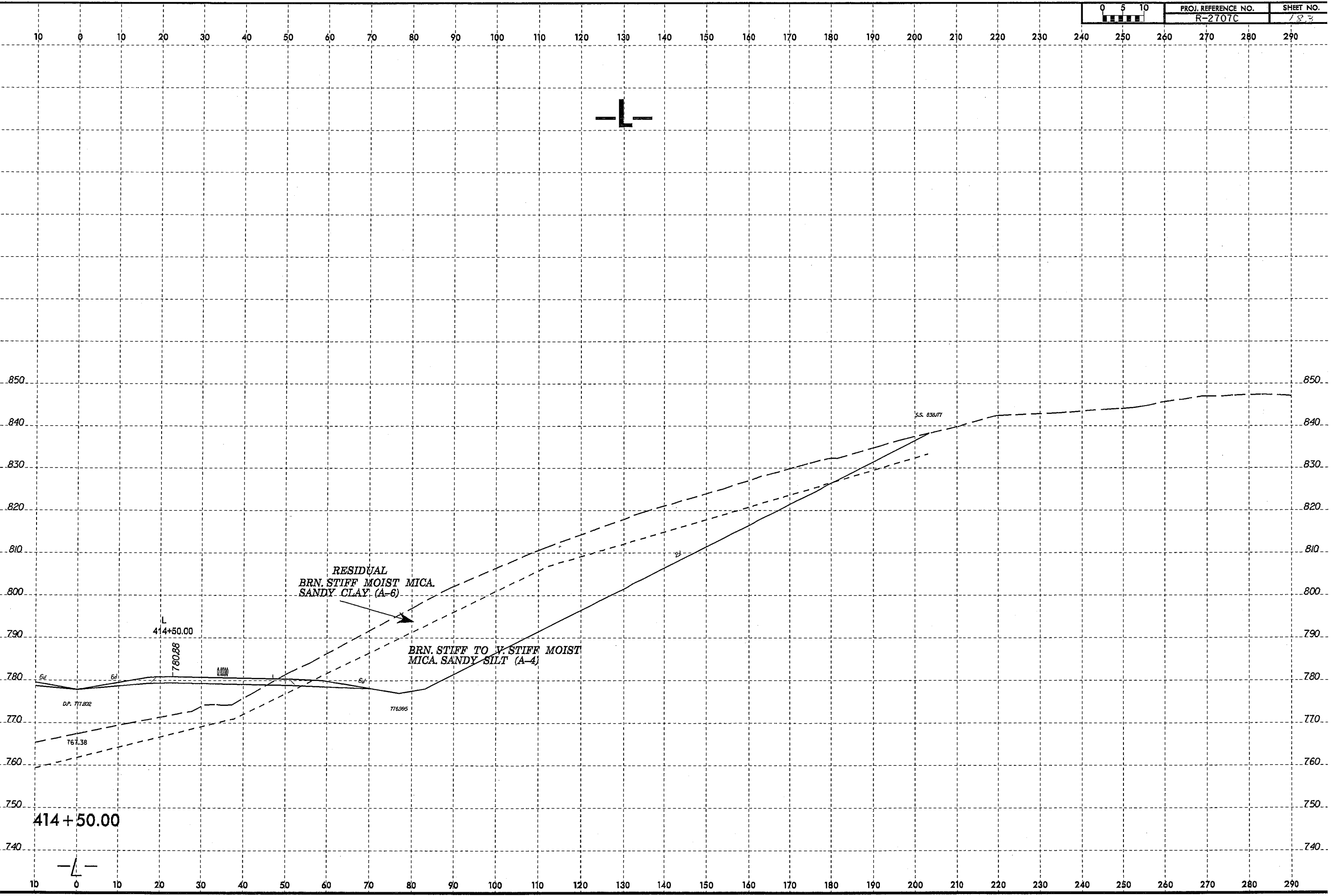
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8/23/99  
15-MAY-2008 09:03  
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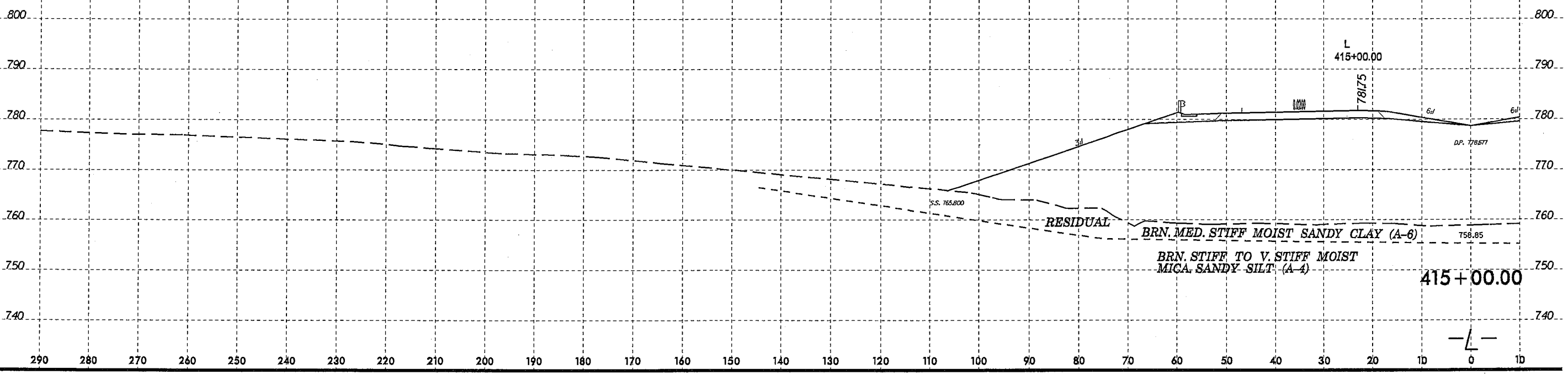
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	183



8/23/99

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	124

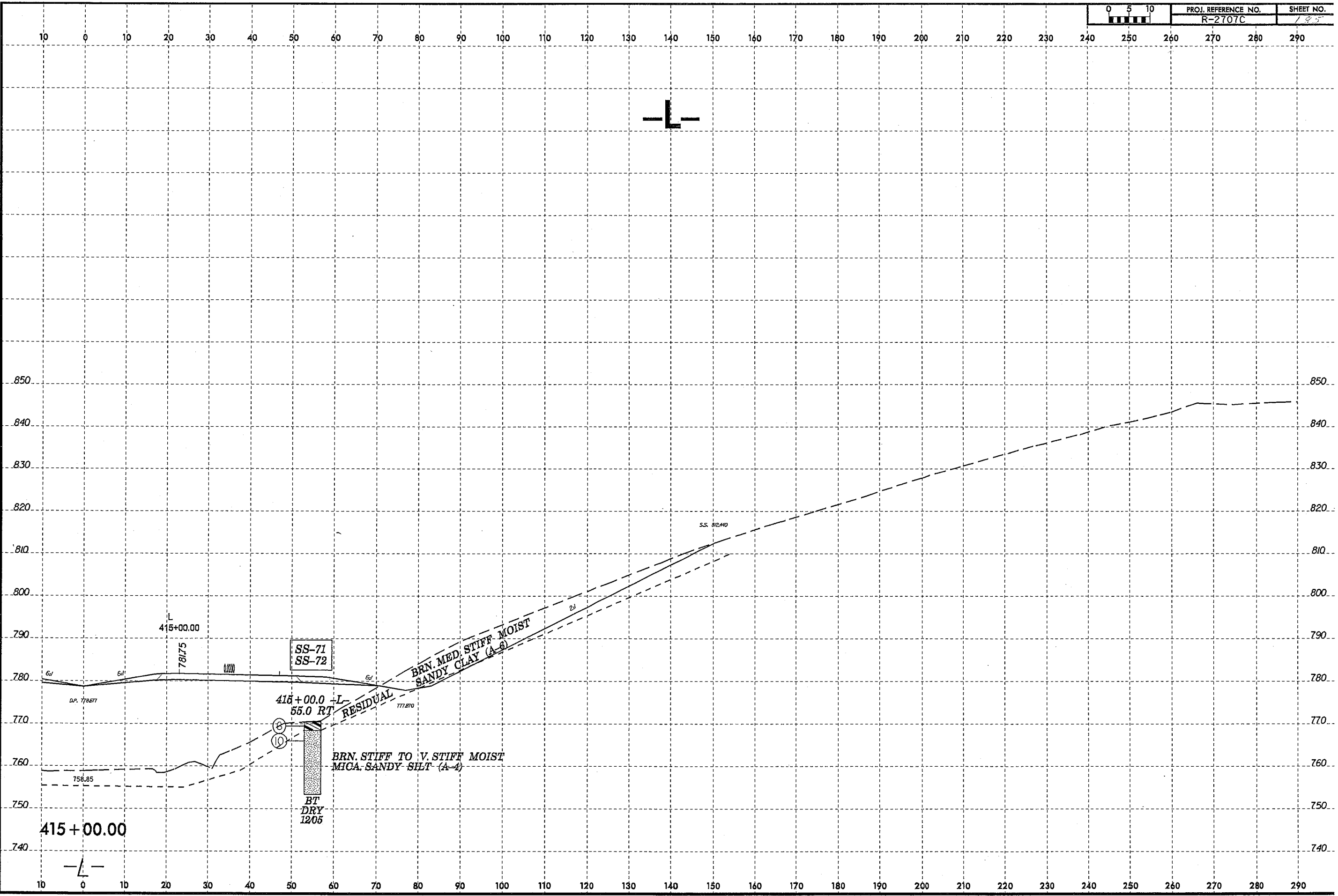
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15-MAY-2008 09:58  
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15-MAY-2008 09:05  
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	185



415 + 00.00

SS-71  
SS-72

415 + 00.0  
55.0 RT

RESIDUAL

BRN. STIFF TO V. STIFF MOIST  
MICA SANDY SILT (A-4)

BT  
DRY  
1205

BRN. MED. STIFF MOIST  
SANDY CLAY (A-6)

SS 812410

771.870

DP. 778671

415+00.00

78175

6.1

6.1

758.85

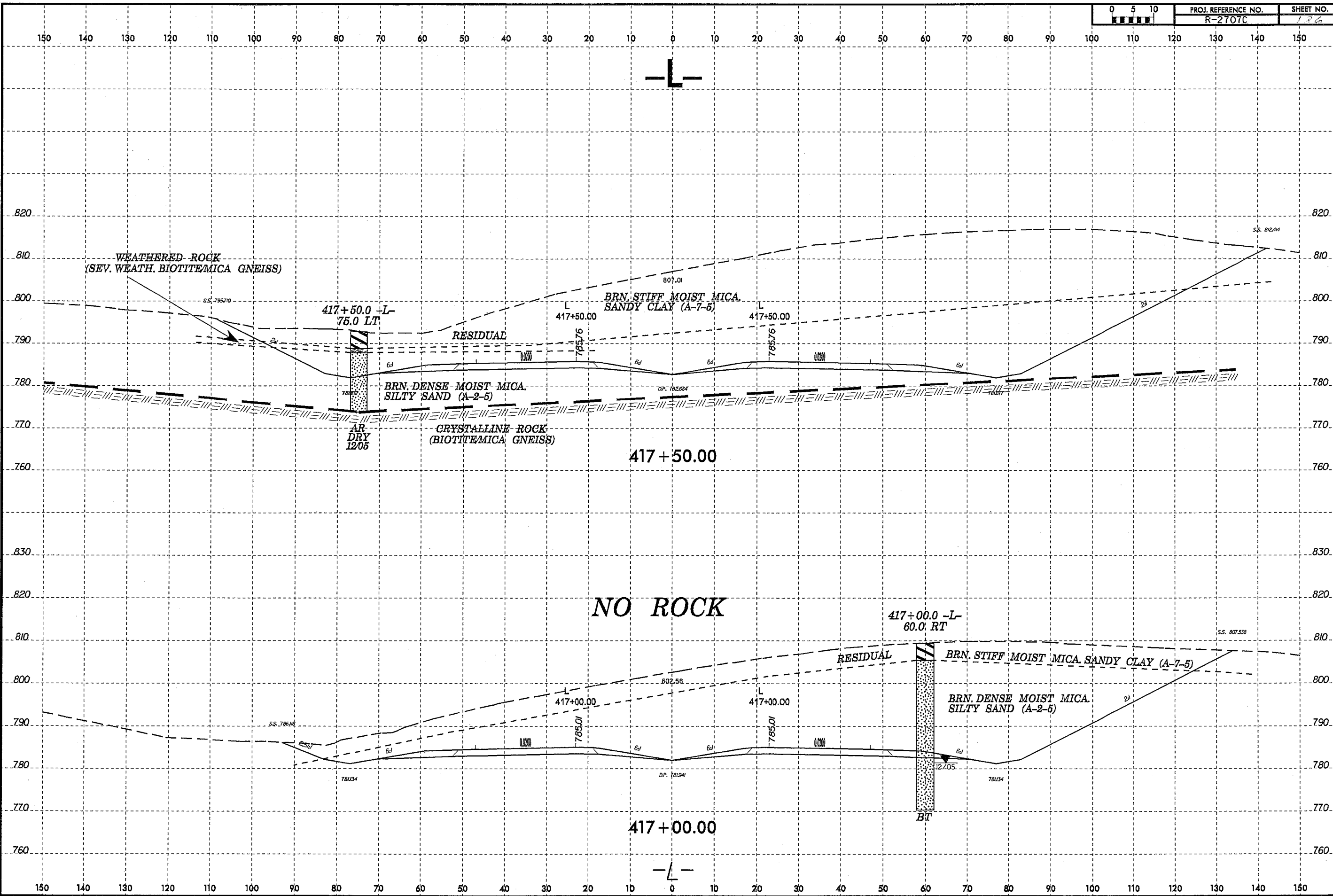
415 + 00.00

L

L

8/23/99

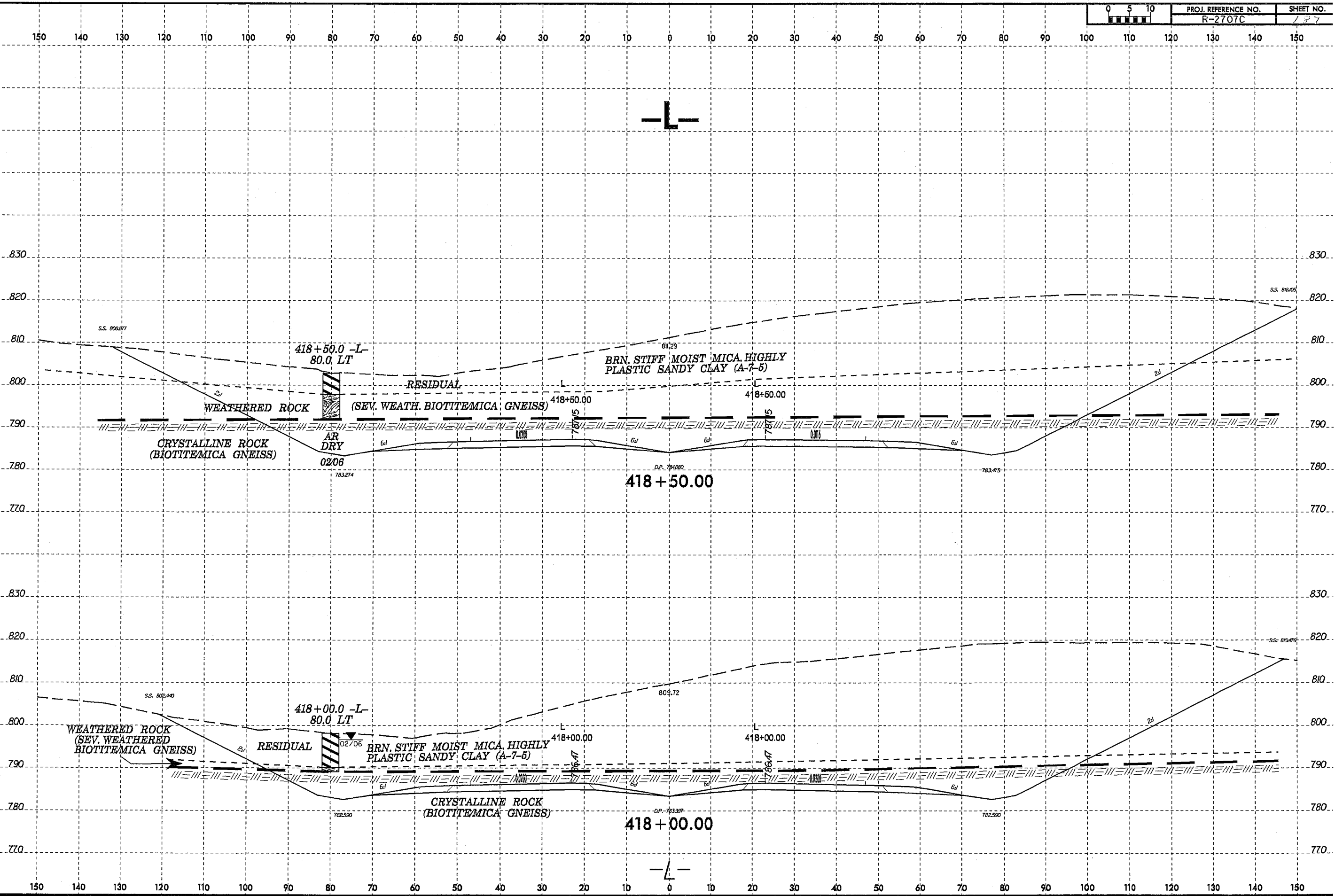
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	126



15-MAY-2008 09:04  
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 chunrjg AT BEH226157

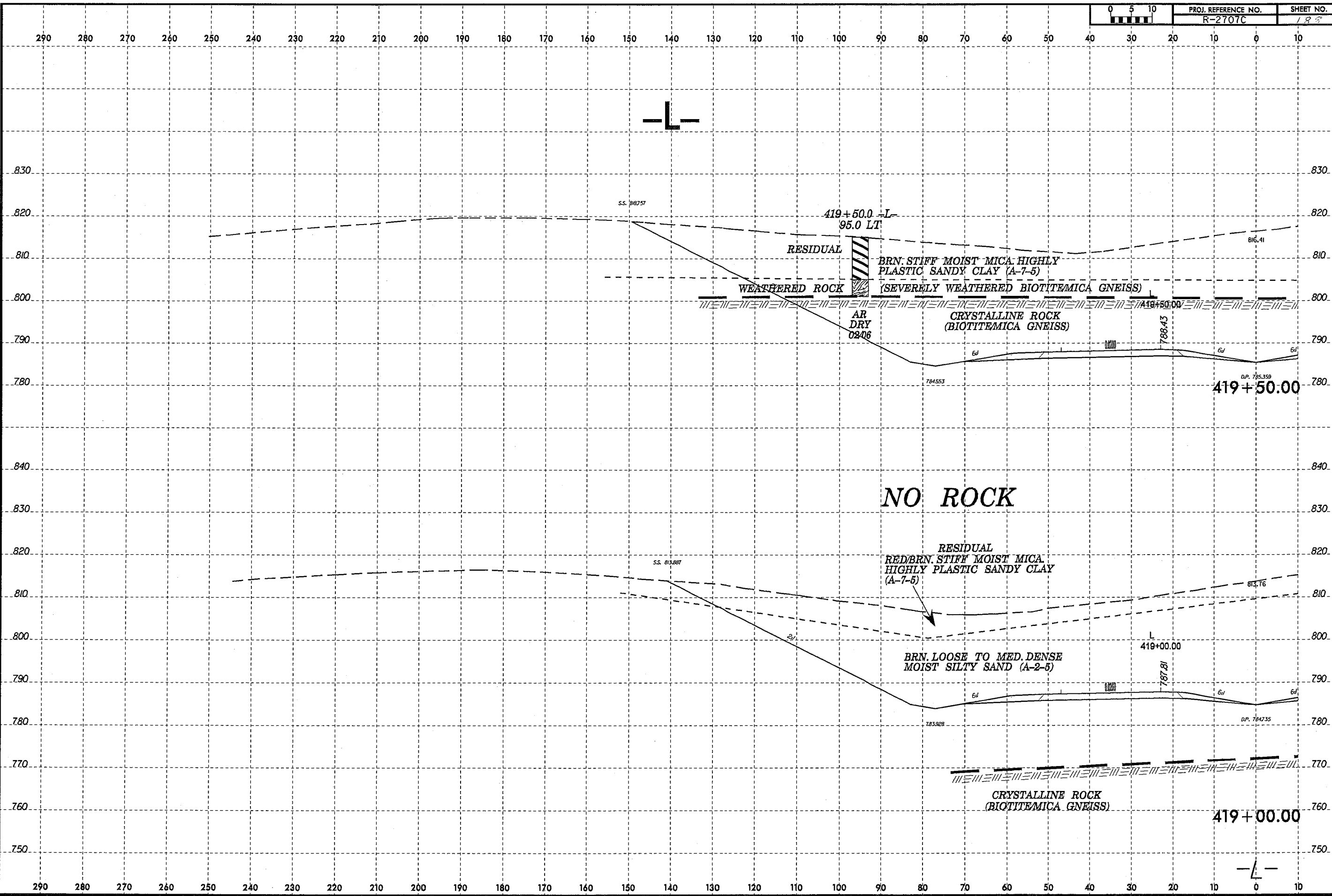
8/23/99  
16-MAY-2008 09:06  
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	177



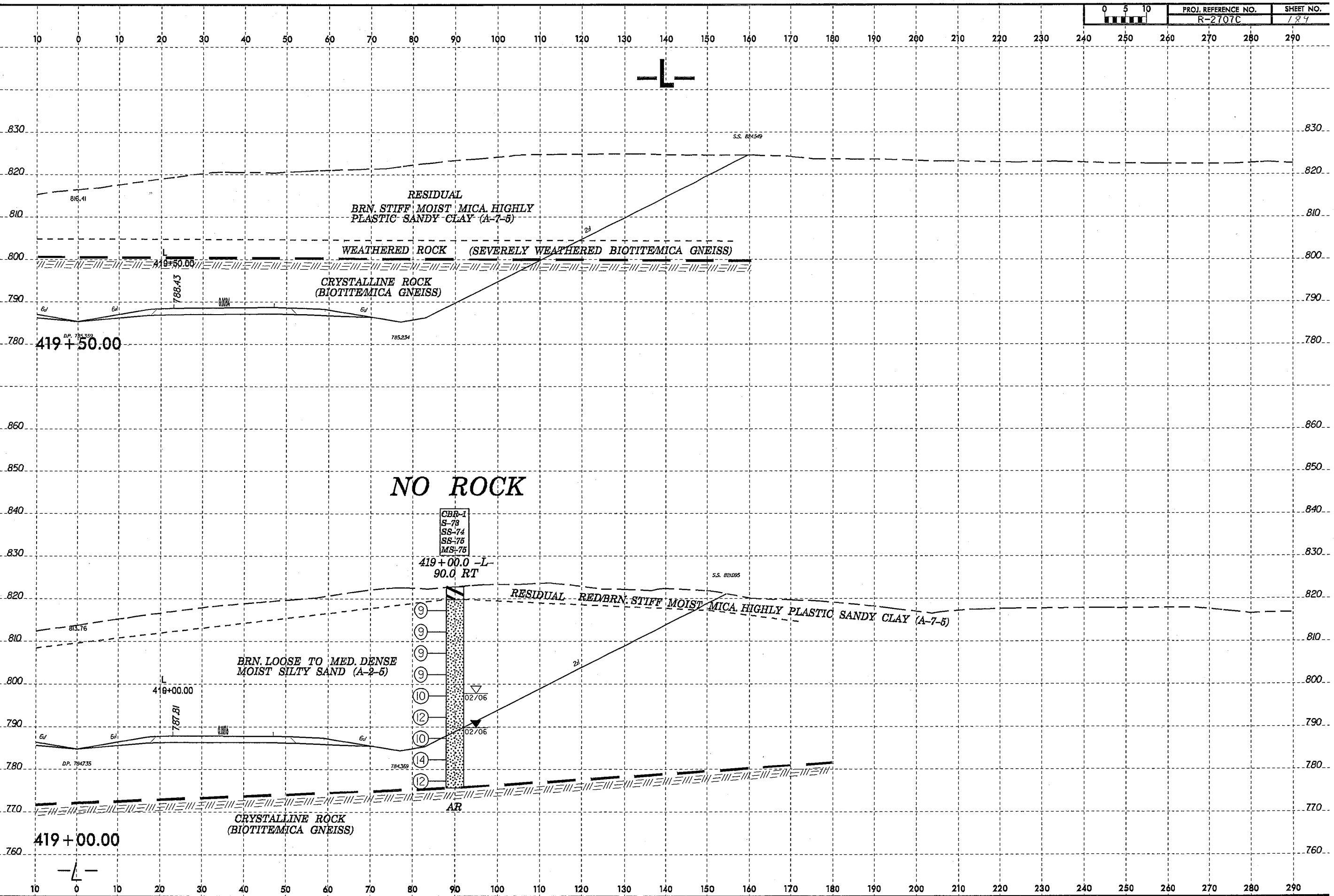
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SOURCER: 11 GENZEB33

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 188
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8/23/99

27-MAY-2008 13:32  
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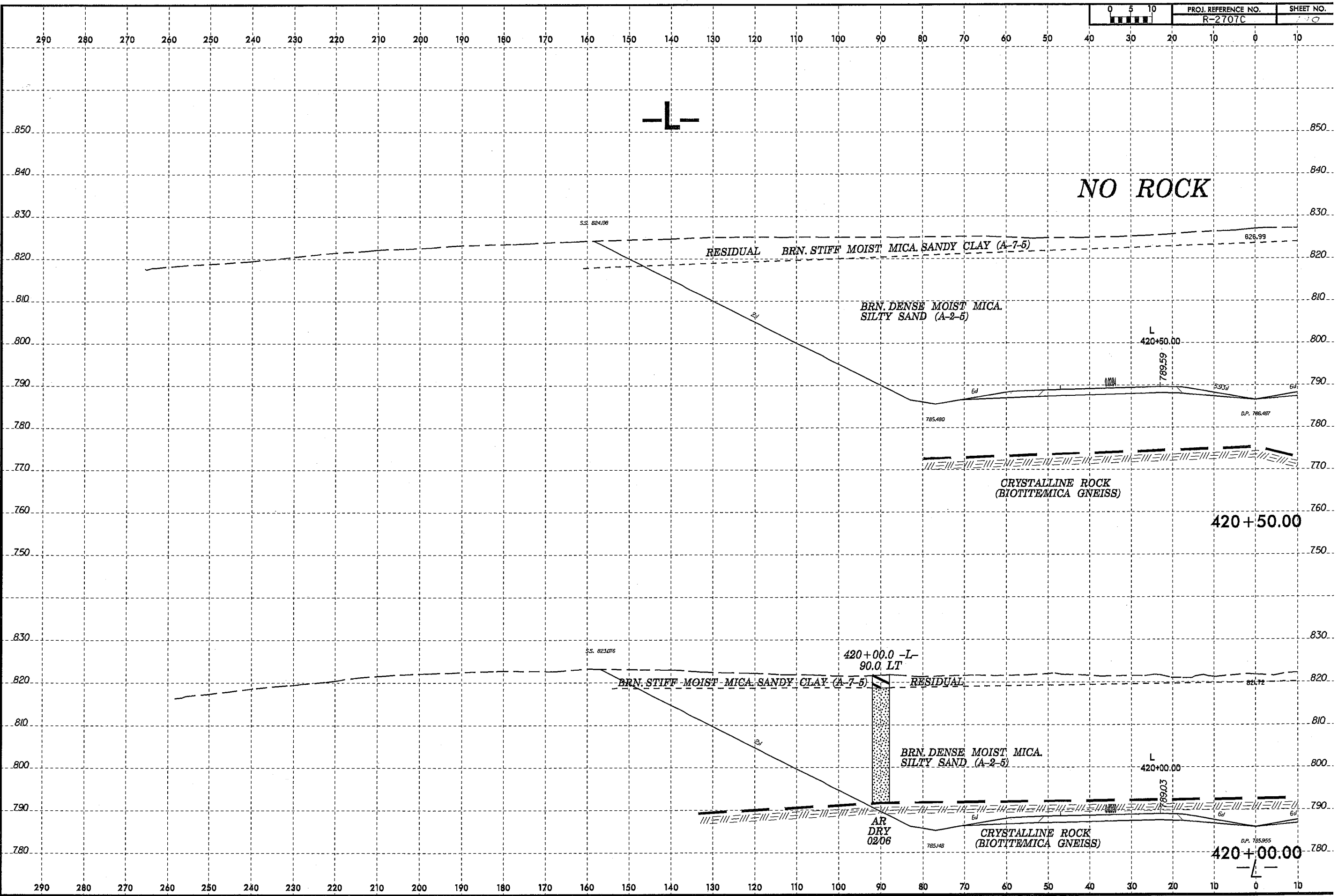


CBR-1
SS-73
SS-74
SS-75
MS-75

419+00.00 -L-  
90.0 RT

8/23/99  
15-MAY-2008 09:12  
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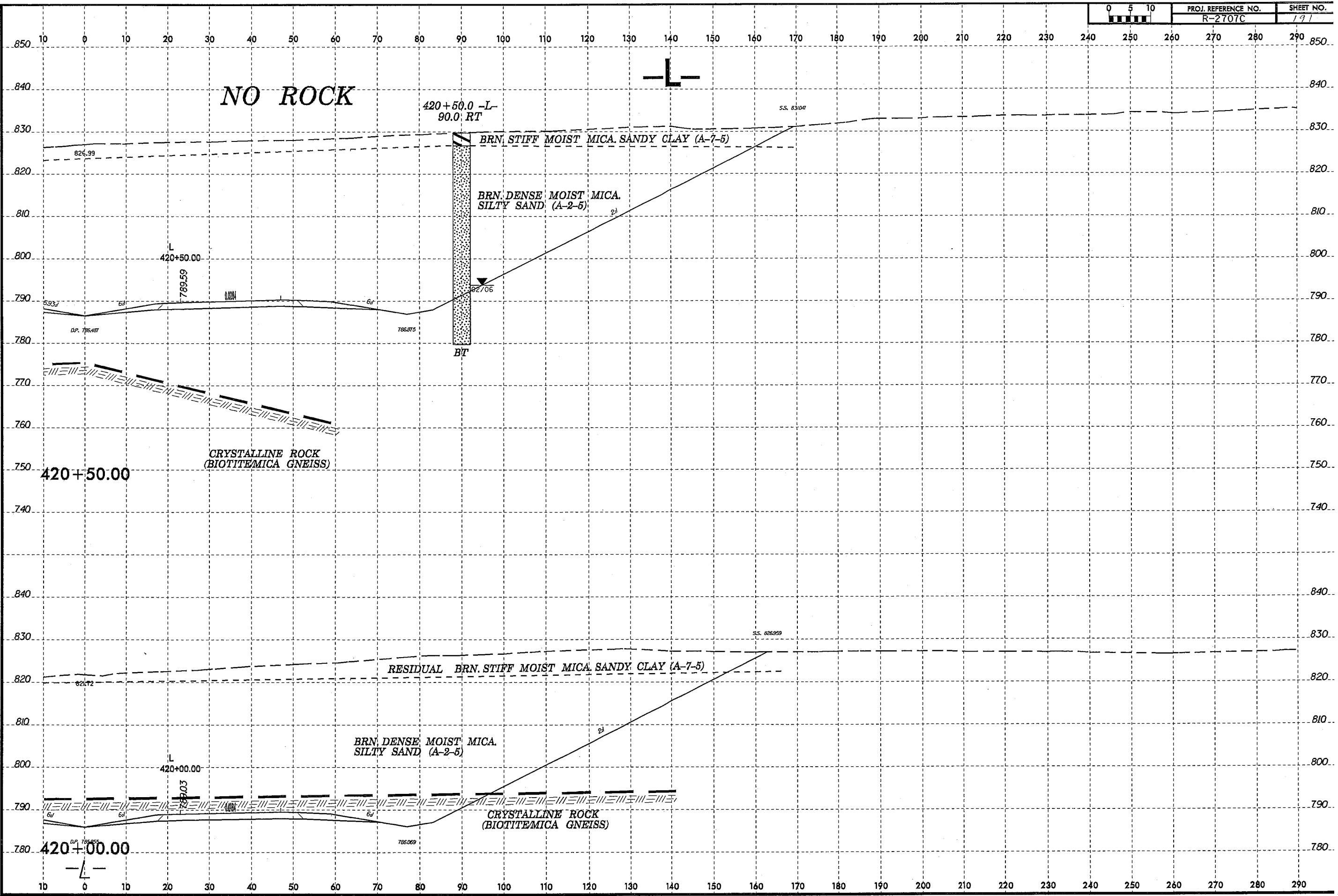
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	10





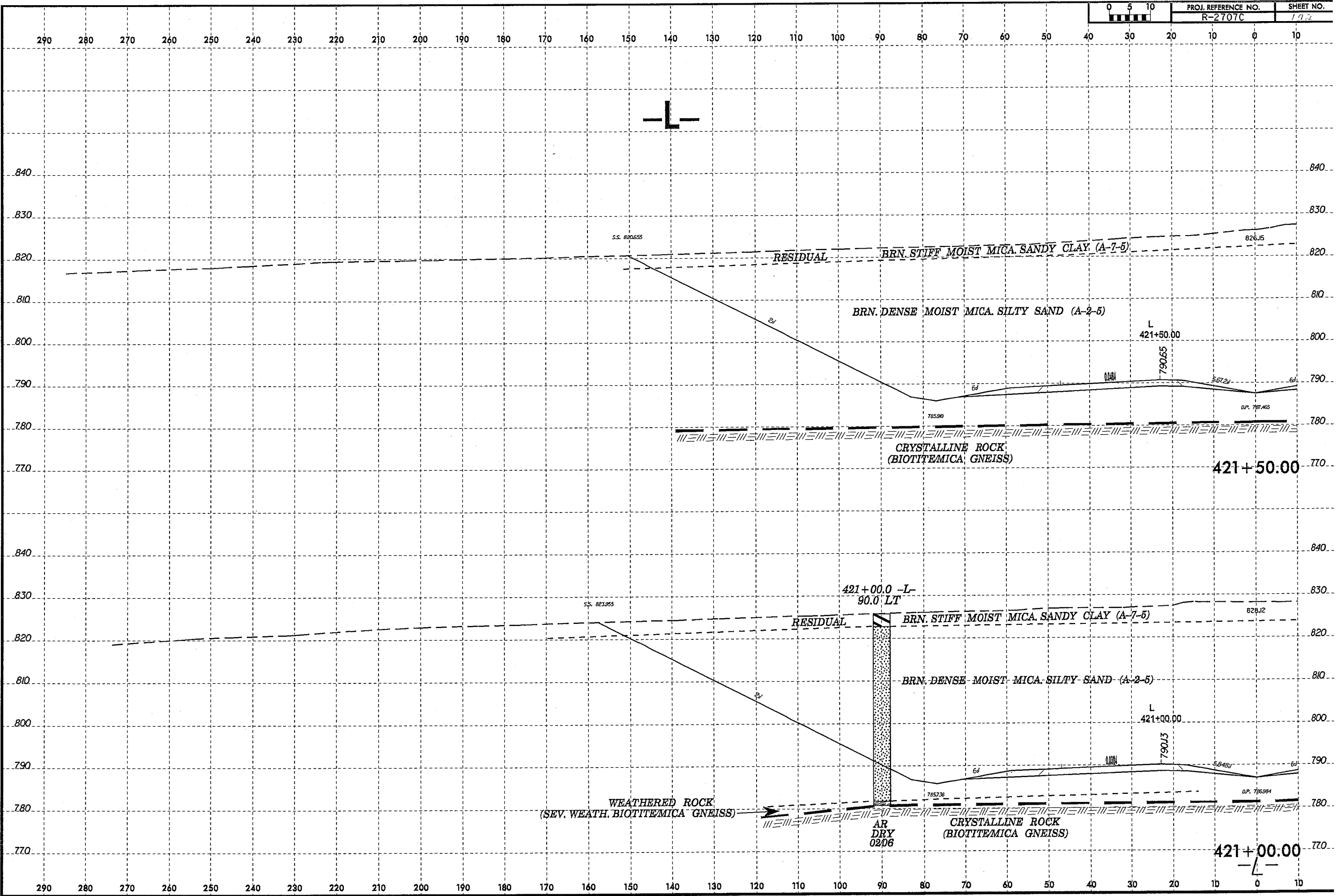
8/23/99  
15-MAY-2008 09:45  
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CHURRIS AT 08/22/05

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	191



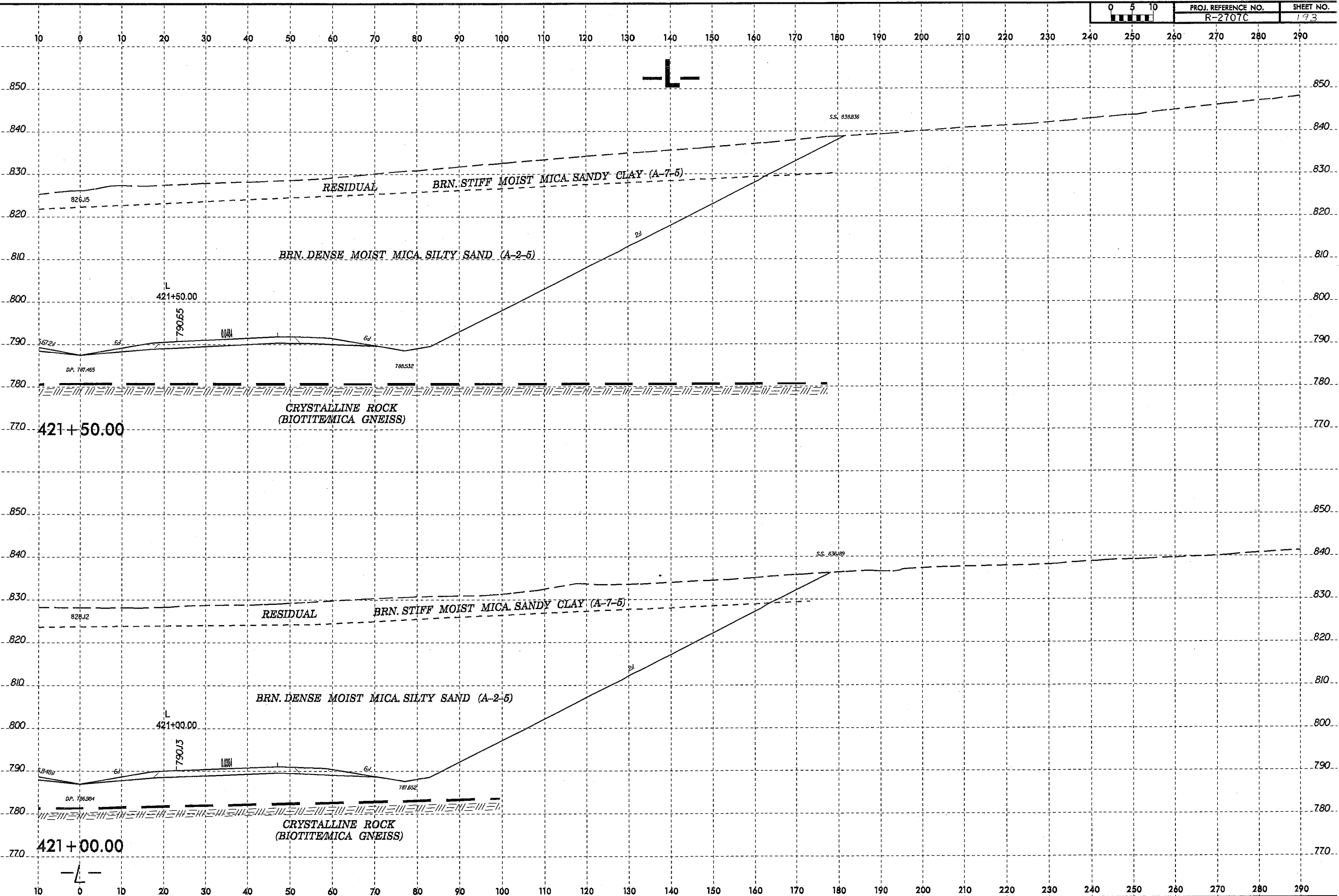
8/23/99  
15-MAY-2008 09:43  
d:\projects\2707c\rev\geo\_rdw\cleveland\cadd\geotech\ssc\2707c\rev\l\_geo\_xst\1.2.dgn  
dwgname: 2707c\rev\l\_geo\_xst\1.2.dgn  
sheet: 1 of 1

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	192

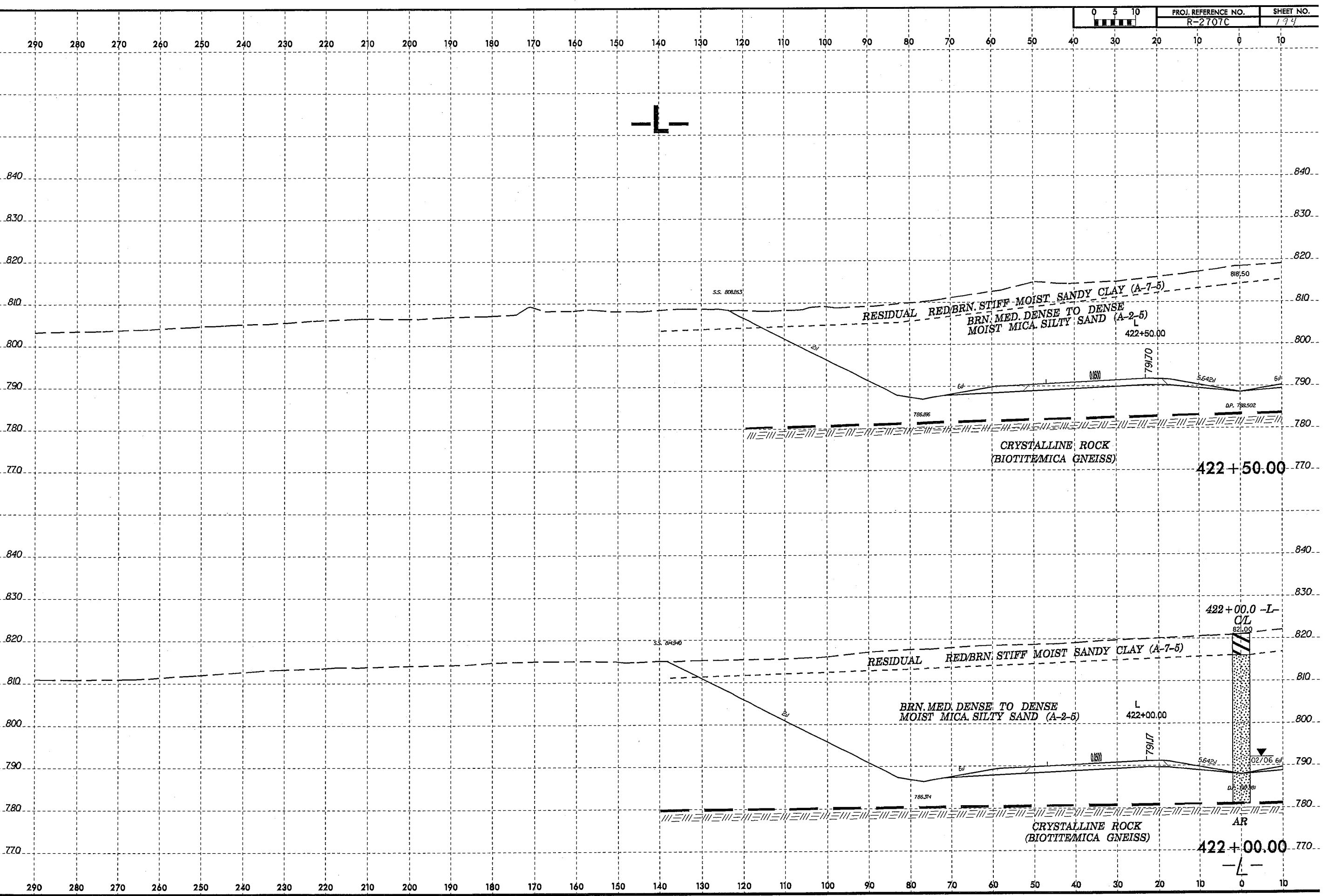


8/23/99

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	193

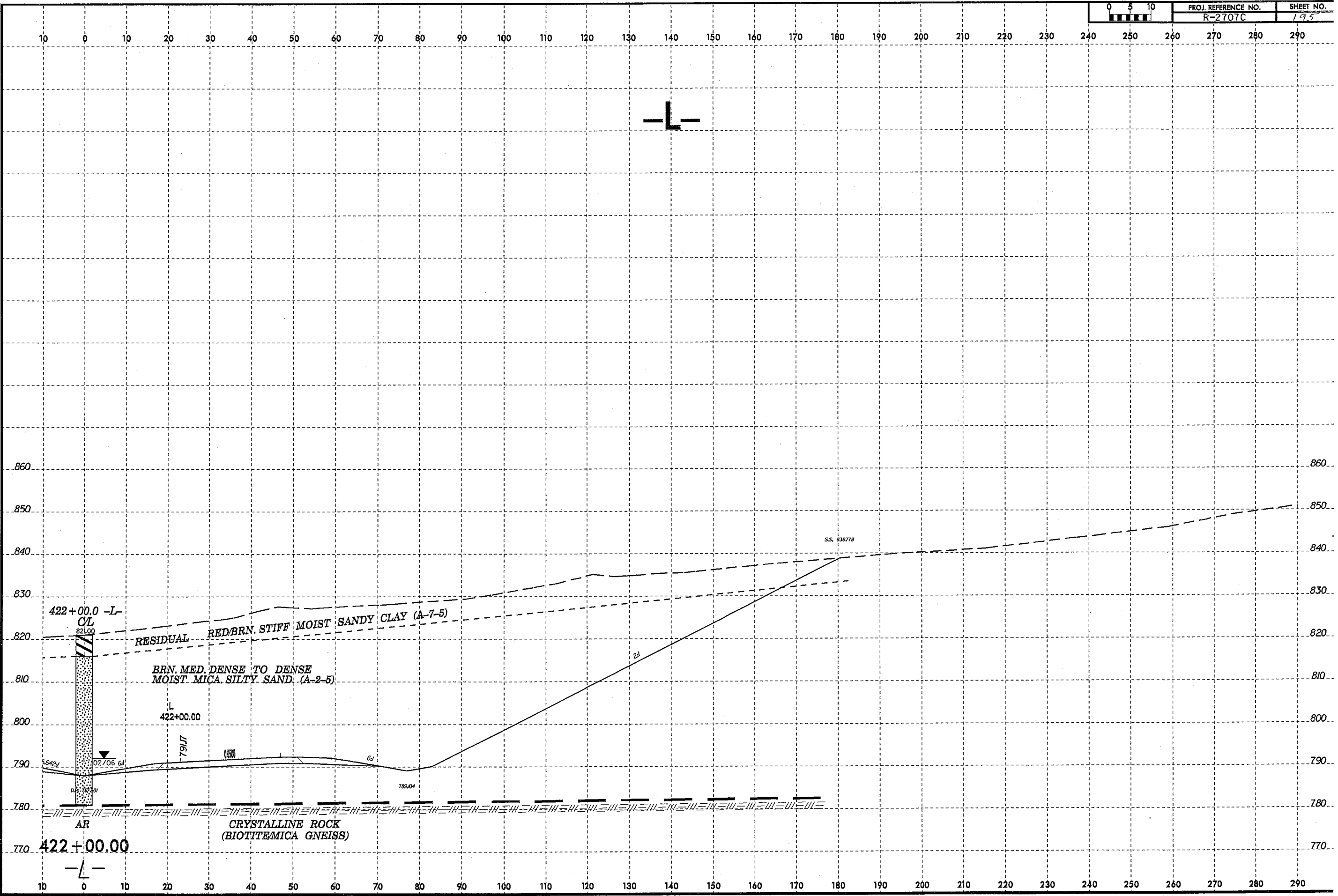


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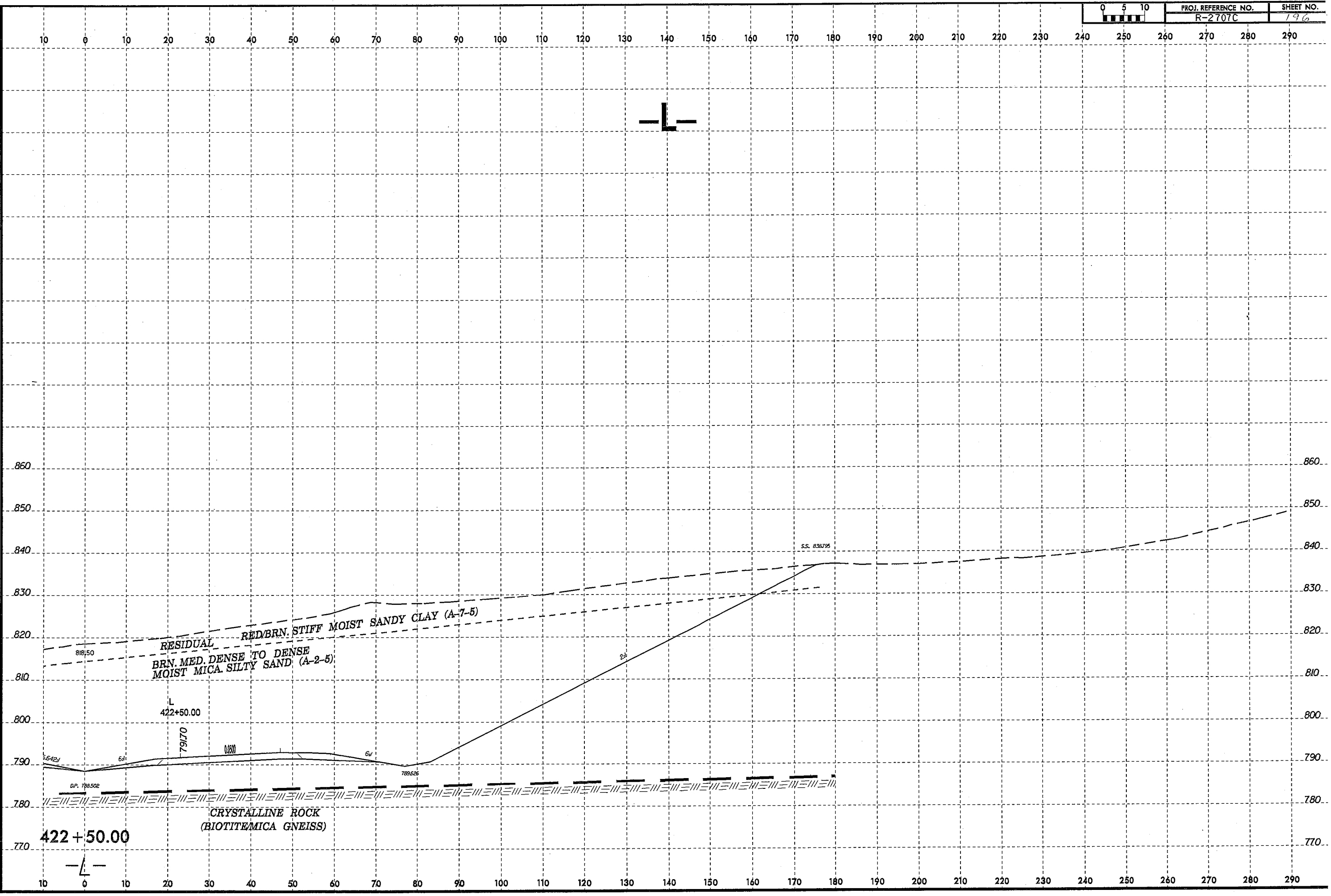
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15-MAY-2008 09:26  
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	195



15-MAY-2008 09:27  
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	196



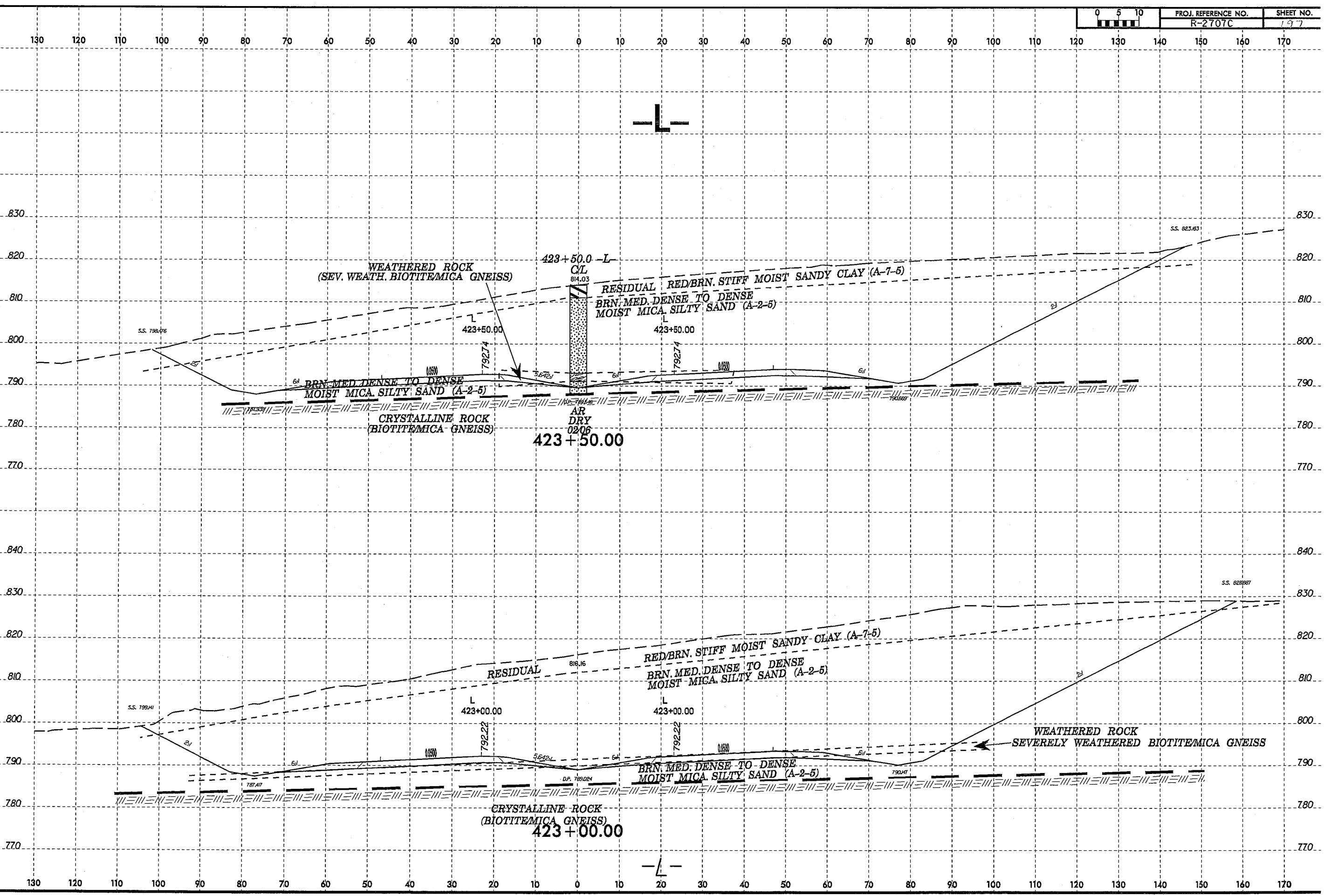
RESIDUAL  
RED/BRN. STIFF MOIST SANDY CLAY (A-7-5)  
BRN. MED. DENSE TO DENSE  
MOIST MICA. SILTY SAND (A-2-5)

CRYSTALLINE ROCK  
(BIOTITE MICA GNEISS)

422+50.00

8/23/99

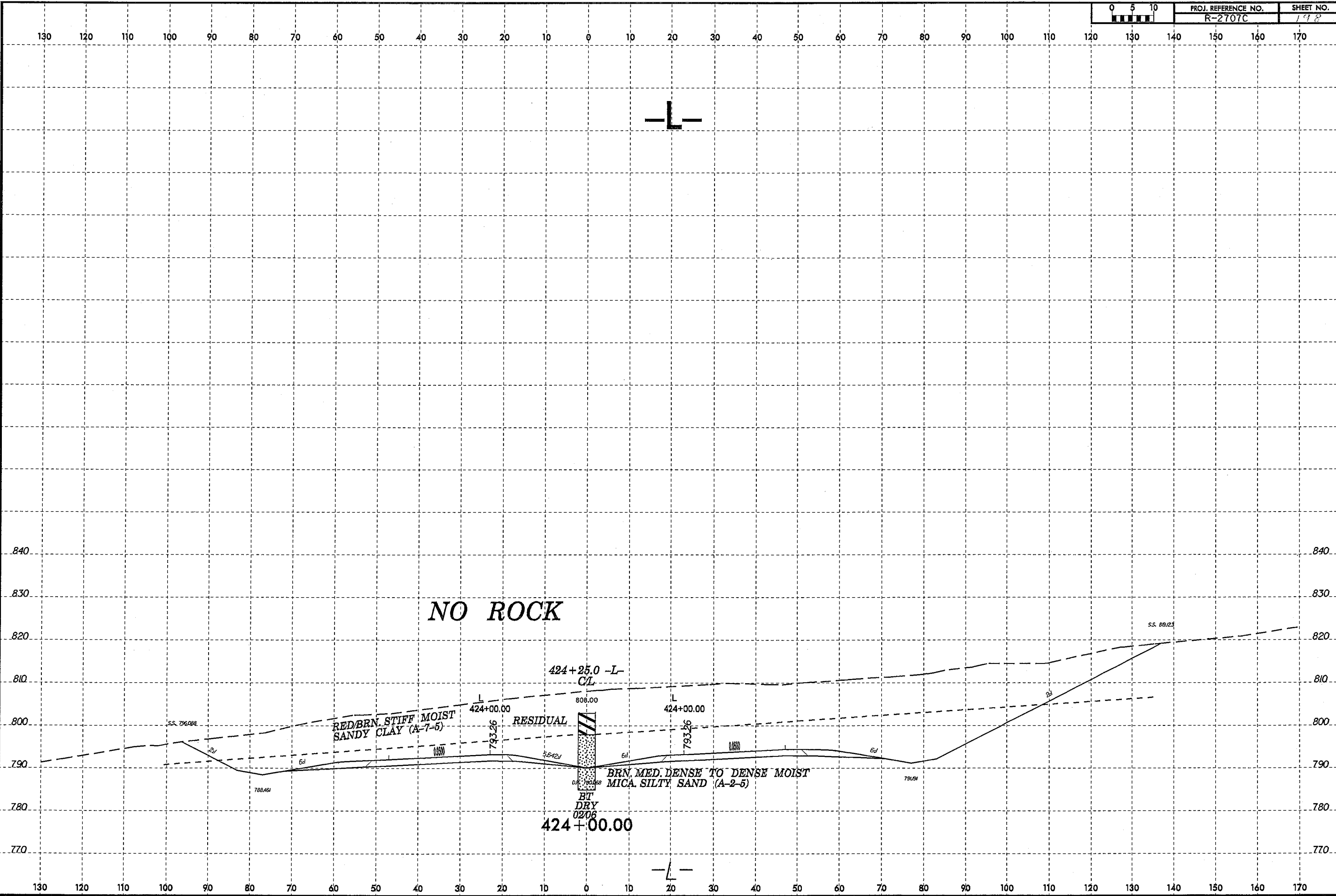
0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 197
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16-MAY-2008 09:16  
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8/23/99  
15-MAY-2008 09:29  
c:\projeos\p\8025\fig\geo\_rdkj-cleveland\codd-geotech\psc.v2707-cl-rev\_l-geo\_xst\_1.2.dgn  
SURF: BT 0206

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	198



NO ROCK

RED/BRN. STIFF MOIST SANDY CLAY (A-7-5)

RESIDUAL

BRN. MED. DENSE TO DENSE MOIST MICA SILTY SAND (A-2-5)

BT DRY 0206

424+00.00

424+25.0 -L-  
CL

424+00.00

424+00.00

808.00

793.26

793.26

791.56

SS 790.88

SS 809.23

788.46

130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120

130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120

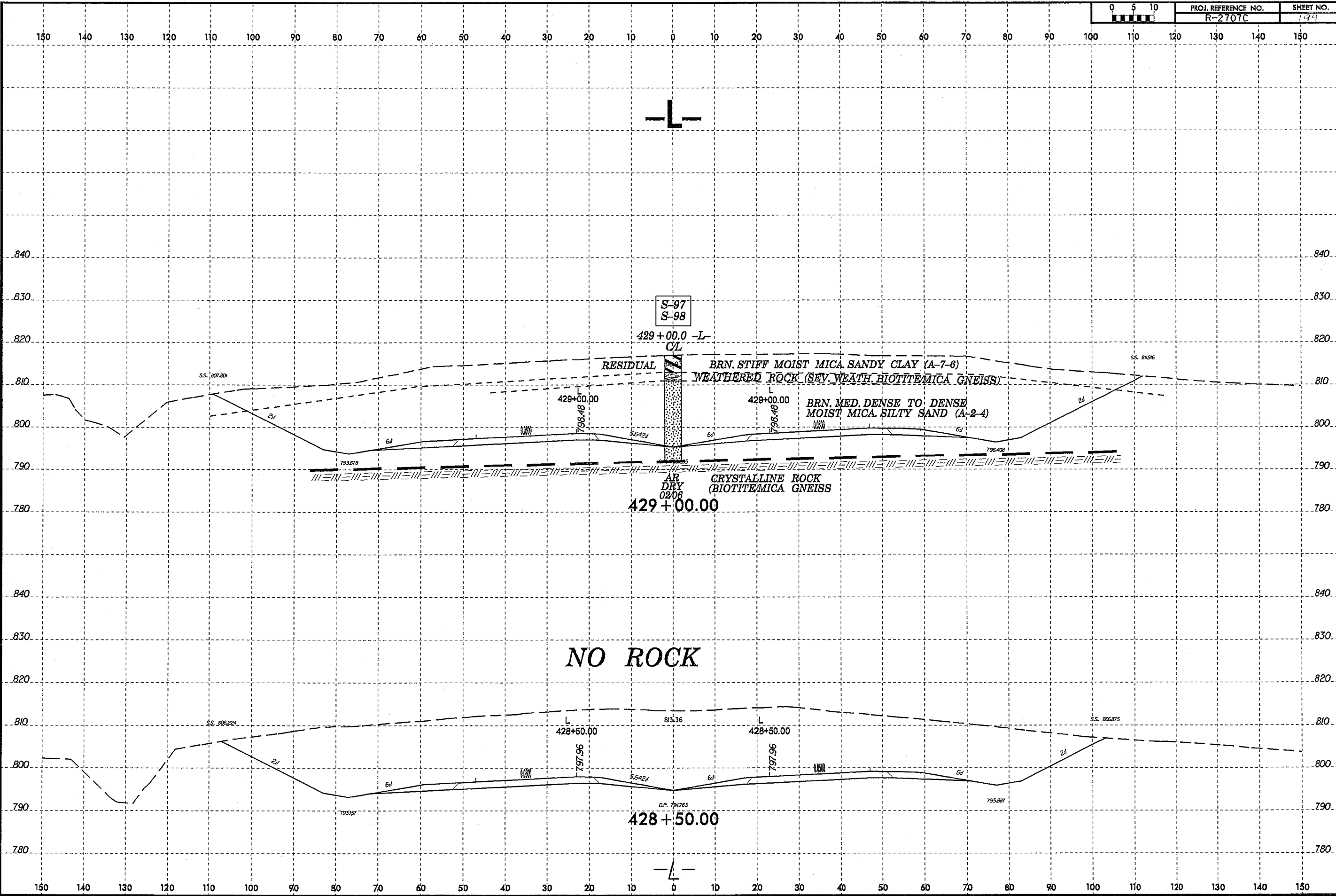
130 140 150 160 170

130 140 150 160 170



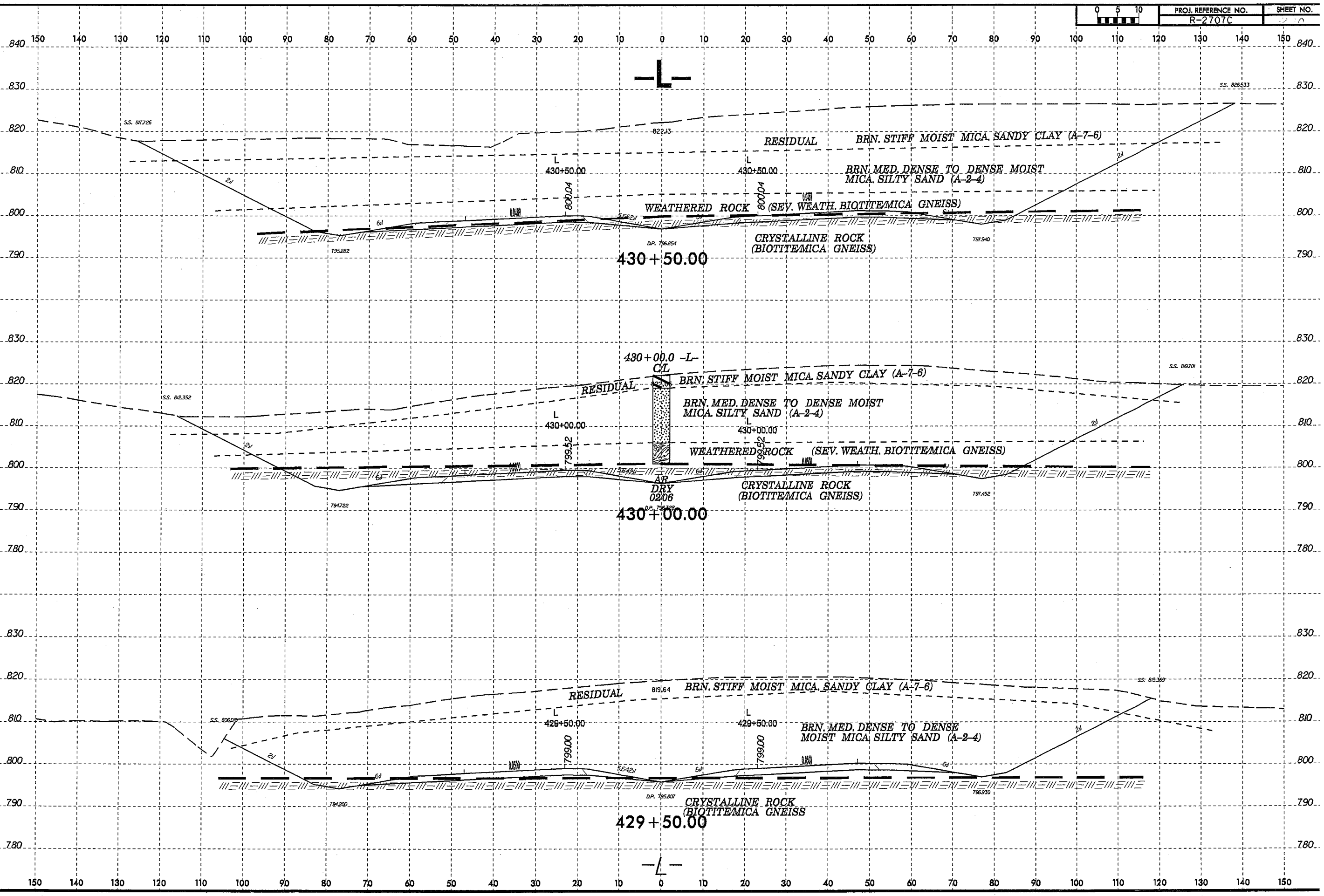
8/23/99  
15-MAY-2008 09:30  
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churris AT GEH26157

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 139
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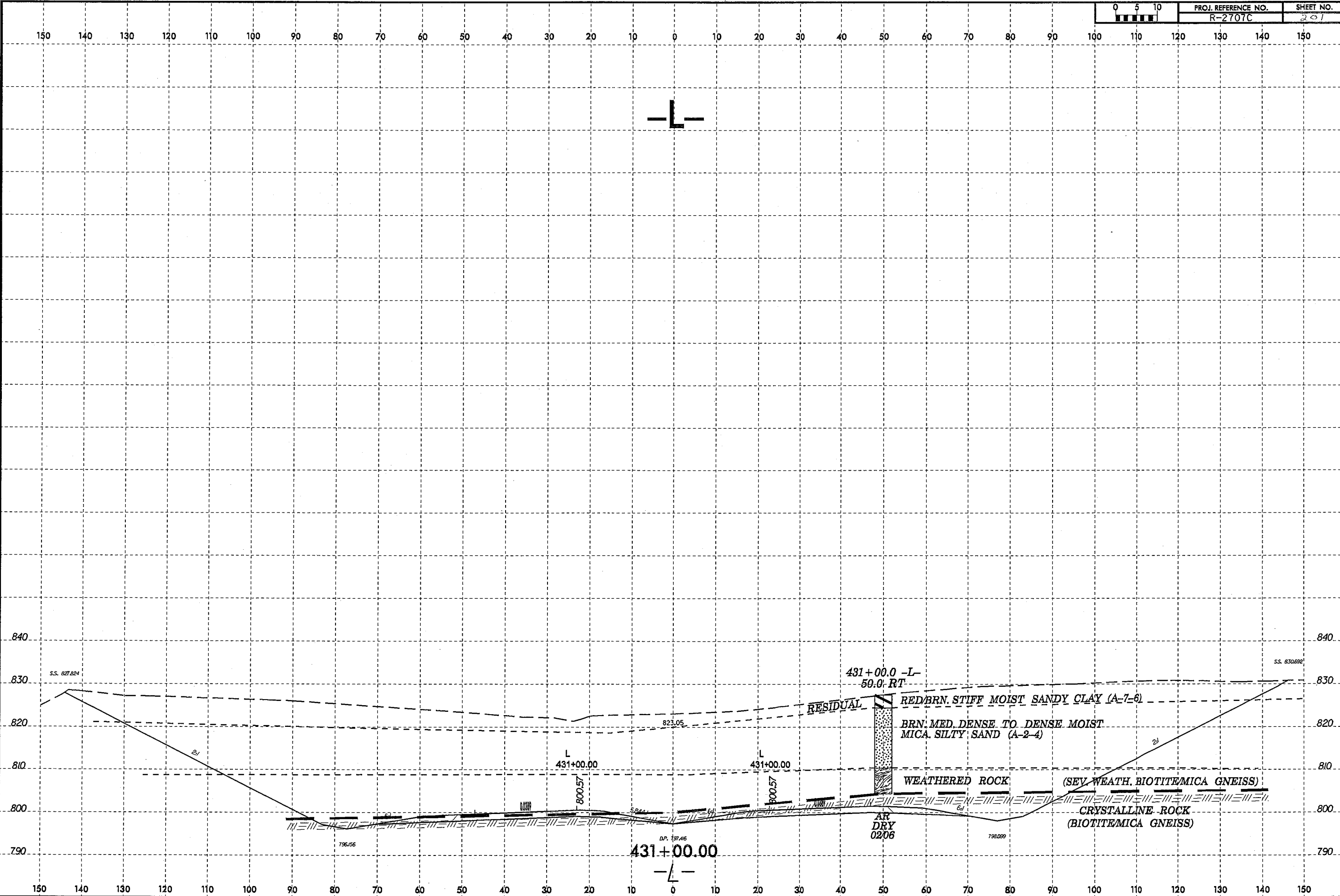
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PROJ. REFERENCE NO. R-2707C  
 SHEET NO. 2700

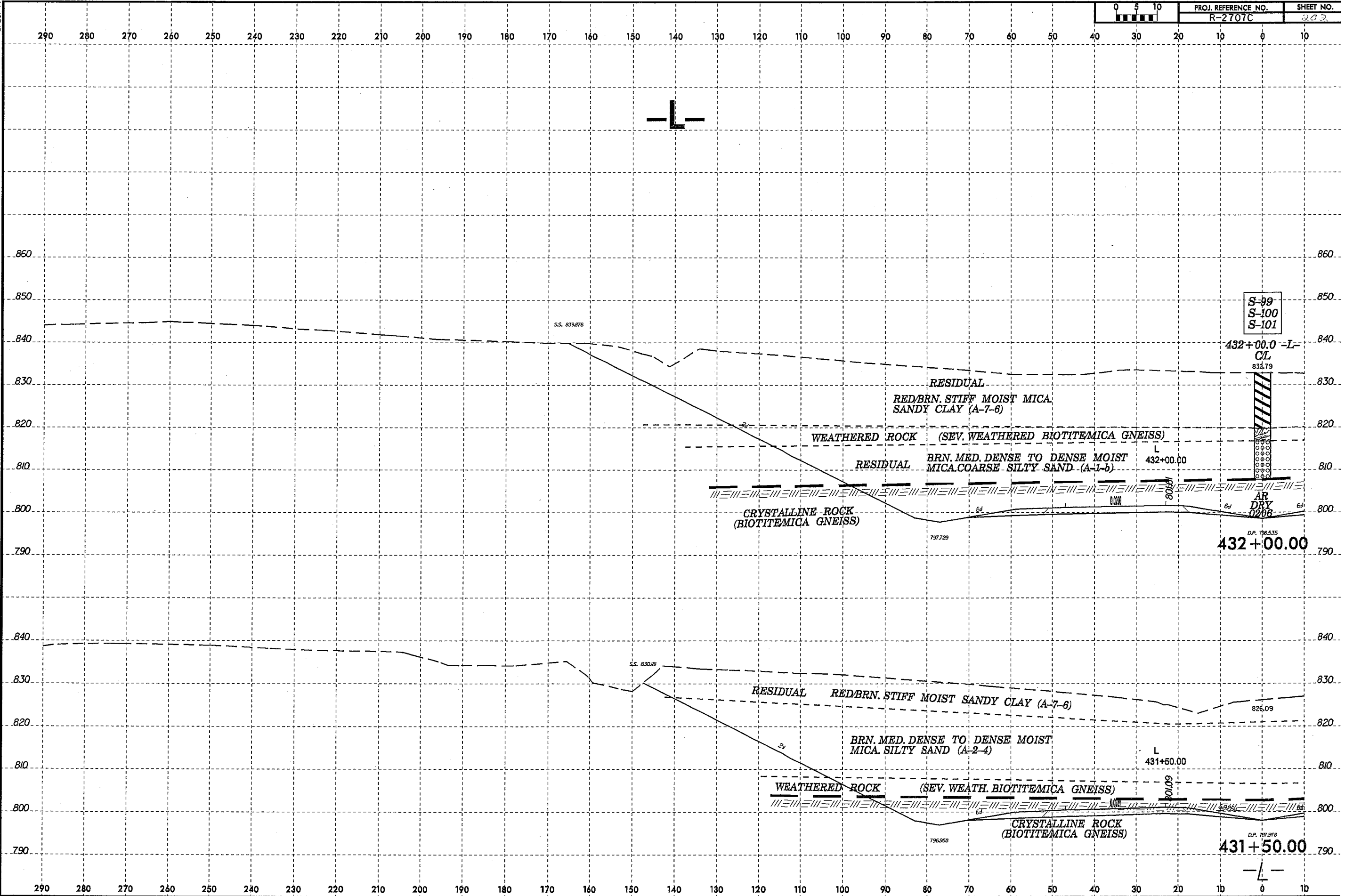


8/23/99  
15-MAY-2008 09:32  
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Author: AL BENZELIS

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 207
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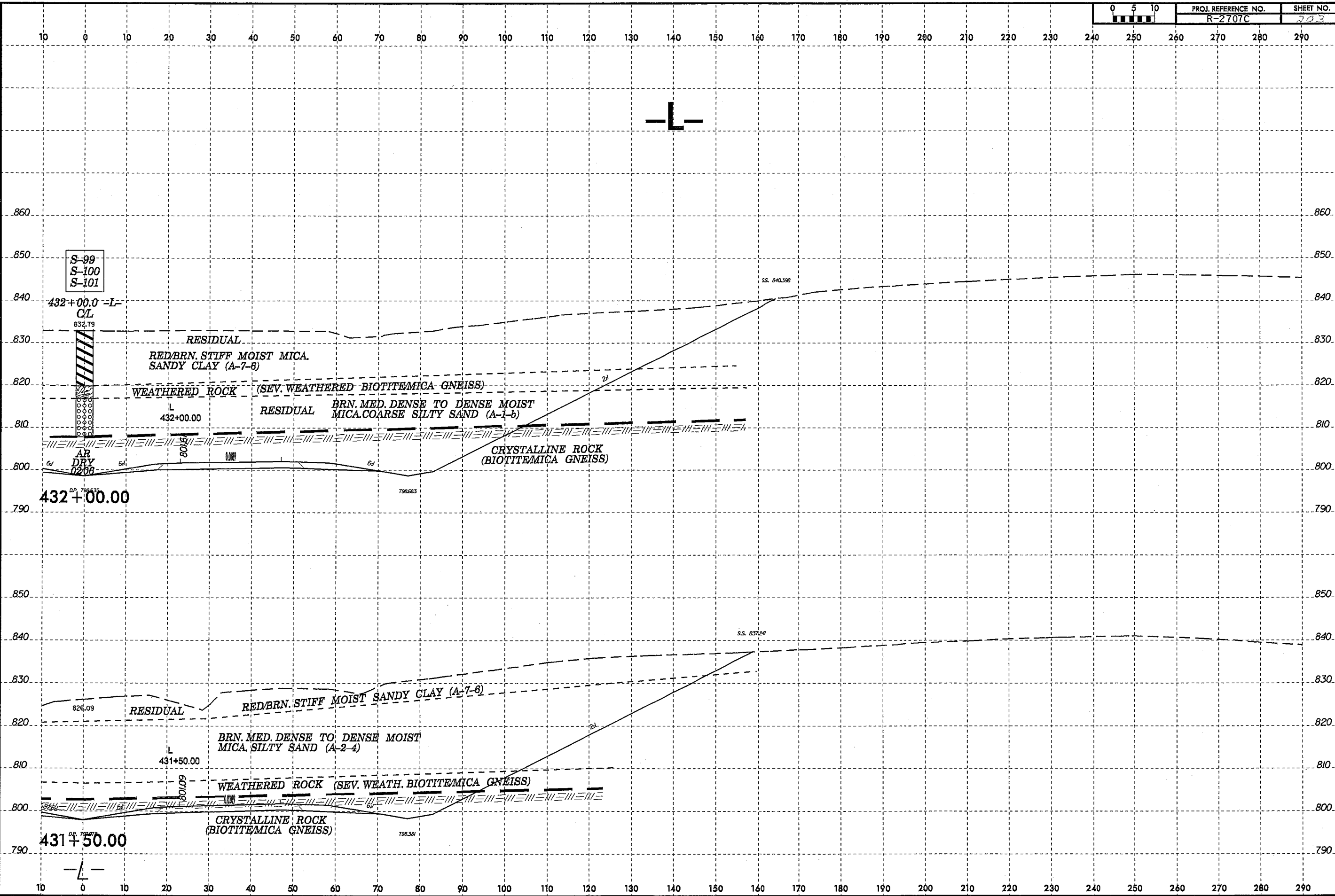
15-MAY-2008 09:35  
c:\projects\p\2707c\geo\_rdwj-cleveland\cadd\_geotech\psc\2707c\rev1\_geo\_xst.l.2.dgn  
Author: RDWJ

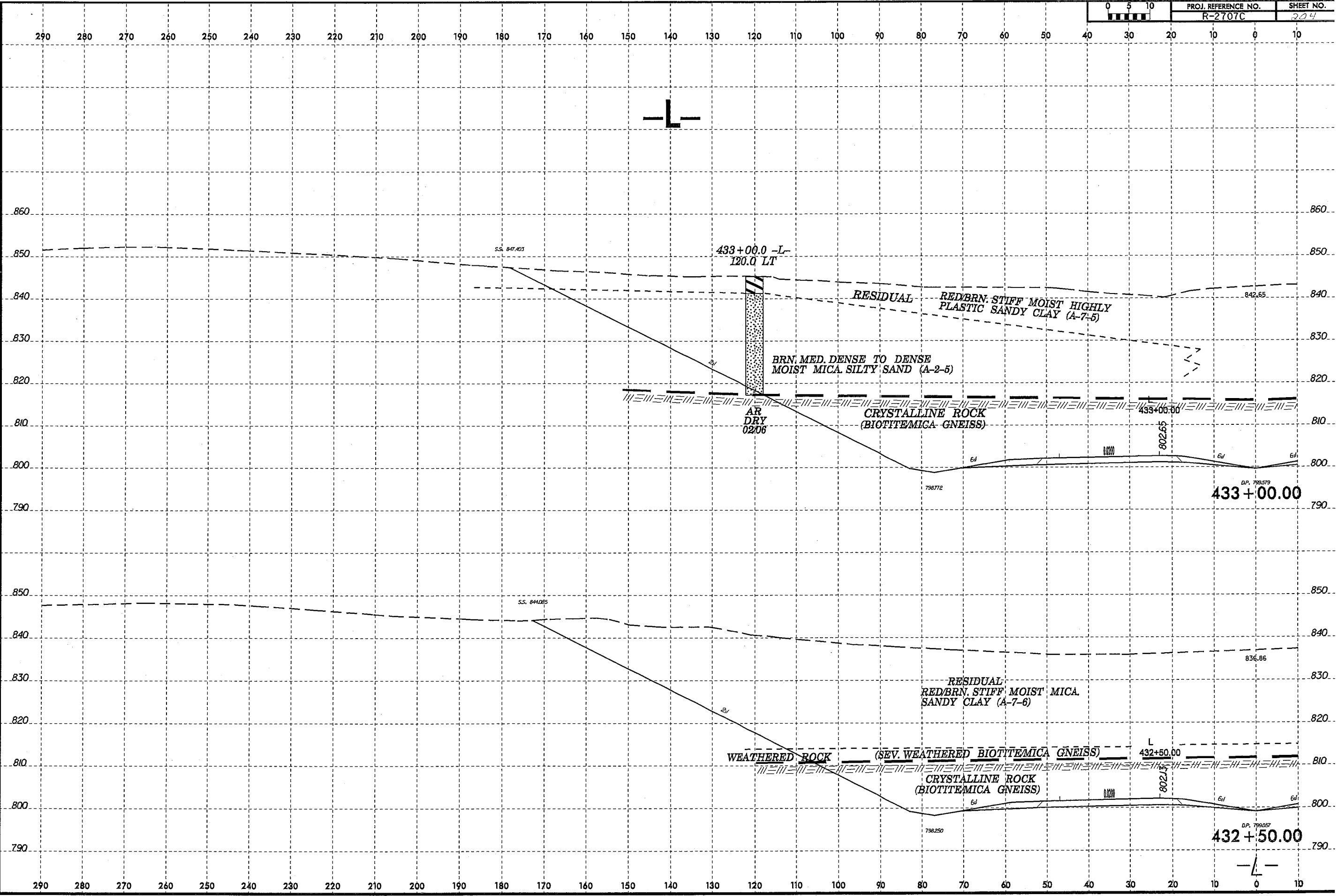


8/23/99

8/23/99  
15-MAY-2008 09:43  
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SHEET NO. 203

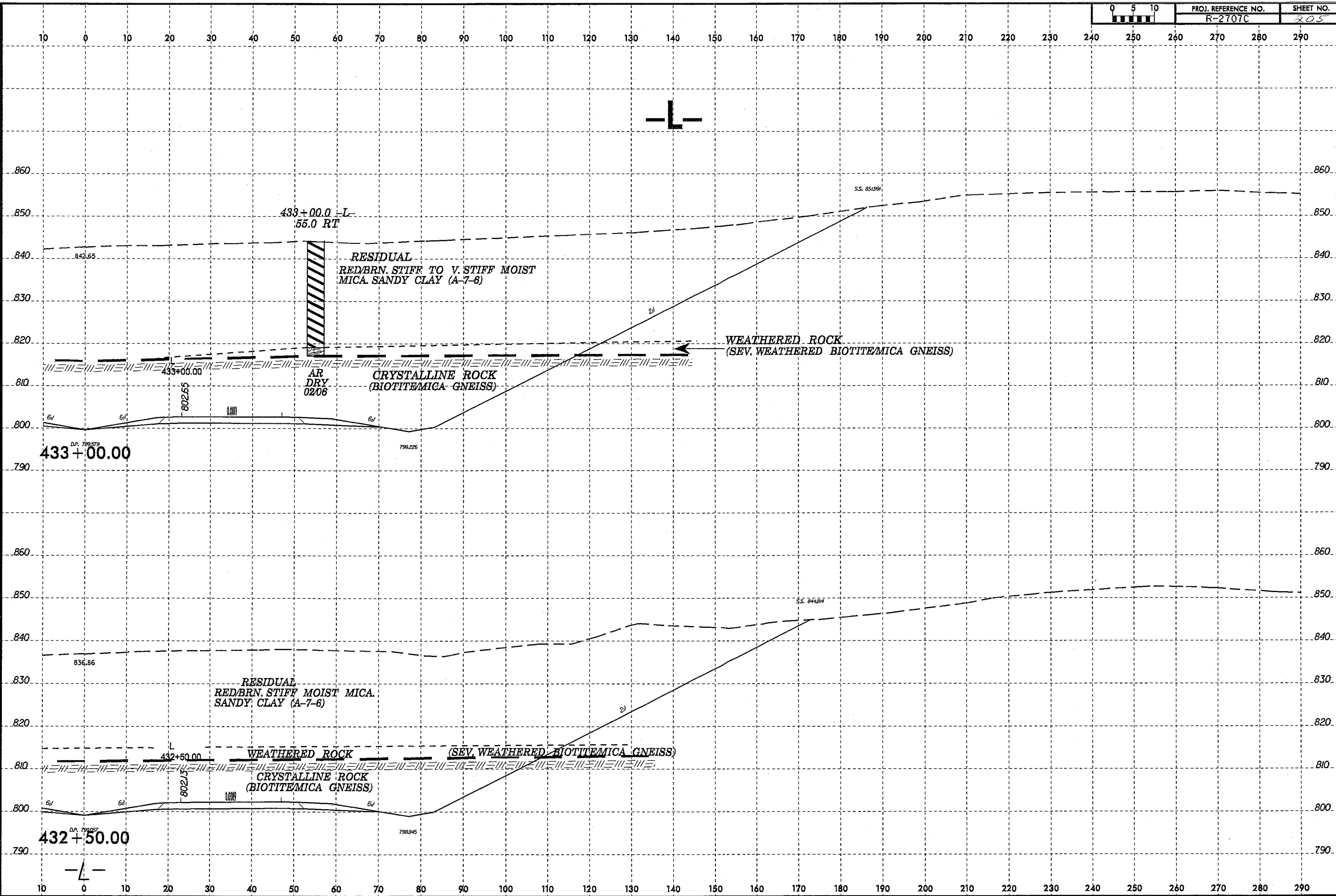
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	203





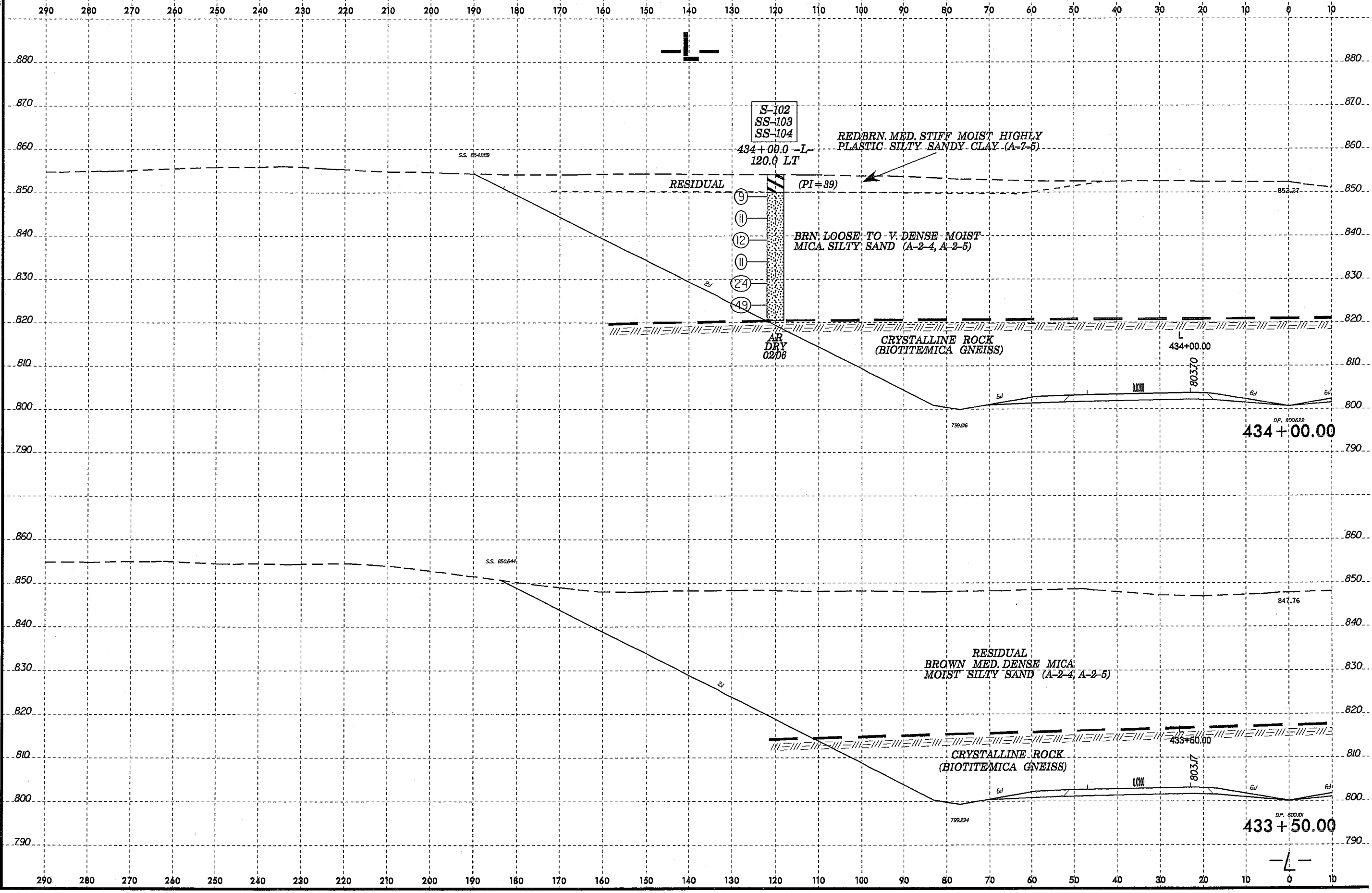
8/23/99

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 205
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15-MAY-2008 09:44  
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drawing: AT GEN226157

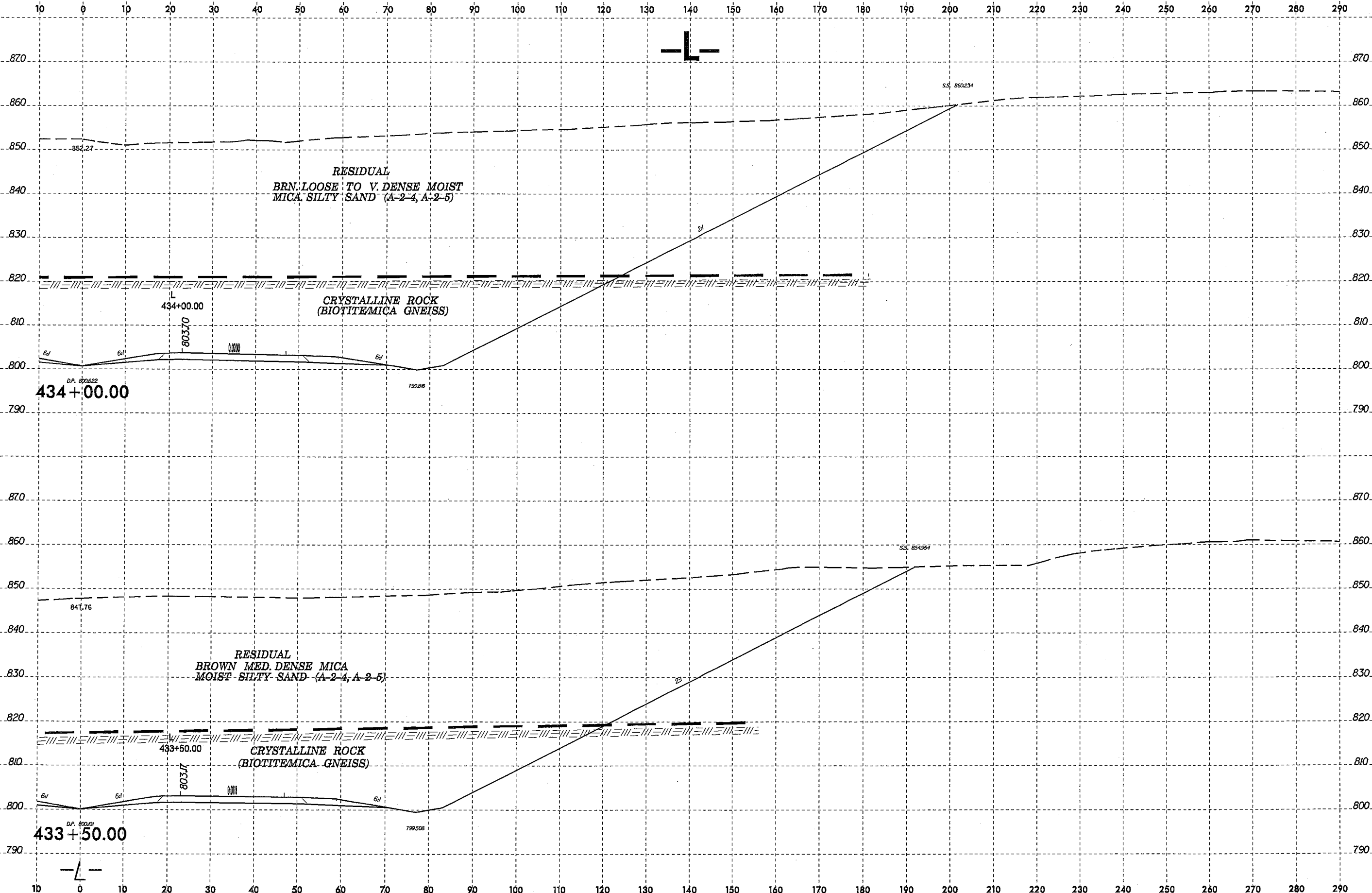
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drawing: AT GE226157





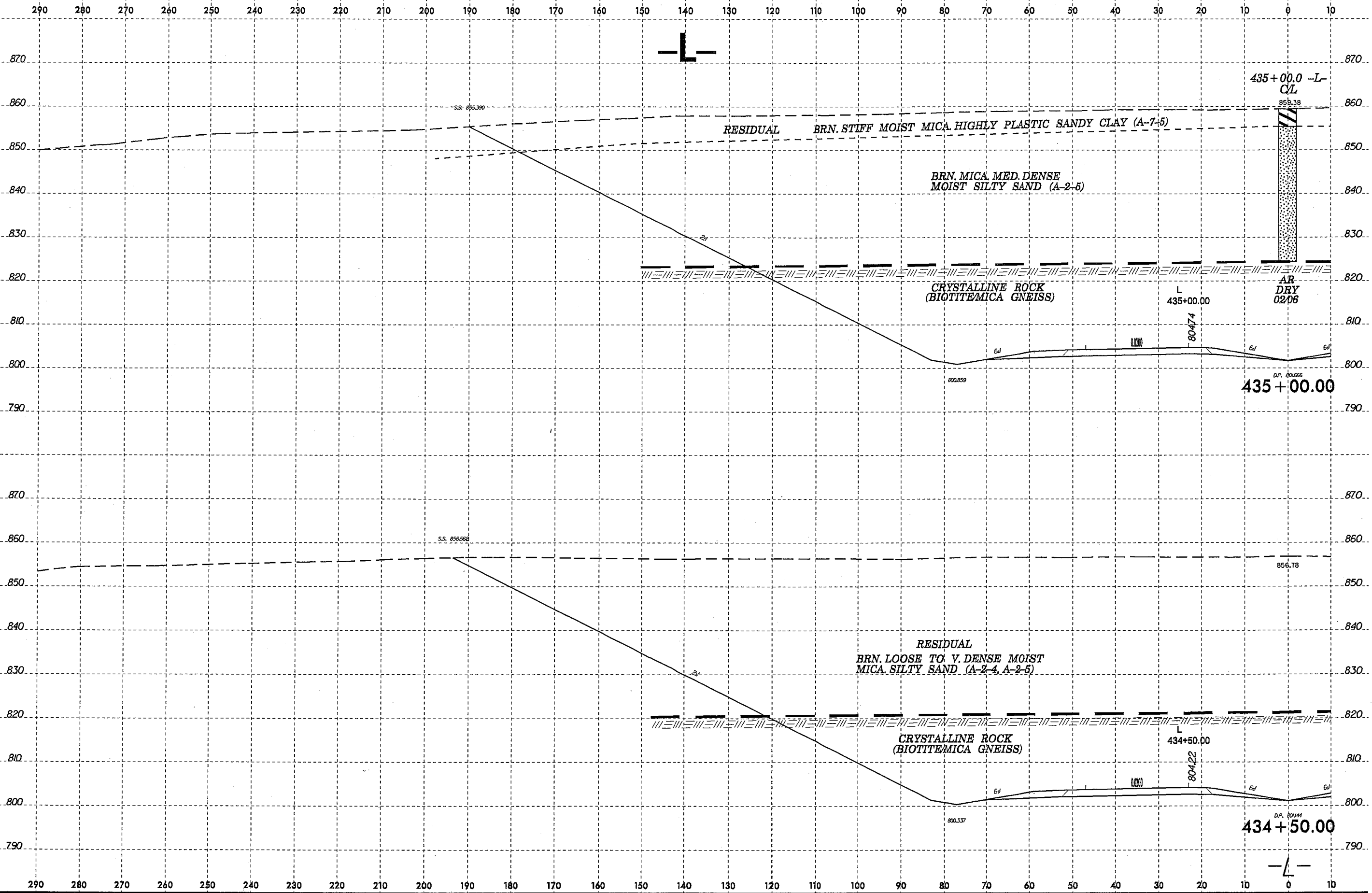
8/23/99  
15-MAY-2008 09:45  
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c:\prj\geogis\2707\2707.dgn  
c:\prj\geogis\2707\2707.dgn  
c:\prj\geogis\2707\2707.dgn  
c:\prj\geogis\2707\2707.dgn

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	227



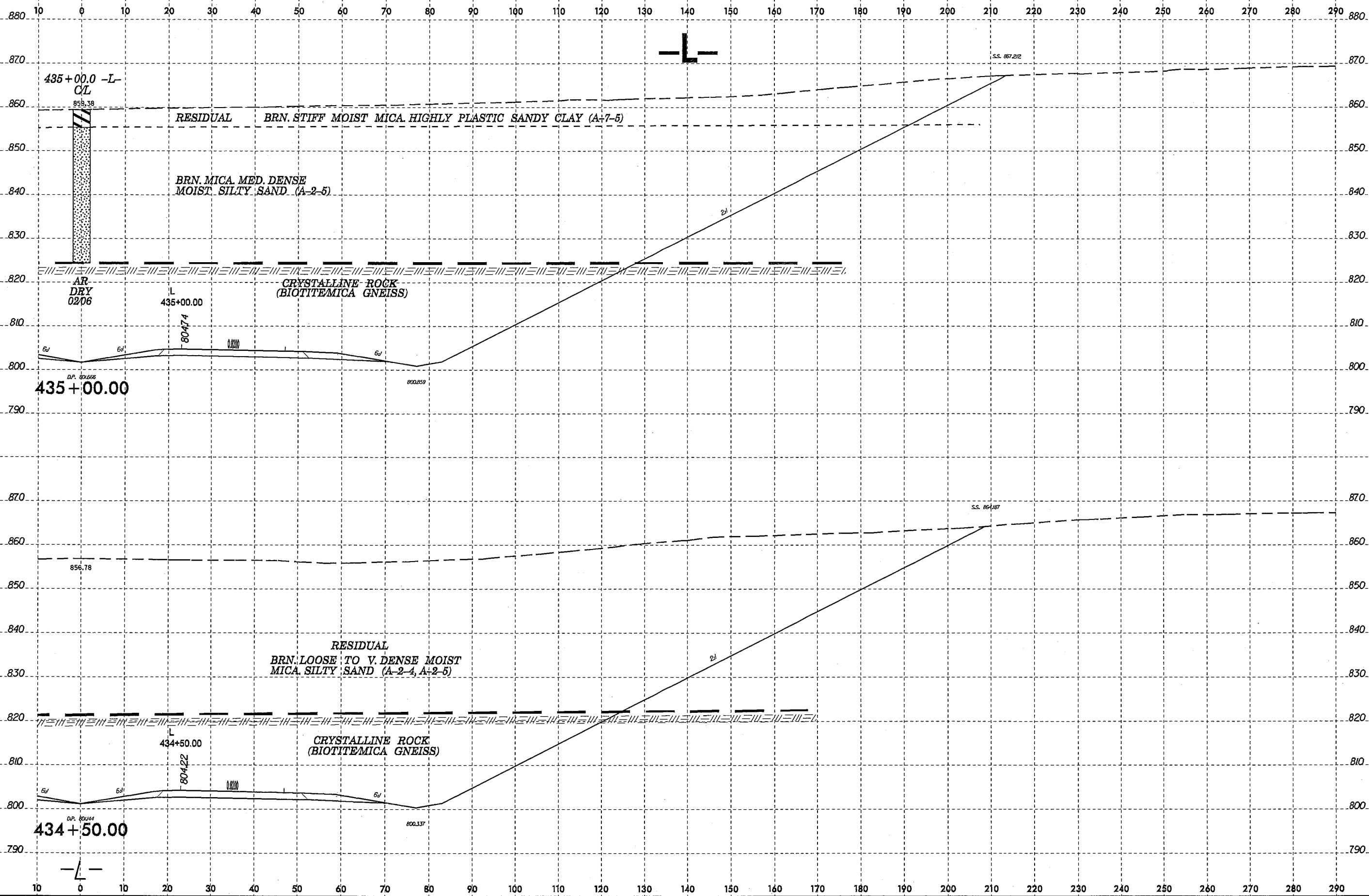
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AL: 06/22/08

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	208



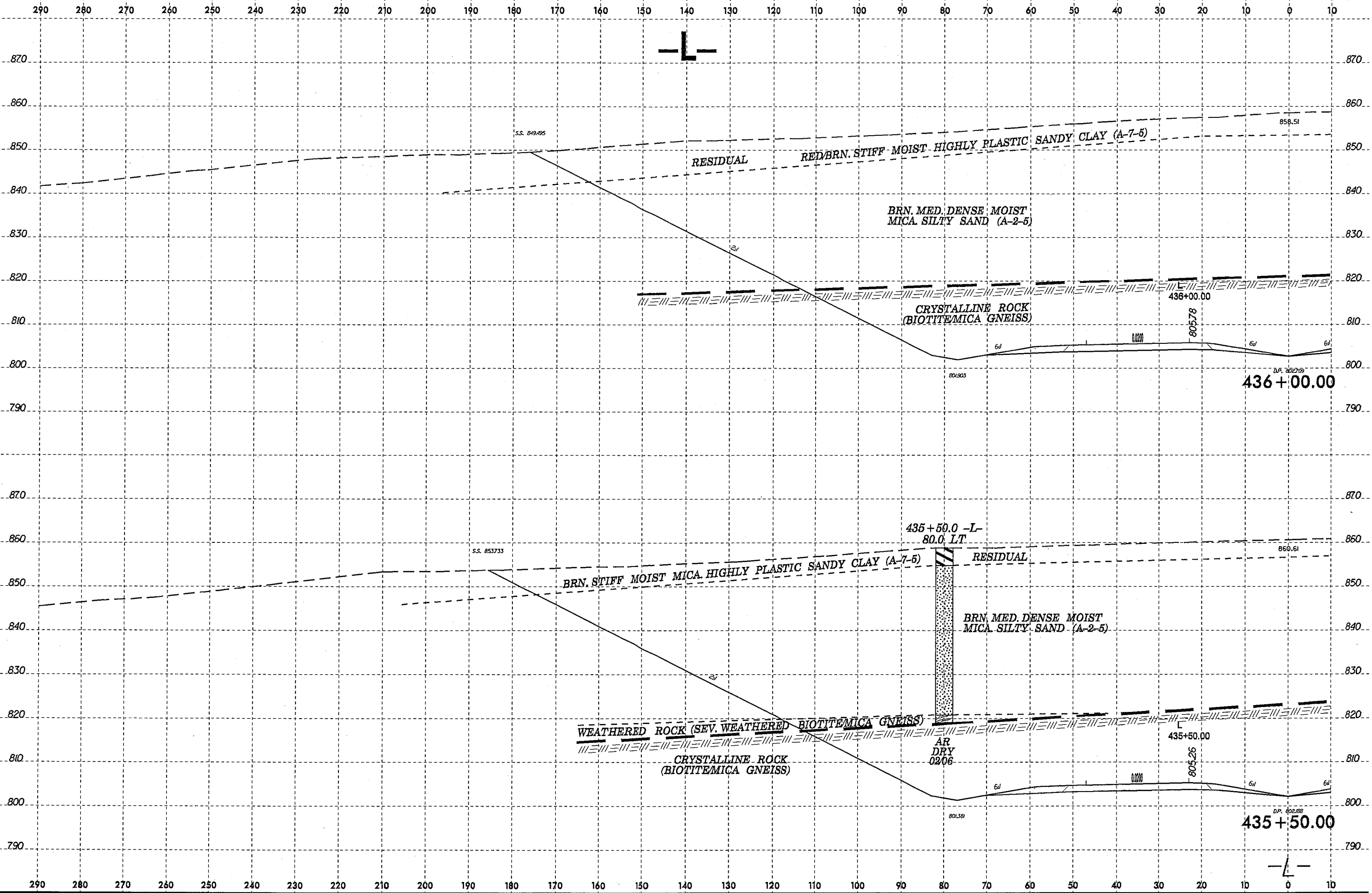
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15-MAY-2008 09:47  
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clburris AT 06/22/07

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	309



8/23/99

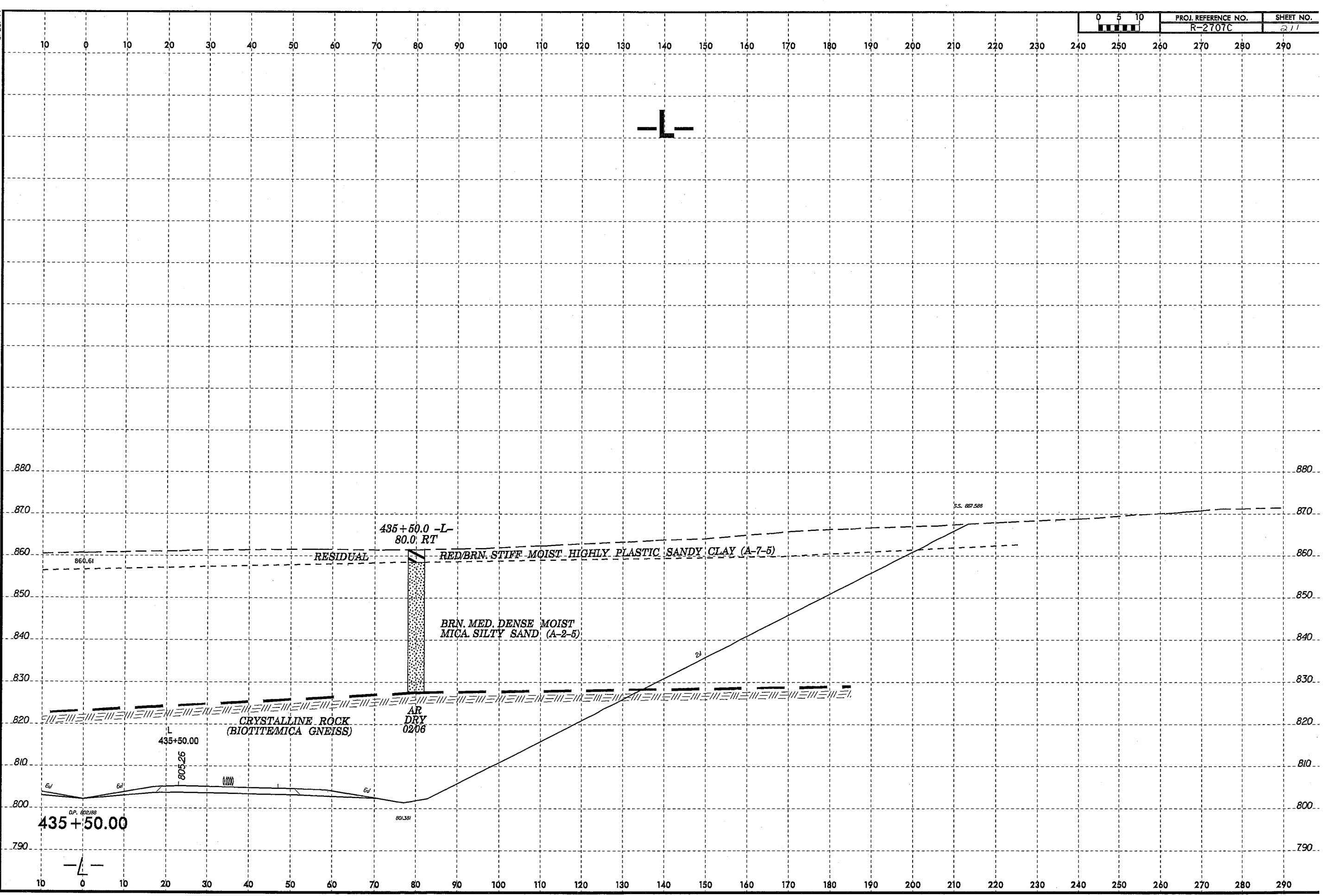
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	2/10



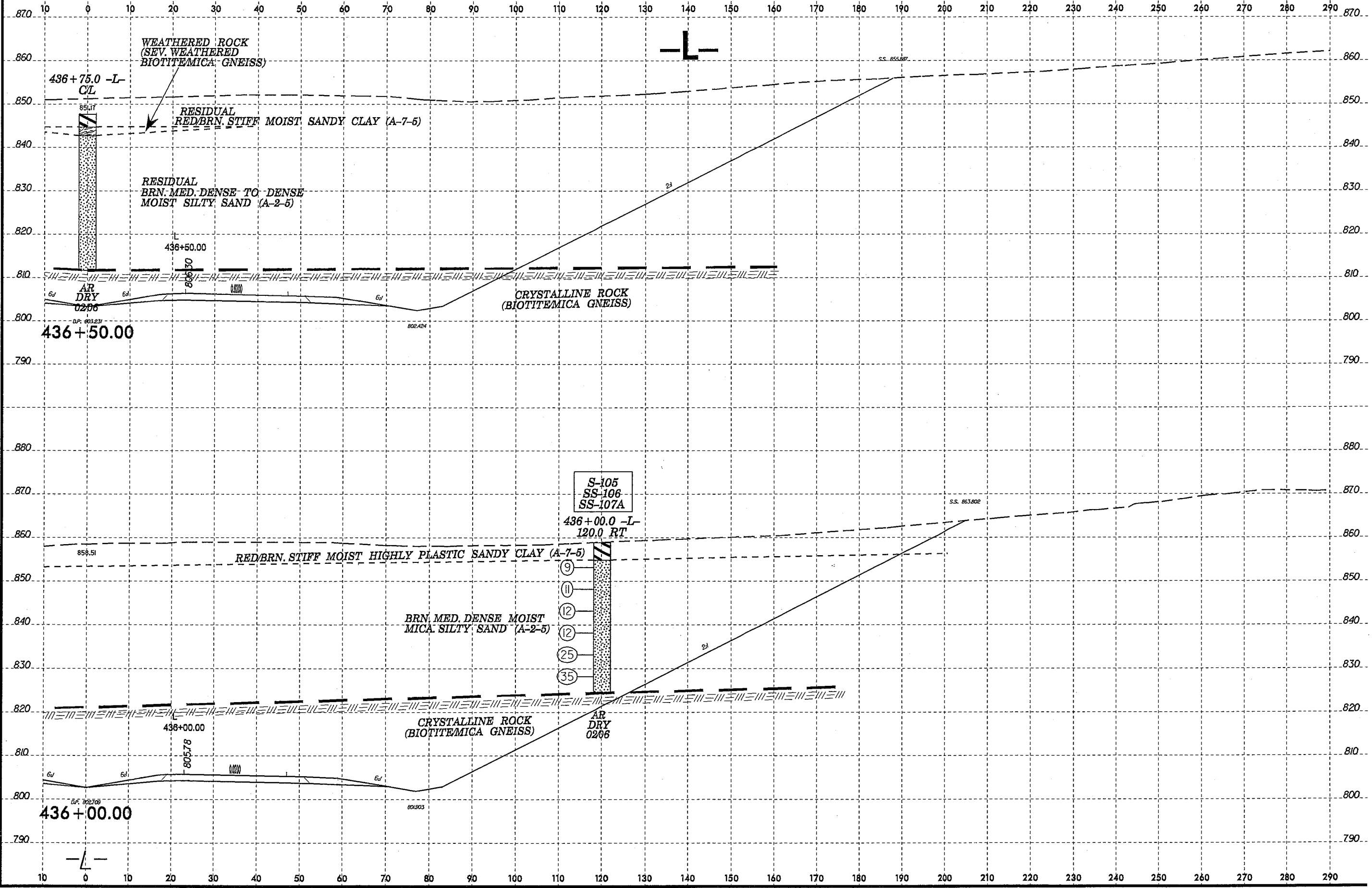
15-MAY-2008 09:38  
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 AT: 064226157

8/23/99  
15-MAY-2008 09:48  
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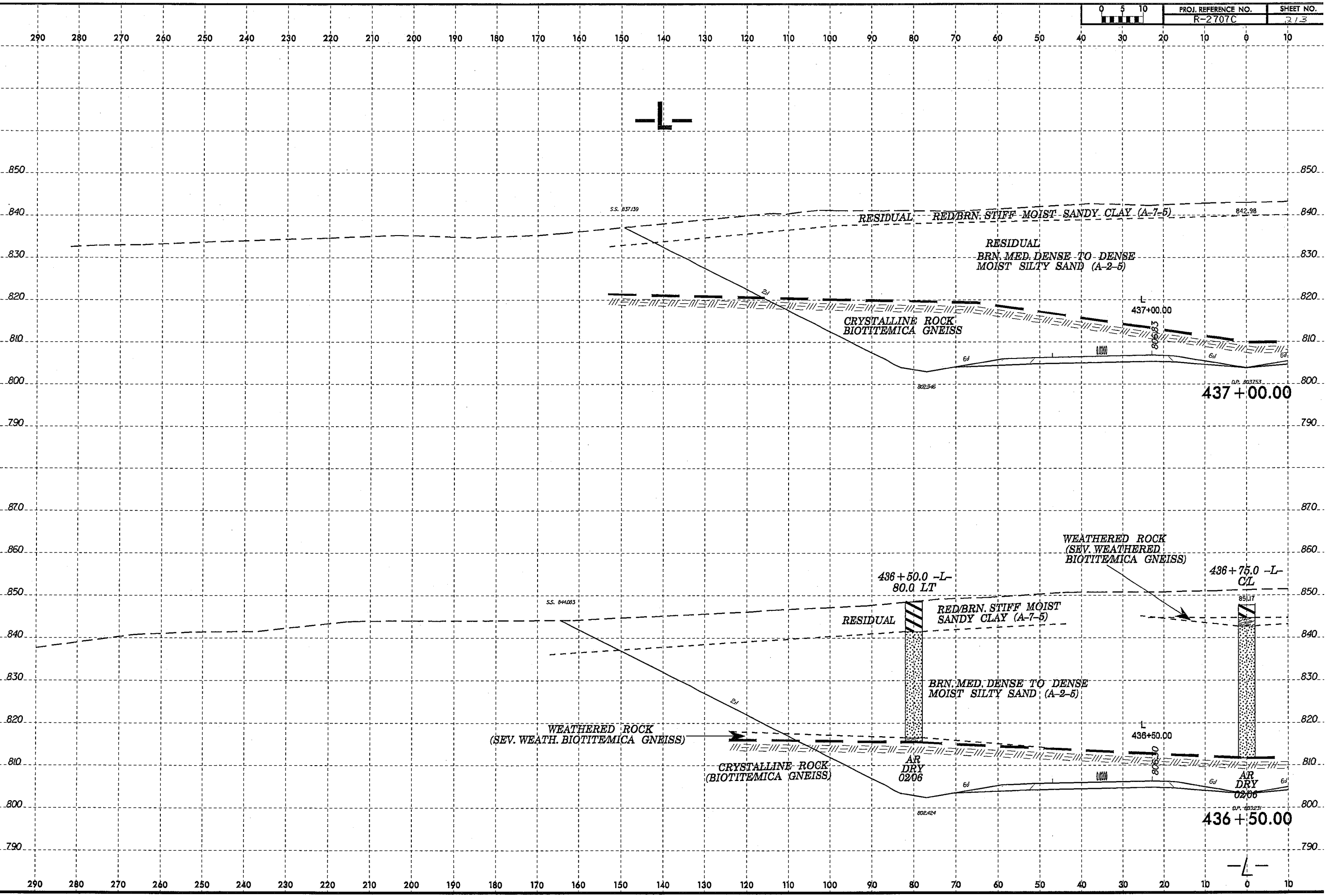
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	211



8/23/99  
27-MAY-2008 13:45  
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Author: AT\_BENJ228157  
Geo: rdmj-cleveland\coadd\_geotech\sscvr2707\civil\geo\_xsa.1.dwg

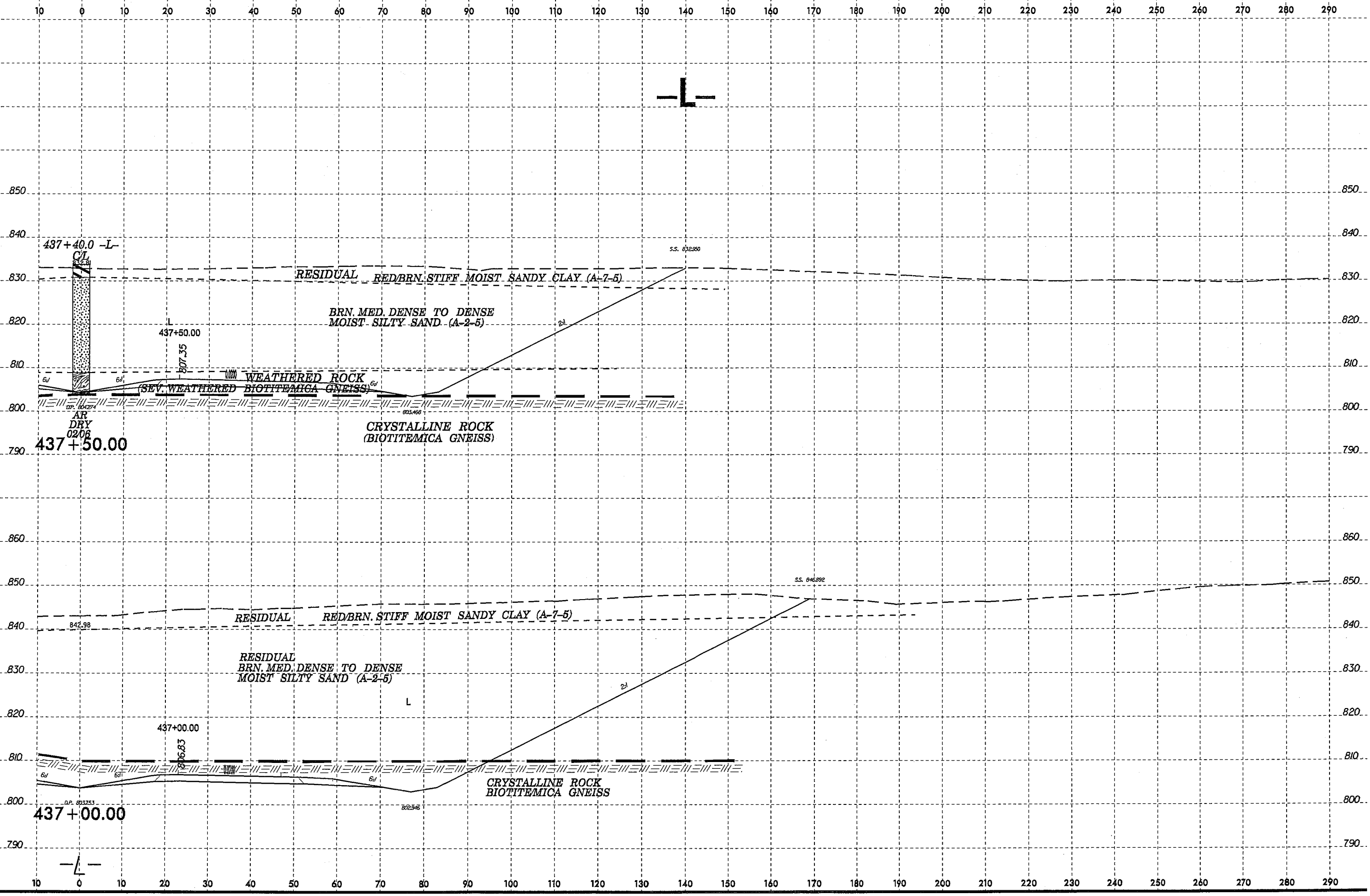


15-MAY-2008 09:39  
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ssu\1.2.dwg  
R1 06/26/07



16-MAY-2008 10:22  
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c:\projects\2707\civil\land\cadd-geotech\ssc\2707\civil-geo\ssu.1.1.dgn  
c:\projects\2707\civil\land\cadd-geotech\ssc\2707\civil-geo\ssu.1.1.dgn

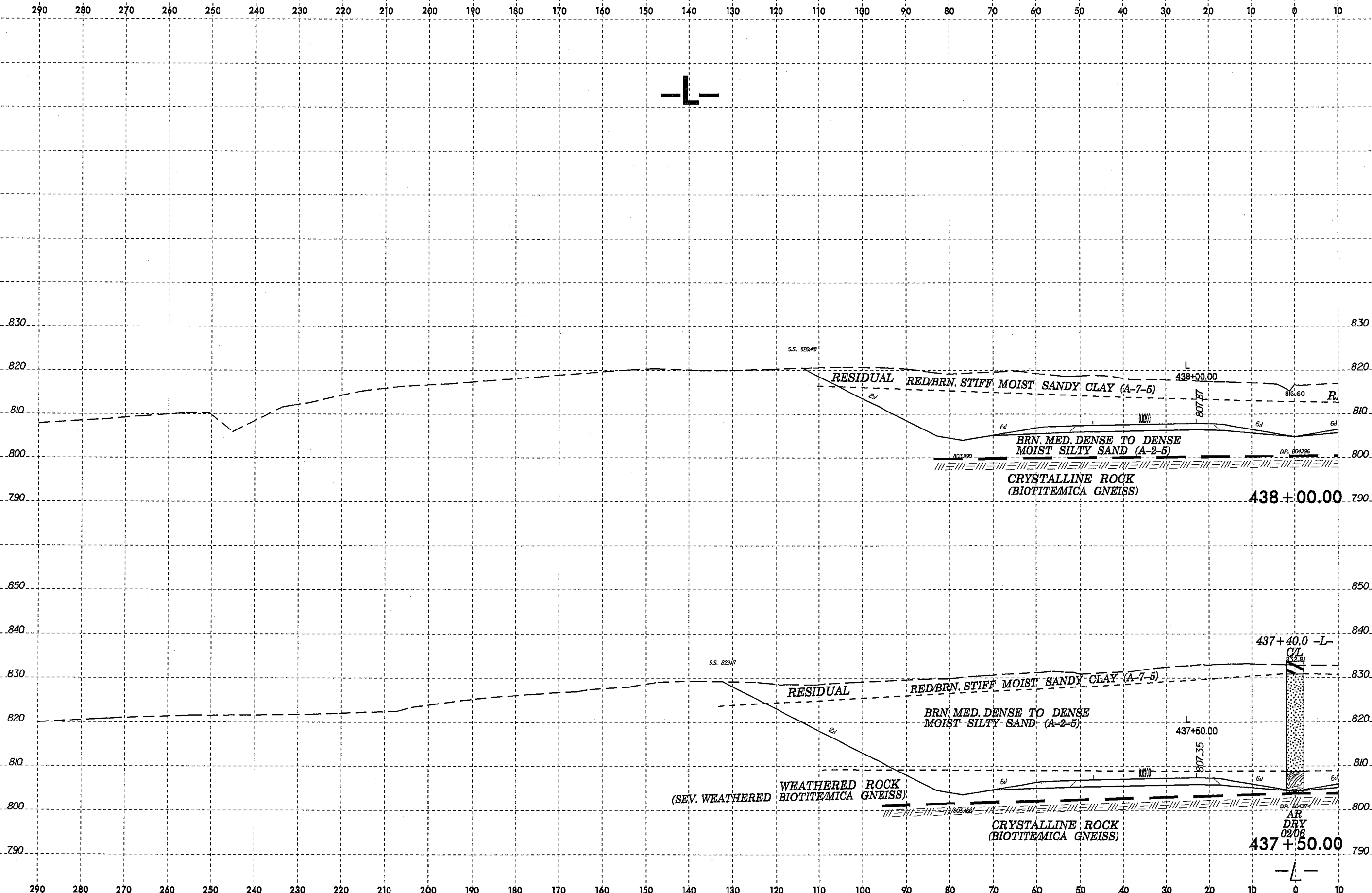
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	214





8/23/99

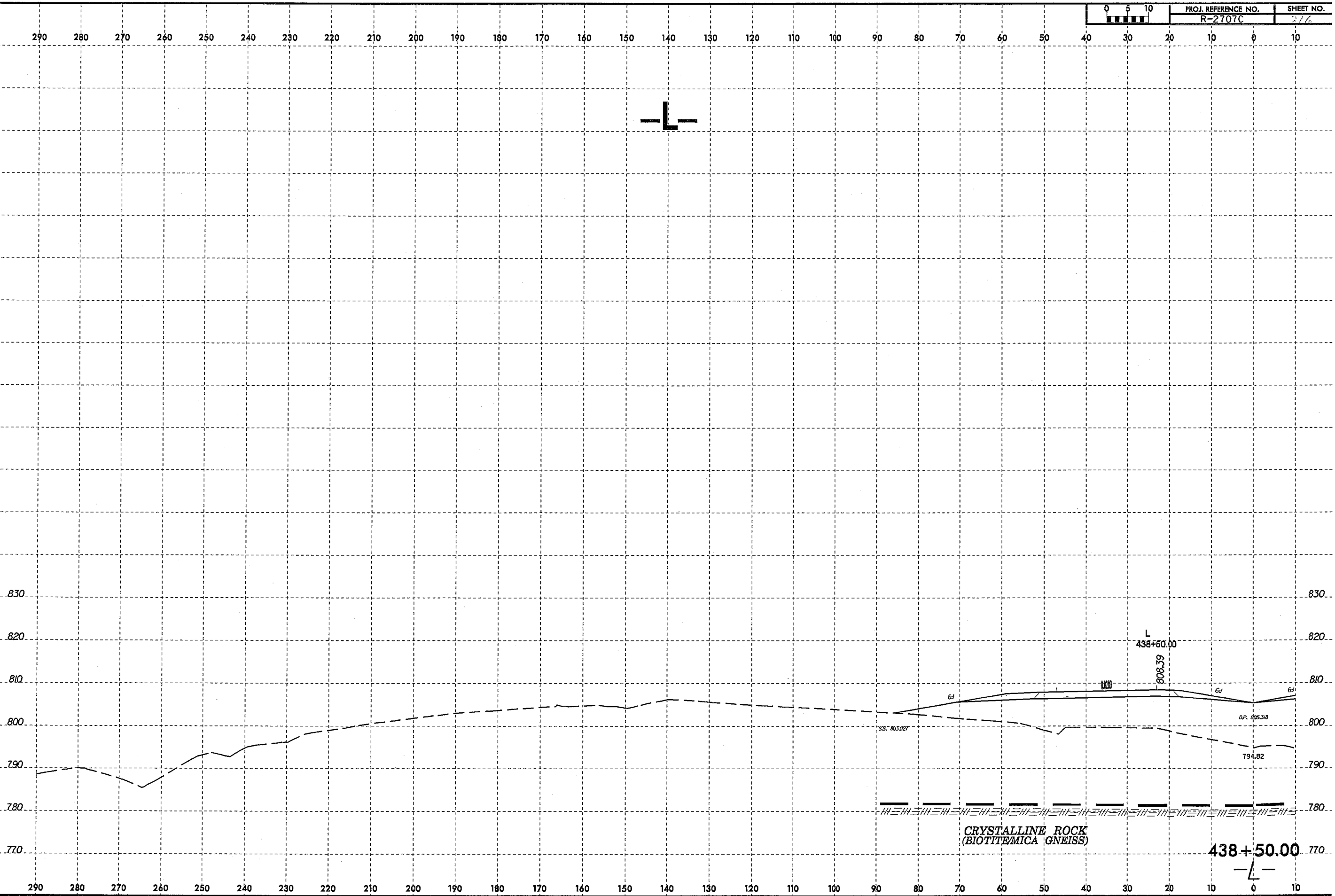
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	215



15-MAY-2008 10:21  
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churr13 AT 06/22/08

8/23/99

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 216
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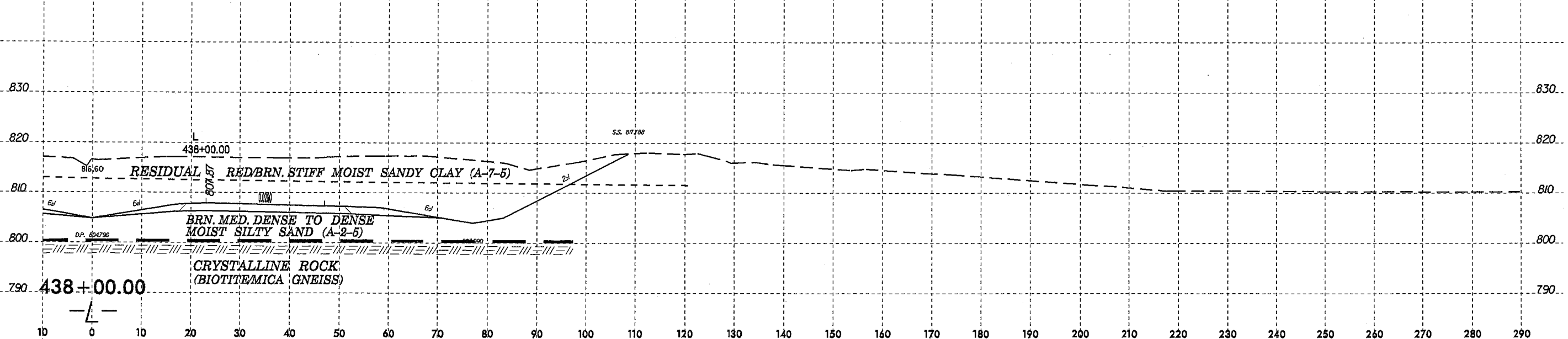
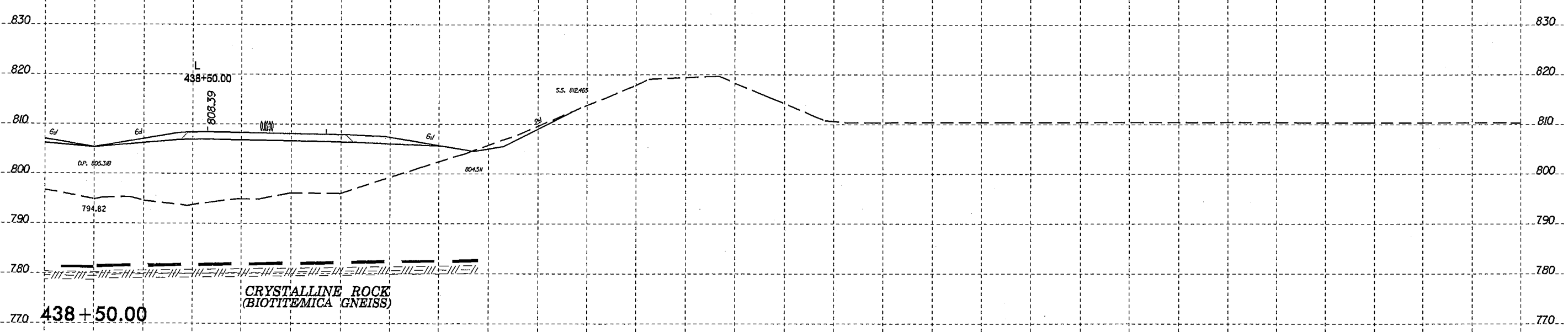
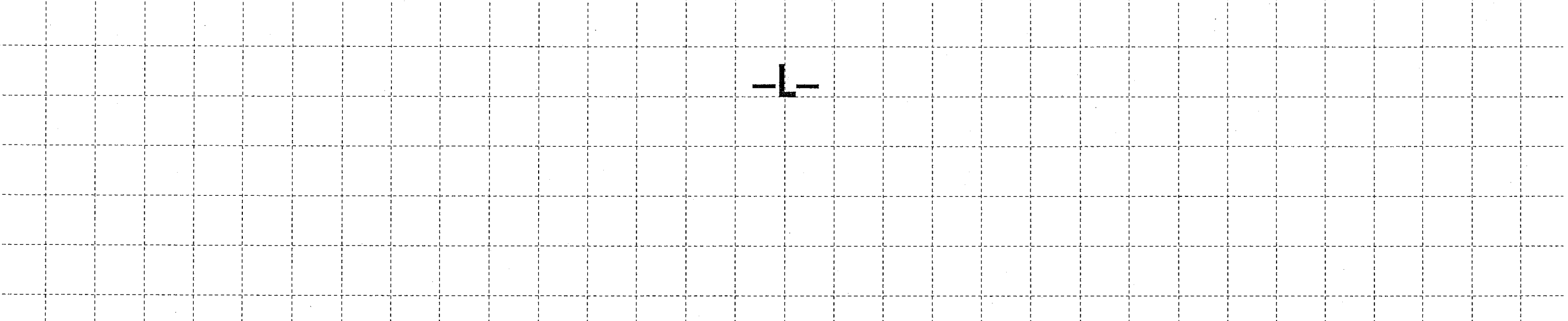


15-MAY-2008 10:33  
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 AL 06H26157

8/23/99

0	5	10	PROJ. REFERENCE NO.	SHEET NO.
[Scale bar]			R-2707C	217

10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290

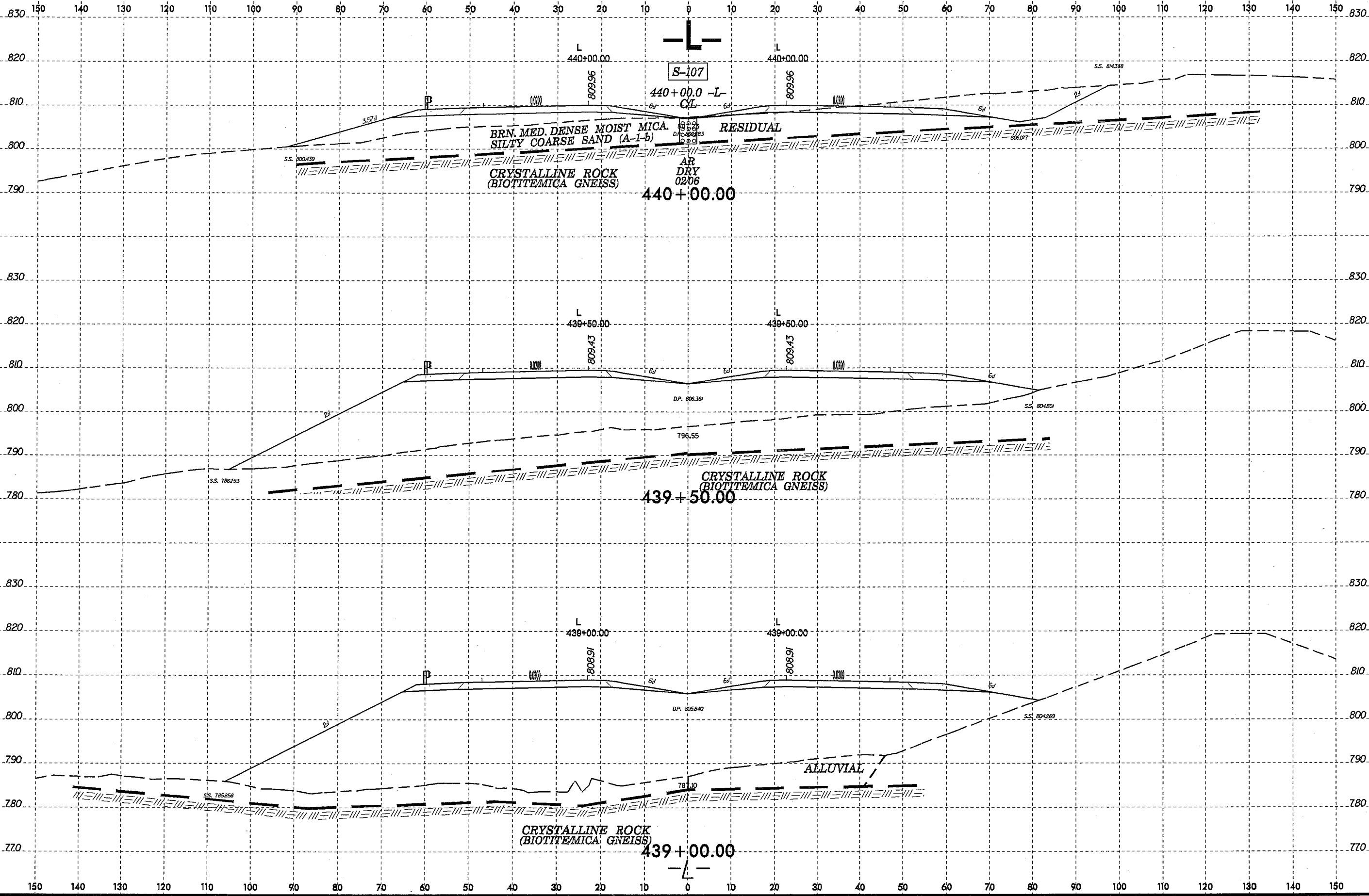


10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290

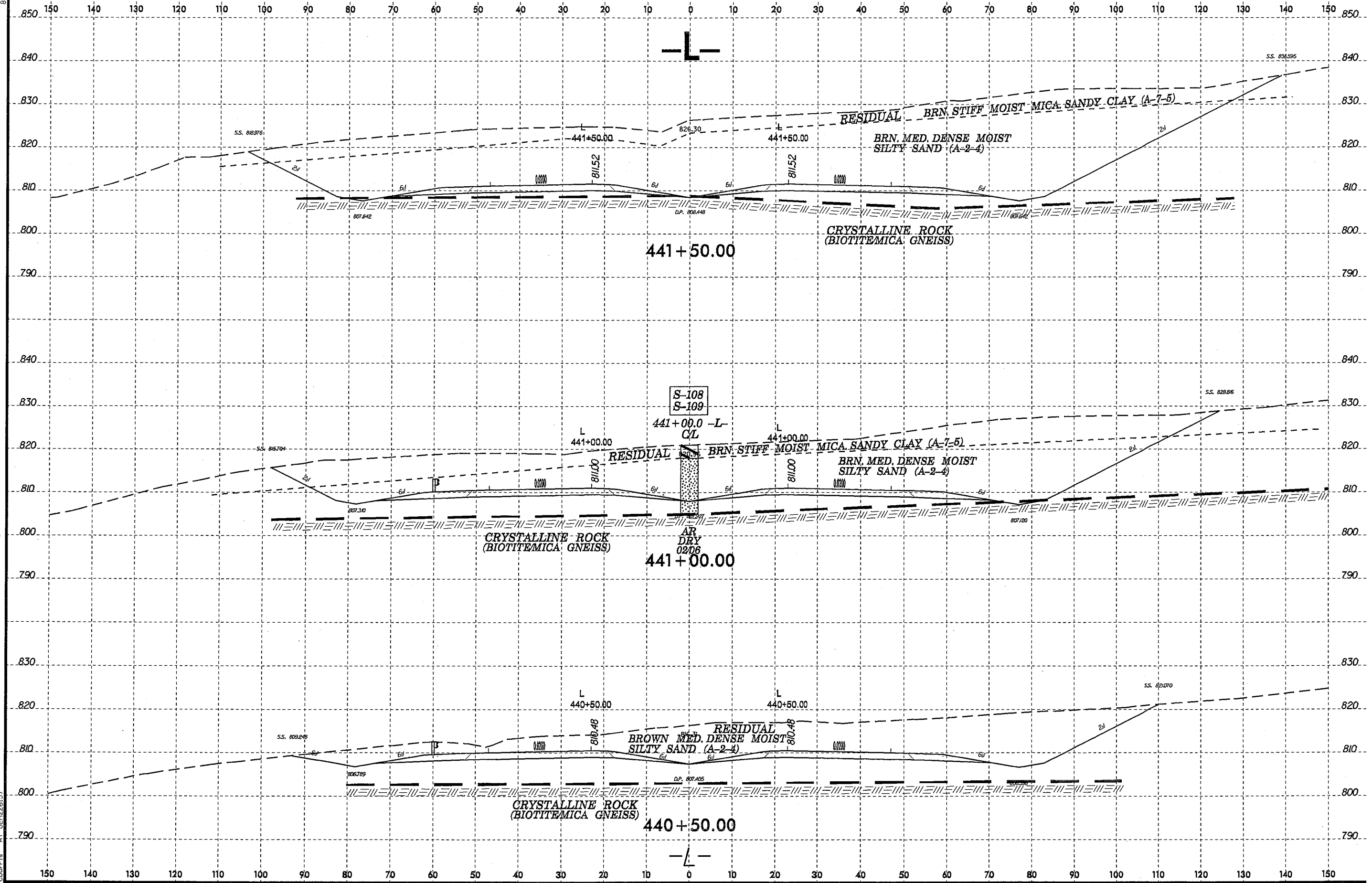
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 8/23/99 AT 08:26:57

8/23/99  
16-MAY-2008 10:35  
d:\projects\2707\5(rev)\_geo\_rdmj-claveland\cadd\geotech\ssc\vr2707c(rev).geo\_xst.1.2.dgn  
churnis AT DEH26157

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 218
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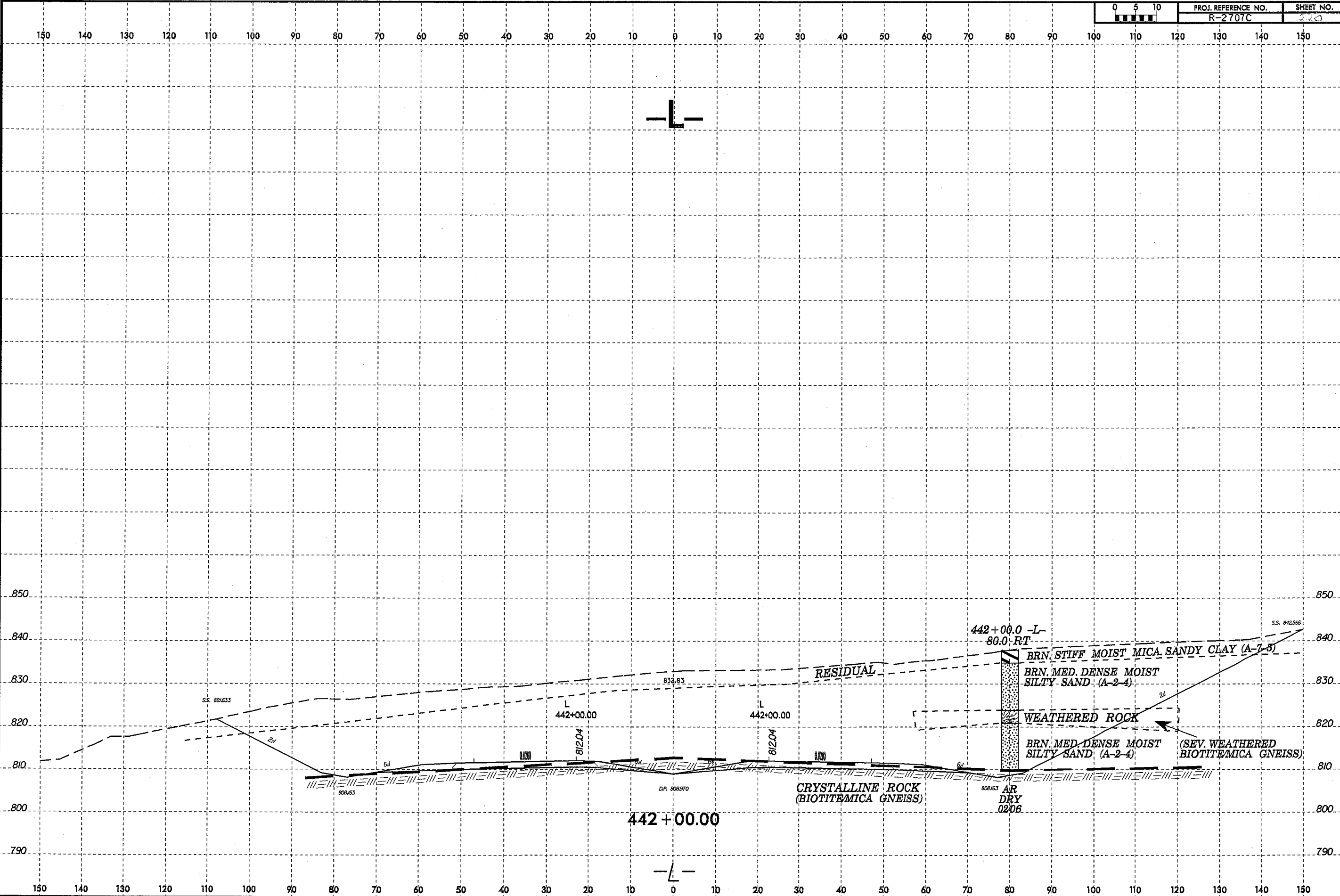


8/23/99  
15-MAY-2008 10:03  
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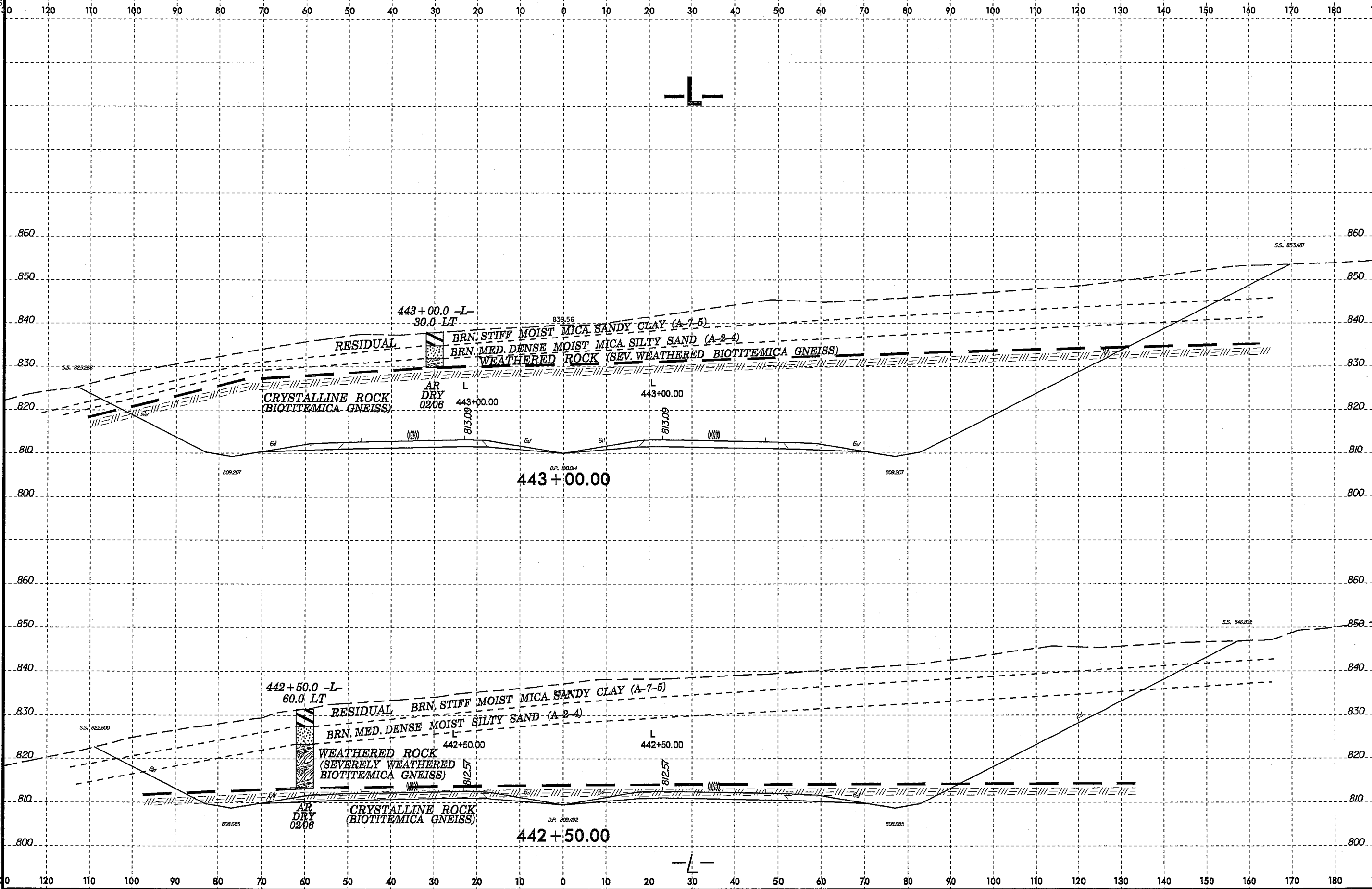
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dwg: 2707\567\geo\_rdwj-cleveland\ceadd\geotech\csc\2707\civ\1\geo\_xsl\1.2.dgn  
sheet: 1 of 1

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 220
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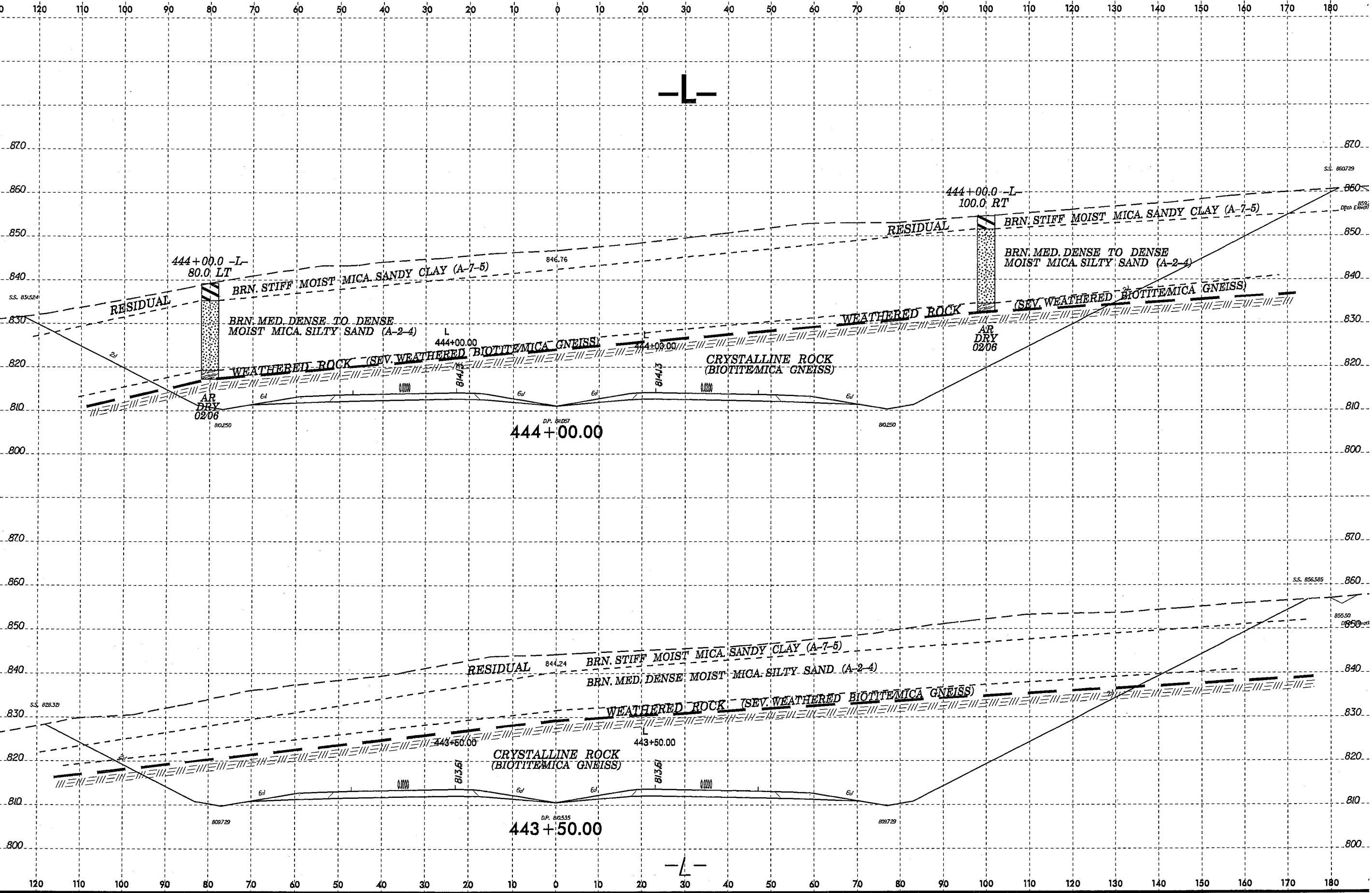
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User: r1\_0626157

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 271
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15-MAY-2008 10:05  
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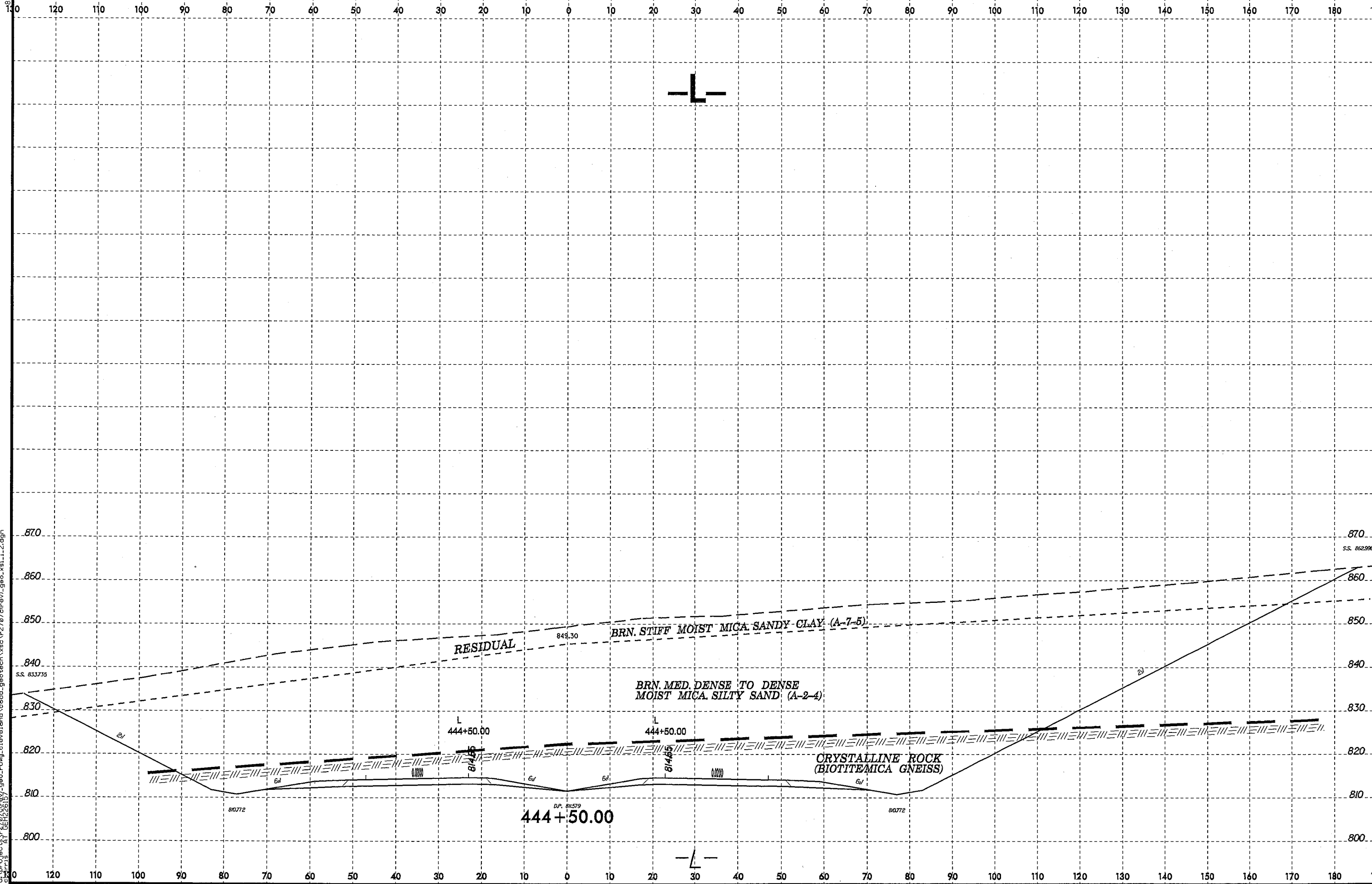
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	222





15-MAY-2008 10:05  
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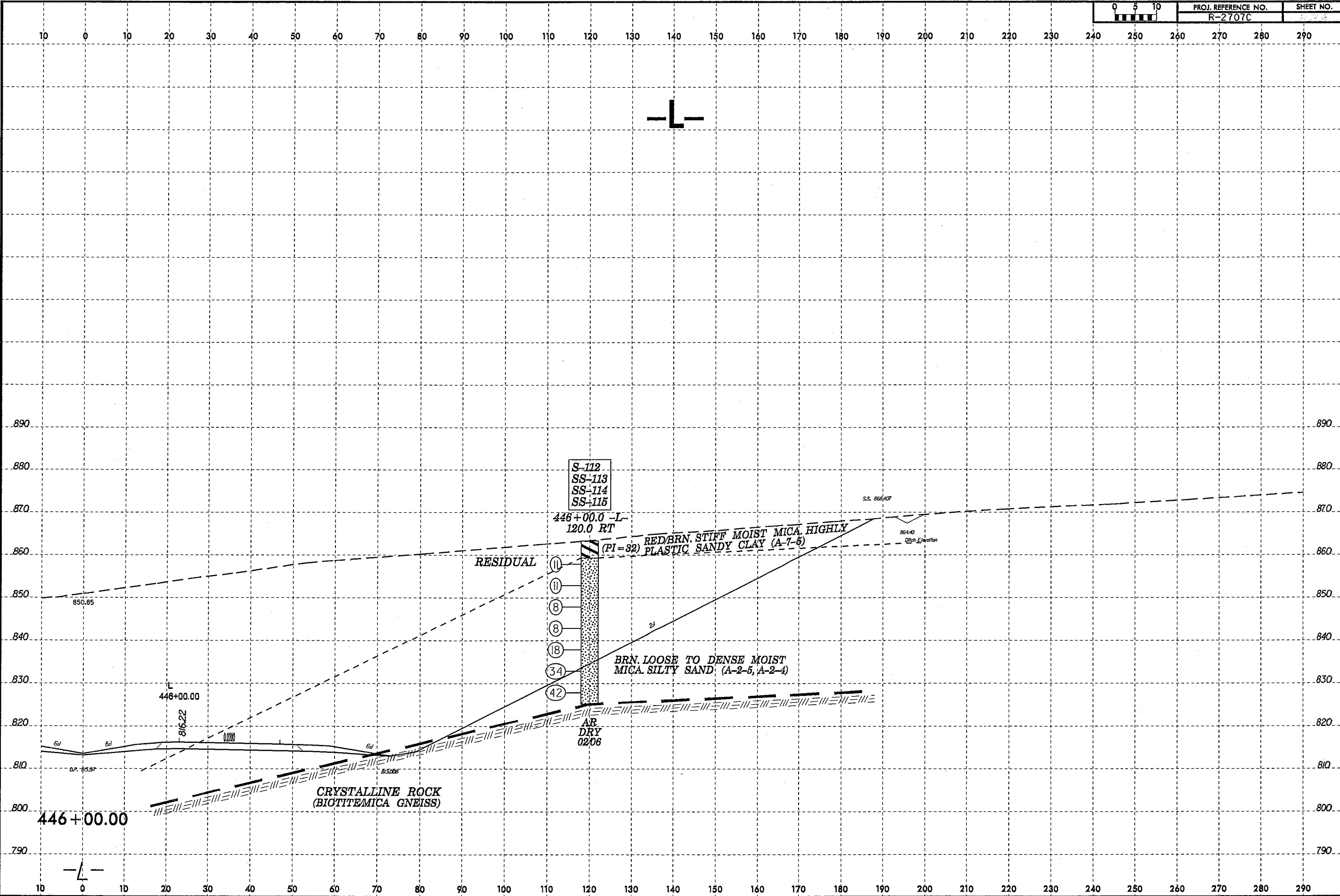
0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 223
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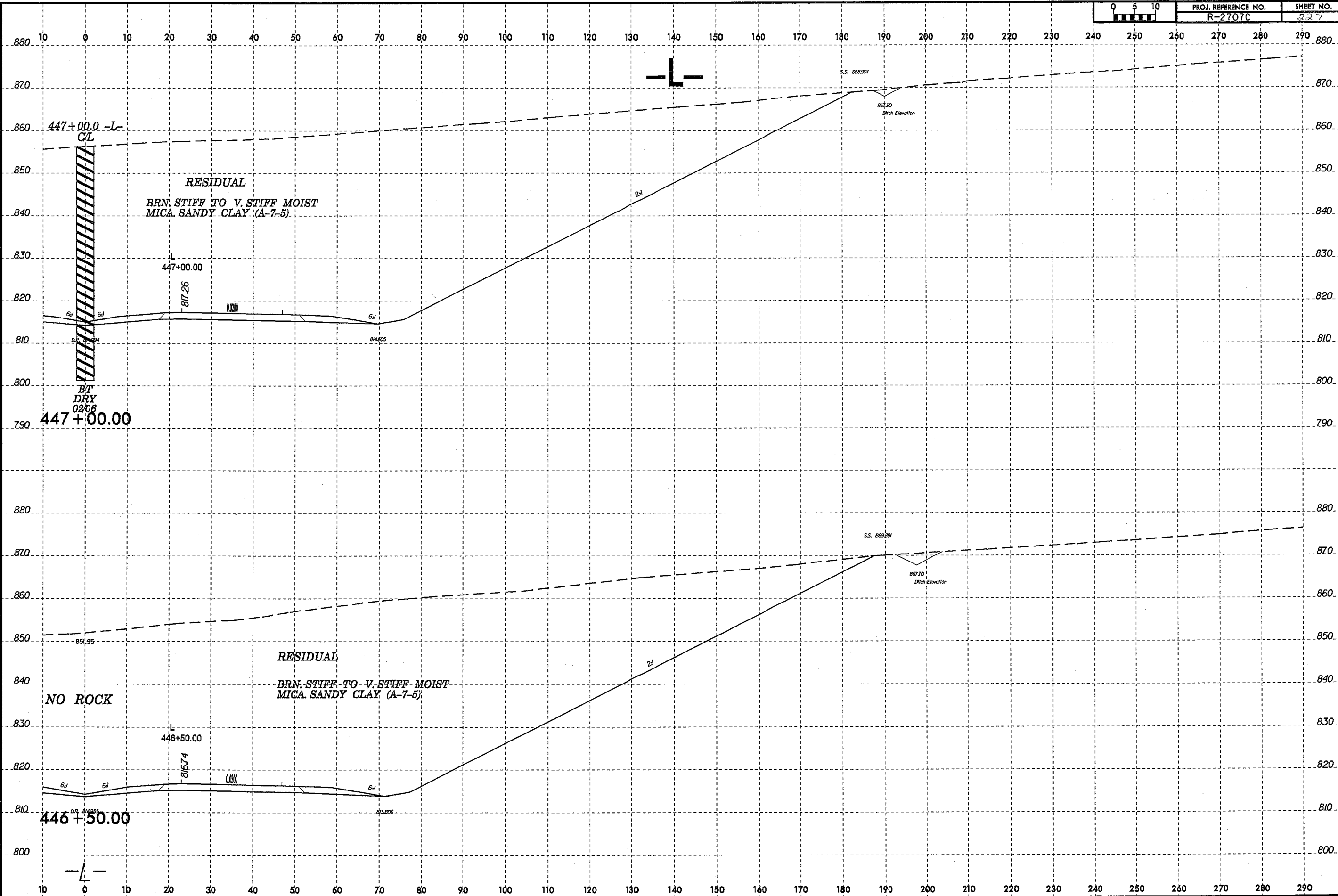


8/23/99  
25-MAY-2008 09:43  
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S:\proj\2707\2707-geo.rdw\cleveland\cadd-geotech\ssc\2707\clev\l\_geo\_xa.1.dgn



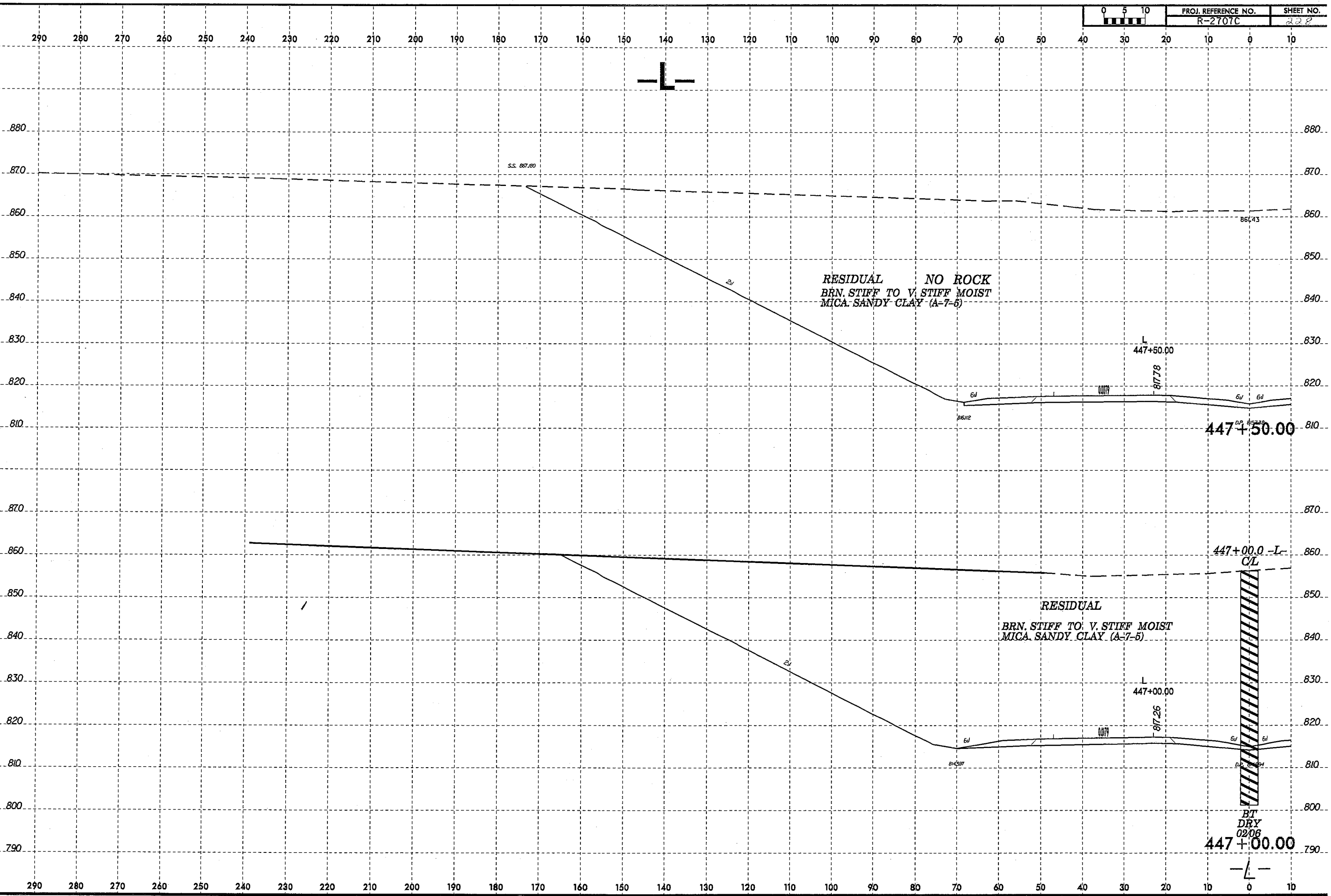
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gburris AT BEH26157

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	227



8/23/99

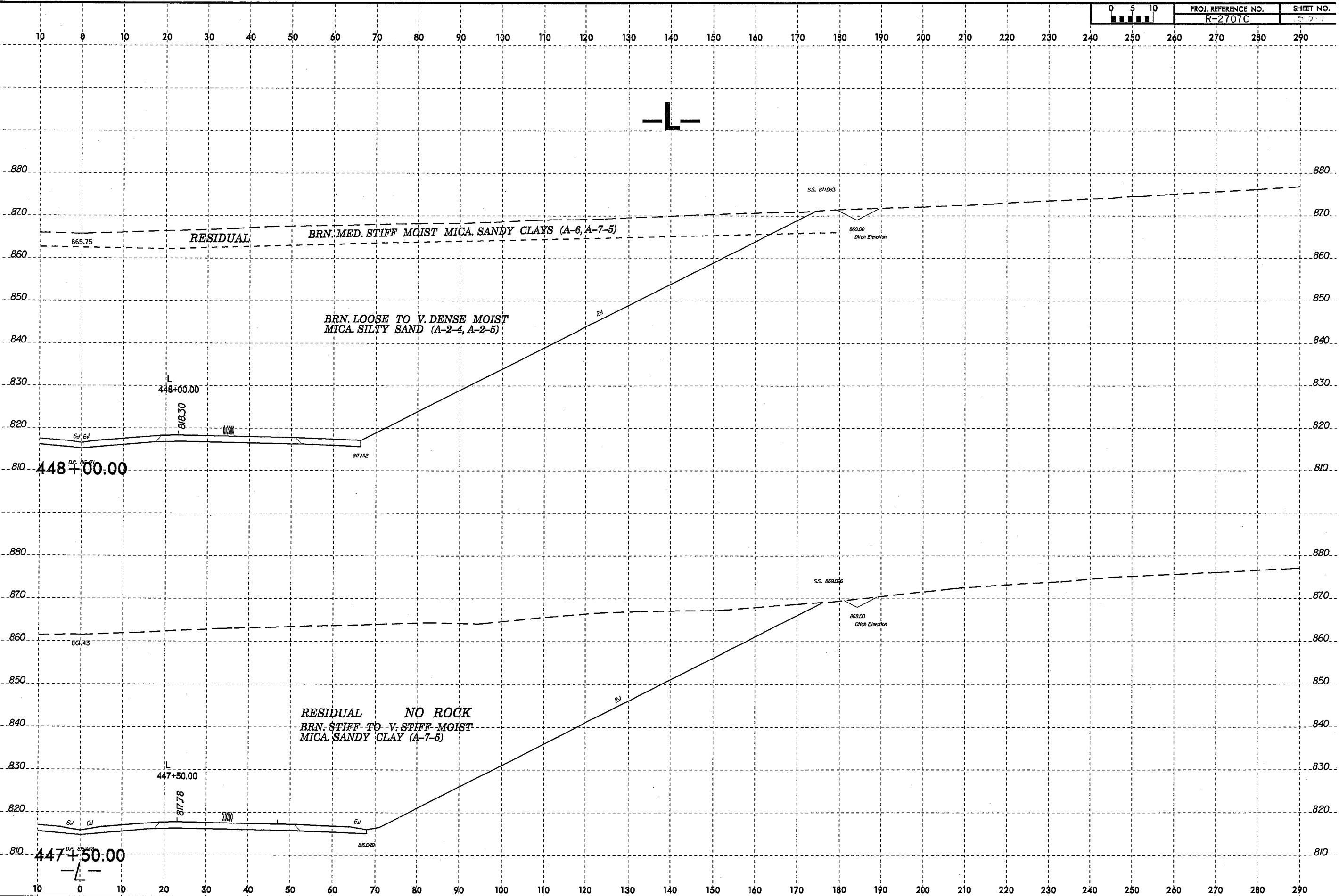
0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 222
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16-MAY-2008 11:23  
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 geotech AT DEH26157

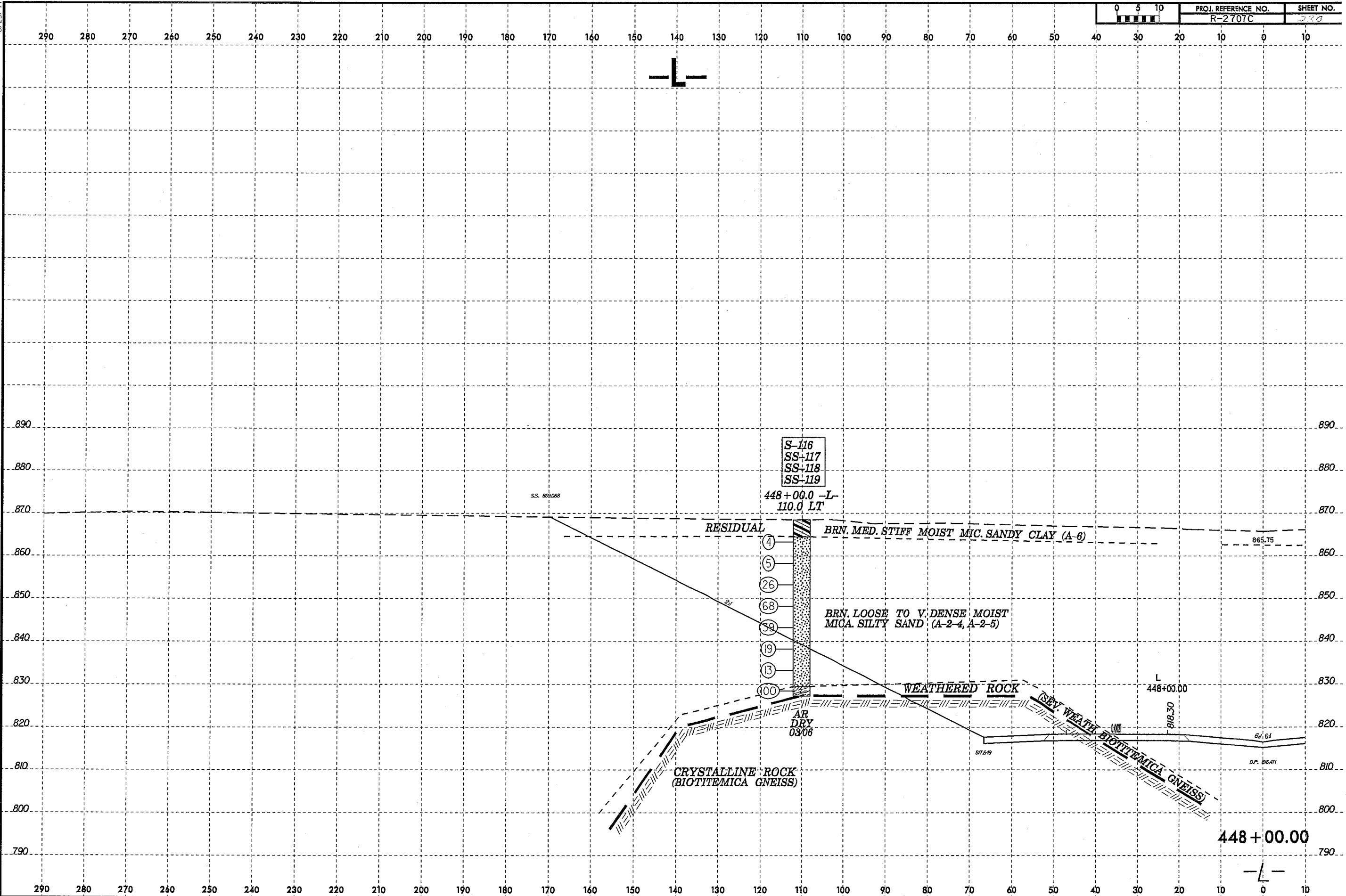
8/23/99  
27-MAY-2008 14:57  
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cburns AT 08:26:15

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	1027



8/23/99  
27-MAY-2008 14:06  
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AT: BHR25157

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 230
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S-116  
SS-117  
SS-118  
SS-119

448+00.0 -L-  
110.0 LT

RESIDUAL

BRN. MED. STIFF MOIST MIC. SANDY CLAY (A-6)

BRN. LOOSE TO V. DENSE MOIST  
MICA SILTY SAND (A-2-4, A-2-5)

WEATHERED ROCK

CRYSTALLINE ROCK  
(BIOTTEMICA GNEISS)

WEATHERED BIOTTEMICA GNEISS

AR  
DRY  
0308

S.S. 865.288

865.75

L  
448+00.00

818.30

816.8

816.61

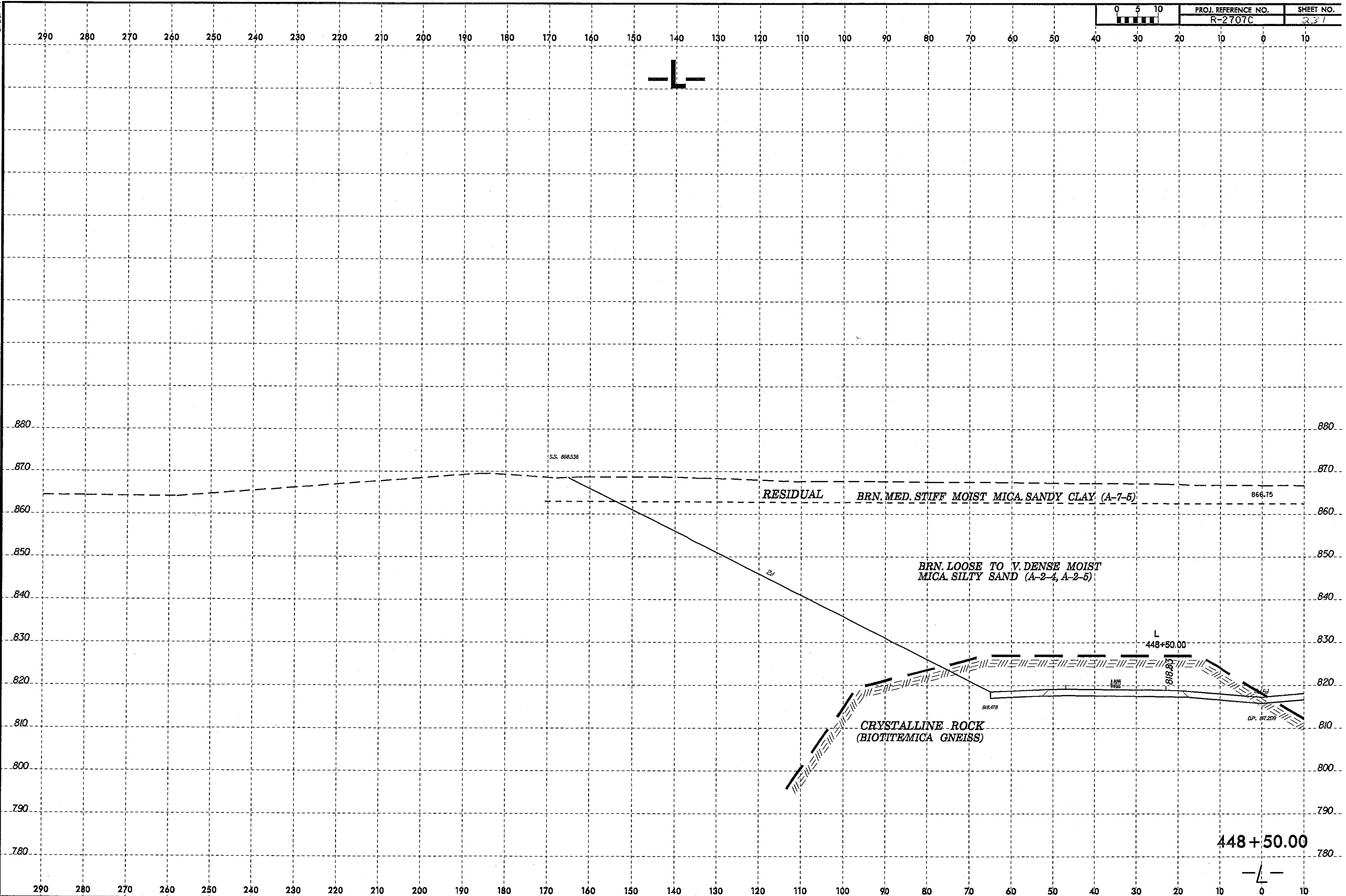
D.P. 816.41

448+00.00



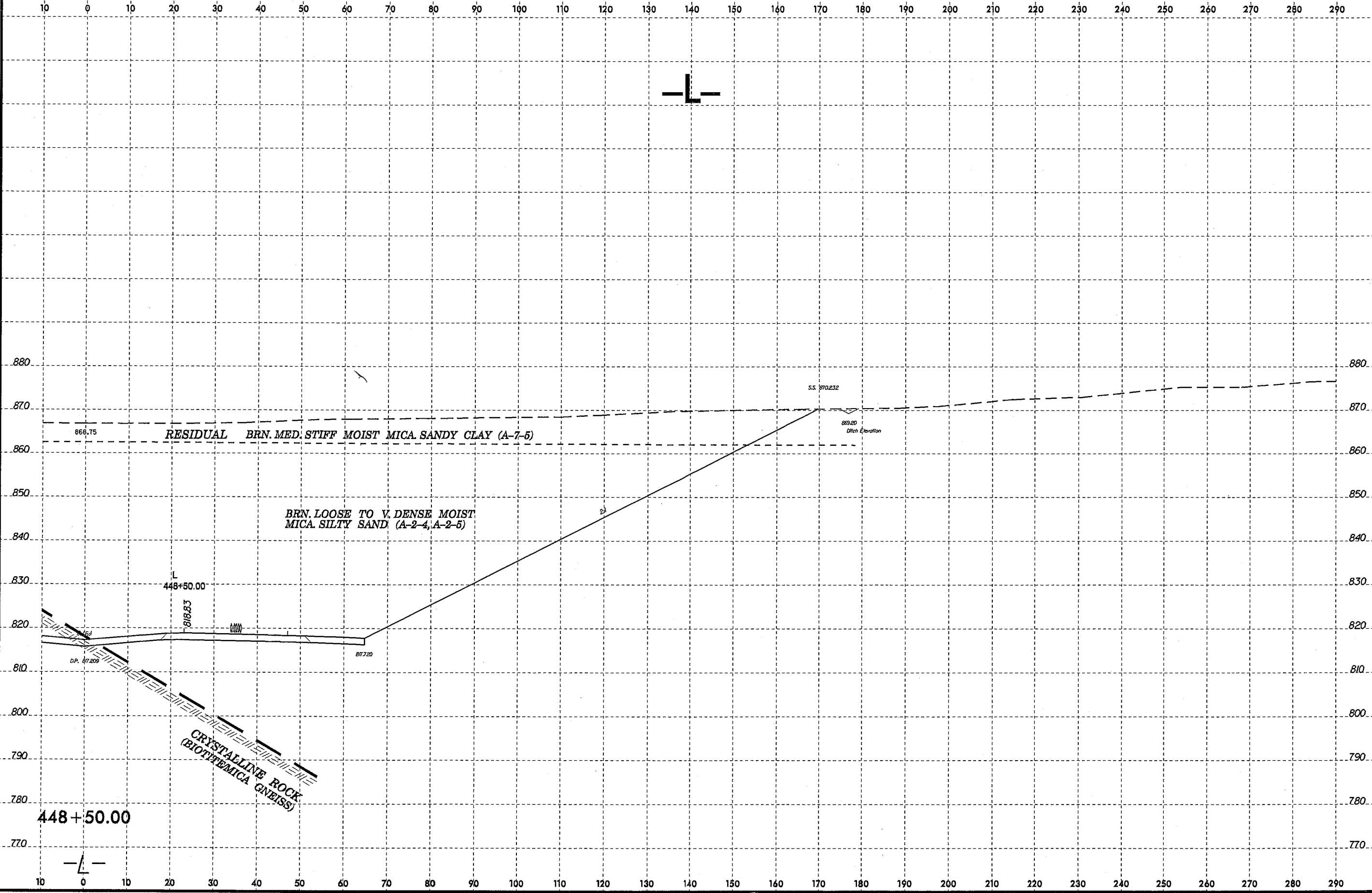
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S:\projects\2707\16\16-geo-rdwy-cleveland\cadd\geotech\axsc\R2707C(rev).GED\_xsl.L\_3.dgn

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 231
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	232



RESIDUAL BRN. MED. STIFF MOIST MICA SANDY CLAY (A-7-5)

BRN. LOOSE TO V. DENSE MOIST MICA SILTY SAND (A-2-4, A-2-5)

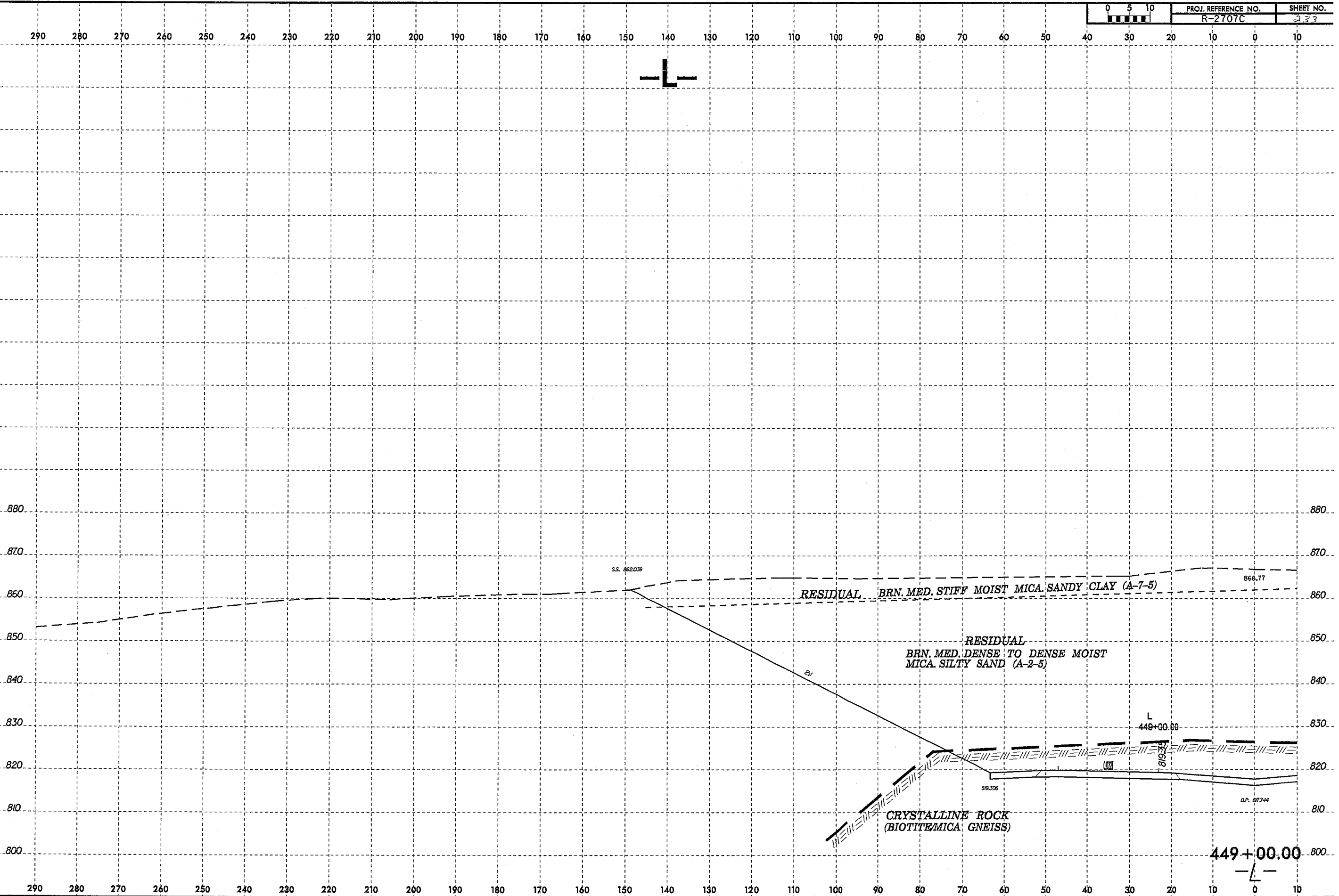
CRYSTALLINE ROCK (BIOTITE MICA GNEISS)

448+50.00



8/23/99  
16-MAY-2008 11:26  
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G:\BURNING

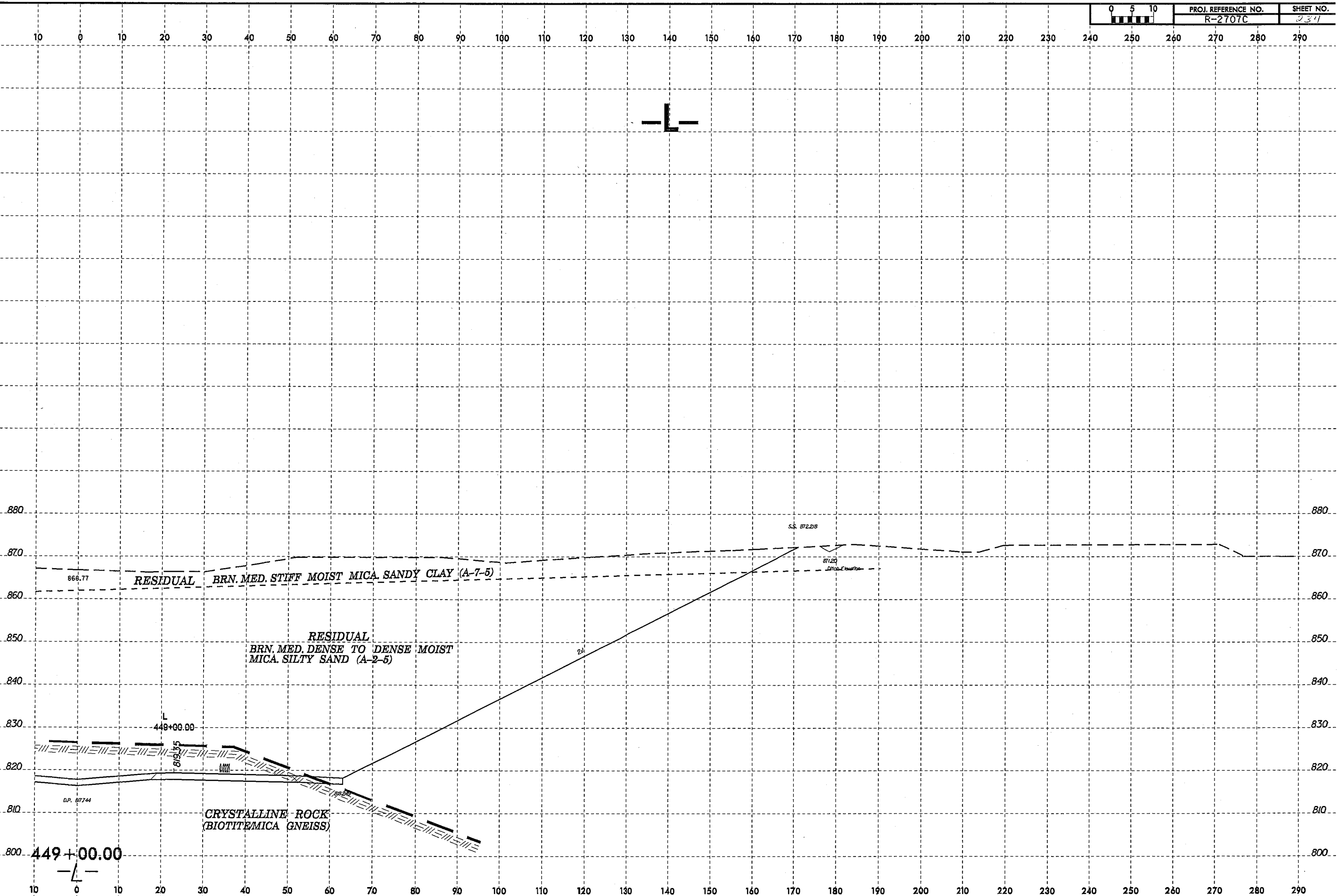
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	233



449+00.00  
-L-

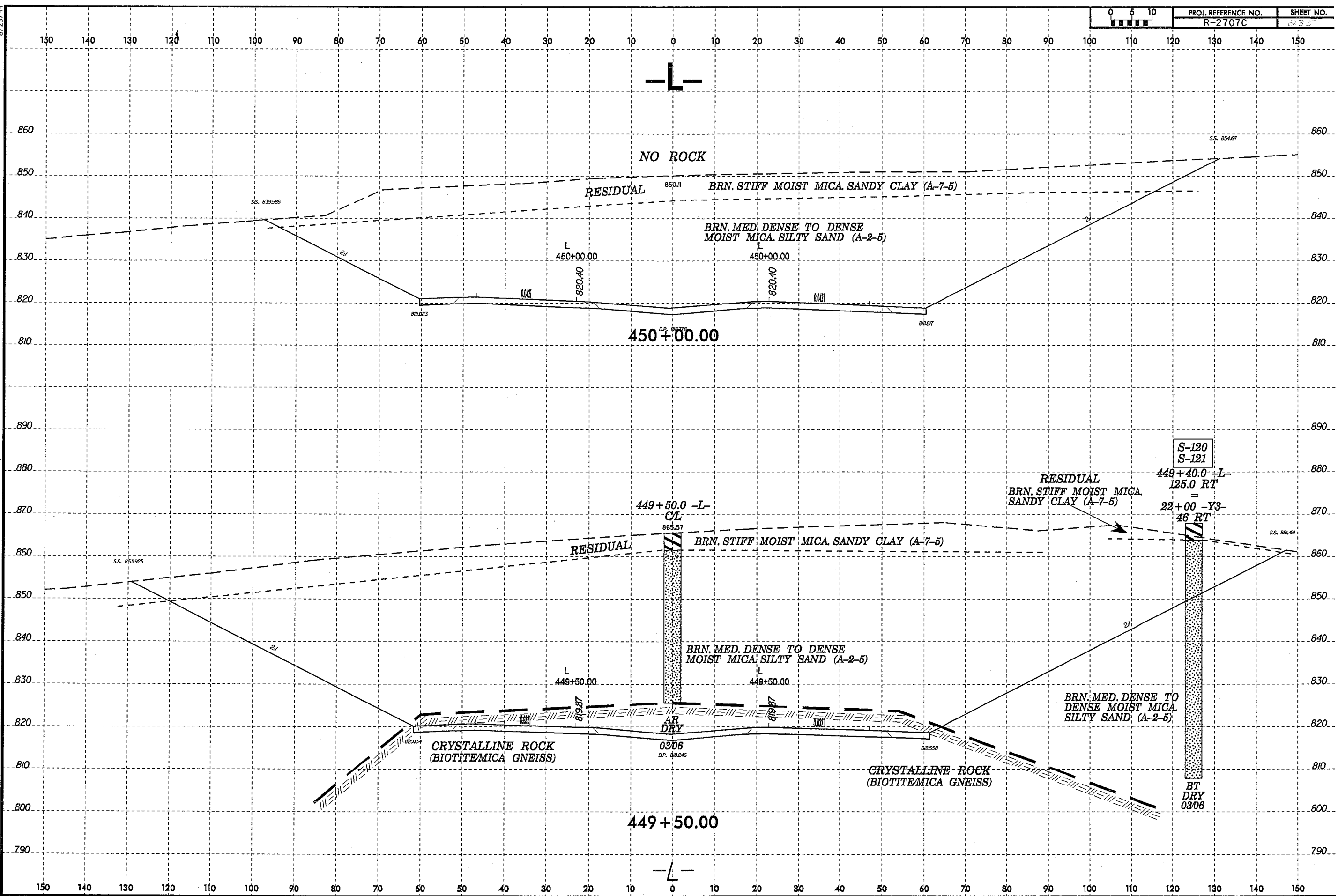
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geoburris AT GEPH26157

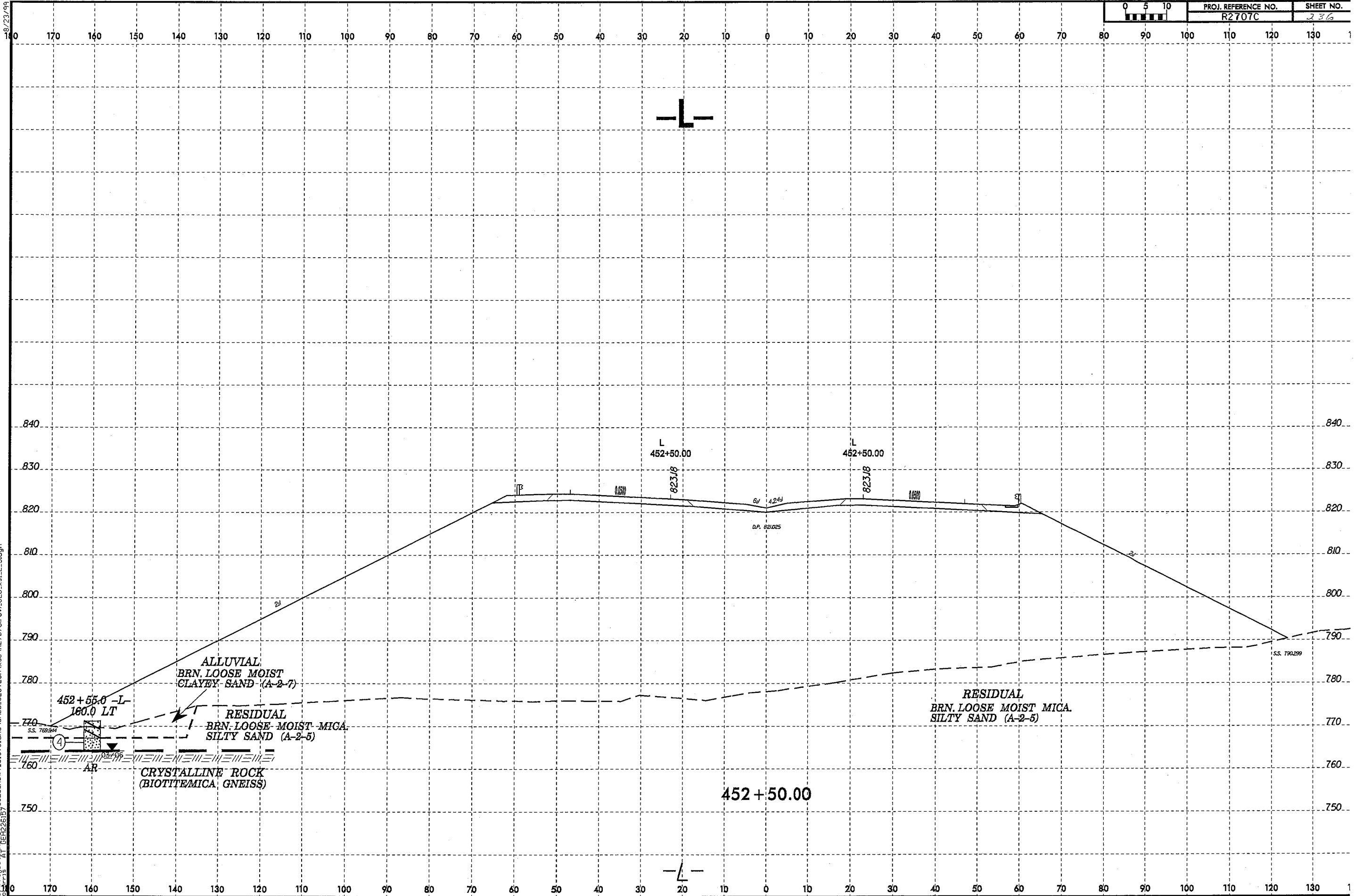
0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 231
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8/23/99  
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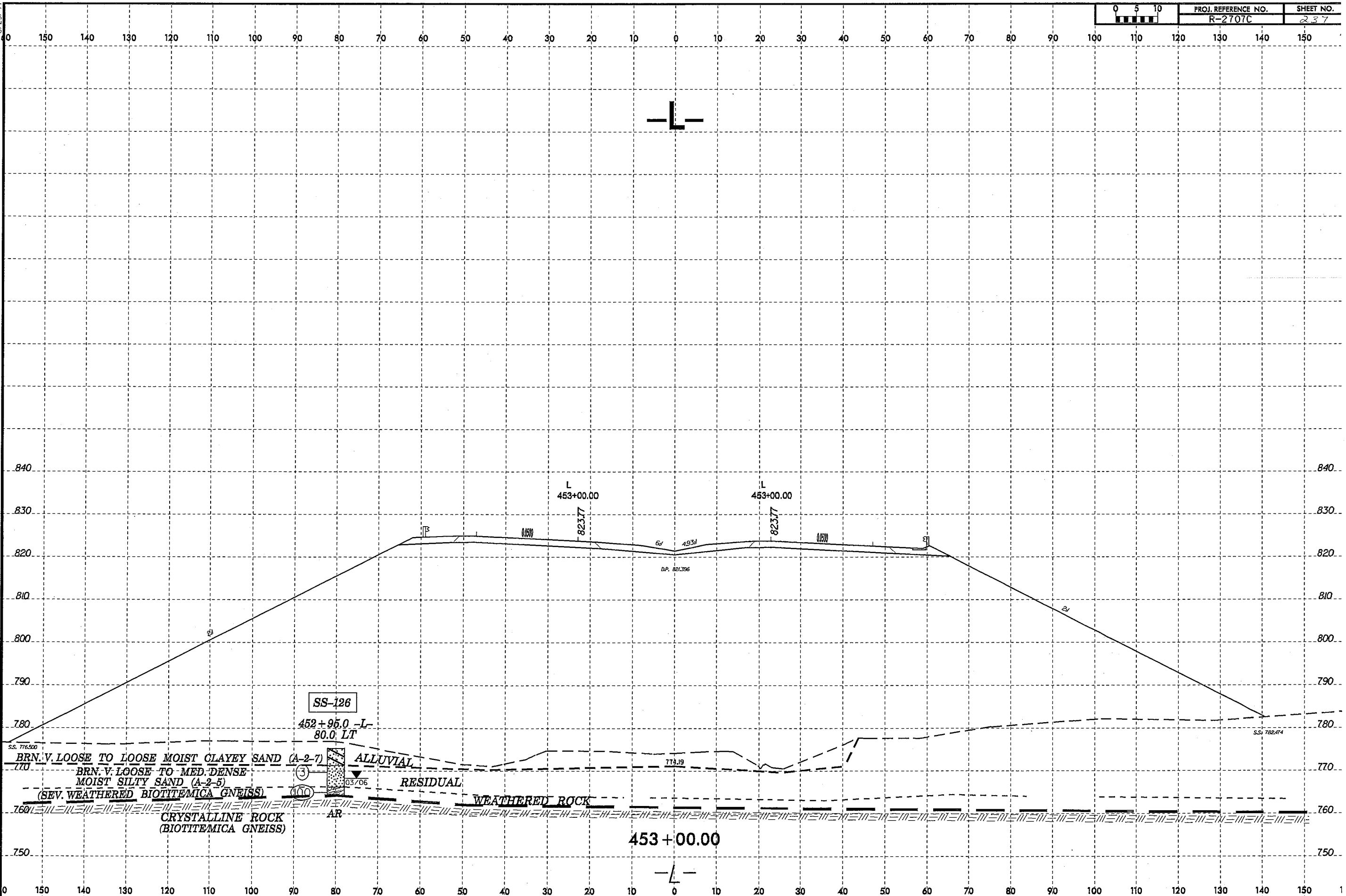
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	R-2707C	23





18/23/99  
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 User: r13 AT GED26167

16-MAY-2008 11:32  
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AT 06/26/07



SS-126  
452+95.0 -L-  
80.0 LT

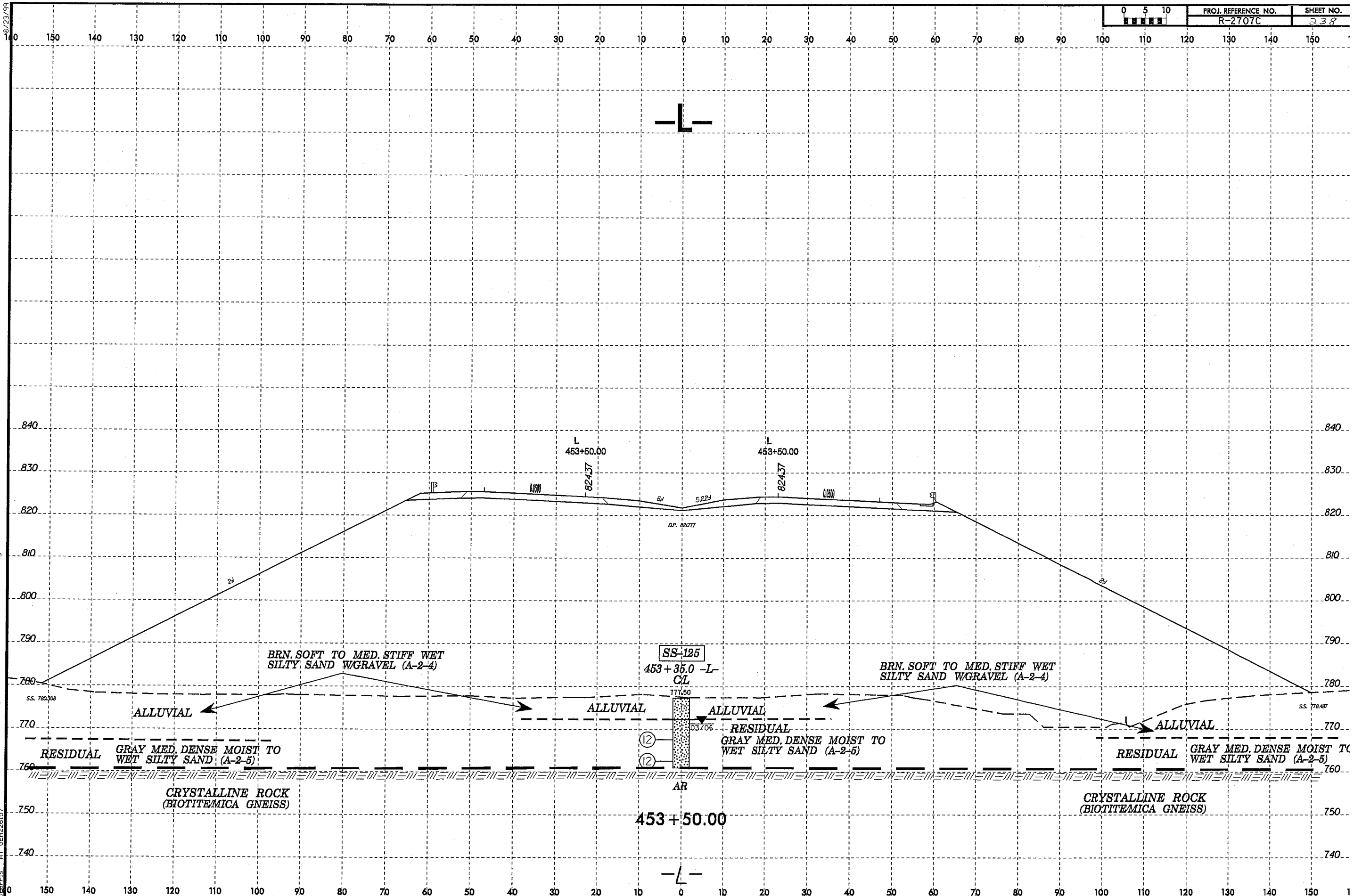
BRN. V. LOOSE TO LOOSE MOIST CLAYEY SAND (A-2-7)  
BRN. V. LOOSE TO MED. DENSE MOIST SILTY SAND (A-2-5)  
(SEV. WEATHERED BIOTTEMICA GNEISS)

CRYSTALLINE ROCK (BIOTTEMICA GNEISS)

ALLUVIAL  
RESIDUAL  
WEATHERED ROCK

453+00.00

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150



BRN. SOFT TO MED. STIFF WET SILTY SAND WGRAVEL (A-2-4)

SS-125

453+35.0 -L- CL

BRN. SOFT TO MED. STIFF WET SILTY SAND WGRAVEL (A-2-4)

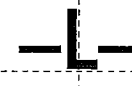
RESIDUAL GRAY MED. DENSE MOIST TO WET SILTY SAND (A-2-5)

RESIDUAL GRAY MED. DENSE MOIST TO WET SILTY SAND (A-2-5)

CRYSTALLINE ROCK (BIOTITEMICA GNEISS)

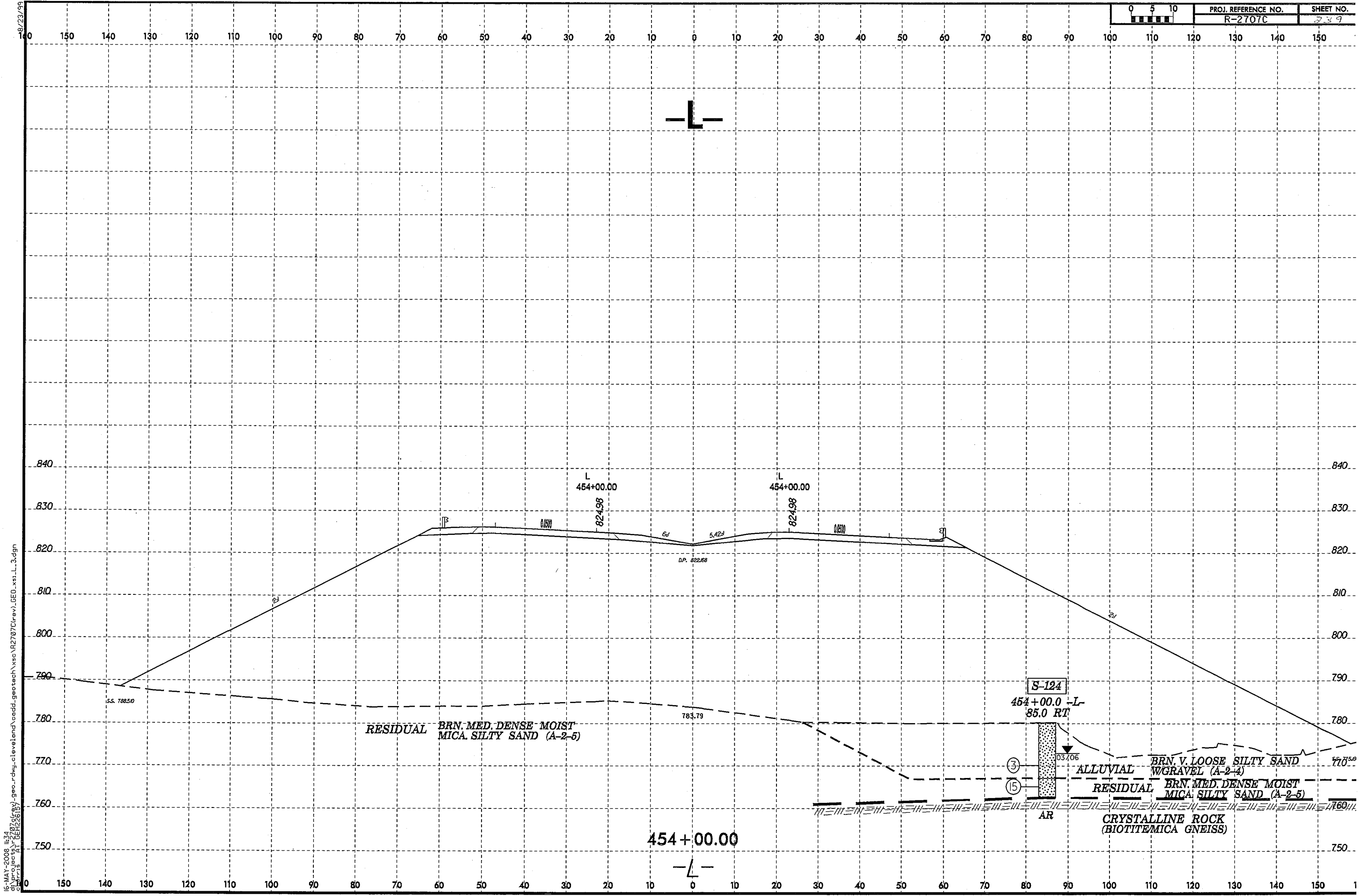
CRYSTALLINE ROCK (BIOTITEMICA GNEISS)

453+50.00



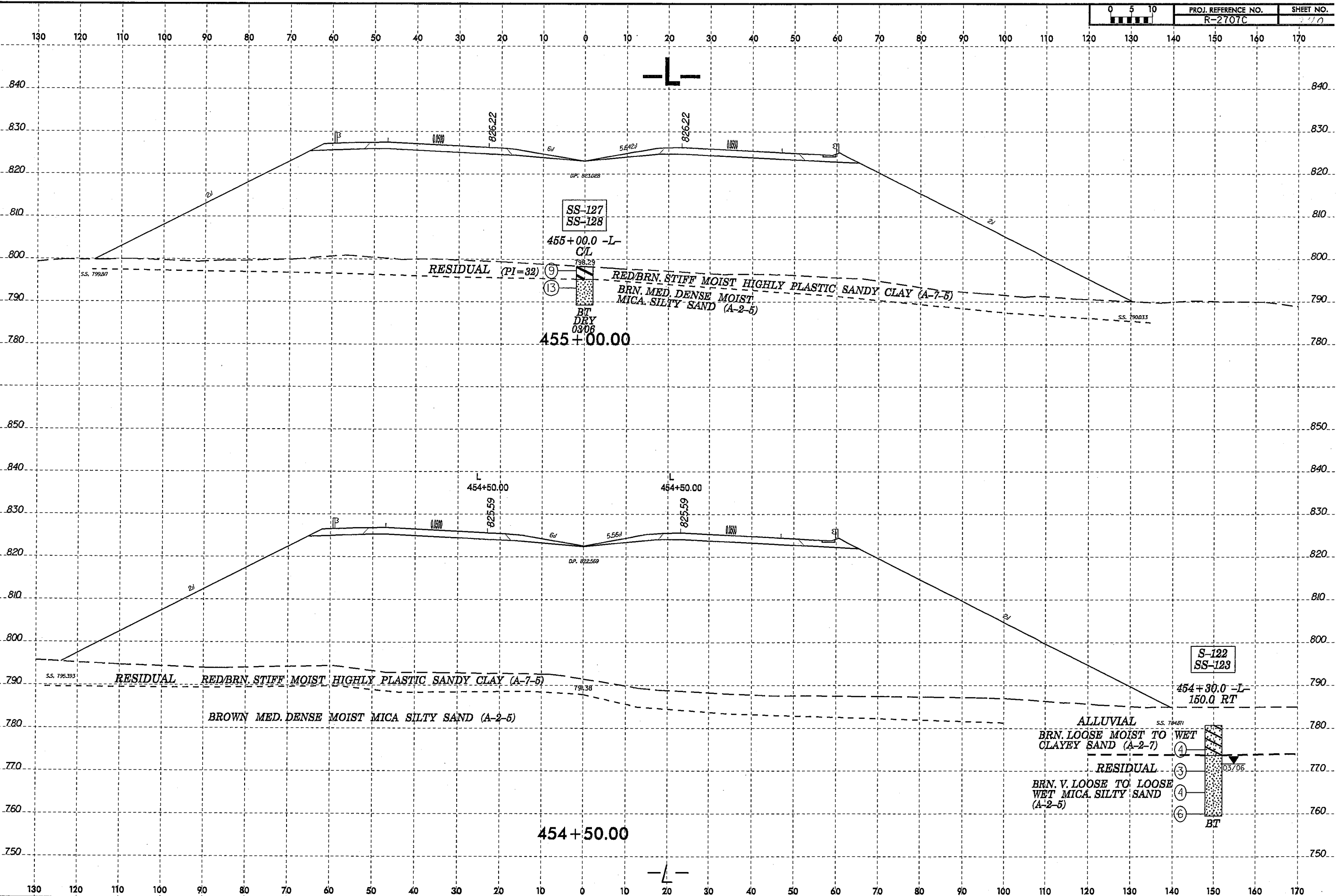
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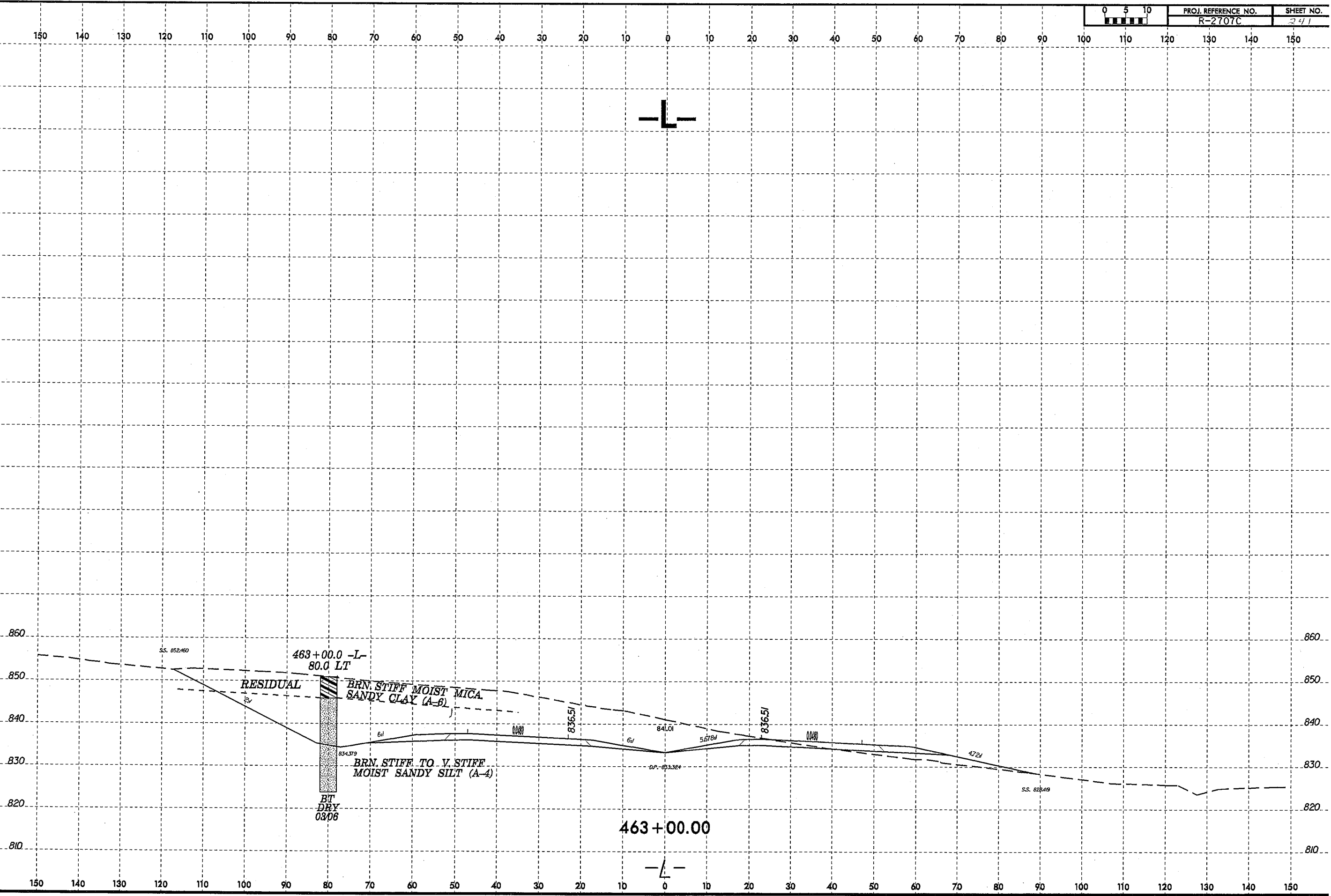
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 Author: R. BERZBERG

16-MAY-2008 11:35  
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BURRIS AT 05/06



8/23/99

0	5	10	PROJ. REFERENCE NO.	SHEET NO.
[Scale bar]			R-2707C	241

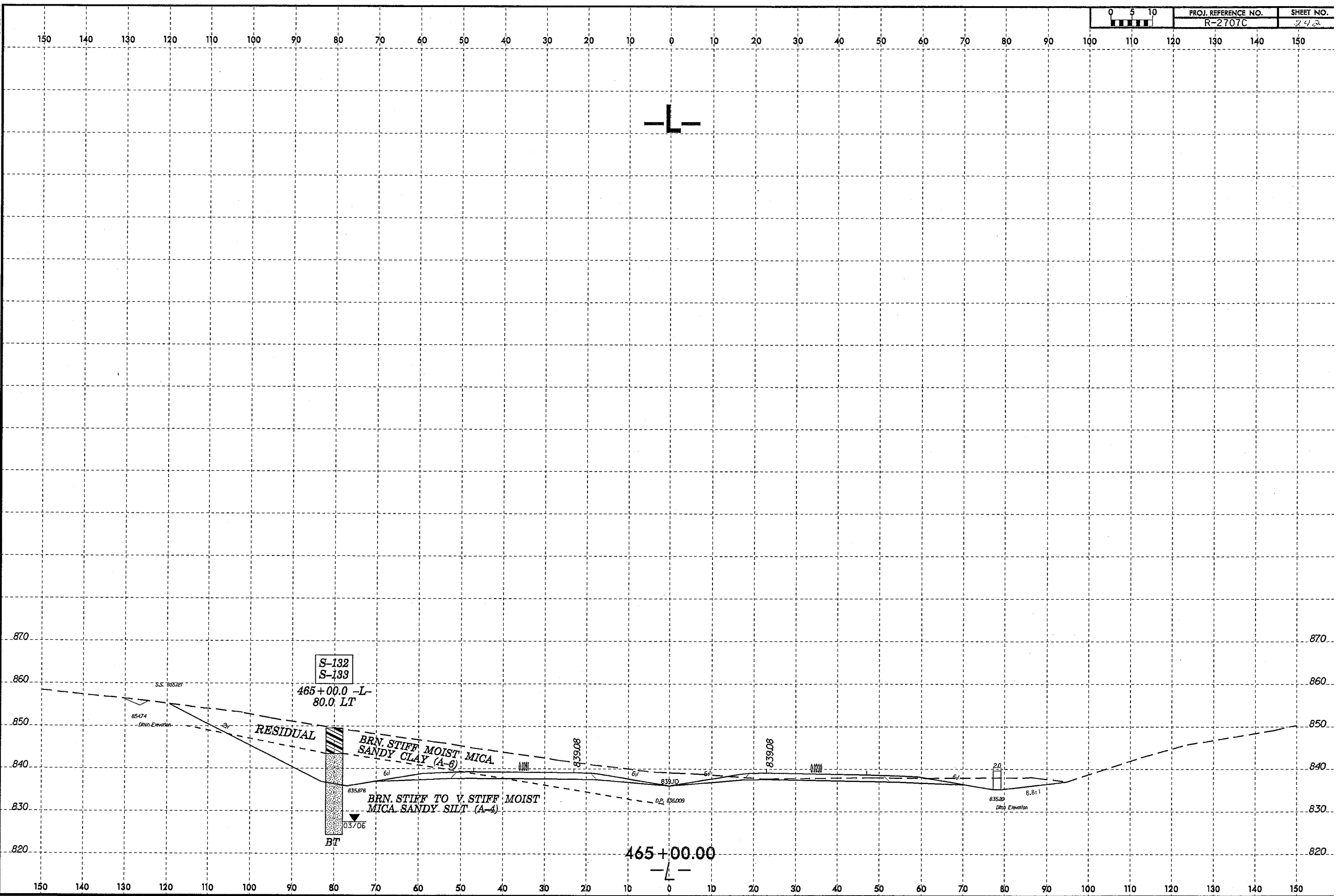


15-MAY-2008 14:41  
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 cburris AT 06/22/08

8/23/99

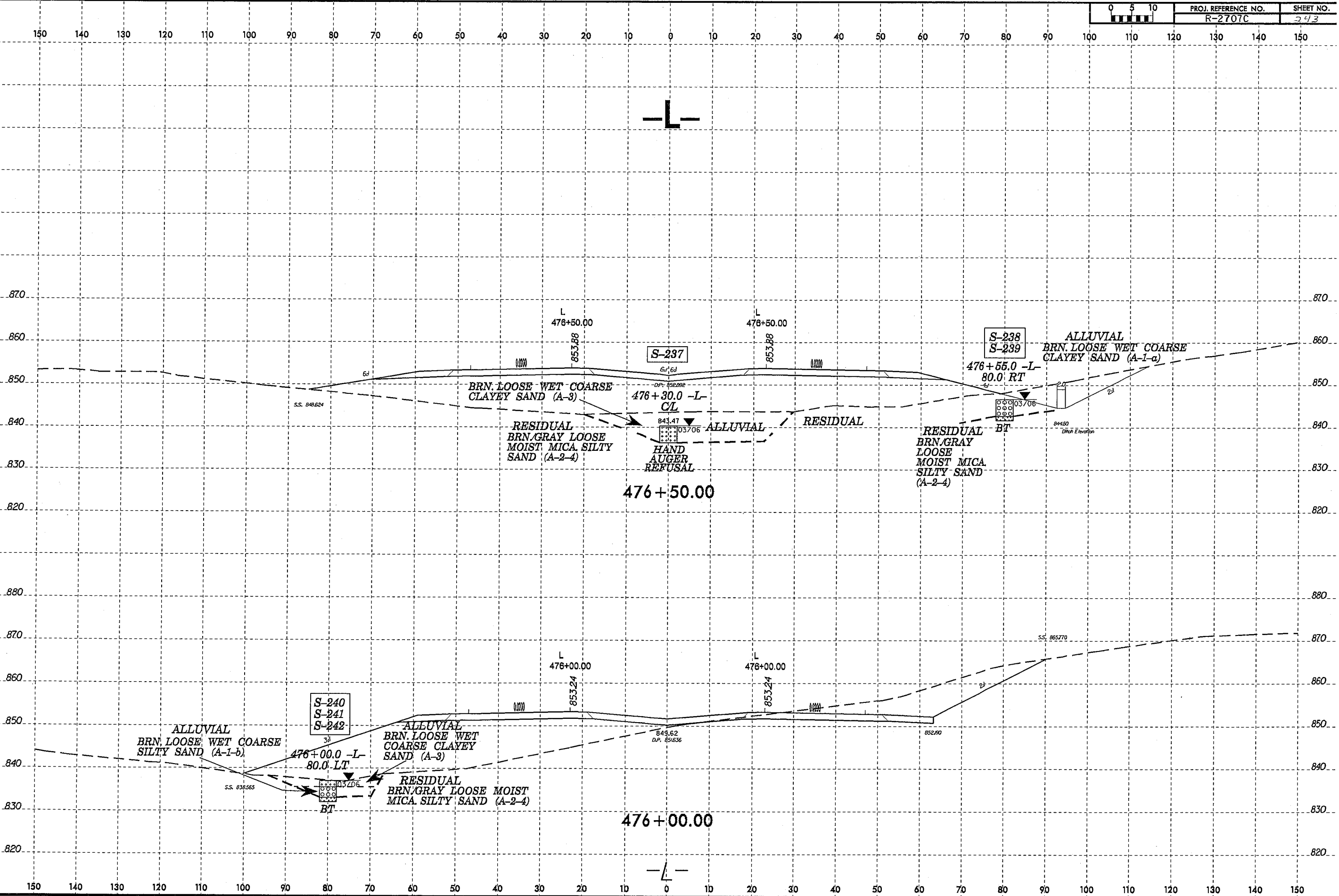
0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	242

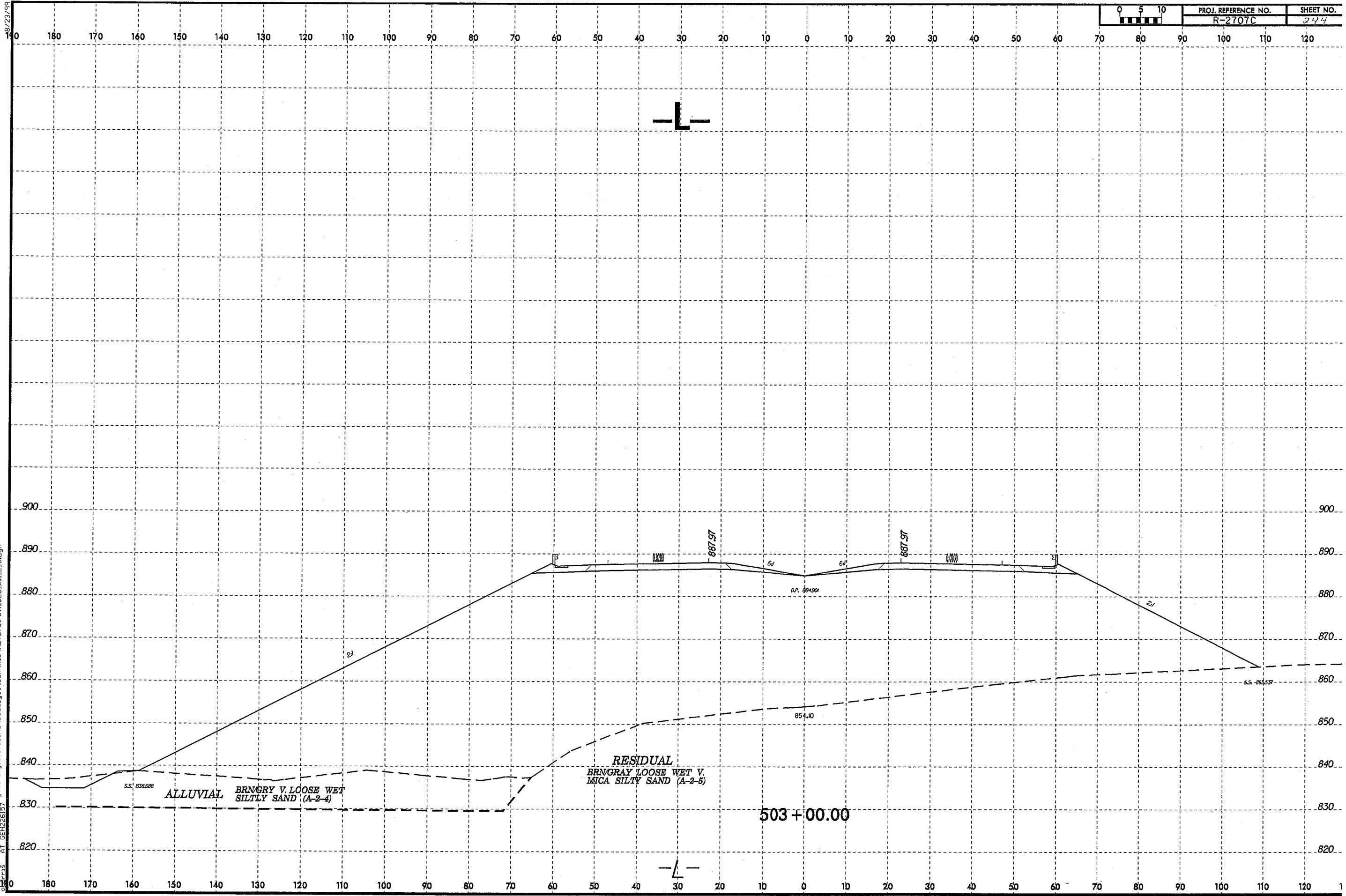
19-MAY-2008 08:25  
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8/23/99  
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0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 243
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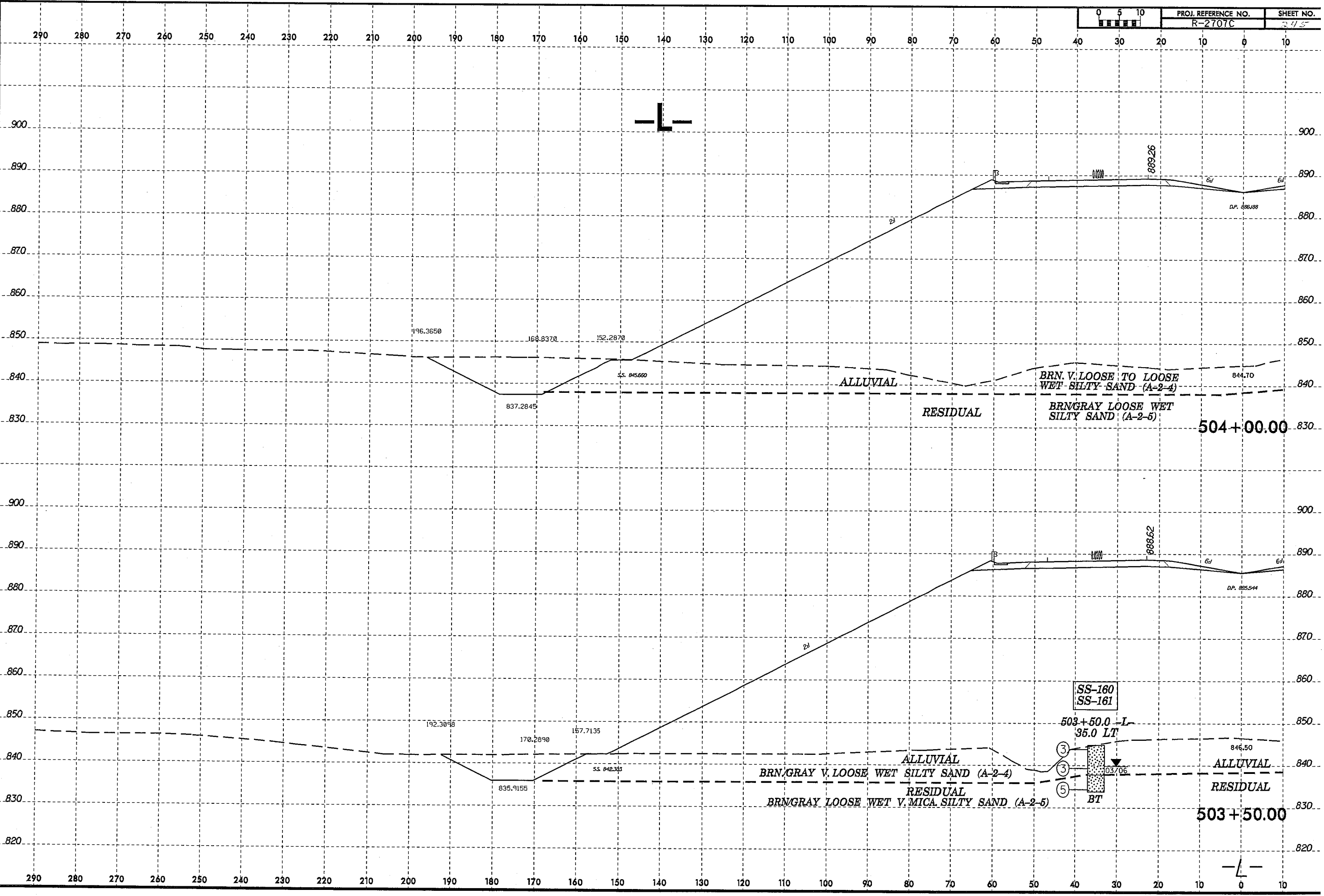




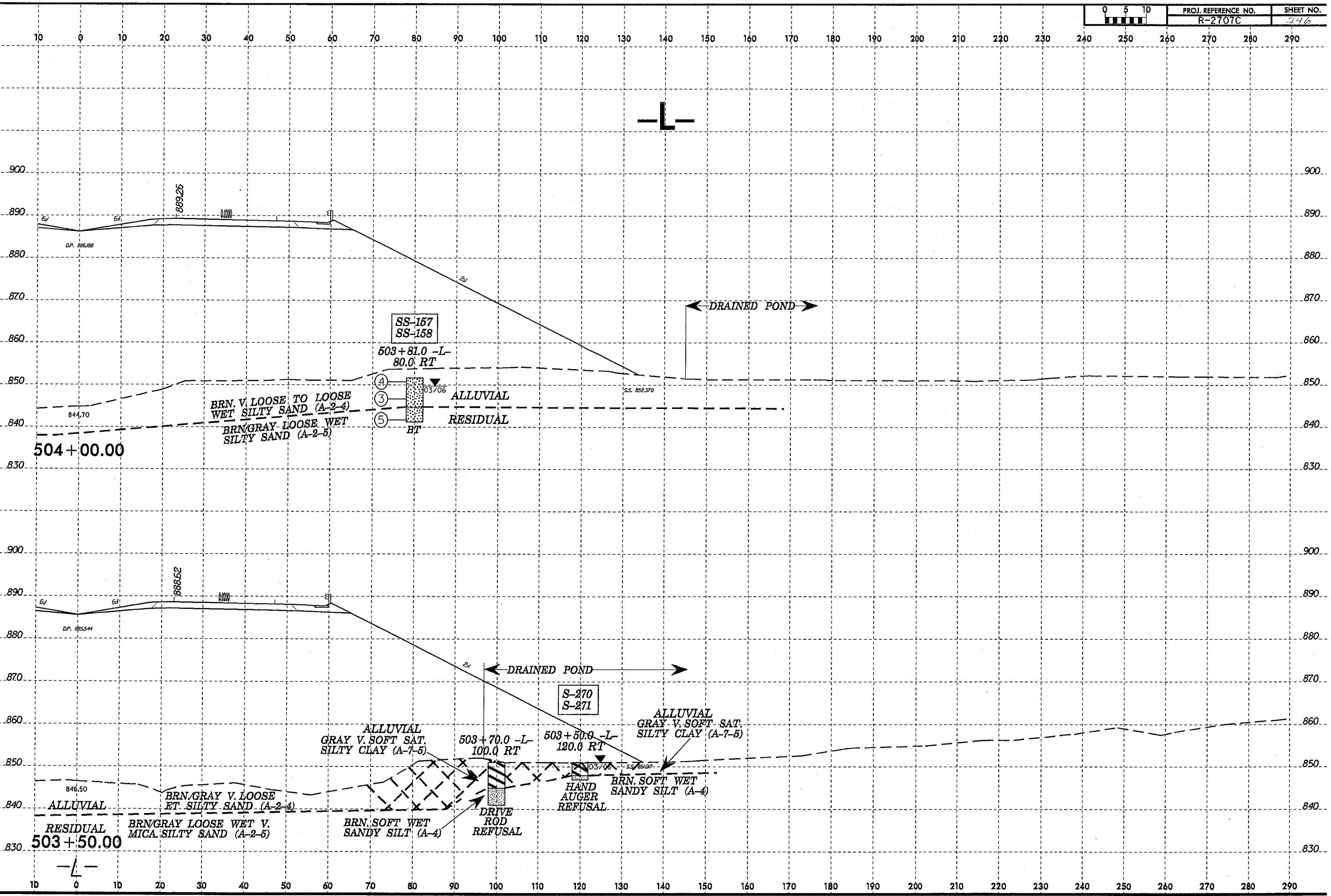
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 SS 838.68  
 SS 861.57

8/23/99  
16-MAY-2008 14:18  
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SSUR13 AT: GEP26157

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	245



8/23/99

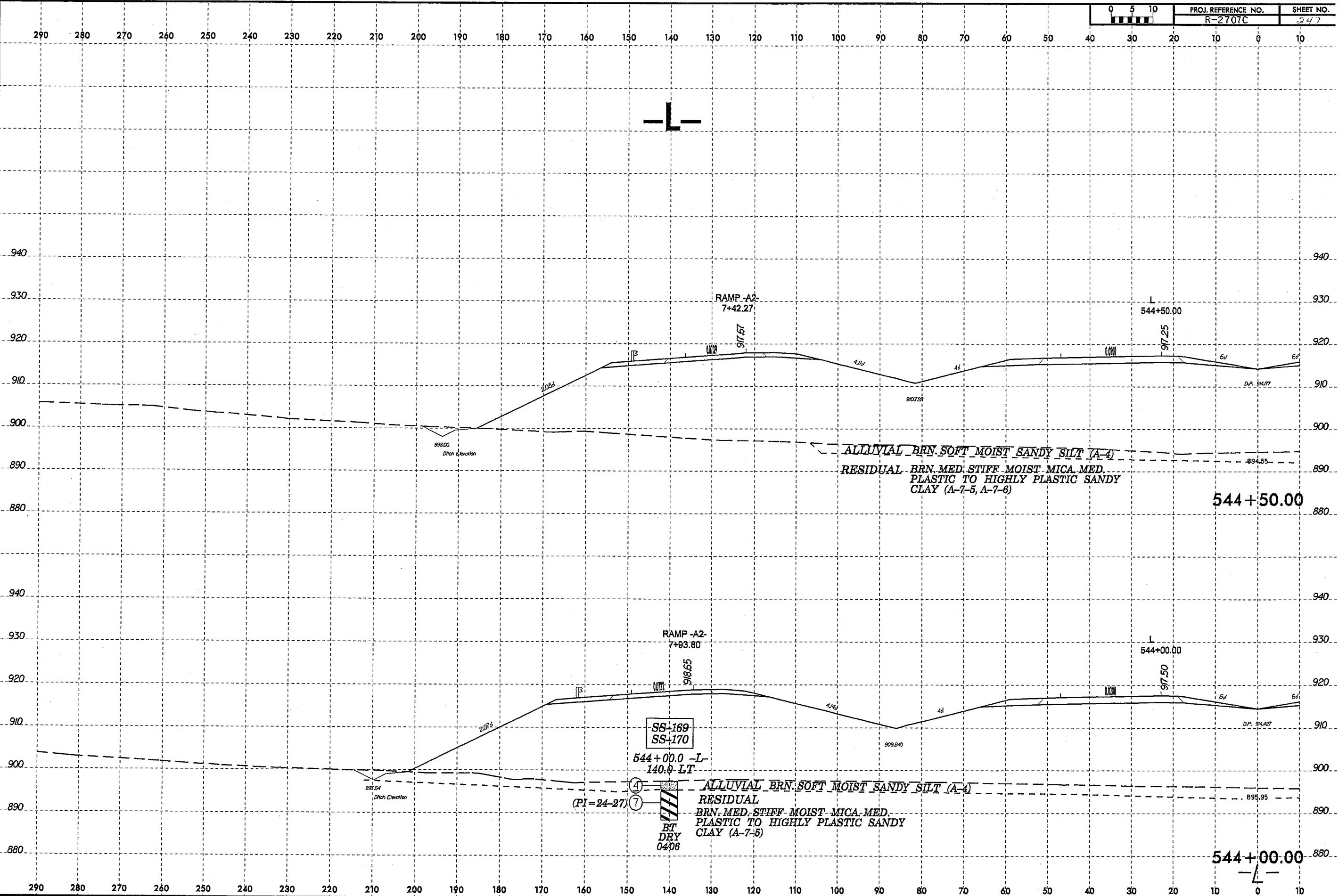


16-MAY-2008 14:19  
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 burris AT 06/26/99

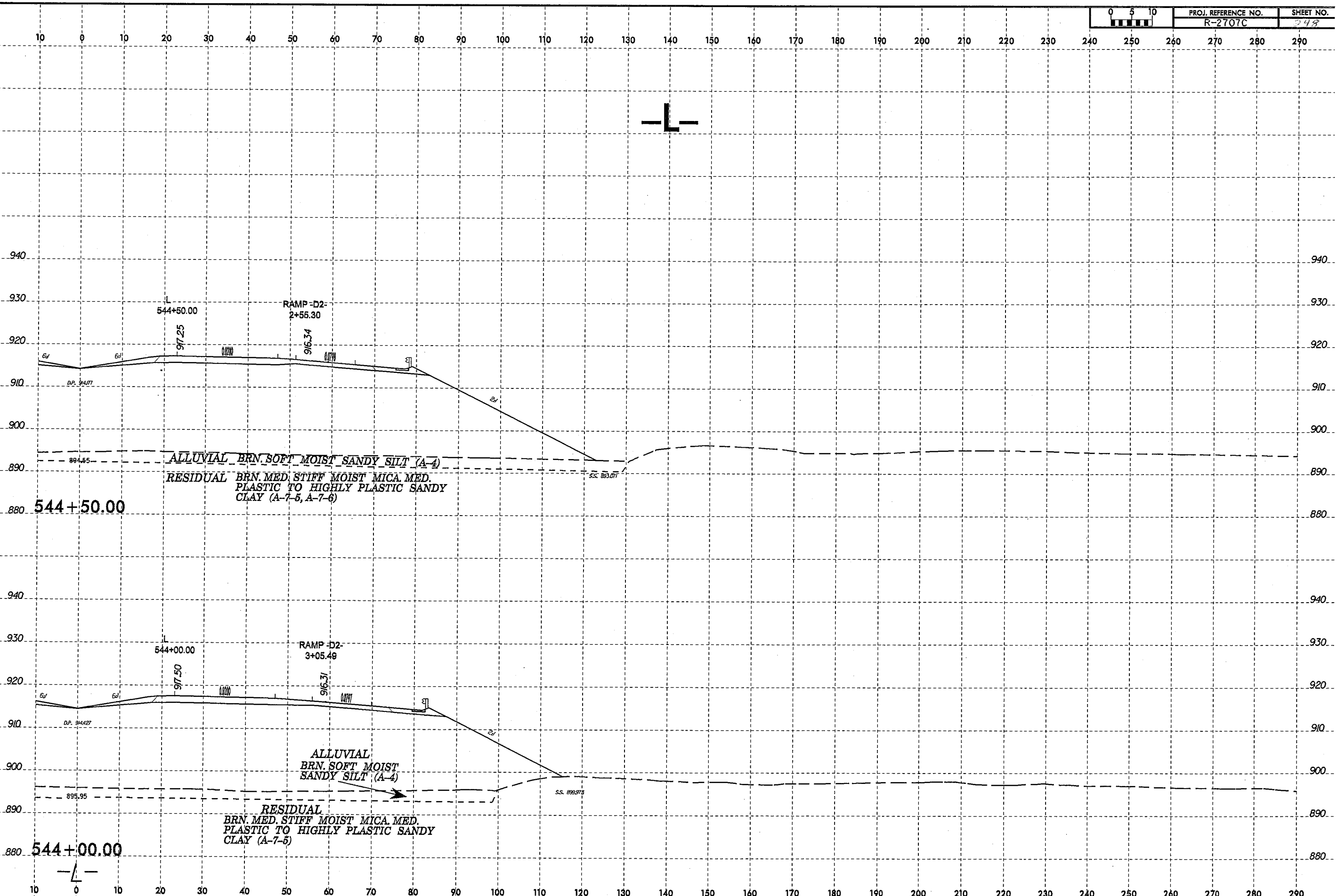


8/23/09  
16-MAY-2008 14:39  
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cburns AT BEH22615

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 247
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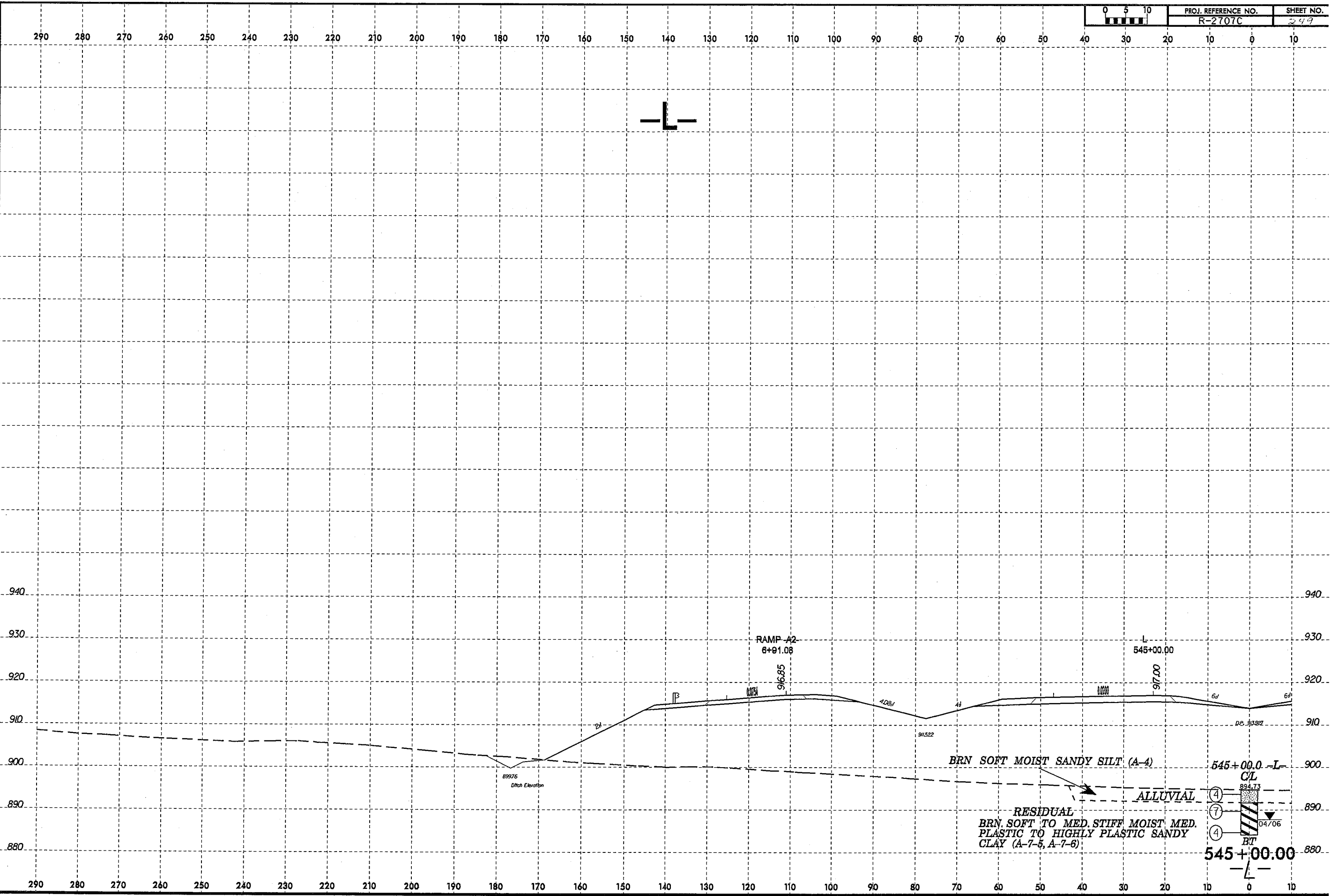


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dwgname



8/23/98

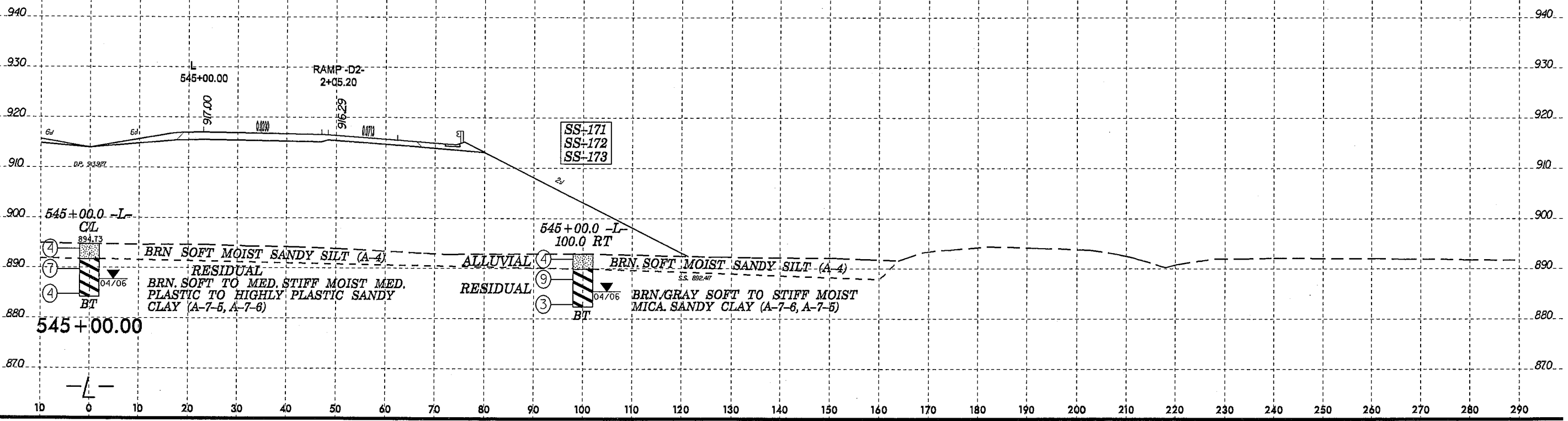
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[Scale Bar]			R-2707C	249



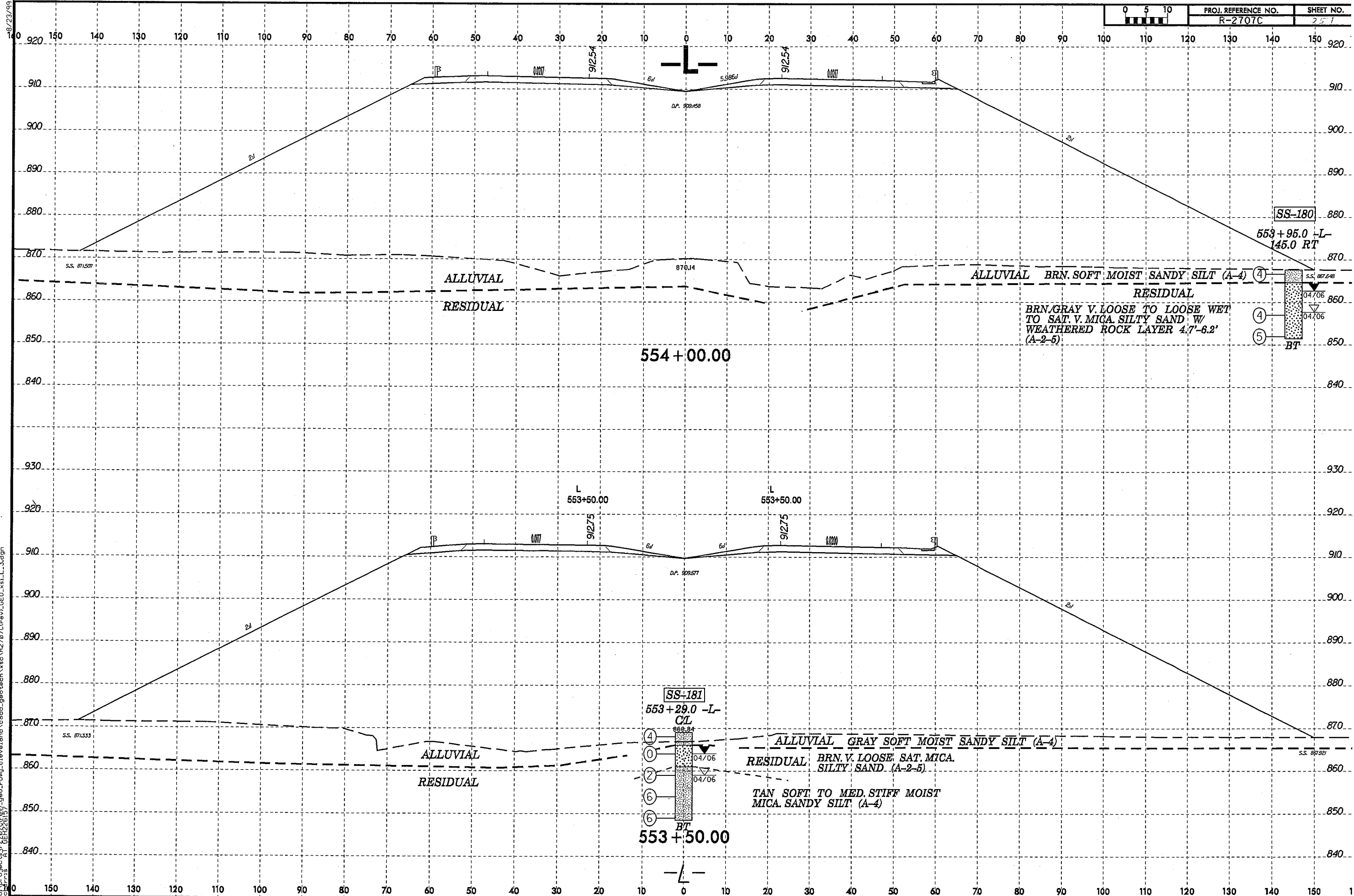
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8/23/99

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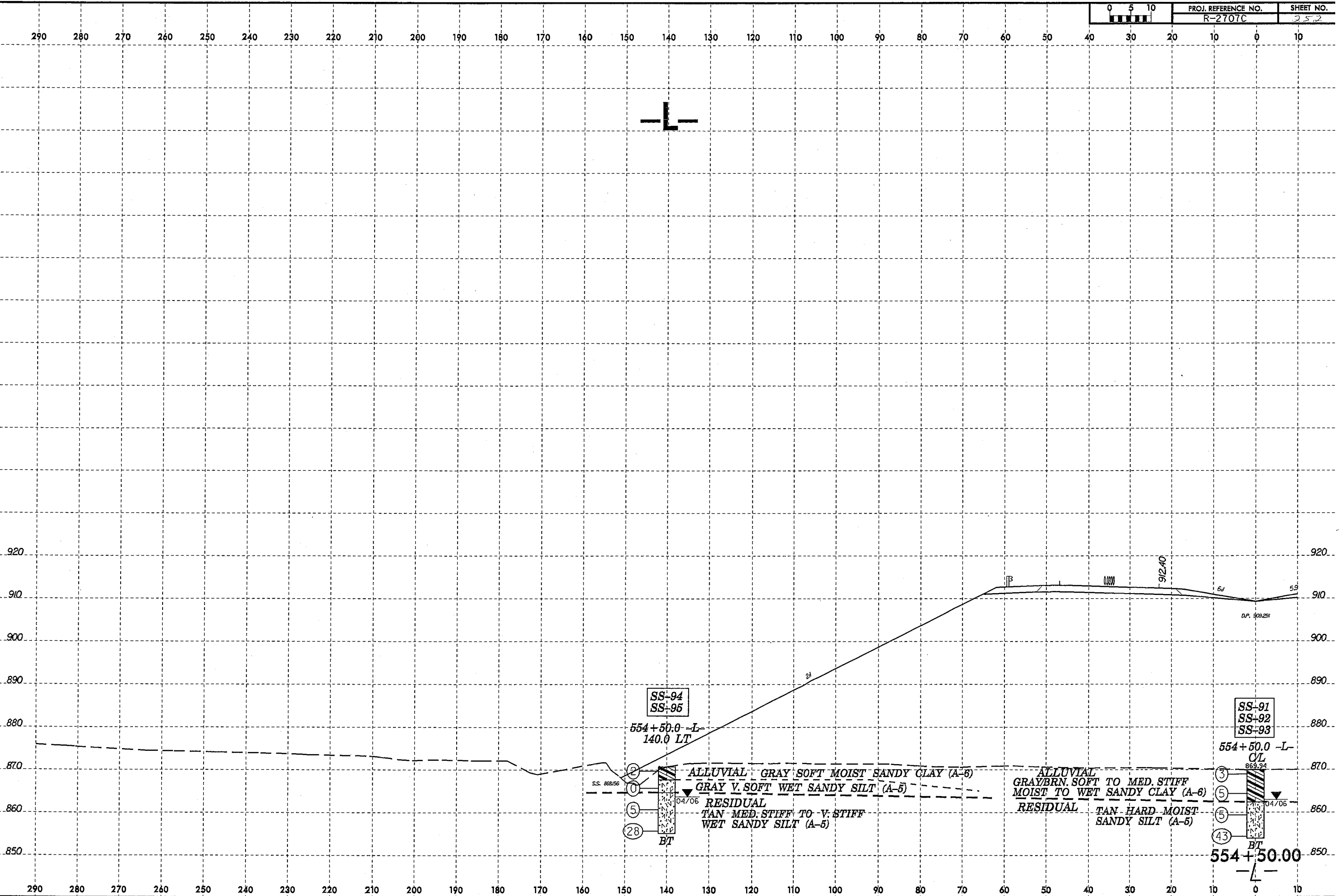
I:\MAY-2008\10\03  
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 burris AT 04/06/99



16-MAY-2008 14:42  
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 User: AT GEH226157

8/23/99  
16-MAY-2008 14:26  
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	2512



SS-94  
SS-95

554+50.0 -L  
140.0 LT

SS 860.56

- ②
- ①
- ⑤
- ②⑧

ALLUVIAL GRAY SOFT MOIST SANDY CLAY (A-6)  
GRAY V. SOFT WET SANDY SILT (A-5)  
RESIDUAL TAN MED. STIFF TO V. STIFF WET SANDY SILT (A-5)

BT

SS-91  
SS-92  
SS-93

554+50.0 -L  
CL 859.34

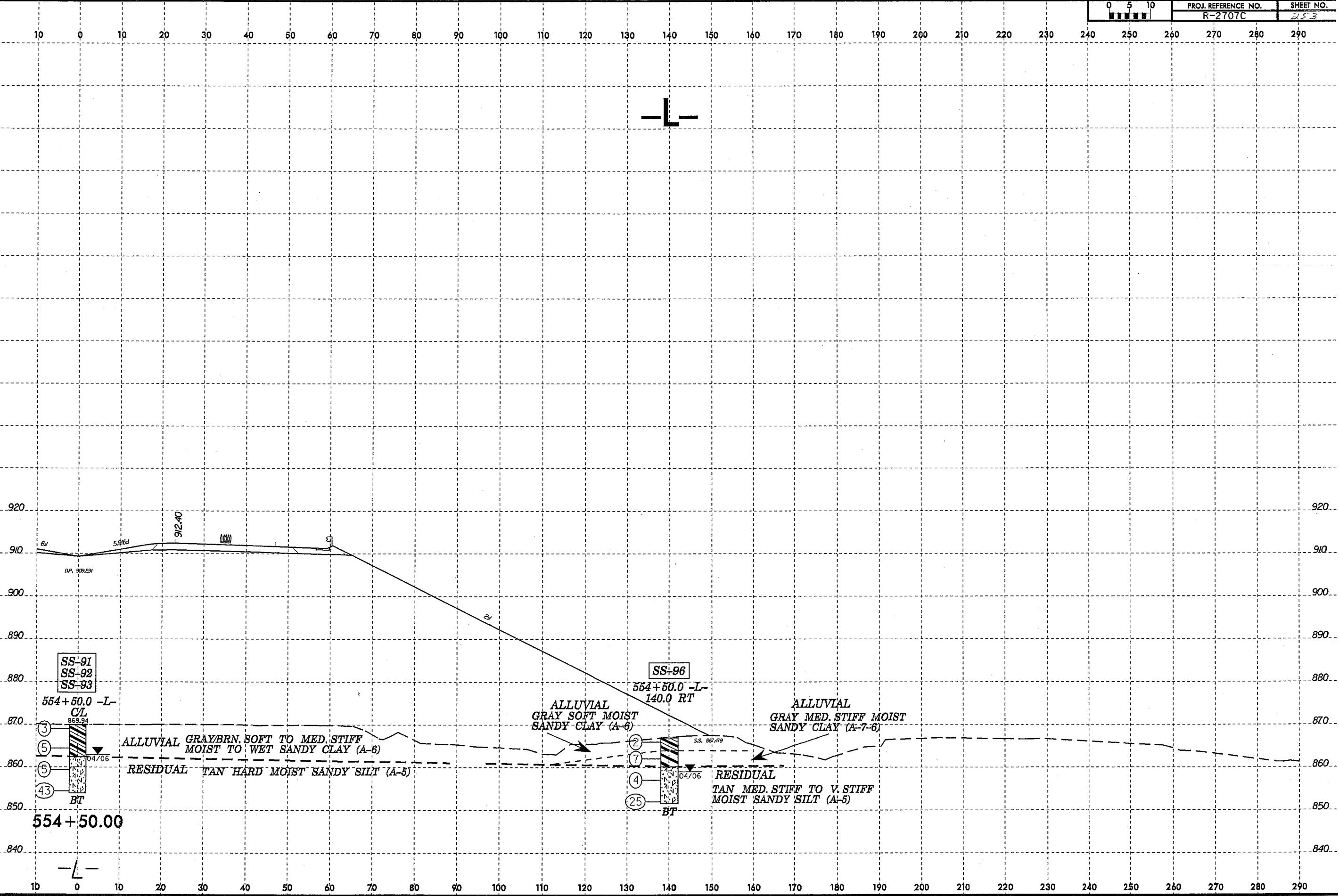
- ③
- ⑤
- ⑤
- ④③

ALLUVIAL GRAYBRN. SOFT TO MED. STIFF MOIST TO WET SANDY CLAY (A-6)  
RESIDUAL TAN HARD MOIST SANDY SILT (A-5)

BT

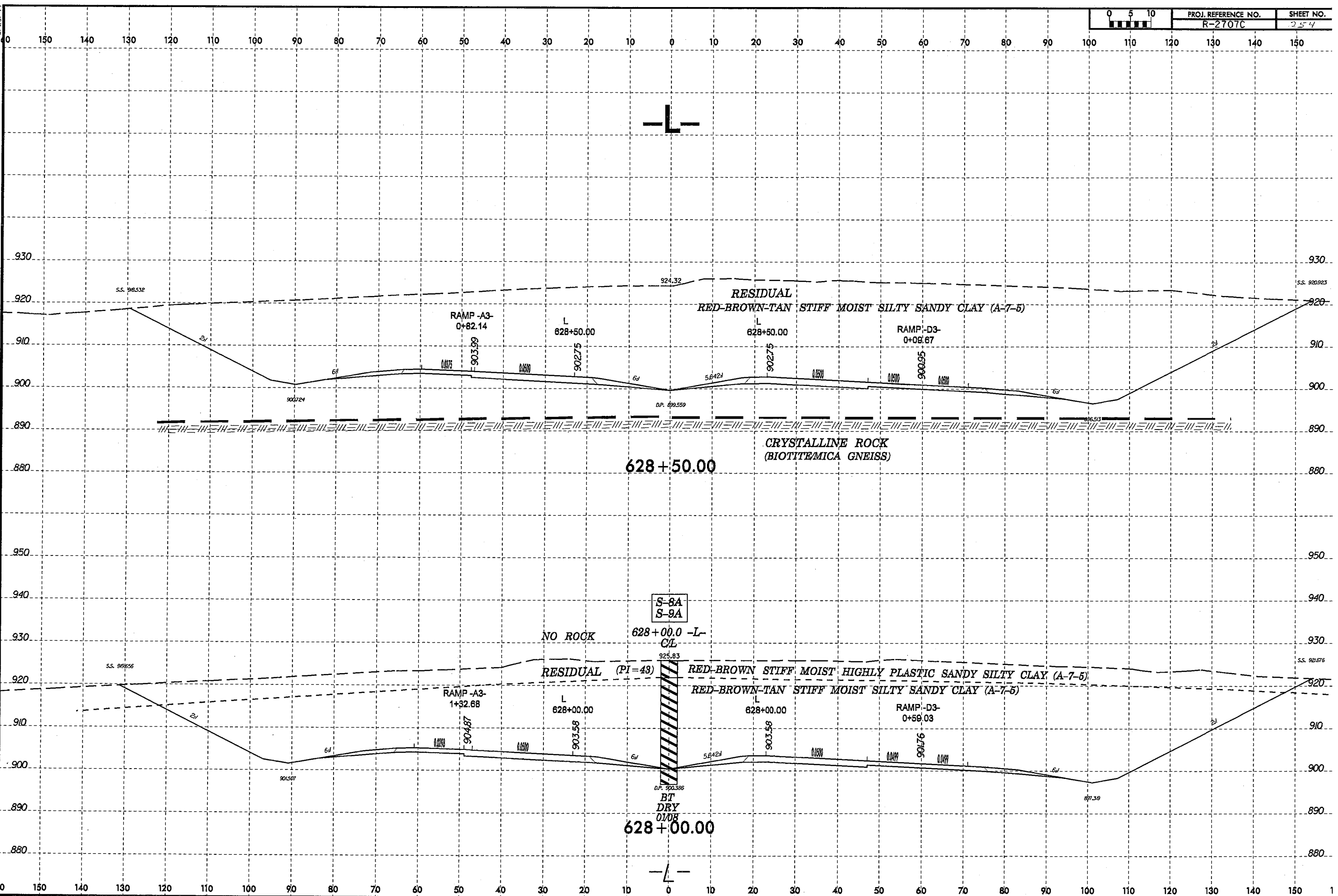
554+50.00

16-MAY-2008 14:27  
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8/23/09

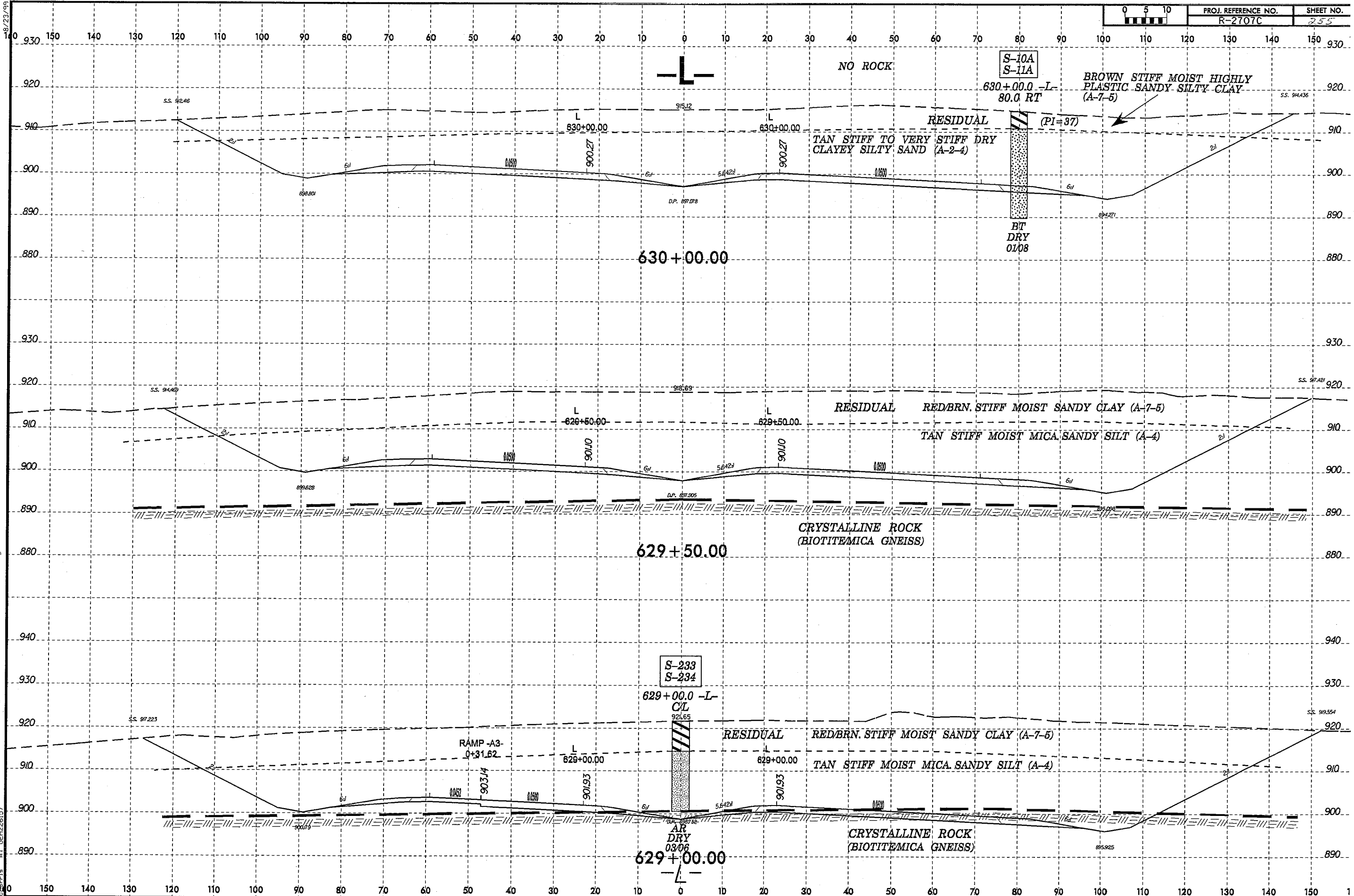


16-MAY-2008 11:45  
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PROJ. REFERENCE NO. R-2707C		
SHEET NO. 254		





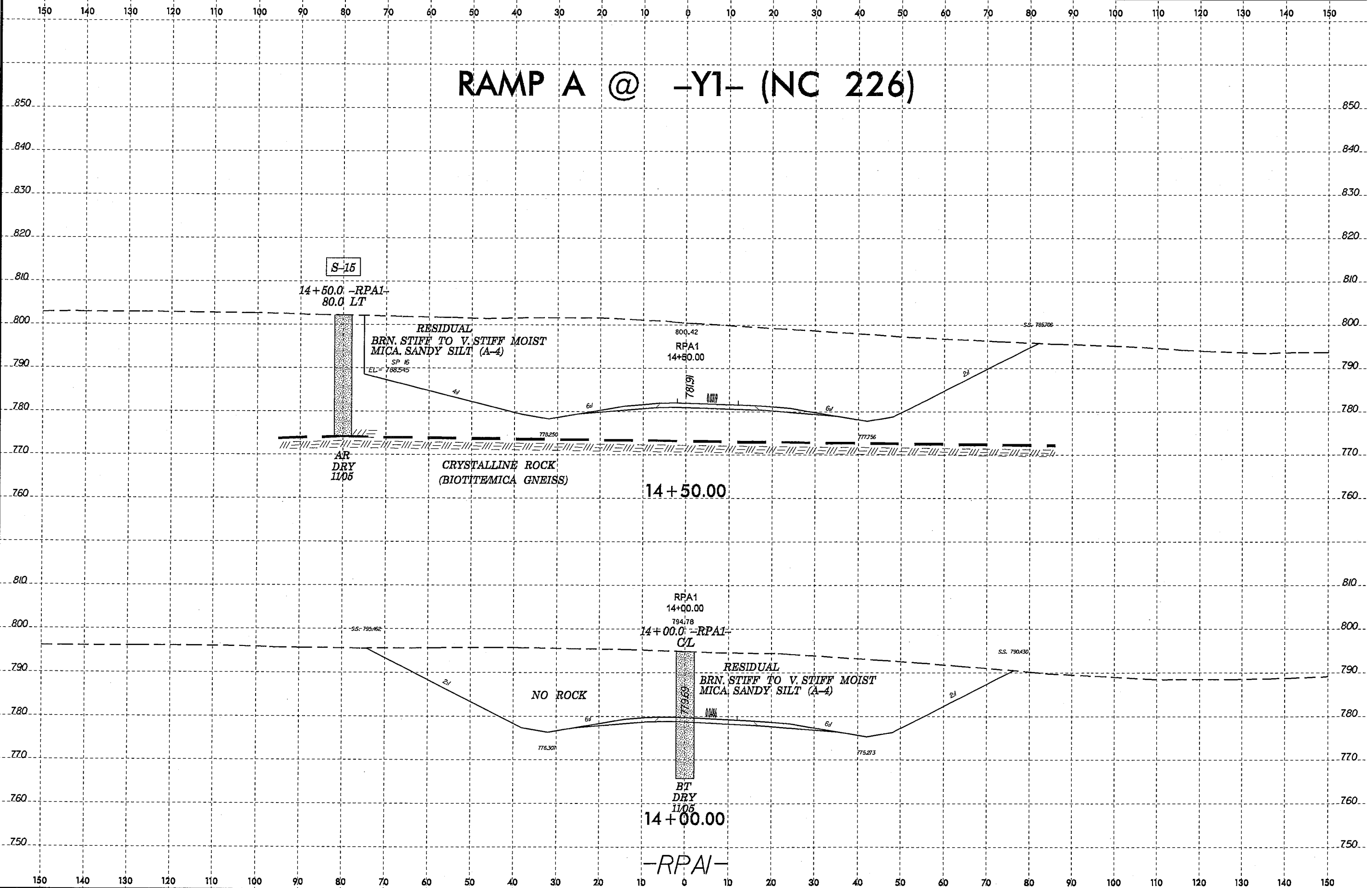


19-MAY-2008 10:10  
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 18/23/99

8/23/99  
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geotechnical\cleveland\cadd\geotech\14+50.00\14+50.00.dgn  
14+50.00

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 256
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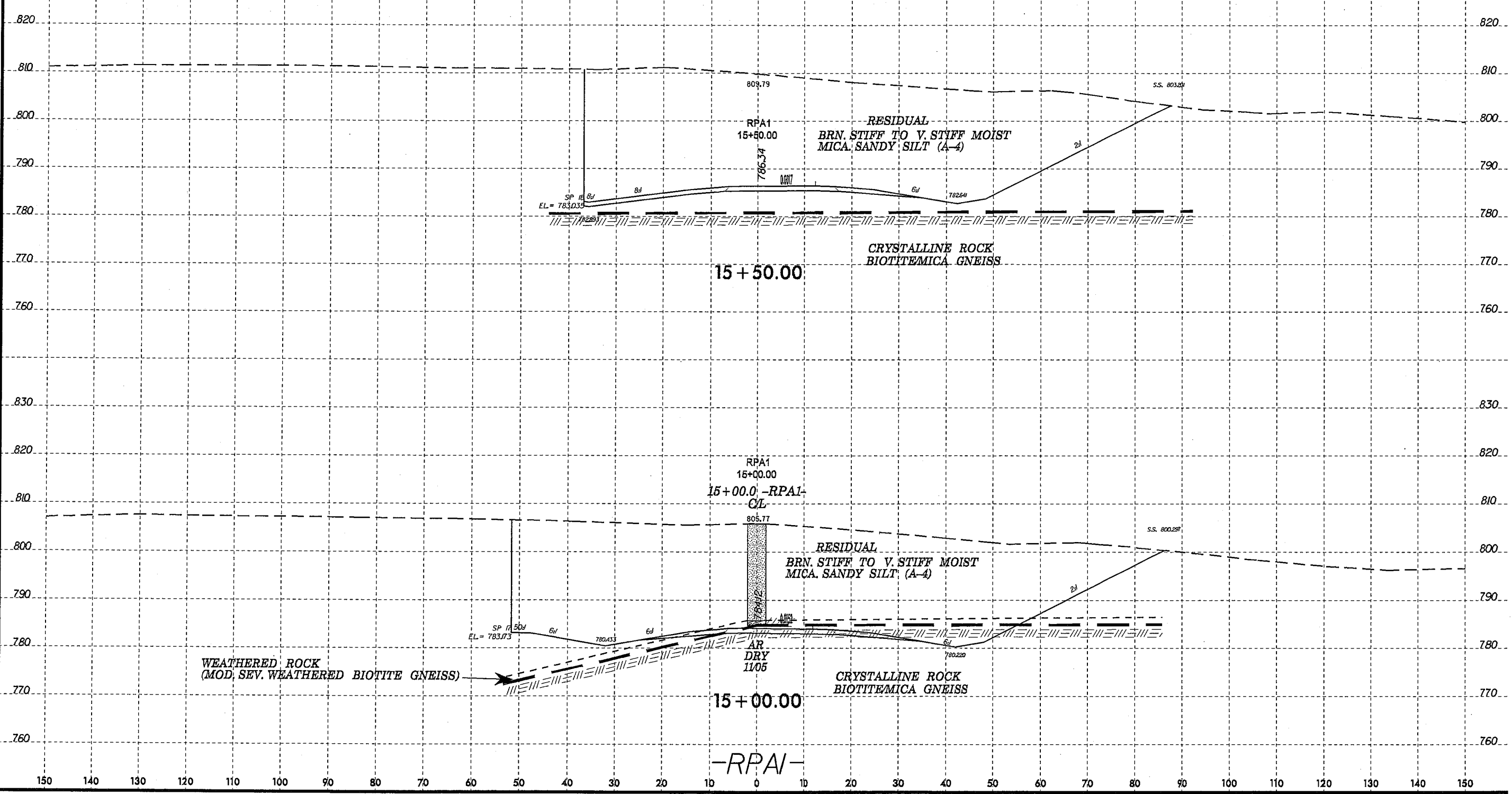
# RAMP A @ -Y1- (NC 226)



8/23/99  
21-APR-2008 13:46  
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0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	257

# RAMP A @ -Y1- (NC 226)



WEATHERED ROCK  
(MOD. SEV. WEATHERED BIOTITE GNEISS)

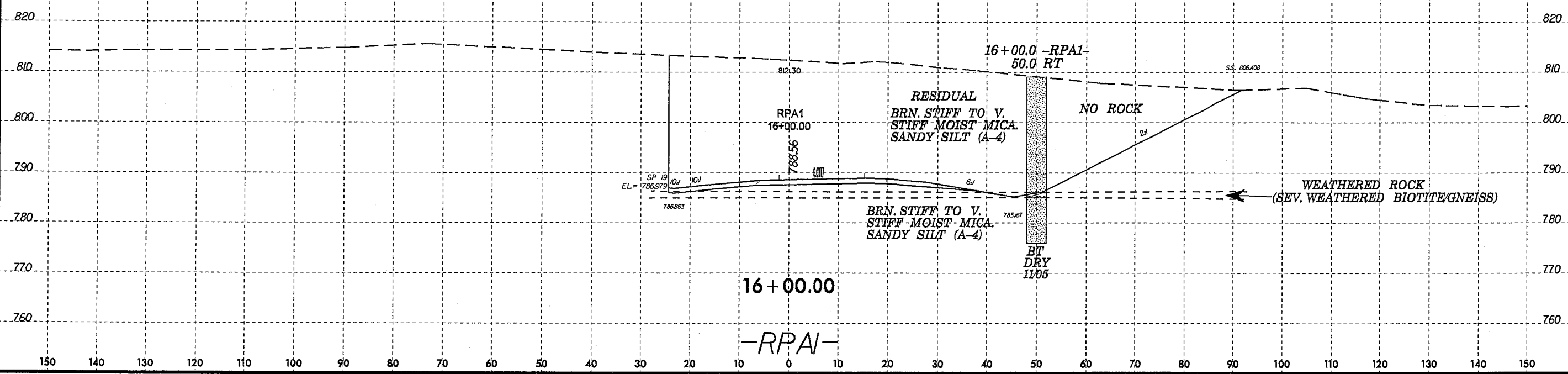
-RPA1-

8/23/99

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	058

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

# RAMP A @ -Y1- (NC 226)

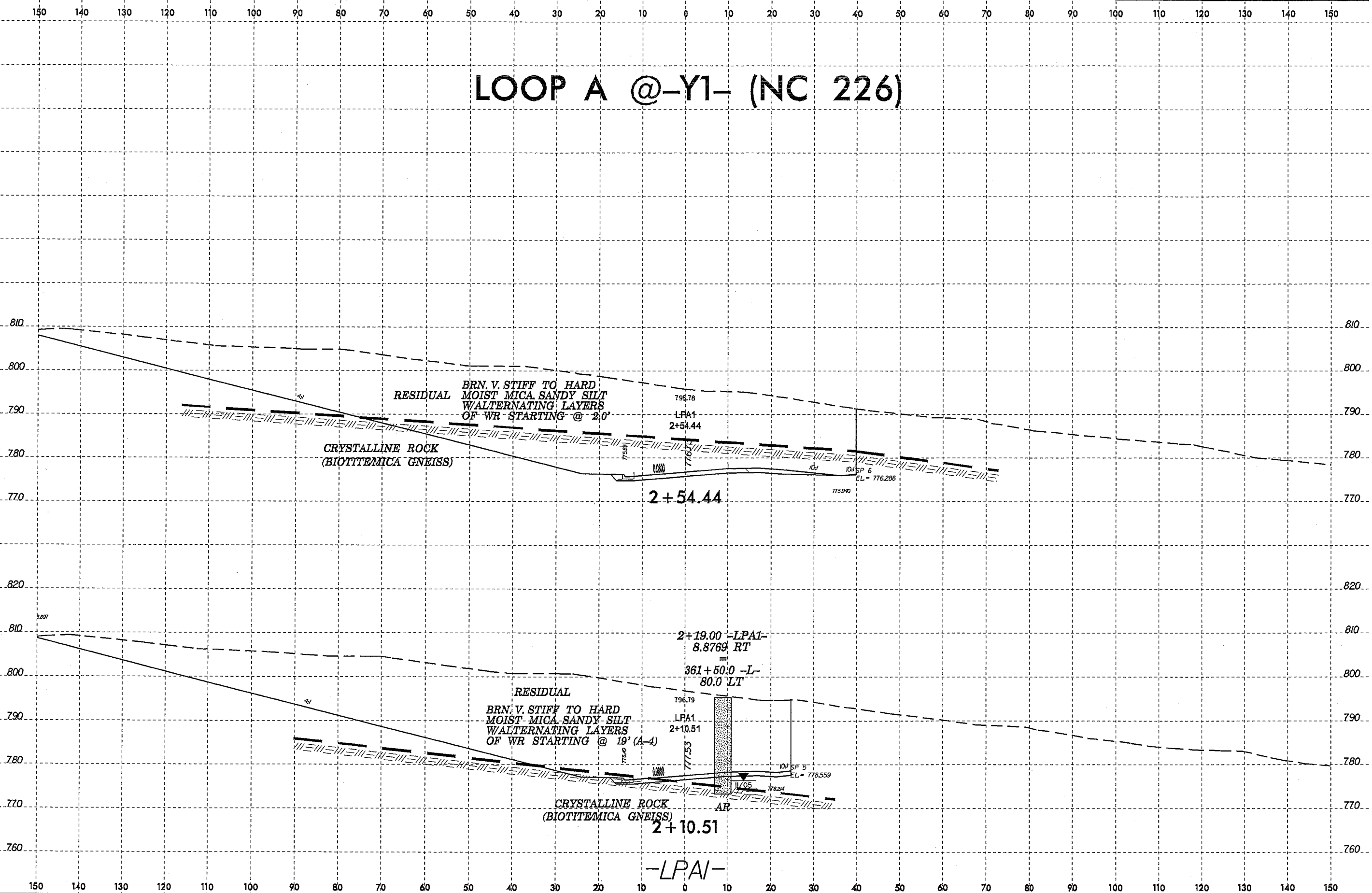


21-APR-2008 13:46 d:\p\proj\2707C\geo\rdh\cleveland\cadd\geotech\asc\VR2707C\_Geo\_x1-RPA1.dgn

8/23/99

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 259
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# LOOP A @-Y1- (NC 226)

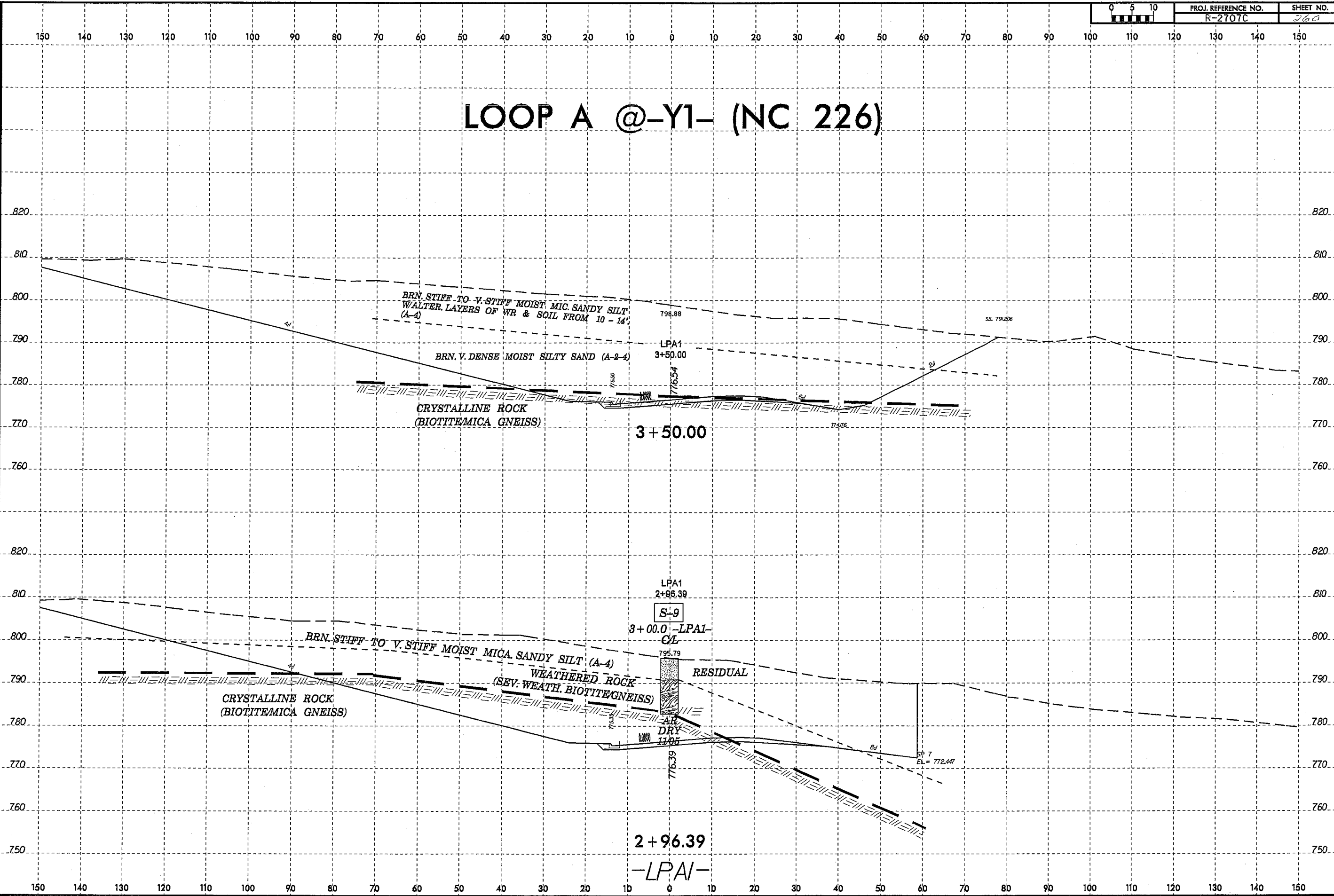


23-APR-2008 09:01  
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 G:\burris

8/23/99

0	5	10
PROJ. REFERENCE NO. R-2707C		
SHEET NO. 260		

# LOOP A @ -YI- (NC 226)

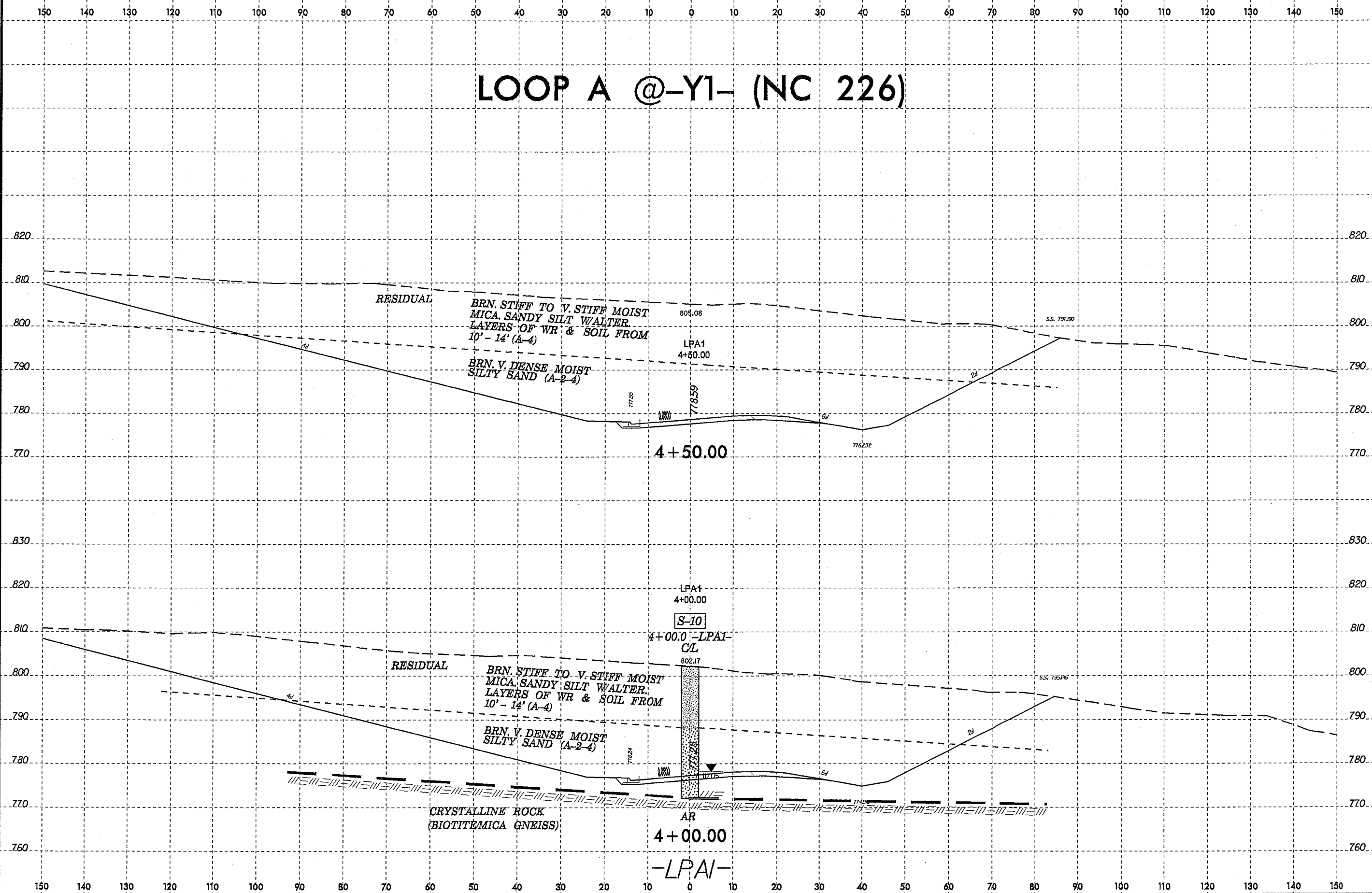


23-APR-2008 09:05  
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8/23/99

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 261
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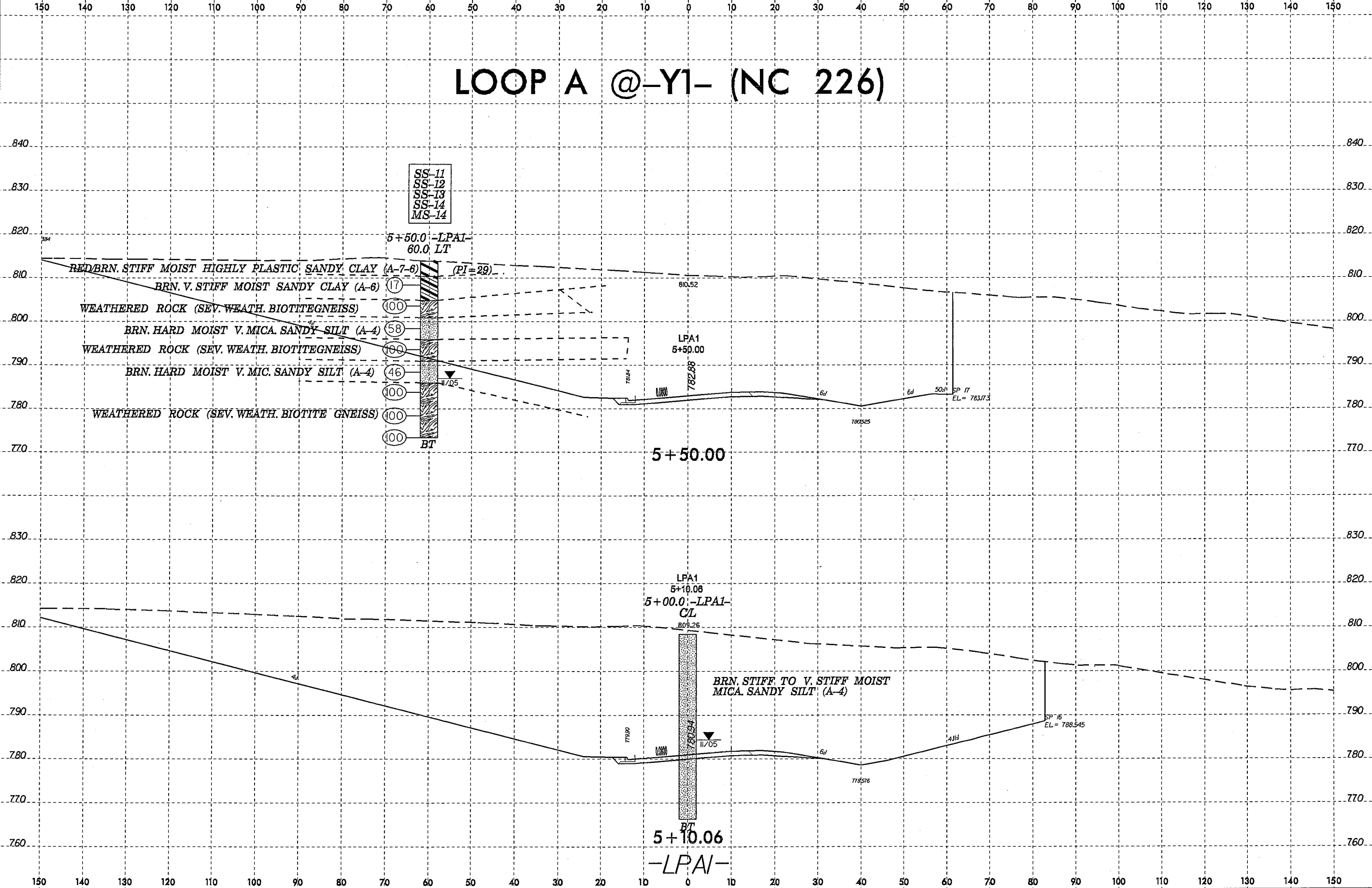
# LOOP A @-Y1- (NC 226)



23-APR-2008 09:03  
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 2707C\loopa\loopa.dgn

8/23/99

# LOOP A @-Y1- (NC 226)

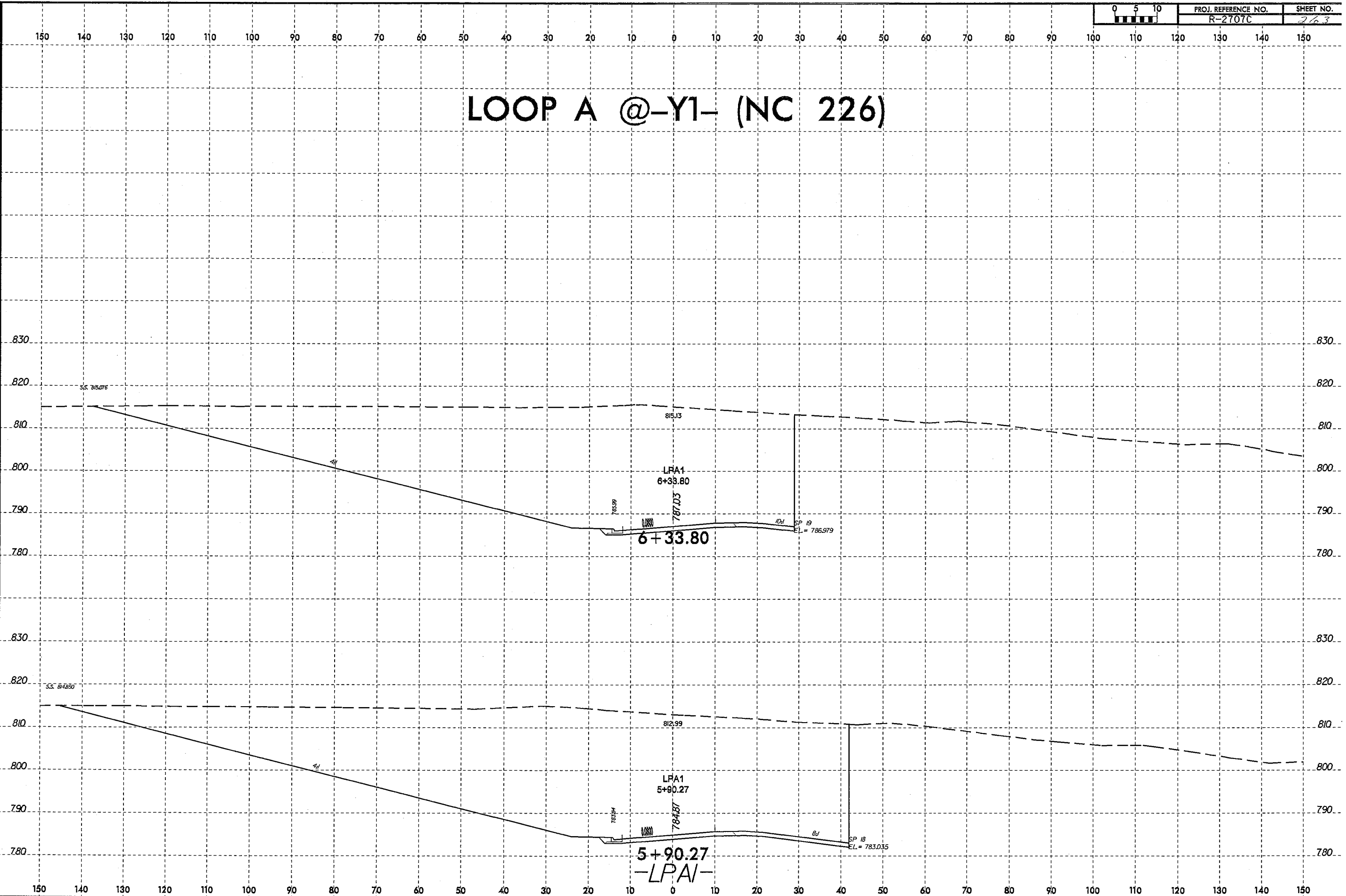


25 APR 2008 09:04  
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# LOOP A @-Y1- (NC 226)

0 5 10	PROJ. REFERENCE NO. R-2707C	SHEET NO. 263
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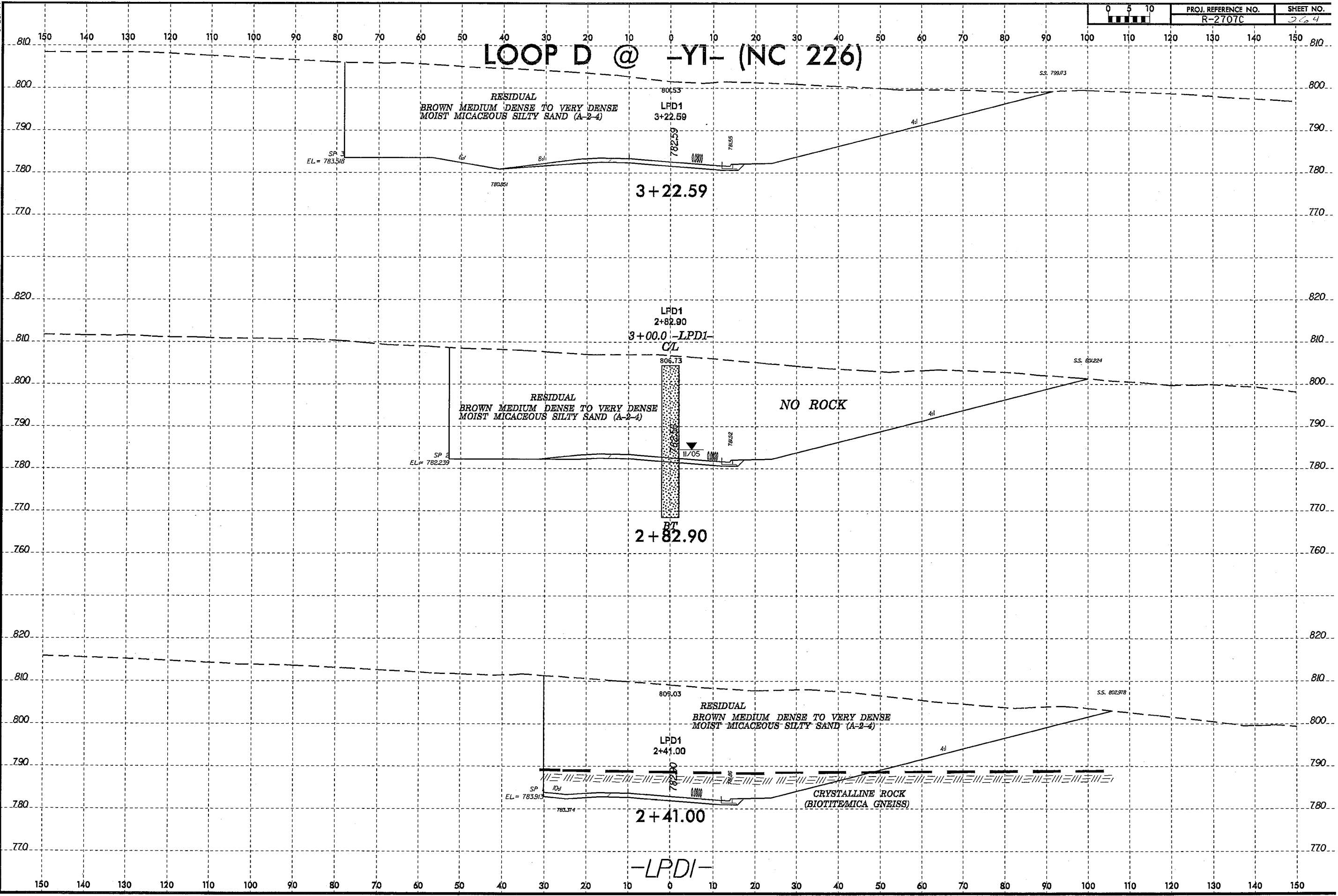


23-APR-2008 09:05  
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 2707C.dwg  
 LPA1.dgn

8/23/99  
23-APR-2008 10:58  
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G:\Projects\12707\civil\rdwy\Cleveland\CADD\_GEO\TECH\XSEC\R2707C(rev)\_LPI.dgn

0 5 10	PROJ. REFERENCE NO.	SHEET NO.
	R-2707C	264

# LOOP D @ -YI- (NC 226)



-LFD1-

SOIL TEST RESULTS

Table with columns: SAMPLE NO., OFFSET, STATION, DEPTH INTERVAL, AASHTO CLASS., L.L., P.I., % BY WEIGHT (C.SAND, F.SAND, SILT, CLAY), % PASSING (SIEVES) (10, 40, 200), % MOISTURE, % ORGANIC, Line or Boring ID.

SOIL TEST RESULTS

Table with columns: SAMPLE NO., OFFSET, STATION, DEPTH INTERVAL, AASHTO CLASS., L.L., P.I., % BY WEIGHT (C.SAND, F.SAND, SILT, CLAY), % PASSING (SIEVES) (10, 40, 200), % MOISTURE, % ORGANIC, Line or Boring ID.

SOIL TEST RESULTS

Table with columns: SAMPLE NO., OFFSET, STATION, DEPTH INTERVAL, AASHTO CLASS., L.L., P.I., % BY WEIGHT (C.SAND, F.SAND, SILT, CLAY), % PASSING (SIEVES) (10, 40, 200), % MOISTURE, % ORGANIC, Line or Boring ID. Rows include samples SS-114 to SS-174.

SOIL TEST RESULTS

Table with columns: SAMPLE NO., OFFSET, STATION, DEPTH INTERVAL, AASHTO CLASS., L.L., P.I., % BY WEIGHT (C.SAND, F.SAND, SILT, CLAY), % PASSING (SIEVES) (10, 40, 200), % MOISTURE, % ORGANIC, Line or Boring ID. Rows include samples SS-175A to SS-242.

**SOIL TEST RESULTS**

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC	Line or Boring ID
							C.SAND	F.SAND	SILT	CLAY	10	40	200			
S-242A	CL	586+00	0.00-3.00	A-7-6(14)	48	22	10.1	25.8	15.8	48.3	100	95	68	-	-	L
S-243	CL	584+00	0.00-3.00	A-6(6)	38	15	15.1	31.5	13.1	40.3	97	90	56	-	-	L
S-244	CL	588+50	0.00-3.00	A-4(0)	21	6	22.8	44.4	10.7	22.2	99	86	39	-	-	L
S-245	CL	608+00	0.00-3.00	A-7-6(20)	59	32	16.1	22.6	4.8	56.5	100	91	65	-	-	L
S-246	CL	582+00	0.00-3.00	A-6(4)	31	14	15.5	39.3	8.9	36.3	100	93	50	-	-	L
S-247	CL	12+50	0.00-3.00	A-6(6)	35	16	21.0	25.2	13.5	40.3	97	85	56	-	-	RP B3
S-248	CL	10+00	0.00-3.00	A-7-6(10)	48	26	23.4	29.8	4.4	42.3	100	88	51	-	-	RP B3
SS-251	CL	3+00	0.00-1.50	A-2-4(0)	17	NP	29.8	47.4	10.7	12.1	100	86	30	-	-	LOOP C3
SS-252	CL	3+00	1.50-3.00	A-6(7)	39	18	14.7	35.3	7.7	42.3	99	92	54	-	-	LOOP C3
S-253	30 LT	29+00	0.00-3.00	A-2-4(0)	24	5	29.6	38.5	7.7	24.2	98	83	35	-	-	Y-4REV
S-254	30 LT	32+00	0.00-3.00	A-6(4)	40	14	18.1	39.9	9.7	32.3	100	92	47	-	-	Y-4REV
S-255	CL	14+00	0.00-3.00	A-6(5)	33	15	19.8	27.4	12.5	40.3	95	84	53	-	-	Y18
S-256	CL	15+50	0.00-3.00	A-6(1)	27	11	23.6	36.9	11.3	28.2	98	86	43	-	-	Y18
S-257	30 RT	28+00	0.00-3.00	A-6(2)	32	13	32.7	28.8	10.3	28.2	95	75	40	-	-	Y14
S-258	50 LT	27+50	0.00-5.00	A-2-4(0)	25	7	36.9	31.9	13.1	18.1	97	74	35	-	-	Y14
S-270	120 RT	503+50	0.00-3.00	A-7-5(33)	84	29	4.2	19.0	36.5	40.3	100	97	83	-	-	L
S-271	120 RT	503+50	3.00-4.00	A-4(0)	36	NP	13.7	49.2	14.9	22.2	97	89	51	-	-	L
S-272	CL	497+00	0.00-3.00	A-7-5(23)	64	29	7.5	24.6	11.5	56.5	100	97	73	-	-	L
S-273	CL	498+00	0.00-3.00	A-7-6(18)	58	32	15.3	24.2	8.1	52.4	97	88	61	-	-	L
MS-273	CL	498+00	0.00-3.00				0.0	0.0	0.0	0.0	0	0	31	-	-	L
S-274	CL	499+00	0.00-4.00	A-7-5(28)	66	35	7.9	21.4	6.3	64.5	100	97	74	-	-	L
S-275	CL	501+00	0.00-4.00	A-7-5(27)	67	34	8.1	20.8	6.7	64.5	100	97	73	-	-	L
S-276	CL	502+00	0.00-4.00	A-6(6)	39	17	7.7	41.9	12.1	38.3	98	95	54	-	-	L
S-277	CL	11+00	0.00-4.00	A-2-4(0)	23	NP	37.2	46.6	7.2	9.1	89	70	18	-	-	RP B2
S-278	CL	11+00	4.00-5.00	A-2-5(0)	45	NP	15.1	62.5	14.3	8.1	98	91	34	-	-	RP B2
S-279	CL	18+50	0.00-2.00	A-2-4(0)	22	3	44.6	31.3	10.1	14.1	87	60	25	-	-	Y 17
S-280	CL	18+50	2.00-4.00	A-7-6(6)	42	20	30.2	24.4	9.1	36.3	96	78	47	-	-	Y 17
S-281	100 RT	18+50	0.00-2.00	A-2-4(0)	33	5	35.3	32.1	16.5	16.1	97	78	35	-	-	Y 17
CBR-1	90 RT	419+00	35.0-40.0	A-7-5(1)	49	12	22.0	50.2	13.7	14.1	99	91	36	-	-	L
ST-1(1,2)	130 RT	400+50	18.7-20.7	A-2-5	50	1	24.4	52.8	20.8	2.0	100	93	27	-	-	L
ST-1(3)	130 RT	400+50	18.7-20.7	A-2-5	53	2	27.2	51.6	19.2	2.0	90	76	24	19.5	-	L
ST-2	120 RT	413+00	31.5-33.4	A-2-5	44	NP	21.7	64.6	9.8	4.0	100	98	20	-	-	

33497.1.4 R-2707C  
US 74 SHELBY BYPASS FROM WEST OF NC 226 TO EAST OF NC 150.

BORING 1 - 390+50 -L-, 75' LT.



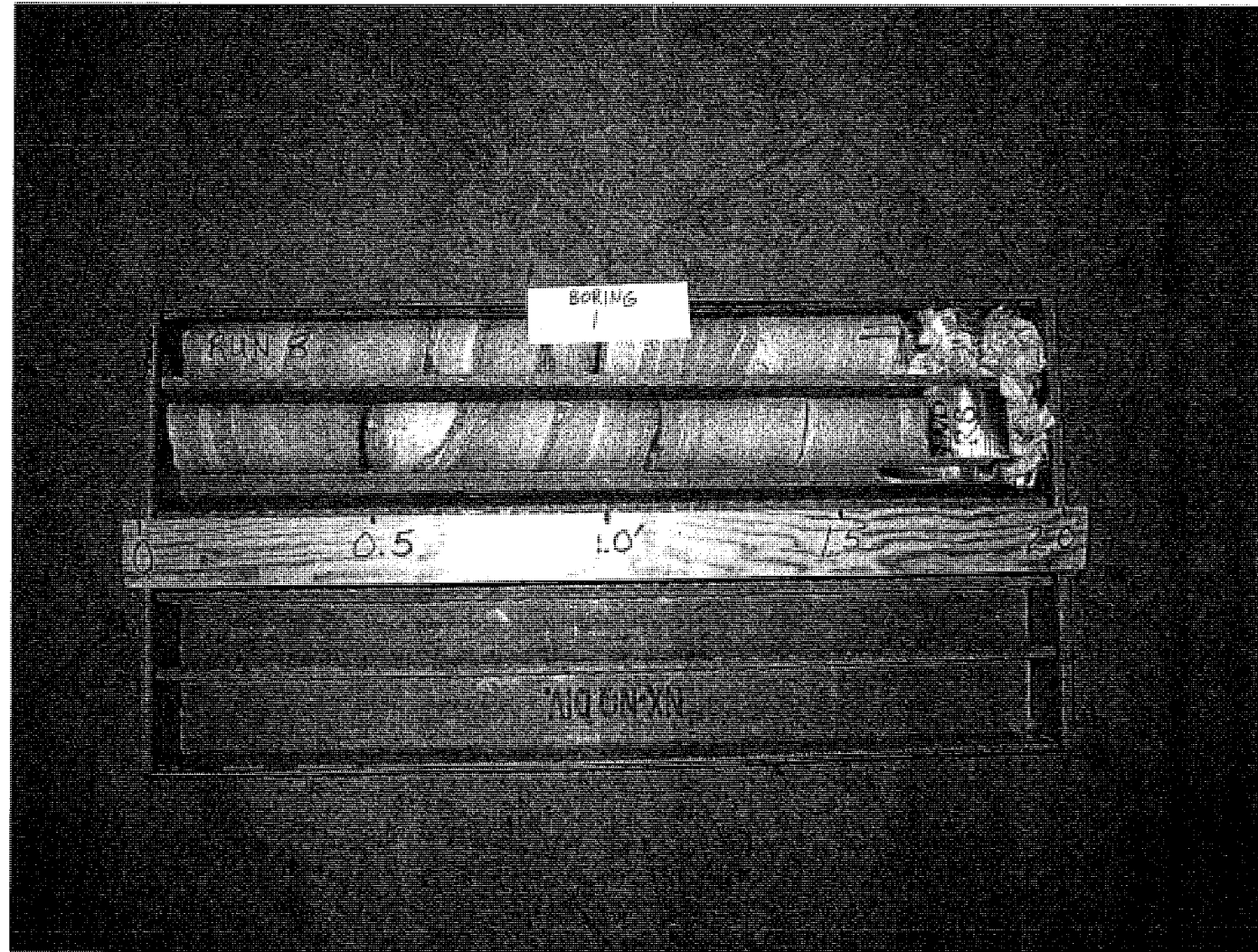
33497.1.4 R-2707C  
US 74 SHELBY BYPASS FROM WEST OF NC 226 TO EAST OF NC 150.

BORING 1 - 390+50 -L-, 75' LT.



33497.1.4 R-2707C  
US 74 SHELBY BYPASS FROM WEST OF NC 226 TO EAST OF NC 150.

BORING 1 - 390+50 -L-, 75' LT.





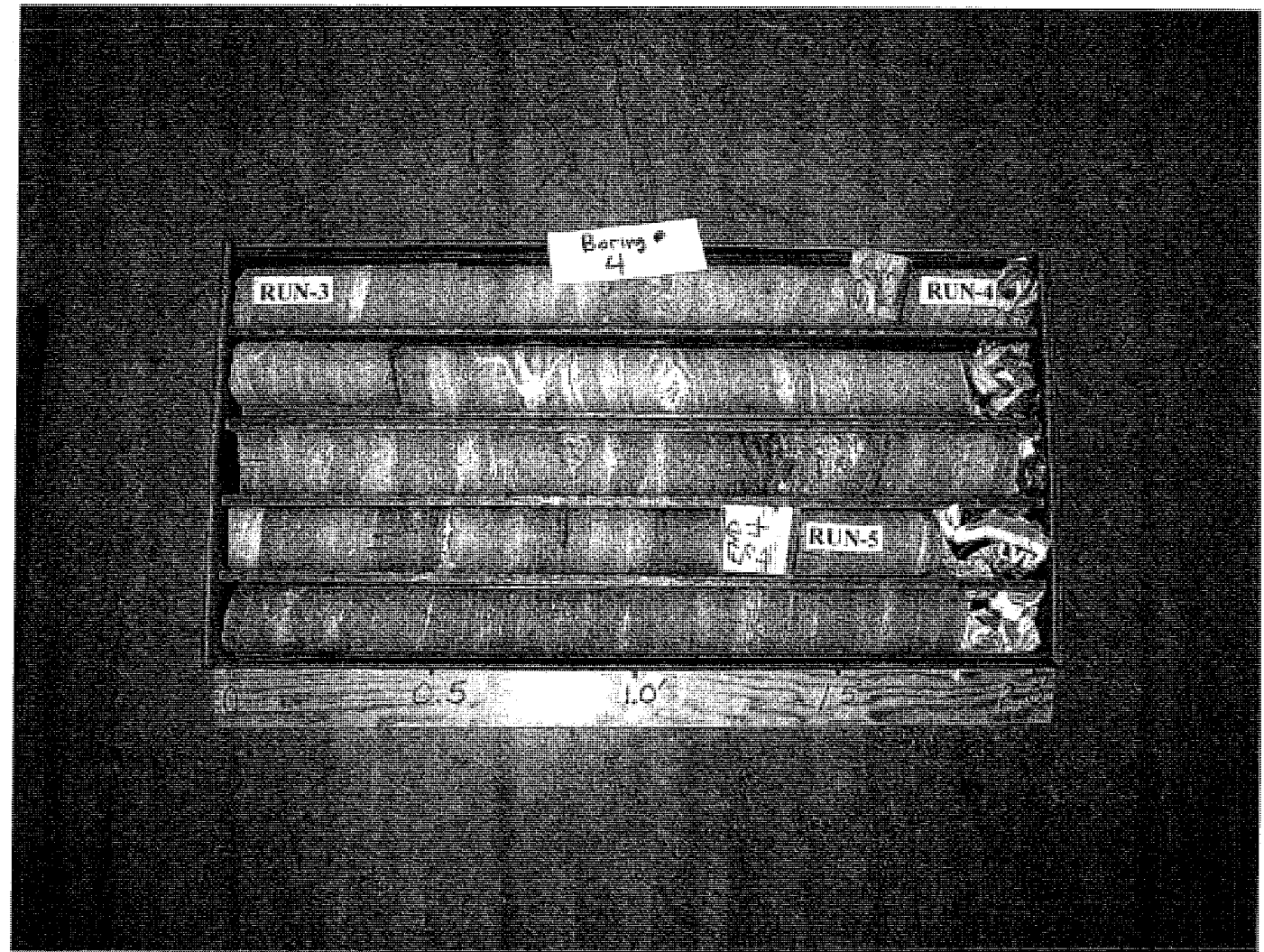
33497.1.4 R-2707C  
US 74 SHELBY BYPASS FROM WEST OF NC 226 TO EAST OF NC 150

BORING 2 - 393+50 -L-, CENTERLINE



33497.1.4 R-2707C  
US 74 SHELBY BYPASS FROM WEST OF NC 226 TO EAST OF NC 150

BORING 4 - 393+00 -L-, 100' LT.



33497.1.4 R-2707C  
US 74 SHELBY BYPASS FROM WEST OF NC 226 TO EAST OF NC 150

BORING 5 - 390+50 -L-, 75' RT.



33497.1.4 R-2707C  
US 74 SHELBY BYPASS FROM WEST OF NC 226 TO EAST OF NC 150

BORING 5 - 390+50 -L-, 75' RT.

