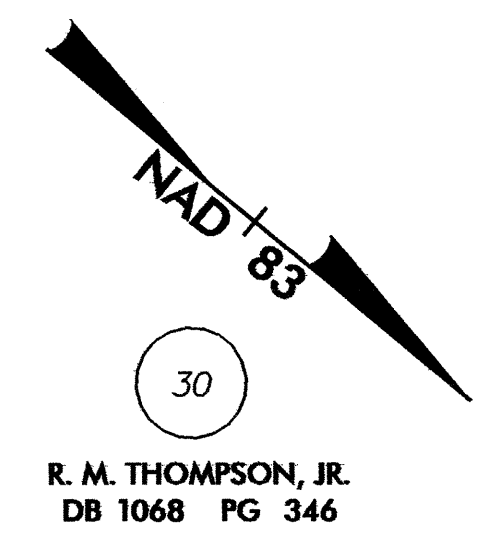
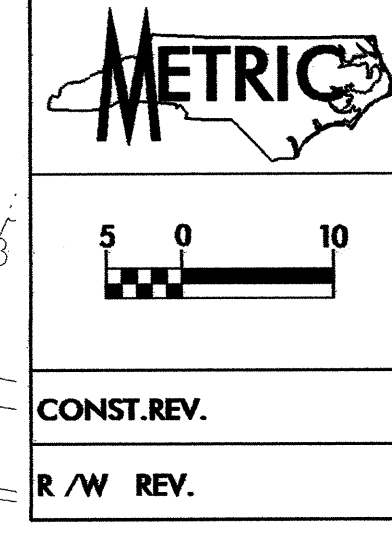


PROJECT REFERENCE NO. R-2206C		SHEET NO. EC-54/CONST.15
R/W SHEET NO.		HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER		
CONST. REV.		
R/W REV.		



SEE SHEETS S-X THRU S-XX
FOR STRUCTURE PLANS

--- L- & -Y11- SLOPE STAKES
--- Y11DET- SLOPE STAKES

30
R. M. THOMPSON, JR.
DB 1068 PG 346

-Y13-
PI Sta 10+87.019
 $\Delta = 6^\circ 50' 18.0''$ (RT)
L = 59.676
T = 29.873
R = 500.000
e = 0.04
RO = 30m

-Y13- POT STA.10+00.000 =
-Y13DET- POT STA.10+00.000

-BY13- 380
-Y13- STA.10+03.035
15.433 (RT)

**7 x 3 x 1
1.5 weir**

10 x 5 x 1

6 x 2 x 1

9 x 4 x 1

**4 x 2 x 1
1.5 weir**

**6 x 3 x 1
1.5 weir**

**6 x 3 x 1
1.5 weir**

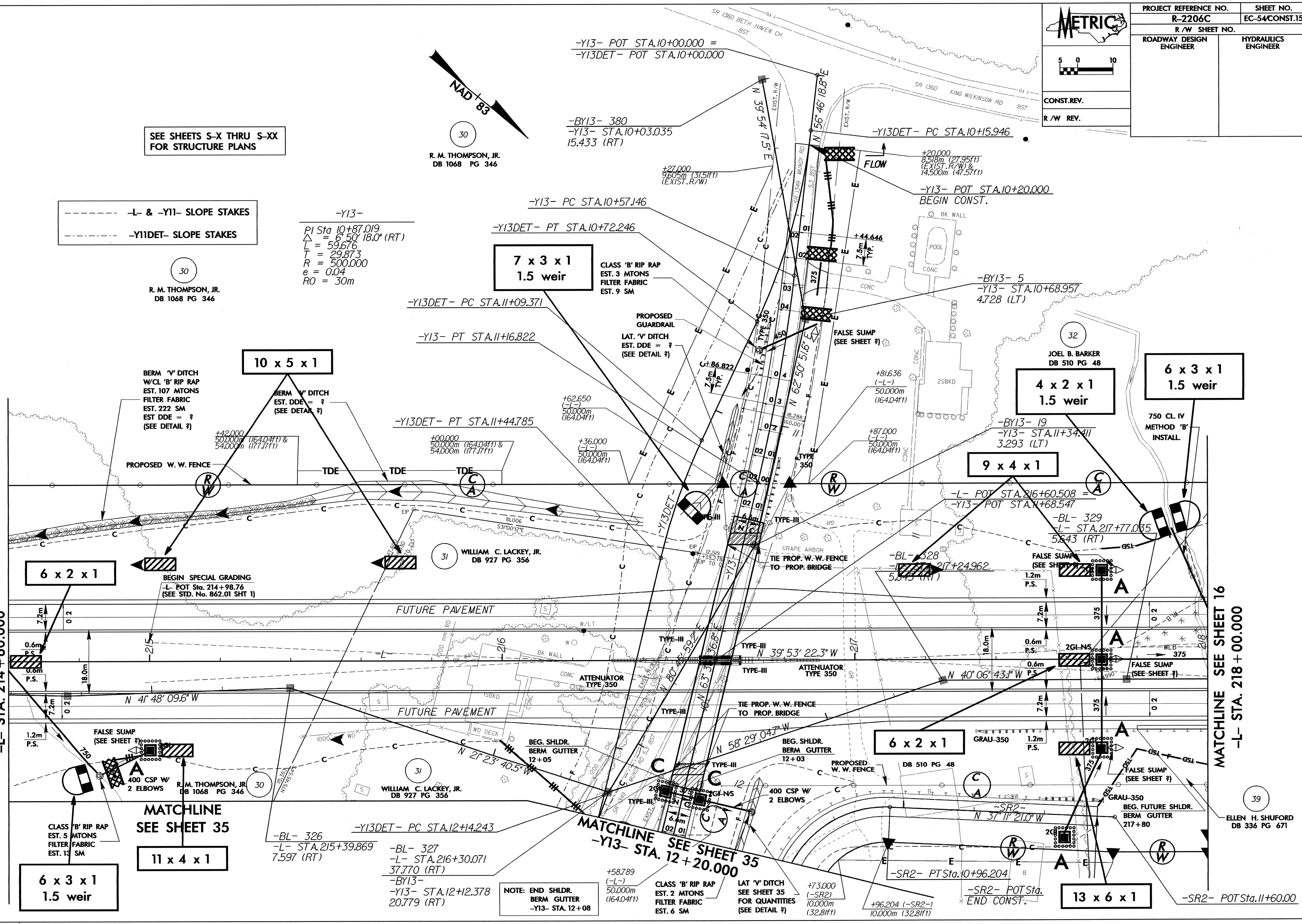
11 x 4 x 1

6 x 2 x 1

13 x 6 x 1

MATCHLINE SEE SHEET 14
-L- STA. 214 + 60.000

MATCHLINE SEE SHEET 16
-L- STA. 218 + 00.000



NOTE: END SHLDR.
BERM GUTTER
-Y13- STA. 12 + 08

CLASS 'B' RIP RAP
EST. 2 MTONS
FILTER FABRIC
EST. 6 SM

LAT 'V' DITCH
SEE SHEET 35
FOR QUANTITIES
(SEE DETAIL ?)

-SR2- POT Sta.
END CONST.

-BL- 326
-L- STA. 215 + 39.869
7.597 (RT)

-BL- 327
-L- STA. 216 + 30.071
37.770 (RT)

-BY13-
-Y13- STA. 12 + 12.378
20.779 (RT)

-L- POT STA. 216 + 60.508 =
-Y13- POT STA. N + 68.547

-BL- 329
-L- STA. 217 + 77.065
5.643 (RT)

-BL- 328
-L- STA. 217 + 24.962
5.875 (RT)

-BY13- 5
-Y13- STA. 10 + 68.957
4.728 (LT)

-Y13- POT STA. 10 + 20.000
BEGIN CONST.

-Y13DET- PC STA. 10 + 15.946

-Y13DET- PT STA. 10 + 72.246

-Y13- PC STA. 10 + 57.146

-Y13DET- PC STA. 11 + 09.371

-Y13- PT STA. 11 + 16.822

-Y13DET- PT STA. 11 + 44.785

MATCHLINE SEE SHEET 35
-Y13- STA. 12 + 20.000

-Y13DET- PC STA. 12 + 14.243

-BL- 327
-L- STA. 216 + 30.071
37.770 (RT)

-BL- 326
-L- STA. 215 + 39.869
7.597 (RT)

39
ELLEN H. SHUFORD
DB 336 PG 671

32
JOEL B. BARKER
DB 510 PG 48

31
WILLIAM C. LACKY, JR.
DB 927 PG 356

30
R. M. THOMPSON, JR.
DB 1068 PG 346

30
R. M. THOMPSON, JR.
DB 1068 PG 346

30
R. M. THOMPSON, JR.
DB 1068 PG 346

31
WILLIAM C. LACKY, JR.
DB 927 PG 356

DB 510 PG 48

0.6m P.S.

0.6m P.S.

0.6m P.S.

1.2m P.S.

0.6m P.S.

0.6m P.S.

0.6m P.S.

0.6m P.S.

0.6m P.S.

0.6m P.S.

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2

0.2