

PROJECT: 48390

REFERENCE: B-6047

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STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

STRUCTURE

SUBSURFACE INVESTIGATION

COUNTY RUTHERFORD

PROJECT DESCRIPTION REPLACE BRIDGE NO.145

OVER FLOYDS CREEK ON SR 2125 (HARRIS

HENRIETTA ROAD)

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	B-6047	1	15

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT, AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

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PERSONNEL

J. KARDON

J. FREGOSI

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TRIGON EXPLORATION

INVESTIGATED BY J. KARDON

DRAWN BY T. WELLS

CHECKED BY X. BARRETT

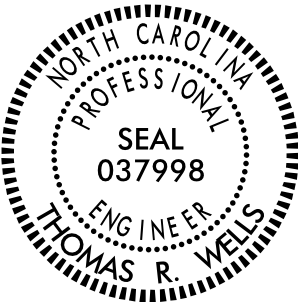
SUBMITTED BY KLEINFELDER, INC.

DATE FEBRUARY 2023

Prepared in the Office of:



KLEINFELDER
Bright People. Right Solutions.
422 GALLIMORE DAIRY ROAD, SUITE B
GREENSBORO, NORTH CAROLINA 27409
NC ENGINEERING FIRM LICENSE NO. F-1312



DocuSigned by:

Thomas R. Wells02/13/2023

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DATE

DOCUMENT NOT CONSIDERED FINAL
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NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION

SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, *VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6*

SOIL LEGEND AND AASHTO CLASSIFICATION

GENERAL CLASS.	GRANULAR MATERIALS (≤ 35% PASSING #200)						SILT-CLAY MATERIALS (> 35% PASSING #200)						ORGANIC MATERIALS		
GROUP CLASS.	A-1	A-3	A-2		A-2		A-4	A-5	A-6	A-7	A-1, A-2	A-3	A-4, A-5	A-6, A-7	
SYMBOL															
% PASSING #10 #40 #200	50 MX 30 MX 15 MX	50 MX 25 MX 10 MX	51 MN 35 MX 35 MX	35 MX 35 MX	35 MX 35 MX	35 MX 36 MN	36 MN 36 MN	36 MN 36 MN	36 MN 36 MN						
MATERIAL PASSING #40 LL PI	— 6 MX	— NP	40 MX 10 MX	41 MN 10 MX	40 MX 11 MN	41 MN 11 MN	40 MX 10 MX	41 MN 10 MX	40 MX 11 MN	41 MN 11 MN	SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER				HIGHLY ORGANIC SOILS
GROUP INDEX	0	0	0	4 MX	8 MX	12 MX	16 MX	NO MX							
USUAL TYPES OF MAJOR MATERIALS	STONE FRAGS. GRAVEL, AND SAND	FINE SAND	SILTY OR CLAYEY GRAVEL AND SAND		SILTY SOILS		CLAYEY SOILS								
GEN. RATING AS SUBGRADE	EXCELLENT TO GOOD						FAIR TO POOR				FAIR TO POOR	POOR	UNSUITABLE		

PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30

CONSISTENCY OR DENSENESS

PRIMARY SOIL TYPE	COMPACTNESS OR CONSISTENCY	RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)	RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT ²)
GENERALLY GRANULAR MATERIAL (NON-COHESIVE)	VERY LOOSE LOOSE MEDIUM DENSE DENSE VERY DENSE	< 4 4 TO 10 10 TO 30 30 TO 50 > 50	N/A
GENERALLY SILT-CLAY MATERIAL (COHESIVE)	VERY SOFT SOFT MEDIUM STIFF STIFF VERY STIFF HARD	< 2 2 TO 4 4 TO 8 8 TO 15 15 TO 30 > 30	< 0.25 0.25 TO 0.5 0.5 TO 1.0 1 TO 2 2 TO 4 > 4

TEXTURE OR GRAIN SIZE

U.S. STD. SIEVE SIZE OPENING (MM)	4	10	40	60	200	270
	4.76	2.00	0.42	0.25	0.075	0.053
BOULDER (BLDR.)						
COBBLE (COB.)						
GRAVEL (GR.)						
COARSE SAND (CSE. SD.)						
FINE SAND (F SD.)						
SILT (SL.)						
CLAY (CL.)						

GRAIN SIZE

MM IN.	305 12	75 3	2.0	0.25	0.05	0.005

SOIL MOISTURE - CORRELATION OF TERMS

SOIL MOISTURE SCALE (ATTERBERG LIMITS)	FIELD MOISTURE DESCRIPTION	GUIDE FOR FIELD MOISTURE DESCRIPTION
LL PL	- SATURATED - (SAT.)	USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE
	- WET - (W)	SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE
	- MOIST - (M)	SOLID; AT OR NEAR OPTIMUM MOISTURE
OM SL	- DRY - (D)	REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE

PLASTICITY

	PLASTICITY INDEX (PI)	DRY STRENGTH
NON PLASTIC	0-5	VERY LOW
SLIGHTLY PLASTIC	6-15	SLIGHT
MODERATELY PLASTIC	16-25	MEDIUM
HIGHLY PLASTIC	26 OR MORE	HIGH

COLOR

DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.

GRADATION

WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.

ANGULARITY OF GRAINS

THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.

MINERALOGICAL COMPOSITION

MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.

COMPRESSIBILITY

	LL < 31	LL = 31 - 50	LL > 50
SLIGHTLY COMPRESSIBLE			
MODERATELY COMPRESSIBLE			
HIGHLY COMPRESSIBLE			

PERCENTAGE OF MATERIAL

	GRANULAR SOILS	SILT - CLAY SOILS	OTHER MATERIAL
ORGANIC MATERIAL			
TRACE OF ORGANIC MATTER	2 - 3%	3 - 5%	TRACE
LITTLE ORGANIC MATTER	3 - 5%	5 - 12%	LITTLE
MODERATELY ORGANIC	5 - 10%	12 - 20%	SOME
HIGHLY ORGANIC	> 10%	> 20%	HIGHLY

GROUND WATER

WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING

STATIC WATER LEVEL AFTER 24 HOURS

PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA

SPRING OR SEEP

MISCELLANEOUS SYMBOLS

ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION

SOIL SYMBOL

ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT

INFERRED SOIL BOUNDARY

INFERRED ROCK LINE

ALLUVIAL SOIL BOUNDARY

DIP & DIP DIRECTION OF ROCK STRUCTURES

TEST BORING

AUGER BORING

CORE BORING

MONITORING WELL

PIEZOMETER INSTALLATION

SLOPE INDICATOR INSTALLATION

CONE PENETROMETER TEST

SOUNDING ROD

TEST BORING WITH CORE

SPT N-VALUE

RECOMMENDATION SYMBOLS

UNDERCUT

SHALLOW UNDERCUT

UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE

UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK

UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL

ABBREVIATIONS

AR - AUGER REFUSAL
BT - BORING TERMINATED
CL - CLAY
CPT - CONE PENETRATION TEST
CSE - COARSE
DMT - DILATOMETER TEST
DPT - DYNAMIC PENETRATION TEST
e - VOID RATIO
F - FINE
FOSS - FOSSILIFEROUS
FRAC. - FRACTURED, FRACTURES
FRAGS. - FRAGMENTS
HL - HIGHLY

MED. - MEDIUM
MICA - MICACEOUS
MOD. - MODERATELY
NP - NON PLASTIC
ORG. - ORGANIC
PMT - PRESSUREMETER TEST
SAP. - SAPROLITIC
SD. - SAND, SANDY
SL. - SILT, SILTY
SLI. - SLIGHTLY
TCR - TRICONE REFUSAL
w - MOISTURE CONTENT
V - VERY

VST - VANE SHEAR TEST
WEA. - WEATHERED
% - UNIT WEIGHT
%g - DRY UNIT WEIGHT

SAMPLE ABBREVIATIONS

S - BULK
SS - SPLIT SPOON
ST - SHELBY TUBE
RS - ROCK
RT - RECOMPACTED TRIAXIAL
CBR - CALIFORNIA BEARING RATIO

EQUIPMENT USED ON SUBJECT PROJECT

DRILL UNITS:

☐ CME-45C

☒ CME-55

☐ CME-550

☐ VANE SHEAR TEST

☐ PORTABLE HOIST

☐

☐

ADVANCING TOOLS:

☐ CLAY BITS

☐ 6" CONTINUOUS FLIGHT AUGER

☒ 8" HOLLOW AUGERS

☐ HARD FACED FINGER BITS

☐ TUNG-CARBIDE INSERTS

☒ CASING ☐ W/ ADVANCER

☐ TRICONE ☐ STEEL TEETH

☒ TRICONE 2-15/16" TUNG-CARB.

☒ CORE BIT

☐

HAMMER TYPE:

☒ AUTOMATIC ☐ MANUAL

CORE SIZE:

☐ -B ☐ -H

☒ -N Q

HAND TOOLS:

☐ POST HOLE DIGGER

☒ HAND AUGER

☒ SOUNDING ROD

☐ VANE SHEAR TEST

☐

☐

ROCK DESCRIPTION

HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:

WEATHERED ROCK (WR)

CRYSTALLINE ROCK (CR)

NON-CRYSTALLINE ROCK (NCR)

COASTAL PLAIN SEDIMENTARY ROCK (CP)

NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.

FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.

FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.

COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.

WEATHERING

FRESH

ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.

VERY SLIGHT (V SLI.)

ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.

SLIGHT (SLI.)

ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.

MODERATE (MOD.)

SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.

MODERATELY SEVERE (MOD. SEV.)

ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. *IF TESTED, WOULD YIELD SPT REFUSAL*

SEVERE (SEV.)

ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. *IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF*

VERY SEVERE (V SEV.)

ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. *IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF*

COMPLETE

ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.

ROCK HARDNESS

VERY HARD

CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.

HARD

CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.

MODERATELY HARD

CAN BE SCRATCHED BY KNIFE OR PICK, GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.

MEDIUM HARD

CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.

SOFT

CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.

VERY SOFT

CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.

FRACTURE SPACING

TERM	SPACING
VERY WIDE	MORE THAN 10 FEET
WIDE	3 TO 10 FEET
MODERATELY CLOSE	1 TO 3 FEET
CLOSE	0.16 TO 1 FOOT
VERY CLOSE	LESS THAN 0.16 FEET

BEDDING

TERM	THICKNESS
VERY THICKLY BEDDED	4 FEET
THICKLY BEDDED	1.5 - 4 FEET
THINLY BEDDED	0.16 - 1.5 FEET
VERY THINLY BEDDED	0.03 - 0.16 FEET
THICKLY LAMINATED	0.008 - 0.03 FEET
THINLY LAMINATED	< 0.008 FEET

INDURATION

FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.

FRIABLE

RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.

MODERATELY INDURATED

GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.

INDURATED

GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.

EXTREMELY INDURATED

SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.

TERMS AND DEFINITIONS

ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.

AQUIFER - A WATER BEARING FORMATION OR STRATA.

ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.

ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.

ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.

CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.

COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.

CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.

DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.

DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.

DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.

FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.

FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.

FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL.

FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.

FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.

JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.

LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.

LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.

MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.

PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.

RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.

ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.

SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.

SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.

SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.

STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.

STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.

STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.

TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.

BENCH MARK: N/A

ELEVATION: N/A FEET

NOTES:

FIAD - FILLED IMMEDIATELY AFTER DRILLING

AR - HAND AUGER REFUSAL

THE BORINGS WERE SURVEYED BY SEPI, A DIVISION OF TRANSYSTEMS USING A SUB CENTIMETER GPS.

DATE: 8-15-14

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

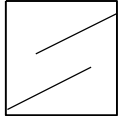
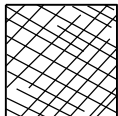
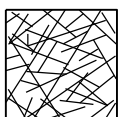
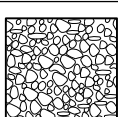
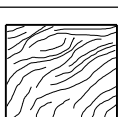
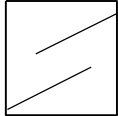
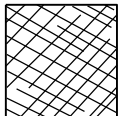
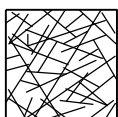
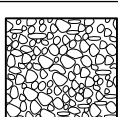
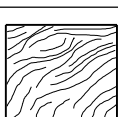
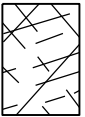
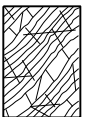
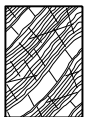
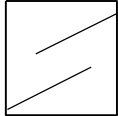
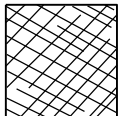
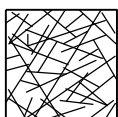
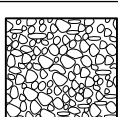
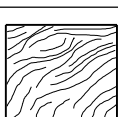
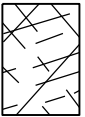
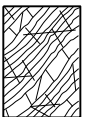
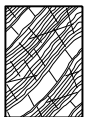
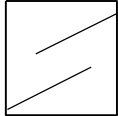
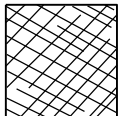
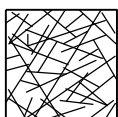
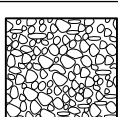
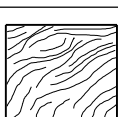
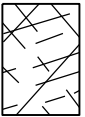
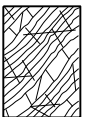
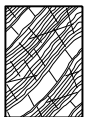
SUBSURFACE INVESTIGATION

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES

FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

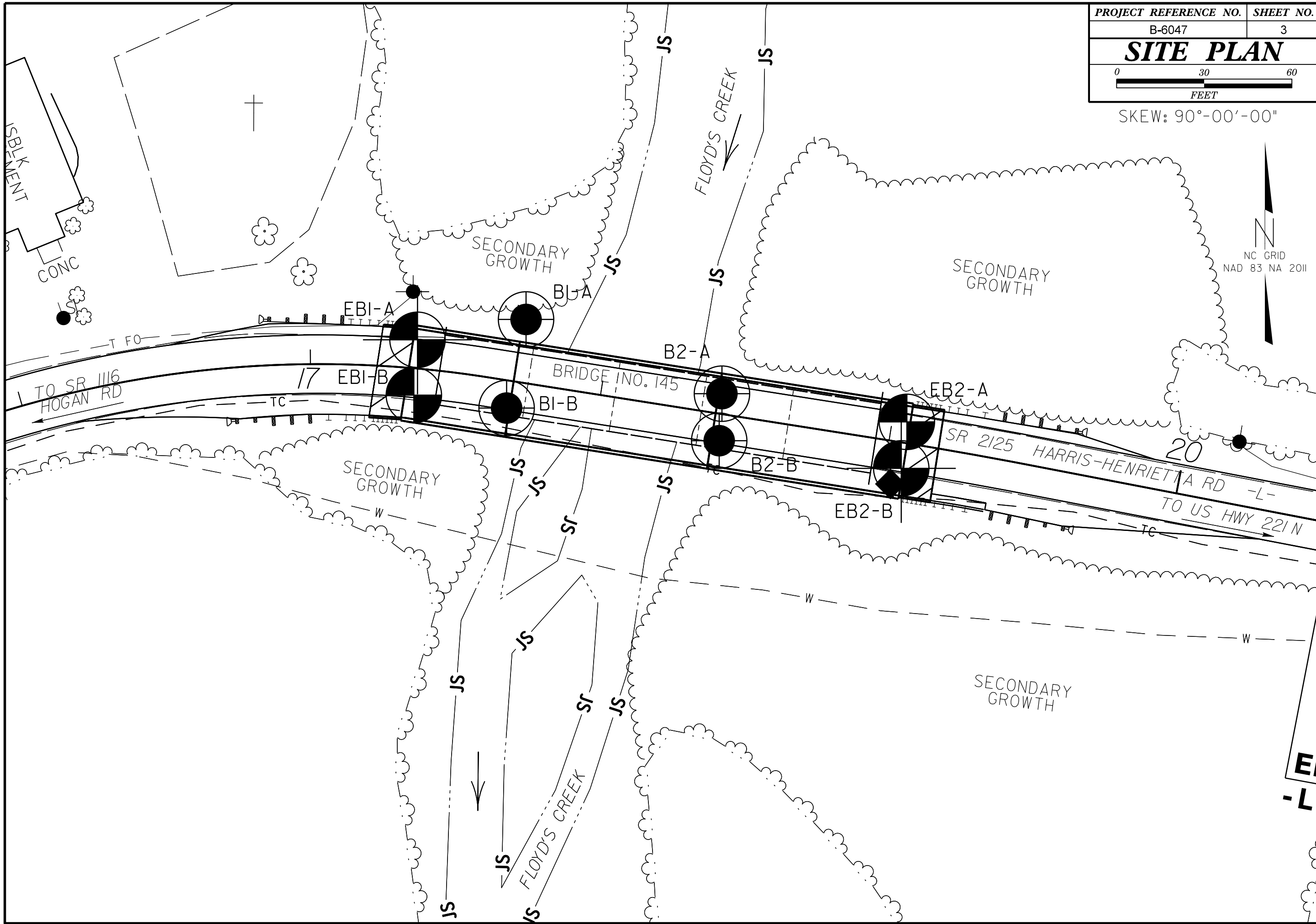
AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

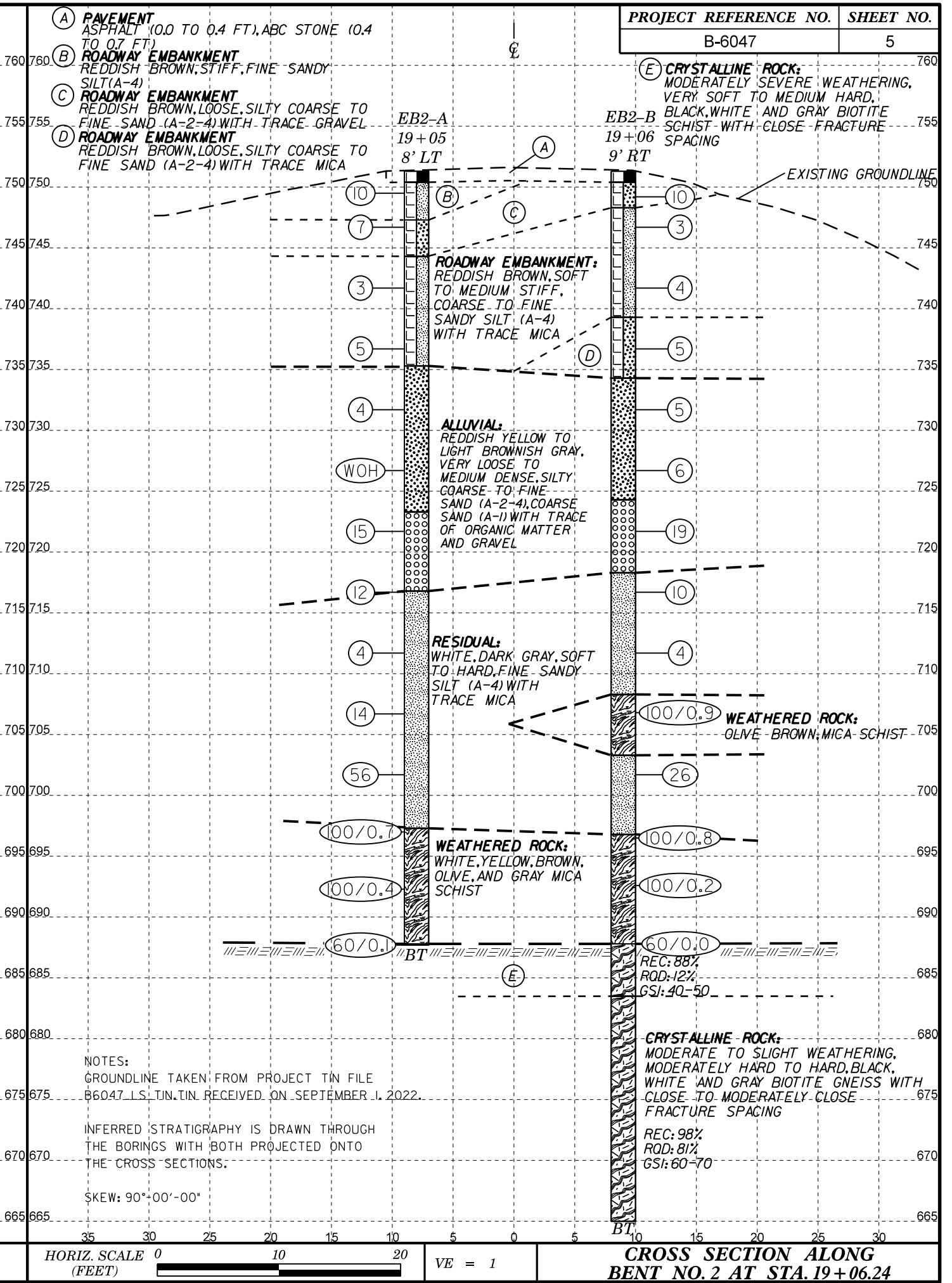
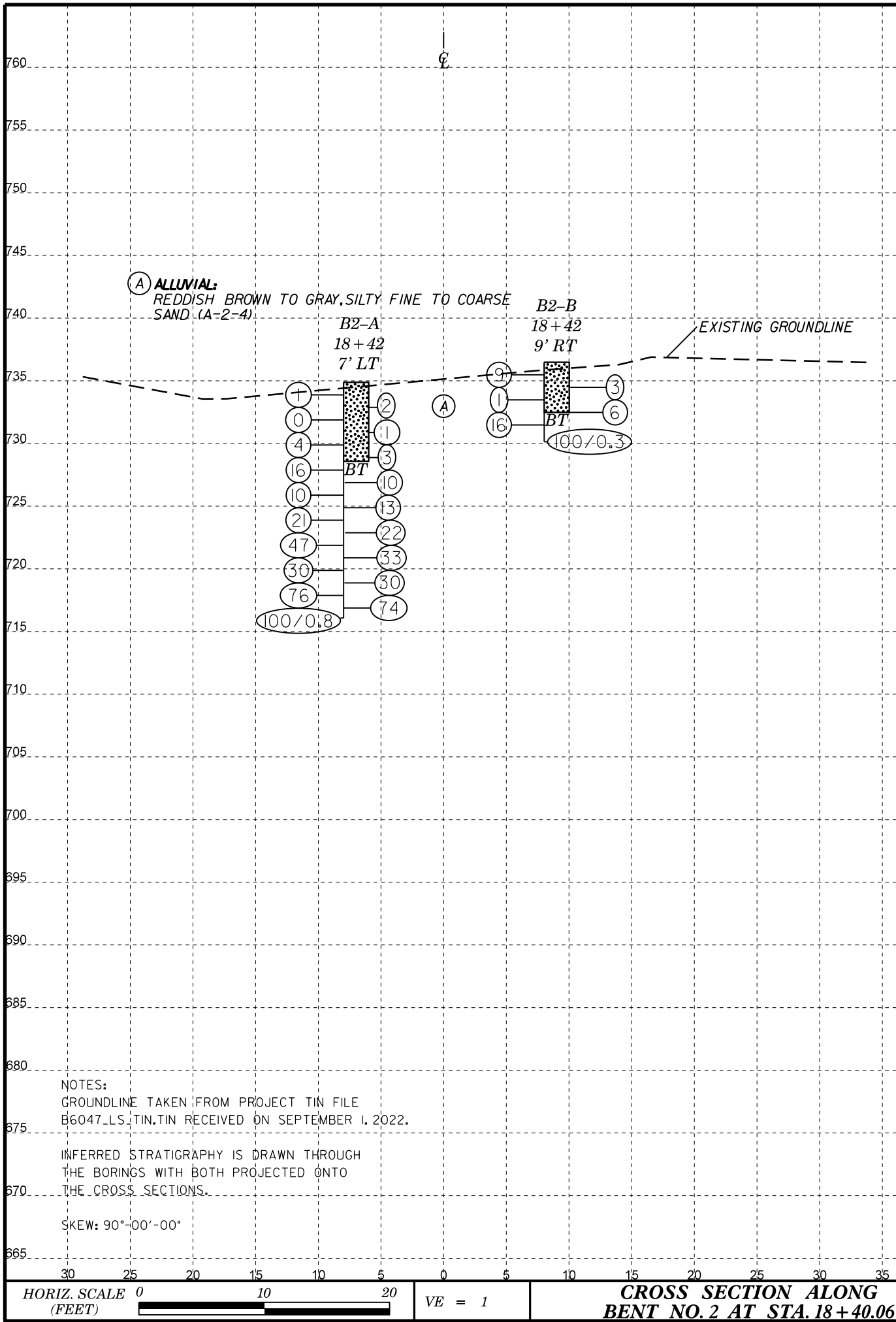
AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000) From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis. STRUCTURE  INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities  BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets  VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets  BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity  DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces  LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes	SURFACE CONDITIONS VERY GOOD Very rough, fresh unweathered surfaces GOOD Rough, slightly weathered, iron stained surfaces FAIR Smooth, moderately weathered and altered surfaces POOR Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments VERY POOR Slickensided, highly weathered surfaces with soft clay coatings or fillings DECREASING SURFACE QUALITY ➡	GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000) From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis. SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes) VERY GOOD - Very Rough, fresh unweathered surfaces GOOD - Rough, slightly weathered surfaces FAIR - Smooth, moderately weathered and altered surfaces POOR - Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments VERY POOR - Very smooth, slickensided or highly weathered surfaces with soft clay coatings or fillings <tr><td>  INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities  BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets  VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets  BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity  DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces  LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes DECREASING INTERLOCKING OF ROCK PIECES ⇓ </td><td> 90 80 70 60 50 40 30 20 10 N/A N/A ➡ Means deformation after tectonic disturbance </td><td>  A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.  B. Sandstone with thin inter-layers of siltstone  C. Sandstone and siltstone in similar amounts  D. Siltstone or silty shale with sandstone layers  E. Weak siltstone or clayey shale with sandstone layers  F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure  G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers  H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces. C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H. 70 60 50 40 30 20 10 A B C D E F G H </td></tr>	 INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities  BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets  VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets  BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity  DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces  LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes DECREASING INTERLOCKING OF ROCK PIECES ⇓	90 80 70 60 50 40 30 20 10 N/A N/A ➡ Means deformation after tectonic disturbance	 A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.  B. Sandstone with thin inter-layers of siltstone  C. Sandstone and siltstone in similar amounts  D. Siltstone or silty shale with sandstone layers  E. Weak siltstone or clayey shale with sandstone layers  F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure  G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers  H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces. C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H. 70 60 50 40 30 20 10 A B C D E F G H
 INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities  BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets  VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets  BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity  DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces  LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes DECREASING INTERLOCKING OF ROCK PIECES ⇓	90 80 70 60 50 40 30 20 10 N/A N/A ➡ Means deformation after tectonic disturbance	 A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.  B. Sandstone with thin inter-layers of siltstone  C. Sandstone and siltstone in similar amounts  D. Siltstone or silty shale with sandstone layers  E. Weak siltstone or clayey shale with sandstone layers  F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure  G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers  H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces. C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H. 70 60 50 40 30 20 10 A B C D E F G H			

PROJECT REFERENCE NO.	SHEET NO.
B-6047	3
SITE PLAN	
0 30 60 FEET	

SKEW: 90°-00'-00"





CORE PHOTOGRAPHS

EB1-A

BOXES 1, 2 & 3: 34.5 - 56.1 FEET

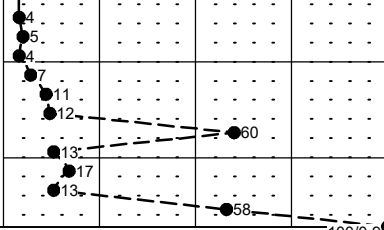


GEOTECHNICAL BORING REPORT
BORE LOG

WBS 48390.1.1			TIP B-6047			COUNTY RUTHERFORD			GEOLOGIST J. Kardon						
SITE DESCRIPTION Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)									GROUND WTR (ft)						
BORING NO. EB1-B			STATION 17+36			OFFSET 9 ft RT			ALIGNMENT -L-			0 HR. 21.9			
COLLAR ELEV. 751.6 ft			TOTAL DEPTH 34.0 ft			NORTHING 555,728			EASTING 1,143,532			24 HR. 22.0			
DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 83% 05/09/2022						DRILL METHOD Mud Rotary			HAMMER TYPE Automatic						
DRILLER R. Toothman			START DATE 10/11/22			COMP. DATE 10/13/22			SURFACE WATER DEPTH N/A						
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)
755															
750	750.7	0.9	7	4	2	6								751.6 GROUND SURFACE 0.0	
745	747.9	3.7	1	1	1	2						M		750.9 ROADWAY EMBANKMENT 0.7	
												M		749.6 Asphalt (0.0 to 0.4 ft), 2.0	
740	743.5	8.1	11	9	6	15						M		ABC Stone (0.4 to 0.7 ft)	
												M		Brown, Silty, Coarse to Fine SAND (A-2-4) with Trace Gravel	6.0
735	738.3	13.3	2	3	4	7						M		Reddish Yellow, Silty CLAY (A-7)	
												M		Reddish Brown, Coarse to Fine Sandy SILT (A-4) with Trace Gravel	
730	733.2	18.4	2	2	11	13						M		732.1 ALLUVIAL 19.5	
												M		Reddish Yellow to Gray, Silty, Coarse to Fine SAND (A-2-4) with Trace Mica and Trace of Organic Matter	
725	728.3	23.3	15	27	22	49						M			
												M		724.6 RESIDUAL 27.0	
720	723.3	28.3	15	11	10	21						M		White and Light Brownish Gray, Coarse to Fine Sandy SILT (A-4)	
														720.6 WEATHERED ROCK 31.0	
	718.2	33.4	100/0.4											717.6 White and Black MICA SCHIST 34.0	
	717.6	34.0	60/0.0											Boring Terminated with Standard Penetration Test Refusal at Elevation 717.6 ft on CRYSTALLINE ROCK: MICA SCHIST	

NCDOT BORE DOUBLE B6047_GEO_BRDG_GINT.GPJ NC_DOT.GDT 2/4/23

GEOTECHNICAL BORING REPORT
BORE LOG

WBS 48390.1.1			TIP B-6047			COUNTY RUTHERFORD			GEOLOGIST J. Fregosi										
SITE DESCRIPTION Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)											GROUND WTR (ft)								
BORING NO. B1-A			STATION 17+70			OFFSET 22 ft LT			ALIGNMENT -L-		0 HR.	N/A							
COLLAR ELEV. 738.3 ft			TOTAL DEPTH 11.9 ft			NORTHING 555,754			EASTING 1,143,570		24 HR.	N/A							
DRILL RIG/HAMMER EFF./DATE N/A						DRILL METHOD Hand Auger/Rod Sounding			HAMMER TYPE N/A										
DRILLER N/A			START DATE 12/14/22			COMP. DATE 12/14/22			SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG MOI	L O G	SOIL AND ROCK DESCRIPTION					
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)				
740																			
735				2	2									738.3	GROUND SURFACE	0.0			
				0	5														
				2	2												736.3	ALLUVIAL Tan Red, Silty Fine SAND (A-2-4)	2.0
4				3															
7				4															
6				6															
45				15															
8				5															
9				8															
7				6															
23				35															
34				66/0.4															
730																			
Boring Terminated at Elevation 726.4 ft in ALLUVIAL: GRAVEL																			
NOTES: Hand Auger Terminated with Auger Refusal at Elevation 734.4 ft in ALLUVIAL: GRAVEL																			

WBS 48390.1.1				TIP B-6047				COUNTY RUTHERFORD				GEOLOGIST J. Fregosi					
SITE DESCRIPTION Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)												GROUND WTR (ft)					
BORING NO. B1-B				STATION 17+69				OFFSET 10 ft RT				ALIGNMENT -L-				0 HR. N/A	
COLLAR ELEV. 736.3 ft				TOTAL DEPTH 12.9 ft				NORTHING 555,723				EASTING 1,143,564				24 HR. N/A	
DRILL RIG/HAMMER EFF./DATE N/A								DRILL METHOD Hand Auger/Rod Sounding				HAMMER TYPE N/A					
DRILLER N/A				START DATE 12/14/22				COMP. DATE 12/14/22				SURFACE WATER DEPTH N/A					
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION				
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				MOI			
740																	
735																	
730				1	0								736.3 GROUND SURFACE 0.0				
				1	2								ALLUVIAL Tan Red, Sandy SILT (A-4) 732.9 3.4				
				5	5												
				2	4												
				5	5												
			6	10													
725				12	10								Boring Terminated at Elevation 723.4 ft in ALLUVIAL: GRAVEL NOTES: Hand Auger Terminated with Auger Refusal at Elevation 732.9 ft in ALLUVIAL: GRAVEL				
				8	11												
				13	32												
				11	25												
				24	38												
			22	22													
			31	69/0.4													

NCDOT BORE DOUBLE B6047_GEO_BRDG_GINT.GPJ NC_DOT.GDT 2/4/23

GEOTECHNICAL BORING REPORT
BORE LOG

WBS 48390.1.1			TIP B-6047			COUNTY RUTHERFORD			GEOLOGIST J. Fregosi								
SITE DESCRIPTION Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)									GROUND WTR (ft)								
BORING NO. B2-A			STATION 18+42			OFFSET 7 ft LT			ALIGNMENT -L-			0 HR. N/A					
COLLAR ELEV. 734.9 ft			TOTAL DEPTH 18.8 ft			NORTHING 555,728			EASTING 1,143,638			24 HR. N/A					
DRILL RIG/HAMMER EFF./DATE N/A						DRILL METHOD Hand Auger/Rod Sounding			HAMMER TYPE N/A								
DRILLER N/A			START DATE 12/14/22			COMP. DATE 12/14/22			SURFACE WATER DEPTH N/A								
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)		
735														734.9	GROUND SURFACE	0.0	
730			1	0		1	-	-	-	-					ALLUVIAL	Reddish Brown to Gray, Silty Fine to Coarse SAND (A-2-4)	6.3
			1	1		2	-	-	-	-							
			0	0		0	-	-	-	-							
			1	0		1	-	-	-	-							
725			2	2		4	-	-	-	-							
			2	1		3	-	-	-	-							
			11	5		16	-	-	-	-							
			4	6		10	-	-	-	-							
			5	5		10	-	-	-	-							
			5	5		13	-	-	-	-							
			6	7		21	-	-	-	-							
			15	6		22	-	-	-	-							
720			8	14		47	-	-	-	-							
			22	25		33	-	-	-	-							
			25	8		30	-	-	-	-							
			17	13		30	-	-	-	-							
			14	16		74	-	-	-	-							
			30	46		76	-	-	-	-							
			28	46		100/0.8	-	-	-	-							
			57	43/0.3			-	-	-	-							

WBS 48390.1.1				TIP B-6047		COUNTY RUTHERFORD		GEOLOGIST J. Fregosi					
SITE DESCRIPTION Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)								GROUND WTR (ft)					
BORING NO. B2-B				STATION 18+42		OFFSET 9 ft RT		ALIGNMENT -L-		0 HR. N/A			
COLLAR ELEV. 736.5 ft				TOTAL DEPTH 5.3 ft		NORTHING 555,712		EASTING 1,143,636		24 HR. N/A			
DRILL RIG/HAMMER EFF./DATE N/A						DRILL METHOD Hand Auger/Rod Sounding			HAMMER TYPE N/A				
DRILLER N/A				START DATE 12/14/22		COMP. DATE 12/14/22		SURFACE WATER DEPTH N/A					
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI L O G	SOIL AND ROCK DESCRIPTION
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			
740													
735				1	8	9	- - -	- - -	- - -			736.5 GROUND SURFACE 0.0	
				2	1	3	- - -	- - -	- - -			ALLUVIAL	
				0	1	1	- - -	- - -	- - -			Reddish Brown, Silty Fine to Coarse SAND	
				2	4	6	- - -	- - -	- - -			(A-2-4)	
				7	9	16	- - -	- - -	- - -			732.5 4.0	
			100/0.3			100/0.3							Boring Terminated at Elevation 731.2 ft in ALLUVIAL: GRAVEL
													NOTES: Hand Auger Terminated with Auger Refusal at Elevation 732.5 ft in ALLUVIAL: GRAVEL

GEOTECHNICAL BORING REPORT

BORE LOG

WBS		48390.1.1		TIP		B-6047		COUNTY		RUTHERFORD		GEOLOGIST		J. Fregosi																									
SITE DESCRIPTION												Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)												GROUND WTR (ft)															
BORING NO.				EB2-A				STATION				19+05				OFFSET				8 ft LT				ALIGNMENT				-L-				0 HR.		Dry					
COLLAR ELEV.				751.3 ft				TOTAL DEPTH				63.6 ft				NORTHING				555,719				EASTING				1,143,701				24 HR.		FIAD					
DRILL RIG/HAMMER EFF./DATE												TRI0055 CME-55 83% 05/09/2022												DRILL METHOD				H.S. Augers				HAMMER TYPE				Automatic			
DRILLER				R. Toothman				START DATE				10/05/22				COMP. DATE				10/05/22				SURFACE WATER DEPTH								N/A							
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT										SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION																				
			0.5ft 0.5ft 0.5ft			0 25 50 75 100													ELEV. (ft) DEPTH (ft)																				
755																																							
	750.5	0.8	8 7 3																																				
750	747.7	3.6	3 3 4																751.3 GROUND SURFACE 0.0 750.6 ROADWAY EMBANKMENT 0.7 Asphalt (0.0 to 0.4 ft) ABC Stone (0.4 to 0.7 ft)																				
	747.7	3.6	3 3 4																747.3 Reddish Brown, Fine Sandy SILT (A-4) 4.0 Reddish Brown, Silty Coarse to Fine SAND (A-2-4) 7.0																				
745	742.7	8.6	1 1 2																744.3 Reddish Brown, Fine Sandy SILT (A-4) with Trace Mica 7.0																				
	742.7	8.6	1 1 2																																				
740	737.7	13.6	2 3 2																																				
	737.7	13.6	2 3 2																																				
735	732.7	18.6	2 2 2																735.3 ALLUVIAL 16.0 Reddish Yellow to Gray, Silty, Coarse to Fine SAND (A-2-4) with Trace of Organic Matter																				
	732.7	18.6	2 2 2																																				
730	727.7	23.6	1 WOH WOH																																				
	727.7	23.6	1 WOH WOH																																				
725	722.7	28.6	2 3 12																723.3 White Light Brownish Gray, Coarse SAND (A-1) with Trace Gravel 28.0																				
	722.7	28.6	2 3 12																																				
720	717.7	33.6	6 6 6																716.8 RESIDUAL 34.5 White, Dark Gray to Olive Brown, Fine Sandy SILT (A-4) with Trace Mica																				
	717.7	33.6	6 6 6																																				
715	712.7	38.6	2 2 2																																				
	712.7	38.6	2 2 2																																				
710	707.7	43.6	3 6 8																																				
	707.7	43.6	3 6 8																																				
705	702.7	48.6	18 26 30																																				
	702.7	48.6	18 26 30																																				
700	697.7	53.6	37 63/0.2																697.3 WEATHERED ROCK 54.0 White and Yellowish Brown MICA SCHIST																				
	697.7	53.6	37 63/0.2																																				
695	692.7	58.6	100/0.4																687.8 CRYSTALLINE ROCK 63.5 MICA SCHIST 63.6 Boring Terminated with Standard Penetration Test Refusal at Elevation 687.7 ft in CRYSTALLINE ROCK: MICA SCHIST																				
	692.7	58.6	100/0.4																																				
690	687.8	63.5	60/0.1																																				
	687.8	63.5	60/0.1																																				

NC DOT BORE DOUBLE B6047 GEO BRDG GINT.GPJ NC DOT.GDT 2/4/23

NC DOT BORE DOUBLE B6047 GEO_BRDG_GINT.GPJ NC_DOT.GDT 2/4/23

WBS 48390.1.1			TIP B-6047			COUNTY RUTHERFORD			GEOLOGIST J. Fregosi				
SITE DESCRIPTION Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)									GROUND WTR (ft)				
BORING NO. EB2-B			STATION 19+06			OFFSET 9 ft RT			ALIGNMENT -L-		0 HR. Dry		
COLLAR ELEV. 751.3 ft			TOTAL DEPTH 86.3 ft			NORTHING 555,703			EASTING 1,143,699		24 HR. FIAD		
DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 83% 05/09/2022						DRILL METHOD Mud Rotary/NQ Core			HAMMER TYPE Automatic				
DRILLER R. Toothman			START DATE 10/06/22			COMP. DATE 10/11/22			SURFACE WATER DEPTH N/A				
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT				SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			
675						Match Line							
670													
665													
Boring Terminated at Elevation 665.0 ft in CRYSTALLINE ROCK: BIOTITE GNEISS													

GEOTECHNICAL BORING REPORT CORE LOG

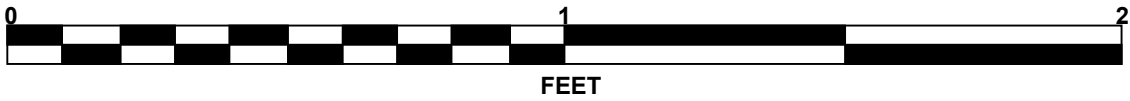
WBS 48390.1.1				TIP B-6047		COUNTY RUTHERFORD		GEOLOGIST J. Fregosi					
SITE DESCRIPTION Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)								GROUND WTR (ft)					
BORING NO. EB2-B		STATION 19+06		OFFSET 9 ft RT		ALIGNMENT -L-		0 HR. Dry					
COLLAR ELEV. 751.3 ft		TOTAL DEPTH 86.3 ft		NORTHING 555,703		EASTING 1,143,699		24 HR. FIAD					
DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 83% 05/09/2022				DRILL METHOD Mud Rotary/NQ Core		HAMMER TYPE Automatic							
DRILLER R. Toothman		START DATE 10/06/22		COMP. DATE 10/11/22		SURFACE WATER DEPTH N/A							
CORE SIZE NQ		TOTAL RUN 22.8 ft											
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) % RQD (ft) %		SAMP. NO.	STRATA REC. (ft) % RQD (ft) %		L O G	ELEV. (ft)	DESCRIPTION AND REMARKS	DEPTH (ft)
687.8												Begin Coring @ 63.5 ft	
685	687.8	63.5	2.8	N=60/0.0 3:26/0.8 2:40/1.0 2:28/1.0	(2.8) 100%	(0.0) 0%		(3.8) 88%	(0.5) 12%		687.8	CRSTALLINE ROCK	63.5
	685.0	66.3	5.0	3:05/1.0 3:17/1.0 3:10/1.0 3:22/1.0 2:57/1.0	(4.4) 88%	(3.8) 76%					683.5	Moderately Severe Weathering, Very Soft to Medium Hard, White, Black and Gray BIOTITE SCHIST with Close Fracture Spacing (GSI: 40-50)	67.8
680	680.0	71.3	5.0	2:53/1.0 2:38/1.0 3:12/1.0 3:38/1.0 3:34/1.0	(4.8) 96%	(4.8) 96%		(18.0) 97%	(15.0) 81%			CRSTALLINE ROCK	
675	675.0	76.3	5.0	4:12/1.0 3:58/1.0 3:56/1.0 2:35/1.0 2:26/1.0	(4.9) 98%	(3.6) 72%						Moderate to Slight Weathering, Moderately Hard to Hard, White, Black and Gray BIOTITE GNEISS with Close to Moderately Close Fracture Spacing (GSI of 60-70)	
670	670.0	81.3	5.0	3:32/1.0 3:04/1.0 2:58/1.0 3:39/1.0 3:38/1.0	(4.9) 98%	(3.3) 66%						(Moderate Weathering, Soft, Black and Gray BIOTITE SCHIST from 80.2 ft to 80.3 ft and 83.0 ft to 83.3 ft)	
665	665.0	86.3									665.0	Boring Terminated at Elevation 665.0 ft in CRYSTALLINE ROCK: BIOTITE GNEISS	86.3

NC DOT CORE DOUBLE B6047 GEO BRDG GINT.GPJ NC DOT.GDT 2/4/23

CORE PHOTOGRAPHS

EB2-B

BOXES 1, 2 & 3: 63.5 - 86.3 FEET



SITE PHOTOGRAPH

Replace Bridge No. 145 over Floyds Creek on SR 2125 (Harris Henrietta Road)



Facing South towards existing bridge