TIP:	U-3609A
COUNTY:	Wayne
DESCRIPTION:	Goldsboro – US 13 (Berkeley Boulevard) from Royal Avenue to South Drive
LET DATE:	May 20, 2014

<u>Roadway and Structure Subsurface</u> <u>**Investigation Information**</u>



March 7, 2013

Mr. Jason Lawing, PE, CFM. **KIMLEY-HORN & ASSOCIATES, INC.** P.O. Box 33068 Raleigh, NC 27636-3068

Re: Culvert Borings Letter Fallin Boulevard Realignment/Berkeley Boulevard Culvert Upgrade Goldsboro, North Carolina GeoTechnologies Project No. 1-10-0646-EA

Mr. Lawing:

As authorized, GeoTechnologies, Inc. is pleased to present the attached subsurface information pertaining to the above referenced project. We understand that the subsurface information will be used by the contractor for help in designing temporary shoring for the culvert upgrade on Berkley Boulevard. Our services included drilling two soil test borings on March 6, 2013 to a depth of about 30 feet at locations shown on the attached Figure 1. Standard penetration testing (ASTM D-1586) was performed at select intervals. Also attached is a generalized subsurface profile (Figure 2) and the individual test borings logs.

GeoTechnologies, Inc. appreciates the opportunity to be of service on this phase of the project. Please contact us if you have any questions concerning this letter or if we may be of additional service on this or other projects.

Sincerely,

GeoTechnologies, Inc.

Of Arral

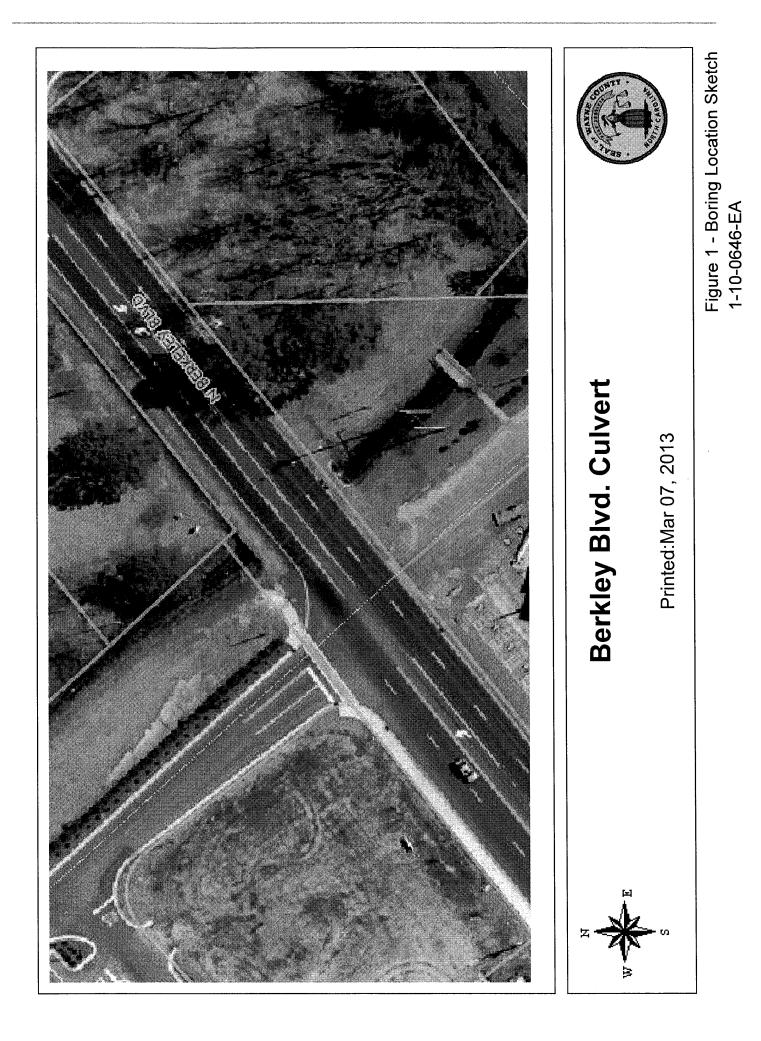
David L. Israel, P.E. Principal Engineer

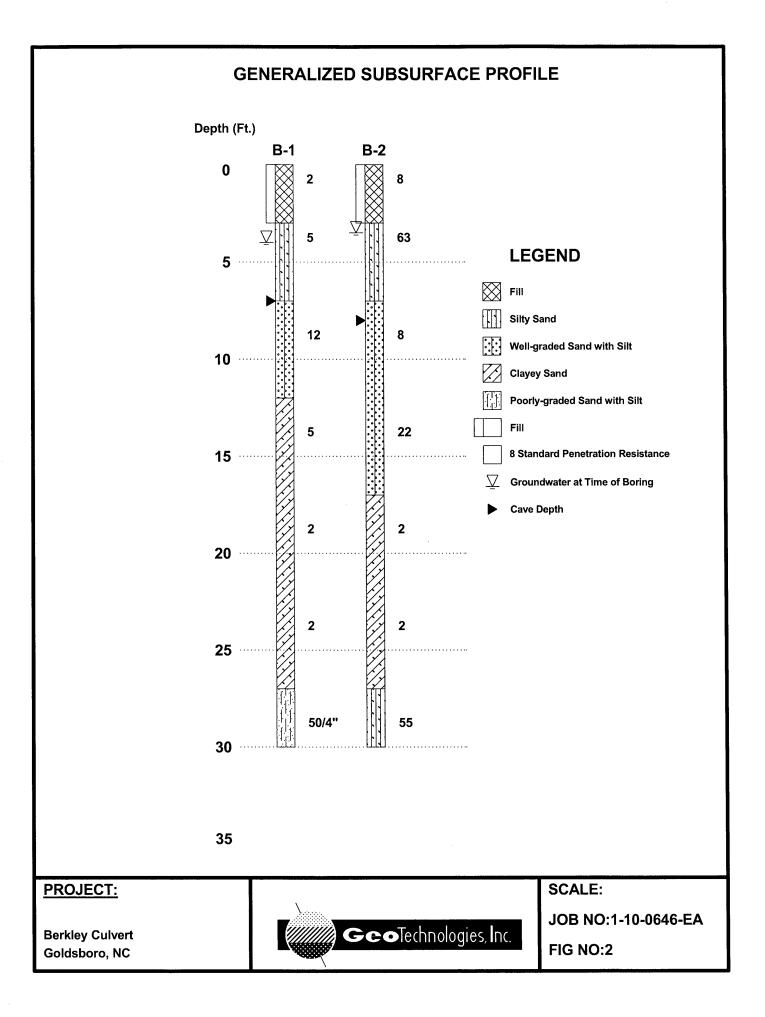
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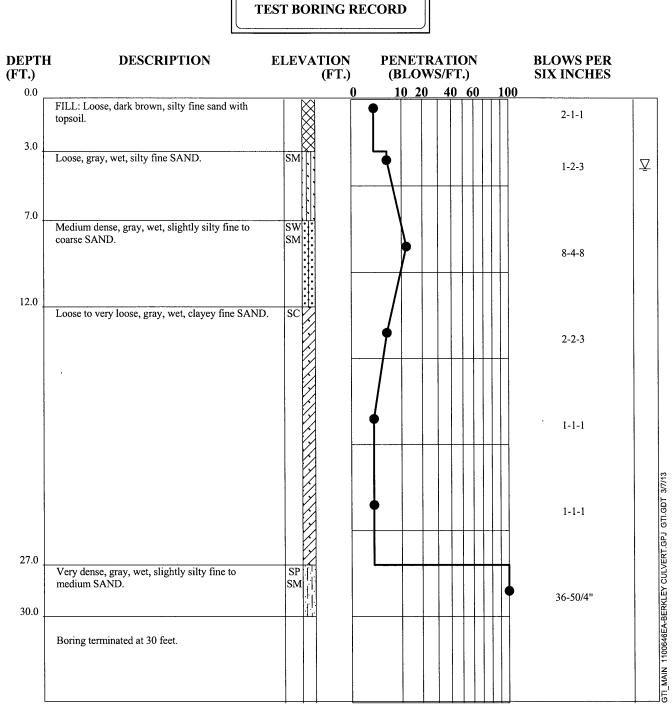
Attachments

1100646ea-culvert

3200 Wellington Ct., Ste. 108 • Raleigh, NC 27615 • Phone 919-954-1514 • Fax 919-954-1428 • www.geotechpa.com • License No. C-0894





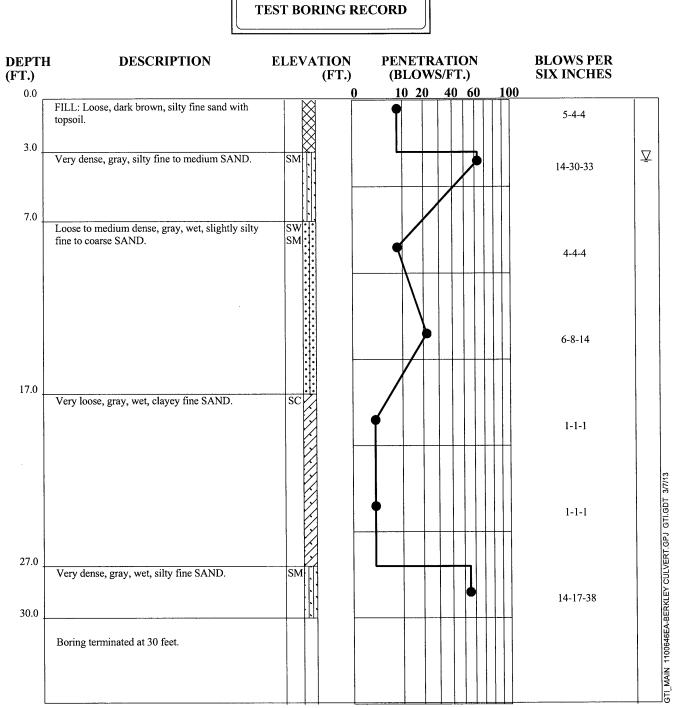


Drilled with ATV rig. Holes backfilled with hole plug.

JOB NUMBER BORING NUMBER B-1 DATE 3-6-13

1-10-0646-EA





Drilled with ATV rig. Holes backfilled with hole plug.

JOB NUMBER **BORING NUMBER** B-2 DATE 3-6-13

1-10-0646-EA



Kimley-Horn & Assoc. Re: Fallin Blvd./Berkeley Blvd. Culvert Upgrade December 22, 2010 Page: 5

TABLE 1TEST BORING LOCATIONS

Fallin Boulevard/Berkeley Boulevard Culvert Extension

GeoTechnologies Project No. 1-10-0646-EA

		NC Grid Coordinates			
Boring #	Location	North	East		
B-1	Roadway	596151	2319480		
B-2	Roadway	596001	2319607		
B-3	Roadway	595912	2319726		
B-4	Culvert	596080	2319238		
B-5	Culvert	596008	2319299		



Kimley-Horn & Assoc. Re: Fallin Blvd./Berkeley Blvd. Culvert Upgrade December 22, 2010 Page: 6

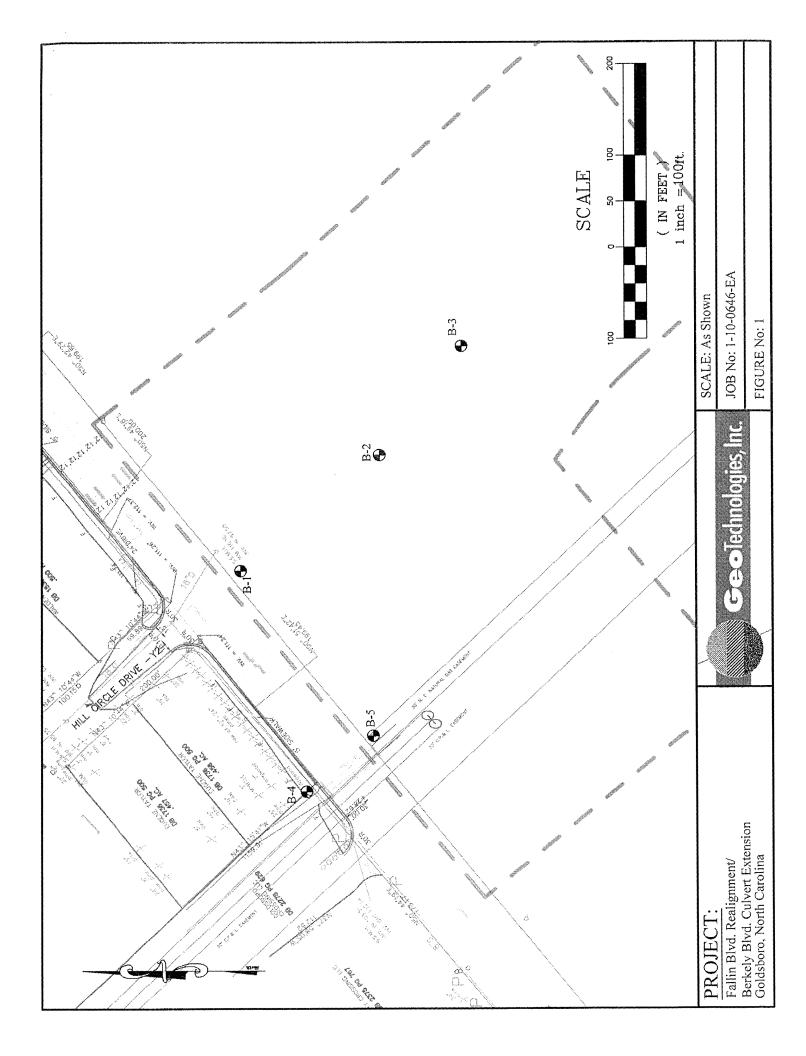
TABLE 2 SUMMARY OF LABORATORY TEST DATA

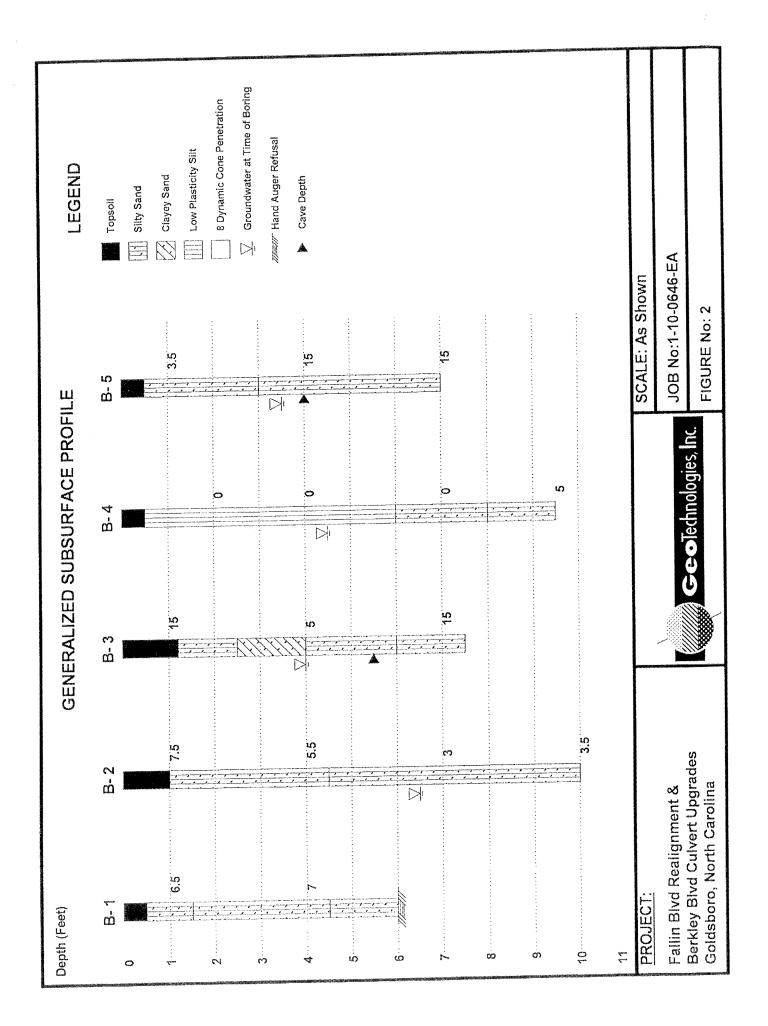
Fallin Boulevard/Berkeley Boulevard Culvert Extension

GeoTechnologies Project No. 1-10-0646-EA

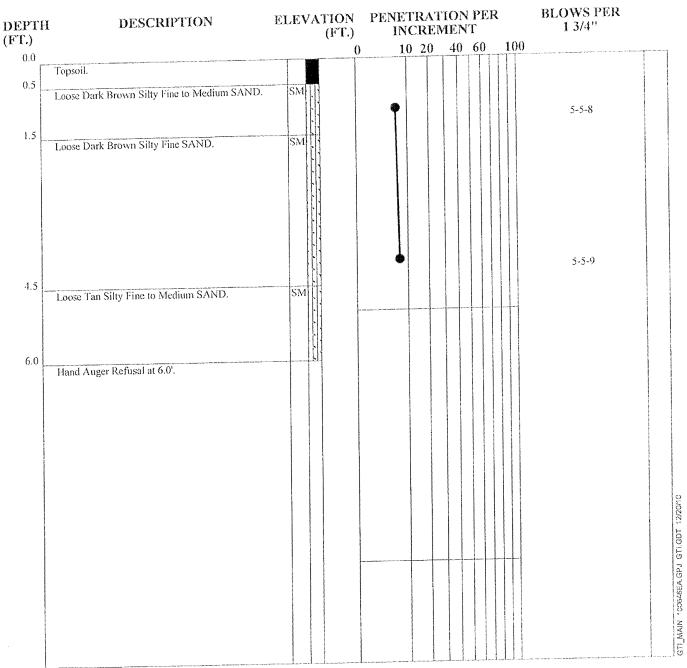
			Atterbei	g Limits	1			
Boring #	Depth (ft)	Unified Soil Classification	Liquid Limit (%)	Plastic Index (%)	% Passing #200 Sieve	Maximum	CBR (%)	Natural Moisture Content (%)
B-1	3	SM	28	2	30.6	-	~	23.3
B-2	1.0 - 3.0	SM	18	0	16.9	121.0	20.8	11.1
B-3	2	SM		-	10.4		-	8.5
B-5	1.5	SM	33	2	-		-	-









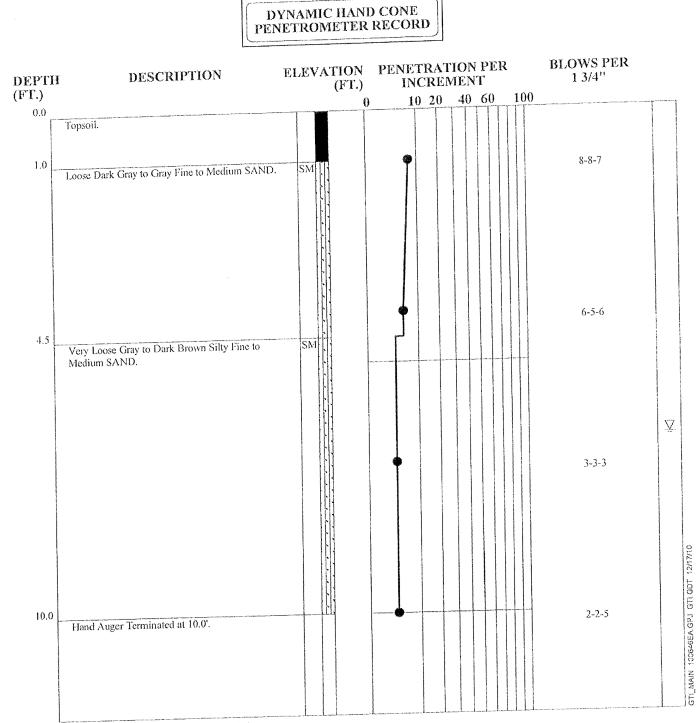


Hand Auger Refusal at 6' on obstruction (possible sewer line).

JOB NUMBER BORING NUMBER B- 1 DATE

1-10-0646-EA



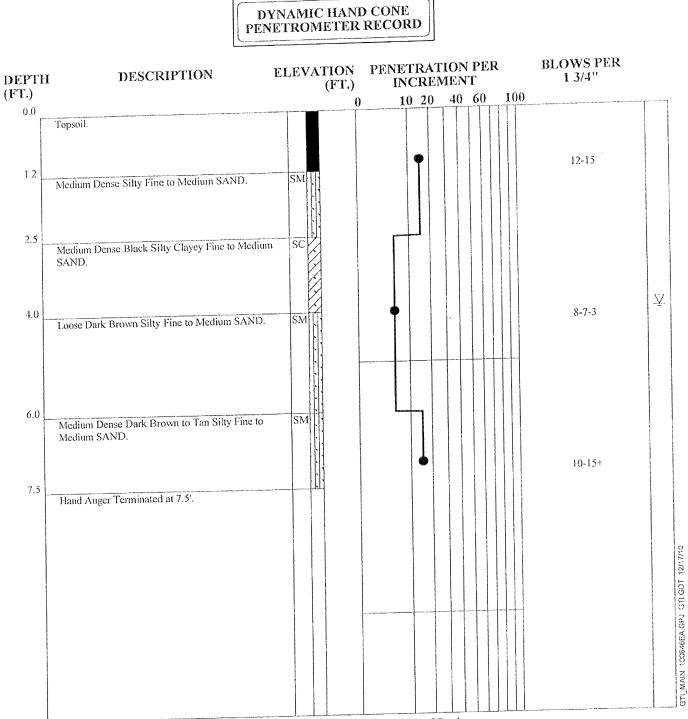


Groundwater at 6.5' at Time of Boring.

JOB NUMBER BORING NUMBER DATE

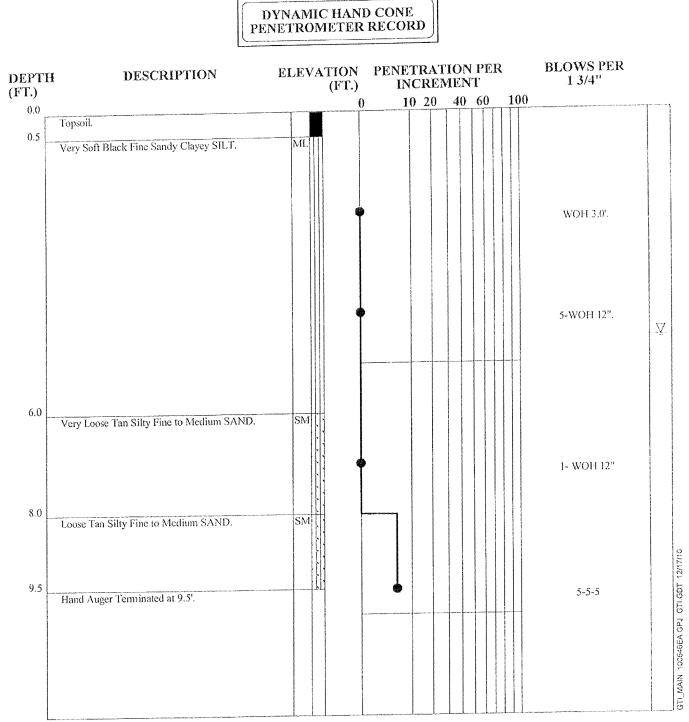
1-10-0646-EA B- 2





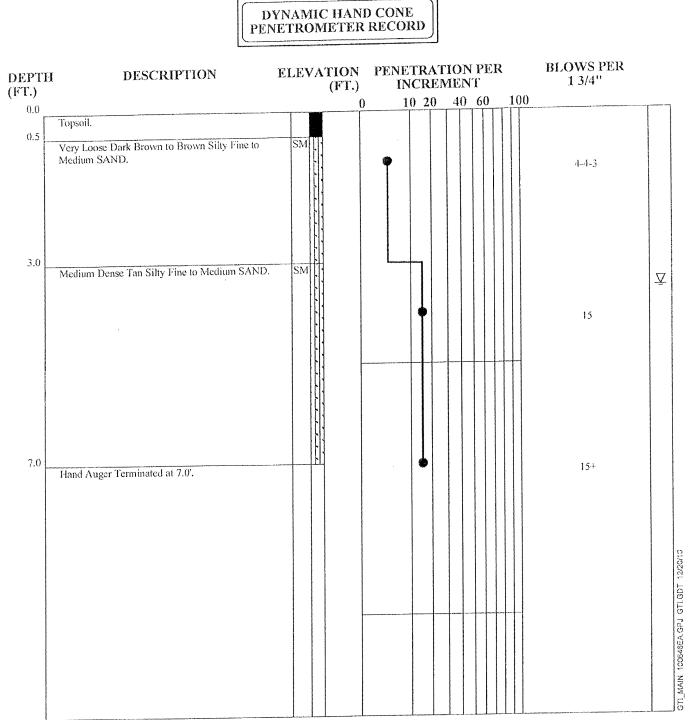
Groundwater at 4.0' at Time of Boring. Boring Caved at 5.5' at Time of Boring.

JOB NUMBER BORING NUMBER DATE 1-10-0646-EA B- 3 GeoTechnologies, Inc.



Groundwater at 4.5' at Time of Boring.

JOB NUMBER BORING NUMBER DATE 1-10-0646-EA B- 4 GeoTechnologies, Inc.



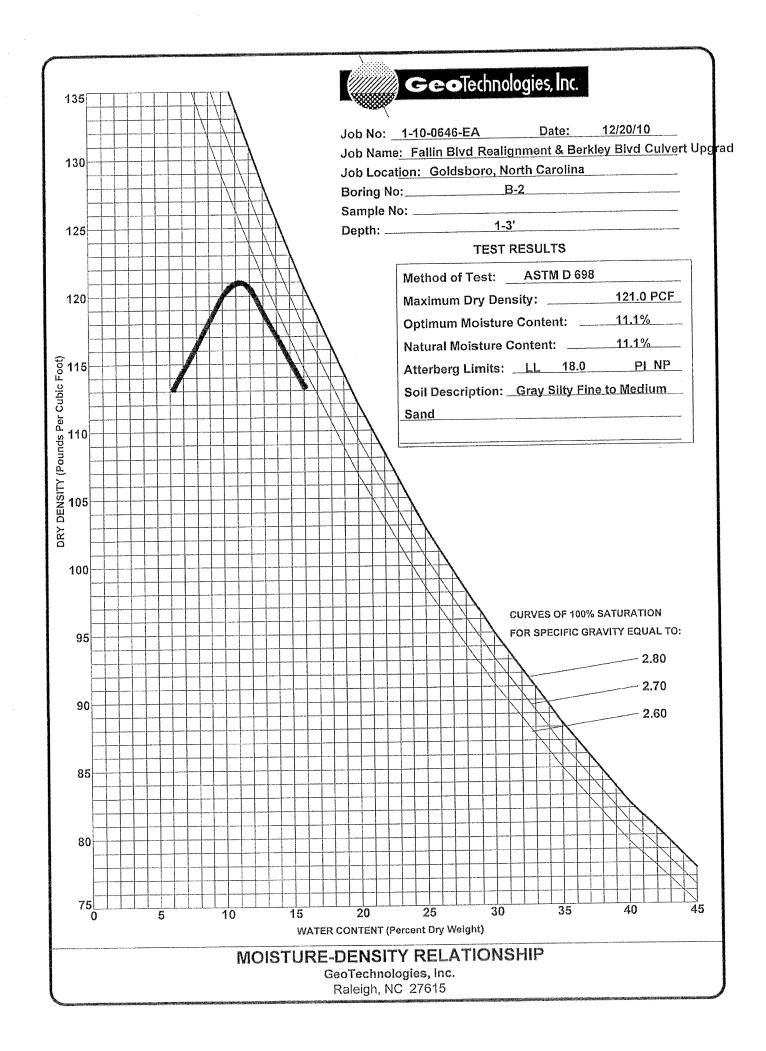
Groundwater at 3.5' at Time of Boring. Boring Caved at 4.0' at Time of Boring..

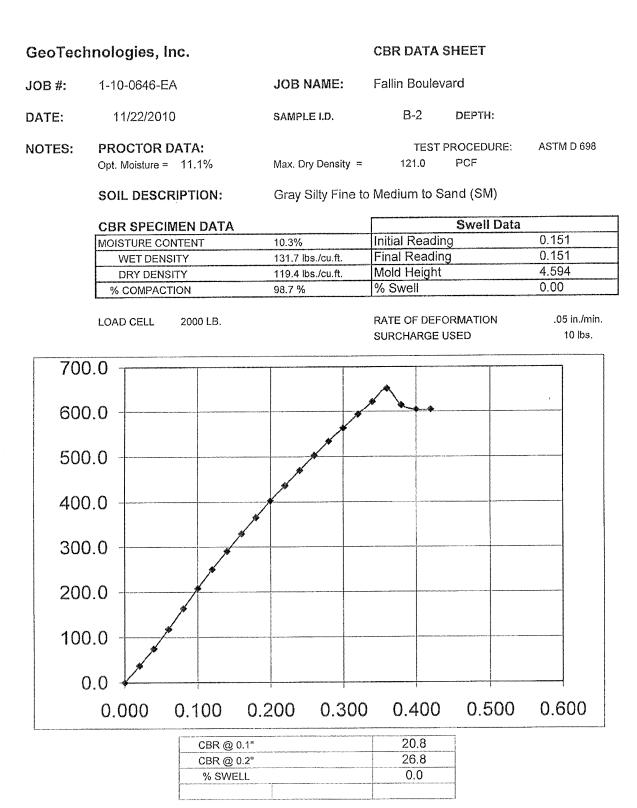
JOB NUMBER BORING NUMBER B- 5 DATE

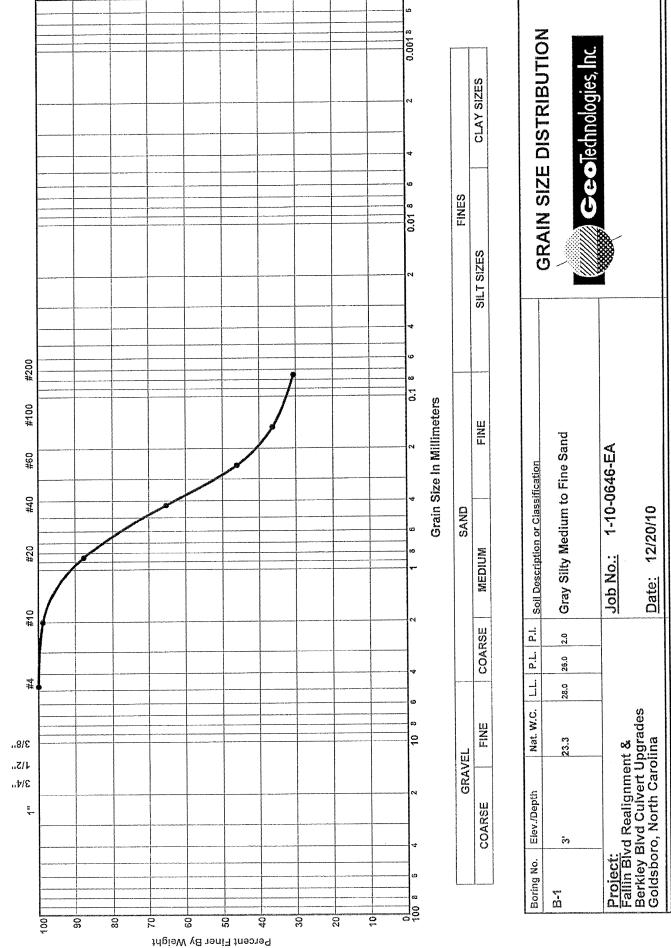
1-10-0646-EA



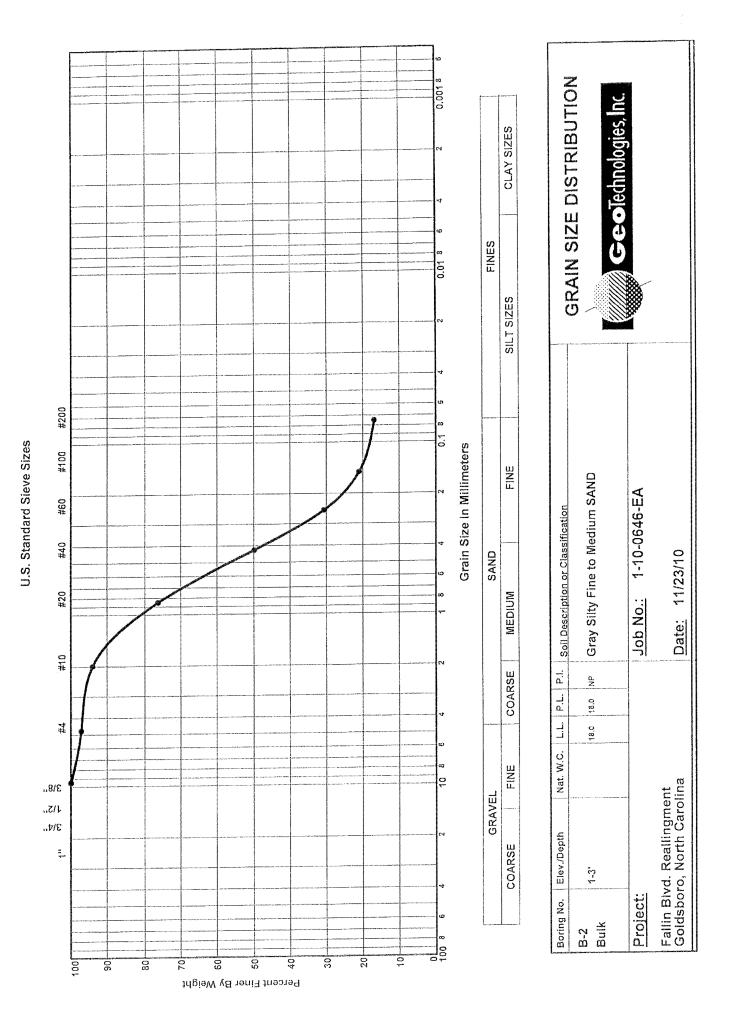
80 (CL) (СН) 70 PLASTICITY 60 50 40 I N D E X 30 20 10 CL MI (ML) (MH) 0 ۶ 0 **x**_____20 100 60 80 40 0 LIQUID LIMIT (LL) PL PI Fines Classification Specimen Identification LL • B-1 Gray Silty Medium to Fine Sand 3' 28 26 2 30.6 X B-2 18 NP 16.9 Gray Silty Fine to Medium Sand 1-3' 18 33 2 Black Silty Sand ► B-5 1.5' 31 1-10-0646-EA JOB NO. Berkley Blvd Culvert Upgrades - Goldsboro, North PROJECT 12/20/10 DATE Carolina **ATTERBERG LIMITS' RESULTS** GeoTechnologies, Inc. Raleigh, NC 27615

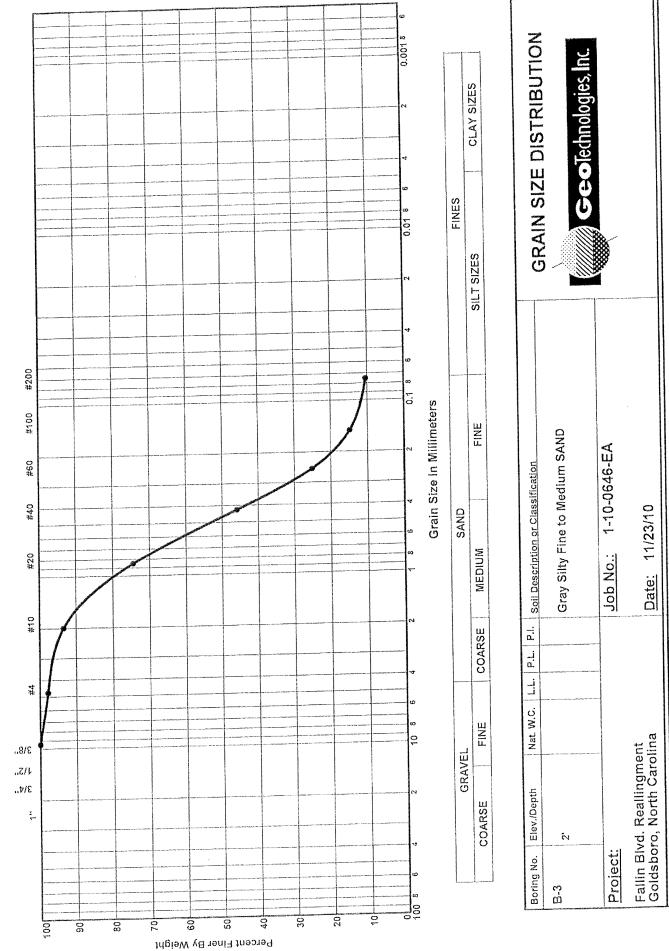






U.S. Standard Sieve Sizes





U.S. Standard Sieve Sizes

Report of Subsurface Investigation Goldsboro Roadway Projects Goldsboro, North Carolina GeoTechnologies Project No. 1-02-0071-EA

Prepared For:

Kimley-Horn & Associates P.O. Box 33068 Raleigh, NC 27636

Prepared By:

GeoTechnologies, Inc., P.A. 3200 Wellington Court, Suite G Raleigh, North Carolina 27615

March 2002



GeoTechnologies, Inc.

3200 Wellington Court, Suite G Raleigh, North Carolina 27615 919-954-1514 Fax 919-954-1428

March 15, 2002

Kimley-Horn & Associates P.O. Box 33068 Raleigh, NC 27636

Attn: Mr. Chuck Nuckols

Re: Report of Subsurface Investigation Goldsboro Roadway Projects – Berkley Boulevard, Royal Avenue And Oak Forest Road Goldsboro, North Carolina GeoTechnologies Project No. 1-02-0071-EA

Gentlemen:

GeoTechnologies, Inc. has completed the authorized subsurface investigation, field testing, laboratory testing, and geotechnical engineering evaluation for the proposed roadway projects in Goldsboro, North Carolina. This report presents the findings of the investigation and recommendations for design and construction of the widening areas.

Subsurface conditions at the site were investigated by completing forty soil test borings. Originally, the borings were to be placed on approximately 200 foot intervals and adjacent to the roadway; however, due to the presence of numerous underground utilities existing immediately adjacent to the roadways, the borings could only be advanced in the 40 locations indicated on the attached Figures 1 through 4. The borings were drilled utilizing a drill rig mounted on an allterrain carrier utilizing 2-1/4 inch diameter hollow stem augers to advance the borings to a termination depth of 10 feet below existing site grade. In these areas, standard penetration testing was completed in accordance with ASTM D-1586 and was utilized to sample the subsurface soils at selected intervals in the borings. Penetration resistances from the soils encountered by the test borings were utilized to evaluate consistency and density of the subsurface materials. Several of the test borings were also probed or advanced by hand augering techniques due to the presence of overhead power lines or inaccessibility due to existing establishments. Standard penetration resistances for the subsurface materials were estimated as the augers were advanced into the subsurface profile and the indicated resistances should therefore also be considered approximate at 7 locations.

Additionally, laboratory Atterberg limits, grain size distribution, standard Proctor compaction, and one-point soaked CBR tests were performed on 10 representative samples.

PROJECT INFORMATION

It is our understanding that the project will involve widening of the existing Berkley Boulevard from Royal Avenue to New Hope Road (Station 10+00 to Station 70+00). Additionally, we understand that widening and construction of new sections of Royal Avenue (Station 10+00 to Station 62+00) and North Oak Forest Road will be conducted.

SUBSURFACE CONDITIONS

Generalized subsurface profiles prepared from the test boring data are attached to this report as Figures 2 through 5 to graphically illustrate subsurface conditions encountered at this site. More detailed descriptions of the conditions encountered at the individual test boring locations are then presented on the attached test boring records.

The subsurface profile consisted of a near surface veneer of topsoil extending to depths of 8 to 12 inches. Topsoil depths in areas adjacent to the existing Central Heights Road, particularly in the agricultural fields, extended up to 18 inches below the site grade. Topsoil materials were underlain by silty and clayey sands extending to the boring termination depth of 10 feet below site grade. Penetration resistances in the sands varied from 2 to 26 blows per foot (bpf). The borings were terminated at 10 feet below existing site grade.

All of the test borings were terminated prior to encountering partially weathered rock. Groundwater was encountered between 2 and 7 feet below the site grade. It should be noted that the subsurface conditions on this site are conducive to the development of perched water and groundwater levels are likely to fluctuate during different times of the year.

LABORATORY INVESTIGATION

The laboratory testing program was directed primarily towards evaluating the subgrade support characteristics of the subsurface soils. Soil samples recovered from the field were visually classified by a geotechnical engineer prior to laboratory testing. The laboratory testing program included the following items which were completed in general accordance with the specified ASTM guidelines:

- 1. Standard Proctor Compaction Tests (ASTM D-698),
- 2. California Bearing Ratio Tests (ASTM D-1883), and
- 3. Grain Size Distribution (ASTM D-1140).

The results of all laboratory tests are attached to this report.

In summary, the results of the standard Proctor compaction tests indicate that the near surface soils at the site have standard Proctor maximum dry densities ranging from approximately 114.0 to 123.9 pounds per cubic foot(pcf) with optimum moisture contents of



approximately 10.2 to 14.0%. The California Bearing Ratio tests completed on samples recovered from the site have design CBR values of between 6.2 to in excess of 20% with negligible swell values. Typically, the soils which exist in this area will exhibit CBR values on the order of about 6% to 10% when properly recompacted to not less than 98% of the standard Proctor maximum dry density. The majority of the soils encountered on this site consist of nonplastic sandy materials and it is our opinion that design CBR values on the order of 6 to 10% are commonly found in the area.

RECOMMENDATIONS

The following recommendations are made based upon a review of the attached test boring data, laboratory testing, our understanding of the proposed construction, and past experience with similar projects and subsurface conditions. Should site grading or roadway alignment change significantly from those now under consideration, we would appreciate being provided with that information so that these recommendations may be confirmed, extended, or modified as necessary.

<u>General Site Conditions</u>. Test borings performed along the route of the proposed roadways indicate the soils to consist predominately of nonplastic silty and clayey sands. The sandy materials were loose in some areas and contained excess moisture content. Some repair work consisting of moisture conditioning and recompacting the surface soils should be anticipated. It should be noted that numerous underground utilities exist immediately adjacent to the existing roadways and that those utility trenches probably have not been backfilled with properly compacted fill in all cases. Our experience has been that utility backfill over lines which are installed as closely spaced as those which exist along this roadway alignment generally are moderately to poorly compacted and will take on significant quantities of moisture during the wetter winter months of the year making those areas unstable.

Based on these findings, we do not anticipate that difficult excavation will be encountered anywhere along the proposed widening project, but the marginal subgrade conditions will exist due to loose, wet sands and over underground utilities. We suggest that the design be based on CBR values of 6 to 10% and that consideration be given to design alternatives for strengthening the roadway section over portions of the utility corridors. Typically, the utility corridors are repaired by excavating slightly deeper and utilizing a geogrid reinforcement such as BX-1100 grid with additional stone replacement. If the depth of the line is such that the appropriate over-excavation and stone replacement cannot be performed, another practice which has been successfully used is to increase the support value of the finished base course by adding approximately 4% cement by weight using a rotor tiller to provide for uniform distribution of this cement in the section. The most appropriate method of repair will need to be determined in the field at the time of construction. Due to very significant potential for having marginal conditions in the utility corridors, we suggest that roadway sections include alternatives for stabilizing the roadway subgrade over the utility corridors. Additionally, the subgrade soils should be scarified and recompacted prior to placement of CABC base course stone or fill. The



specific method and location of repairs will need to be evaluated in the field during grading activities.

Site Grading Considerations. The initial grading process should begin with the removal of all vegetation and topsoil from those areas designed for construction of the proposed widening areas. We anticipate that stripping thickness will generally be on the order of 6 to 12 inches; however, these measurements may be thicker in agricultural areas. At these locations, stripping thickness on the order of 8 to 18 inches may be required to adequately remove all roots and organics. Once stripping is completed, we recommend that all areas to receive fill be proofrolled with a partially loaded dump truck or similar piece of rubber tired equipment in order to identify any areas exhibiting subgrade deflection. Any area which ruts or pumps excessively under the action of rubber tired equipment should be properly cut to firm material and replaced with properly compacted structural fill or reworked and recompacted in place. Once the proposed widening areas or new roadways have been stripped, we recommend that a geotechnical engineer visit with the contractor on the site to provide additional recommendations regarding horizontal and vertical limits of repair and the necessity of utilizing a geogrid reinforcement or additional stone. Any off-site borrow fill used should consist of silty or clayey sands or low plasticity silts or clays having AASHTO soil classifications of A-1, A-2, A-3, A-4, or A-6. These materials should not be compacted to less than 95% of the standard Proctor maximum dry density except for the final foot beneath pavement subgrades where this requirement should be increased to 100% of the standard Proctor maximum. It is recommended that quality control testing be performed to verify that proper soil density specifications are being met, and to insure the placement of fill is being performed in a controlled manner.

Since the on-site soils are moisture sensitive, the contractor should be prepared to moisture condition the near surface soils as needed to achieve proper compaction. Fill materials should be compacted within 2% of the optimum moisture content. High near surface moisture conditions could result in rutting or pumping of the near surface soils which will require repair in the form of undercut and structural fill replacement or discing, drying, and recompacting; however, the exact limits of these repairs cannot be determined until the area has been proofrolled.

<u>Pavement Design Recommendations</u>. Laboratory standard Proctor compaction and 96 hour soaked CBR tests were performed on samples obtained from various locations which appear to be at or near finished grade. GeoTechnologies has utilized design CBR values ranging from 6 to 10 percent from averages for each section, based on the results of the CBR testing and our past experience with similar soil conditions.

Specific pavement designs are provided for Berkley Road, Royal Avenue West, and Royal Avenue extension (Central Heights and Oak Forest). Additionally, designs have been provided utilizing CABC base coarse stone as well as an alternate design utilizing full depth asphalt. The most important factors affecting pavement life in the area of the site are the condition of the subgrade immediately prior to base course stone placement or paving and post construction drainage. It is important that subgrades be reworked and compacted to not less than 100% of the standard Proctor maximum dry density immediately prior to base course stone



placement or paving. We recommend that all pavement areas be detailed to promote positive drainage away from paved areas. Pavement designs for these conditions, based on the traffic volumes estimated for 2,015 as provided by Kimley Horn & Associates, are as follows:

Section	S12.5B (in)	I19.0B (in)	B25.0B (in)	ABC (in)
Berkley Road	3	3	4.5	
	3	3		10
Royal Avenue West	3	3	4.0	
	3	3		10
Royal Avenue Extension	3	3	4.5	
	3	3		10

CABC base course stone should be compacted to 100% of the standard Proctor maximum dry density and all materials should comply with guidelines established by NCDOT for Roads and Structures. Surface asphalt(S12.5B and I19.0B) should be placed in lifts not less than 1.0 inch in thickness and should not to exceed 2.5 inches in thickness. H binder(B25.0B) should be placed in lifts not less than 2.0 inches in thickness and should not to exceed 4.0 inches in thickness.

GeoTechnologies, Inc. appreciates the opportunity to have provided you with our services on this phase of the project. Please contact us if you should have questions regarding this report or if we may be of further assistance.

Very truly yours,

GeoTechnologies, Inc.

WWWWWWWWWWWWW SFAI 026472 'QSUK NAP

Toby Mallik, P.E.

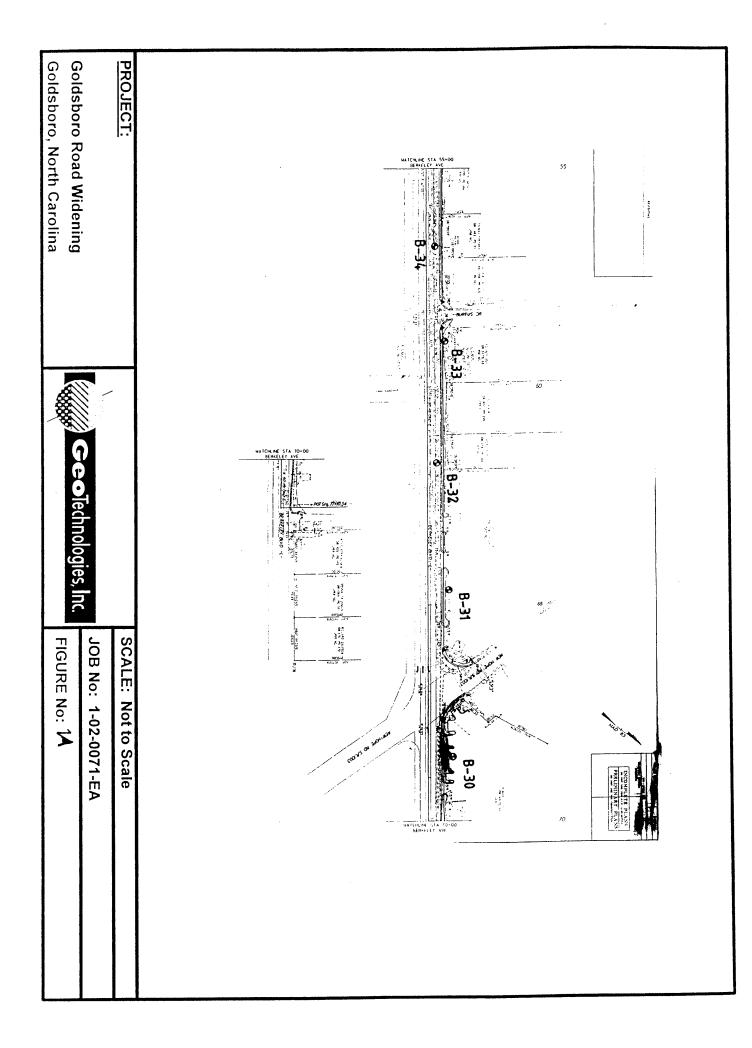
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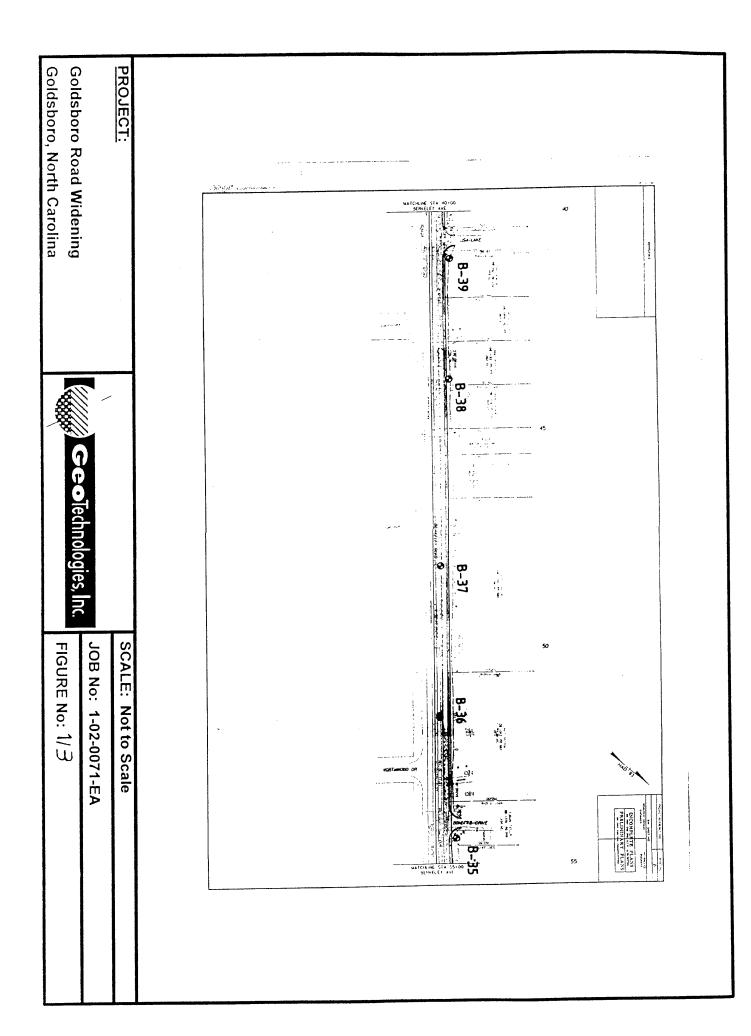
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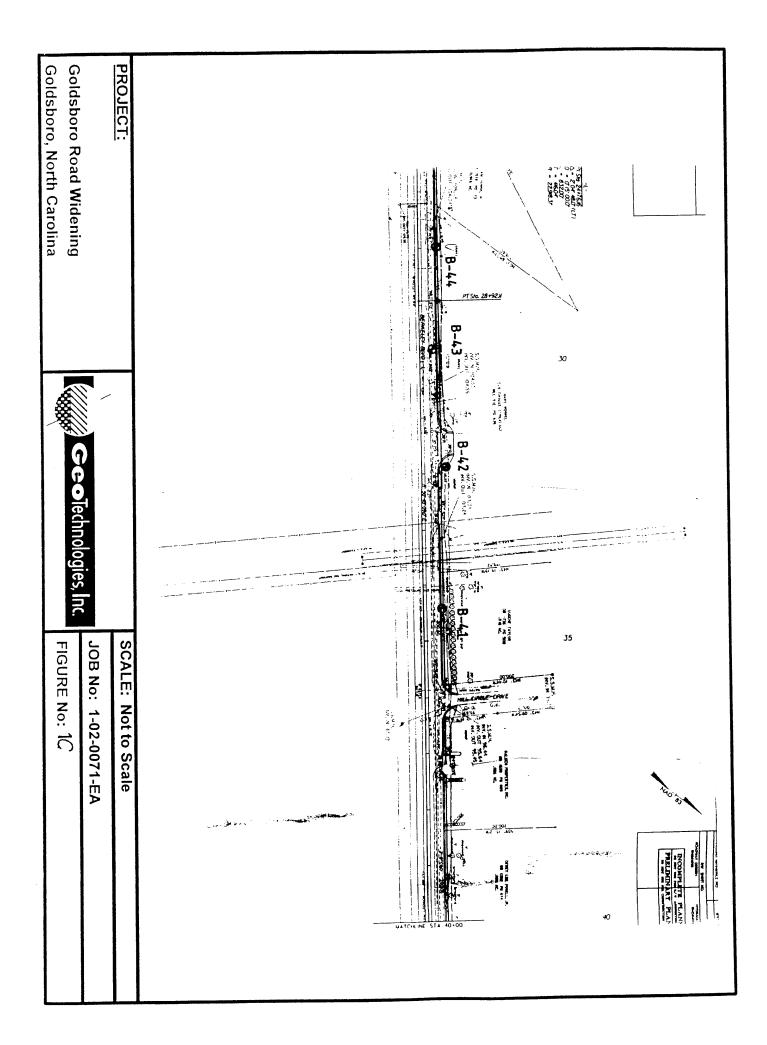
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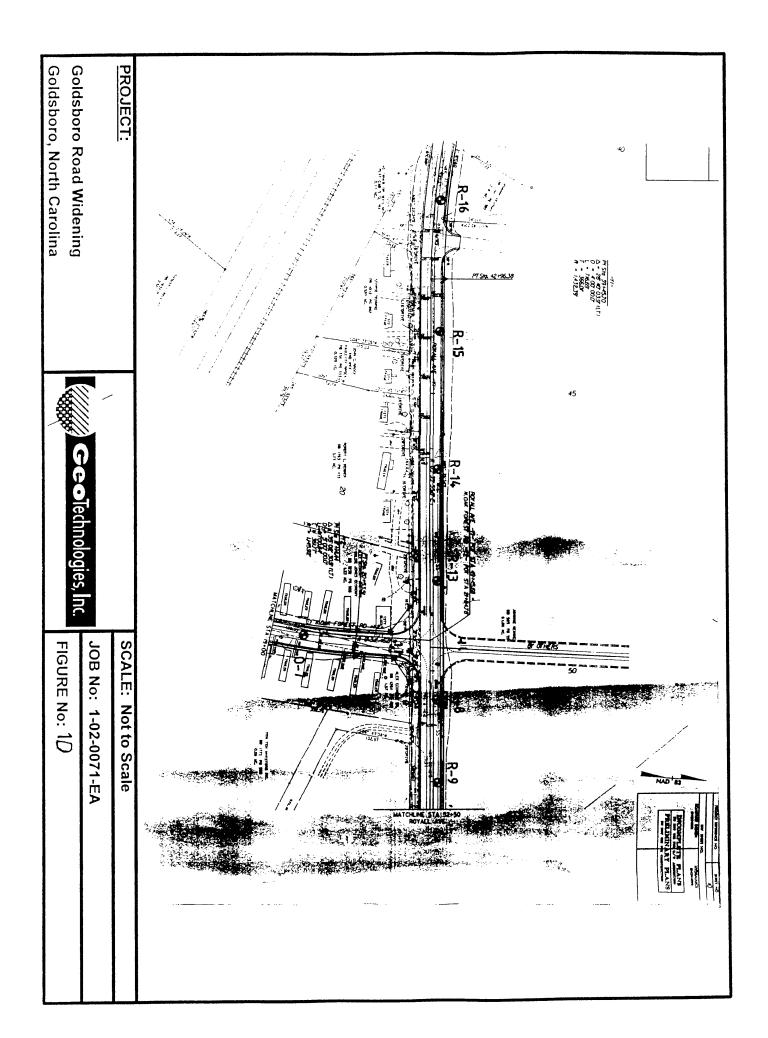
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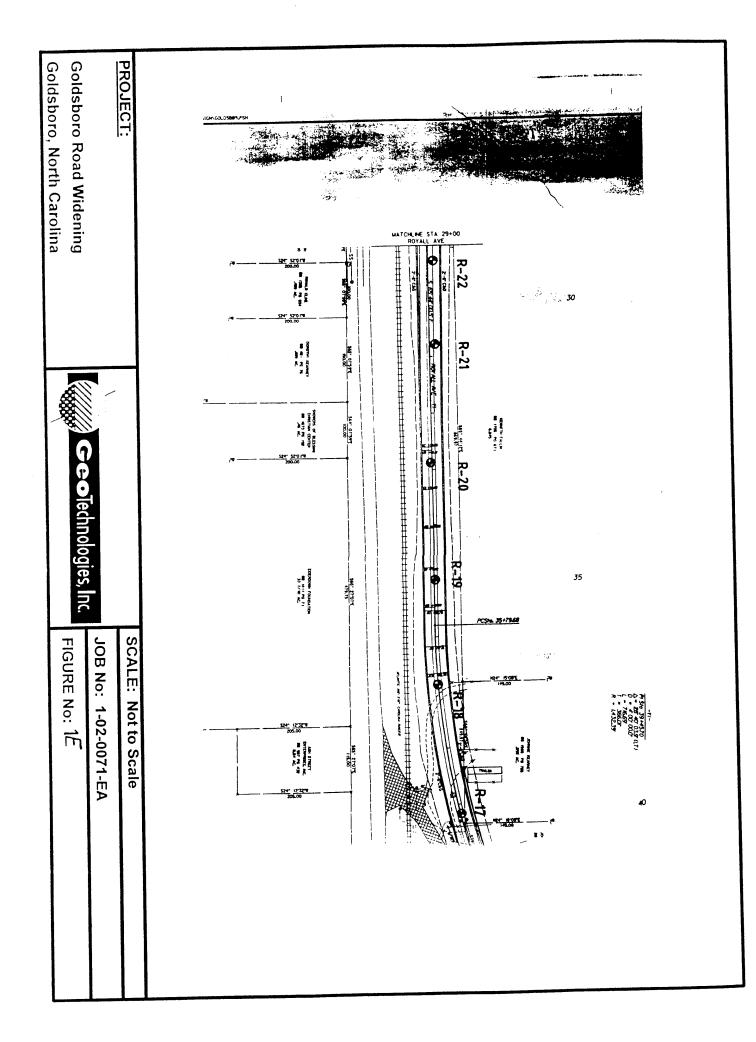


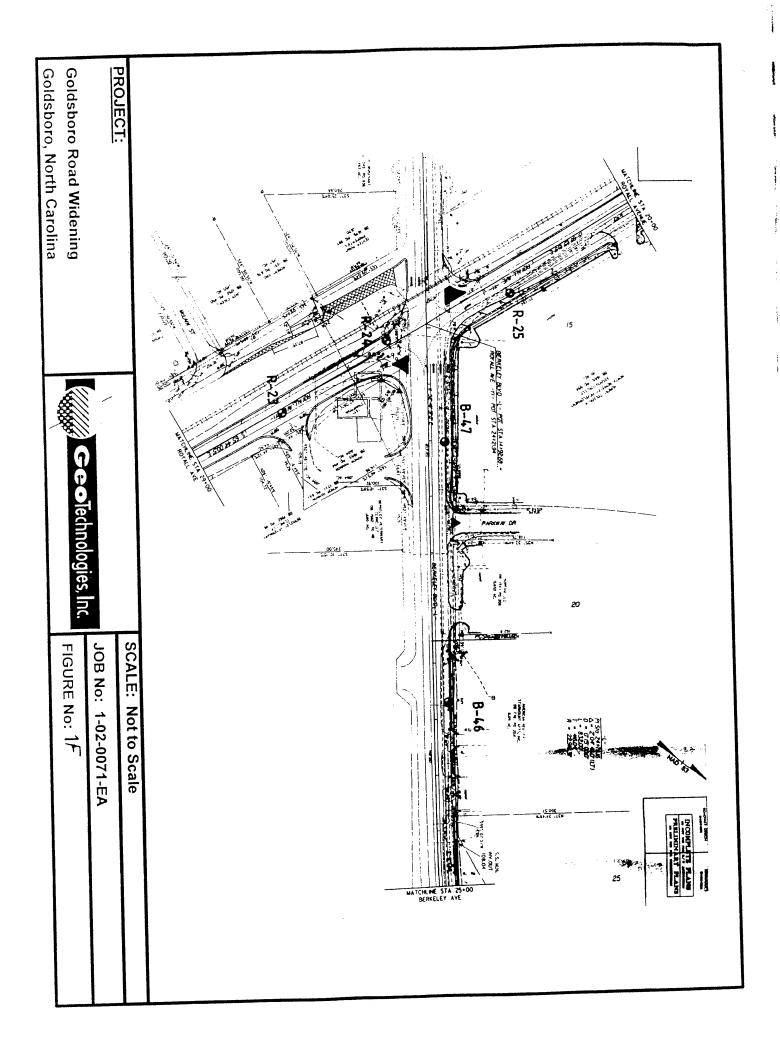


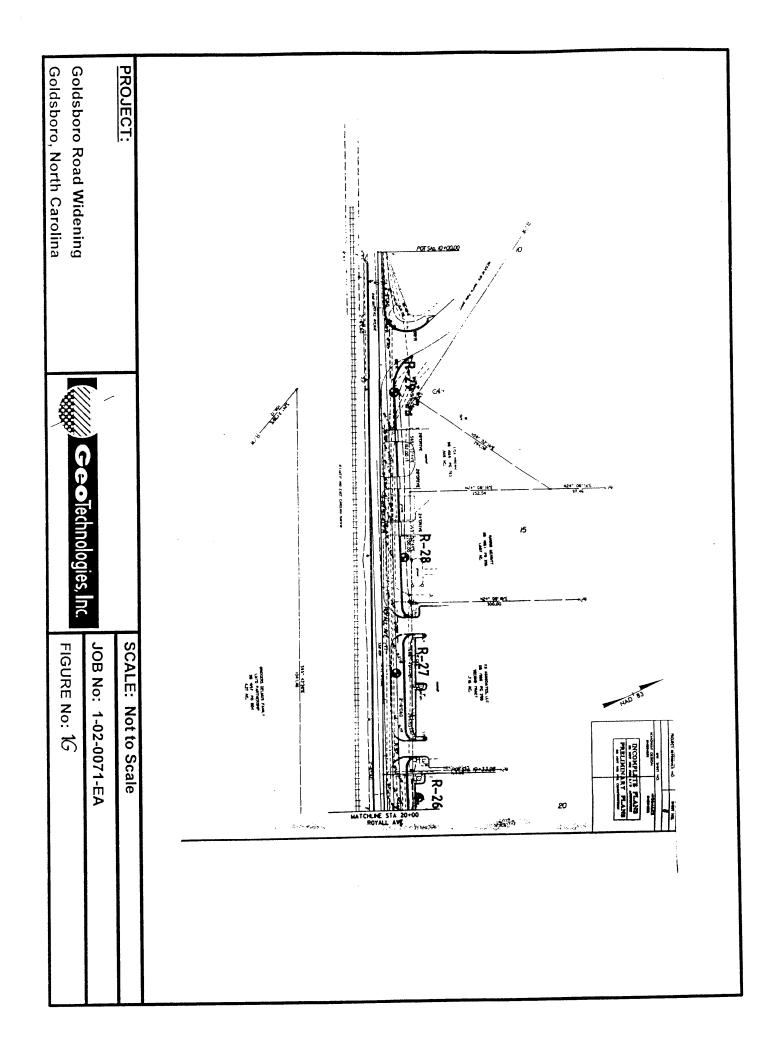




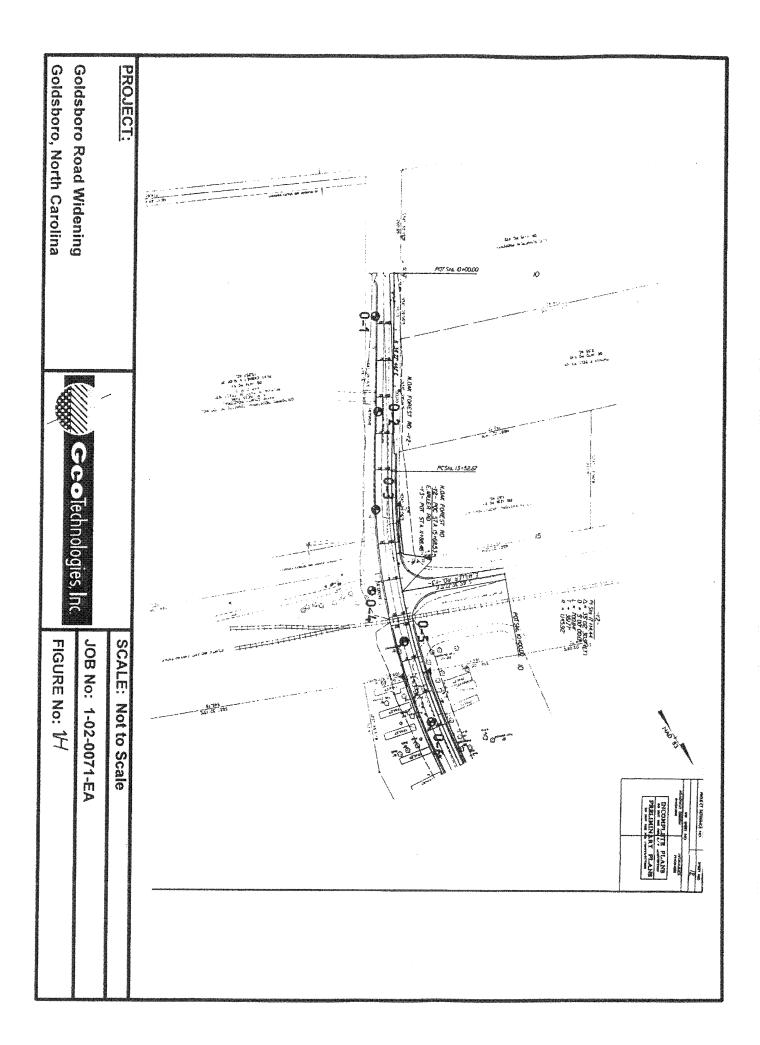


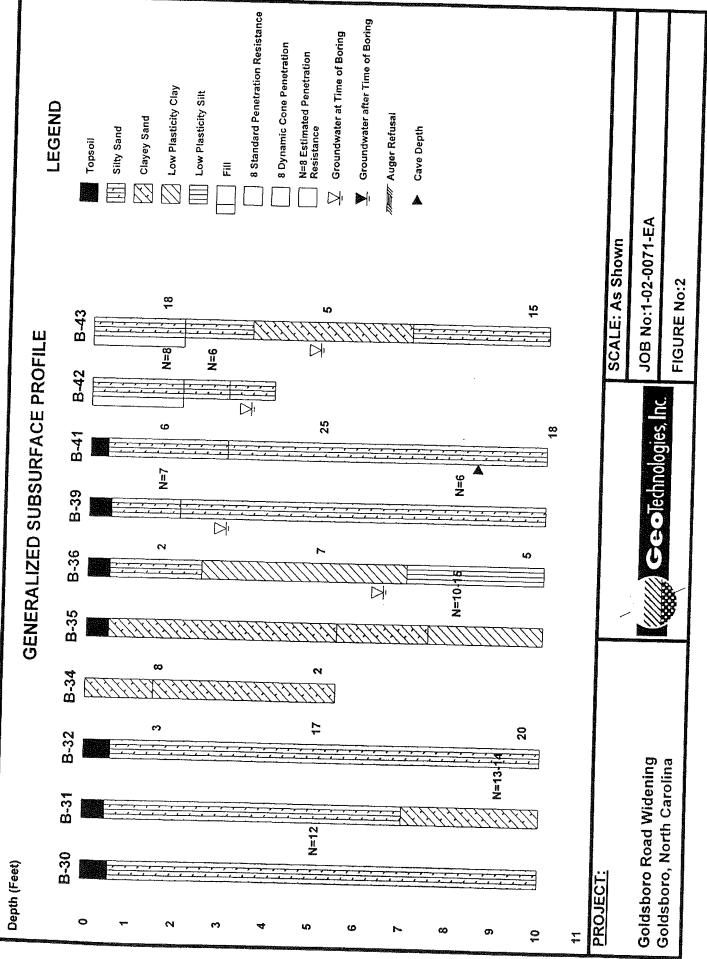


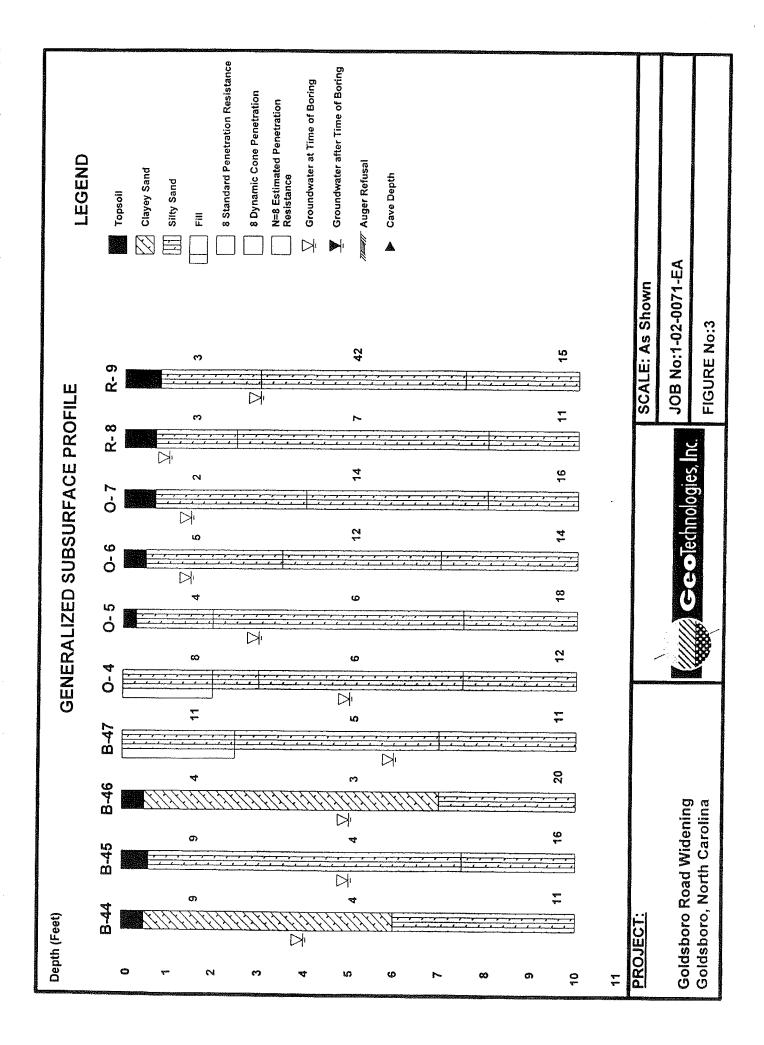


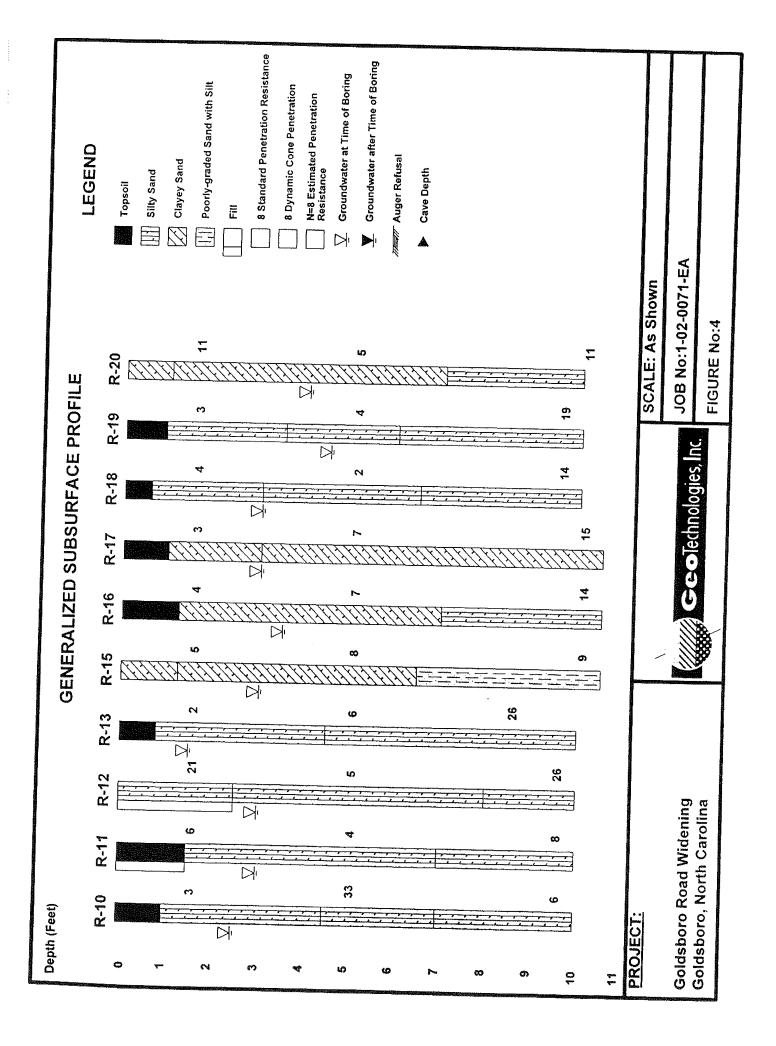


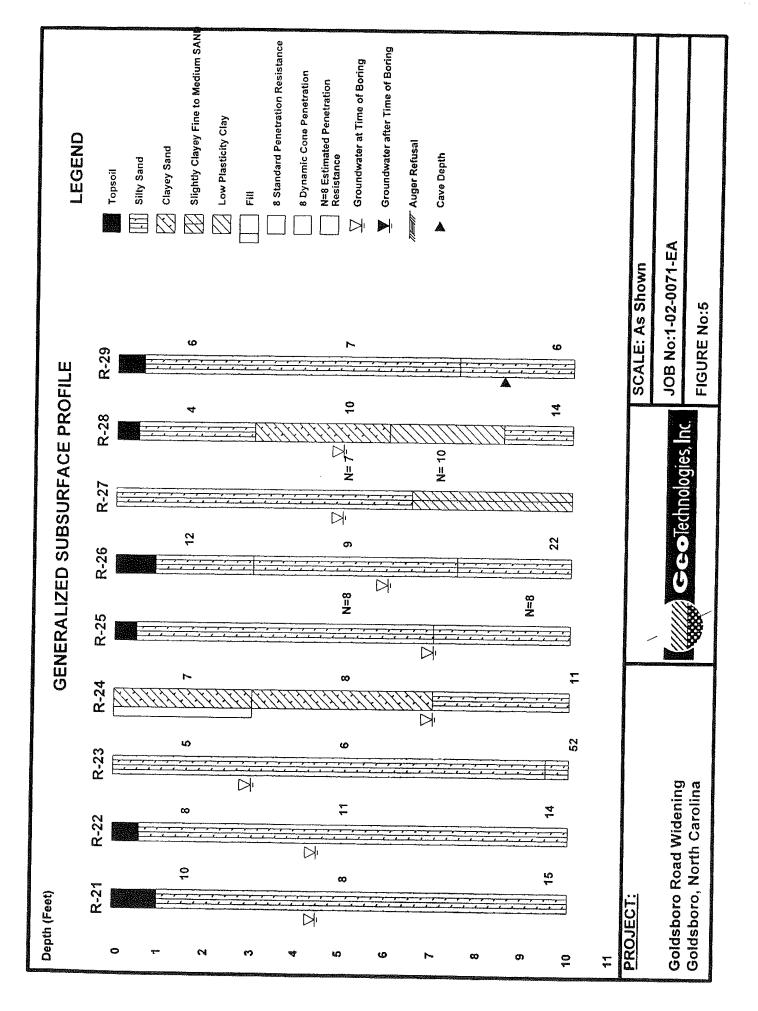
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TEST BORING RECORD

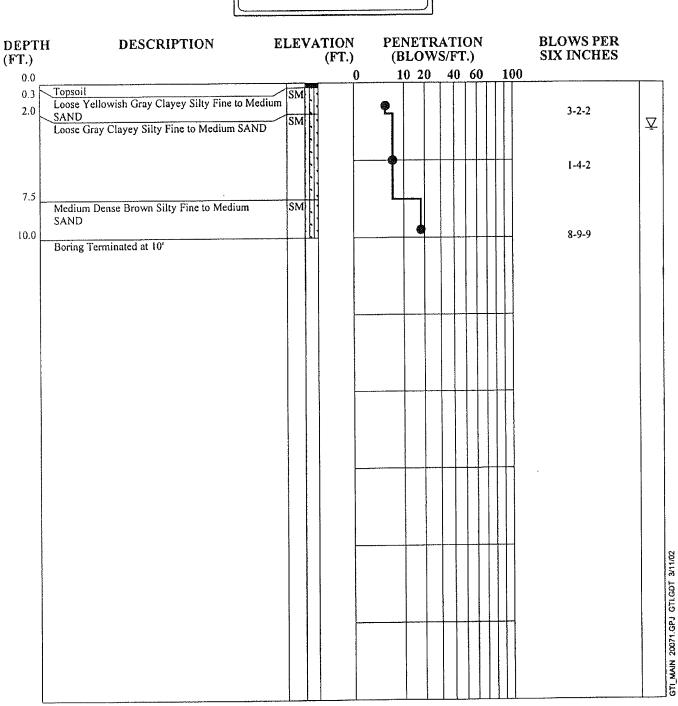
)EPTH FT.)	DESCRIPTION	ELEV	ATIO (FT	N .)	PENET (BLO)	'RAT WS/H	TON T.)		BLOWS PER SIX INCHES	
0.0				0	10 20		0 60	10		
2.0	Fill - Loose Yellowish Brown Silty Fine to Medium SAND Loose Black Silty Fine to Medium SAND	SM SM			•				5-4-4	
	Grayish Black Silty Fine to Medium SAND w/Occasional Clay	SM			∮				3-3-3	Ţ
7.5	N. 11									
10.0	Medium Dense Light Brown Slightly Silty Fine to Medium SAND	SM								
	Boring Terminated at 10'		-						5-5-7	
				þ			+			
				}				.		
										1
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Groundwater encountered at 5' at time of boring.

JOB NUMBER1-02-00BORING NUMBER0-4DATE2-8-02

1-02-0071-EA O- 4 2-8-02



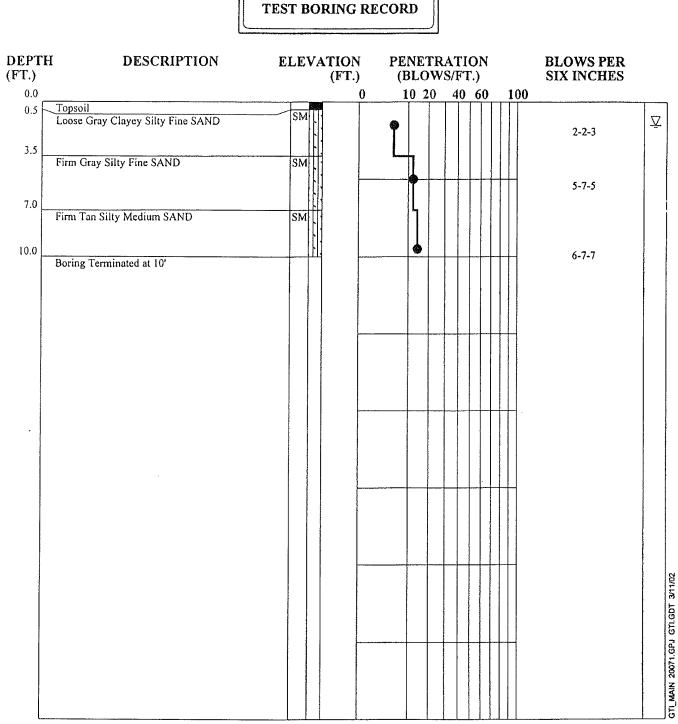


TEST BORING RECORD

Groundwater encountered at 3' at time of boring.

JOB NUMBER BORING NUMBER DATE 1-02-0071-EA O- 5 2-8-02

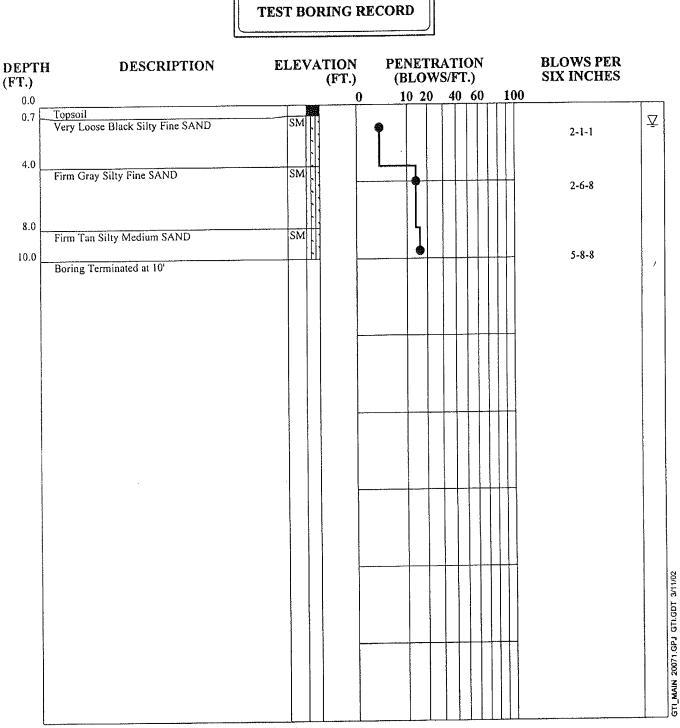




JOB NUMBER **BORING NUMBER** 0-6 DATE 2-11-02

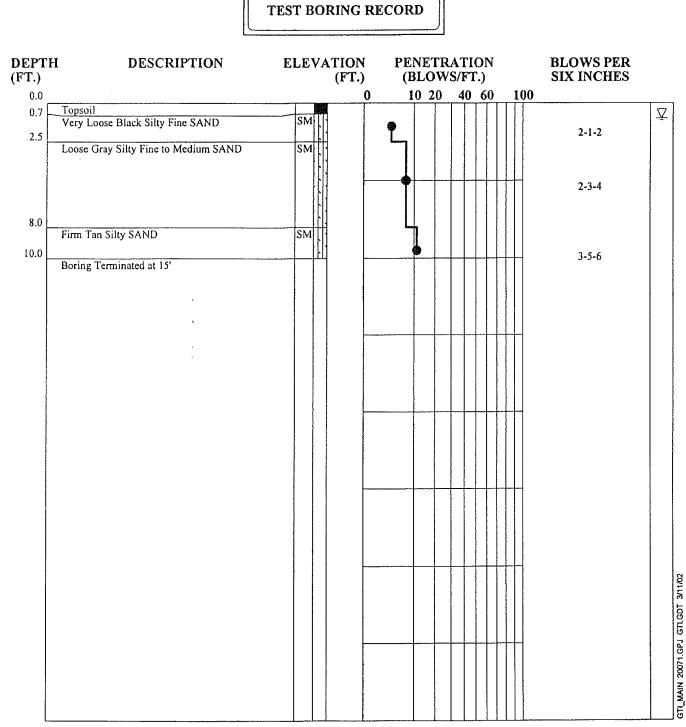
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JOB NUMBER BORING NUMBER DATE 1-02-0071-EA O- 7 2-11-02

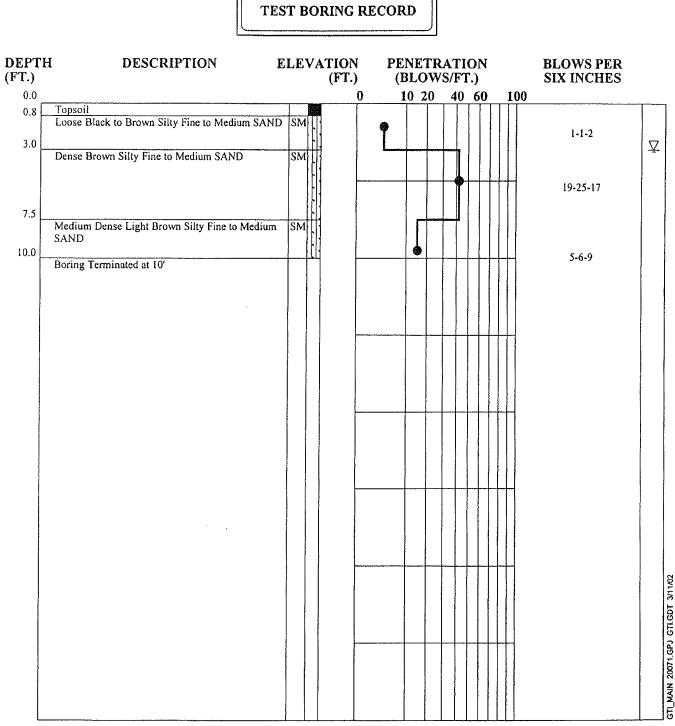




JOB NUMBER 1-BORING NUMBER R-DATE 2-

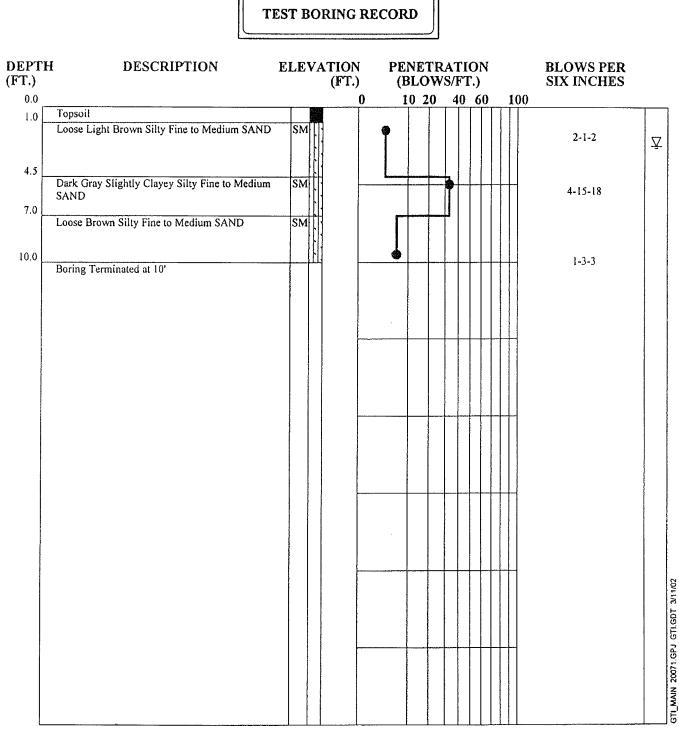
1-02-0071-EA R- 8 2-11-02





JOB NUMBER BORING NUMBER DATE 1-02-0071-EA R- 9 2-11-02

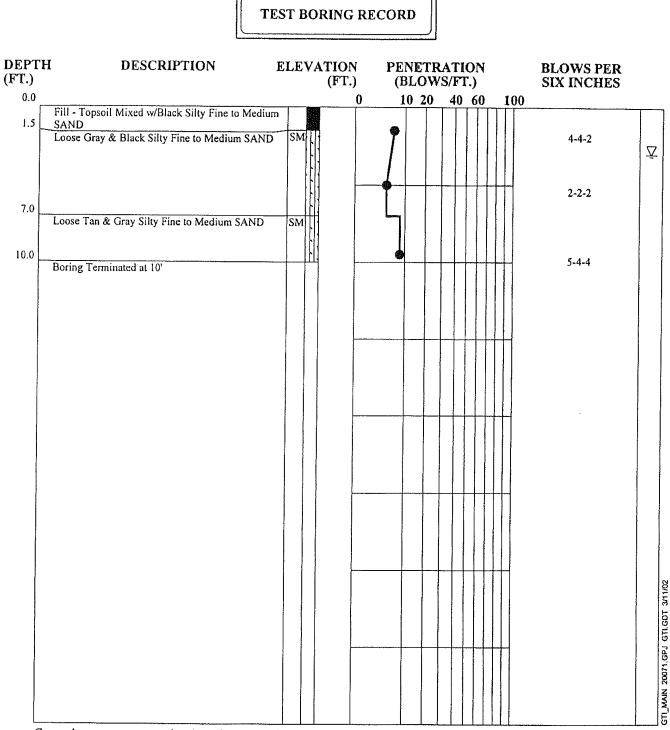




JOB NUMBER BORING NUMBER R-10 DATE 2-11-02

1-02-0071-EA

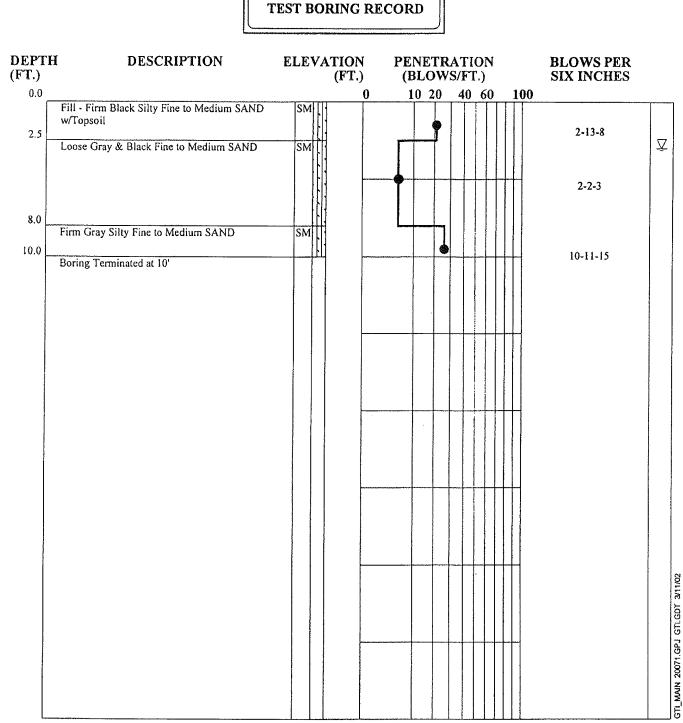




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1-02-0071-EA R-11 2-11-02

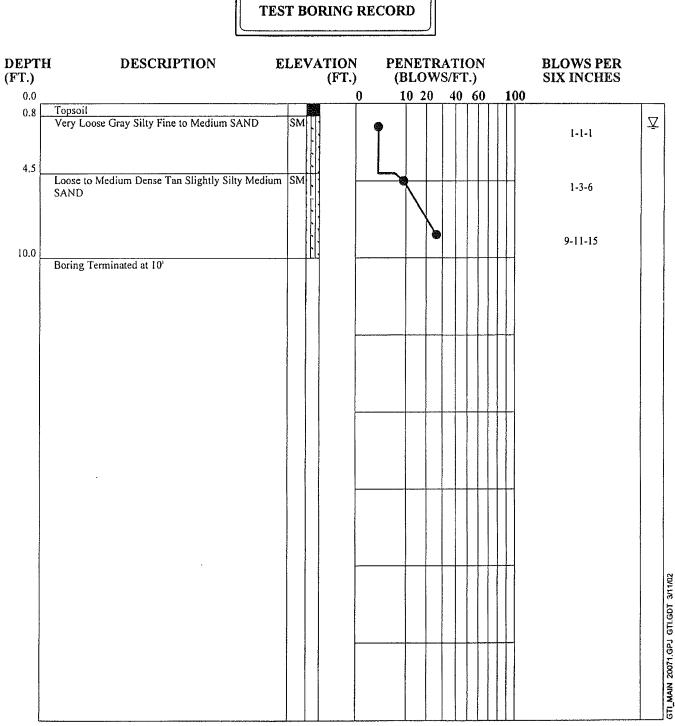




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1-02-0071-EA

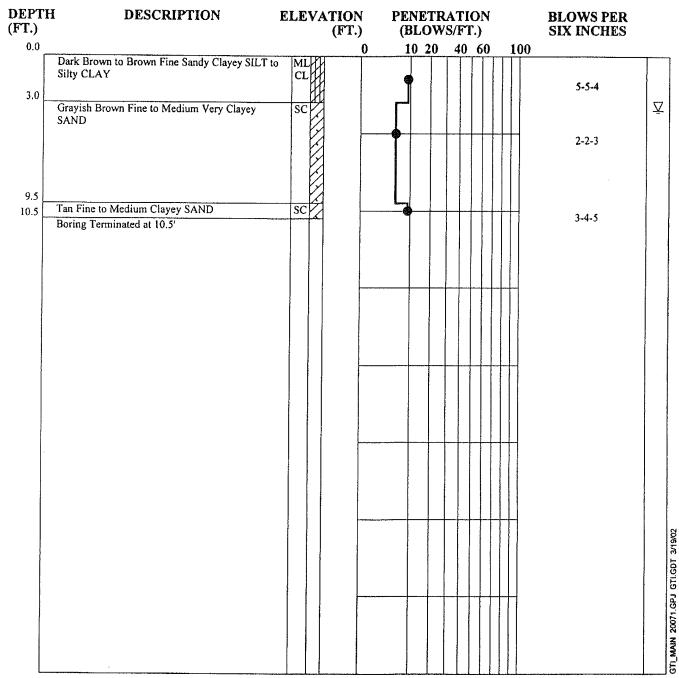




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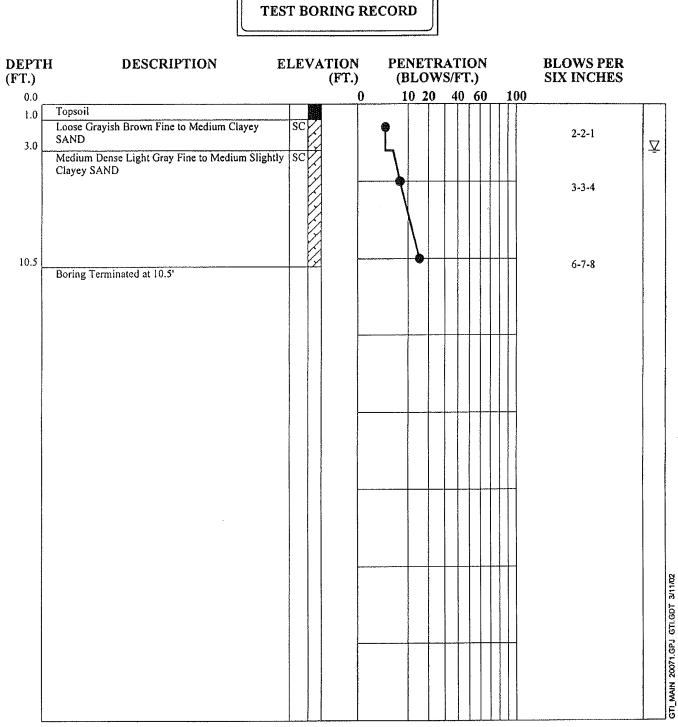




JOB NUMBER1-02-00BORING NUMBERR-14DATE2-8-02

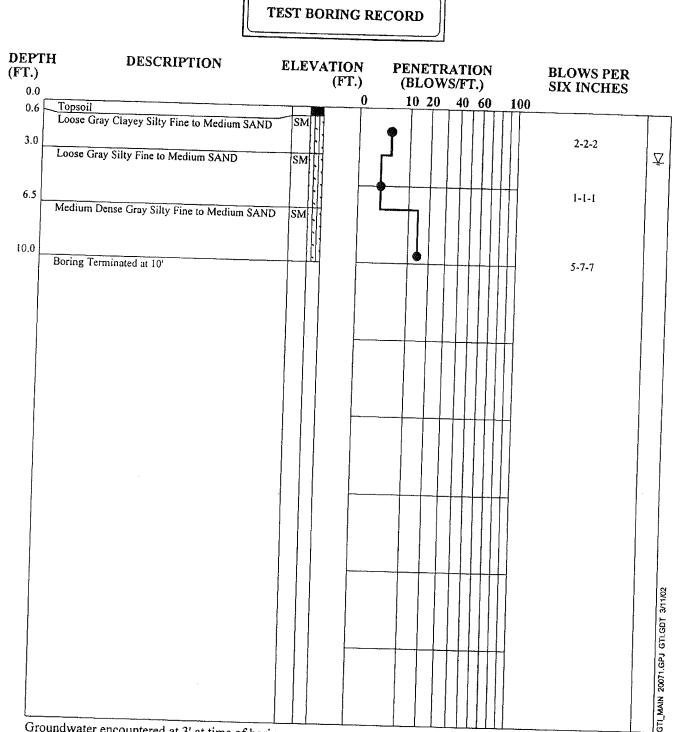
1-02-0071-EA R-14 2-8-02





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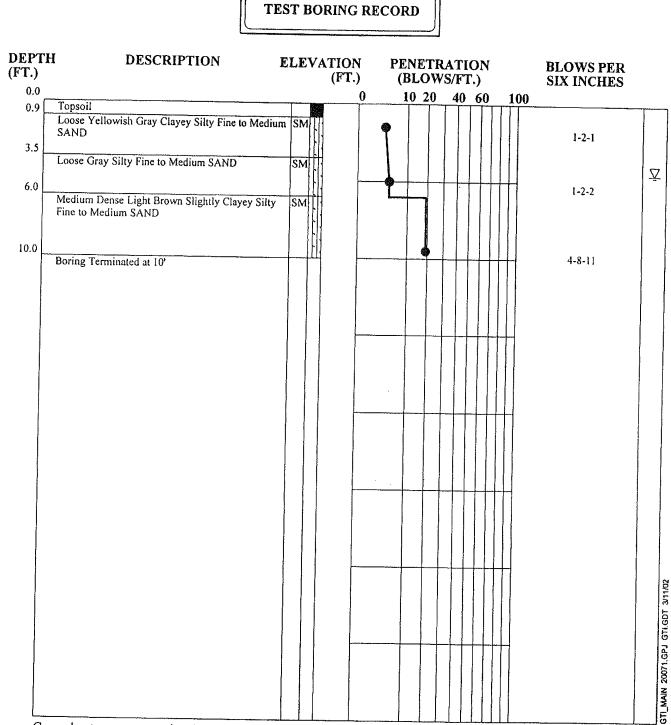




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1-02-0071-EA R-18 2-8-02

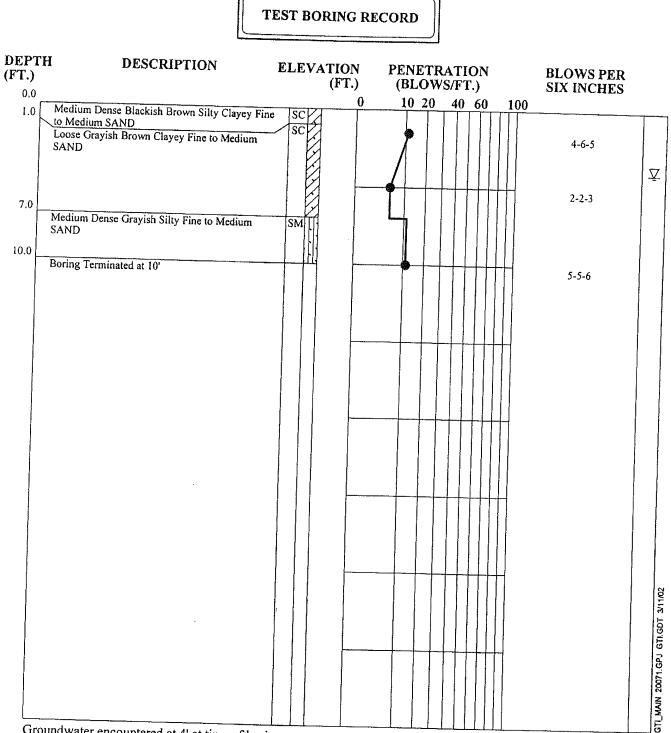




JOB NUMBER BORING NUMBER DATE

1-02-0071-EA R-19 2-8-02

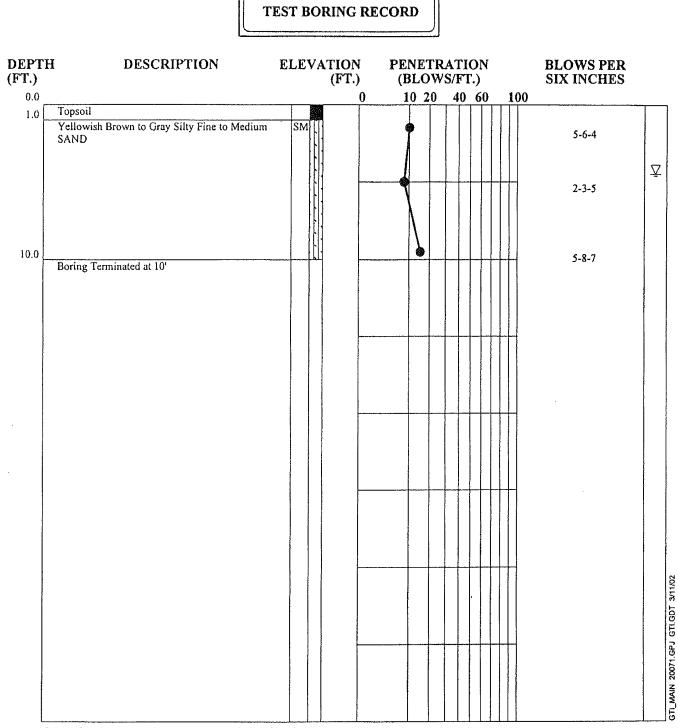




JOB NUMBER **BORING NUMBER** R-20 DATE 1-8-02

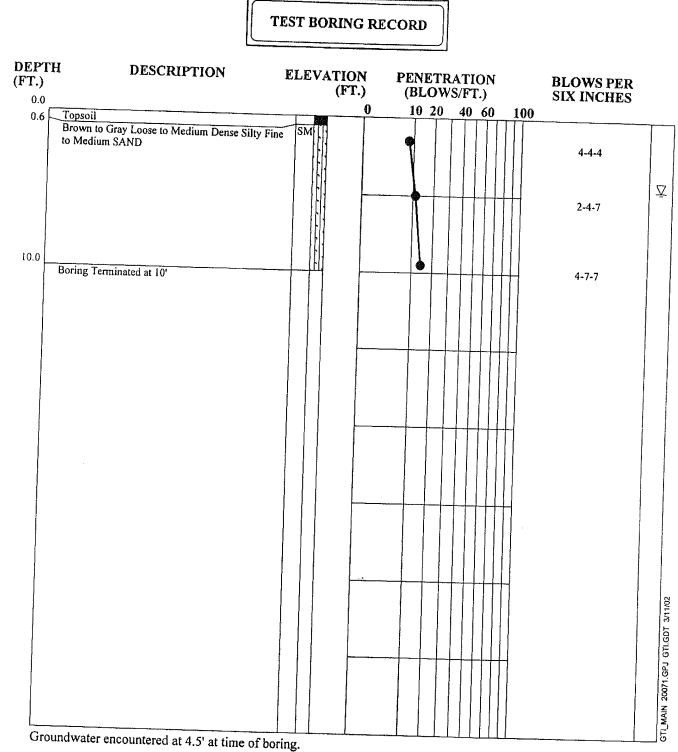
1-02-0071-EA





JOB NUMBER BORING NUMBER DATE 1-02-0071-EA R-21 2-8-02

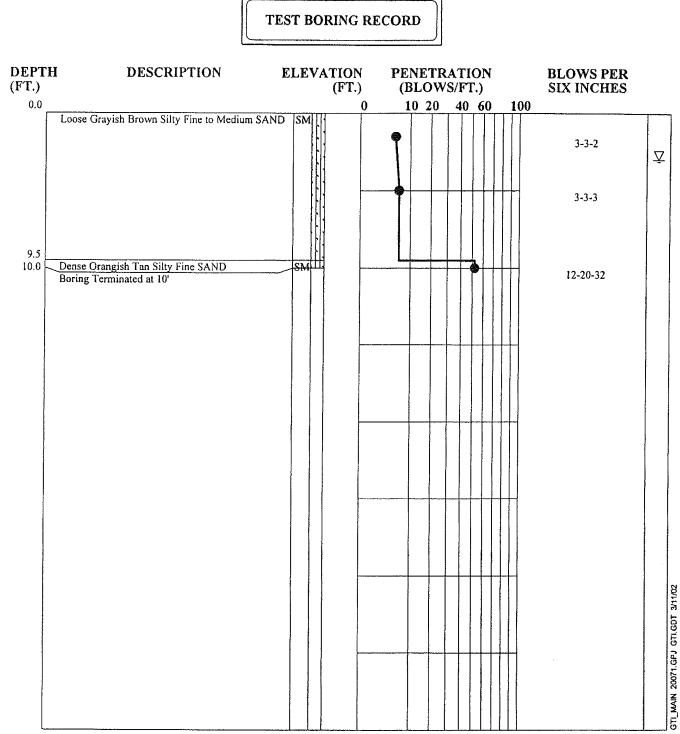




JOB NUMBER **BORING NUMBER** R-22 DATE 2-8-02

1-02-0071-EA





JOB NUMBER BORING NUMBER DATE 1-02-0071-EA R-23 1-8-02



TEST BORING RECORD

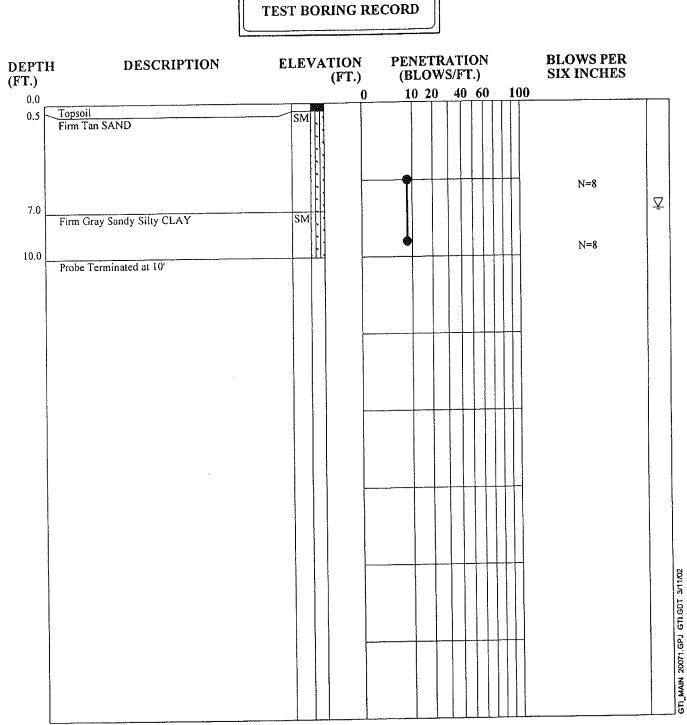
ЕРТН Г.)	I DESCRIPTION E	ELEVATION (FT.)]	PENETRATION (BLOWS/FT.)						BLOWS PER SIX INCHES		
0.0				(0	10	20	4() 6	0	10	00		
3.0 SA	l - Loose Brown Slightly Clayey Fine to Mediun ND					•	T						4-4-3	
Lo Me	ose Grayish Brown Slightly Clayey Fine to edium SAND	SC							_				3-4-4	
7.0	dium Dense Light Gray Silty Fine to Medium	SM				L								Σ
0.0	ND													
Bo	ring Terminated at 10'												4-6-5	
						_								
-										_				
		1												

Groundwater encountered at 7' at time of boring.

JOB NUMBER BORING NUMBER R-24 2-12-02

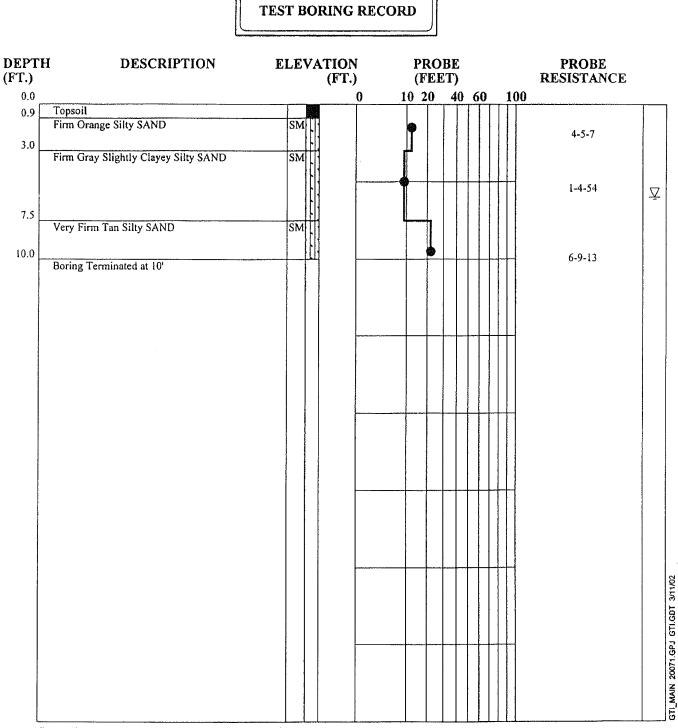
1-02-0071-EA





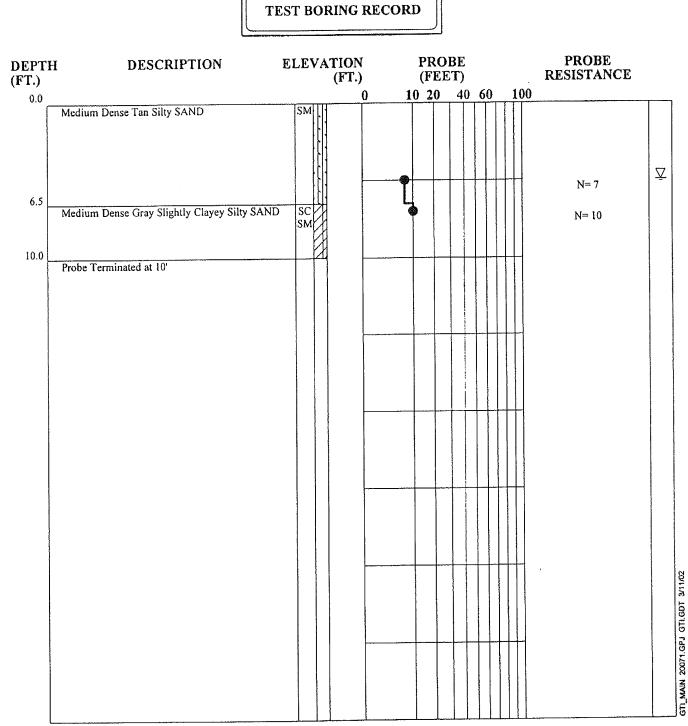
JOB NUMBER BORING NUMBER DATE 1-02-0071-EA R-25 2-12-02





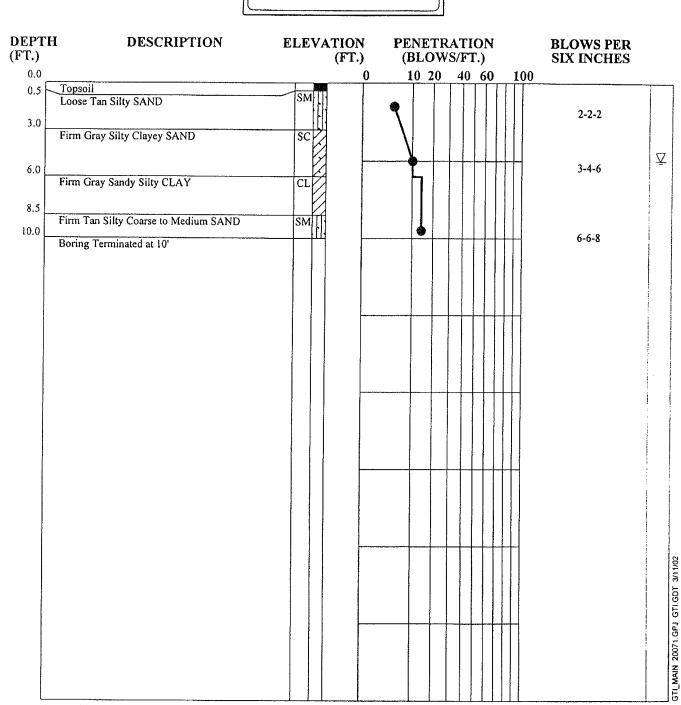
JOB NUMBER BORING NUMBER DATE 1-02-0071-EA R-26 2-12-02





JOB NUMBER BORING NUMBER DATE 1-02-0071-EA R-27 2-12-02





TEST BORING RECORD

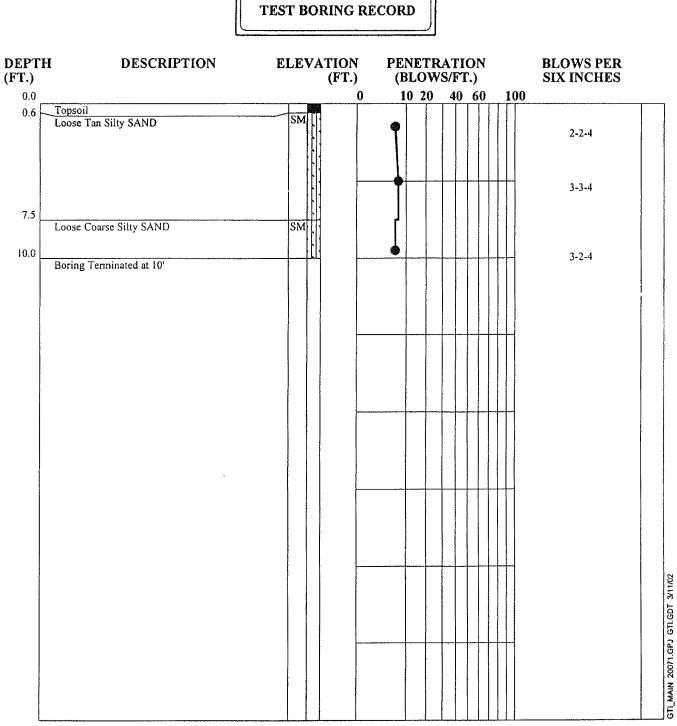
Groundwater encountered at 5' at time of boring.

JOB NUMBER BORING NUMBER R-28 DATE 2-12-02

PAGE 1 OF 1

1-02-0071-EA



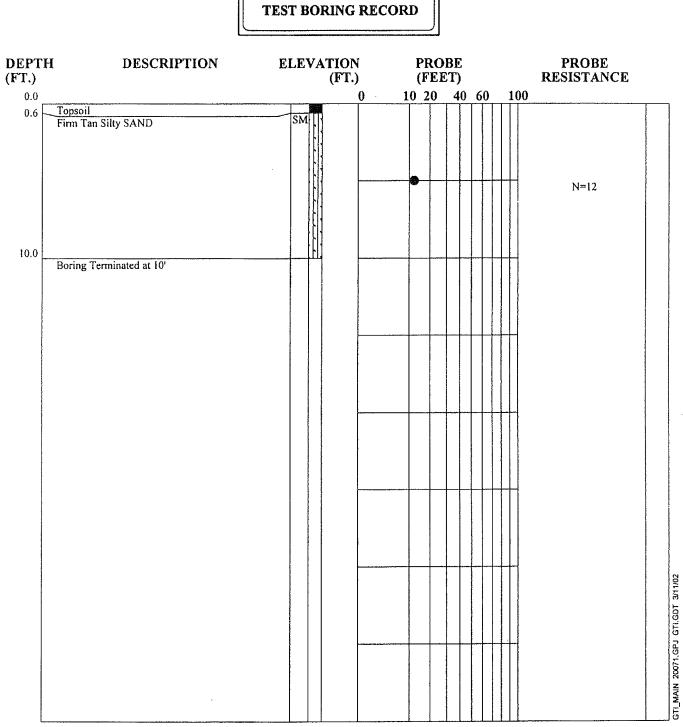


Boring Caved at 8.5' and Dry at at Time of Boring.

JOB NUMBER BORING NUMBER DATE

1-02-0071-EA R-29 2-12-02

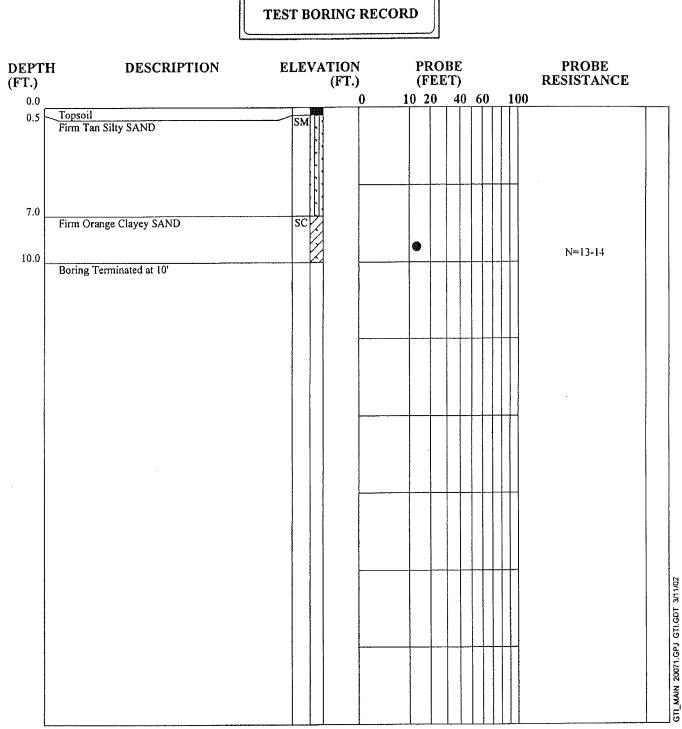




JOB NUMBER BORING NUMBER DATE

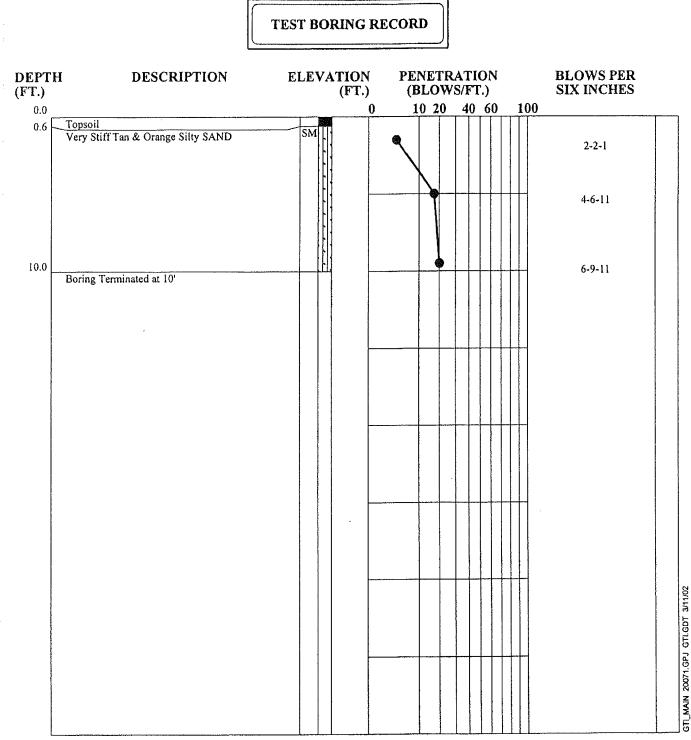
1-02-0071-EA B-30 2-12-02





JOB NUMBER BORING NUMBER DATE 1-02-0071-EA B-31 2-12-02

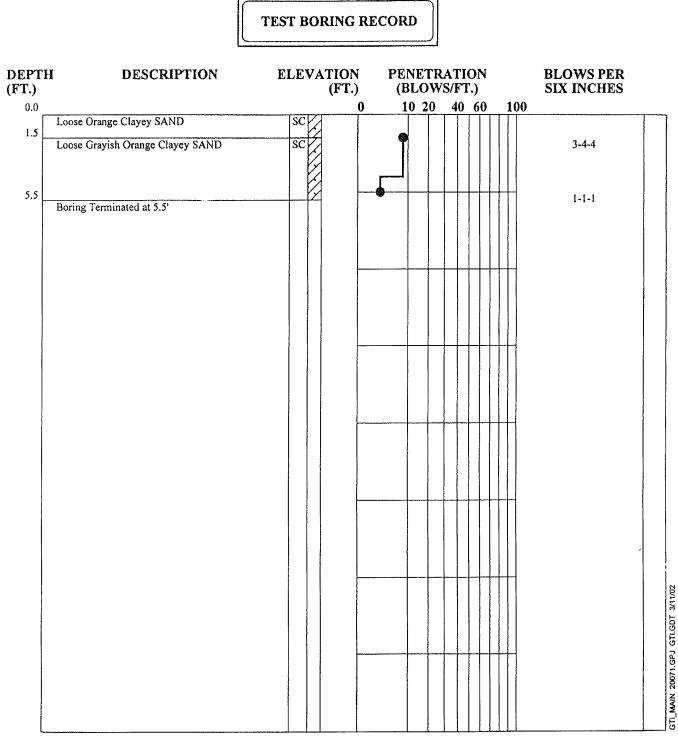




JOB NUMBER **BORING NUMBER** B-32 2-12-02 DATE

1-02-0071-EA

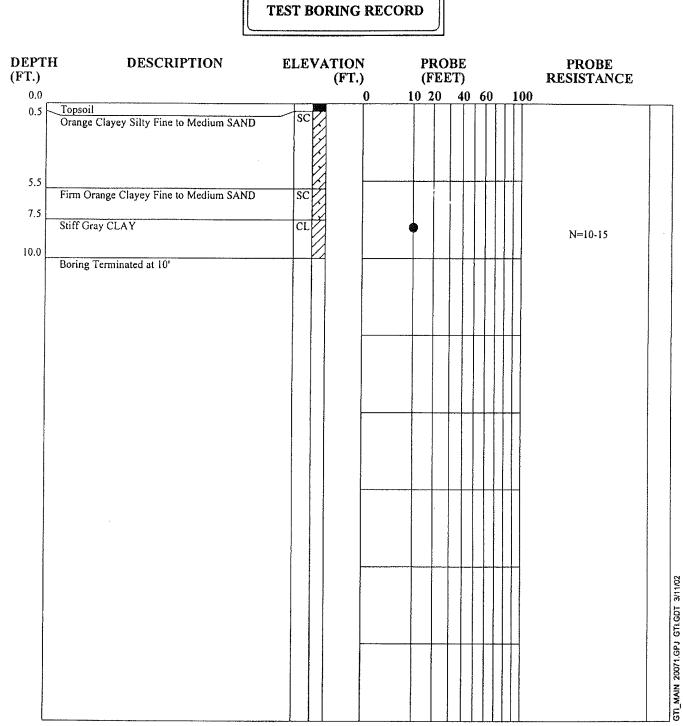




Groundwater not encountered at time of boring. Possible sewer line at 5.5'.

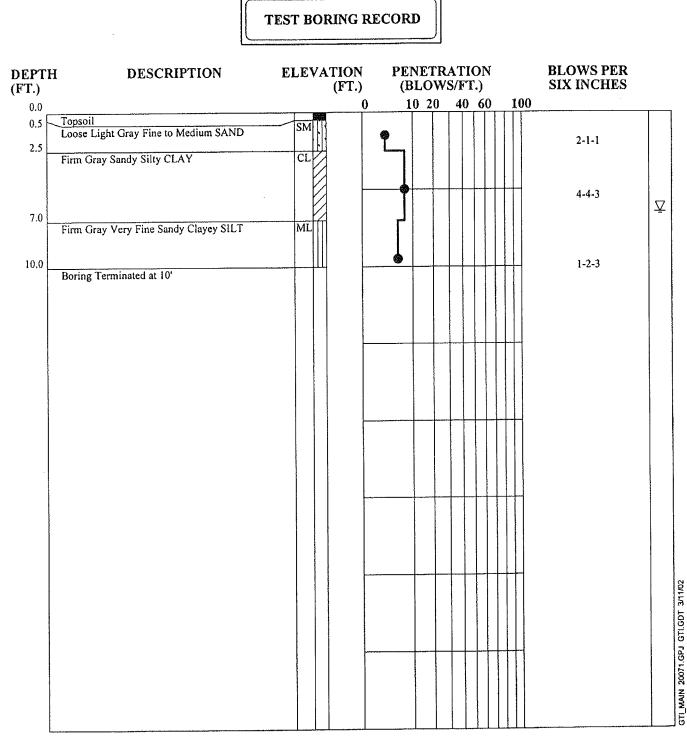
JOB NUMBER BORING NUMBER DATE 1-02-0071-EA B-34 2-12-02





JOB NUMBER BORING NUMBER DATE 1-02-0071-EA B-35 2-12-02

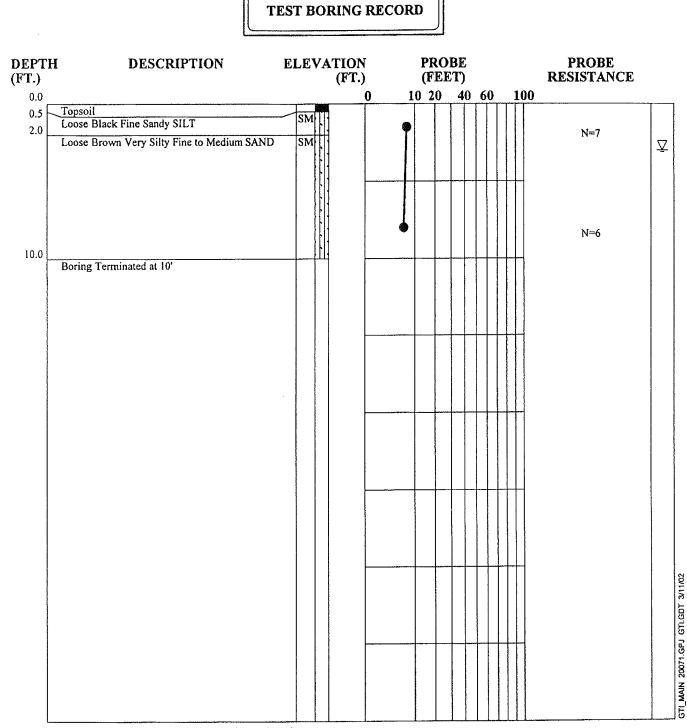




Groundwater encountered at 6.5'

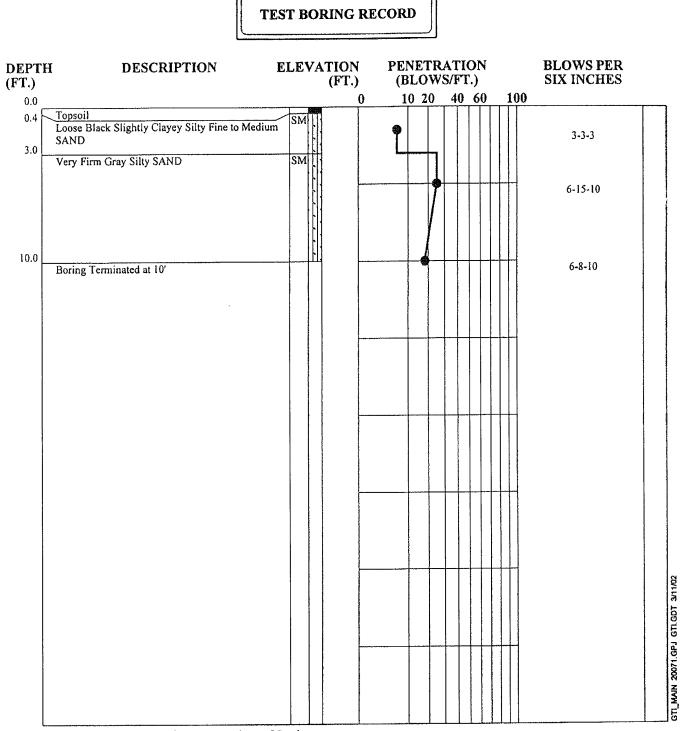
JOB NUMBER BORING NUMBER DATE 1-02-0071-EA B-36 2-12-02





JOB NUMBER BORING NUMBER DATE 1-02-0071-EA B-39 2-12-02

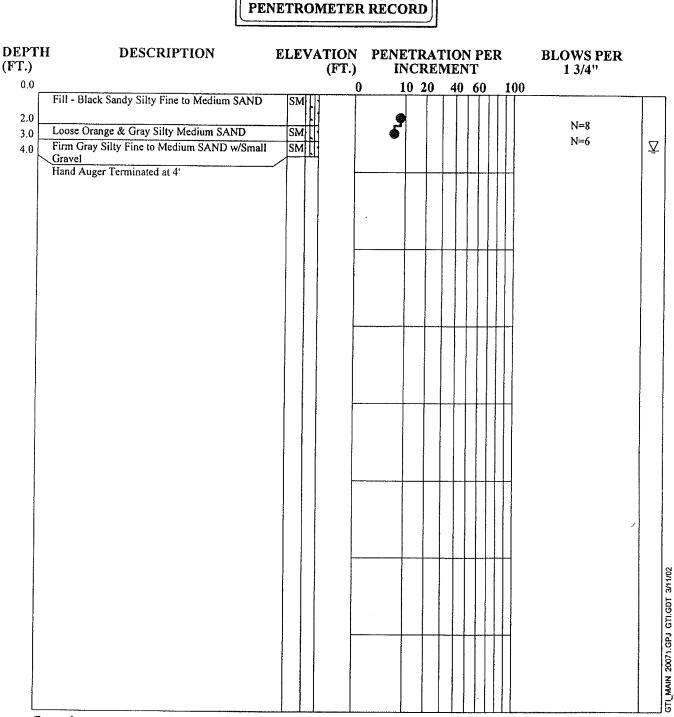




Boring Caved at 3.5' and Dry at at Time of Boring.

JOB NUMBER BORING NUMBER DATE 1-02-0071-EA B-41 2-12-02





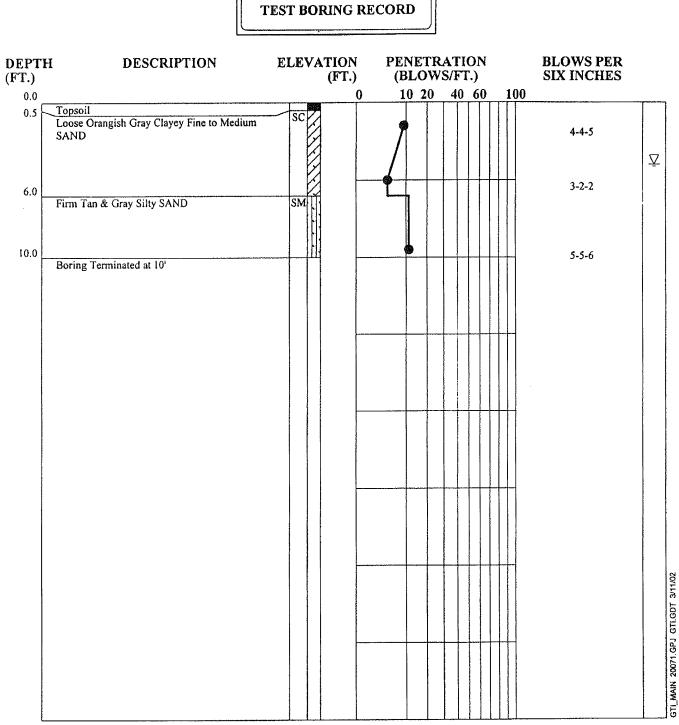
DYNAMIC HAND CONE

Groundwater encountered at 3.5' at time of boring.

JOB NUMBER1-02-0BORING NUMBERB-42DATE2-12-0

1-02-0071-EA B-42 2-12-02



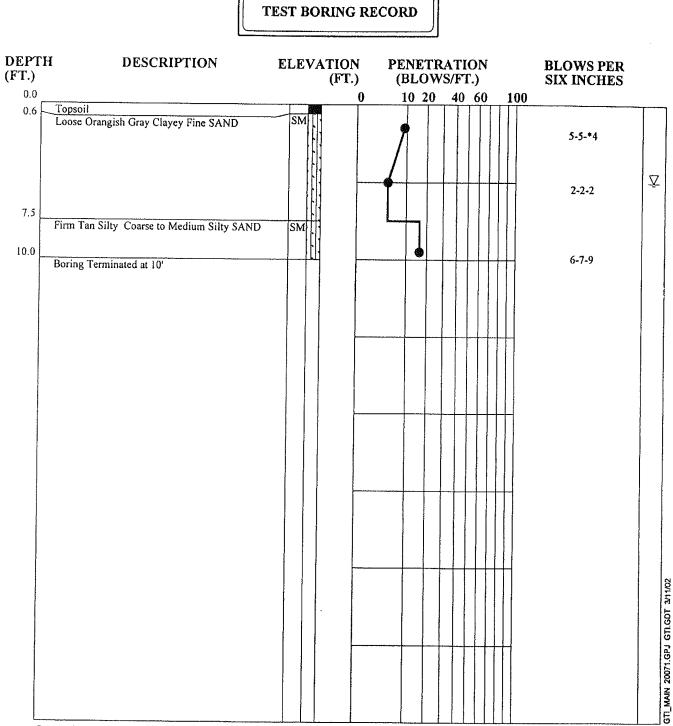


Groundwater encountered at 4' at time of boring

JOB NUMBER BORING NUMBER DATE 1-02-0071-EA B-44 2-13-02



PAGE 1 OF 1



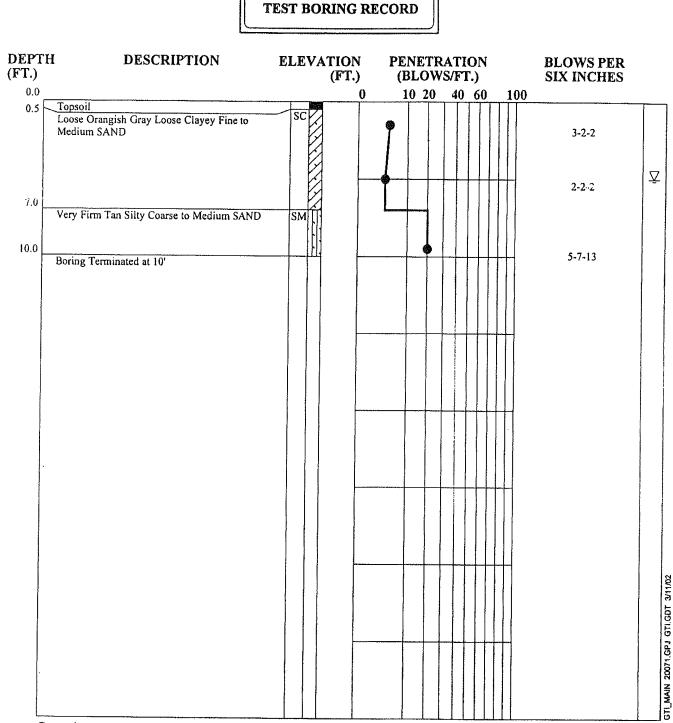
Groundwater encountered at 5' at time of boring

JOB NUMBER **BORING NUMBER** B-45 DATE 2-13-02

1-02-0071-EA



PAGE 1 OF 1

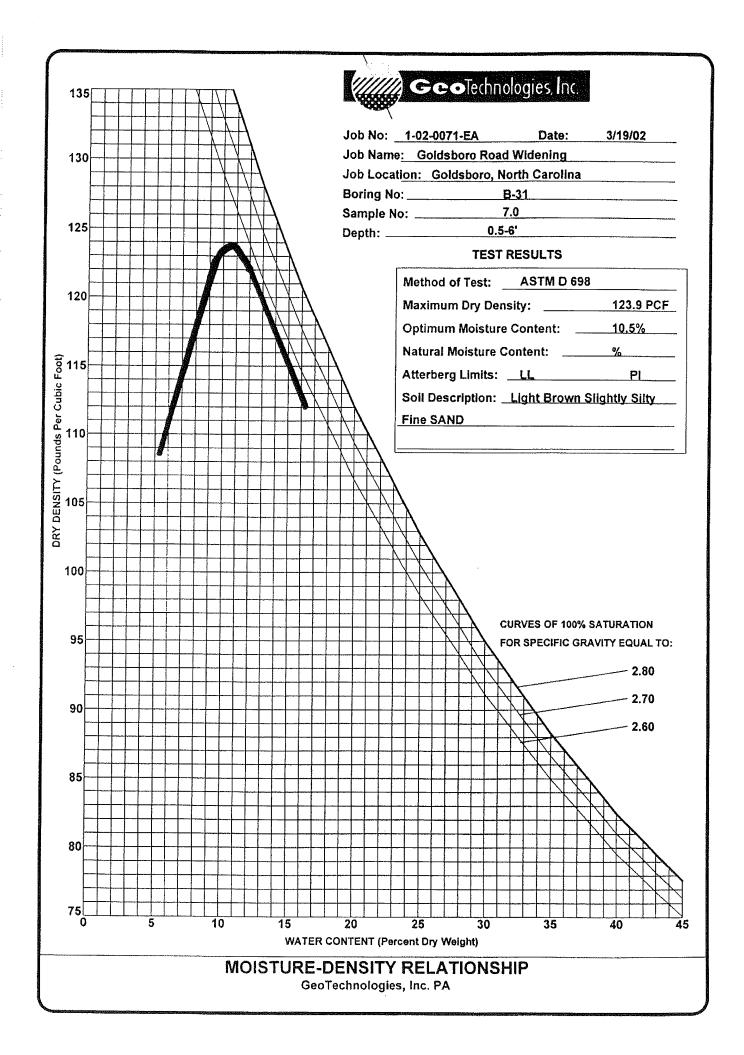


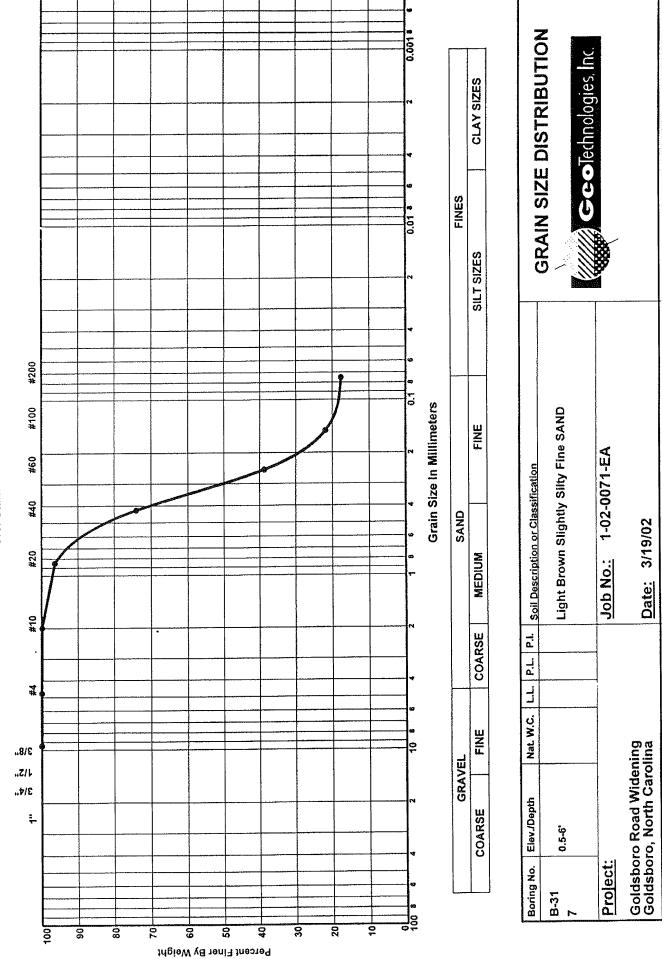
Groundwater encountered at 5' at time of boring

JOB NUMBER BORING NUMBER DATE 1-02-0071-EA B-46 2-13-02



PAGE 1 OF 1



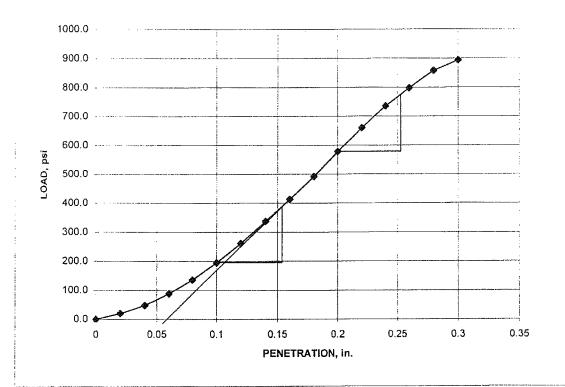


CBR DATA SHEET

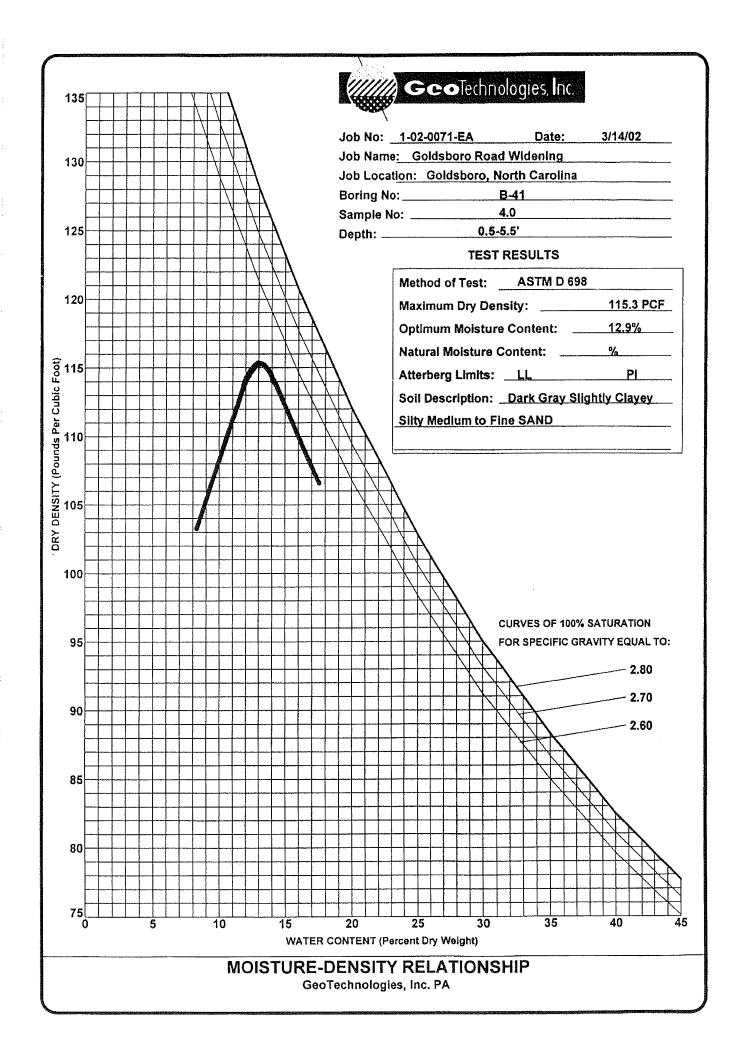
JOB #:	1-02-0071-EA		JOB NAME:	Goldsboro R	d. Widening	
DATE:	2/21/02		SAMPLE I.D.	B-31	DEPTH:	0.5-6.0'
NOTES:	PROCTOR DAT/ Opt. Moisture =	A: 10.5%	Max. Dry Density =	TEST 123.9	PROCEDURE: PCF	ASTM D 698

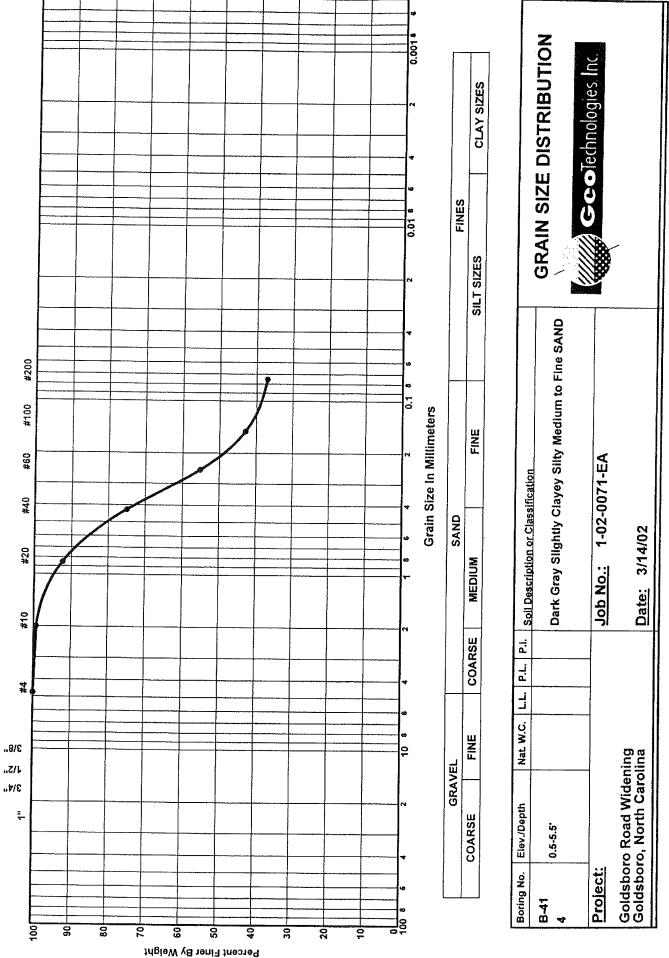
SOIL DESCRIPTION: Light Brown Silty Fine SAND

CBR SPECIMEN DATA		Swell Data	1
MOISTURE CONTENT	10.5%	Initial Reading	0.147
WET DENSITY	134.9 lbs./cu.ft.	Final Reading	0.152
DRY DENSITY	122.1 lbs./cu.ft.	Mold Height	4.585
% COMPACTION	98.5 %	% Swell	0.1
PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min
PROVING RING CONSTANT	1.80	SURCHARGE USED	10 lbs.



CBR @ 0.1"	Corrected	38.0
CBR @ 0.2"	Corrected	51.0
% SWELL		0.1

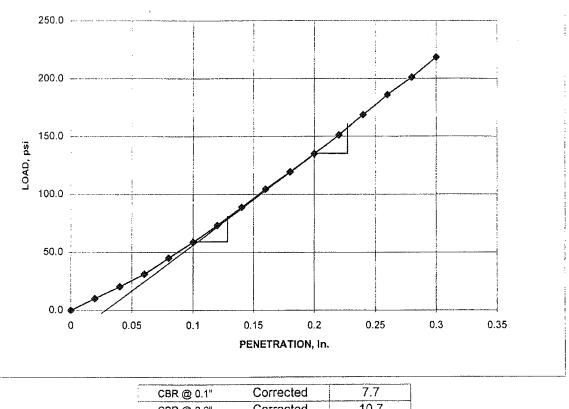




GeoTech	nologies, Inc.	CBR DATA SHEET			
JOB #:	1-02-0071-EA	JOB NAME:	Goldsboro Rd. Widening		
DATE:	2/21/02	SAMPLE I.D.	В-41 DEPTH: 0.5-5.5'		
NOTES:	PROCTOR DATA: Opt. Moisture = 12.9%	Max, Dry Density =	TEST PROCEDURE: ASTM D 698 115.3 PCF		
	SOIL DESCRIPTION:	Dark Gray Slight	ly Clayey Silty Medium-Fine SAND		

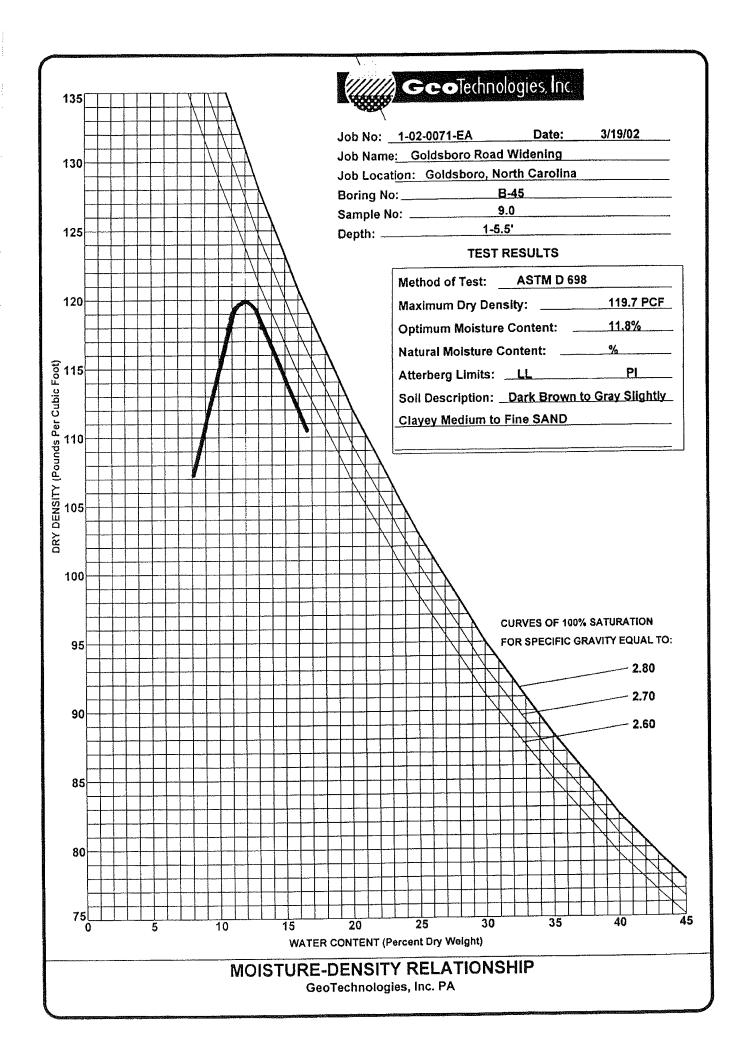
CBR SPECIMEN DATA		Swell I	Data
MOISTURE CONTENT	12.9%	Initial Reading	0.062
WET DENSITY	130.3 lbs./cu.ft.	Final Reading	0.076
DRY DENSITY	115.4 lbs./cu.ft.	Mold Height	4.593
% COMPACTION	100.1 %	% Swell	0.3

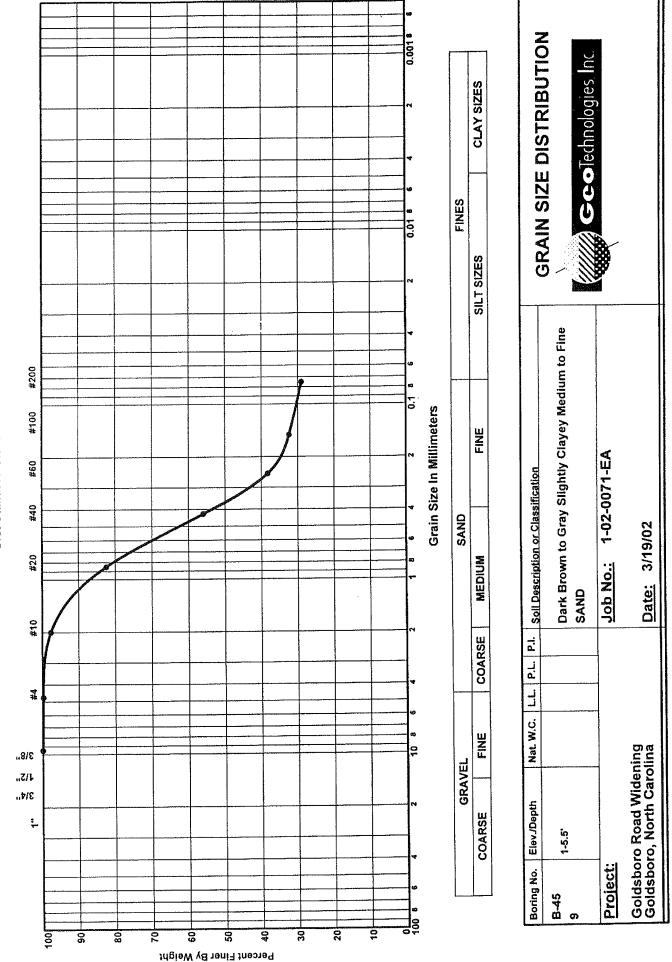
PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min.
PROVING RING CONSTANT	1.80	SURCHARGE USED	10 lbs.



CBR @ 0.1"	Corrected	1.1
CBR @ 0.2"	Corrected	10.7
% SWELL		0.3

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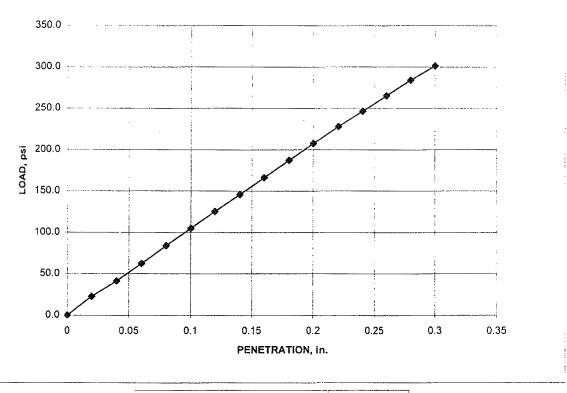
CBR DATA SHEET

JOB #:	1-02-0071-EA		JOB NAME:	Gold	dsboro R	d. Widening	
DATE:	2/21/02		SAMPLE I.D.		B-45	DEPTH:	1.0-5.5'
NOTES:	PROCTOR DATA	: 11.8%	Max. Dry Density =		TEST F 119.7	PROCEDURE: PCF	ASTM D 698

SOIL DESCRIPTION: Dark Brown Grey Clayey Medium-Fine SAND

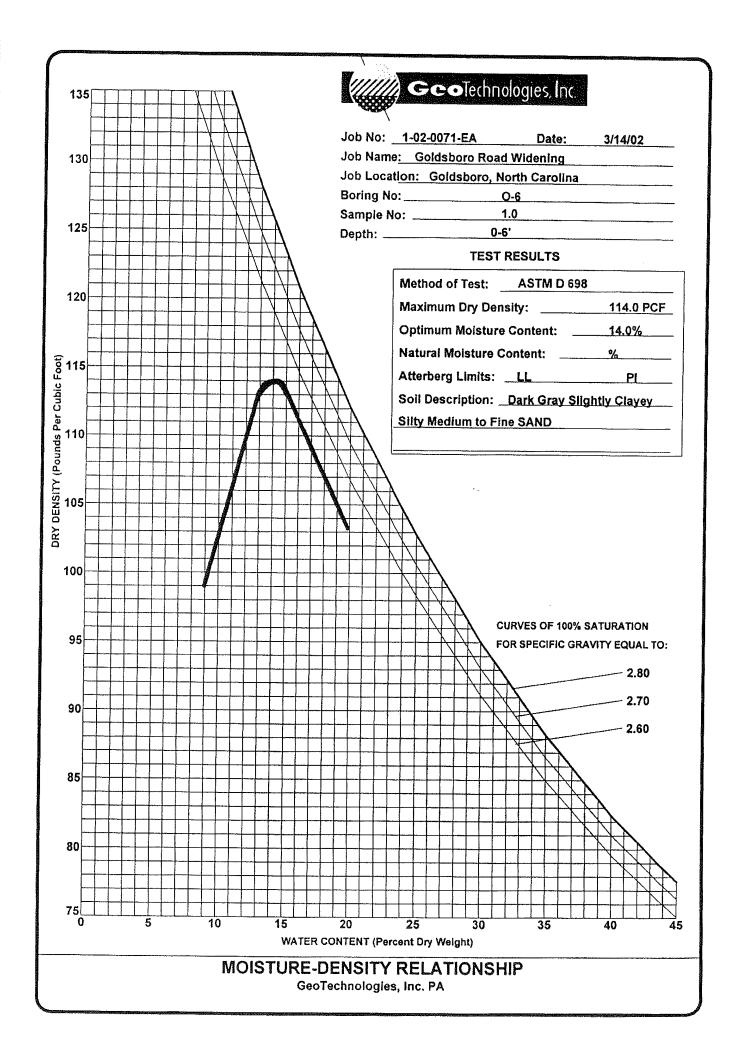
CBR SPECIMEN DATA		Swell I	Data
MOISTURE CONTENT	11.8%	Initial Reading	0.145
WET DENSITY	133.6 lbs./cu.ft.	Final Reading	0.150
DRY DENSITY	119.5 lbs./cu.ft.	Mold Height	4.589
% COMPACTION	99.8 %	% Swell	0.1

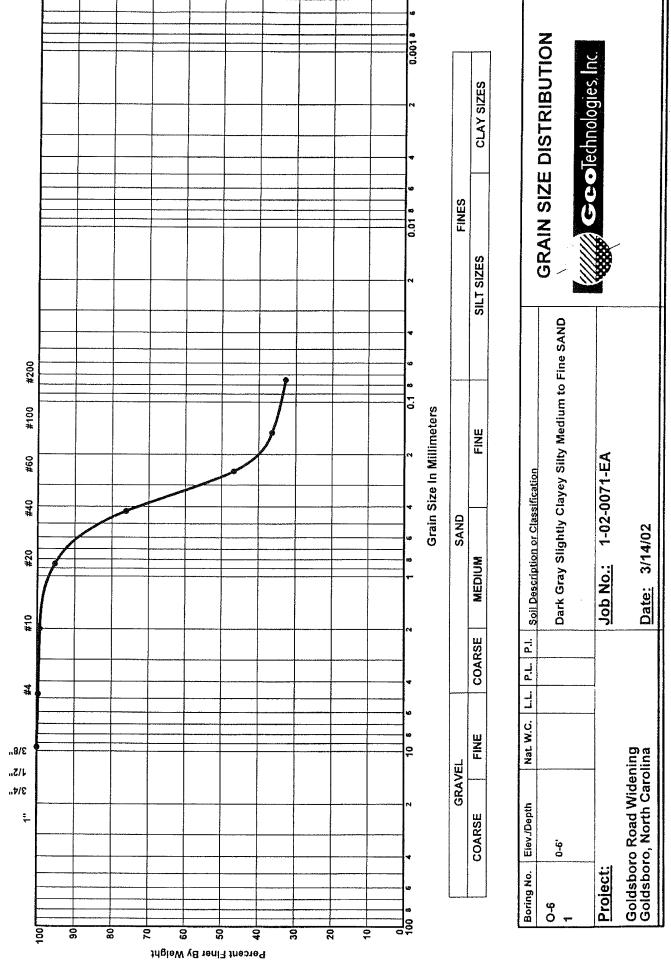
PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min.
PROVING RING CONSTANT	1.80	SURCHARGE USED	10 lbs.



13.8
0.1

:



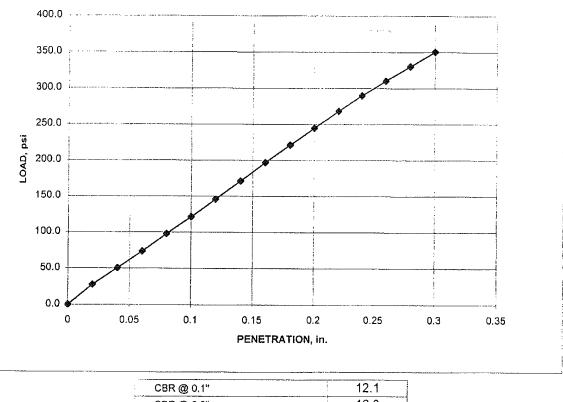


GeoTechnologies, Inc. **CBR DATA SHEET** JOB #: 1-02-0071-EA JOB NAME: Goldsboro Rd. Widening DATE: 2/21/02 SAMPLE I.D. O-6 DEPTH: **PROCTOR DATA:** NOTES: TEST PROCEDURE: ASTM D 698 Opt. Moisture = 14.0% Max. Dry Density = 114.0 PCF SOIL DESCRIPTION: Dark Gray Slightly Clayey Silty Medium-Fine SAND **CBR SPECIMEN DATA** Swell Data MOISTURE CONTENT 14.0% Initial Reading 0.178 WET DENSITY 129.0 lbs./cu.ft. **Final Reading** 0.183 DRY DENSITY 113.2 lbs./cu.ft. Mold Height

99.3 %

PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min.
PROVING RING CONSTANT	1.80	SURCHARGE USED	10 lbs.

% Swell

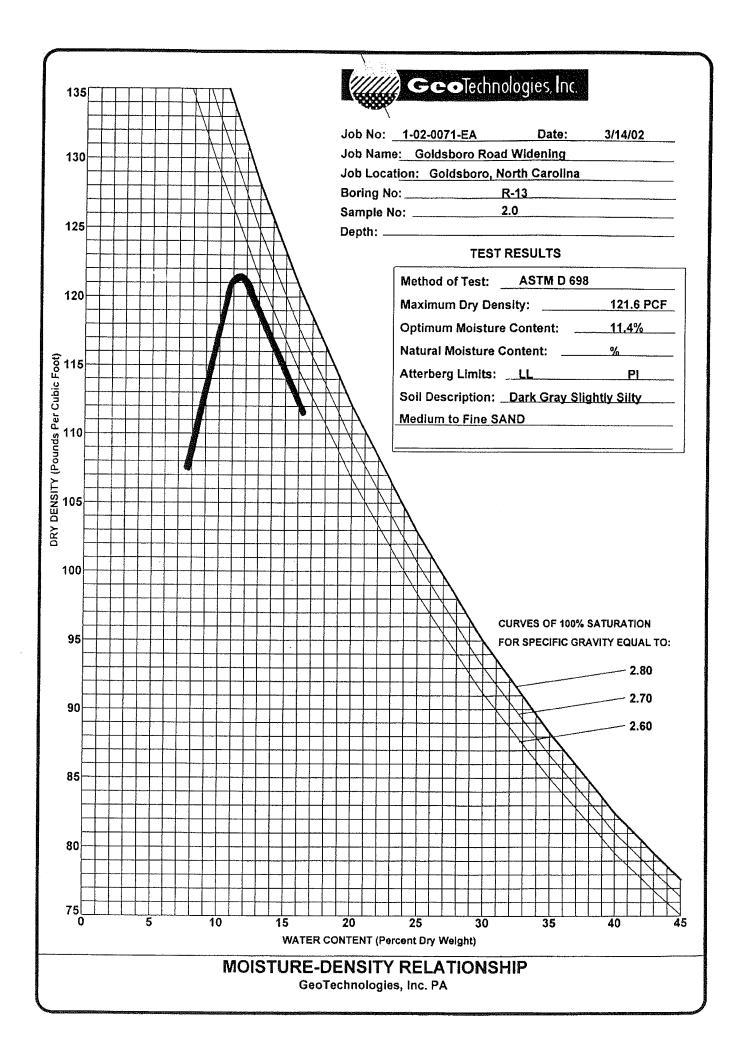


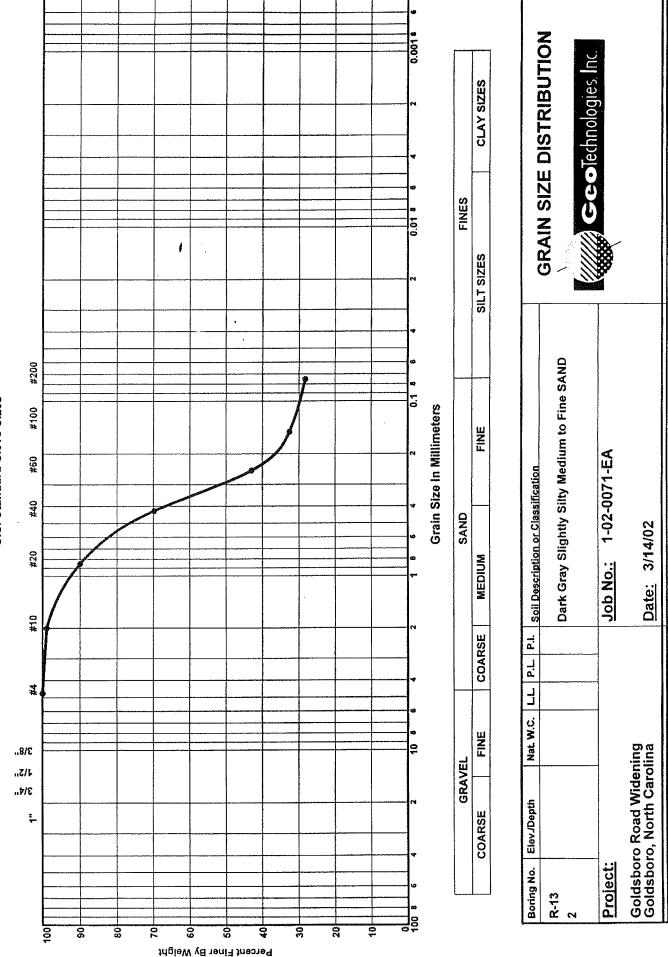
CBR @ 0.1"	12.1
CBR @ 0.2"	16.3
% SWELL	0.1

% COMPACTION

4.587

0.1





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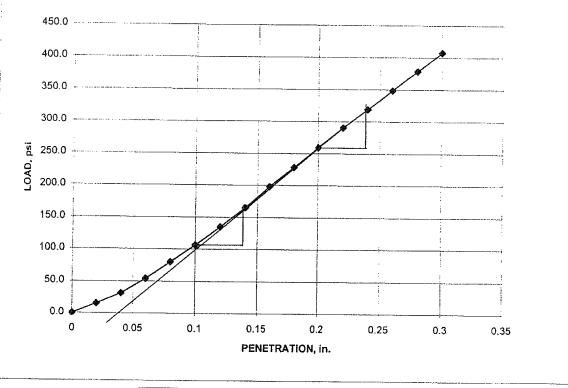
CBR DATA SHEET

SURCHARGE USED

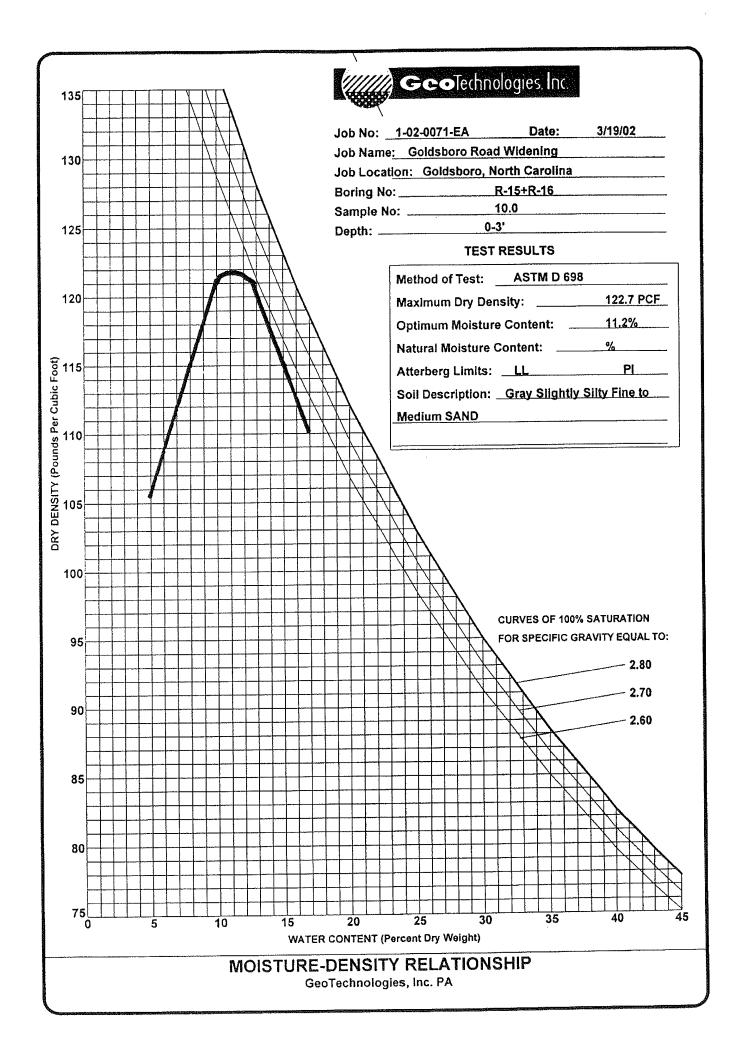
10 lbs.

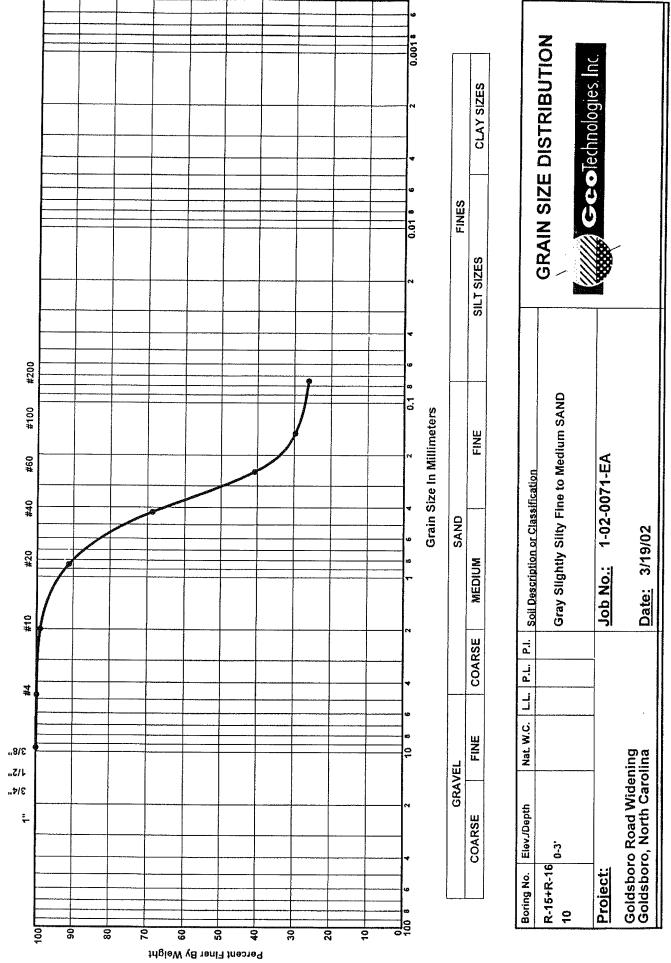
	CBR SPECIMEN DATA	Г	Swall Data	
	SOIL DESCRIPTION:	Dark Gray Silty M	ledium-Fine SAND	
NOTES:	PROCTOR DATA: Opt. Moisture = 11.4%	Max. Dry Density =	TEST PROCEDURE: 121.6 PCF	ASTM D 698
DATE:	2/21/02	SAMPLE I.D.	R-13 DEPTH:	
JOB #:	1-02-0071-EA	JOB NAME:	Goldsboro Rd. Widening	

CBR SPECIMEN DATA		Swell Data	3
MOISTURE CONTENT	11.4%	Initial Reading	0.205
WET DENSITY	136.1 lbs./cu.ft.	Final Reading	0.206
DRY DENSITY	122.2 lbs./cu.ft.	Mold Height	4.587
% COMPACTION	100.5 %	% Swell	0.0
PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min.
PROVING RING CONSTANT	1.80	SURCHARGE USED	10 lbs



CBR @ 0.1"	16.5
CBR @ 0.2"	21.3
% SWELL	0.0





CBR DATA SHEET

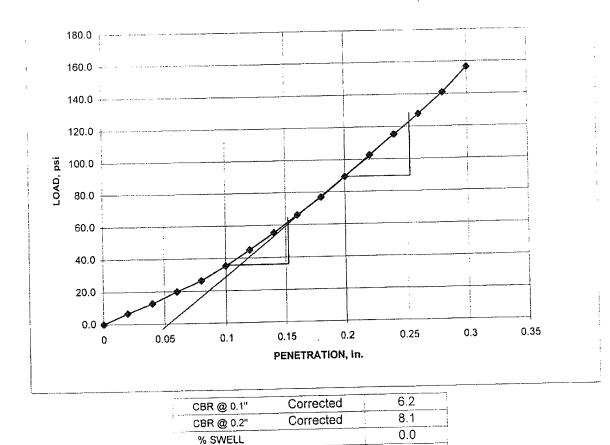
JOB #:	1-02-0071-EA	JOB NAME:	Goldsboro Rd. Widening	
DATE:	2/21/02	SAMPLE I.D.	R-15+R16 DEPTH:	0.0-3.0'
NOTES:	PROCTOR DATA: Opt. Moisture = 11.2%	Max. Dry Density =	TEST PROCEDURE: 122.7 PCF	ASTM D 698

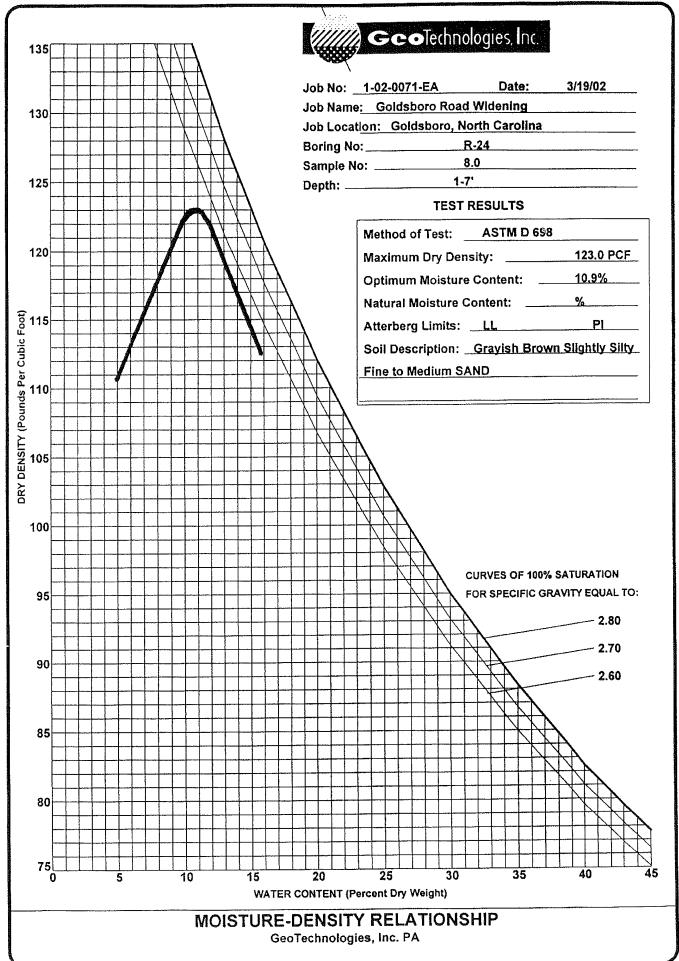
SOIL DESCRIPTION:

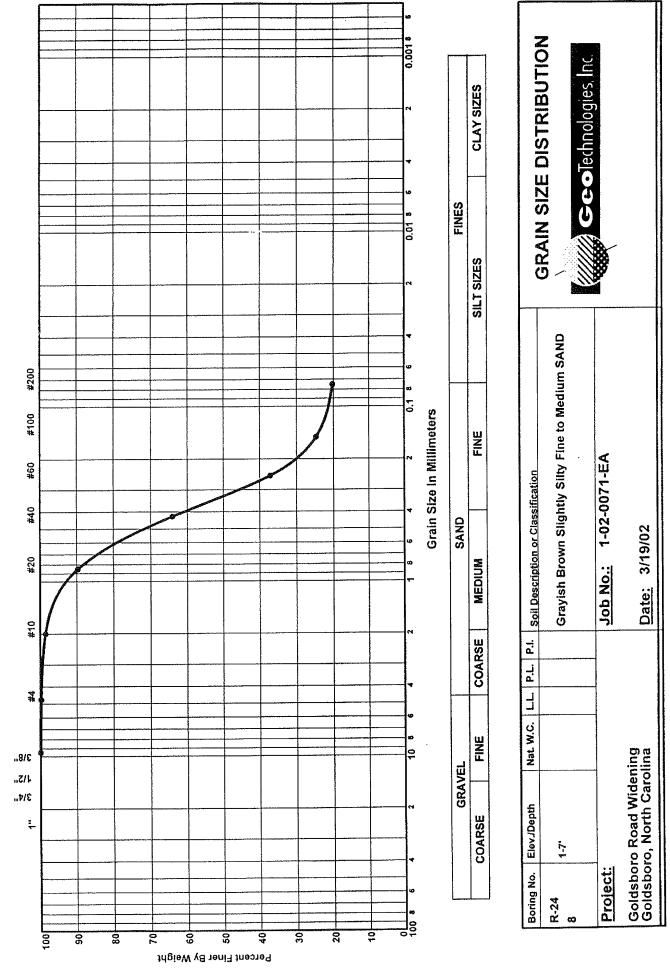
Grey Silty Medium-Fine Sand

	Swell	Data
11.2%	Initial Reading	0.212
		0.214
		4.586
	% Swell	0.0
	11.2% 136.0 lbs./cu.ft. 122.3 lbs./cu.ft. 99.7 %	11.2% Initial Reading 136.0 lbs./cu.ft. Final Reading 122.3 lbs./cu.ft. Mold Height

PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min.
	(00	SURCHARGE USED	10 lbs.
PROVING RING CONSTANT	1.80	SUKCHARGE USED	10.000







PROVING RING CONSTANT

CBR DATA SHEET

SURCHARGE USED

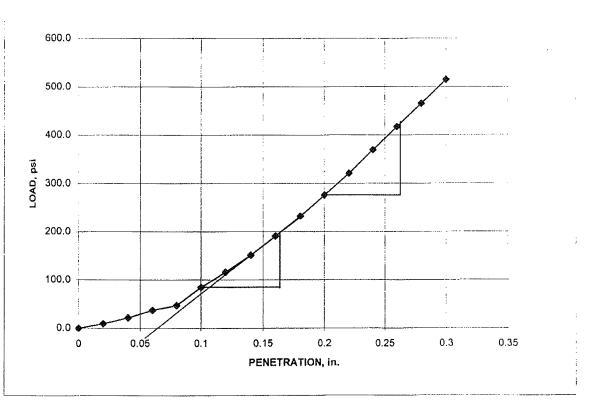
10 lbs.

JOB #:	1-02-0071-EA		JOB NAME:	Goldsboro F	Rd. Widening	
DATE:	2/21/02		SAMPLE I.D.	R-24	DEPTH:	1.0-7.0'
NOTES:	PROCTOR DATA Opt. Moisture =	A: 10.9%	Max. Dry Density =	TEST 123.0	PROCEDURE: PCF	ASTM D 698

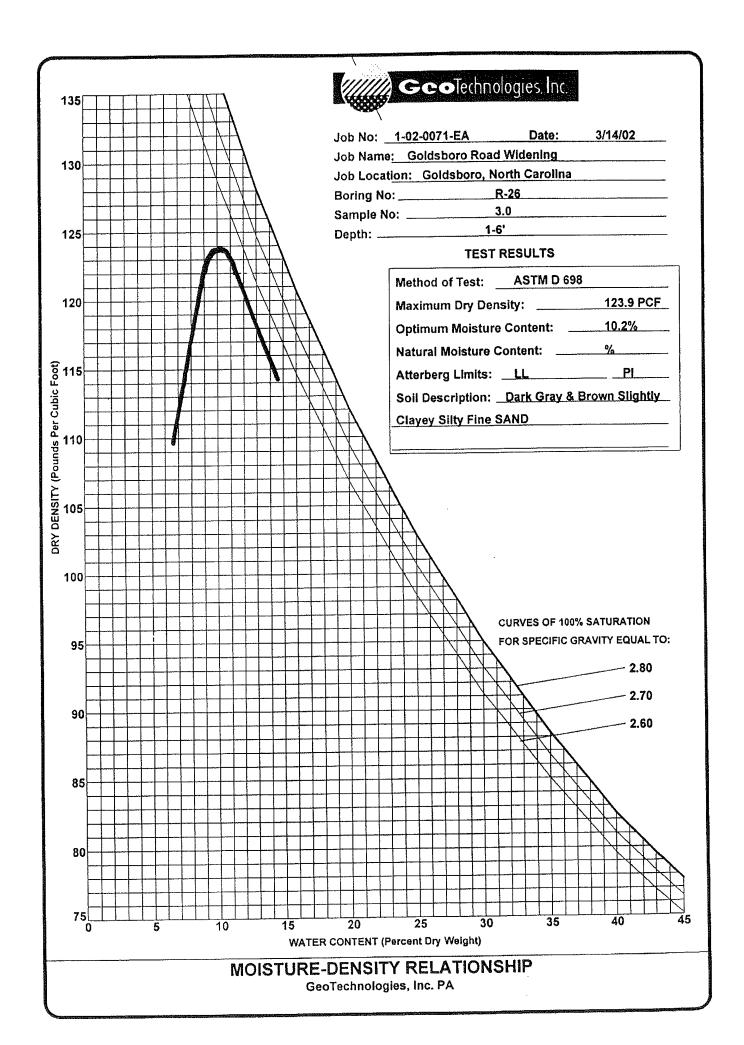
SOIL DESCRIPTION: Gray Brown Silty Medium-Fine SAND

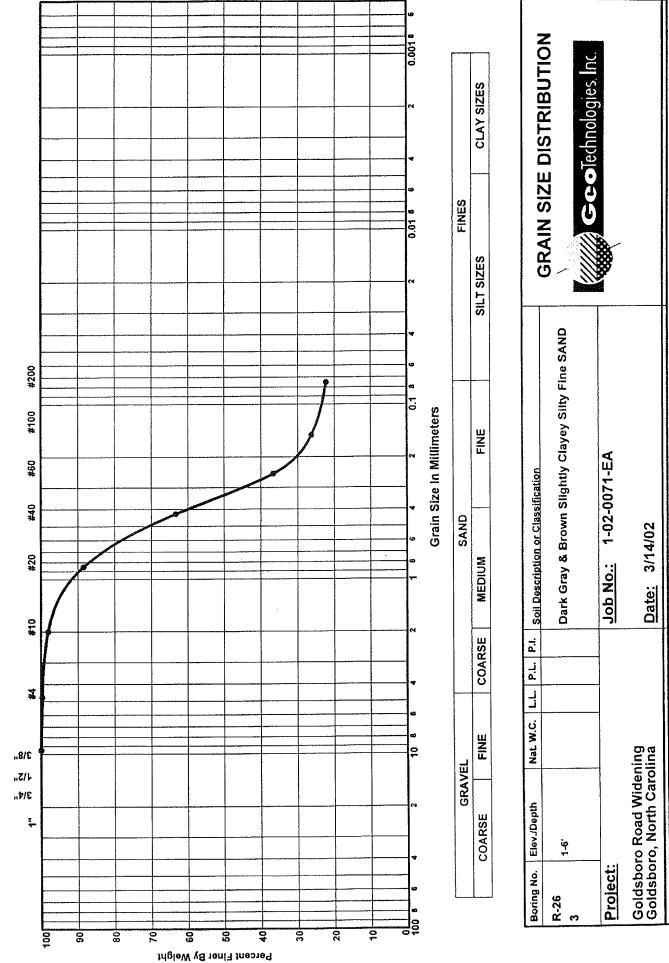
CBR SPECIMEN DATA		Swell Data	1
MOISTURE CONTENT	10.9%	Initial Reading	0.160
WET DENSITY	136,4 lbs./cu.ft.	Final Reading	0.158
DRY DENSITY	123.0 lbs./cu.ft.	Mold Height	4.584
% COMPACTION	100.0 %	% Swell	0.0
PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min.

1.80



28.0
0.0



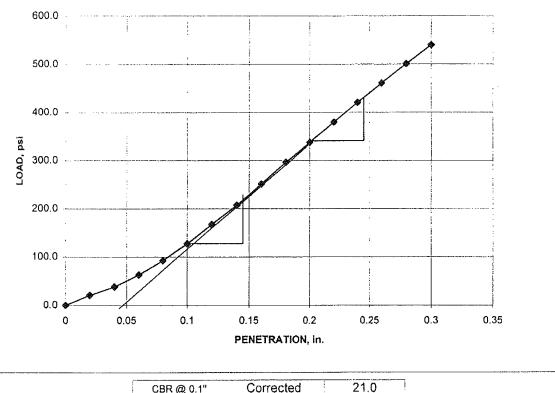


JOB #: 1-02-0071-EA JOB NAME: Goldsboro Rd. Widening DATE: 2/21/02 R-26 SAMPLE I.D. DEPTH: 1.0-6.0' NOTES: **PROCTOR DATA:** TEST PROCEDURE: ASTM D 698 Opt. Moisture = 10.2% Max. Dry Density = 123.9 PCF

SOIL DESCRIPTION: Dark Gray Brown Slightly Clayey Silty Fine SAND

CBR SPECIMEN DATA		Swell I	Data
MOISTURE CONTENT	10.2%	Initial Reading	0.151
WET DENSITY	134.6 lbs./cu.ft.	Final Reading	0.150
DRY DENSITY	122.1 lbs./cu.ft.	Mold Height	4.583
% COMPACTION	98.6 %	% Swell	0.0

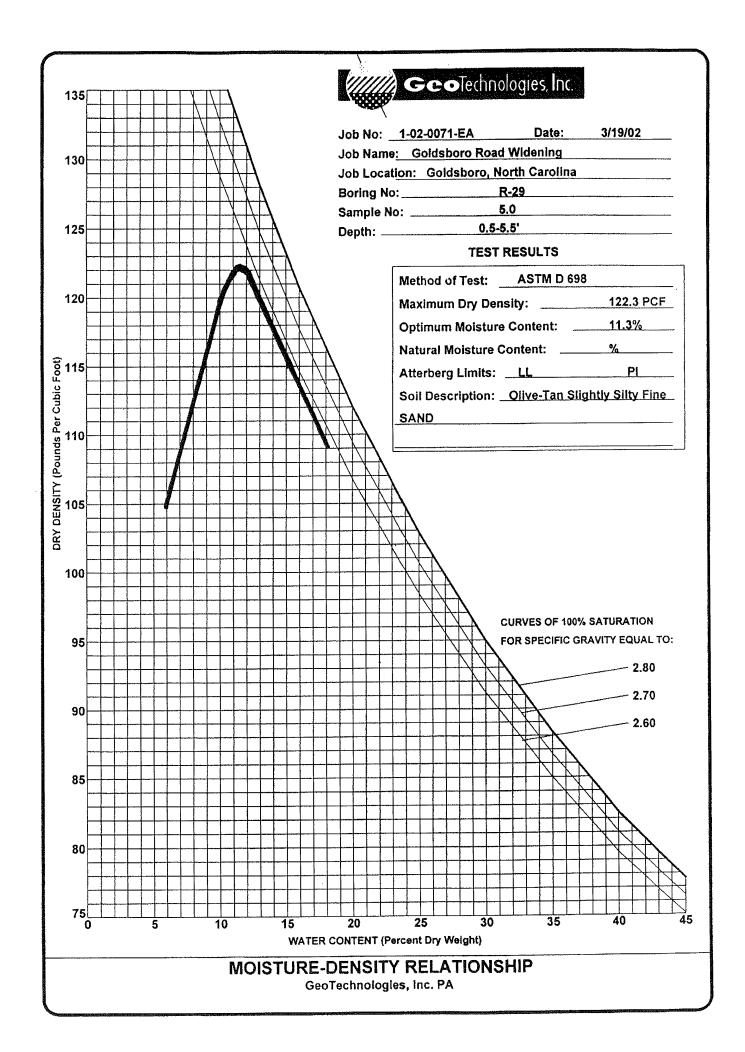
PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min.
PROVING RING CONSTANT	1.80	SURCHARGE USED	10 lbs.

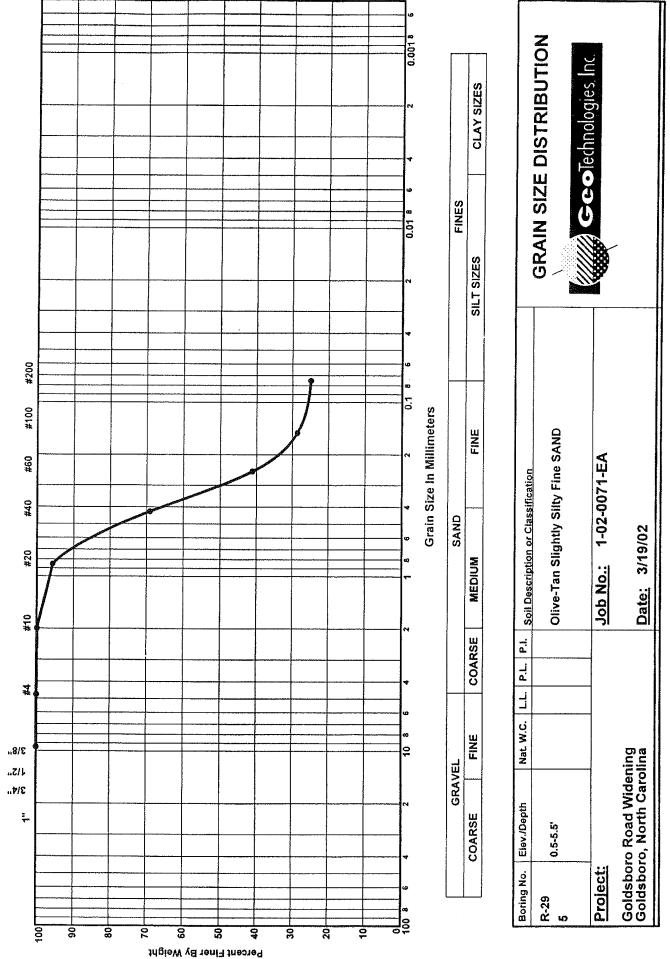


CBR @ 0.1"	Corrected	21.0
CBR @ 0.2"	Corrected	28.0
% SWELL		0.0

GeoTechnologies, Inc.

CBR DATA SHEET





CBR DATA SHEET

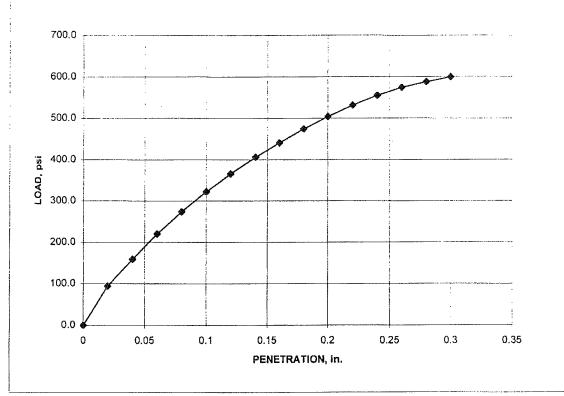
JOB #:	1-02-0071-EA		JOB NAME:	Goldsboro	Rd. Widening	
DATE:	2/21/02		SAMPLE I.D.	R-29	DEPTH:	0.5-5.5
NOTES:	PROCTOR DATA Opt. Moisture =	: 11.3%	Max. Dry Density =	TES 122.3	T PROCEDURE: PCF	ASTM D 698

Olive Tan Silty Fine CAND SOIL DESCRIPTION:

CBR SPECIMEN DATA		Swell Data	1
MOISTURE CONTENT	11.3%	Initial Reading	0.301
WET DENSITY	134.1 lbs./cu.ft.	Final Reading	0.303
DRY DENSITY	120.5 lbs./cu.ft.	Mold Height	4.597
% COMPACTION	98.5 %	% Swell	0.0
PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in /min

PROVING RING USED PROVING RING CONSTANT

200 lb.	RATE OF DEFORMATION	.05 in./min.
1.80	SURCHARGE USED	10 lbs.

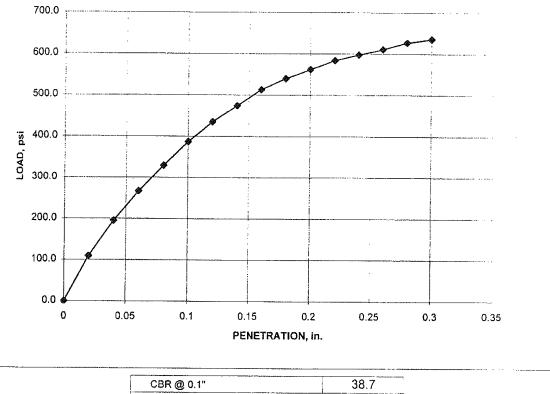


33.6
0.0

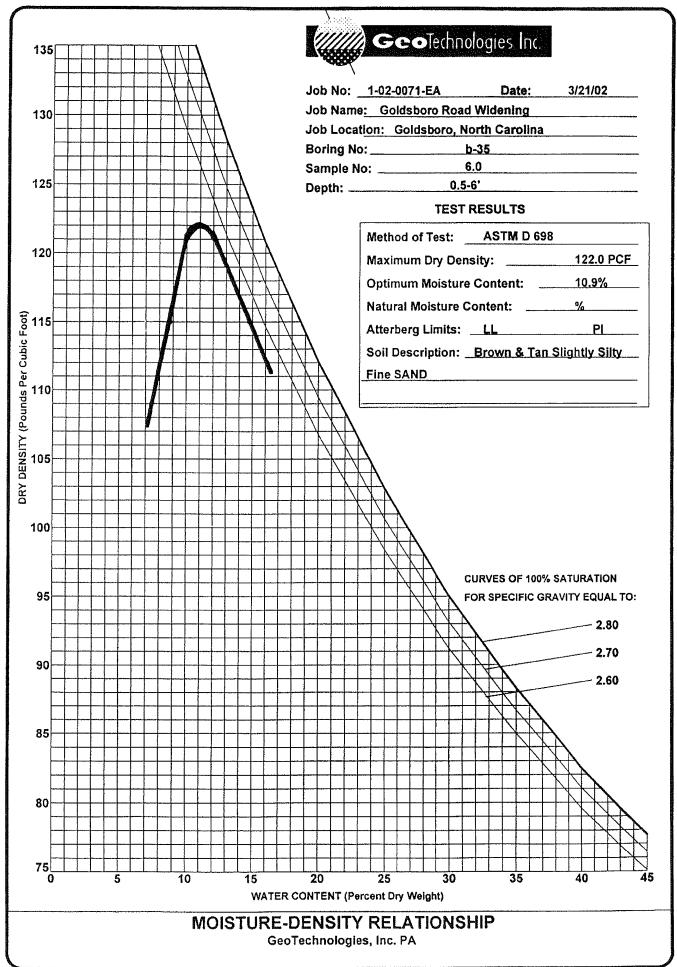
GeoTech	nologies, Inc.	•	•	СВ	R DATA	SHEET	
JOB #:	1-02-0071-EA		JOB NAME:	Gol	dsboro F	d. Widening	
DATE:	2/21/02		SAMPLE I.D.		B-35	DEPTH:	.05-6.0'
NOTES:	PROCTOR DATA Opt. Moisture =	: 10.9%	Max. Dry Density =		TEST 122.0	PROCEDURE: PCF	ASTM D 698
	SOIL DESCRIPTI	DN:	Brown Tan Slight	tly Si	Ity Fine S	AND	

CBR SPECIMEN DATA		Swell	Data
MOISTURE CONTENT	10.9%	Initial Reading	0.352
WET DENSITY	135.3 lbs./cu.ft.	Final Reading	0.353
DRY DENSITY	122.0 lbs./cu.ft.	Mold Height	4.594
% COMPACTION	100.0 %	% Swell	0.0

PROVING RING USED	2200 lb.	RATE OF DEFORMATION	.05 in./min.
PROVING RING CONSTANT	1.80	SURCHARGE USED	10 lbs.



CBR @ 0.1"	38.7
CBR @ 0.2"	37.5
% SWELL	0.0



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