# STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS** 

GEOTECHNICAL ENGINEERING UNIT

# **STRUCTURE**

SUBSURFACE INVESTIGATION

STATE PROJECT 33481.1.1 I.D. NO. B-4128 F.A. PROJECT\_*BRSTP-1549(4)* COUNTY GUILFORD PROJECT DESCRIPTION BRIDGE NO. 73 ON -L- (SR 1549, MACKAY RD.) OVER BULL RUN CREEK AT STA. 24+02

INVENTORY

| STATE   | STATE P   | ROJECT REFERENCE NO. | SHEET<br>NO. | TOTAL |
|---------|-----------|----------------------|--------------|-------|
| N.C.    | 3348      | 31.1.1 (B-4128)      | 1            | 16    |
| STATE I | PROJ. NO. | F. A. PROJ. NO.      | DESCRIP      | TION  |
| 3348    | 1.1.1     | BRSTP-1549(4)        | P.E.         |       |
|         |           |                      | CONS         | Т.    |

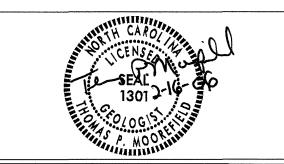
#### **CAUTION NOTICE**

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WAS MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FILED BORING LOGS, ROCK CORES, AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL UNIT @ (9)9) 250-4088. NEITHER THE SUBSURFACE PLANS AND REPORTS, NOR THE FIELD BORING LOGS, ROCK CORES, OR SOIL TEST DATA IS PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARLY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORNICS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION, THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS THE BILDER OF CONTINUE TO A CADITORED THAT DETAILS SHOWN OF THE SUBSUITAGE FLANS
ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING
AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN
INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY INFORMATION ON HIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED, TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THIS PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

INVESTIGATED BY T.P. MOOREFIELD PERSONNEL N.D. MOHS N.T. ROBERSON D.W. DIXON SUBMITTED BY\_N.T. ROBERSON H.R. CONLEY FEBRUARY 2006 M.L. REEDER



NOTE - BY HAVING REQUESTED THIS INFORMATION THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS

DRAWN BY: T.T. WALKER, N.D. MOHS

**CONTENTS:** SHEET DESCRIPTION

6,7

8

9-12

13

14

15

TITLE SHEET

SITE PLAN

-L- PROFILE

CROSS SECTIONS -DET- PROFILE

SCOUR REPORT

SOIL TEST RESULTS

CORE PHOTOGRAPHS

SITE PHOTOGRAPH

STRUCTURE INVENTORY REPORT

BORE LOGS & CORE REPORT

LEGEND

FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

NOTE - THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS BEING ACCURATE NOR IT IS CONSIDERED TO BE PART OF THE PLANS, SPECIFICATIONS, OR CONTRACT FOR THE PROJECT.

### NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

### SUBSURFACE INVESTIGATION

|   | SOIL AND ROCK LEGEND, TERM  | IS, SYMBOLS, AND ABBREVIATIONS   |  |
|---|---|--|--|
| SOIL DESCRIPTION  | GRADATION   | ROCK DESCRIPTION   | TERMS AND DEFINITIONS  |
| SOIL IS CONSIDERED TO BE THE UNCONSOLIDATED, SEMI-CONSOLIDATED OR WEATHERED EARTH MATERIALS WHICH CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER, AND WHICH YIELDS LESS THAN  | MELL GRADED: INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE UNIFORM- INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. (ALSO POORLY GRADED)   | HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WHEN TESTED, WOULD YIELD SPT REFUSAL. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL.            | ALLUVIUM (ALLUV.) - SOILS WHICH HAVE BEEN TRANSPORTED BY WATER.  |
| 100 BLOWS PER FOOT ACCORDING TO STANDARD PENETRATION TEST (AASHTO 1206, ASTM D-1586), SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM AND BASIC DESCRIPTIONS GENERALLY SHALL INCLUDE:   | GAP-GRADED- INDICATES A MIXTURE OF UNIFORM PARTICLES OF TWO OR MORE SIZES.  | SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.  IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE | AQUIFER - A WATER BEARING FORMATION OR STRATA.   |
| CONSISTENCY, COLOR, TEXTURE, MOISTURE, AGSHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. EXAMPLE:   | ANGULARITY OF GRAINS  THE ANGULARITY OR ROUNDNESS OF BOIL GRAINS ARE DESIGNATED BY THE TERMS; ANGULAR,  | OF WEATHERED ROCK.  ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLOWS:  | ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.  ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS.   |
| VERY STIFF, GRAY SRITY CLAY, MOST WITH INTERBEDOED FINE SAND LAVERS, HIGHLY PLASTIC, A-7-6  | SUBANGULAR, SUBROUNDED, OR ROUNDED.   | WEATHERED ROCK (WR) NON-COASTAL PLAIN MATERIAL THAT YIELDS SPT N VALUES > 100 BLOWS PER FOOT.  | OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, AS SHALE, SLATE, ETC.   |
| SOIL LEGEND AND AASHTO CLASSIFICATION   | MINERALOGICAL COMPOSITION   | CRYSTALLINE FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT   | ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IS IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE  |
| GENERAL GRANULAR MATERIALS SILT-CLAY MATERIALS CLASS. (35% PASSING *200) (785% PASSING *200) ORGANIC MATERIALS  | MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAQLIN, ETC. ARE USED IN DESCRIPTIONS WHENEVER THEY ARE CONSIDERED OF SIGNIFICANCE.   | ROCK (CR) WOULD YIELD SPT REFUSAL IF TESTED, ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.  | GROUND SURFACE.  CALCAREOUS (CALC.) - SOILS WHICH CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.  |
| GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5 CLASS. A-1-a A-1-b A-2-5 A-2-5 A-2-5 A-2-7 A-1 A-5 A-3 A-6, A-7   | COMPRESSIBILITY   | NON-CRYSTALLINE FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YELLD SPT REFUSAL IF TESTED. ROCK TYPE  | COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM  |
| CLASS. A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-7-6 A-3 A-6, A-7 SYMBOL  | SLIGHTLY COMPRESSIBLE LIOUID LIMIT LESS THAN 30  MODERATELY COMPRESSIBLE LIOUID LIMIT 31-50   | COASTAL PLAIN COASTAL PLAIN SEDIMENTS CEMENTED INTO BOCK BUT MAY NOT YIELD   | OF SLOPE.  |
| Z PASSING   | HIGHLY COMPRESSIBLE LIQUID LIMIT GREATER THAN 50  PERCENTAGE OF MATERIAL  | SEDIMENTARY ROCK SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANOSTONE, CEMENTED (CP) SHELL BEDS, ETC.  | CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.  |
| * 10 50 MX GRANULAR SILT- MUCK, CLAY PEAT SOILS COLO. PEAT  | ORGANIC MATERIAL GRANULAR SILT- CLAY SOILS SOILS OTHER MATERIAL   | WEATHERING   | <u>DIKE</u> - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.  |
| - 200 15 MX 25 MX 10 MX 35 MX 35 MX 35 MX 35 MX 36 MX | TRACE OF DRGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10%   | FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING, ROCK RINGS UNDER HAMMER IF CRYSTALLINE.  | <u>DIP</u> - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.   |
| LIQUID LINET 46 MX41 MN 46 MX41 MN 48 MX41 MN 48 MX41 MN 48 MX11 MN 50ILS WITH PLASTIC INDEX 6 MX N.P. 10 MX10 MX10 MX10 MX10 MX10 MX10 MX11 MN 11 MN | MODERATELY ORGANIC 5 - 10% 12 - 20% SOME 20 - 35%   | VERY SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN,   | DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF  |
| GROUP INDEX 0 0 0 4 MX 8 MX 12 MX 16 MX No MX MODERATE ORGANIC  | HIGHLY ORGANIC >10% >20% HIGHLY 35% AND ABOVE  GROUND WATER   | (V.SLI.) CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY, ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.  | THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.  |
| USUAL TYPES STONE FRACS, FINE SILTY OR CLAYEY SILTY CLAYEY ORGANIC  | WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING.  | SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR                              | FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.   |
| OF MAJOR GRAVEL AND SAND GRAVEL AND SAND SOILS MATTER   | STATIC WATER LEVEL AFTER 24 HOURS.  | CRYSTALS ARE DULL AND DISCOLORED, CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS, MODERATE SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS, IN                                     | FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.  |
| GEN. RATING AS A EXCELLENT TO GOOD FAIR TO POOR POOR UNSUITABLE   | E PERCHED WATER, SATURATED ZONE OR WATER BEARING STRATA   | (MOD.) GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY, ROCK HAS   | FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.   |
| SUBGRADE P.I. OF A-7-5 ≤ L.L 30 ; P.I. OF A-7-6 > L.L 30  | SPRING OR SEEPAGE   | DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.  | FLOOD PLAIN (F.P.) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM,  |
| CONSISTENCY OR DENSENESS  | MISCELLANEOUS SYMBOLS   | MODERATELY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL SEVERE AND DISCOLORED AND A MAJORITY SHOW KAQLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH          | FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN  |
| PRIMARY SOIL TYPE COMPACTNESS OR CONSISTENCY RANGE OF UNCONFINED PENETRATION RESISTENCE COMPRESSIVE STRENGTH  | ROADWAY EMBANKMENT  WITH SOIL DESCRIPTION  POPULATION  SPT CPT  SPT CPT  POPULATION  SPT CPT  SPT CPT | (MOD. SEV.) AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK, ROCK GIVES 'CLUNK' SOUND WHEN STRUCK,  IF TESTED, WOULD YIELD SPT REFUSAL  | THE FIELD.   |
| VERY LODGE  | DESIGNATIONS  | SEVERE ALL ROCKS EXCEPT QUARTZ DISCOLORED OR STAINED, ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED  | JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.  LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO  |
| GRANULAR LOOSE 4 TO 10  | SOIL SYMBOL AUGER BORING S- BULK SAMPLE   | IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN.  | ITS LATERAL EXTENT.  |
| MATERIAL DENSE 10 10 30 10 30 10 30 10 30 10 50 10 50 10 50 10 50 10 50   | ARTIFICIAL FILL OTHER THAN ROADWAY EMBANKMENTS  ARTIFICIAL FILL OTHER THAN CORE BORING SS- SPLIT SPOON SAMPLE   | IF TESTED, YIELDS SPT. N. VALUES > 100 BPF  VERY SEVERE ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED, ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT   | LENS - A BODY OF SOIL OR ROCK THAT THINS DUT IN ONE OR MORE DIRECTIONS.  MOTILED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTILING IN   |
| VERY SOFT   | ST- SHELBY TUBE  MONITORING WELL  SAMPLE  | (V. SEV.)  THE MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE SUCH THAT ONLY MINOR                   | SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.  PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN   |
| GENERALLY   SOFT   2 TO 4   0.25 TO 0.5   | SINFERRED ROCK LINE  A PIEZOMETER  RS- ROCK SAMPLE  | VESTIGES OF THE ORIGINAL ROCK FABRIC REMAIN. IF TESTED, YIELDS SPT N VALUES < 100 BPF  | INTERVENING IMPERVIOUS STRATUM.  |
| MATERIAL STIFF 8 TO 15 1 TO 2 (COHESIVE) VERY STIFF 15 TO 30 2 TO 4   | INSTALLATION RT- RECOMPACTED  SLOPE INDICATOR TRIAXIAL SAMPLE   | COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS                     | RESIDUAL SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.  |
| HARD >30 >4   | 25/825 DIP/DIP DIRECTION OF SLOPE INDICATOR INTAXIAL SAMPLE INSTALLATION CBR - CBR SAMPLE   | ALSO AN EXAMPLE.  ROCK HARDNESS  | ROCK DUALITY DESIGNATION (R.O.D.) - A MEASURE OF ROCK DUALITY DESCRIBED BY: TOTAL LENGTH OF ROCK SEGMENTS EDUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. |
| TEXTURE OR GRAIN SIZE   | SPT N-VALUE   | VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK, BREAKING OF HAND SPECIMENS REQUIRES  | SAPROLITE (SAP.) - RESIDUAL SOIL WHICH RETAINS THE RELIC STRUCTURE OR FABRIC OF THE  |
| U.S. STD. SIEVE SIZE 4 10 40 60 200 270 OPENING (MM) 4.76 2.0 0.42 0.25 0.075 0.053   | KEF - SPI REPUSAL   | SEVERAL HARD BLOWS OF THE GEOLOGISTS PICK.   | PARENT ROCK.  SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND  |
| BOULDER COBBLE GRAVEL COARSE FINE SILT CLAY   | ABBREVIATIONS  AR - AUGER REFUSAL PMT - PRESSUREMETER TEST  | HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.   | RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, WHICH HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS   |
| (BLDR.) (COB.) (GR.) (CSE. SD.) (F. SD.) (SL.) (CL.)  | BT - BORING TERMINATED SD SAND, SANDY   | MODERATELY CAN BE SCRATCHED BY KNIFE OR PICK, GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGISTS PICK, HAND SPECIMENS CAN BE DETACHED                               | SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR  |
| GRAIN MM 305 75 2.0 0.25 0.05 0.005<br>SIZE IN 12' 3'   | CL CLAY SL SILT, SILTY CPT - CONE PENETRATION TEST SLI SLIGHTLY   | BY MODERATE BLOWS.   | SLIP PLANE.  STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR B.P.F.) OF   |
| SOIL MOISTURE - CORRELATION OF TERMS  | CSE COARSE TCR - TRICONE REFUSAL DMT - DILATOMETER TEST DPT - DYNAMAC PENETRATION TEST TO THE TRICONE REFUSAL T   | MEDIUM CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. HARD CAN BE EXCAVATED IN SMALL CHIPS TO PEICES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE                    | A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER, SPT REFUSAL IS LESS THAN 0.1 FOOT PENETRATION                         |
| SOIL MOISTURE SCALE FIELD MOISTURE GUIDE FOR FIELD MOISTURE DESCRIPTION   | e - VOID RATIO 76 - DRY UNIT WEIGHT   | POINT OF A GEOLOGISTS PICK.  SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK, CAN BE EXCAVATED IN FRAGMENTS  | WITH 60 BLOWS.   |
| - SATURATED - USUALLY LIQUID; VERY WET, USUALLY   | F FINE W - MOISTURE CONTENT FOSS FOSSILIFEROUS V VERY   | FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.   | STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.   |
| (SAT.) FROM BELOW THE GROUND WATER TABLE  | FRAC FRACTURED VST - VANE SHEAR TEST FRAGS FRAGMENTS  | VERY CAN BE CARVED WITH KNIFE, CAN BE EXCAVATED READILY WITH POINT OF PICK, PIECES   INCH  | STRATA ROCK QUALITY DESIGNATION (S.R.Q.D.) - A MEASURE OF ROCK QUALITY DESCRIBED BY: TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 10 CENTIMETERS DIVIDED                                |
| PLASTIC RANGE - WET - (W) SEMISOLID, REQUIRES DRYING TO   | MED MEDIUM  | FINGERNAIL.  | BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.   |
| (PI) PLASTIC LIMIT ATTAIN OPTIMUM MOISTURE  | EQUIPMENT USED ON SUBJECT PROJECT   | FRACTURE SPACING BEDDING   | TOPSOIL (T.S.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.  |
| OM OPTIMUM MOISTURE - MOIST - (M) SOLID; AT OR NEAR OPTIMUM MOISTURE  | DRILL UNITS:  ADVANCING TOOLS:  HAMMER TYPE:  X AUTOMATIC MANUAL  | TERM SPACING IERM THICKNESS  VERY WIDE MORE THAN 10 FEET VERY THICKLY BEDDED > 4 FEET  | BENCH MARK: -BL6- 19+96 AT -L- STATION 24+41, 14' LT   |
| SL SHRINKAGE LIMIT  | MOBILE B CLAY BITS  | WIDE 3 TO 10 FEET THICKLY BEDDED 1.5 - 4 FEET  MODERATELY CLOSE 1 TO 3 FEET THINLY BEDDED 0.16 - 1.5 FEET  | ELEVATION: 771.9 FEET  |
| - DRY - (D) REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE  | 6° CONTINUOUS FLIGHT AUGER CORE SIZE:   | CLOSE 0.16 TO 1 FEET VERY THINLY BEDDED 0.03 - 0.16 FEET VERY CLOSE 1 FSS THAN 0.16 FFET THICKLY LAMINATED 0.008 - 0.03 FEET   | NOTES:   |
| PLASTICITY  | A S HOLLOW HOUSERS  | THINLY LAMINATED < 0.008 FEET  INDURATION  |  |
| PLASTICITY INDEX (PI) DRY STRENGTH  | CME-45C X HARD FACED FINGER BITS X -NXWL.   | FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF THE MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.  |  |
| NONPLASTIC         0-5         VERY LOW           LOW PLASTICITY         6-15         SLIGHT  | X CME-550 X CASING X N/ ADVANCED  | FRIGHT F RUBBING WITH FINGER FREES NUMEROUS GRAINS:  | ·  |
| MED. PLASTICITY 16-25 MEDIUM HIGH PLASTICITY 26 OR MORE HIGH  | PORTABLE HOIST TRICONE STEEL TEETH POST HOLE DIGGER   | GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.  MODERATELY INDUBATED. GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE:   |  |
| COLOR   | TRICONE STUDE CORP HAND HIGER   | MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER,   |  |
| DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YEL-BRN, BLUE-GRAY)   | T CORE BIT SOUNDING ROD   | INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.   |  |
| MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.  | OTHER OTHER OTHER OTHER   | EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE;   |  |
|   | J OHER  | SAMPLE BREAKS ACROSS GRAINS.   |  |
|   |   |  | REVISED 09/15/00   |

STATE PROJECT NO. SHEET NO. TOTAL SHEETS
33481.1.1 2 16

ID B-4128



# STATE OF NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

MICHAEL F. EASLEY
GOVERNOR

LYNDO TIPPETT SECRETARY

February 15, 2006

STATE PROJECT:

33481.1.1 (B-4128)

F.A. PROJECT:

BRSTP-1549(4)

COUNTY:

Guilford

DESCRIPTION:

Bridge No. 73 on -L- (SR 1549) over Bull Run Creek at Station 24+02.0

SUBJECT:

Geotechnical Report – Structure Inventory

#### **Project Description**

A single-span bridge, 100-feet in length with a 120° skew, is proposed at the same location on -L- (SR 1549, Mackay Rd.) over Bull Run Creek to replace the existing structure. The new bridge is 64 feet in width and will accommodate four travel lanes. The existing structure is 40 feet in length and 25 feet in width. An onsite temporary detour bridge is to be constructed approximately 59 feet upstream of the existing bridge. The project is located in Guilford County within the city limits of Greensboro.

The subsurface investigation for the structure was conducted during January 2006 using an ATV-mounted CME-550 drill machine. Two Standard Penetration Test borings were performed at each end bent location. Boring EB2-A was cored using NXWL core equipment. Two borings were completed at the detour end bent locations in March 2005 using an ATV-mounted CME-550 drill machine. All borings were advanced until crystalline rock was encountered. Representative soil samples were obtained for visual classification in the field and selected samples were sent to the Materials and Tests Unit for laboratory analysis.

#### Physiography and Geology

The project is located in gently rolling terrain of the Piedmont Physiographic province. The project area is suburban, with housing developments and an apartment complex nearby. The area along Bull Run Creek is wooded. Geologically, the project is located within the Carolina Slate Belt and is underlain by metamorphosed gabbro and diorite.

#### **Soil Properties**

Soils encountered at the project site include roadway embankment, artificial fill, alluvial and residual soils.

Roadway embankment was encountered at end bent one. Embankment soils are from 9.0 to 9.5 feet thick, and are composed of orange-brown, soft, moist, silty clay (A-7-6) at EB1-A, and brown, medium stiff, moist, clayey sand (A-2-6) at EB1-B. The embankment at EB1-B is associated with the former alignment of the roadway.

SHEET 3 OF 16 33481.1.1 (B-4128) Guilford Co.

Artificial fill was encountered at end bent two. These soils are associated with a sewer line easement that parallels Bull Run Creek. Artificial fill ranges from 10.0 to 10.8 feet thick, and consists of brown, soft, moist to wet, sandy silt (A-4).

Alluvial soils were encountered at the end bent one boring locations. The alluvial soils range from 4.1 to 6.2 feet in thickness. These soils consist of orange-tan, very soft, wet, sandy silt (A-4), and tan to brown, loose, moist to saturated, silty sand (A-2-4). The alluvial soils were deposited on residual soil and weathered rock.

Residual soils were encountered at all boring locations and range from 1.2 to 8.5 feet in thickness. The residual soils consist of gray to green-gray, dense to very dense, moist to wet, silty sand (A-2-4), and gray, very dense, coarse sand and gravel (A-1-b). The residual soils are underlain by weathered and/or crystalline rock.

#### **Rock Properties**

Weathered rock was derived from the underlying bedrock consisting of metamorphosed diorite (metadiorite) and metamorphosed gabbro (metagabbro). The weathered rock ranges in thickness from 1.7 to 6.2 feet. Weathered rock was encountered in all borings except EB2 -DET-. The top of weathered rock ranges in elevation from 752.9 feet at EB1-B to 755.9 feet at EB2-B.

Crystalline rock was encountered at each boring location. The top of crystalline rock ranges in elevation from 743.2 feet at DET-1- to 753.5 feet at EB2-B. Crystalline rock at end bent one is metadiorite while rock at end bent two is metagabbro. Core recovery ranged from 92% to 100%, with an average of 95%. Rock Quality Designation (RQD) ranges from 62% to 78%, with an average of 80%. More detailed rock descriptions can be found in the Core Boring Report.

#### **Temporary Detour Structure**

A temporary detour structure will be constructed approximately 59 feet north of the existing bridge at -DET- STA. 24+00. The structure has a total length of 85 feet. Borings DET-1 and DET-2, were drilled along the -DET- alignment to provide additional information for the detour structure.

Geologic conditions along the -DET- alignment should correlate directly to those encountered along the main structure.

#### **Groundwater**

Groundwater was present in all borings. The groundwater elevations ranged from 756.0 feet at EB1-DET- to 761.1 feet at EB2-A and EB2 -DET-. Surface water in Bull Run Creek was measured at elevation 757.1 feet in January 2006.

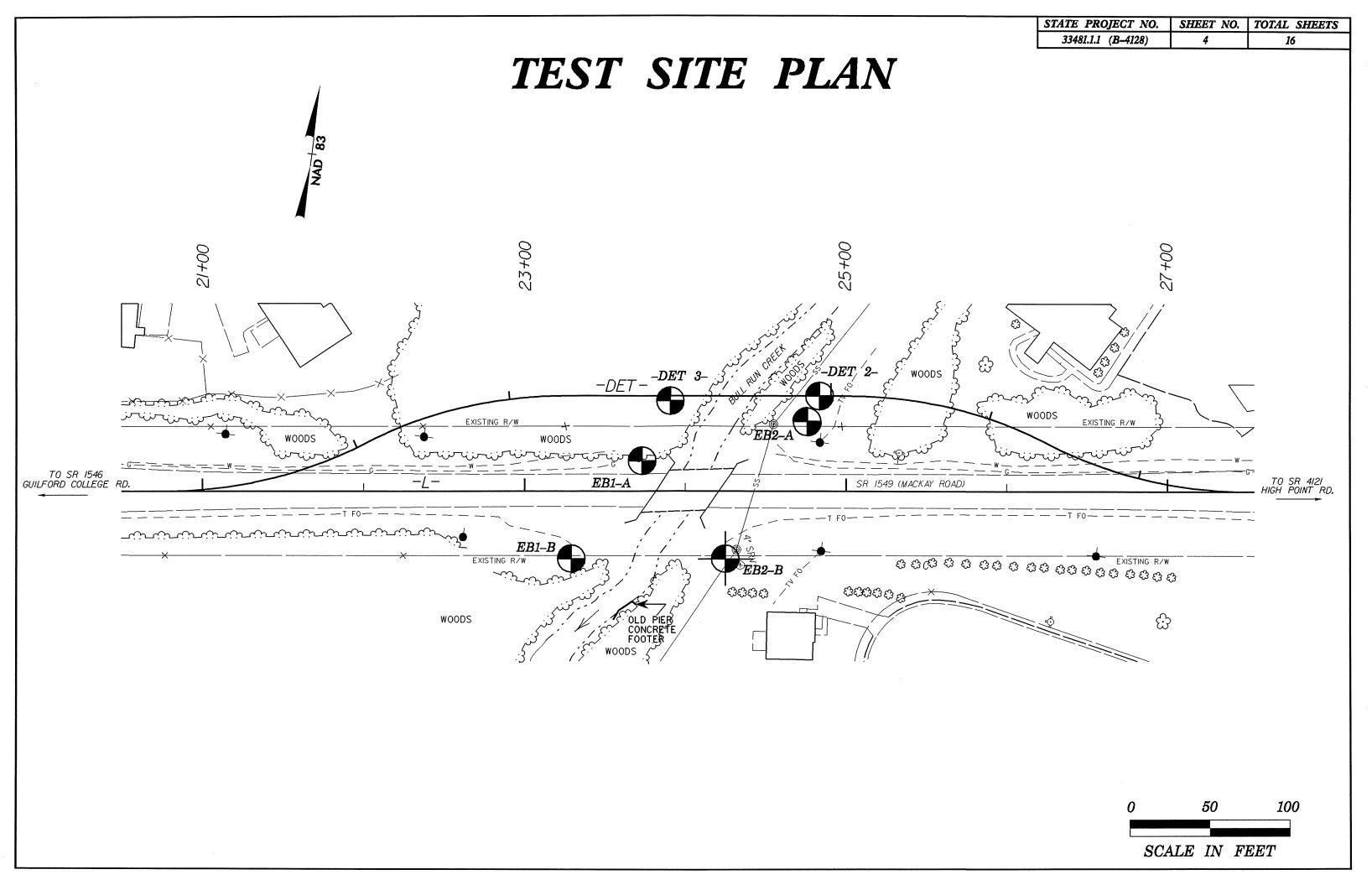
#### **Notice**

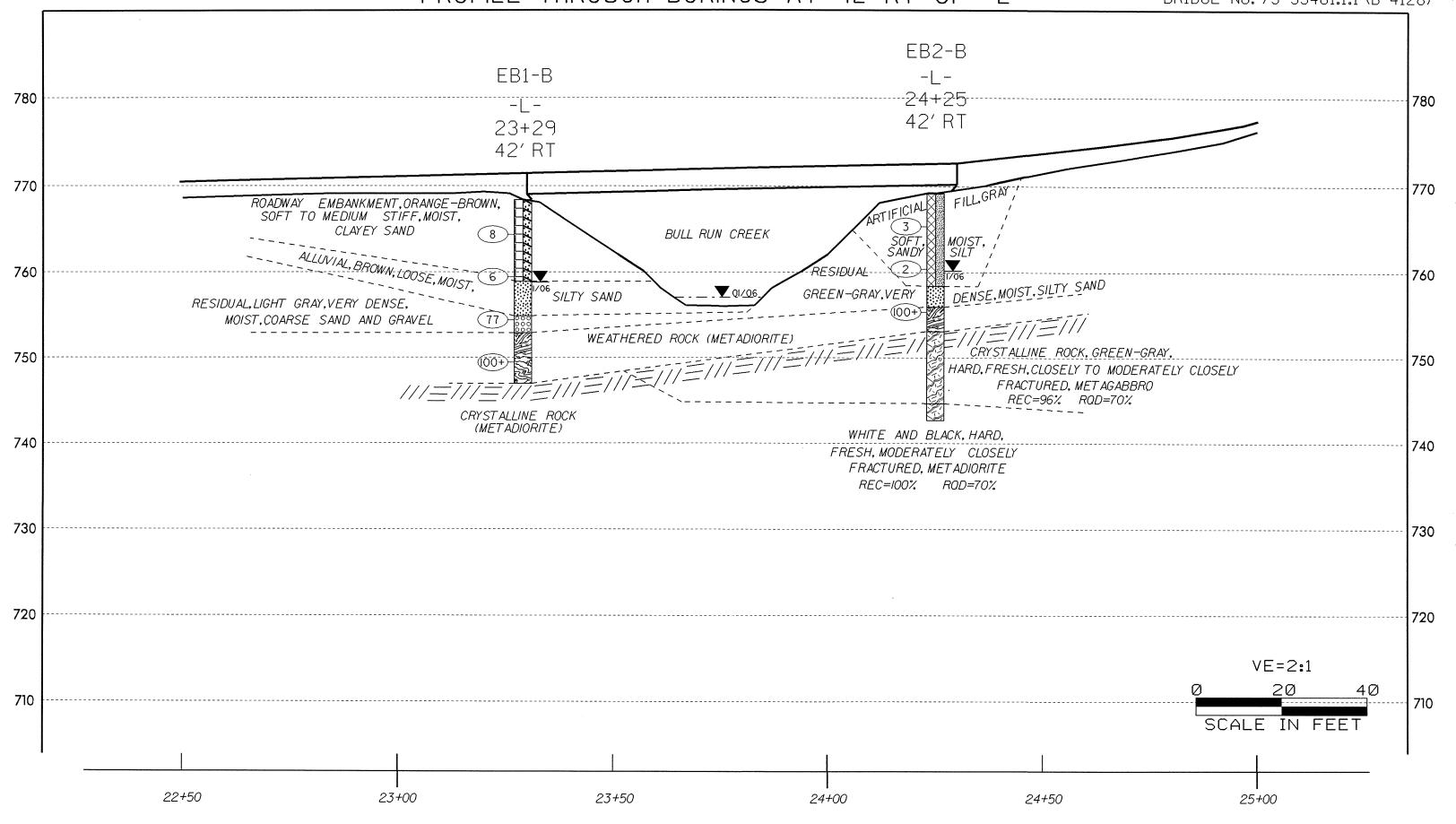
This Geotechnical foundation report is based on the Bridge Survey and Hydraulic Report for Bull Run Creek dated May 2, 2005 and the Preliminary General Drawing dated October 25, 2005. If significant changes are made in the design or location of the proposed structure, the subsurface information should be reviewed and modified as necessary.

repared by,

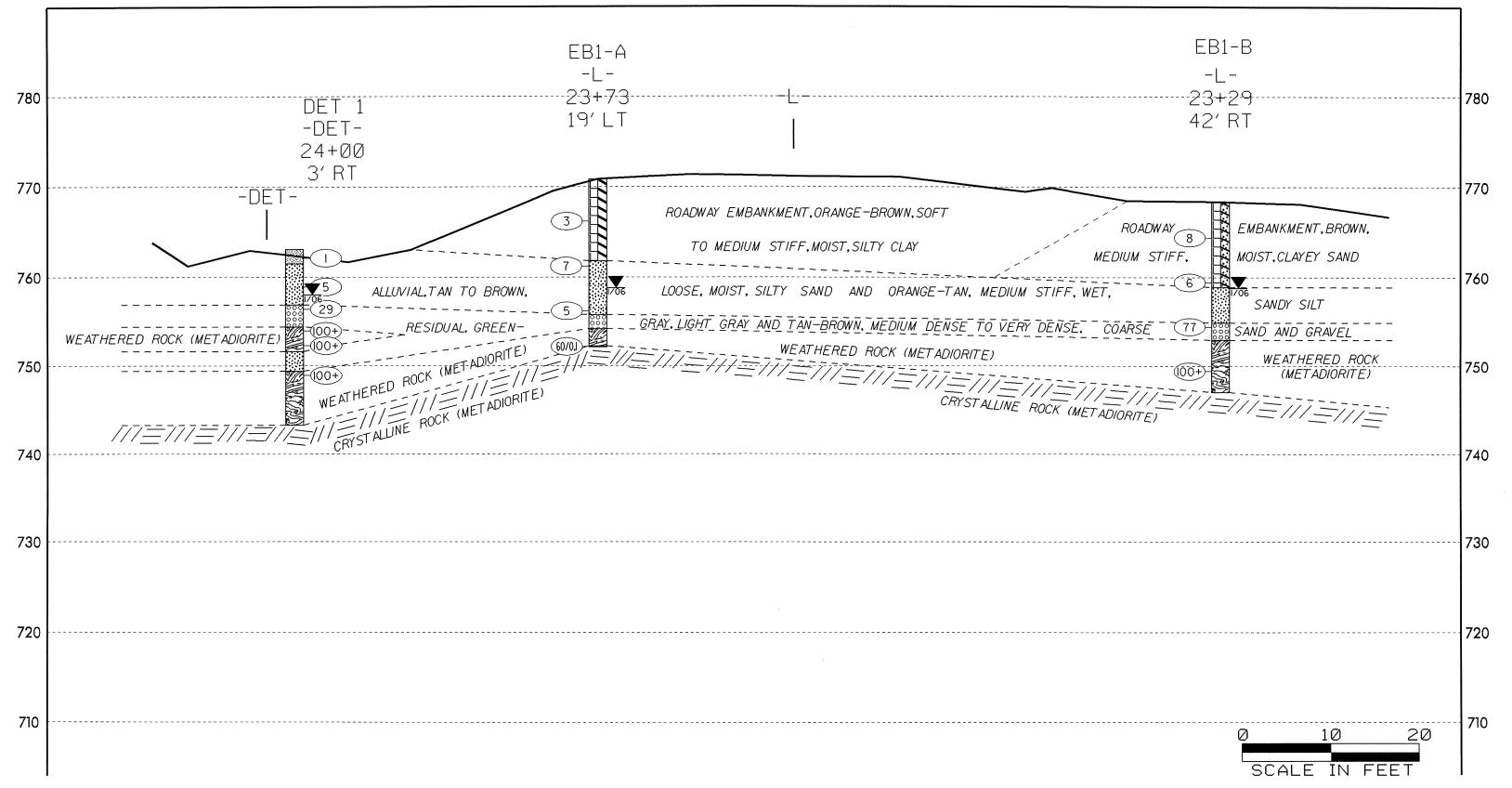
Nathan Mohs

**Engineering Geologist** 

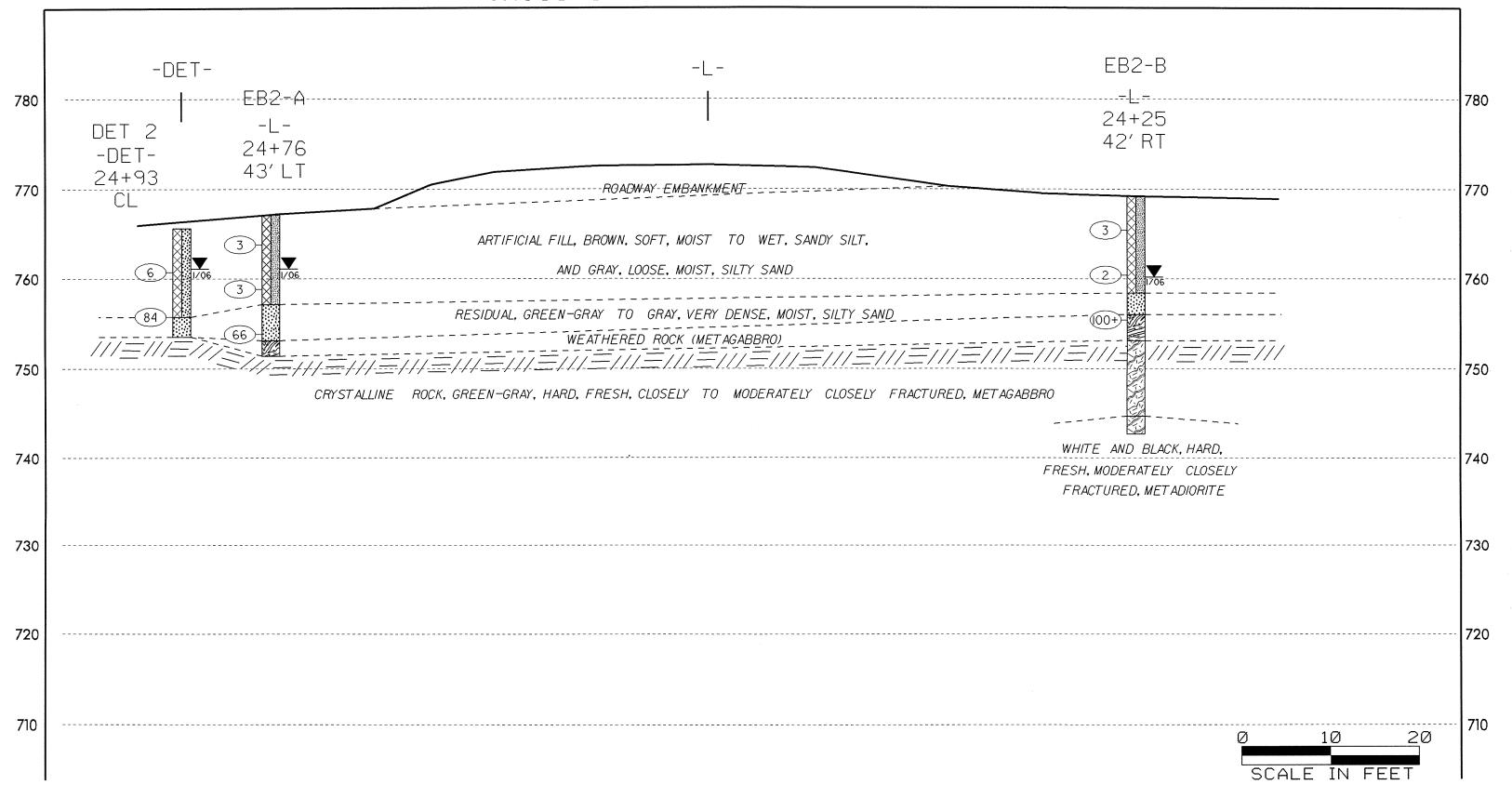


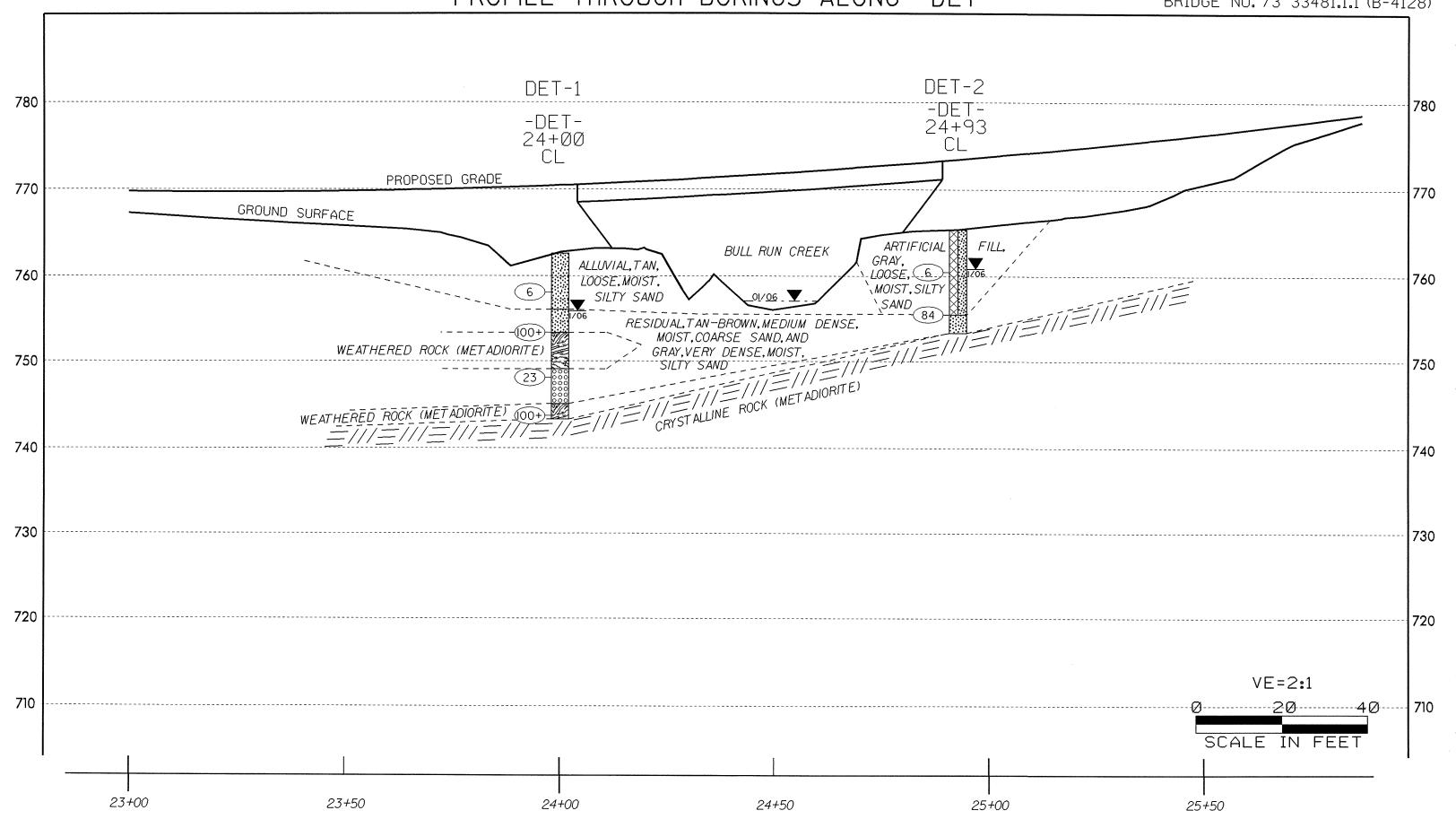


# CROSS SECTION THROUGH END BENT I



## CROSS SECTION THROUGH END BENT 2





north carolina department of transportation — north carolina department of transportation — GEOTECHNICAL UNIT BORING LOG

GEOTECHNICAL UNIT BORING LOG

|   |                                |  |                               | UNIT BORING             | LOG SHEET 9 OF 16              |
|---|--------------------------------|--|-------------------------------|-------------------------|--------------------------------|
| PROJECT NO. 33481.1.1 ID. B-4128 COUNTY GUILFORD GEOLOGIS                       | ST N.D. MOHS                   | <b>PROJECT NO.</b> 33481.1.1 <b>ID</b> . | B-4128 <b>COUNTY</b>          | GUILFORD GEO            | PLOGIST N.D. MOHS              |
| SITE DESCRIPTION BRIDGE NO. 73 ON -L- (SR 1549, MACKAY RD.)OVER BULL RU         | JN CREEK GROUND WATER          | SITE DESCRIPTION BRIDGE NO.              |                               | 9, MACKAY RD.)OVER BUL  | L RUN CREEK GROUND WATER       |
| BORING NO. EBI-A BORING LOCATION 23+73 OFFSET 19'LT ALIGNME                     | ENT -L- 0 HR. DRY              | BORING NO. EBI-B BORING LO               | CATION 23+29                  |                         | GNMENT -L- 0 HR. 9.8'          |
| COLLAR ELEVATION 770.8' NORTHING 826879' EASTING 173015                         | <b>24 HR</b> . 12 <b>.</b> 0′  | COLLAR ELEVATION 768.4'                  | <b>NORTHING</b> 826815'       |                         | 730134′ <b>24 HR.</b> 9.6′     |
| TOTAL DEPTH 18.7' DRILL MACHINE CME-550 DRILL METHOD H.S. AUGERS                | HAMMER TYPE AUTOMATIC          | TOTAL DEPTH 21.4' DRILL MAC              | CHINE CME-550                 | DRILL METHOD H.S. AUGER |                                |
| START DATE 1/6/06 COMPLETION DATE 1/6/06 SURFACE WATER DEPTH N                  | /A DEPTH TO ROCK 18.6'         | START DATE 1/5/06 COM                    | IPLETION DATE 1/5/06          |                         |                                |
| ELEV. DEPTH BLOW COUNT PEN. BLOWS PER FOOT SAMPLE                               | SOIL AND ROCK                  | DEPTHIBLOW COUNTIDES                     |                               |                         | SOIL AND ROCK                  |
| (FT.) 0.510.510.5 (FT.) 0 25 50 75 100 NUMBER MOI. G                            | DESCRIPTION                    | ELEV. (FT.) 0.510.510.51(FT.             |                               | 75 100 NUMBER MOI.      |                                |
| <u> </u>  |                                | 768.4                                    |                               |                         |                                |
| 770.8 ±   |                                | +  |                               |                         |                                |
| 770.8 +   |                                | 765.0 + 3.0   1   5   3   1.0            | )  =\frac{1}{8} = = = = = = = |                         | ROADWAY EMBANKMENT,            |
| ‡ 3.6   1   2   1   1.0     ₹ \$\bar{3} = -  -  -  -  -  -  -  -  -  -  -  -  - | ROADWAY EMBANKMENT,            |  |                               |                         | BROWN, CLAYEY SAND             |
| 765.0 +   | ORANGE-BROWN, SILTY CLAY       | 760.0 + 8.0   2   4   2   1.0            | )   -                         | <sub>M</sub>            | <u> </u>                       |
|   |                                | 1 100.0 + 1   1   2   10                 |                               | <u>M</u>                | ALLEW/AL                       |
| 8.6 5 4 3 1.0   | ALLINIAL                       | + 17 0 4 17 0 0 1 10 1 10                |                               | =====                   | ALLUVIAL,<br>BROWN, SILTY SAND |
| 760.0 ±   | ALLUVIAL,                      | 755.0 + 13.0   10   29   48   1.0        | )                             |                         | !+?NI                          |
| 13.6 2 3 2 1.0 ×5-+   SAT.  | TAN-BROWN, SILTY SAND          |  |                               |                         | COARSE SAND AND GRAVEL         |
| 755.0 +   | RESIDUAL,                      | 750.0 + 18.0   59   41   0.8             | 8                             | - 100± x                |                                |
| 18.6 60 0.1   | GRAY, COARSE SAND              |  |                               |                         | WEATHERED ROCK (METADIORITE)   |
| 750.0 +          SPI_REFUSAL_AI   | WEATHERED ROCK (METADIORITE)   | 745.0                                    | = AUGER REFUSA                | XI- XT                  | 3                              |
|   | CRYSTALLINE ROCK (METADIORITE) | 145.0 <u>+</u>                           | ELEVATION 747.                |                         |                                |
|   |                                | <u> </u>                                 | ON CRYSTALLIN                 |                         |                                |
| 745.0 +   |                                | 740.0 ±                                  | METADIORI                     |                         |                                |
|   |                                |  |                               |                         |                                |
| 740.0 +   |                                | 735.0 +                                  |                               |                         |                                |
|   | ·                              | '''                                      |                               |                         |                                |
| 775 0   |                                |  |                               |                         |                                |
| 735.0 ±   |                                | 730.0 +                                  |                               |                         |                                |
| <u> </u>  |                                |  |                               |                         |                                |
| 730.0 +   |                                | 725.0 +                                  |                               |                         |                                |
| <u> </u>  |                                |  |                               |                         |                                |
| 725.0 +   |                                | 720.0 =                                  |                               |                         |                                |
|   |                                | 1 20.0 ±                                 |                               |                         |                                |
| 7000 +  |                                |  |                               |                         |                                |
| 720.0 +   |                                | 715.0 +                                  |                               |                         |                                |
| <u> </u>  |                                |  |                               |                         |                                |
| 715.0 +   |                                | 710.0 ‡                                  |                               |                         |                                |
|   |                                |  |                               |                         |                                |
| 710.0 +   |                                | 705.0                                    |                               |                         |                                |
|   |                                | 705.0 ±                                  |                               |                         |                                |
|   |                                |  |                               |                         |                                |
| 705.0 +   |                                | 700.0 🛨                                  |                               |                         |                                |
|   |                                |  |                               |                         |                                |
| 700.0 +   |                                | 695.0 +                                  |                               |                         |                                |
|   | 1                              | *****                                    |                               | _                       |                                |
| 695 0 <del> </del>  | 1                              |  |                               |                         |                                |
| 695.0 +   |                                | 690.0 🛨                                  |                               | -                       |                                |

|             |                  |                  |         |        | GE<br>—     |         |                |                    | · · · · · · · · · · · · · · · · · · · |          | BOR              |           |          |         |            | SHEET 10 C         |
|-------------|------------------|------------------|---------|--------|-------------|---------|----------------|--------------------|---------------------------------------|----------|------------------|-----------|----------|---------|------------|--------------------|
|             | ROJECT           |                  |         |        |             |         |                | 4128               |                                       | Y GUILF  |                  | G         | GEOL     | OGIST N | I.D. MOH   | S                  |
| <del></del> | ITE DESC         |                  |         |        |             |         |                |                    |                                       |          | Y RD.)OVI        | ER BI     | ULL      | . RUN C | REEK       | GROUND W           |
|             | ORING N          |                  |         |        | BORIN       |         |                |                    |                                       | OFFSE    | <b>T</b> 43′LT   | A         | ALIG     | nment - | L-         | <b>0 HR.</b> 5.5   |
| CO          | OLLAR E          | ELEVA            | TION    |        |             |         |                |                    | 26917′                                |          | EASTI            | <b>VG</b> | 173      | 30269′  |            | 24 HR. 6.0         |
| TO          | OTAL DE          | EPTH             | 15.7'   |        | DRILI       | L MA    | CHINE          | 3 CME-550          |                                       | DRILL ME | THOD H.S.        | AUGE      | ERS      | ,       | HAMMER     | TYPE AUTOMA        |
| ST          | TART DA          | ATE              | /6/0    | )6     |             | CON     | MPLET          | ION DATE           | 1/6/06                                | S S      | URFACE WA'       | CER DE    | EPTH     |         |            | TO ROCK 15.7       |
| E           | ELEV.            |                  | TH BL(  |        |             |         |                | BLOWS<br>25        | PER I                                 |          | SAMPLE<br>NUMBER |           |          |         | SOIL AN    | ND ROCK<br>RIPTION |
|             |                  |                  | 0.0     | 310.   | 3 0.        | 3   1   | •/             |                    |                                       |          |                  | , MO      | <u> </u> | ,       | DESCI      |                    |
| 7           | 767.1 -          | <u> </u>         |         |        |             |         |                |                    |                                       |          |                  |           |          |         |            |                    |
| 1           | 765 <b>.</b> 0 – | <u>+</u> ,       | 3 1     | 1      | 2           | ·       | ╮╽╽╁           | <br>- <del>3</del> |                                       |          |                  | W         | X        |         |            |                    |
| '           |                  | ‡ <sup>∠</sup> • |         |        |             | .   1.0 | ✓     <u>↑</u> |                    |                                       |          | -                | **        |          |         | ∆RTIFI∩!   | AL FILL,           |
|             | -                | ‡                |         |        |             |         |                |                    |                                       |          | _                | _         |          |         |            | ANDY SILT          |
| 70          | 760 <b>.</b> 0 – | <del>†</del> 7.  | 3 1     | .   2  | 2   1       | 1.0     | y∐c            | -3 +               |                                       | -        |                  |           |          |         | DIVOTING O | MIDI JILI          |
|             |                  | <u> </u>         |         |        |             |         |                | \                  |                                       | =====    | _                |           |          | <u></u> |            |                    |
| 71          | 755 O =          | £ .~             | 7 0     | a   _  | ٦ ـ ـ ـ ـ ـ | , .     | <u> </u>       |                    | = -                                   | <u></u>  | ]                |           |          |         | RESI       | DUAL,              |
|             | 755 <b>.</b> 0 – | £ 12.            | .s   2k | 0   2' | 7 3         | /   1.0 | J    -         |                    |                                       | X        | SS-5             | М         | 7/       | ∯ GP    |            | , SILTY SAND       |
|             | _                | <u> </u>         |         |        |             |         |                |                    |                                       |          |                  |           | 7/       | WEAT!   | HERED RO   | CK (METAGABBF      |
| 75          | 750 <b>.</b> 0 – | F                |         |        |             |         | 1 1            | _AUGER_            |                                       | l l      |                  |           |          |         |            |                    |
|             | _                | Ŧ                |         |        |             |         |                | ELEVATION          | 4                                     | E .      |                  |           |          |         |            |                    |
| -           | 745.0            | Ŧ                |         |        |             |         |                | ONTERYS            |                                       | 1        | _                |           |          | :       |            |                    |
| 1           | 745.0 -          | F                |         |        |             |         | -              | KME                | LACABE                                | 3RO)     | -                |           |          |         |            |                    |
|             | -                | Ŧ                |         |        |             |         | -              |                    |                                       |          |                  |           |          |         |            |                    |
| 7           | 740 <b>.</b> 0 – | <del>-</del>     |         |        |             |         |                |                    | = = = =                               | _        | -                |           |          |         |            |                    |
|             | -                | ‡                |         |        |             |         |                |                    |                                       |          | _                |           |          |         |            |                    |
|             |                  | ‡                |         |        |             |         | -              |                    |                                       |          | -                |           |          |         |            |                    |
| 7:          | 735 <b>.</b> 0 – | <b>†</b>         |         |        |             |         | -              |                    |                                       |          |                  |           |          |         |            |                    |
|             |                  | ‡                |         |        |             |         |                |                    |                                       | _        |                  |           |          |         |            |                    |
| 7:          | 730 <b>.</b> 0 – | ‡                |         |        |             |         |                |                    |                                       |          | _                |           |          |         |            |                    |
|             | -                | ‡                |         |        |             |         | -              |                    |                                       |          | -                |           |          |         |            |                    |
|             |                  | ‡                |         | .      |             |         | -              |                    |                                       |          |                  |           |          |         |            |                    |
| '           | 725 <b>.</b> 0 – | $\pm$            |         |        |             |         |                |                    |                                       |          |                  |           |          |         |            |                    |
|             | =                | ŧ                |         |        |             |         |                |                    |                                       |          | -                |           |          |         |            |                    |
| 72          | 720 <b>.</b> 0 – | F                |         |        |             |         | -              |                    |                                       |          |                  |           |          |         |            |                    |
|             | 7                | Ŧ                |         |        |             |         |                |                    |                                       |          |                  |           |          |         |            |                    |
| 7           | 715.0            | <u> </u>         |         |        |             |         |                |                    |                                       |          |                  |           |          |         |            |                    |
| '           |                  | ‡                |         |        | 1           |         |                |                    | <u> </u>                              |          | -                |           |          |         |            |                    |
|             |                  | ‡                |         |        |             |         | -              |                    |                                       |          |                  |           |          |         |            |                    |
| 7           | 710.0            | <del> </del>     |         |        |             |         | -              |                    | = = = =                               |          |                  |           |          |         |            |                    |
|             |                  | _                |         |        |             |         |                |                    |                                       |          |                  |           |          |         |            |                    |
| 7,          | 705 <b>.</b> 0 – | <u> </u>         |         |        |             |         |                |                    |                                       |          | -                |           |          |         |            |                    |
| '           | . 55.0           | <u> </u>         |         |        |             |         | -              | +                  |                                       |          |                  |           |          |         |            |                    |
|             | 3                | <u> </u>         |         |        |             |         |                |                    |                                       |          | 1                |           |          |         |            |                    |
| 70          | 700 <b>.</b> 0 – | <del> -</del>    |         |        |             |         |                |                    |                                       |          | _                |           |          |         |            |                    |
|             | =                | ±                |         |        |             |         |                |                    |                                       |          | -                |           |          |         |            |                    |
|             | 205 A =          | <u> </u>         |         |        |             |         | -              |                    |                                       |          |                  |           |          |         |            |                    |
| 0           | 695 <b>.</b> 0 – | F                |         |        |             |         |                |                    |                                       |          | 7                |           |          |         |            |                    |
|             | -                | F                |         |        |             |         |                |                    |                                       |          |                  |           |          |         |            |                    |
| 1           | ,                |                  | 1       |        |             |         | 1 1            |                    |                                       |          | J 1              | i i       |          | 1       |            |                    |

#### CHEET II OF IC

|           |                  |               | @    | <b>》</b> 医( | OTI   | echi     | NIC  | AL U                           | TIME          | BOR              | IN@ | j  |        | G  |                  |                         |
|-----------|------------------|---------------|------|-------------|-------|----------|--|--------------------------------|---------------|------------------|-----|--|--------|--|------------------|-------------------------|
| PROJECT   | <b>NO.</b> 3     | 348I <b>.</b> | 1.1  |             | ID.   | 3-4128   | (  | OUNTY                          | GUILFOF       | RD.              | G   | EOLO   | GIST   | N.D. MOH                                       | 1S               |                         |
| SITE DESC |                  |               |      |             |       |          | <del></del>                                      |                                | MACKAY        |                  |     |  |        |  |                  | ROUND WATER             |
| BORING N  |                  | 32-B          |      |             | G LOC |          | 24+2   |                                | OFFSET        | 42' RT           |     |  | MENT   | -L-  |                  | HR. N/A                 |
| COLLAR E  |                  |               | 769. |             |       | ORTHING  |  | 826′                           |               | EASTIN           |     |  | 0228′  |  |                  | HR. 9.0'                |
| TOTAL DE  |                  |               |      |             |       | INE CME  |  |                                | RILL METH     |                  |     |  | N1 / A |  |                  | AUTOMATIC               |
| START DA  | DEPTH            |               |      |             |       | LETION D |  | PER FO                         |               | FACE WAT         | T   | 71   | IN/A   |  |                  | OCK 15.7'               |
| ELEV.     | (FT.)            | 1             |      |             | (FT.) |          | 25   |                                |               | SAMPLE<br>NUMBER | моі | . G  |        | SOIL A<br>DESCF                                |                  |                         |
| 769.2 -   |                  |               |      |             |       | 11       | <del>                                     </del> |                                | <del>  </del> |                  |     | X  |        |  |                  |                         |
| 765.0     | 2.8              | 2             | 2    | 1           | 1.0   | X-3      |  |                                |               |                  | M   |  |        | ARTIFION BROWN,                                |                  |                         |
| 760.0     | 7.8              | WOH           | WOH  | 2           | 1.0   | ¥2       |  |                                |               | SS-6             | M 🔻 | Ż  |        |  | SIDUAL           |                         |
| 755.0     | 12.8             | 20            | 54   | 46          | 0.8   |          |  |                                | 100+          |                  | M   |  |        | GREEN-GRAY<br>ATHERED RO                       | CK (M            | Y SAND<br>ETAGABBRO)    |
| 750.0     | -<br>-<br>-      |               |      |             |       |          |  |                                |               |                  |     | STATE OF THE STATE |        | CRYSTAL<br>N-GRAY, HA<br>TO MODER<br>FRACTUREI | RD, FRI<br>ATELY | ESH, CLOSELY<br>CLOSELY |
| 745.0     | -<br>-<br>-      |               |      |             |       |          |  |                                |               |                  |     |  |        | REC=96%<br>WHITE AND<br>ESH, MODER             |                  | HARD,                   |
| 740.0     | -<br>-<br>-<br>- |               |      |             |       | ELEVA    | LION   | RMINAJE<br>742.7 je<br>CLINEJE | EETIN         |                  |     |  | /"     | FRACTURE<br>REC=100%                           | D, MET<br>ROD    | ADIORITE<br>=70%        |
| 735.0     | -<br>-<br>-      |               |      |             |       |          | 1  | DIORITE                        | 1 1           |                  |     |  |        |  |                  |                         |
| 730.0     | <del>-</del>     |               |      |             |       |          |  |                                |               |                  |     |  |        |  |                  |                         |
| 725.0     |                  | ,             |      |             |       |          |  |                                |               |                  |     |  |        |  |                  |                         |
| 720.0     | -<br>-<br>-      |               |      |             |       |          |  |                                |               |                  |     |  |        |  |                  |                         |
| 715.0     | -<br>-<br>-<br>- |               |      |             |       |          |  |                                |               |                  |     |  |        |  |                  |                         |
| 710.0     | -<br><br>        |               |      |             |       |          |  |                                |               |                  |     |  |        |  |                  |                         |
| 705.0     | <br><br>         |               |      |             |       |          |  |                                |               |                  |     |  |        |  |                  |                         |
| 700.0     | -<br><br>        |               |      |             |       |          |  |                                |               |                  |     |  |        |  |                  |                         |
| 695.0     | -<br>-<br><br>-  |               |      |             |       |          |  |                                |               |                  |     |  |        |  |                  |                         |
| 690.0     | -<br>-<br>       |               |      | ,           |       |          |  |                                |               |                  |     |  |        |  |                  |                         |

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

|                |              |                  |        |             |             |                  |   |                          | SHEET    OF 16                         |
|----------------|--------------|------------------|--------|-------------|-------------|------------------|---|--------------------------|--|
|                |              |                  |        |             |             | C                | ORE BORING REPORT                                       |                          |  |
| PRO            | DJECT:       | 33481.           | 1.1    | ID          | :B-4        | 128              | COUNTY: Guilford  |                          | BORING NO: EB2-B                       |
| DES            | SCRIPTI      | ON: Bri          | dge No | o. 73 or    | n -L- (SI   | R 1549, M        | ackay Rd.)over Bull Run Creek                           |                          |  |
| LOC            | NOITA        | OF BORII         | NG:    | -L- St      | ation 24    | l+25, 42' F      | RT  | COMPL                    | ETION DATE: 1/10/2006                  |
| COL            | LAR or       | GROUND           | ELE\   | /ATION      | :769        | .2_ft            | CORE SIZE: NXWL   | GEOLOGIST:               | N. D. Mohs                             |
| COF            | RE EQU       | IPMENT:          |        |             | СМЕ         | -550, Cas        | sing with advancer                                      | DRILLER:                 | H. R. Conley                           |
| E1 E\/         | DEPTH        | DRILL            | RUN    | REC         | RQD         | 00000            |   | ,                        |  |
| (ft)           | (ft)         | (min/ft)         | (ft)   | (ft)<br>(%) | (ft)<br>(%) | SAMPLE<br>NUMBER |   | ICATION and REMAR        |  |
| 753.1          | 16.1         | 1:32<br>1:21     |        | 3.4         | 2.1         |                  | Crystalline rock, green-gray, hard, fresh, closely to r | moderately closely frac  | tured, Metagabbro.                     |
|                |              | 1:19<br>:20/0.4' | 3.4    | (100%)      | (62%)       |                  |   |                          |  |
| 749.7<br>749.7 | 19.5<br>19.5 | 1:20             |        |             |             |                  | Crystalline rock, green-gray, hard, fresh, closely to n | noderately closely frac  | tured, Metagabbro.                     |
|                |              | 1:07<br>1:03     | 5.0    | 4.6         | 3.9         |                  | \$  |                          |  |
| 744.7          | 24.5         | 1:30<br>1:21     |        | (92%)       | (78%)       |                  |   |                          |  |
| 744.7          | 24.5         | 1:44<br>1:40     |        | 2.0         | 1,4         |                  | Crystalline rock, white and black, hard, fresh, moder   | ately closely fractured, | Metadiorite.                           |
|                |              |                  | 2.0    | (100%)      |             |                  |   |                          |  |
| 742.7          | 26.5         |                  |        | (           | (( 0 / 0 /  |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          | ************************************** |
|                |              |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          |  |
|                | -            |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          |  |
|                | . [          |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  |   |                          | ·                                      |
|                |              |                  |        |             |             |                  |   |                          |  |
|                | -            |                  |        |             |             |                  |   |                          |  |
| l              | F            |                  |        |             |             |                  |   |                          |  |
|                |              |                  |        |             |             |                  | BOREHOLE TERMINATED AT ELEVATION OF                     | 742.7 FEET, IN ROCK      | <                                      |

GEOTECHNICAL UNIT BORING LOG

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION NORTH CAROLINA DEPARTMENT OF TRANSPORTATION GEOTECHNICAL UNIT BORING LOG **SHEET** 12 **OF** 16

| PROJECT NO. 33481.1.1 ID.               | B-4I28 <b>COUNTY</b> GUILFOI   | RD <b>GROLOG</b> I   | ST N.D. MOHS                                    | PROJECT NO.    | 33481.1.1   | ID.            | B-4I28 C0  | UNTY GUILFO                     | RD GFOLO              | OGIST J.I. MILKOVITS              |
|---|--|--|---|----------------|-------------|----------------|--|---------------------------------|-----------------------|-----------------------------------|
|   | 3 ON -L- (SR 1549, MACKAY  | The state of the s |   |                |             |                |  |                                 | RD.)OVER BULL         |                                   |
| BORING NO. DET-I BORING LOC             |  |  |   | BORING NO.     |             | BORING LOC     |  |                                 |                       | WENT -DET- 0 HR. DRY              |
|   | NORTHING 826919'   | EASTING 1730   |   | COLLAR ELEV    | <del></del> | <del></del>    | NORTHING 8269                                    |                                 |                       | 50274′ 24 HR. 4.5′                |
|   |  | HOD H.S. AUGERS  | HAMMER TYPE AUTOMATIC                           | TOTAL DEPTH    |             | <del>. ,</del> | HINE CME-550                                     |                                 | HOD H.S. AUGERS       |                                   |
|   | The state of the s | RFACE WATER DEPTH  |   | START DATE     |             |                | PLETION DATE 3/                                  |                                 |                       |                                   |
| DEPTH BLOW COUNT PEN.                   |  | T 7. 1   |   |                |             | COUNT PEN      |  |                                 | RFACE WATER DEPTH     |                                   |
| ELEV. (FT.) 0.5/0.5/0.5 (FT.)           |  | SAMPLE NUMBER MOI. G   | SOIL AND ROCK<br>DESCRIPTION                    | 1 F 1 F 1/ 1   |             | 0.5/0.5 (FT.   |  |                                 | SAMPLE ONUMBER MOI. G | SOIL AND ROCK<br>DESCRIPTION      |
| 763.1 0.0 1 0 1 1.0                     |  |  | ALLUVIAL,                                       | 1 =            |             |                |  |                                 |                       |                                   |
| 760.0 + 3.2   2   2   3   1.0           | <del>                                  </del>  | SS-9 <u>\$</u>   | ORANGE-TAN, SANDY SILT                          | 765.6          |             |                |  |                                 |                       | 3                                 |
| 5.7 3 12 17 1.0                         | 1171-5-11  |  | TAN, SILTY SAND                                 |                | 3.9 4       | 4 2 1.0        |  |                                 |                       |                                   |
| 755.0 + 8.2   18   79   21   0.6        |  | SS-IO S  | RESIDUAL,<br>GREEN-GRAY, COARSE SAND AND GRAVEL | 760.0 +        | 3.9   4     | 4   2   1.0    |  |                                 | SS-∥ M ▼              | ARTIFICIAL FILL, GRAY, SILTY SAND |
| 10.7 100 10.3                           | 1     - 100 +7   |  | WEATHERED ROCK (METADIORITE)                    |                | 001         | 4 80 1.0       |  |                                 |                       |                                   |
| 750.0 + 13.2   2   11   89   0.9        |  |  | RESIDUAL,                                       | 755.0 +        | 8.9 4       | 4   80   1.0   |  | <u></u> x84                     | M 🕌                   | RESIDUAL, GRAY, SILTY SAND        |
| 1                                       |  |  | GREEN-GRAY, SILTY SAND                          | =              |             |                | <del>                                     </del> |                                 |                       | RESIDUAL, GRAT, SILTT SAND        |
| 745.0 +                                 |  |  | WEATHERED ROCK (METADIORITE)                    | 750.0 +        |             |                | - AUGER- REF                                     | USAL-AT                         |                       |                                   |
| + + + + + + - + - + - + - + - + - + - + |  |  |   | +              |             |                | ĒLĒVĀĪIŌN =                                      | 153.5 # EE-1  <br>L'LINE ROCK - |                       |                                   |
| 740.0 ‡                                 | TAUGER REFUSAL AT T  |  |   | 745.0 ‡        |             |                | METAD  |                                 |                       |                                   |
| 140.00                                  | LECEVATION 743.2 FEET. ON CRYSTALLINE ROCK   |  |   | 143.0          |             |                |  |                                 |                       |                                   |
| 735.0 +                                 | (METADIORITE)  |  |   | 740.0          |             |                |  |                                 |                       |                                   |
| 133.0 +                                 |  |  |   | 140.0 <u>T</u> |             |                |  |                                 |                       |                                   |
|   |  |  |   |                |             |                |  |                                 |                       |                                   |
| 730.0 +                                 |  |  |   | 735.0 +        |             |                |  |                                 |                       |                                   |
|   |  |  |   | ‡              |             |                |  |                                 |                       |                                   |
| 725.0 +                                 |  |  |   | 730.0 ‡        |             |                |  |                                 |                       |                                   |
|   |  |  |   | ‡              |             |                |  |                                 |                       |                                   |
| 1700 0 ‡                                |  |  |   | 1 +            |             |                |  |                                 |                       |                                   |
| 720.0 +                                 |  |  |   | 725.0 +        |             |                |  |                                 |                       |                                   |
|   |  |  |   | ‡              |             |                |  |                                 |                       |                                   |
| 715.0 +                                 |  |  |   | 720.0 +        |             |                |  |                                 |                       |                                   |
|   |  |  |   | 1 1            |             |                |  |                                 |                       |                                   |
| 1 1 1 1                                 |  |  |   | +              |             |                |  |                                 |                       |                                   |
| 710.0 +                                 |  |  |   | 715.0 —        |             |                |  |                                 |                       |                                   |
|   |  |  |   | 1 ‡            |             |                |  |                                 |                       |                                   |
|   |  |  |   | l ±            |             |                |  | <del> </del>                    |                       |                                   |
| 705.0 +                                 | + + +  |  |   | 710.0 —        |             |                |  |                                 |                       |                                   |
|   |  |  |   |                |             |                |  |                                 |                       |                                   |
|   |  |  |   | 1 +            |             |                | 11   | ++                              |                       |                                   |
| 700.0 +                                 |  |  |   | 705.0 +        |             |                |  |                                 |                       |                                   |
|   |  |  |   | 1              |             |                |  |                                 |                       |                                   |
| 1 1 1 1                                 |  |  |   | 1 +            |             |                |  |                                 |                       |                                   |
| 695.0 —                                 |  |  |   | 700.0 🛨        |             |                |  |                                 |                       |                                   |
|   |  |  |   | 1 ‡            |             |                |  | t                               |                       |                                   |
|   |  |  |   | 1 +            |             |                |  |                                 |                       |                                   |
| 690.0 —                                 |  |  |   | 695.0 +        |             |                |  | T                               |                       |                                   |
|   |  |  |   | 1 1            |             |                |  | 1                               |                       |                                   |
|   | 11===-   |  |   | 1 +            |             |                |  |                                 |                       |                                   |
| 685.0 +                                 |  |  |   | 690.0 +        |             |                |  | T                               |                       |                                   |
|   |  |  |   | '              |             |                |  |                                 |                       |                                   |

PROJ. NO. - 33481.1.1 ID NO. - B-4128 COUNTY - GUILFORD

SHEET 13 OF 16

| EB1-A  |        |         |          |          |      |      |        |        |        |      |       |         |         |          |         |
|--------|--------|---------|----------|----------|------|------|--------|--------|--------|------|-------|---------|---------|----------|---------|
|        |        |         | S        | OIL 7    | TE.  | ST   | RE     | SUL    | TS     |      |       |         |         |          |         |
| SAMPLE |        |         | DEPTH    | AASHTO   |      |      |        | % BY W | /EIGHT |      | % PAS | SING (S | (SIEVES | %        | %       |
| NO.    | OFFSET | STATION | INTERVAL | CLASS.   | L.L. | P.I. | C.SAND | F.SAND | SILT   | CLAY | 10    | 40      | 200     | MOISTURE | ORGANIC |
| SS-3   | 19 LT  | 23+73   | 3.6-5.1  | A-7-6(6) | 41   | 16   | 26.1   | 19.0   | 30.6   | 24.3 | 92    | 76      | 54      | -        | -       |
| SS-4   | 19 LT  | 23+73   | 8.6-10.1 | A-2-4(0) | 21   | NP   | 54.7   | 30.7   | 8.6    | 6.1  | 91    | 66      | 15      | -        | -       |

EB1-B

|        |        |         | S         | OIL T    | TE   | ST   | RE     | SUL    | LTS  |      |    |    |     |          |         |
|--------|--------|---------|-----------|----------|------|------|--------|--------|------|------|----|----|-----|----------|---------|
| SAMPLE |        |         |           |          |      |      |        |        |      |      |    |    |     |          |         |
| NO.    | OFFSET | STATION | INTERVAL  | CLASS.   | L.L. | P.I. | C.SAND | F.SAND | SILT | CLAY | 10 | 40 | 200 | MOISTURE | ORGANIC |
| SS-1   | 42 RT  | 23+29   | 3.0-4.5   | A-2-6(1) | 36   | 14   | 32.6   | 20.9   | 26.3 | 20.2 | 64 | 49 | 32  | -        | -       |
| SS-2   | 42 RT  | 23+29   | 13.0-14.5 | A-1-B(0) | 22   | NP   | 56.5   | 24.3   | 17.2 | 2.0  | 63 | 37 | 14  | -        | -       |

EB2-A

|        |        |         | S         | OIL T    | TE.  | ST   | RE     | SUI    | LTS    |      |       |         |         |          |         |
|--------|--------|---------|-----------|----------|------|------|--------|--------|--------|------|-------|---------|---------|----------|---------|
| SAMPLE |        |         | DEPTH     | AASHTO   |      |      |        | % BY V | VEIGHT |      | % PAS | SING (S | SIEVES) | %        | %       |
| NO.    | OFFSET | STATION | INTERVAL  | CLASS.   | L.L. | P.I. | C.SAND | F.SAND | SILT   | CLAY | 10    | 40      | 200     | MOISTURE | ORGANIC |
| SS-5   | 43 LT  | 24+76   | 12.3-13.8 | A-2-4(0) | 22   | NP   | 53.8   | 22.5   | 23.7   | 0.0  | 100   | 61      | 28      | -        | -       |

EB2-B

|        |        |         | S        | OIL T  | TE.  | ST   | RE     | SUL    | LTS    |      |       |         |        |          |         |
|--------|--------|---------|----------|--------|------|------|--------|--------|--------|------|-------|---------|--------|----------|---------|
| SAMPLE |        |         | DEPTH    | AASHTO |      |      |        | % BY W | /EIGHT |      | % PAS | SING (S | IEVES) | %        | %       |
| NO.    | OFFSET | STATION | INTERVAL | CLASS. | L.L. | P.I. | C.SAND | F.SAND | SILT   | CLAY | 10    | 40      | 200    | MOISTURE | ORGANIC |
| SS-6   | 42 RT  | 24+25   | 7.8-9.3  | A-4(1) | 28   | 9    | 28.1   | 24.5   | 27.1   | 20.2 | 93    | 76      | 48     | -        |         |

DET-1

| <i>DUI-</i> 1     |        |         |          |          |      |      |        |        |        |      |       |         |        |          |         |
|-------------------|--------|---------|----------|----------|------|------|--------|--------|--------|------|-------|---------|--------|----------|---------|
| SOIL TEST RESULTS |        |         |          |          |      |      |        |        |        |      |       |         |        |          |         |
| SAMPLE            |        |         | DEPTH    | AASHTO   |      |      |        | % BY W | /EIGHT |      | % PAS | SING (S | IEVES) | %        | %       |
| NO.               | OFFSET | STATION | INTERVAL | CLASS.   | L.L. | P.I. | C.SAND | F.SAND | SILT   | CLAY | 10    | 40      | 200    | MOISTURE | ORGANIC |
| SS-8              | 3 RT   | 24+00   | 0.0+1.5  | A-4(2)   | 26   | 9    | 26.9   | 26.1   | 26.7   | 20.2 | 100   | 87      | 50     | -        | •       |
| SS-9              | 3 RT   | 24+00   | 3.2-4.7  | A-2-4(0) | 20   | 1    | 59.1   | 19.9   | 10.8   | 10.1 | 95    | 55      | 22     | -        | -       |
| SS-10             | 3 RT   | 24+00   | 6.2-7.2  | A-1-B(0) | 20   | 4    | 55.5   | 22.1   | 16.4   | 6.1  | 54    | 32      | 14     | -        | •       |

DET-2

| SOIL TEST RESULTS |        |         |          |          |      |      |             |        |      |      |                    |    |     |          |         |
|-------------------|--------|---------|----------|----------|------|------|-------------|--------|------|------|--------------------|----|-----|----------|---------|
| SAMPLE            |        |         | DEPTH    | AASHTO   |      |      | % BY WEIGHT |        |      |      | % PASSING (SIEVES) |    |     | %        | %       |
| NO.               | OFFSET | STATION | INTERVAL | CLASS.   | L.L. | P.I. | C.SAND      | F.SAND | SILT | CLAY | 10                 | 40 | 200 | MOISTURE | ORGANIC |
| SS-11             | CL     | 24+93   | 3.9-5.4  | A-2-4(0) | 21   | NP   | 43.3        | 36.2   | 8.5  | 12.1 | 93                 | 73 | 22  | •        | -       |



# FIELD SCOUR REPORT

| WBS:                              | 33481.1.1 TIP:                   | B-4128 COUNTY: Guilford                                |        |  |  |  |  |  |
|-----------------------------------|----------------------------------|--|--------|--|--|--|--|--|
| DESCRIPTION(1): B                 | 3ridge No. 73 on -L- (SR 1       | 1549, Mackay Rd.) over Bull Run Creek                  |        |  |  |  |  |  |
| EXISTING BRIDGE                   |                                  |  |        |  |  |  |  |  |
| Information from:                 | Field Inspection Other (explain) | X Microfilm (reel pos:)                                |        |  |  |  |  |  |
|                                   |                                  | Total Bents: 2 Bents in Channel: 0 Bents in Floodplain | n: _ 2 |  |  |  |  |  |
| EVIDENCE OF SO<br>Abutments or En | nd Bent Slopes: None.            |  |        |  |  |  |  |  |
| Interior Bents: N                 | N/A                              |  |        |  |  |  |  |  |
| Channel Bed: N                    | None.                            |  |        |  |  |  |  |  |
| Channel Bank: N                   | None.                            |  |        |  |  |  |  |  |
| EXISTING SCOUF                    |                                  |  |        |  |  |  |  |  |
| Type(3): R                        | tip Rap.                         |  |        |  |  |  |  |  |
| Extent(4): N                      | ninor along channel banks        | in front of wingwalls.                                 |        |  |  |  |  |  |
| Effectiveness(5): E               | :ffective.                       |  |        |  |  |  |  |  |
| Obstructions(6): N                | lone.                            |  |        |  |  |  |  |  |

#### **INSTRUCTIONS**

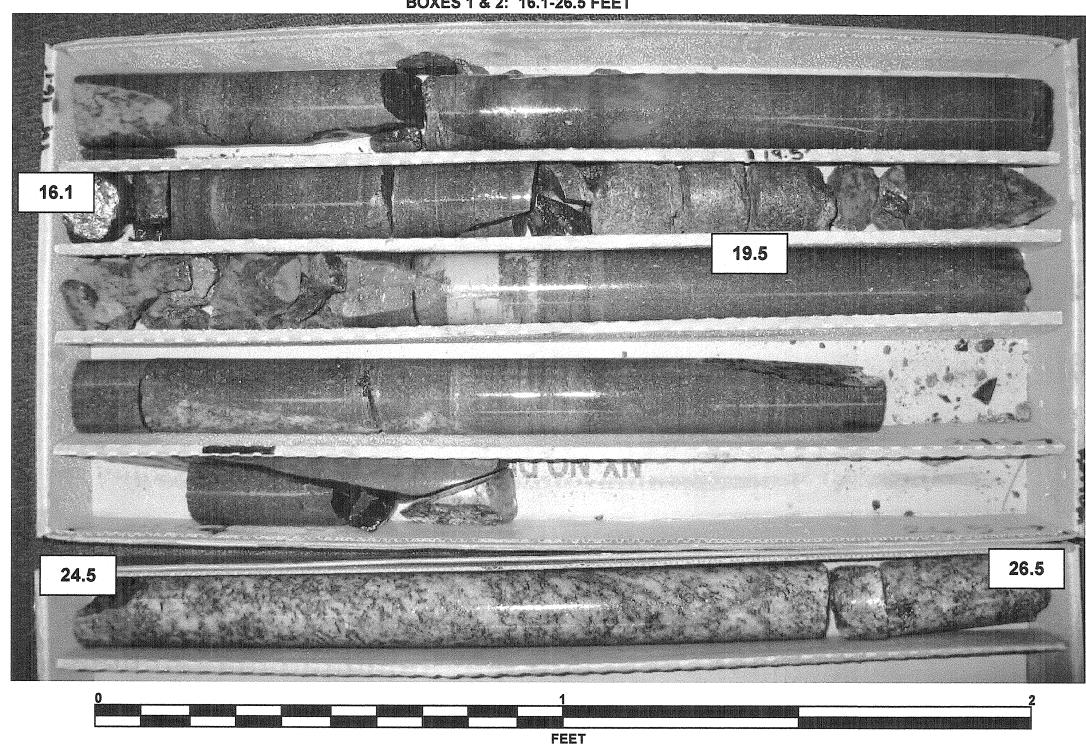
- 1 Describe the specific site's location, including route number and body of water crossed.
- 2 Note scour evidence at existing end bents or abutments (e.g. undermining, sloughing, degradations).
- 3 Note existing scour protection (e.g. rip rap).
- 4 Describe extent of existing scour protection.
- 5 Describe whether or not the scour protection appears to be working.
- 6 Note obstructions such as dams, fallen trees, debris at bents, etc.
- 7 Describe the channel bed material based on observation and/or samples. Include any lab results with report.
- 8 Describe the channel bank material based on observation and/or samples. Include any lab results with report.
- 9 Describe the material covering the banks (e.g. grass, trees, rip rap, none).
- 10 Determine the approximate floodplain width from field observation or a topographic map.
- 11 Describe the material covering the floodplain (e.g. grass, trees, crops).
- 12 Use professional judgement to specify if the stream is degrading, aggrading, or static.
- 13 Describe potential and direction of the stream to migrate laterally during the bridge's life (approx. 100 years).
- Give the geotechnically adjusted scour elevation (GASE) expected over the life of the bridge (approx. 100 years). This elevation can be given as a range across the site, or for each bent. Discuss the relationship between the Hydraulics Unit theoritical scour and the GASE. If the GASE is dependent on scour counter measures, explain (e.g. rip rap armoring on slopes). The GASE is based on the erodability of materials, giving consideration to the influence of joints, foliation, bedding characteristics, % core recovery, % RQD, differential weathering, shear strength, observations at existing structures, other tests deemed appropriate, and overall geologic conditions at the site.

|                 |                    |   | DESIGN INFO  | RMATION   |  |          |  |  |  |  |  |  |
|-----------------|--------------------|---|--|-----------|--|----------|--|--|--|--|--|--|
| Channel         | Bed Mater          | ial(7): Sand, gra   | Sand, gravel, and boulders.  |           |  |          |  |  |  |  |  |  |
|                 |                    |   |  |           |  |          |  |  |  |  |  |  |
| Channel F       | Pank Matar         | ial(8): Sand.   | Cond   |           |  |          |  |  |  |  |  |  |
| Chamere         | Dalik Malei        | iai(6). <u>Saiiu.</u>   |  |           |  |          |  |  |  |  |  |  |
|                 |                    | WHERE THE PROPERTY OF STATE AND AND AND ADDRESS AND |  |           |  |          |  | Proceedings of the Committee of Andrews  |  |  |  |  |
| Channe          | l Bank Cov         | rer(9): Trees, sh   | Trees, shrubs, and vines.  |           |  |          |  |  |  |  |  |  |
| Flood           | المامنية ١٨/١ماليا | -(10). Ai   |  |           |  |          |  |  |  |  |  |  |
| F1000           | ipiain vvidti      | n(10): Approxim   | Approximately 150'   |           |  |          |  |  |  |  |  |  |
| Flood           | lplain Cove        | r(11): Trees, sh  | Tagge about a surface and according to the su |           |  |          |  |  |  |  |  |  |
|                 |                    |   | rees, snrubs, and grass.   |           |  |          |  |  |  |  |  |  |
|                 | Stream is          | s(12): Agg  | rading [   | Degrading | X  | Static   |  |  |  |  |  |  |
| hannel Migratio | n Tendenc          | v(13): West   |  |           |  |          |  |  |  |  |  |  |
| name mgratio    | ir rendene,        | y(10). vvest.   |  |           |  |          |  |  |  |  |  |  |
| Observations a  | and Other (        | Comments:   |  |           |  |          |  |  |  |  |  |  |
|                 |                    |   |  |           |  |          |  |  |  |  |  |  |
|                 |                    |   |  |           |  |          |  |  |  |  |  |  |
| GEOTECHNIC      | :ΔΙΙΥΔΠ.           | IUSTED SCOU   | ELEVATIONS(14)   | Feet      |  | Meters   |  |  |  |  |  |  |
| 02012011110     | ALL! AD            | 00125 0000.   | LEEVATIONO(14)   | 1 661     | **************************************   | IVICIOIS |  |  |  |  |  |  |
|                 | BI                 | <u>ENTS</u>   |  |           |  |          |  |  |  |  |  |  |
|                 | ·                  | B1 B2   | B3 B4  |           |  |          |  |  |  |  |  |  |
|                 | anes, Lt           |   |  |           |  |          |  |  |  |  |  |  |
|                 | anes, Rt           |   |  |           |  |          |  | NAMES ASSESSED AS A PROCESSOR OF THE PARTY O |  |  |  |  |
|                 | anes, Lt           |   |  |           |  |          |  |  |  |  |  |  |
| NB La           | anes, Rt           |   |  |           |  |          |  |  |  |  |  |  |
|                 |                    |   |  |           |  |          |  | MENTION TO A ST. ST. ST. SALES   |  |  |  |  |
|                 | L.                 |   |  | <u> </u>  |  |          |  |  |  |  |  |  |
| Comparison of   | GASE to I          | Hydraulics Unit t   | poorotical accur-  |           |  |          |  |  |  |  |  |  |
| Companson of    | GASE 10 1          | Tyuraunos Orne u  | leoretical scour.  |           |  |          |  |  |  |  |  |  |
|                 |                    |   |  |           |  |          |  |  |  |  |  |  |
|                 |                    |   |  |           |  |          |  |  |  |  |  |  |
| SOIL ANALYS     | SIS RESUL          | TS FROM CHA   | NNEL BED AND BA  | NK MATER  | IAL  |          |  |  |  |  |  |  |
| Bed or Bank     | Bank               | Bed   |  |           |  |          |  |  |  |  |  |  |
| Sample No.      | SS-8               | SS-4  |  |           |  |          |  | THE RESIDENCE OF A STREET STATE OF THE STREET  |  |  |  |  |
| Retained #4     |                    |   |  |           | MATERIA PROPERTY CONTROL OF THE STATE OF THE |          |  |  |  |  |  |  |
| Passed #10      | 100                | 91  | The Control of the Co |           | THE RESERVE OF THE PARTY OF THE |          |  |  |  |  |  |  |
| Passed #40      | 87                 | 66  |  |           |  |          |  |  |  |  |  |  |
| Passed #200     | 50                 | 15  |  |           |  |          |  |  |  |  |  |  |
| Coarse Sand     | 26.9               | 54.7  |  |           |  |          |  | The second of th |  |  |  |  |
| Fine Sand       | 26.1               | 30.7  |  |           |  |          |  |  |  |  |  |  |
| Silt            | 26.7               | 8.6   |  |           |  |          |  | PROPERTY AND ADDRESS.  |  |  |  |  |
| Clay            | 20.2               | 6.1   |  |           |  |          |  | Address and the construction of the states   |  |  |  |  |
| LĹ              | 26                 | 21  |  |           |  |          |  | ARREST CO. ACC. COMM. COMM.  |  |  |  |  |
| PI              | 9                  | NP  |  |           |  |          |  | and the later than th |  |  |  |  |
| AASHTO          | A-4(2)             | A-2-4(0)  | MANAGEMENT TO THE PROPERTY OF  |           |  |          |  |  |  |  |  |  |
| Station         | 24+25              | 23+29   | AMPRICA CONTRACTOR CON |           |  |          |  |  |  |  |  |  |
| Offset          | 3 RT               | 19 LT   | ****   |           |  |          |  |  |  |  |  |  |
| Depth           | 0.0'-1.5'          |   |  |           |  |          |  |  |  |  |  |  |

| Reported by: | attu  | Mh      | Date: | 1/9/2006 |
|--------------|-------|---------|-------|----------|
|              | Natha | in Mohs |       |          |

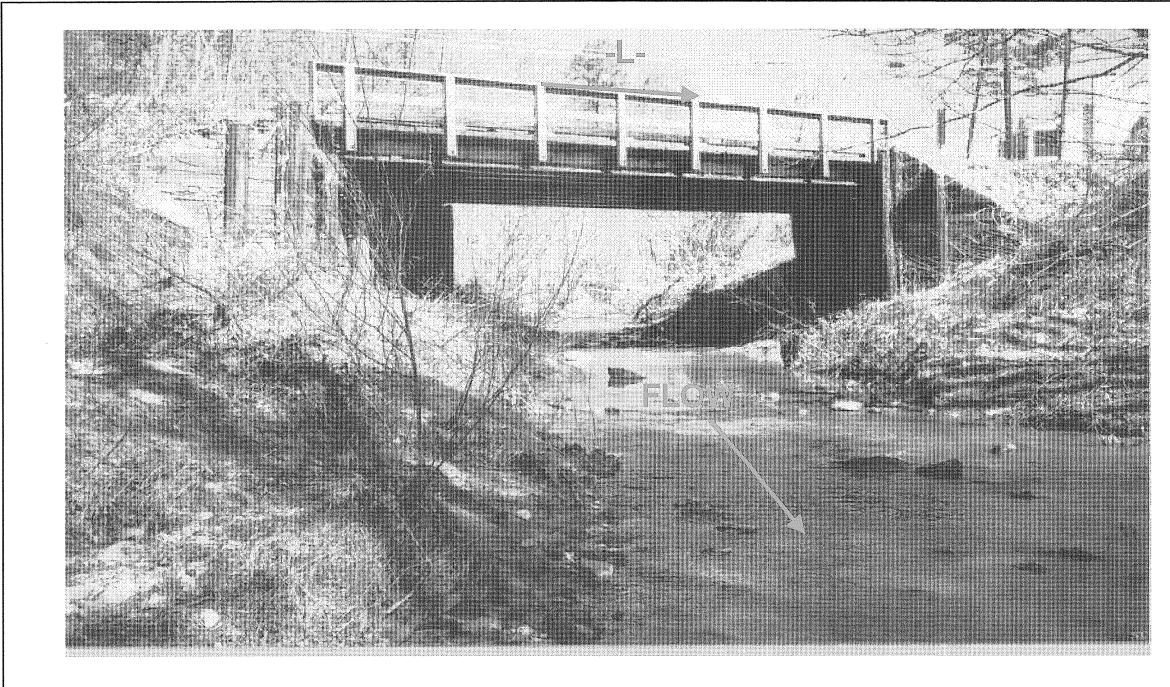
# **CORE PHOTOGRAPHS** EB2-B

BOXES 1 & 2: 16.1-26.5 FEET



SITE PHOTO

BRIDGE NO. 73 OVER BULL RUN CREEK ON SR 1549 (MACKAY RD.)



LOOKING NORTH