

REFERENCE: U-5108

PROJECT: 42370

SEE SHEET 3 FOR PLAN SHEET LAYOUT
AT TIME OF INVESTIGATION

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	U-5108	1	

ROADWAY
SUBSURFACE INVESTIGATION

COUNTY MECKLENBURG
PROJECT DESCRIPTION NORTHCROSS DRIVE EXTENSION
FROM EXISTING END OF NORTHCROSS DRIVE
TO WESTMORELAND DRIVE

INVENTORY

CONTENTS

LINE	STATION	PLAN	PROFILE
-L-	10+00 to 94+55	4-10	-
-LI-	10+00 to 20+10.59	10,11	-
-Y-	10+00 to 13+17.95	4	-
-YI-	10+00 to 12+27	10	-
-Y2-	10+00 to 11+04.60	10	-
-Y3-	10+00 to 11+12.63	10	-
-Y4-	10+00 to 11+11.04	11	-
-Y5-	10+00 to 11+71.64	11	-
-Y6-	10+00 to 25+59.95	11,12	-
-RABA-	10+00 to 12+32.91	11,11A	-
-RABB-	10+00 to 11+47.75	11,11A	-
-RABC-	10+00 to 12+41.61	11,11A	-
-RABD-	10+00 to 13+14.22	11,11A	-

CROSS SECTIONS

LINE	STATION	SHEETS
-L-	26+50 to 94+50	13-55
-LI-	10+00 to 20+10.59	56-61
-Y6-	10+00 to 25+50	62-70
-RABA-	10+00 to 12+25	71-73
-RABB-	10+00 to 11+25	74-76
-RABC-	10+00 to 12+25	77-79
-RABD-	10+00 to 13+00	80-83

APPENDICES

APPENDIX	TITLE	SHEETS
A	LABORATORY TEST RESULTS	84-85

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

- NOTES:
- THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
 - BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

PERSONNEL

- P.M. WEAVER
- C.R. PASTRANA
- D.M. NANCE
- B.R. LONG
- HPC
- HDR

INVESTIGATED BY ESP Associates, Inc.
DRAWN BY C.R. PASTRANA
CHECKED BY P.M. WEAVER
SUBMITTED BY ESP Associates, Inc.
DATE November 2023

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SIGNATURE _____ DATE _____

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NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
 DIVISION OF HIGHWAYS
 GEOTECHNICAL ENGINEERING UNIT
SUBSURFACE INVESTIGATION
 SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION										GRADATION										ROCK DESCRIPTION										TERMS AND DEFINITIONS																																																																																																																																																																																																																																																																																																																																																													
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 208, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6										WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.										HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:										ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.																																																																																																																																																																																																																																																																																																																																																													
SOIL LEGEND AND AASHTO CLASSIFICATION										ANGULARITY OF GRAINS										WEATHERED ROCK (WR)										NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.																																																																																																																																																																																																																																																																																																																																																													
MINERALOGICAL COMPOSITION										CRYSTALLINE ROCK (CR)										FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.										NON-COASTAL PLAIN SEDIMENTARY ROCK (NCR)										FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.																																																																																																																																																																																																																																																																																																																																																			
COMPRESSION										NON-CRYSTALLINE ROCK (NCR)										COASTAL PLAIN SEDIMENTARY ROCK (CP)										COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.																																																																																																																																																																																																																																																																																																																																																													
PERCENTAGE OF MATERIAL										WEATHERING										FRESH										ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.																																																																																																																																																																																																																																																																																																																																																													
GROUND WATER										VERY SLIGHT (IV SL.)										SLIGHT (SL.)										MODERATE (MOD.)										MODERATELY SEVERE (MOD. SEV.)										SEVERE (SEV.)										VERY SEVERE (IV SEV.)										COMPLETE																																																																																																																																																																																																																																																																																																																					
MISCELLANEOUS SYMBOLS										ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION										SOIL SYMBOL										ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT										INFERRED SOIL BOUNDARY										INFERRED ROCK LINE										ALLUVIAL SOIL BOUNDARY																																																																																																																																																																																																																																																																																																																															
RECOMMENDATION SYMBOLS										UNDERCUT										SHALLOW UNDERCUT										UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE										UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK										UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL																																																																																																																																																																																																																																																																																																																																									
ABBREVIATIONS										AR - AUGER REFUSAL										BT - BORING TERMINATED										CL - CLAY										CPT - CONE PENETRATION TEST										CSE - COARSE										DPT - DILATOMETER TEST										DPT - DYNAMIC PENETRATION TEST										e - VOID RATIO										F - FINE										FOSS. - FOSSILIFEROUS										FRAC. - FRACTURED, FRACTURES										FRAGS. - FRAGMENTS										HI. - HIGHLY										MED. - MEDIUM										MICA. - MICACEOUS										MOD. - MODERATELY										NP - NON PLASTIC										ORG. - ORGANIC										PMT - PRESSUREMETER TEST										SAP. - SAPROLITIC										SD. - SAND, SANDY										SL. - SILT, SILTY										SLI. - SLIGHTLY										TCR - TRICONE REFUSAL										w - MOISTURE CONTENT										V - VERY										VST - VANE SHEAR TEST										WEA. - WEATHERED										UNIT WEIGHT										DRY UNIT WEIGHT										SAMPLE ABBREVIATIONS										S - BULK										SS - SPLIT SPOON										ST - SHELBY TUBE										RS - ROCK										RT - RECOMPACTED TRIAXIAL										CBR - CALIFORNIA BEARING RATIO									
EQUIPMENT USED ON SUBJECT PROJECT										DRILL UNITS:										ADVANCING TOOLS:										HAMMER TYPE:										CORE SIZE:										HAND TOOLS:																																																																																																																																																																																																																																																																																																																																									
PLASTICITY										NON PLASTIC										SLIGHTLY PLASTIC										MODERATELY PLASTIC										HIGHLY PLASTIC										PLASTICITY INDEX (PI)										DRY STRENGTH										VERY LOW										SLIGHT										MEDIUM										HIGH																																																																																																																																																																																																																																																																																							
COLOR										DESCRIPTORS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-BROWN). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.										FRACTURE SPACING										BEDDING										INDURATION										FRAGILE										MODERATELY INDURATED										INDURATED										EXTREMELY INDURATED																																																																																																																																																																																																																																																																																																											
BENCH MARK: FILE 'u5108_is_tin.tin' WAS USED TO DETERMINE GROUND ELEVATION AT BORINGS										ELEVATION:										FEET										NOTES:										F.I.A.D. = FILLED IMMEDIATELY AFTER DRILLING																																																																																																																																																																																																																																																																																																																																																			

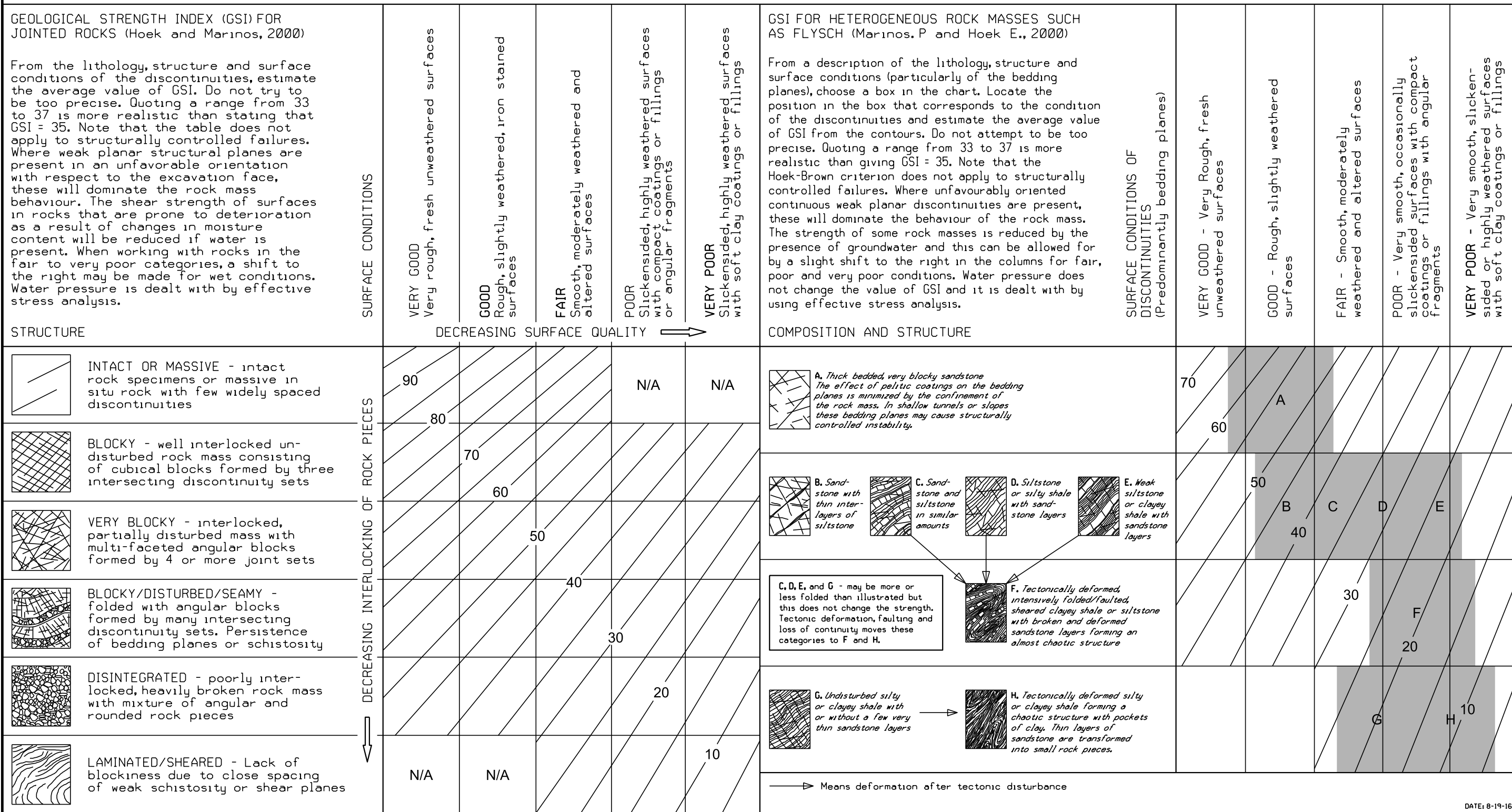
NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES
FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)



09/08/19

TIP PROJECT: U-5108

STATE OF NORTH CAROLINA
DIVISION OF HIGHWAYS

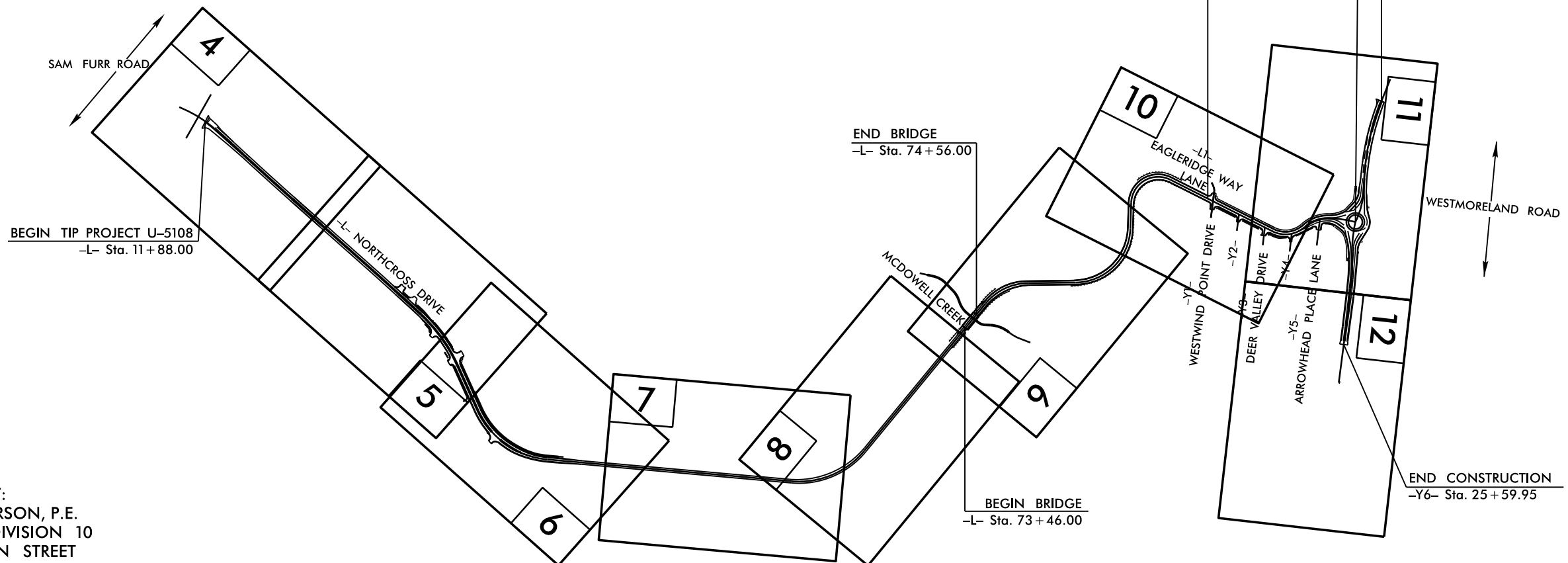
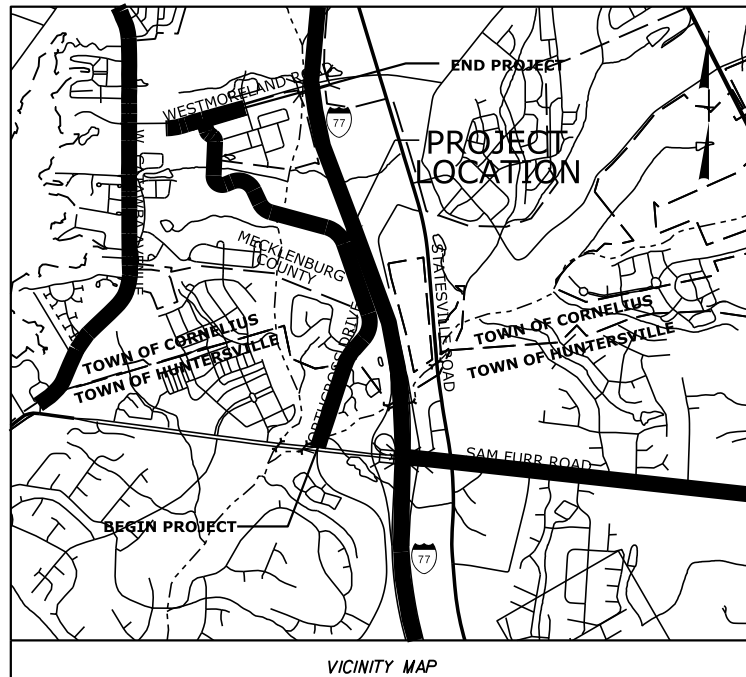
MECKLENBURG COUNTY

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	U-5108	3	90
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
42370.1.1		PE	
42370.2.2	STBGDA-1001(078)	RW & UTIL.	
42370.3.3	STBGDA-1001(078)	CONST.	

DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED

LOCATION: NORTHCROSS DRIVE EXTENSION FROM END OF NORTHCROSS DRIVE TO WESTMORELAND ROAD

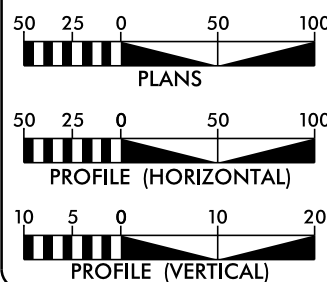
TYPE OF WORK: GRADING, DRAINAGE, PAVING, AND STRUCTURES



NCDOT CONTACT:
SEAN EPPERSON, P.E.
NCDOT - DIVISION 10
716 W. MAIN STREET
ALBEMARLE, NC 28001

CLEARING ON THIS PROJECT SHALL BE PERFORMED TO THE LIMITS ESTABLISHED BY NCDOT METHOD III
THIS PROJECT IS WITHIN THE MUNICIPAL BOUNDARIES OF THE CITY OF CORNELIUS AND HUNTERSVILLE

GRAPHIC SCALES



DESIGN DATA

ADT 2022 = 9900 VPD
 ADT 2040 = 16800 VPD
 K = 10%
 D = 70%
 T = 4%*
 V = 25 - 40 MPH

FUNCTIONAL CLASSIFICATION: COLLECTOR
URBAN MAJOR

* 1% TTST 3% DUAL REGIONAL TIER

PROJECT LENGTH

LENGTH ROADWAY TIP PROJECT U-5108 = 1.736 MILES
 LENGTH STRUCTURE TIP PROJECT U-5108 = 0.021 MILES
 TOTAL LENGTH TIP PROJECT U-5108 = 1.757 MILES

PLANS PREPARED FOR THE NCDOT BY:

Kimley»Horn

200 South Tryon, Suite 200
Charlotte, North Carolina 28202
NC License #F-0102

2019 STANDARD SPECIFICATIONS

RIGHT OF WAY DATE:
JUNE 19, 2019

LETTING DATE:
JUNE 16, 2020

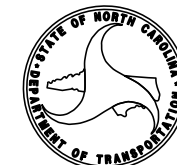
TONY SPACEK, P.E.
PROJECT ENGINEER

BRANDON MURR, EIT
PROJECT DESIGN ENGINEER

HYDRAULICS ENGINEER

SIGNATURE: _____
ROADWAY DESIGN ENGINEER

SIGNATURE: _____
P.E.



\$FILE\$

\$DATE\$

CONTRACT:

RW PLANS

November 10, 2023

STATE PROJECT: 42370.1.1 (U-5108)
 COUNTY: Mecklenburg
 DESCRIPTION: Northcross Drive Extension from end of Northcross Drive to Westmoreland Drive
 SUBJECT: Geotechnical Inventory

Project Description

This proposed project is located in Cornelius, North Carolina and has a total project length of approximately 2 miles. The project begins at -L- Station 11+88 (the intersection of Northcross Drive and Sam Furr Road) and the proposed construction and improvements to the project corridor consists of the following:

- -L- Station 11+88 to -L- Station 27+65: milling and resurfacing of the existing roadway with no grade changes.
- -L- Station 27+65 to -L- Station 94+55: the construction of a new, two-lane roadway on a new location
- -L- Station 36+00 to -L- Station 43+50: the construction of a noise wall (-NB3-) varying between 23.5 feet and 29.0 feet left of -L-
- -L- Station 73+46 to -L- Station 74+46: the construction of a single-span bridge over McDowell Creek
- -L- Station 94+55: the project ties into the existing Eagleridge Way Lane (-L1-)
- -L1- (Eagleridge Way Lane) Station 10+00 to -L1- Station 20+10.59: widening and realignment of -L1- plus the construction of a multi-use path on the left side of the roadway and the addition of a roundabout at the intersection of -L1- and -Y6- (Westmoreland Drive)
- -L- Station 91+70(±): the installation of a 60-inch RCP-IV drainage pipe for the drainage feature at the bottom of the proposed embankment
- -Y6- Station 10+00 to -Y6 Station 25+59.95: widening of -Y6- and the construction of the roundabout mentioned in the bullet above

The project area is primarily consist of and single-family homes and businesses on the south end of the project and of single-family homes on the north end of the project. The middle portion of the project where the new roadway construction will be performed consists mainly of farmland. Intersections along the project includes Sam Furr Road (-Y-), Westwind Point Drive (-Y1-), -Y2-, Deer Valley Drive (-Y3-), -Y4-, Arrowhead Place Lane (-Y5-), and Westmoreland Drive (-Y6-).

It is our understanding that two Transco gas lines are present between approximately -L- Stations 46+50 and 48+00. The tops of the gas lines are reportedly approximately 5 feet below the existing groundline.

Proposed maximum project embankments heights are approximately 27 feet, while proposed maximum cut depths are approximately 5 feet.

This geotechnical investigation was confined to the areas of proposed construction.

Initial site scoping and the beginning of boring layout was performed on November 1, 2018. The field bridge/roadway investigation was performed from November 5 through 16, 2018 through and on December 17, 2018. ESP returned to the site on October 22, 2019 to layout the borings for the noise wall investigation, and performed the noise wall investigation on November 16, 2019. Standard Penetration Test borings were advanced with a D-50 drill machine equipped with an automatic hammer. Rock Coring was required at End Bent 1 of the bridge with a CME 45 drill machine using NQ-size coring equipment. Hand auger borings were also performed at selected locations. Representative soil samples were collected for visual classification in the field and for laboratory analyses.

The following alignments were investigated. Subsurface cross sections of these alignments are included in this report.

Alignment	Station
-L-	26+50 to 94+55.00
-L1-	10+00 to 20+10.59
-Y6-	10+00 to 25+59.95
-RABA-	10+00 to 12+32.91
-RABB-	10+00 to 11+47.75
-RABC-	10+00 to 12+41.61
-RABD-	10+00 to 13+14.22

Physiography and Geography

The project corridor is located in the Kings Mountain Belt of the Piedmont physiographic province. “The Kings Mountain Belt includes metasedimentary sequences with interlayered quartzite, metaconglomerate, marble, and schists derived from both sedimentary and volcanic protoliths” (*The Geology of the Carolinas*, Horton and Zullo, 1991). Rocks of the Kings Mountain Belt are intensely deformed and it is dominated by steeply dipping units striking northeast to north-northeast. The age of the rocks are Paleozoic to late Proterozoic, and the deformation on the leading edge of the Carolina terrane as it collided with North America may be recorded in the deformation of the rocks in the Kings Mountain Belt. Rock was encountered during this investigation in the borings performed for the bridge (-L- Stations 73+46 to 74+52), and in the boring at -L- Station 43+00. The rock encountered consisted of metamorphosed quartz diorite.

The topography along the project corridor generally consist of gently rolling hills. The proposed roadway along Northcross Drive (-L-) and Eagleridge Way Lane (-L1-) generally slopes up from the south to north with elevations ranging from approximately 704 feet (MSL) to approximately 777 feet (MSL), while the proposed roadway along Westmoreland Drive (-Y6-) generally slopes down from the west to east with elevations ranging from approximately 787 feet (MSL) to approximately 768 feet (MSL). Swampy areas are present in the vicinity of the proposed bridge over McDowell Creek and immediately adjacent to the drainage feature at approximately -L- Station 91+70.

Soil Properties

Soils encountered within this project area have been divided into four categories: alluvial deposits, artificial fill, residual soils, and weathered rock.

Asphalt pavement (either existing roadway or drive/parking areas) was present at the existing ground surface at the following borings: RWAL1-1, RWAL1-2, RWAL1-3, RWAL1-4, and L_4000. The asphalt encountered within these borings ranges in thickness from 1 inch to 1 foot. The pavement design investigation performed by the NCDOT for this project indicates that the asphalt pavement within the existing Northcross Drive roadway ranges from 1.75 to 5.5 inches in thickness with base stone thicknesses ranging from 2.5 to 8 inches, while the asphalt pavement within the existing Eagleridge Way Lane roadway ranges from 2.75 to 4 inches in thickness with base stone thicknesses ranging from 6.5 to 7 inches.

Surficial organic soils were encountered in all of the Borings for this project with the exception of the RWAL1 borings, L_4000, L_4100, L_4800 to L_5900, the four borings performed for the bridge (EB1-A, EB1-B, EB2-A, and EB2-B), and Y6_1772. The thickness of the topsoil encountered ranged from approximately 2 inches to approximately 10 inches with the average topsoil thickness being approximately 5 inches.

Soils identified as alluvial deposits were encountered in the borings drilled for the bridge (EB1-A, EB1-B, EB2-A, and EB2-B), and in borings L_7550 and L_9175. The alluvial deposits range in depth from approximately 3 feet to approximately 20 feet below the existing ground surface and were generally classified as soft, sandy silt (A-4), sandy clay (A-6), and silty clay (A-7), and as very loose to loose, silty sand (A-2-4). Standard Penetration Test (SPT) blow counts within the alluvium ranged from 2 to 8 blows per foot (bpf).

Material identified as artificial fill was encountered in boring RWAL1-5. Artificial fill is fill material placed outside of the roadway embankment by entities other than the NCDOT and thus without the quality and compaction controls inherent in roadway embankment construction. The artificial fill extended to a depth of approximately 1 foot below the existing ground surface and sampled as a gravel and topsoil mix.

Residual soils were encountered in all borings drilled for this project with the exception of borings EB1-A, EB2-B, Y6_1450RT, Y6_2100, Y6_2300LT, Y6_2300RT, and Y6_2500. The residual soils generally classified as very loose to very dense, silty sand (A-2-4) and moderately plastic clayey sand (A-2-7), and as soft to hard, sandy silt (A-4), clayey silt (A-5), sandy clay (A-6), and silty clay (A-7-5 and A-7-6). The majority of the residual soils encountered were silty clays ranging from slightly to highly plastic. SPT blow counts within the residual soil ranged from 2 to 94 bpf. All borings with the exception of L_4300, L_7250, EB1-A, EB1-B, EB2-A, EB2-B, L-7550, and L_9175 were terminated within residual soils.

Weathered rock is defined as material that has weathered from the parent bedrock and that exhibits SPT N values greater than 100 blows per foot but less than 60 blows per 0.1 foot. The weathered rock on this project is Metamorphosed Quartz Diorite and was encountered directly underlying alluvial material or underlying the residual soil at depths ranging from approximately 3 feet to approximately 39 feet below the existing ground surface. Borings L_7250, L_7550, and L_9175 were terminated within weathered rock.

Rock Properties

Crystalline rock was encountered either directly underlying the alluvium in boring EB1-A, directly underlying the residual soil in borings L_4300, EB2-A, and EB2-B, and underlying the weathered rock in boring EB1-B. The depths to the top of the crystalline rock ranged from approximately 6 feet to approximately 24 feet below the existing ground surface. The crystalline rock classifies as Metamorphosed Quartz Diorite. The crystalline rock cored in borings EB1-A and EB1-B had recovery (REC) values ranging from 94 percent to 100 percent, Rock Quality Designation (RQD) values ranging from 94 percent to 100 percent, and Geological Strength Index

(GSI) values ranging from 70 to 100 indicating very good quality rock. Borings L_4300, EB1-A, EB1-B, EB2-A, and EB2-B were terminated on or in crystalline rock.

Groundwater Properties

Ground water data was collected in November and December, 2018. Ground water depths ranged from approximately 2 to 12 feet below the existing ground surface, and groundwater elevations ranged from approximately 703 to approximately 733 feet above sea level.

Areas of Special Geotechnical Interest

- 1) The following areas sections were found to contain potentially (or existing) unstable slope conditions:

Alignment	Station(±)	Offset(±)
-L-	74+56 to 75+75	70' lt. to 27' lt. & 23' rt. to 56' rt.

- 2) The following sections contain soft, cohesive soils which have the potential to cause embankment/subgrade and/or slope stability problems during construction:

Alignment	Station(±)
-L-	53+25 to 54+75
-L-	90+75 to 93+25
-Y6-	13+75 to 16+00
-RABB-	10+00 to 10+60
-RABC-	10+00 to 10+60

- 3) The following sections contain soils with greater than 4 percent organic content (including topsoil greater than 4 inches thick) which have the potential to cause embankment/subgrade and or slope stability problems during construction:

Alignment	Station(±)
-L-	29+75 to 30+75
-L-	33+75 to 39+25
-L-	41+75 to 43+75
-L-	44+75 to 47+25
-L-	59+75 to 73+25
-L-	74+75 to 94+55
-L1-	14+50 to 18+50
-Y6-	10+00 to 16+00
-RABB-	10+00 to 10+60
-RABC-	10+60 to 12+41.61
-RABD-	12+10 to 13+14.22
-Y6-	20+50 to 25+59.95

- 4) The following sections contain high plasticity soils which have the potential to cause embankment/subgrade and or slope stability problems during construction:

Alignment	Station(±)
-L-	26+00 to 43+75
-L-	47+25 to 72+25
-L-	77+75 to 82+75
-L-	93+25 to 94+55
-L1-	10+00 to 20+10.59
-RABA-	10+00 to 11+35
-RABB-	10+60 to 11+47.75
-RABC-	10+60 to 12+41.61
-RABD-	10+00 to 12+10

- 5) The following sections contain wet to saturated soils which have the potential to cause embankment/subgrade and or slope stability problems during construction:

Alignment	Station(±)
-L-	44+75 to 47+25
-L-	73+25 to 77+75
-L-	90+75 to 91+75

- 6) The following section contains groundwater within 6 feet of the proposed grade:

Alignment	Station(±)
-L-	76+25 to 77+75

- 7) The following section contains artificial fill material. Artificial fill is fill material placed outside of the roadway embankment by entities other than the NCDOT and thus without the quality and compaction controls inherent in roadway embankment construction. The artificial fill encountered extended to a depth of approximately 1 foot below the existing ground surface:

Alignment	Station to Station (±)	Offset (±)
-L-	32+75 to 33+25	12' LT to +49' LT

Water Wells

Water wells were not identified within the project boundaries during the site investigation for this project. Should any water wells be found within the proposed right of way limits on this project, they should be sealed in accordance with the North Carolina Department of Transportation Standard Specification, Section 205, "Sealing Abandoned Wells".

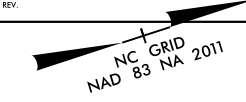
-L-			
PI Sta 10+85.56	PI Sta 12+02.12	PI Sta 15+34.50	PI Sta 17+38.96
$\Delta = 7^{\circ} 30' 20.3" (RT)$	$\Delta = 10^{\circ} 17' 12.9" (RT)$	$\Delta = 0^{\circ} 42' 54.7" (RT)$	$\Delta = 1^{\circ} 02' 14.5" (LT)$
$D = 7^{\circ} 38' 22.0"$	$D = 7^{\circ} 38' 22.0"$	$D = 1^{\circ} 31' 40.4"$	$D = 0^{\circ} 17' 11.3"$
$L = 98.25'$	$L = 134.66'$	$L = 46.81'$	$L = 362.10'$
$T = 49.19'$	$T = 67.51'$	$T = 23.40'$	$T = 181.06'$
$R = 750.00'$	$R = 750.00'$	$R = 3,750.00'$	$R = 20,000.00'$
SE = MATCH EXIST.	SE = MATCH EXIST.	SE = MATCH EXIST.	SE = MATCH EXIST.
RO = MATCH EXIST.	RO = MATCH EXIST.	RO = MATCH EXIST.	RO = MATCH EXIST.

FOR -L- PROFILE, SEE SHEET 13

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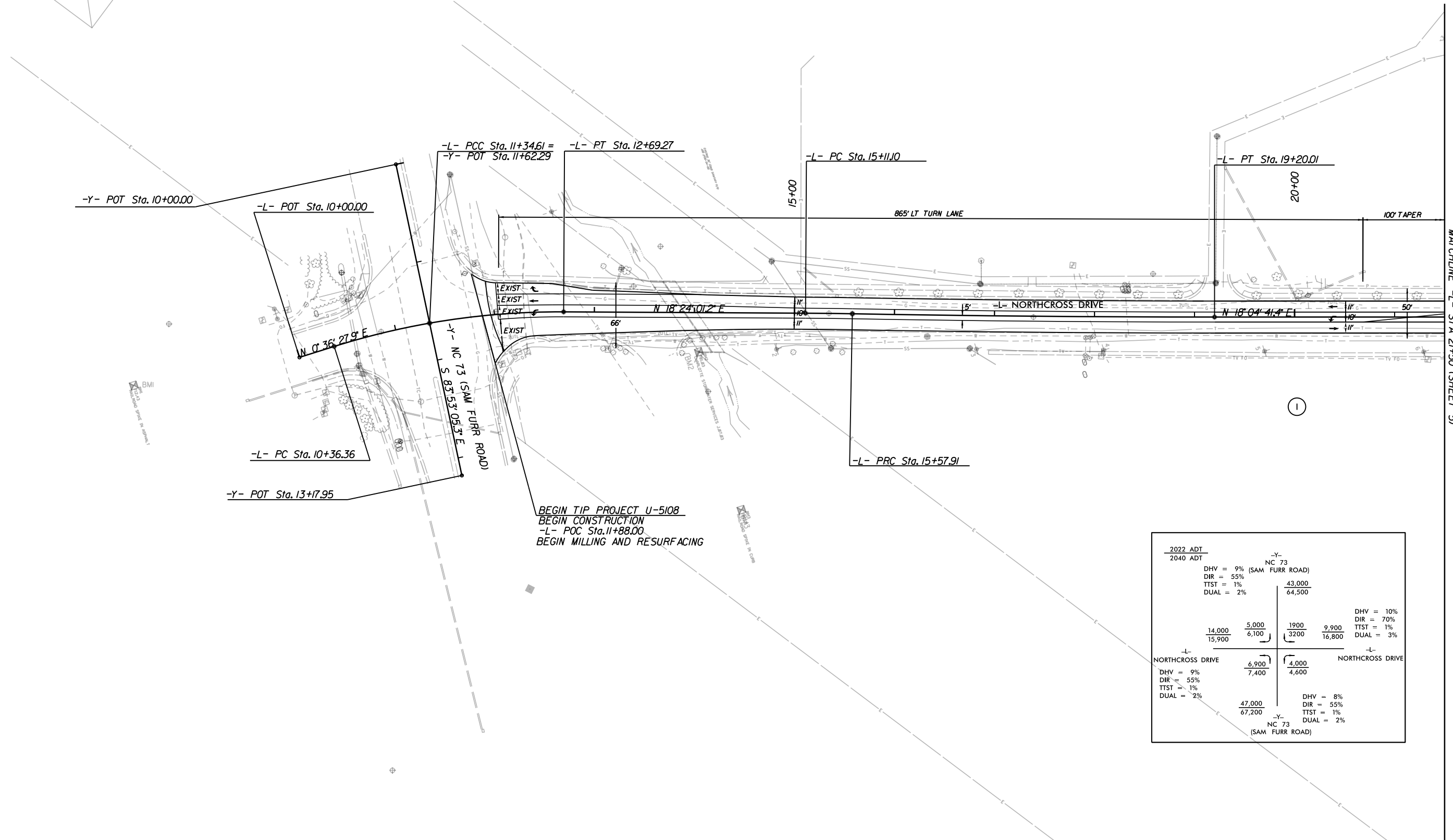
RIGHT-OF-WAY REV.
CONST. REV.



PROJECT REFERENCE NO.	SHEET NO.
U-5108	4
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

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REVISIONS



BEGIN TIP PROJECT U-5108
BEGIN CONSTRUCTION
-L- POC Sta. 11+88.00
BEGIN MILLING AND RESURFACING

2022 ADT		-Y- NC 73 (SAM FURR ROAD)		-L- NORTH CROSS DRIVE		-L- NORTH CROSS DRIVE	
2040 ADT		NC 73 (SAM FURR ROAD)		NORTH CROSS DRIVE		NORTH CROSS DRIVE	
DHV = 9%	DIR = 55%	TTST = 1%	DUAL = 2%	DHV = 10%	DIR = 70%	TTST = 1%	DUAL = 3%
14,000	5,000	1,900	3,200	4,000	4,600	47,000	67,200
15,900	6,100	43,000	64,500	6,900	7,400	8,000	11,000
						DUAL = 2%	
						DUAL = 2%	

\$DATE\$
\$FILE\$

MATCHLINE -L- STA 21+50 (SHEET 5)

-L-

PI Sta 27+73.78	PI Sta 32+12.48
$\Delta = 1^{\circ}21'44.0"$ (RT)	$\Delta = 22^{\circ}43'29.1"$ (RT)
D = 0'17"11.3"	D = 5'43"46.5"
L = 475.51'	L = 396.62'
T = 237.77'	T = 200.95'
R = 20,000.00'	R = 1,000.00'
SE = MATCH EXIST.	SE = 3.4%
RO = MATCH EXIST.	RO = 94'
	DS = 40 MPH

FOR -L- PROFILE, SEE SHEET 13

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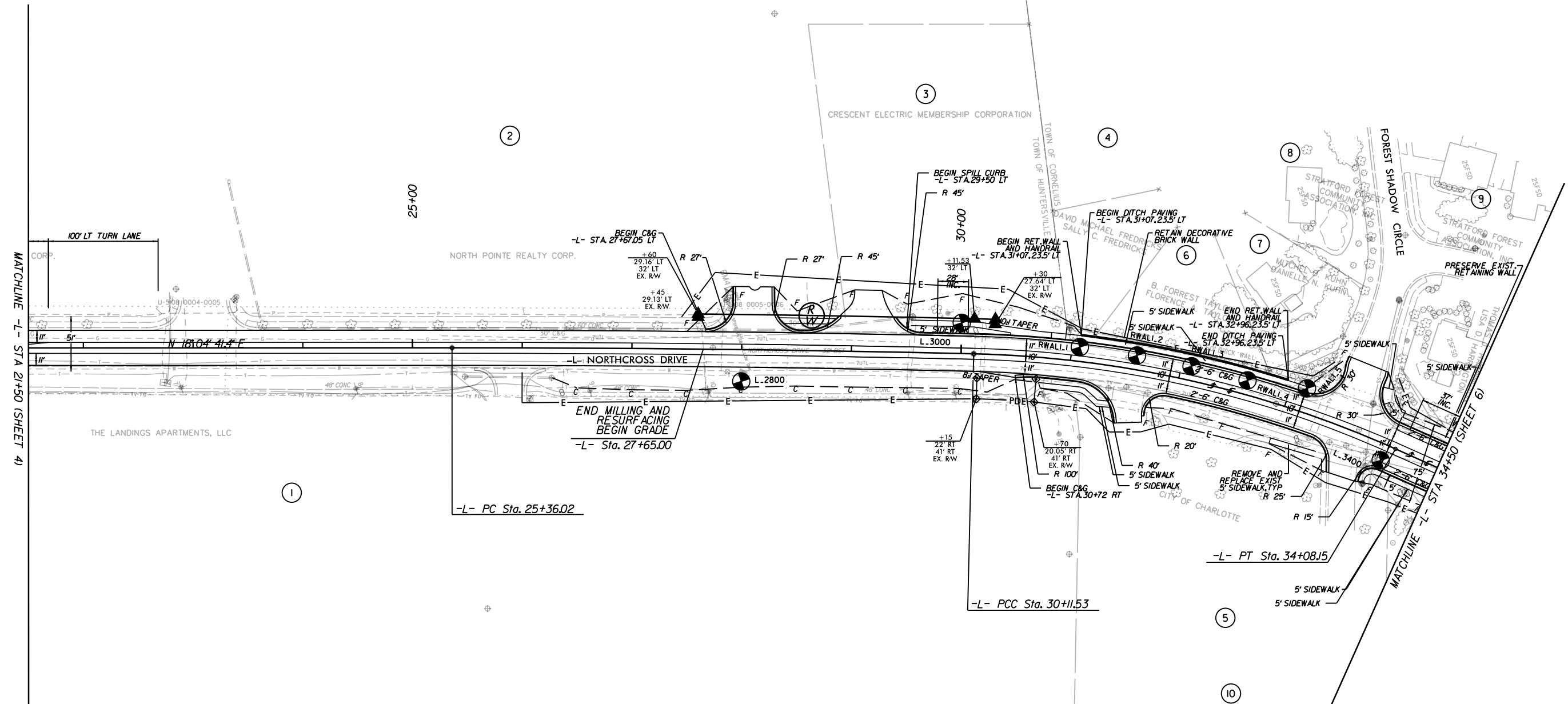
RIGHT-OF-WAY REV.
CONST. REV.

PROJECT REFERENCE NO. U-510B	SHEET NO. 5
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



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REVISIONS



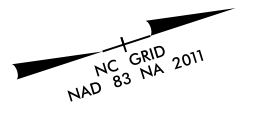
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-L-
 FOR -L- PROFILE, SEE SHEET 14
 PI Sta 40+28.98
 $\Delta = 60' 35" 59.4" (LT)$
 $D = 10' 44" 58.8"$
 $L = 563.74'$
 $T = 311.46'$
 $R = 533.00'$
 $SE = 4\%$
 $RO = 112'$
 $DS = 40 \text{ MPH}$

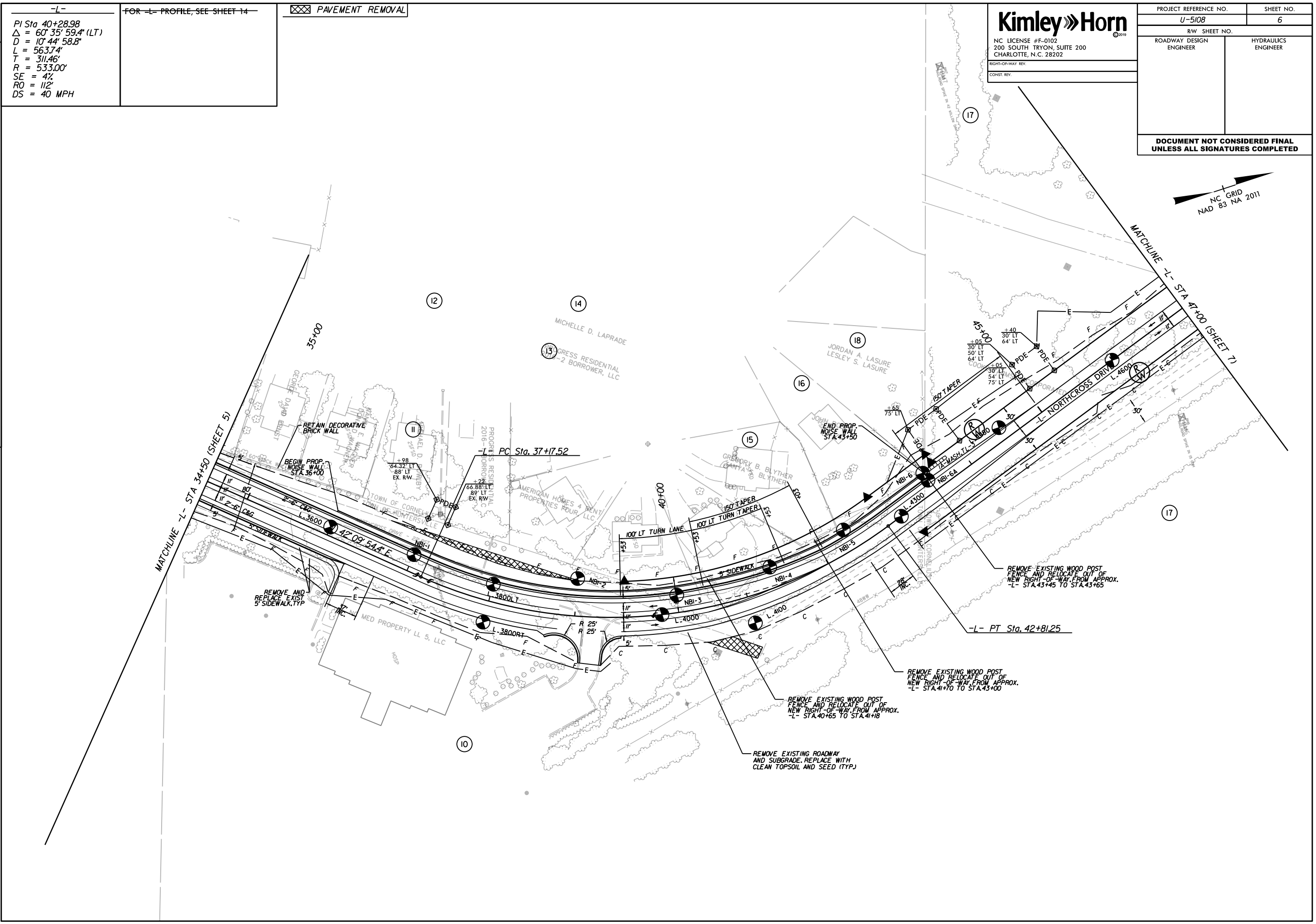
☒ PAVEMENT REMOVAL

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 RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. U-5108	SHEET NO. 6
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



REVISIONS



\$DATE\$
\$FILE\$

-L-
 PI Sta 61+08.65
 $\Delta = 55^\circ 36' 10.2" (LT)$
 $D = 10^\circ 44' 58.8"$
 $L = 517.25'$
 $T = 281.04'$
 $R = 533.00'$
 $SE = 4\%$
 $RO = 112'$
 $DS = 40 \text{ MPH}$

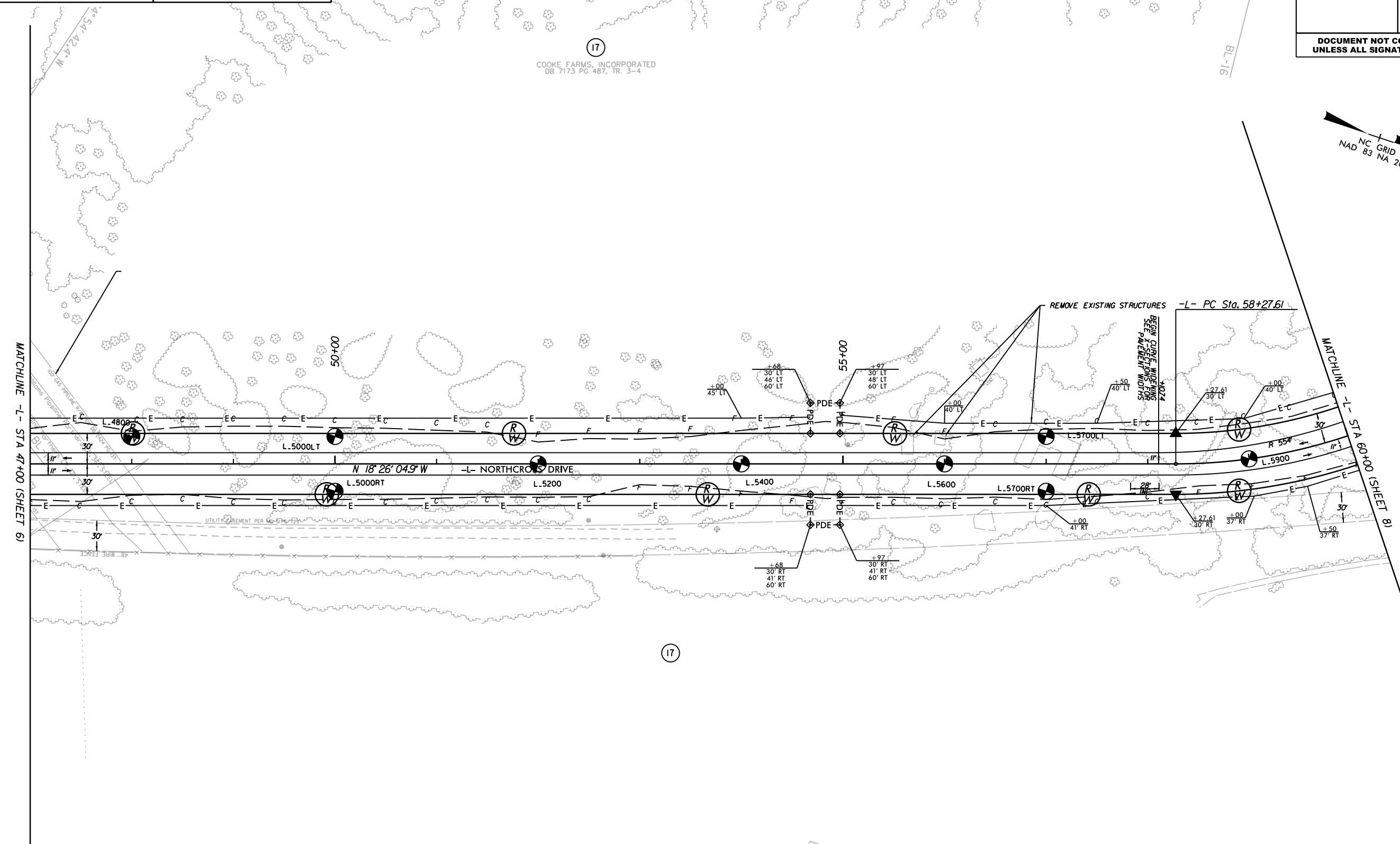
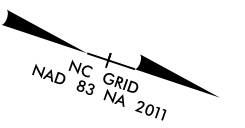
FOR =L= PROFILE, SEE SHEET 14

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 200 SOUTH TRYON, SUITE 200
 CHARLOTTE, N.C. 28202
 RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. U-5108	SHEET NO. 7
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

REVISIONS

(17)
 COOKE FARMS, INCORPORATED
 DB 7173 PG 487, TR. 3-4



MATCHLINE -L- STA 47+00 (SHEET 6)

MATCHLINE -L- STA 60+00 (SHEET 8)

THE LOCALIZED...
 IS BASED ON THE...
 WITH NAD 83/NA...
 NORTHING: 5922...
 THE AVERAGE CORN...
 (GRID)...
 LOCALIZED HORN...
 THE N.C. C...
 15405-1

\$DATE\$
 \$FILE\$

-L-
 PI Sta 61+08.65
 $\Delta = 55^\circ 36' 10.2" (LT)$
 $D = 10^\circ 44' 58.8"$
 $L = 517.25'$
 $T = 281.04'$
 $R = 533.00'$
 $SE = 4\%$
 $RO = 112'$
 $DS = 40 \text{ MPH}$

FOR -L- PROFILE, SEE SHEET 15

Kimley»Horn

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 200 SOUTH TRYON, SUITE 200
 CHARLOTTE, N.C. 28202

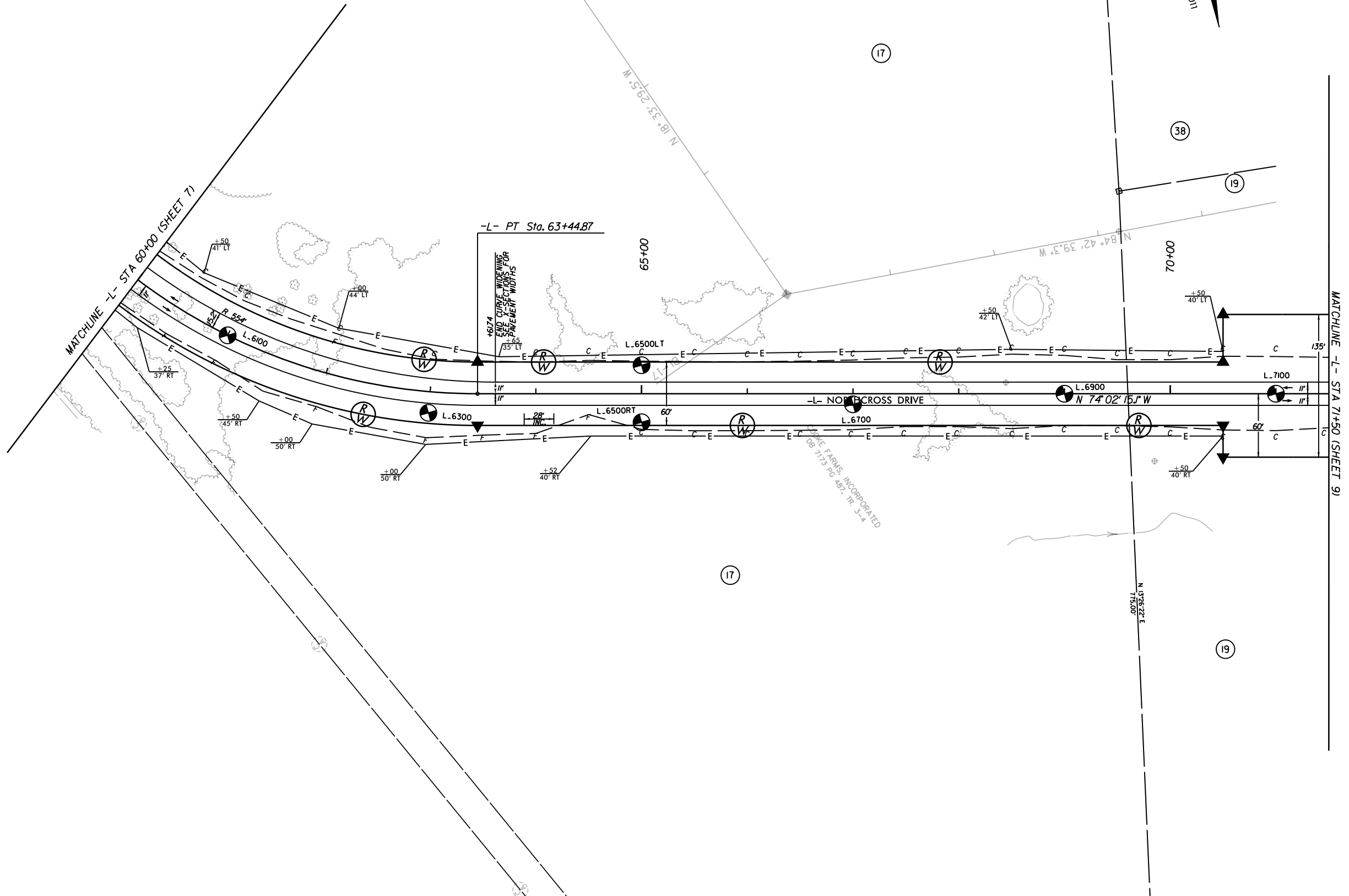
RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. U-5108	SHEET NO. 8
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

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REVISIONS

BL. STATION 58+27.00 131' LEFT
 N 65°58'44" E 144.1533
 ELEVATION = 753.90
 B.M. 9
 RAILROAD SPIKE IN BASE OF 24 MAPLE



\$DATE\$
 \$FILE\$

GREENWAY REMOVAL

BEGIN CONSTRUCTION

-GW-L- POT Sta. 10+00.00

-GW-L- PC Sta. 11+27.84

-GW-L- PC Sta. 11+96.69

-GW-L- PT Sta. 10+40.82

PI Sta 77+10.59 Δ = 49° 48' 21.7" (RT) D = 16' 22' 12.8" L = 304.25' T = 162.49' R = 350.00' SE = 2% RO = 56' DS = 30 MPH	PI Sta 84+87.20 Δ = 87° 27' 55.6" (LT) D = 16' 22' 12.8" L = 534.30' T = 334.85' R = 350.00' SE = 2% RO = 56' DS = 30 MPH
---	---

-FOR L- PROFILE, SEE SHEET 15 AND 16

-FOR GW-L- PROFILE, SEE SHEET 18

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CONST. REV.

PROJECT REFERENCE NO. SHEET NO.

U-5108 9

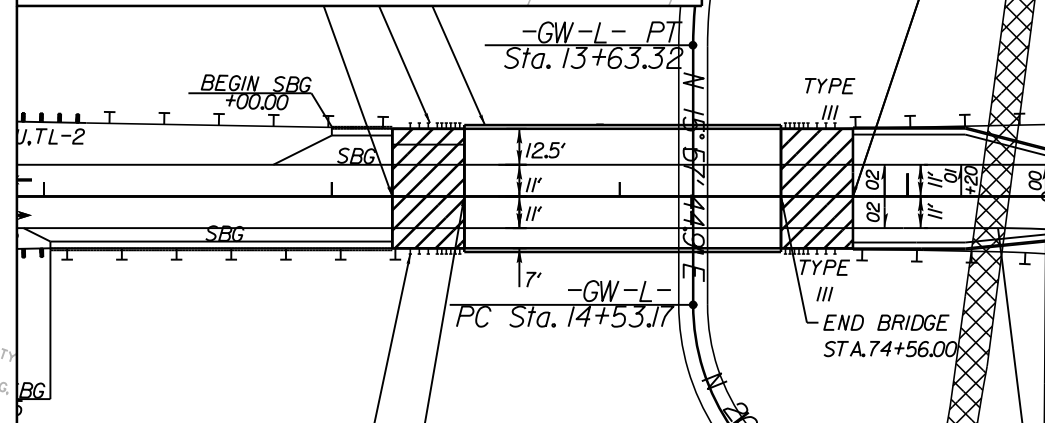
RW SHEET NO.

ROADWAY DESIGN ENGINEER HYDRAULICS ENGINEER

ROADWAY DESIGN ENGINEER HYDRAULICS ENGINEER

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PI Sta 10+85.59 Δ = 33° 14' 24.9" (RT) D = 38' 11' 49.9" L = 87.02' T = 44.77' R = 150.00'	PI Sta 12+27.84 Δ = 23° 27' 58.5" (RT) D = 38' 11' 49.9" L = 61.43' T = 31.15' R = 150.00'	PI Sta 13+24.98 Δ = 29° 59' 33.4" (LT) D = 38' 11' 49.9" L = 78.52' T = 40.18' R = 150.00'
PI Sta 14+78.16 Δ = 36° 51' 21.8" (LT) D = 76' 23' 39.7" L = 48.24' T = 24.99' R = 75.00'	PI Sta 16+00.77 Δ = 36° 35' 43.0" (RT) D = 28' 38' 52.4" L = 127.74' T = 66.13' R = 200.00'	PI Sta 17+02.38 Δ = 18° 10' 50.5" (LT) D = 22' 55' 05.9" L = 79.33' T = 40.00' R = 250.00'



SKETCH OF BRIDGE IN RELATIONSHIP TO PAVEMENT

REVISIONS

MATCHLINE -L- STA 7+50 (SHEET 8)

COOKE FARMS, INCORPORATED
DB 7173 PG 487, TR. 5

CRESCENT ELECTRIC
MEMBERSHIP CORPORATION
DB 9437 PG 110
MB 49 PG 597

MECKLENBURG COUNTY
DB 23232 PG 739
MB 49 PG 595-597, LOTS E, G.

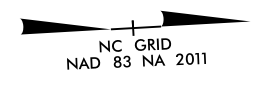
\$DATE\$
\$FILE\$

-L-	-LI-	-YI-	-YI-
PI Sta 91+15.66	PI Sta 15+81.77	PI Sta 10+16.68	PI Sta 10+46.56
$\Delta = 14^{\circ} 56' 03.7" (RT)$	$\Delta = 69^{\circ} 12' 48.7" (LT)$	$\Delta = 8^{\circ} 28' 49.9" (RT)$	$\Delta = 27^{\circ} 05' 58.4" (RT)$
$D = 33^{\circ} 42' 12.2"$	$D = 31^{\circ} 49' 51.6"$	$D = 25^{\circ} 27' 53.2"$	$D = 104^{\circ} 10' 26.9"$
$L = 341.02'$	$L = 217.44'$	$L = 33.30'$	$L = 26.01'$
$T = 266.51'$	$T = 124.21'$	$T = 16.68'$	$T = 13.25'$
$R = 170.00'$	$R = 180.00'$	$R = 225.00'$	$R = 55.00'$
$SE = 4\%$	$SE = NC$	$SE = NC$	$SE = NC$
$RO = 56'$	$RO = NONE$	$RO = NONE$	$RO = NONE$
$DS = 25 MPH$	$DS = 20 MPH$		

-FOR=L- PROFILE, SEE SHEET 16
-FOR=LI- PROFILE, SEE SHEET 16

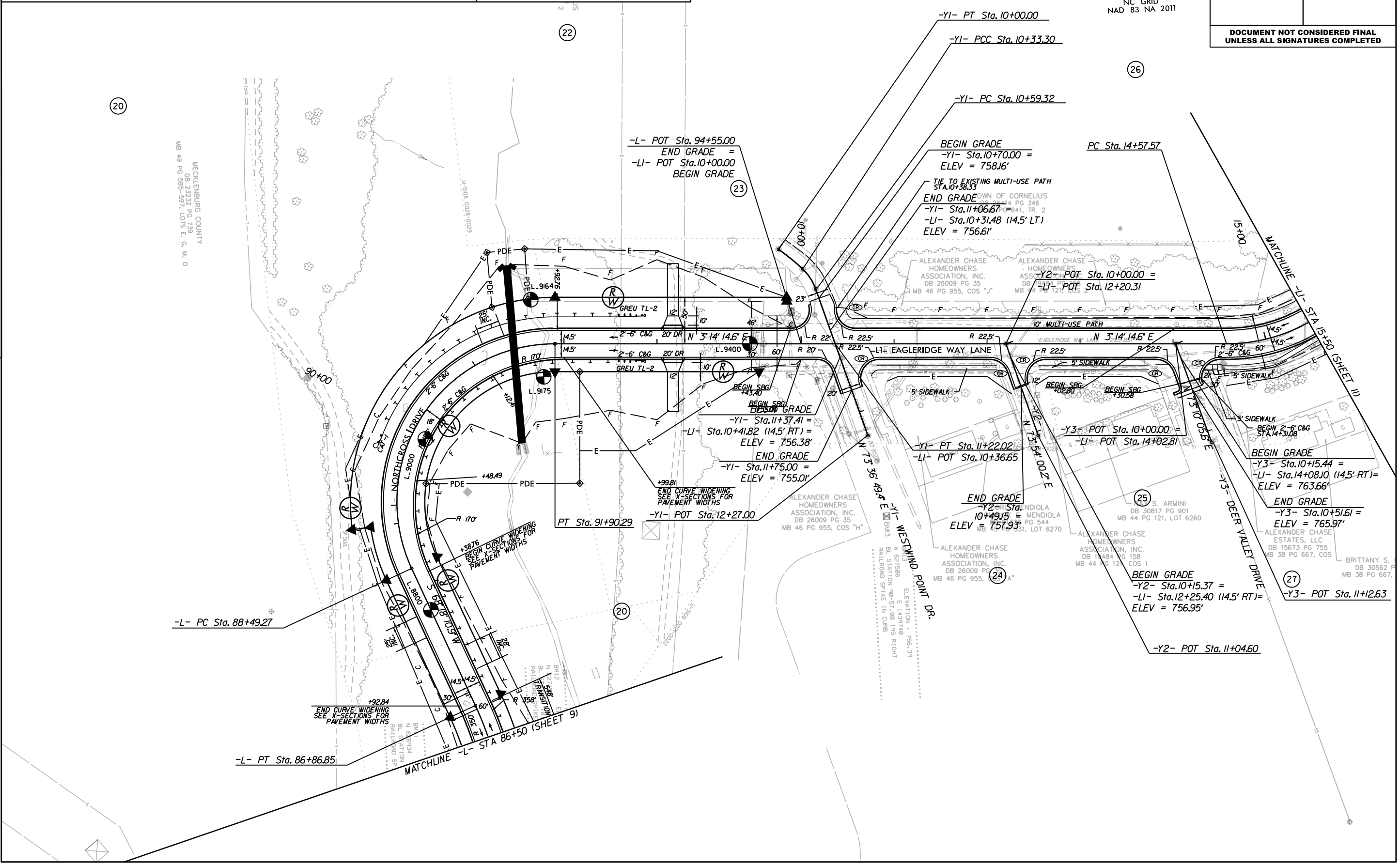
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 CHARLOTTE, N.C. 28202

PROJECT REFERENCE NO. U-5108	SHEET NO. 10
RW SHEET NO.	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	



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REVISIONS



\$DATE\$
\$FILE\$

-LI-		
PI Sta 15+81.77	PI Sta 17+67.02	PI Sta 19+29.95
$\Delta = 69^{\circ}12'48.7"$ (LT)	$\Delta = 46^{\circ}20'24.1"$ (RT)	$\Delta = 10^{\circ}04'12.5"$ (RT)
D = 31'49" 51.6"	D = 26'38" 57.1"	D = 6'13" 40.1"
L = 217.44'	L = 173.89'	L = 161.70'
T = 124.21'	T = 92.02'	T = 81.06'
R = 180.00'	R = 215.00'	R = 920.00'
SE = NC	SE = NC	SE = NC
RO = NONE	RO = NONE	RO = NONE
DS = 20 MPH	DS = 20 MPH	DS = 20 MPH

-Y6-		
PI Sta 12+85.45	PI Sta 16+74.96	PI Sta 19+15.56
$\Delta = 20^{\circ}43'41.1"$ (LT)	$\Delta = 25^{\circ}18'12.4"$ (RT)	$\Delta = 15^{\circ}39'38.4"$ (LT)
D = 3'41" 47.4"	D = 11'27" 33.0"	D = 5'58" 05.9"
L = 560.75'	L = 220.81'	L = 262.40'
T = 283.47'	T = 112.24'	T = 132.02'
R = 1,550.00'	R = 500.00'	R = 960.00'
SE = 6.2%	SE = NC	SE = NC
RO = 223	RO = NONE	RO = NONE
DS = 50 MPH	DS = 20 MPH	DS = 20 MPH

-FOR -Y6- PROFILE, SEE SHEET 17-

RAB DETAIL, SEE SHEET 11B

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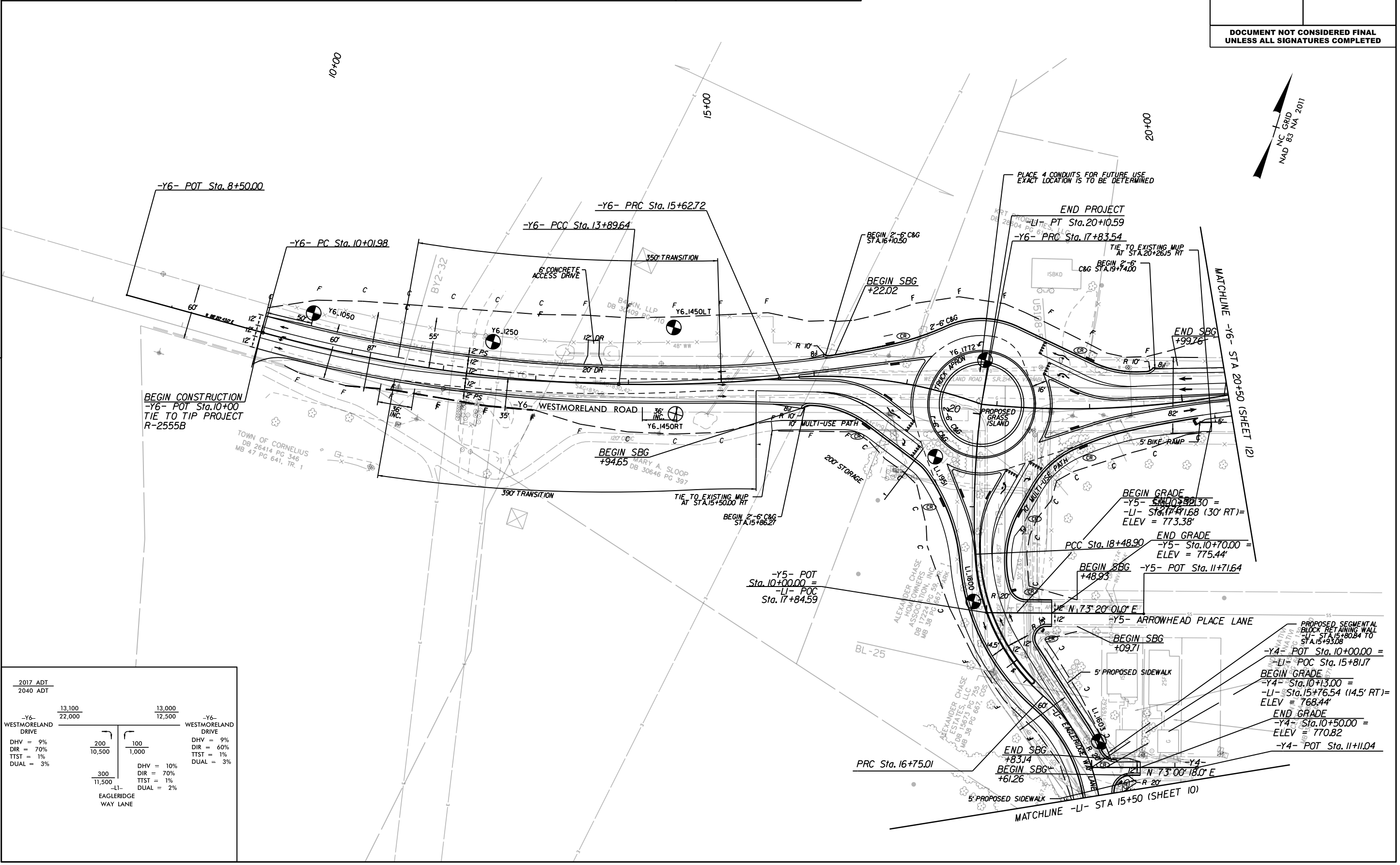
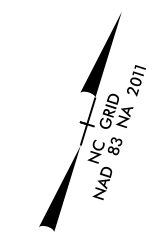
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CONST. REV.

PROJECT REFERENCE NO. U-5108	SHEET NO. 11
RW SHEET NO.	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	

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REVISIONS



2017 ADT	2040 ADT
13,100	13,000
22,000	12,500

-Y6- WESTMORELAND DRIVE		-Y6- WESTMORELAND DRIVE	
DHV = 9%	200	DHV = 9%	100
DIR = 70%	10,500	DIR = 60%	1,000
TTST = 1%		TTST = 1%	
DUAL = 3%		DUAL = 3%	

-LI- EAGLERIDGE WAY LANE	
DHV = 10%	300
DIR = 70%	11,500
TTST = 1%	
DUAL = 2%	

\$DATE\$
\$FILE\$

ROUNDAABOUT GEOMETRY SHEET



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PROJECT REFERENCE NO. U-5108	SHEET NO. 11A
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

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-RABB- PI Sta 10+42.11 Δ = 4° 49' 21.5" (LT) D = 5' 43' 46.5" L = 84.17' T = 42.11' R = 1,000.00'	-RABB- PI Sta 11+16.08 Δ = 12° 08' 33.8" (LT) D = 19' 05' 54.9" L = 63.58' T = 31.91' R = 300.00'
---	---

-RABB- Sta.10+00.00 =
-Y6- Sta.16+00.00 (17.54' LT)
ELEV = 772.35'

-Y6- Sta.17+25.50
-RAB- Sta.12+62.22
ELEV = 775.15'

-RABB- +40.00
774.19 (HP)

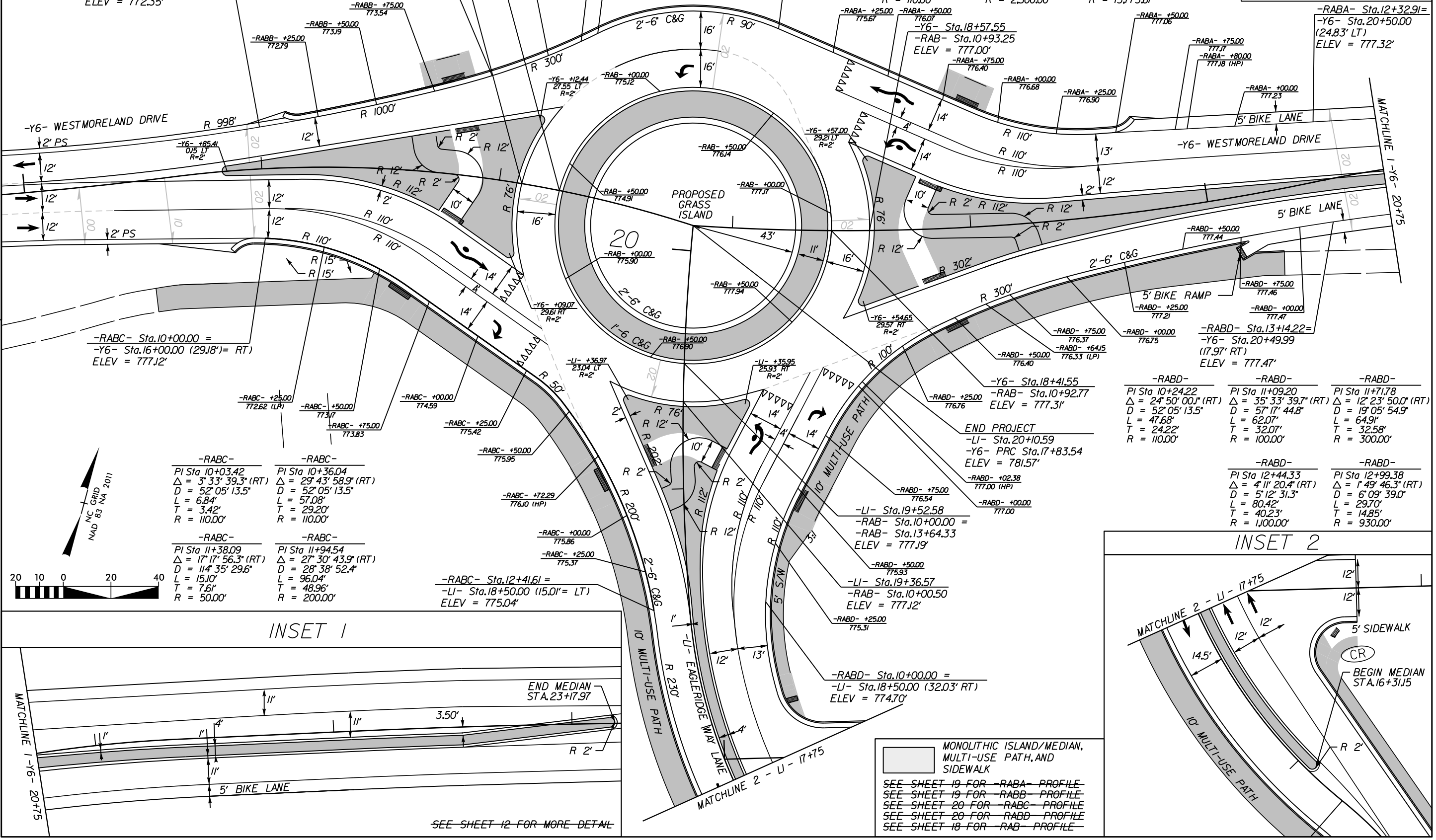
-RAB- Sta.11+62.24 =
-RABA- Sta.10+00.00 =
-Y6- Sta.18+16.71 (84.24' LT)
ELEV = 775.22'

-RABA-
PI Sta 11+5.80
Δ = 27° 38' 35.8" (LT)
D = 52' 05' 13.5"
L = 53.07'
T = 27.06'
R = 110.00'

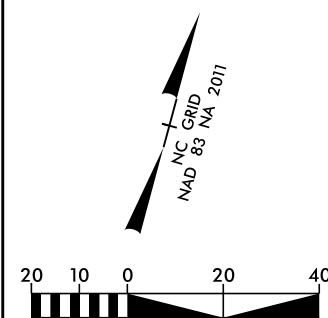
-RABA-
PI Sta 11+45.10
Δ = 0° 09' 03.6" (RT)
D = 2' 17' 30.6"
L = 6.59'
T = 3.29'
R = 2.500.00'

-RABA-
PI Sta 11+80.60
Δ = 0° 16' 04.5" (LT)
D = 0' 24' 57.5"
L = 64.40'
T = 32.20'
R = 13,773.61'

-RABA- Sta.12+32.91 =
-Y6- Sta.20+50.00
(24.83' LT)
ELEV = 777.32'



REVISIONS



-RABC- PI Sta 10+03.42 Δ = 3° 33' 39.3" (RT) D = 52' 05' 13.5" L = 6.84' T = 3.42' R = 110.00'	-RABC- PI Sta 10+36.04 Δ = 29° 43' 58.9" (RT) D = 52' 05' 13.5" L = 57.08' T = 29.20' R = 110.00'
--	---

-RABC- PI Sta 11+38.09 Δ = 17° 17' 56.3" (RT) D = 114' 35' 29.6" L = 15.10' T = 7.61' R = 50.00'	-RABC- PI Sta 11+94.54 Δ = 27° 30' 43.9" (RT) D = 28' 38' 52.4" L = 96.04' T = 48.96' R = 200.00'
--	---

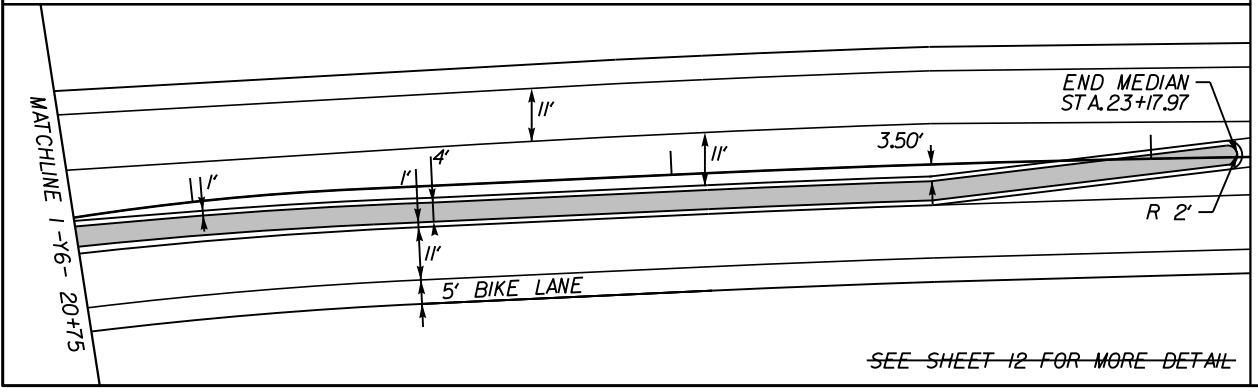
-RABC- Sta.12+41.61 =
-LI- Sta.18+50.00 (15.01' LT)
ELEV = 775.04'

END PROJECT
-LI- Sta.20+10.59
-Y6- PRC Sta.17+83.54
ELEV = 781.57'

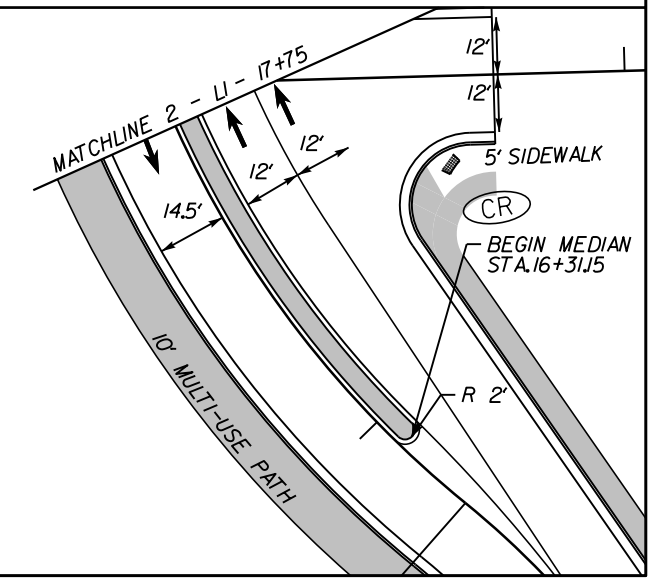
-RABD- PI Sta 10+24.22 Δ = 24° 50' 00.1" (RT) D = 52' 05' 13.5" L = 47.68' T = 24.22' R = 110.00'	-RABD- PI Sta 11+09.20 Δ = 35° 33' 39.7" (RT) D = 57' 17' 44.8" L = 62.07' T = 32.07' R = 100.00'	-RABD- PI Sta 11+71.78 Δ = 12° 23' 50.0" (RT) D = 19' 05' 54.9" L = 64.91' T = 32.58' R = 300.00'
---	---	---

-RABD- PI Sta 12+44.33 Δ = 4° 11' 20.4" (RT) D = 5' 12' 31.3" L = 80.42' T = 40.23' R = 1,000.00'	-RABD- PI Sta 12+99.38 Δ = 1° 49' 46.3" (RT) D = 6' 09' 39.0" L = 29.70' T = 14.85' R = 930.00'
---	---

INSET 1



INSET 2



MONOLITHIC ISLAND/MEDIAN,
MULTI-USE PATH, AND
SIDEWALK
SEE SHEET 19 FOR -RABA- PROFILE
SEE SHEET 19 FOR -RABB- PROFILE
SEE SHEET 20 FOR -RABC- PROFILE
SEE SHEET 20 FOR -RABD- PROFILE
SEE SHEET 18 FOR -RAB- PROFILE

\$DATE\$
\$FILES\$

SEE SHEET 12 FOR MORE DETAIL

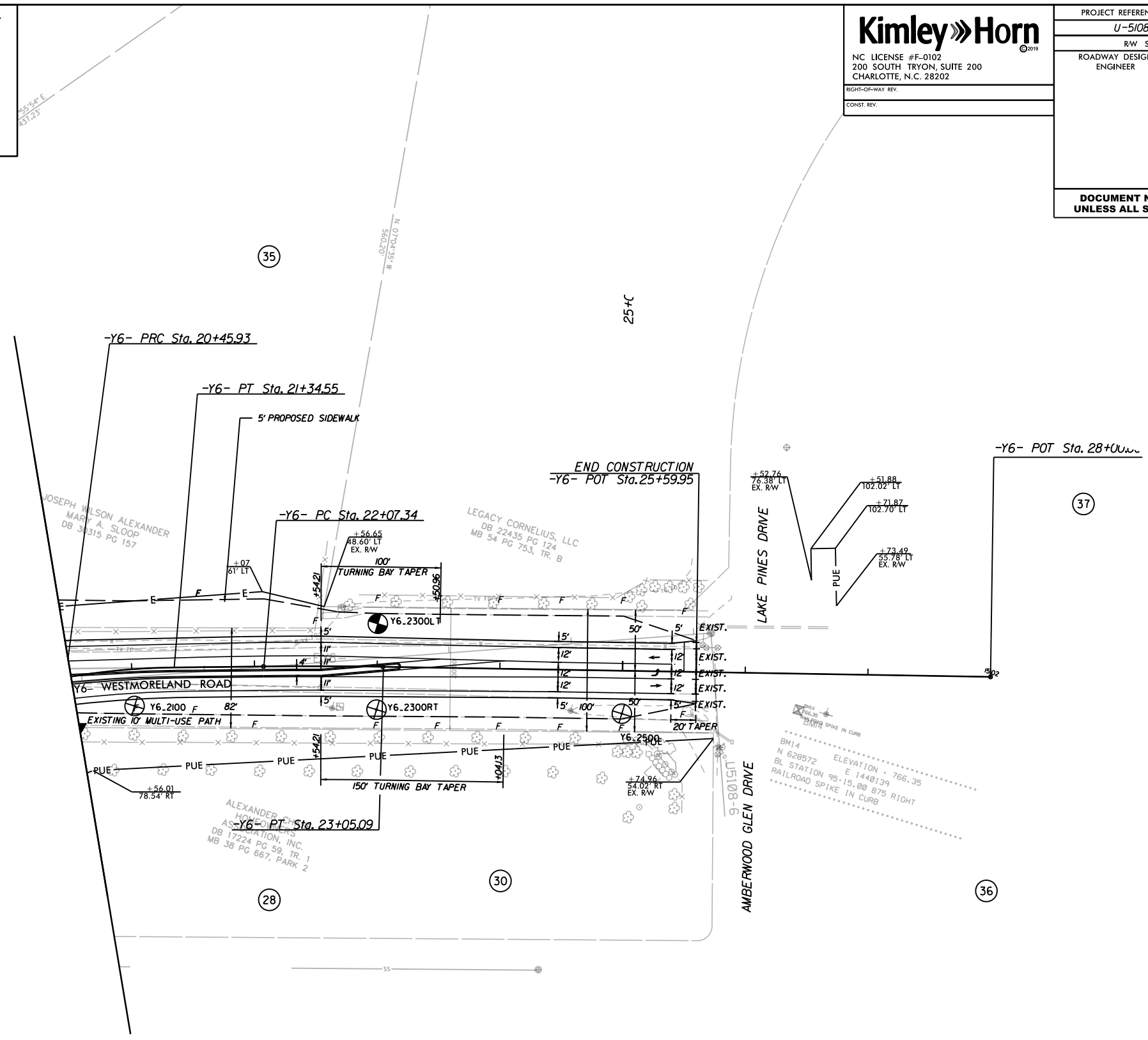
-Y6-
 PI Sta 20+90.34 PI Sta 22+56.02
 $\Delta = 9'13''52.1''$ (RT) $\Delta = 1'35''37.1''$ (RT)
 $D = 10'25''02.7''$ $D = 1'38''13.3''$
 $L = 88.61'$ $L = 97.35'$
 $T = 44.40'$ $T = 48.68'$
 $R = 550.00'$ $R = 3,500.00'$
 $SE = NC$ $SE = MATCH EXIST.$
 $RO = NONE$ $RO = MATCH EXIST.$
 $DS = 20 MPH$

FOR -Y6- PROFILE, SEE SHEET 17-

Kimley»Horn
 NC LICENSE #F-0102
 200 SOUTH TRYON, SUITE 200
 CHARLOTTE, N.C. 28202
 RIGHT-OF-WAY REV.
 CONST. REV.

PROJECT REFERENCE NO. U-5108	SHEET NO. 12
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

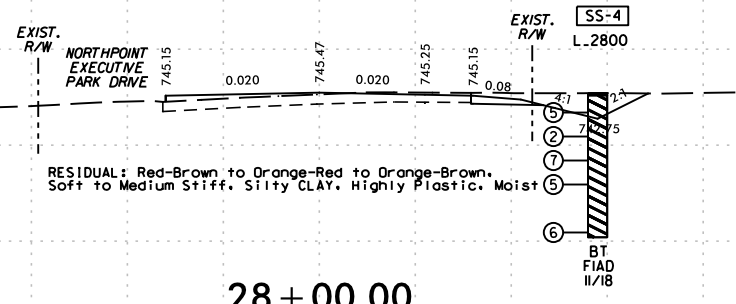
REVISIONS



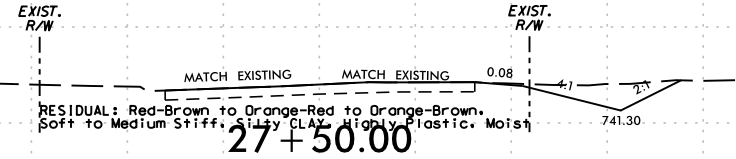
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6/23/16

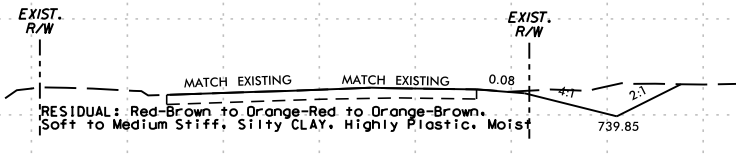
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SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT			% PASSING (SIEVES)			% MOISTURE	% ORGANIC	
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-4	29' RT	28+00	1.0-2.5	A-7-5	35	17.5	15	11	14	60	100	91	77	31.0	-



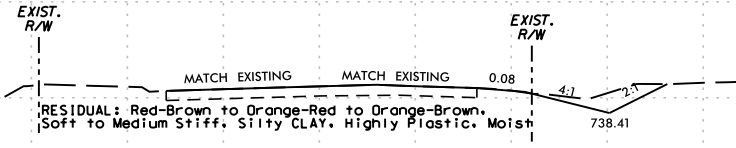
28 + 00.00



27 + 50.00



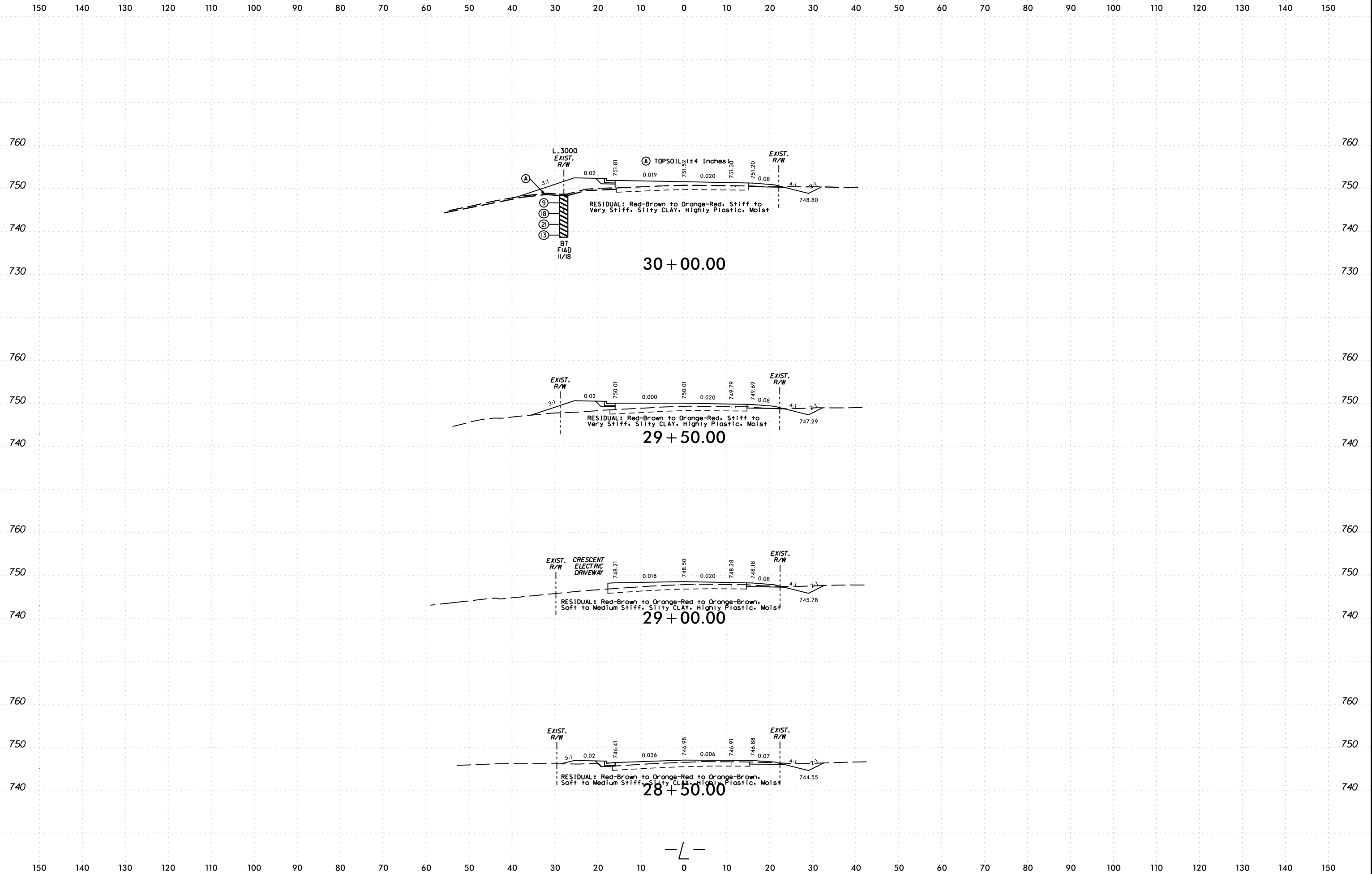
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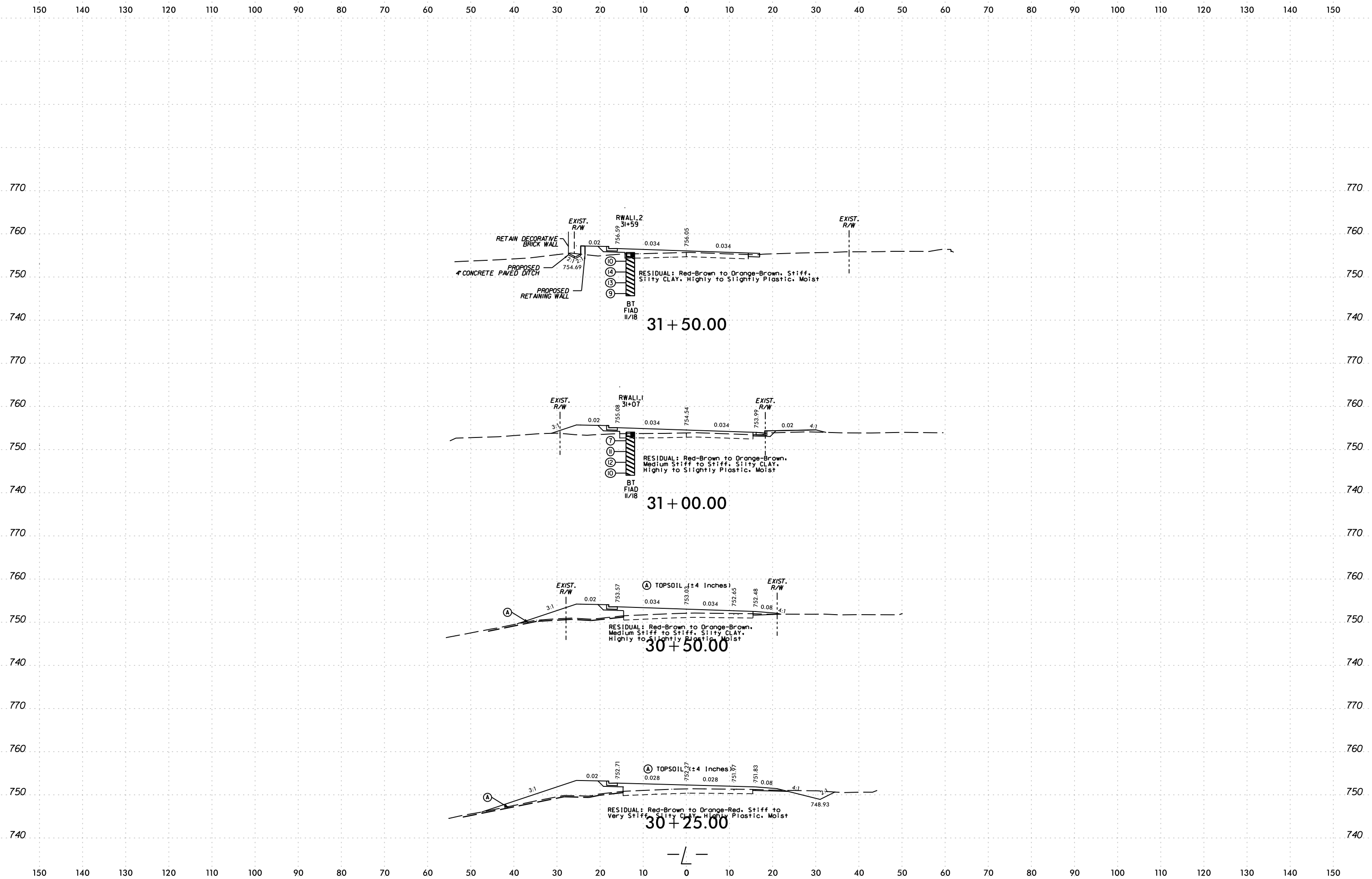


26 + 50.00

NOTE: End Grade -L- STA. 94+55
 Begin Milling and Resurfacing -LI- STA. 10+00
 -L- STA. 94+55 = -LI- STA. 10+00

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 r.pastorano





6/23/16

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770 770

760 760

750 750

740 740

790 790

780 780

770 770

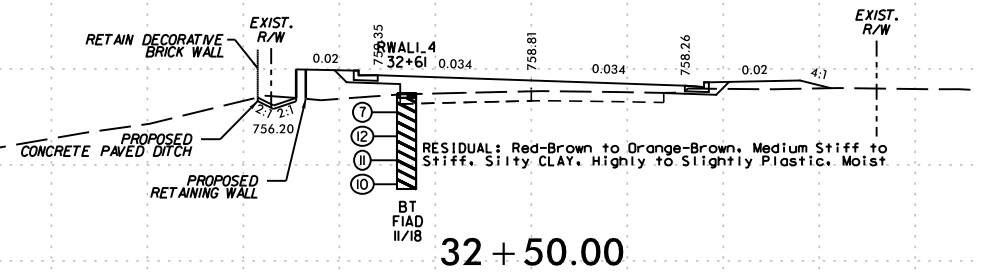
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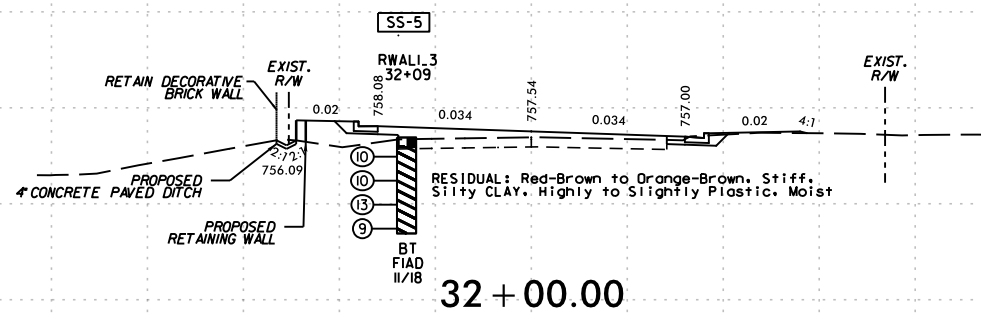
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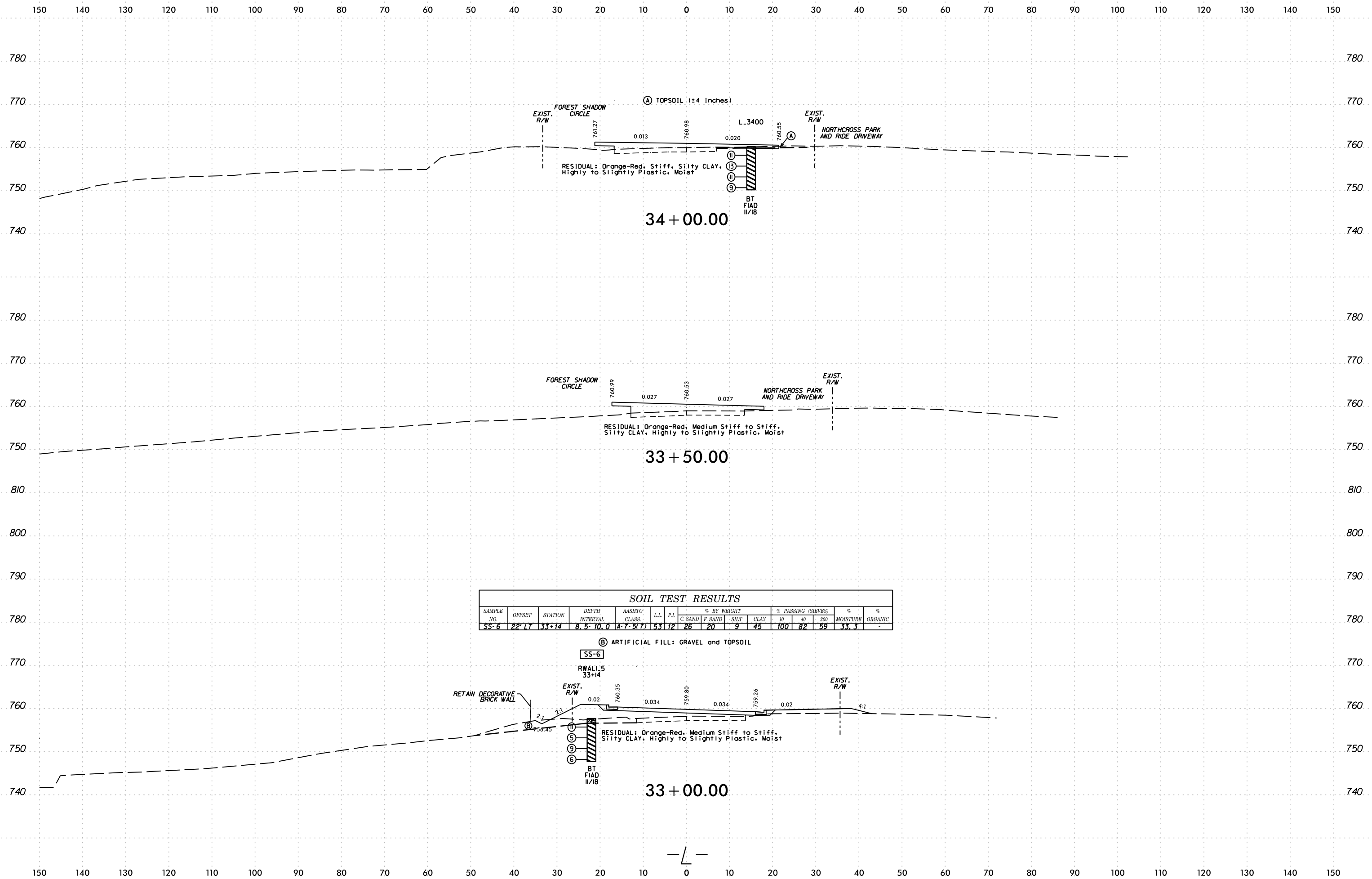
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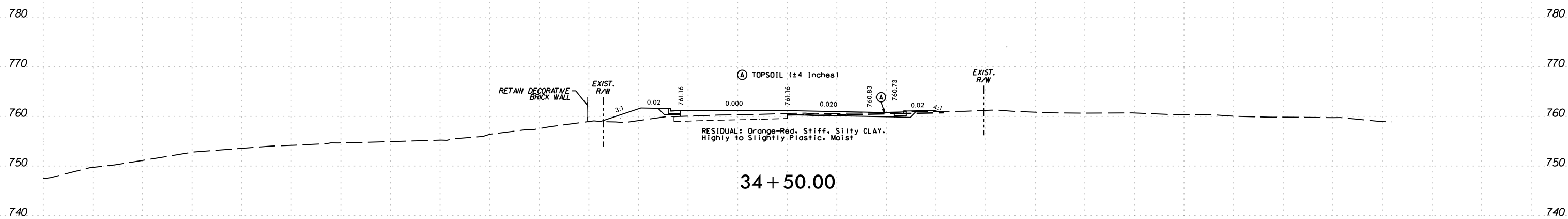
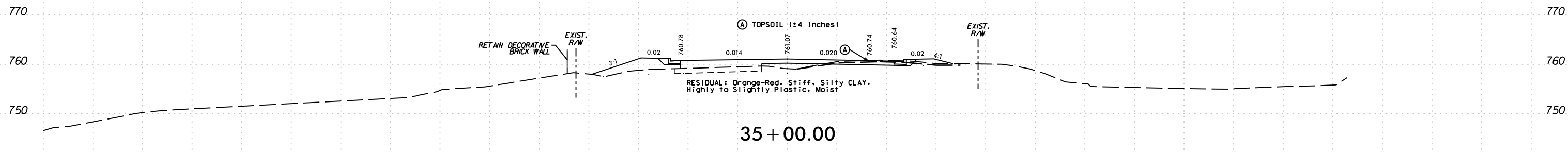
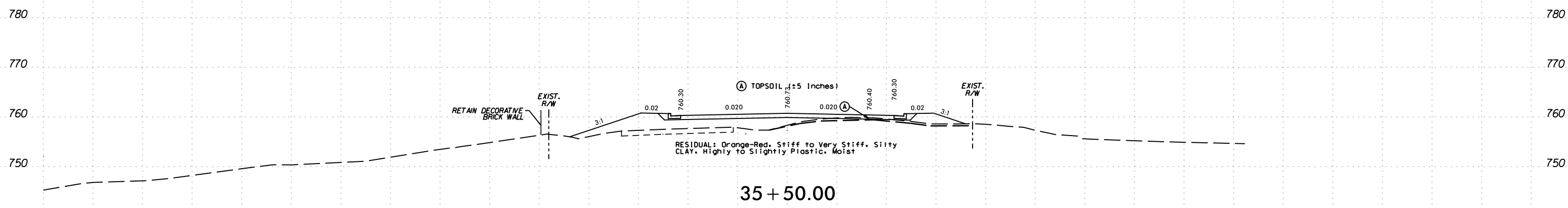
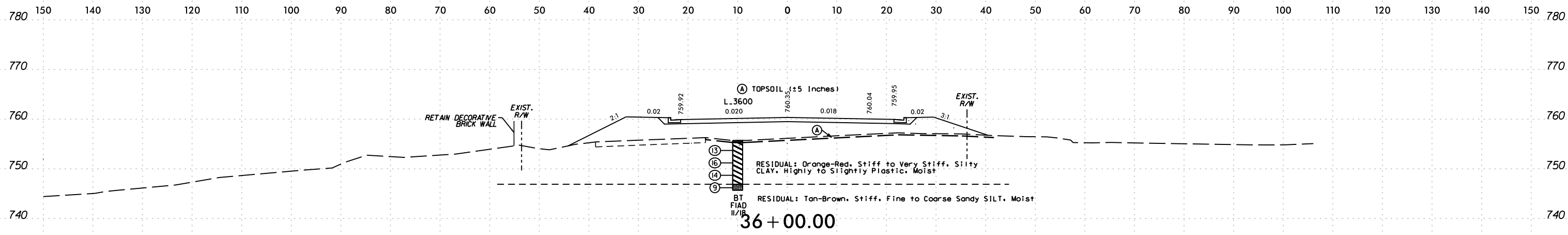
SOIL TEST RESULTS																
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC	
							C. SAND	F. SAND	SILT	CLAY	10	40	200			
SS-5	13' LT	32+09	1.0-2.5	A-7-5	27	11	41	21	16	13	50	99	87	66	30.0	-



—L—



SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-6	22' LT	33+14	8.5 - 10.0	A-7.5(7)	53	12	26	20	9	45	100	82	59	33.3	-

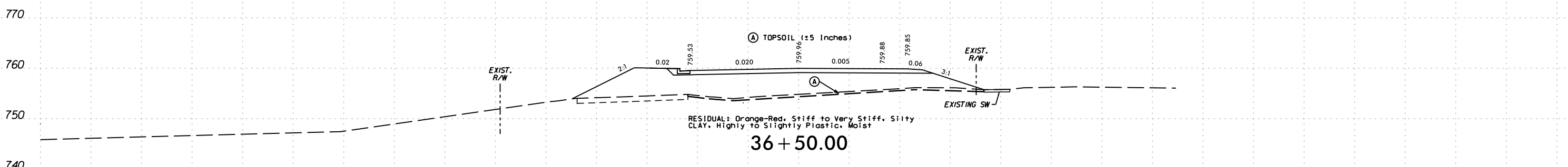
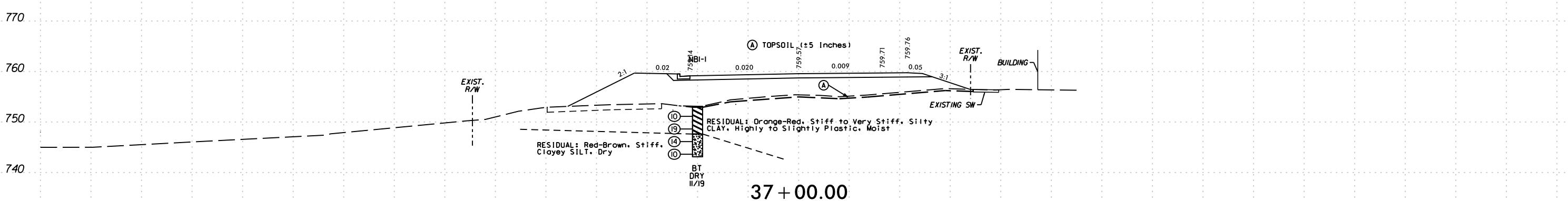
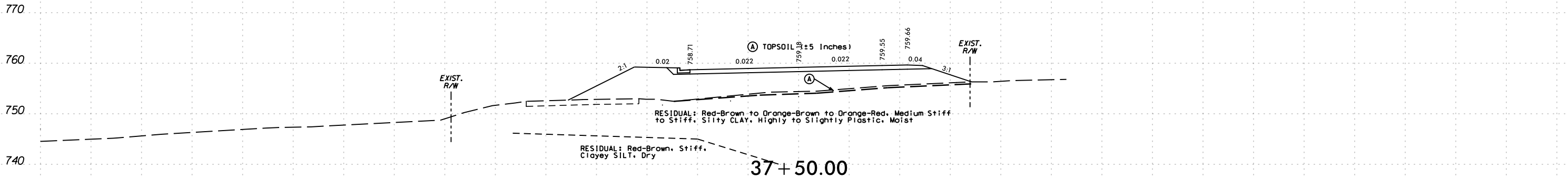


6/23/16



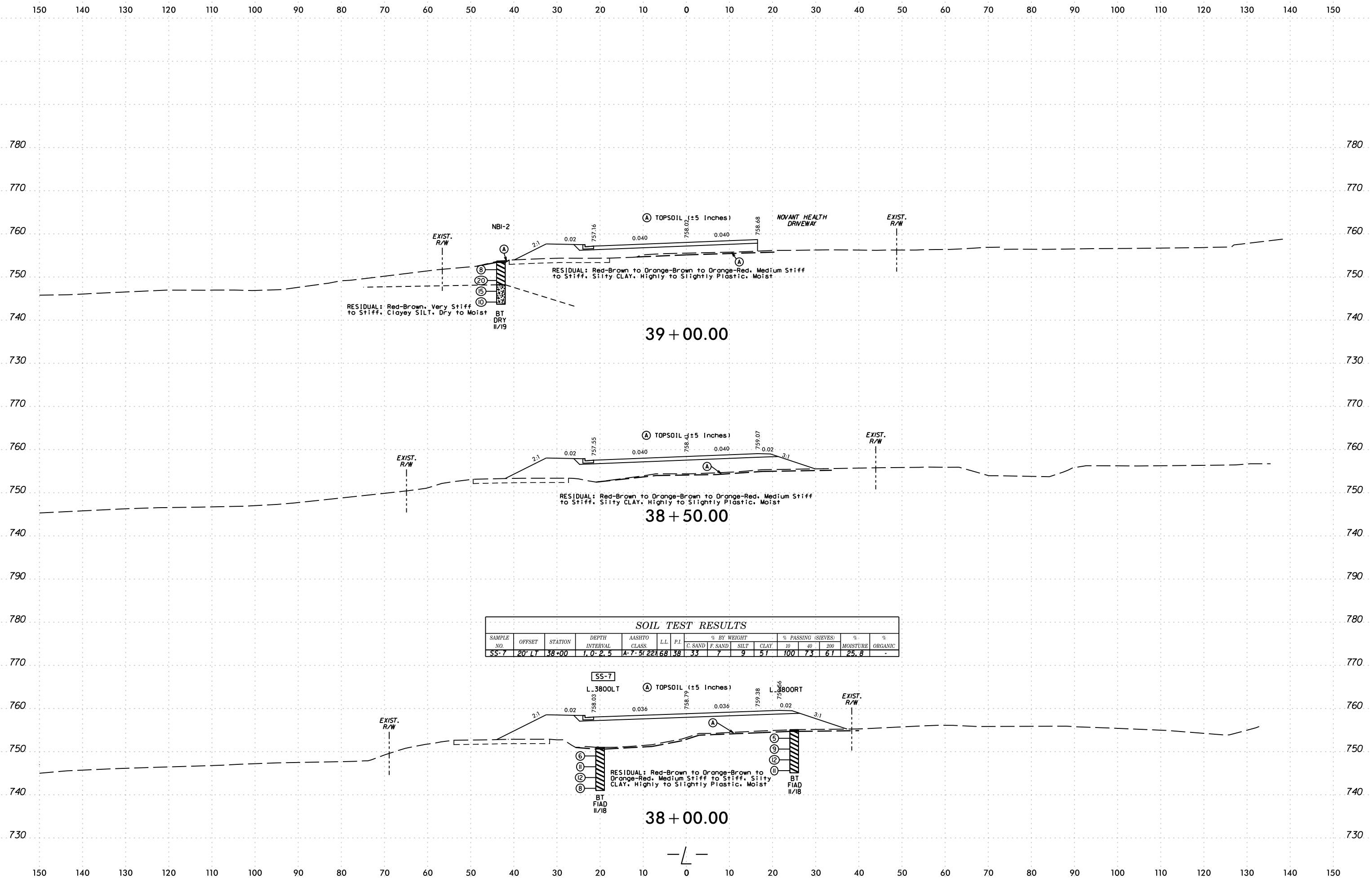
PROJ. REFERENCE NO.	SHEET NO.
U-5108	19

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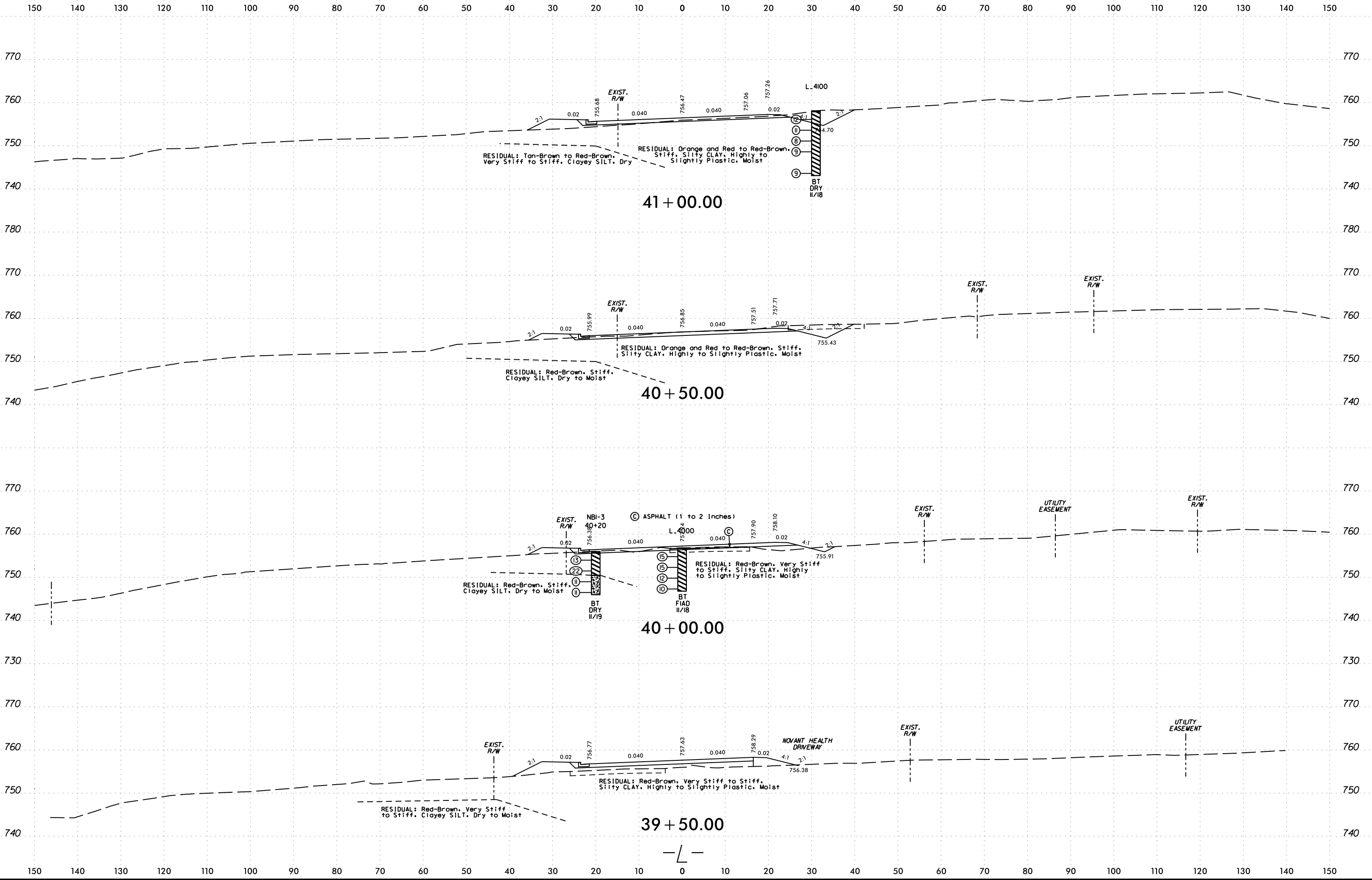


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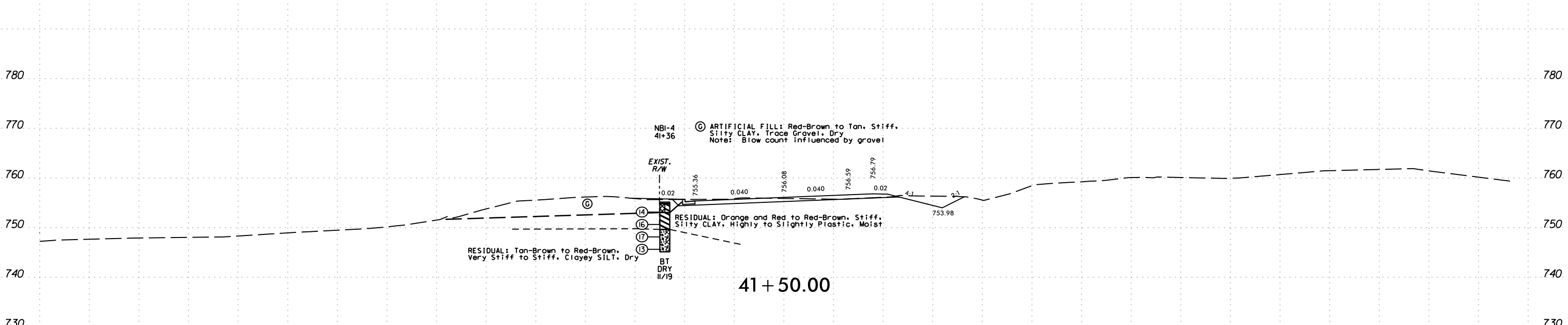
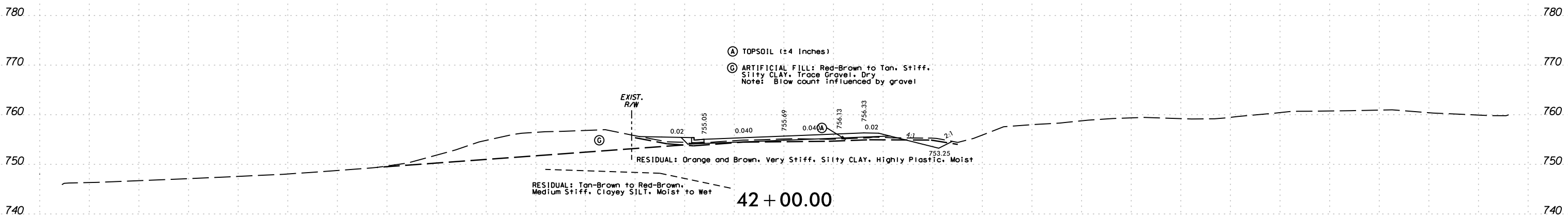
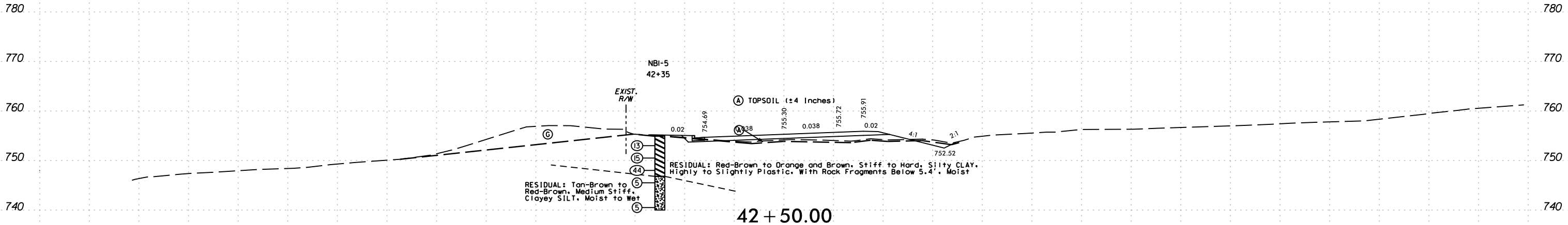


6/23/16

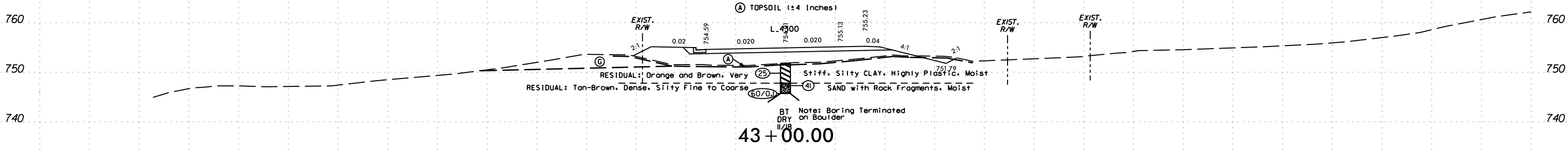
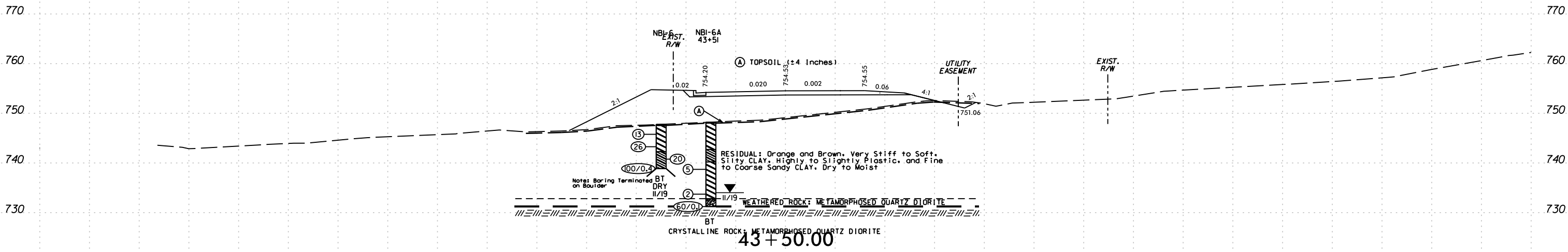
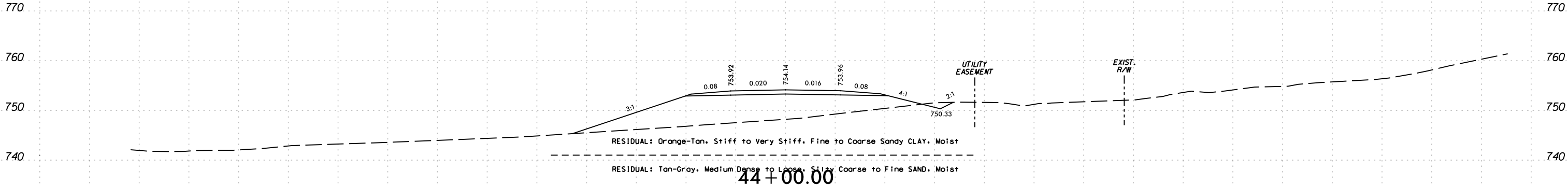


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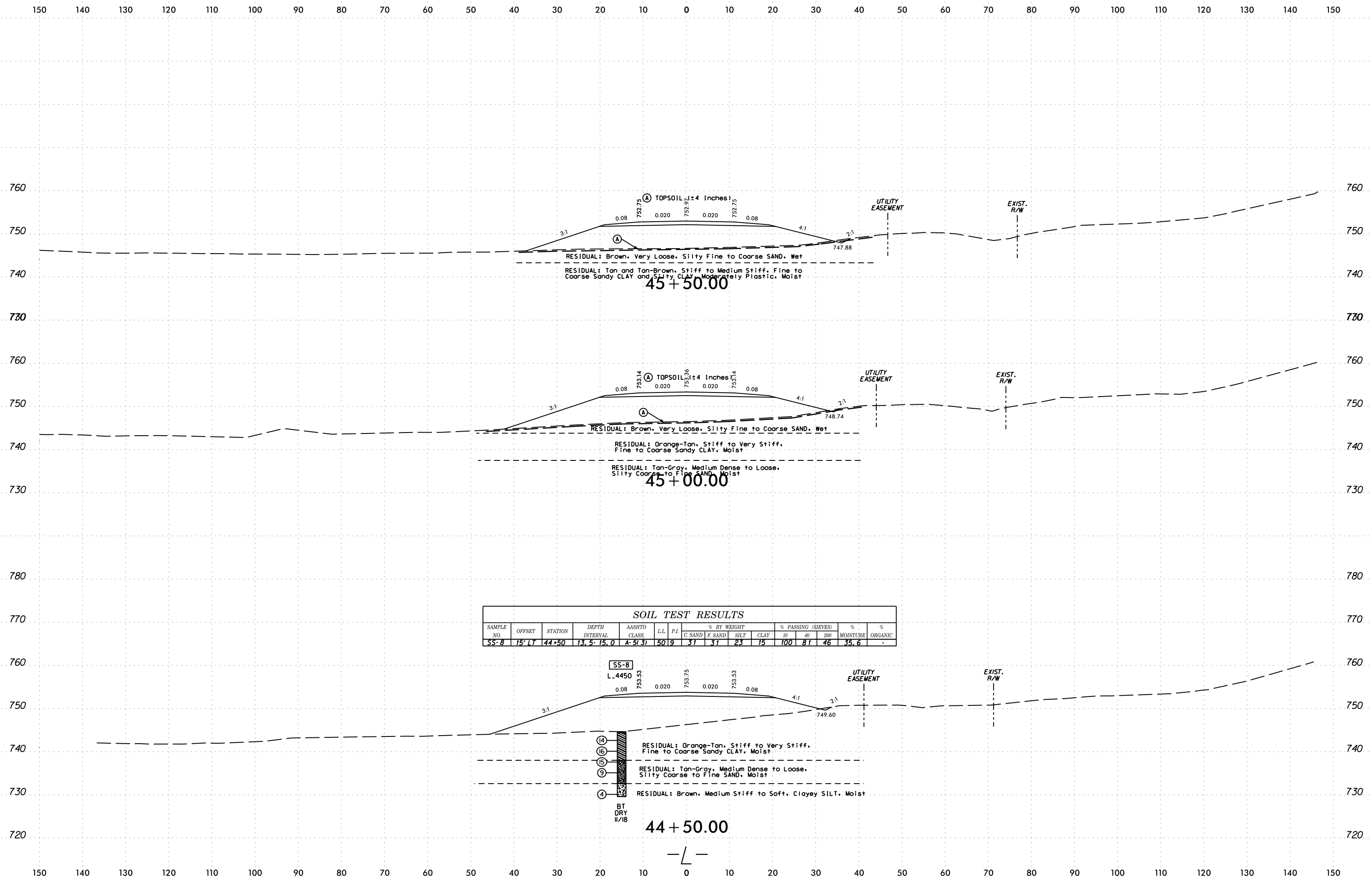


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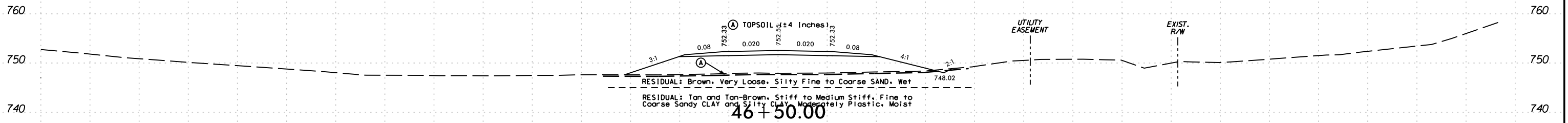
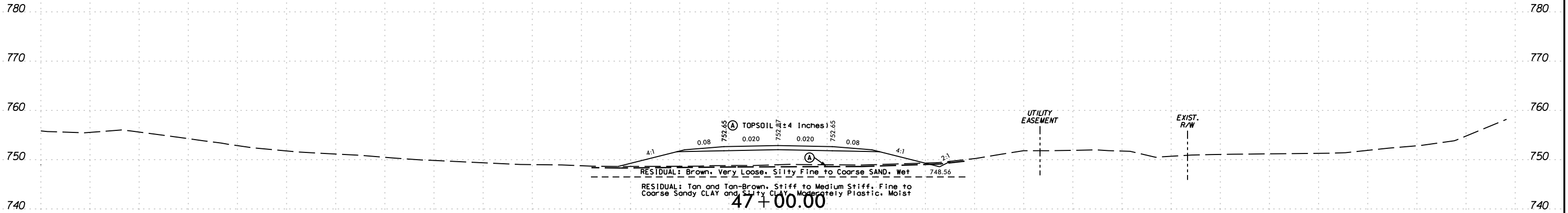


SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-8	15' LT	44+50	13.5-15.0	A-5(3)	50	19	31	31	23	15	100	81	46	35.6	-

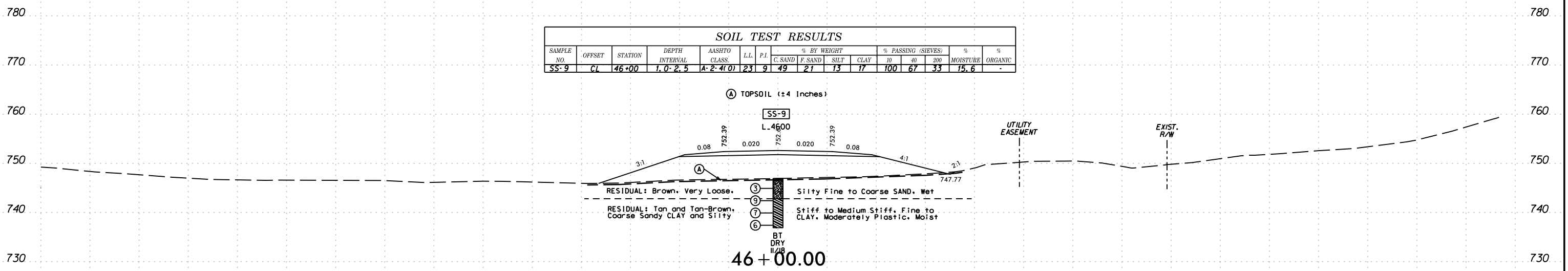
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 r.pastorano

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SOIL TEST RESULTS

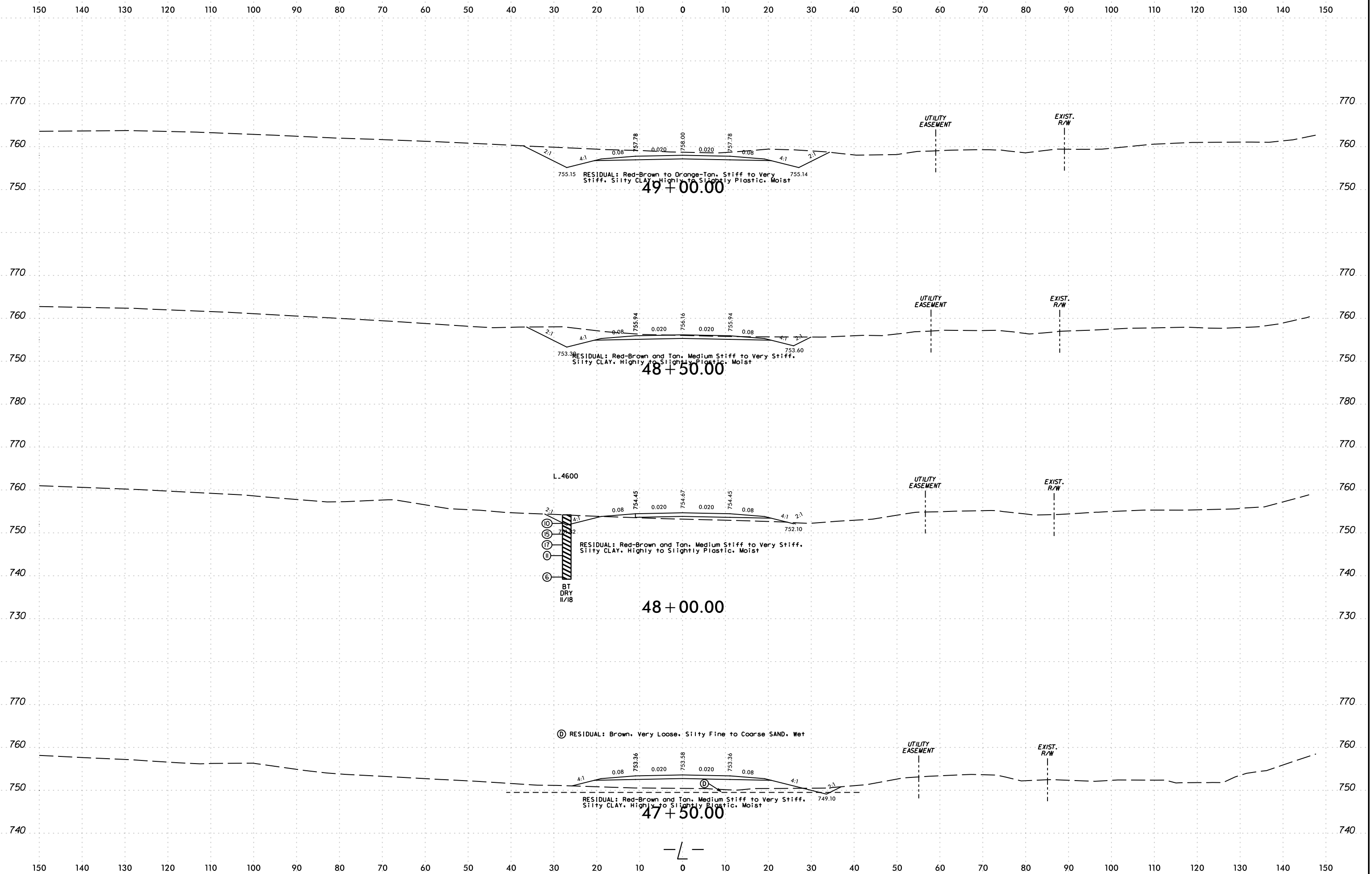
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							C. SAND	F. SAND	SILT	CLAY	10	40			200
SS-9	CL	46+00	1.0-2.5	A-2-4(0)	23	9	49	21	13	17	100	67	33	15.6	-



6/23/16



PROJ. REFERENCE NO.	SHEET NO.
U-5108	26



RESIDUAL: Red-Brown to Orange-Tan, Stiff to Very Stiff, Silty CLAY, Highly to Slightly Plastic, Moist

49 + 00.00

RESIDUAL: Red-Brown and Tan, Medium Stiff to Very Stiff, Silty CLAY, Highly to Slightly Plastic, Moist

48 + 50.00

RESIDUAL: Red-Brown and Tan, Medium Stiff to Very Stiff, Silty CLAY, Highly to Slightly Plastic, Moist

48 + 00.00

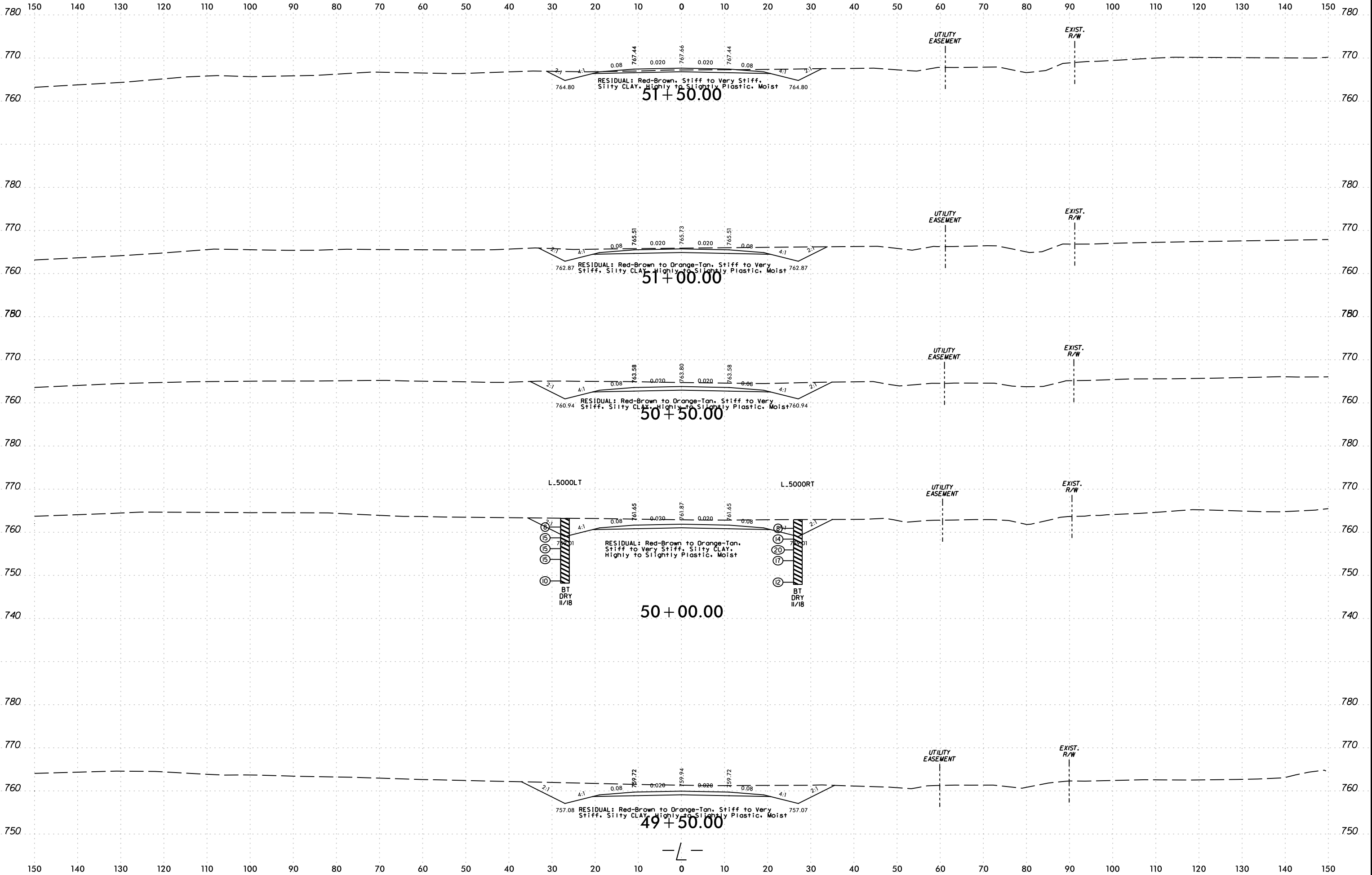
RESIDUAL: Brown, Very Loose, Silty Fine to Coarse SAND, Wet

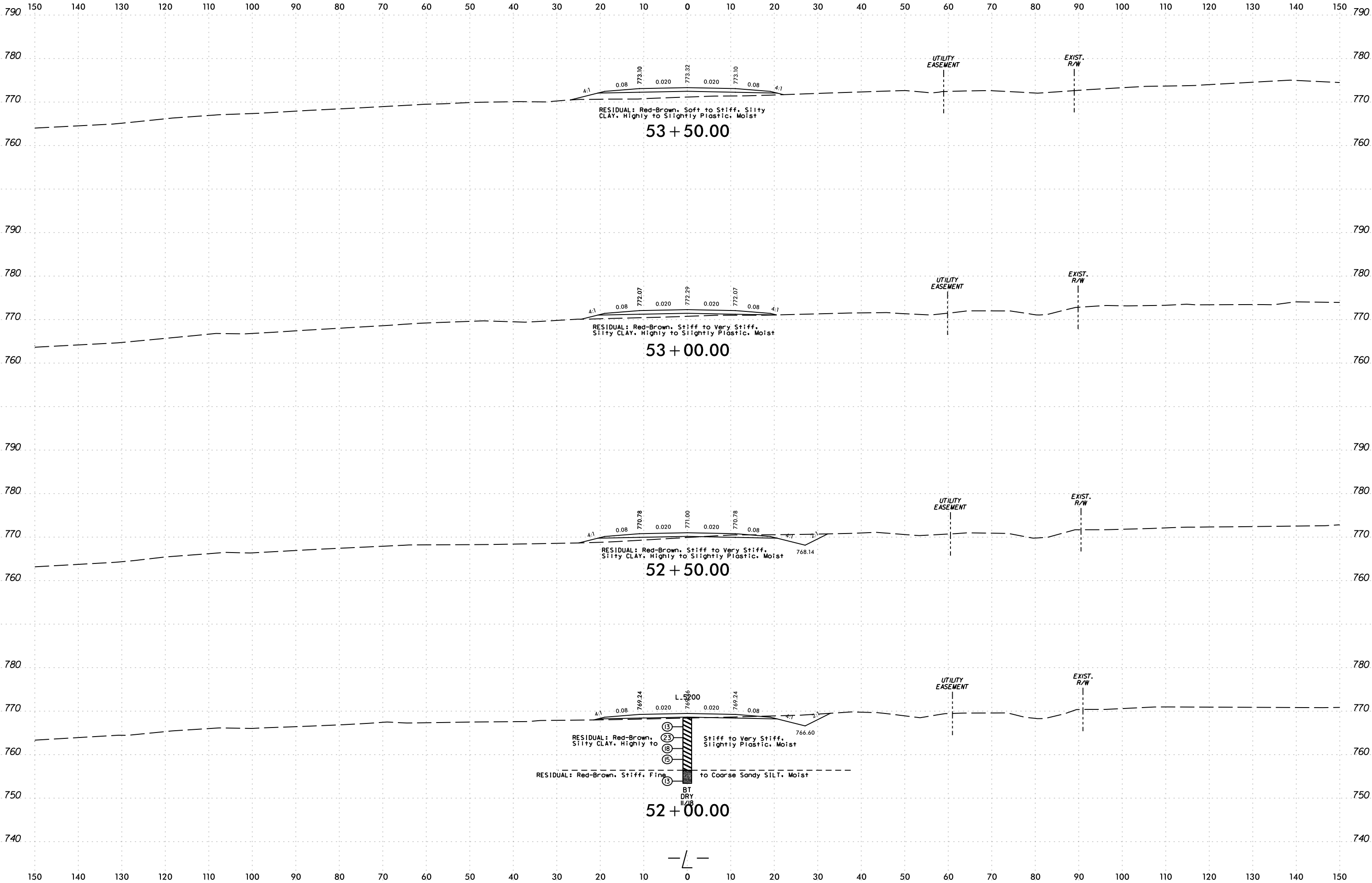
47 + 50.00

RESIDUAL: Red-Brown and Tan, Medium Stiff to Very Stiff, Silty CLAY, Highly to Slightly Plastic, Moist

-L-

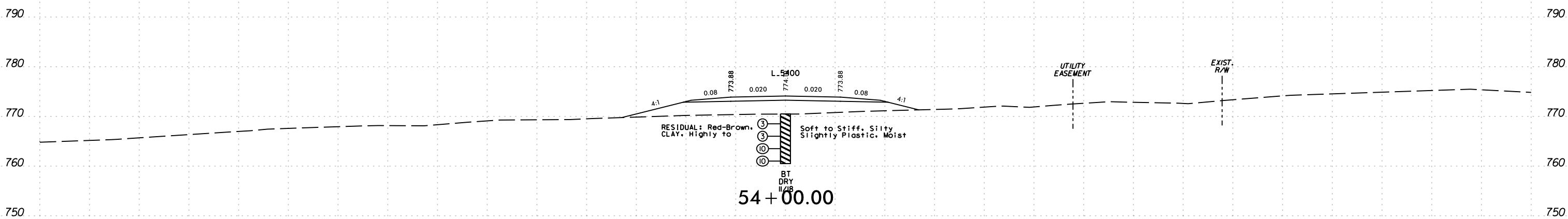
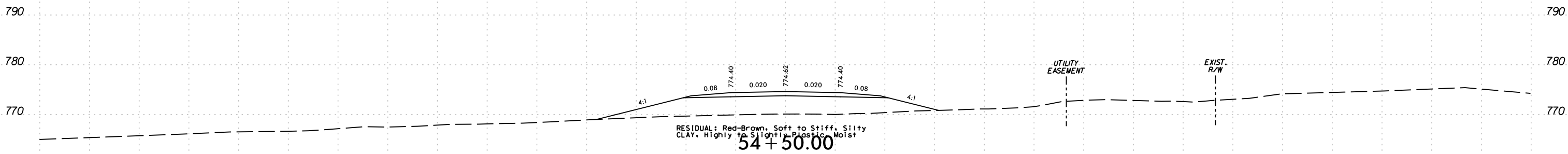
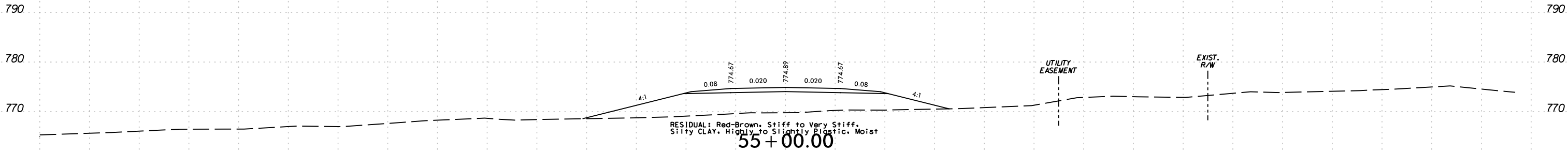
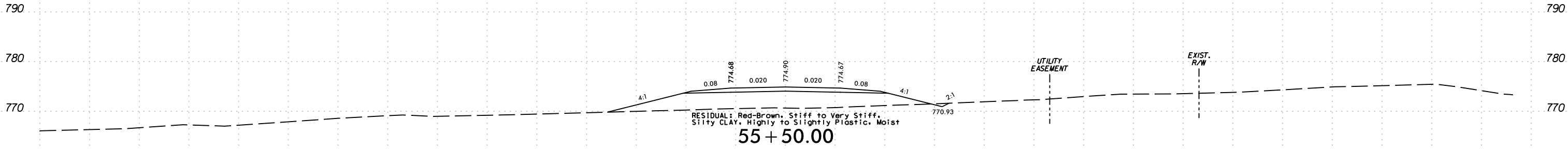
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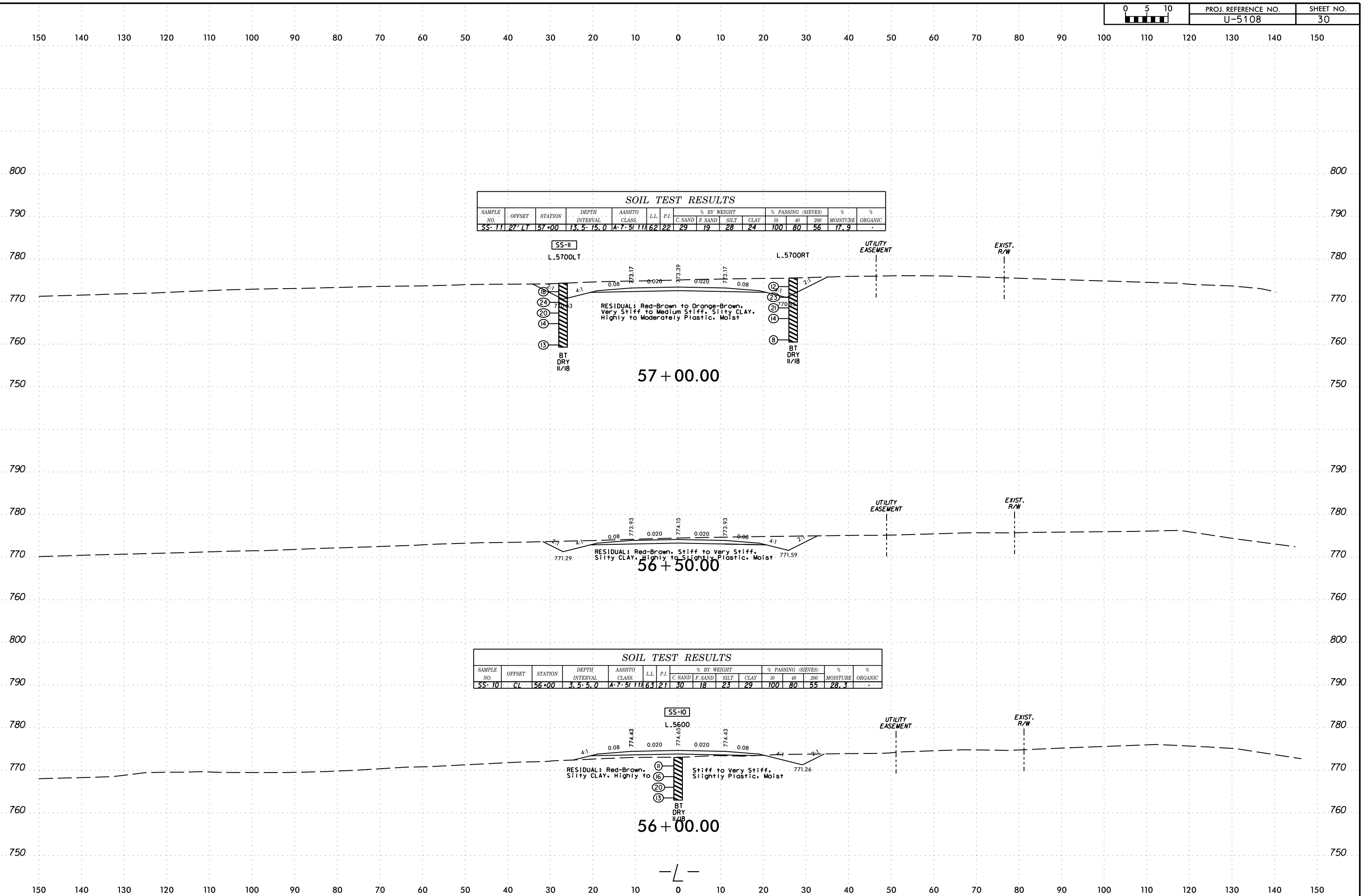






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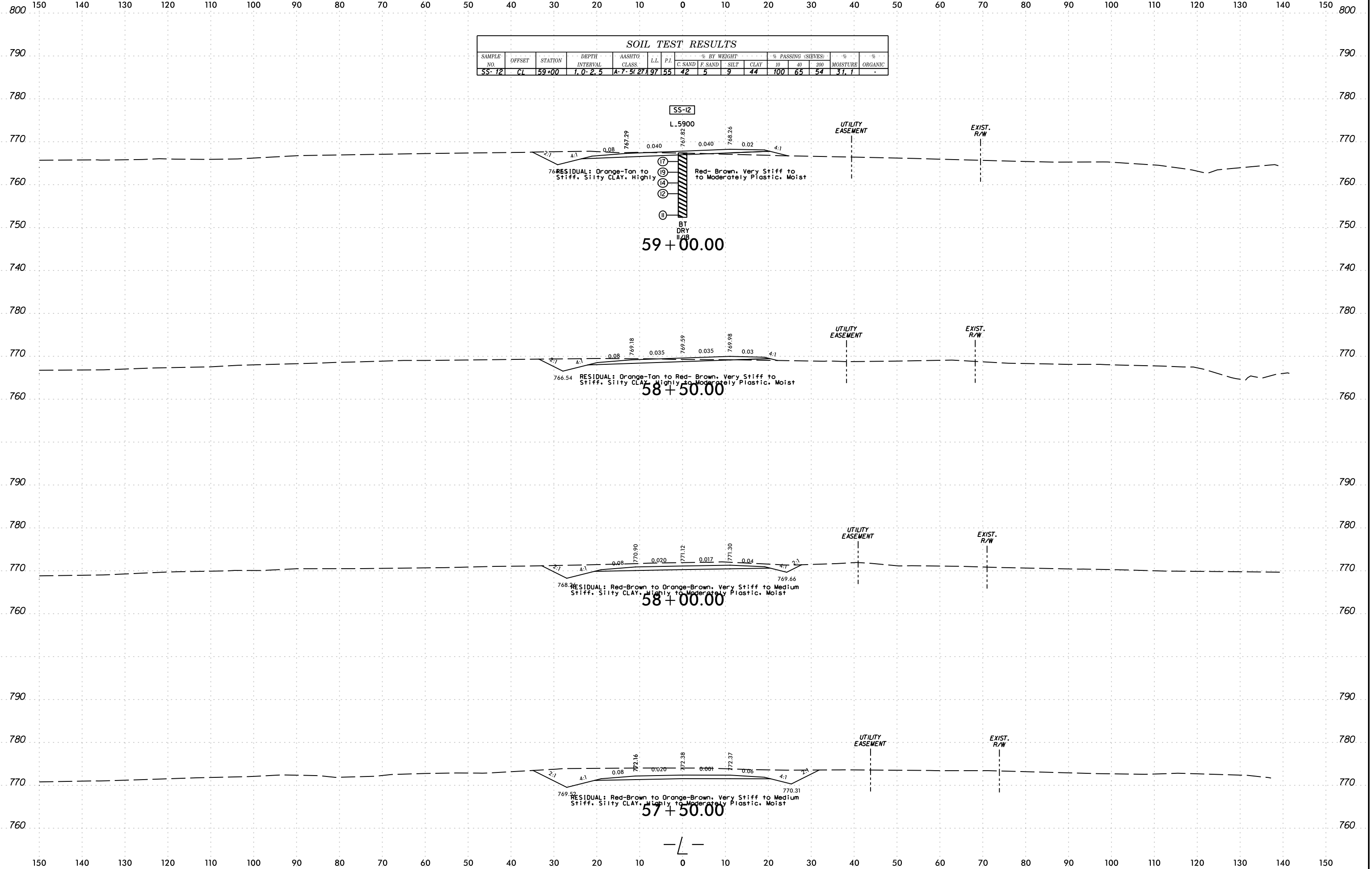
SOIL TEST RESULTS

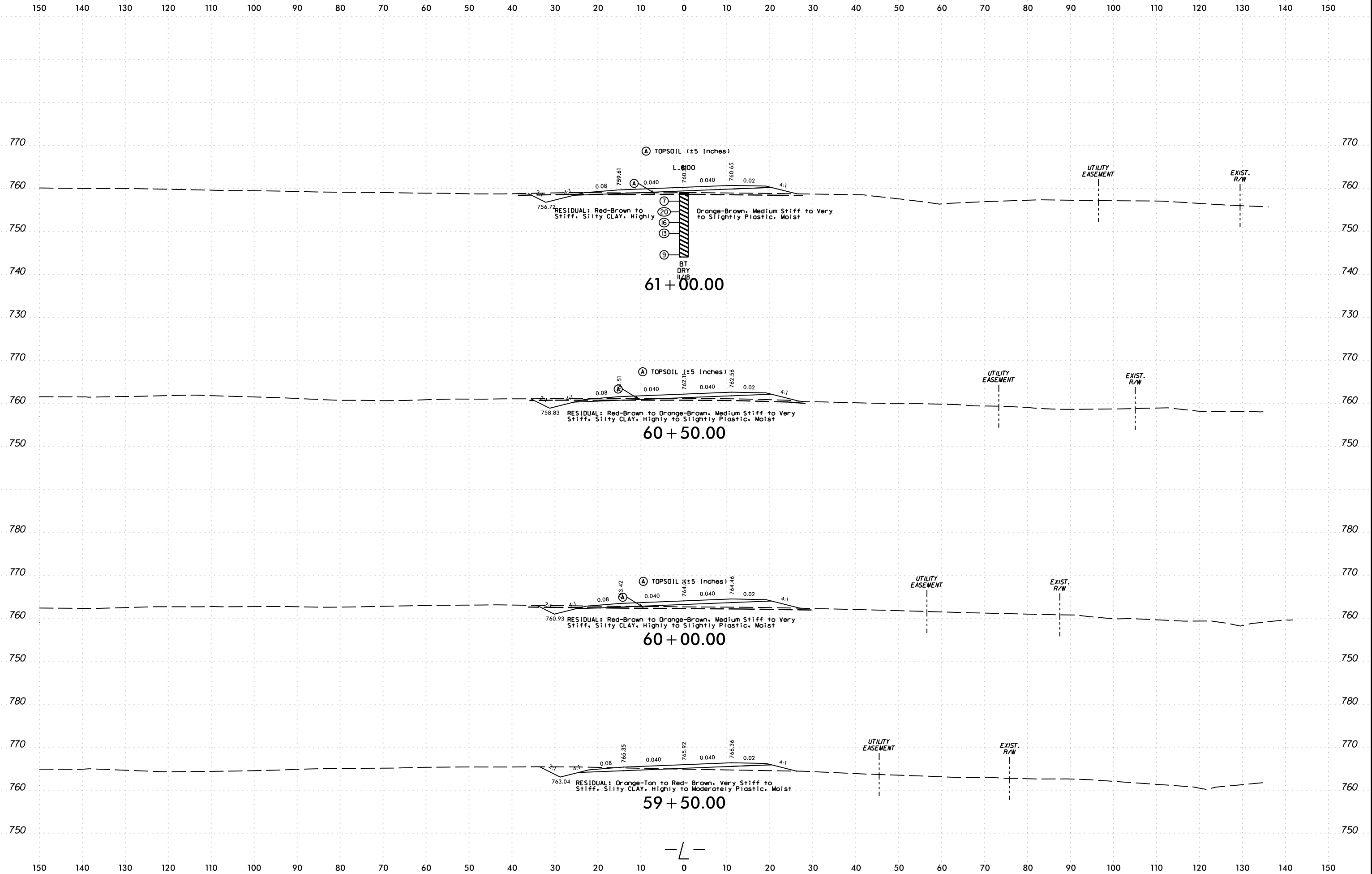
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							C. SAND	F. SAND	SILT	CLAY	#10	#40	#200		
SS-11	27' LT	57+00	13.5- 15.0	A-7.5(1)	62	22	29	19	28	24	100	80	56	17.9	-

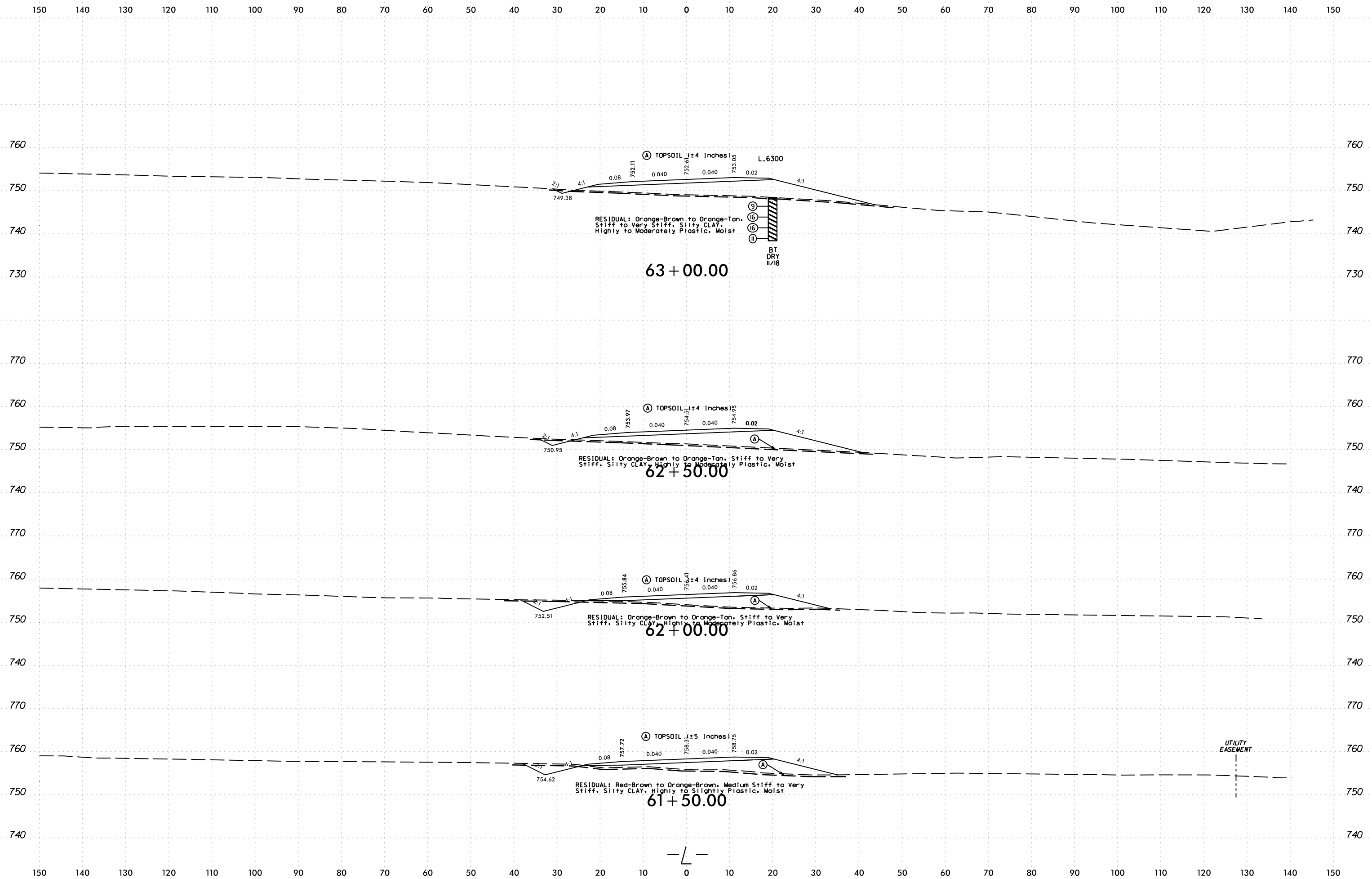
SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	#10	#40	#200		
SS-10	CL	56+00	3.5- 5.0	A-7.5(1)	63	21	30	18	23	29	100	80	55	28.3	-

SOIL TEST RESULTS																
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			MOISTURE	ORGANIC	
							C SAND	F SAND	SILT	CLAY	10	40	200			
SS-12	CL	59+00	1.0-2.5	A-7.5	27	19	55	42	5	9	44	100	65	54	31.1	-







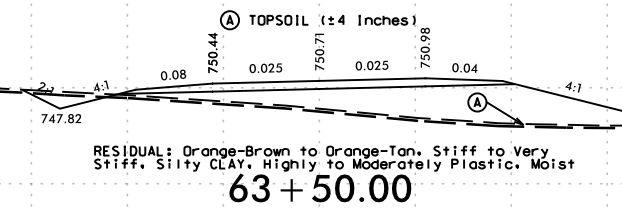
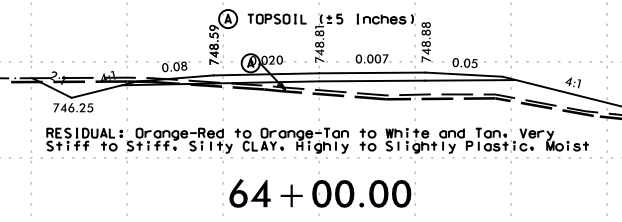
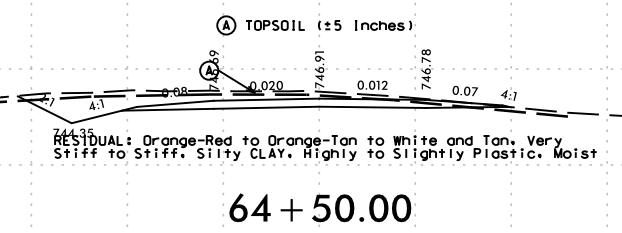
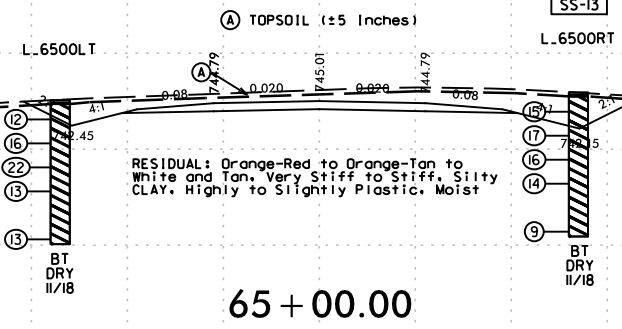
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UTILITY EASEMENT

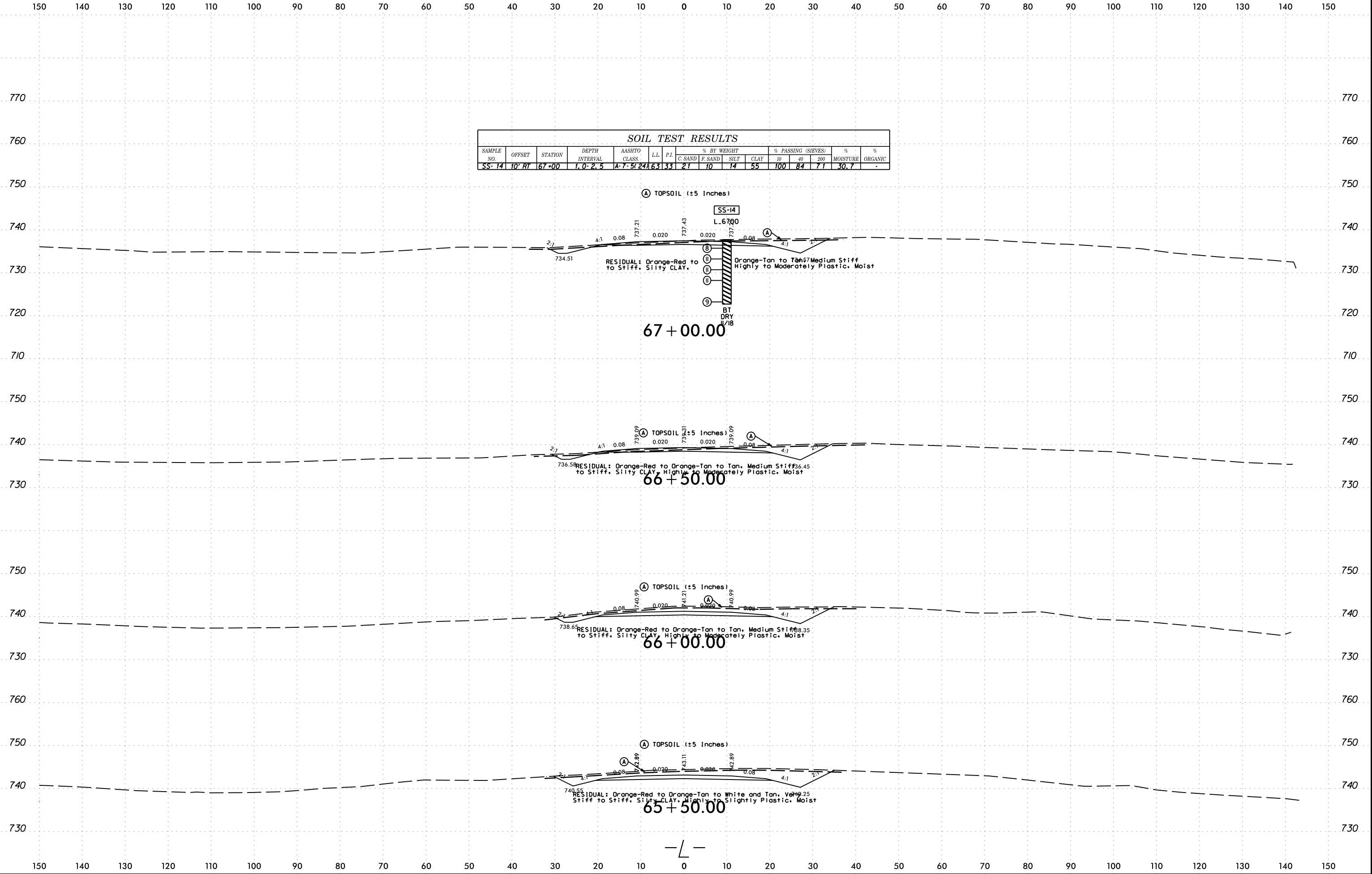
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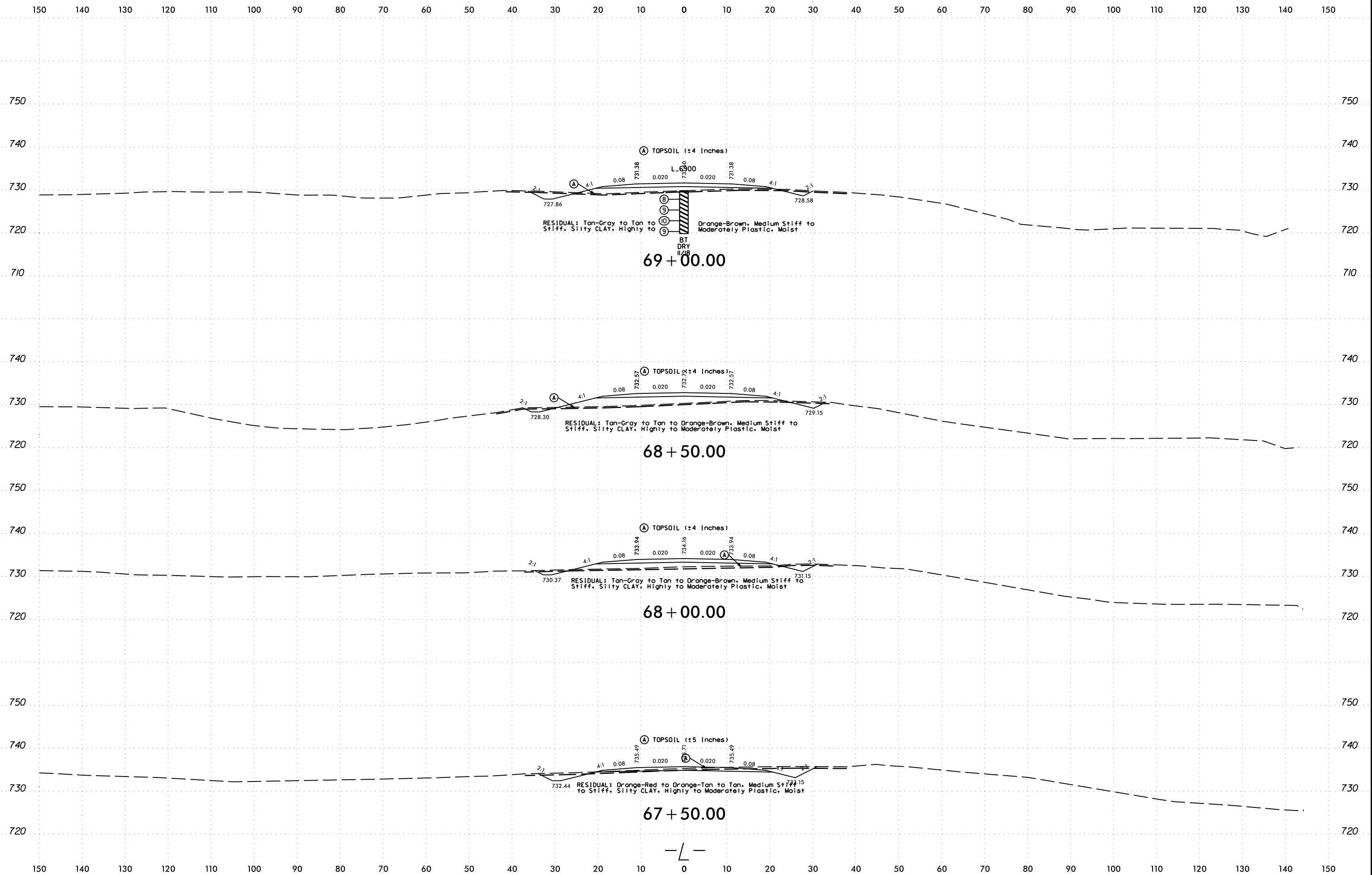
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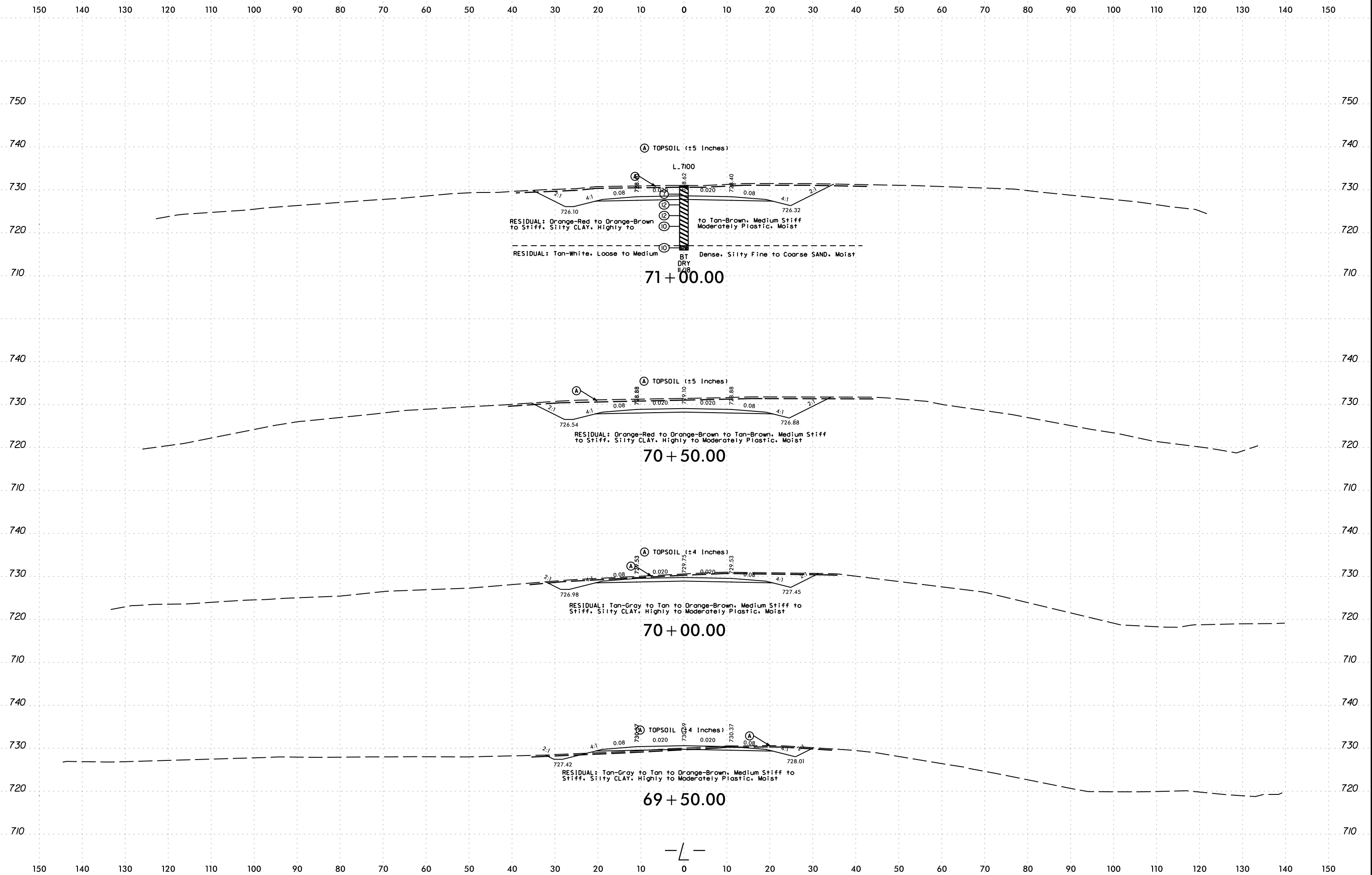
SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-13	27' RT	65+00	8.5-10.0	A-7.5(9)	51	18	28	21	28	23	99	79	56	15.8	-



— L —





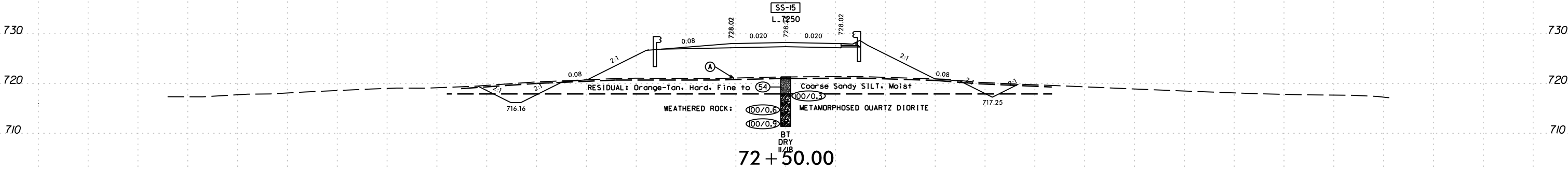


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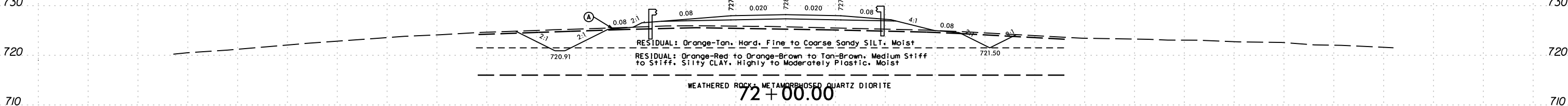
760 750 740 730 720 710 700 750 740 730 720 710 700 750 740 730 720 710 700

SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-15	CL	72+50	1.0-2.5	A-4(0)	NP	NP	36	32	21	11	96	72	37	15.8	-

(A) TOPSOIL (±4 Inches)

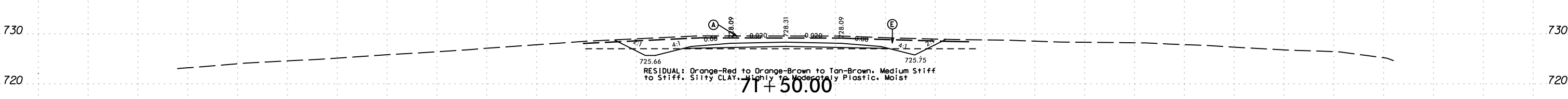


(A) TOPSOIL (±4 Inches)

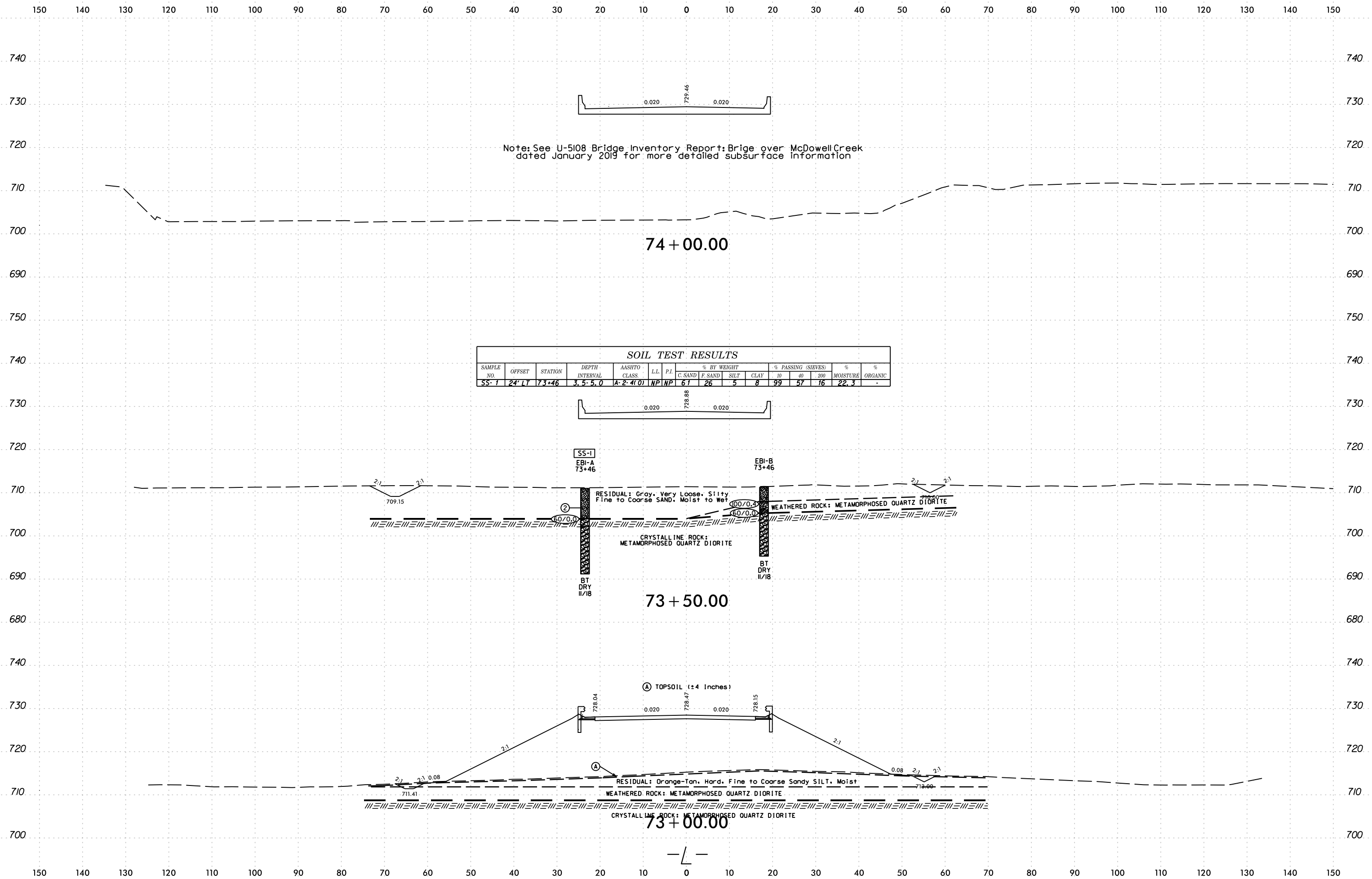


(A) TOPSOIL (±5 Inches)

(E) RESIDUAL: Orange-Tan, Hard, Fine to Coarse Sandy SILT, Moist



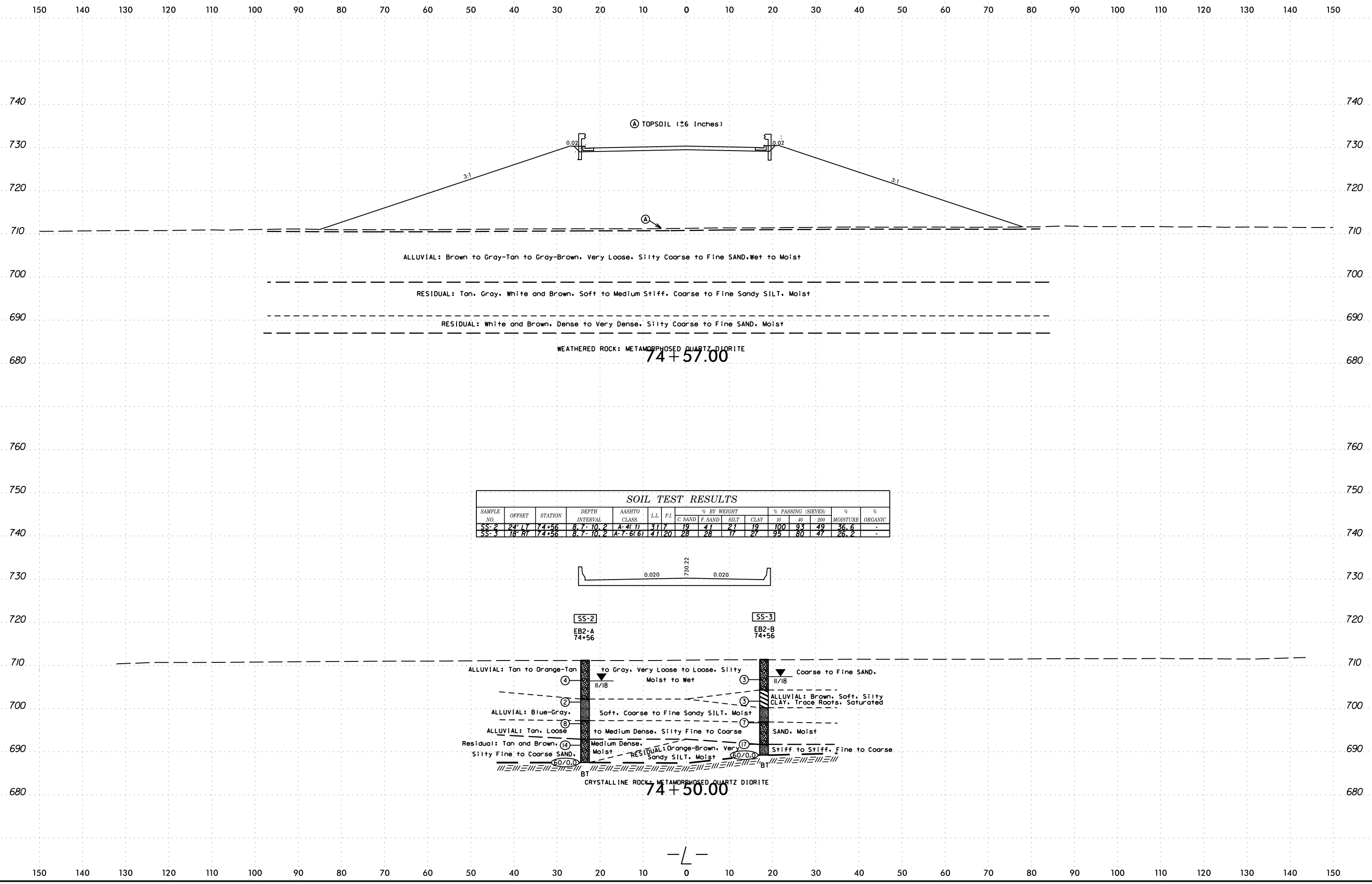
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SOIL TEST RESULTS

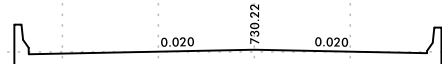
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C SAND	F SAND	SILT	CLAY	10	40	200		
SS-1	24' LT	73+46	3.5'-5.0'	A-2-4(0)	NP	NP	61	26	5	8	99	57	16	22.3	-

12/9/2019 9:34:47 AM
 Z:\Projects\2018\GIS\CV05.300.U-5108 (Northcross)\US108.GEOTECH\XSC\U-5108_Geo_xsi.L.dgn
 rps:ena



SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	PI	% BY WEIGHT				% PASSING (SIEVES)			MOISTURE	ORGANIC
							C. SAND	F. SAND	SILT	CLAY	#10	#40	#200		
SS-2	24' LT	74+56	8.7-10.2	A-4(1)	31.7	19	41	21	19	100	93	49	36.6	-	
SS-3	18' RT	74+56	8.7-10.2	A-7-6(6)	41.20	28	28	17	27	95	80	47	26.2	-	



EB2-A
74+56

EB2-B
74+56

ALLUVIAL: Tan to Orange-Tan to Gray. Very Loose to Loose. Silty Moist to Wet

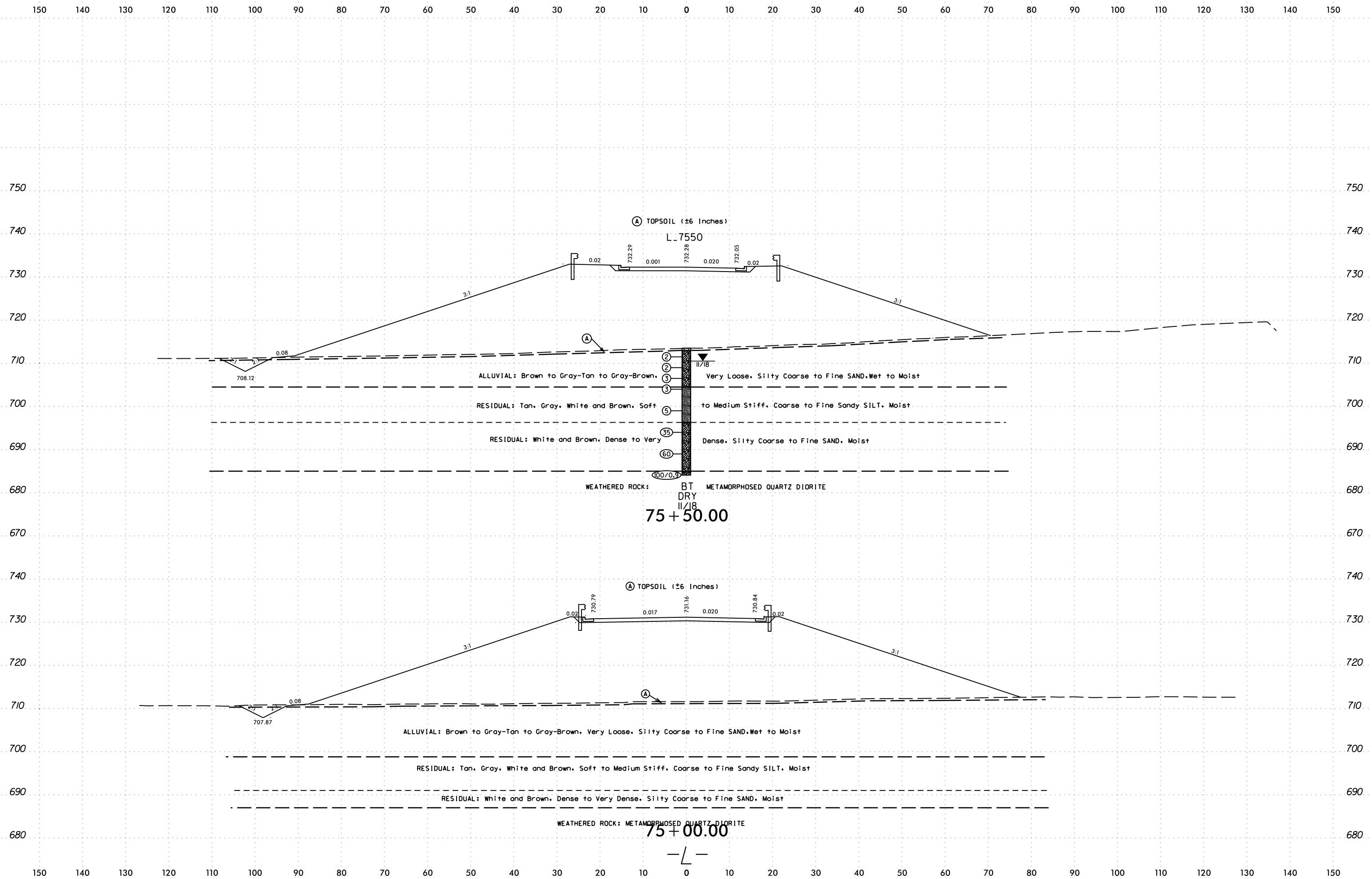
ALLUVIAL: Blue-Gray. Soft. Coarse to Fine Sandy SILT. Moist

ALLUVIAL: Tan, Loose to Medium Dense. Silty Fine to Coarse SAND. Moist

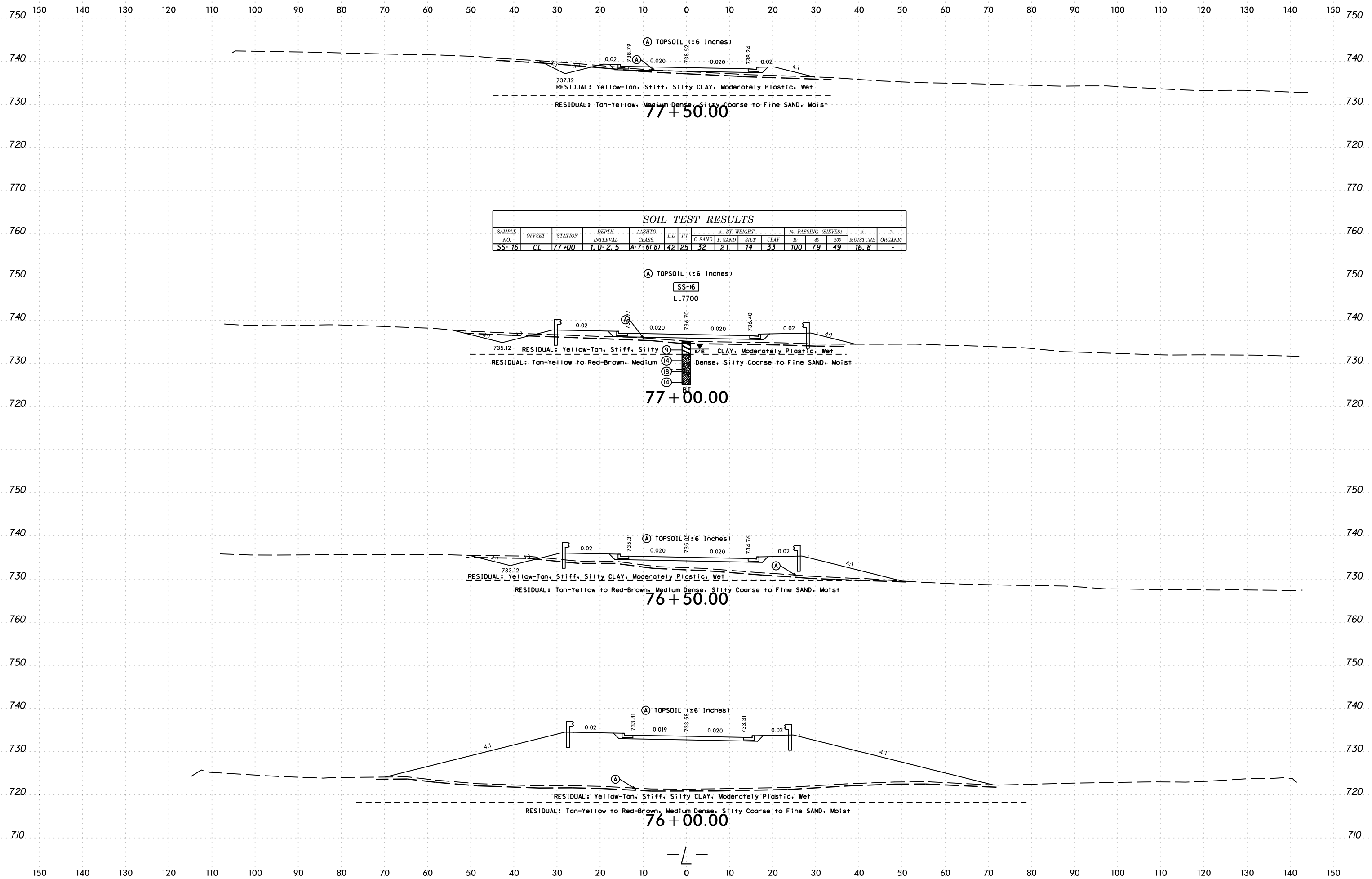
Residual: Tan and Brown. Medium Dense. Moist

RESIDUAL: Orange-Brown. Very Stiff to Stiff. Fine to Coarse Sandy SILT. Moist

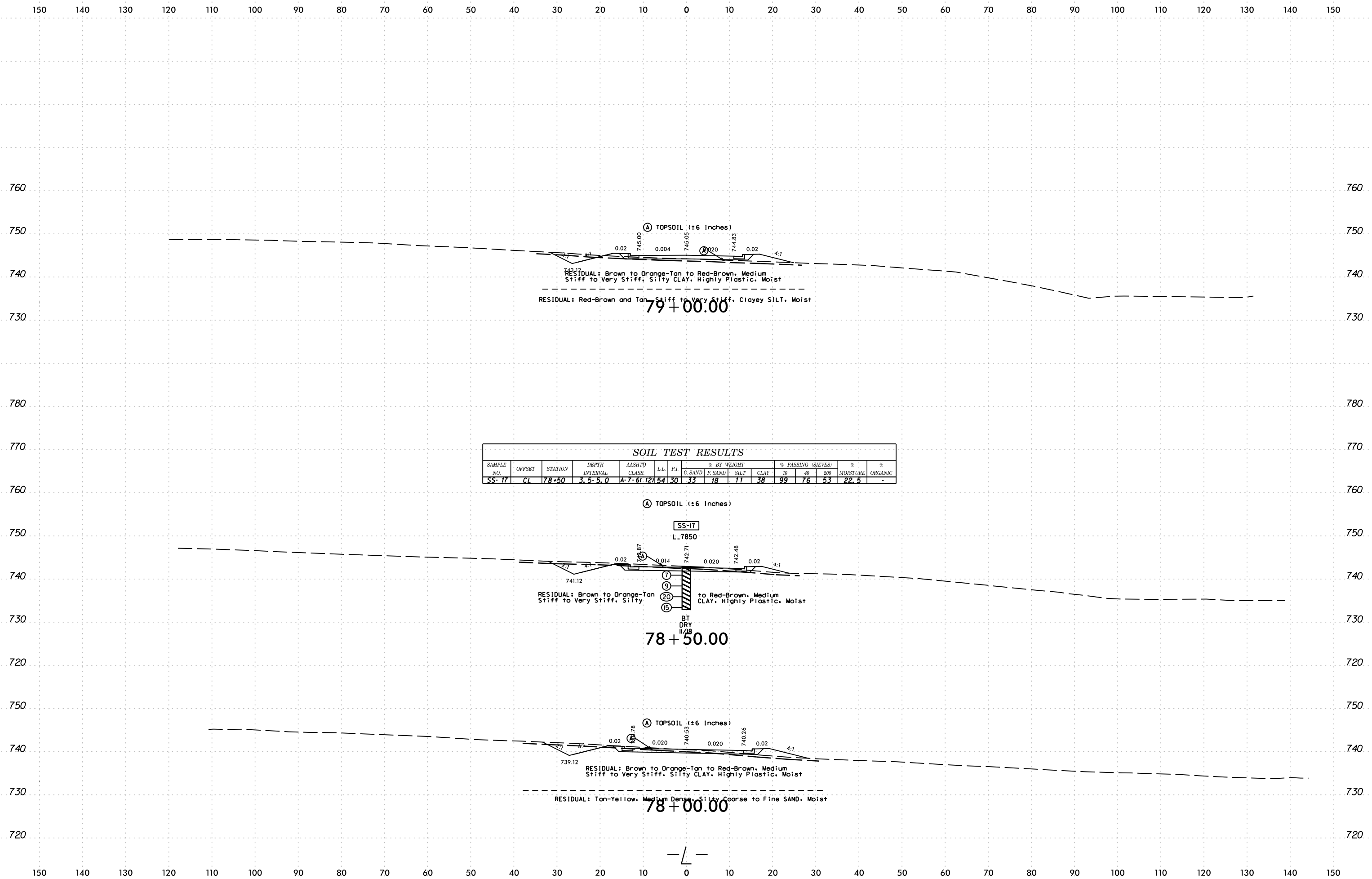
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 r.pastore



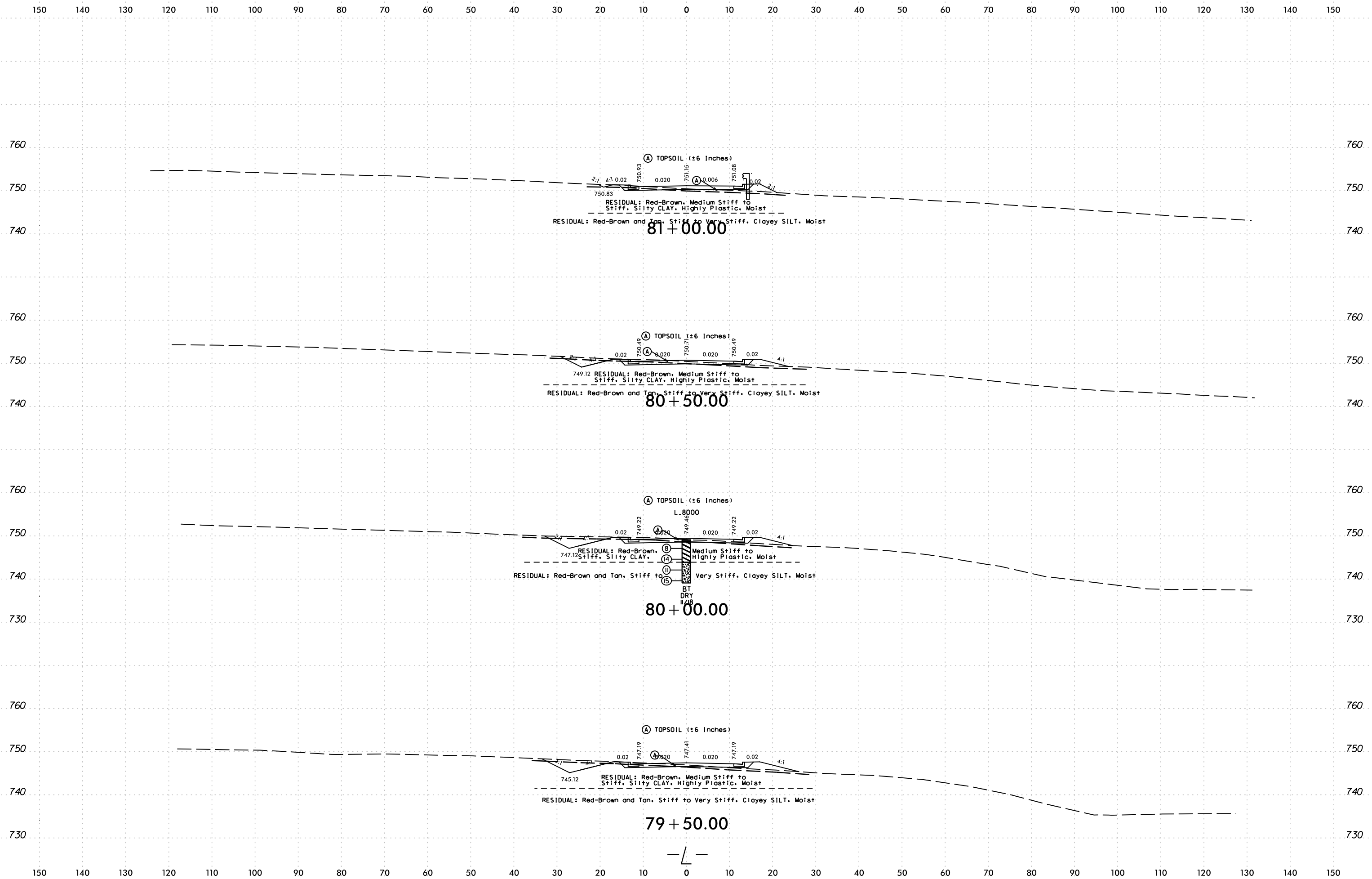
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 r.pastor



SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC	
							C. SAND	F. SAND	SILT	CLAY	#10	#40	#200			
SS-17	CL	78+50	3.5-5.0	A-7-61	121	54	30	33	18	11	38	99	76	53	22.5	-

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 r.pastorano

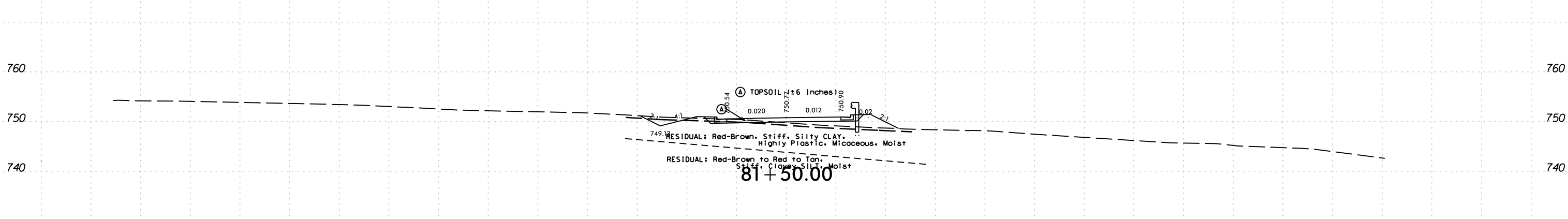
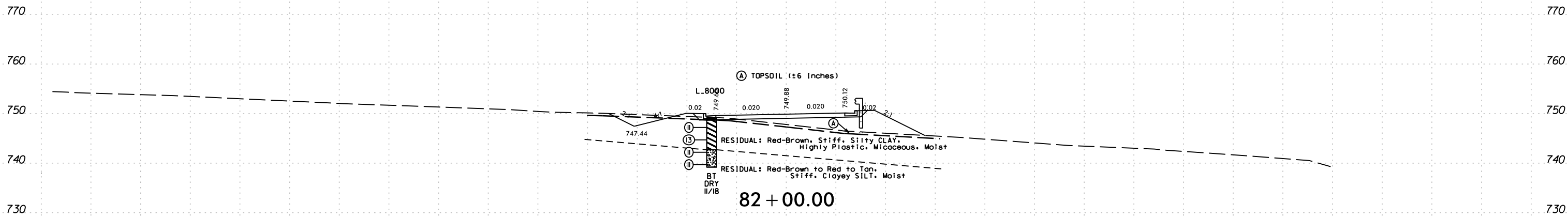
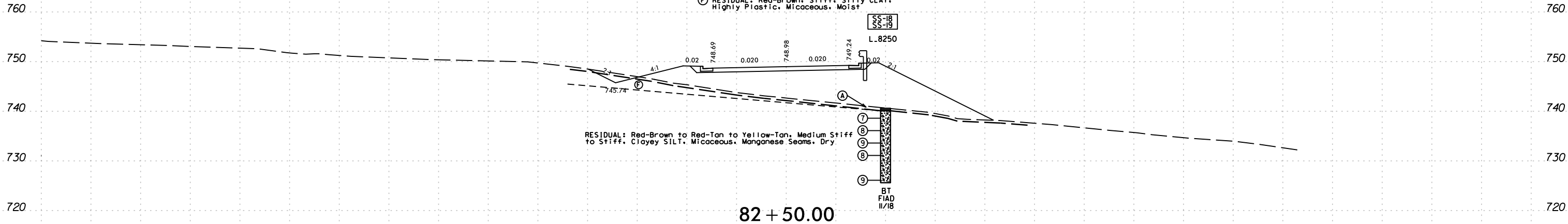


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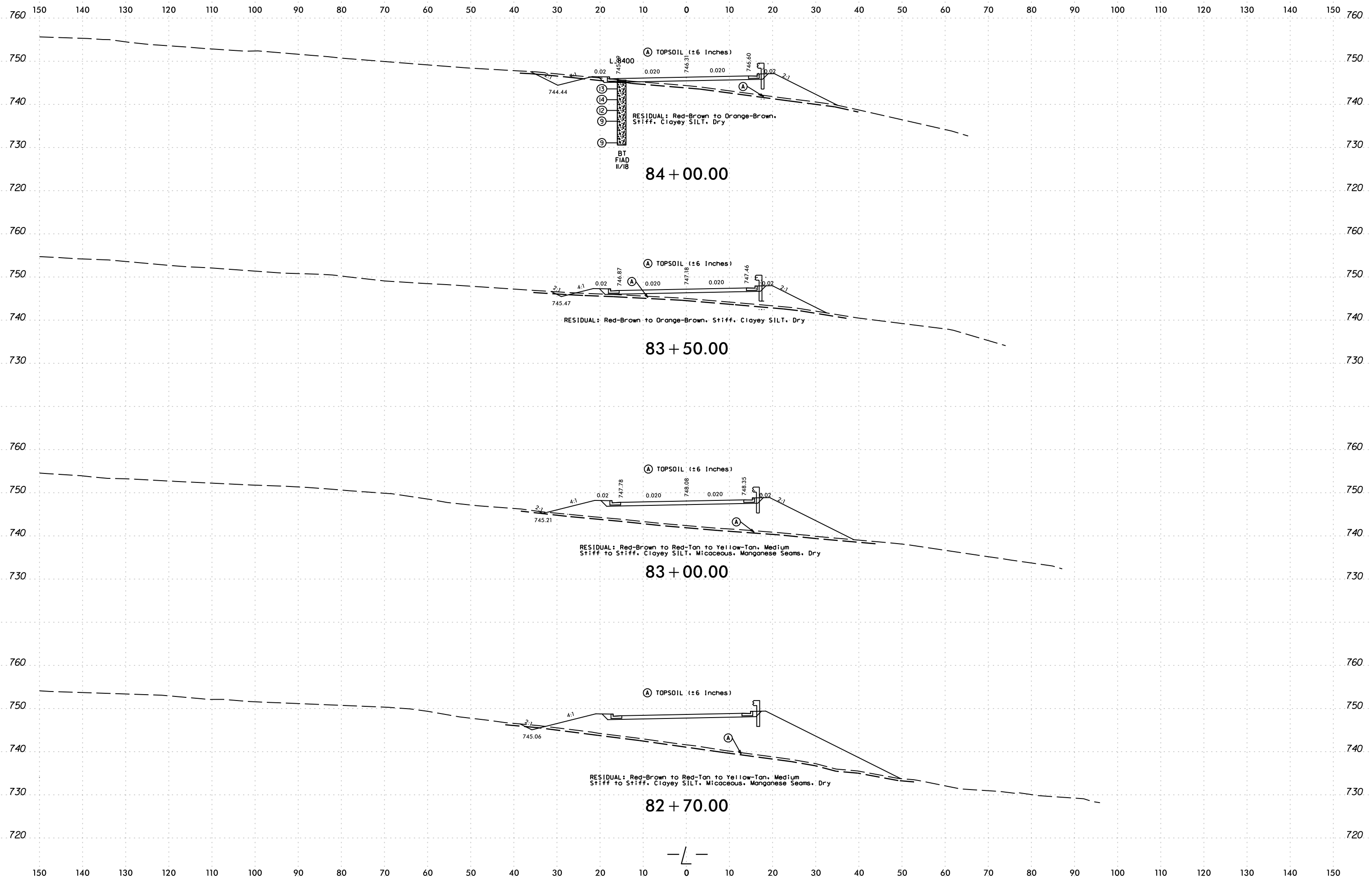
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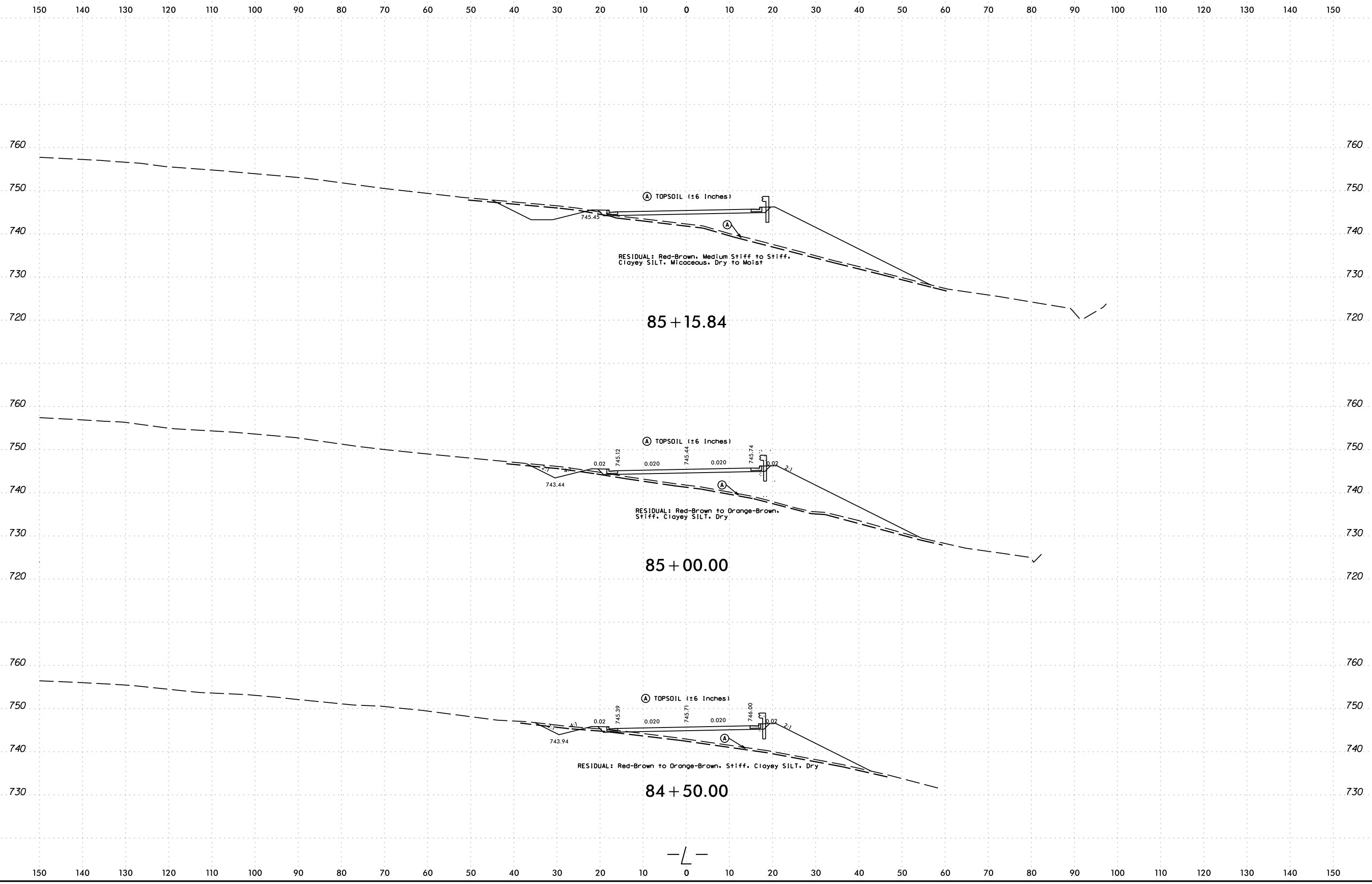
SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	PI	% BY WEIGHT				% PASSING (SIEVES)			MOISTURE	ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-18	20' RT	82+50	3.5-5.0	A-5(3)	51	10	36	21	20	23	100	75	48	27.8	-
SS-19	20' RT	82+50	8.5-10.0	A-5(1)	52	9	37	28	22	13	100	75	42	21.2	-

- (A) TOPSOIL (±6 Inches)
- (F) RESIDUAL: Red-Brown, Stiff, Silty CLAY, Highly Plastic, Micaceous, Moist

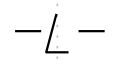


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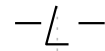
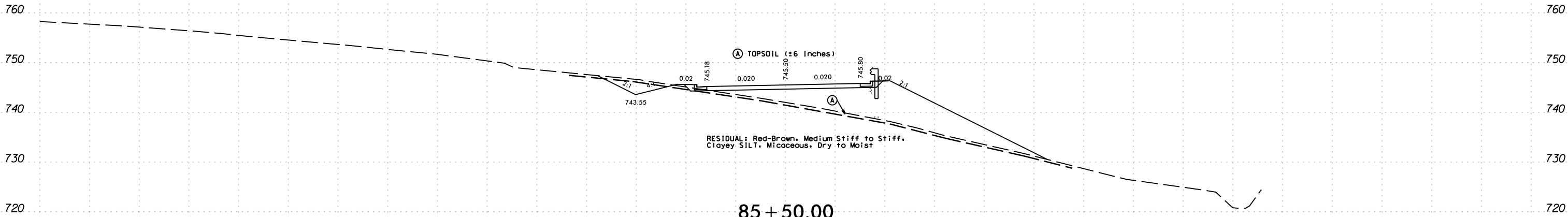
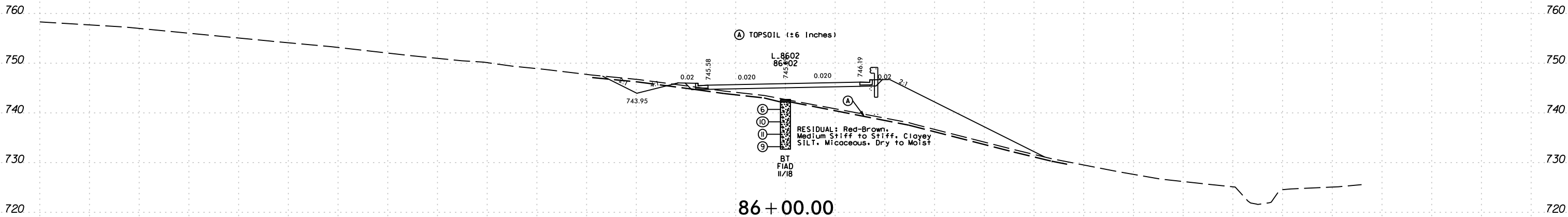
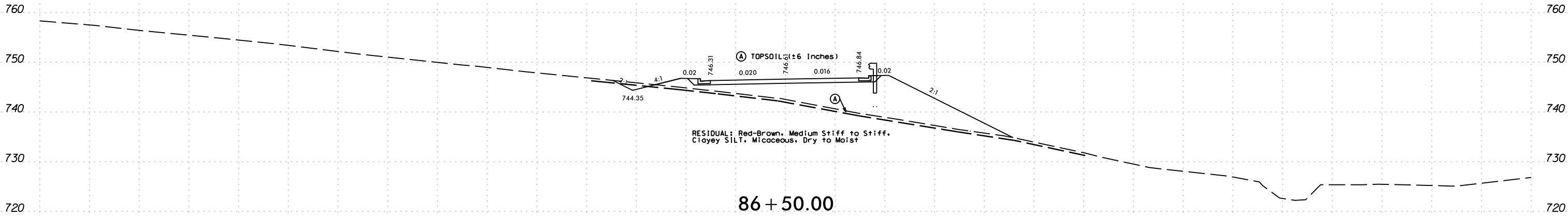


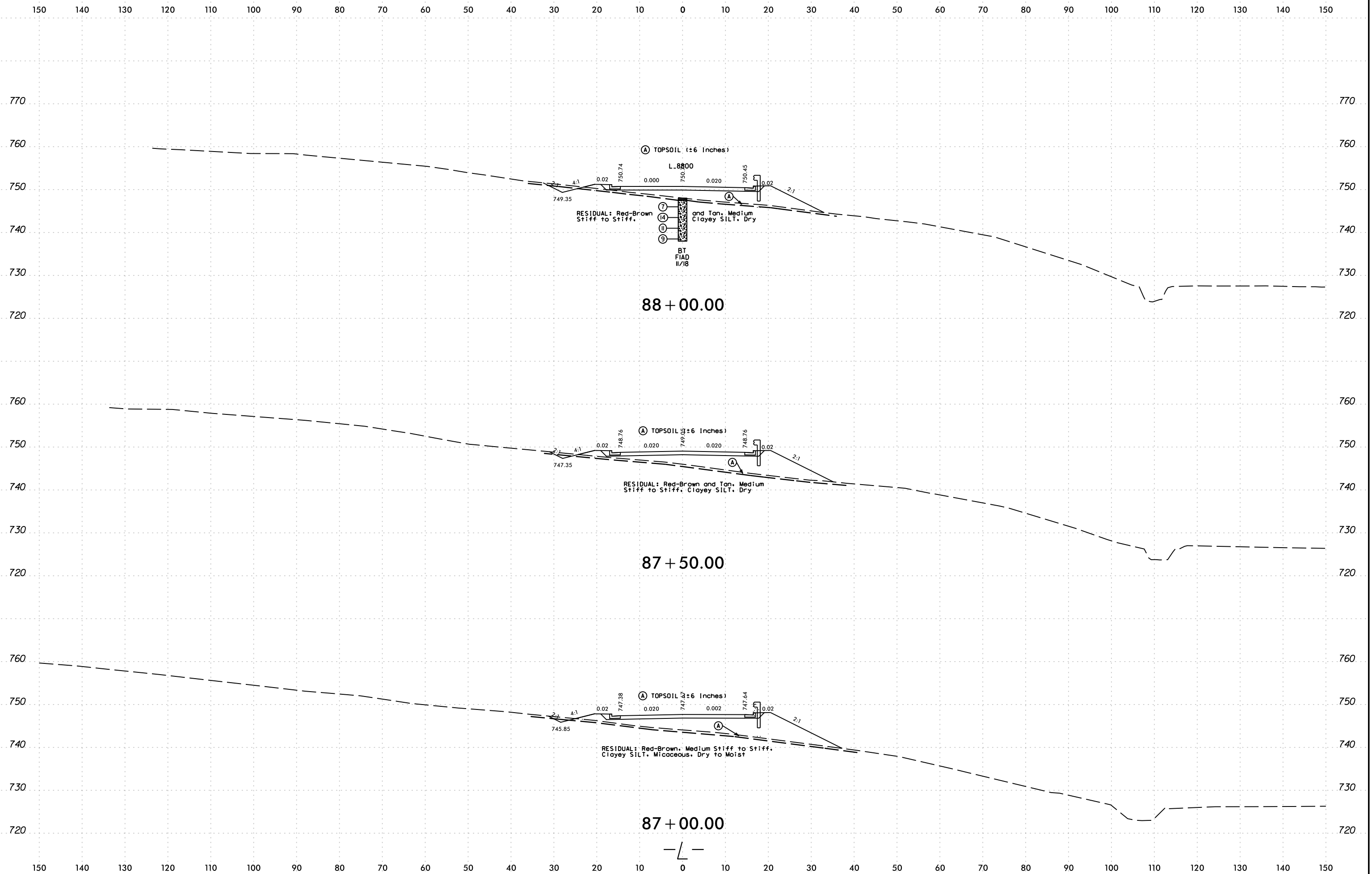
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r.pastorano



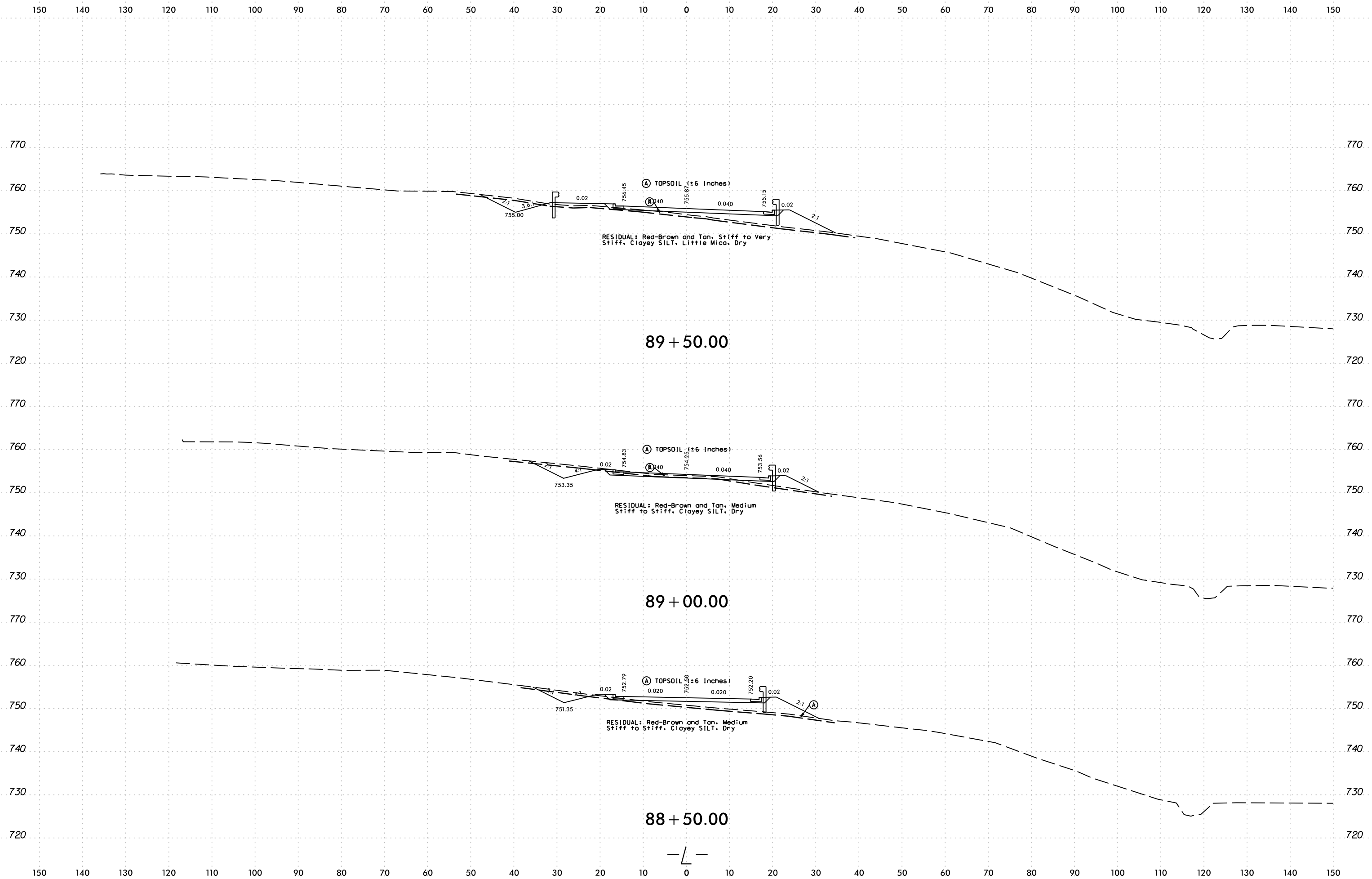


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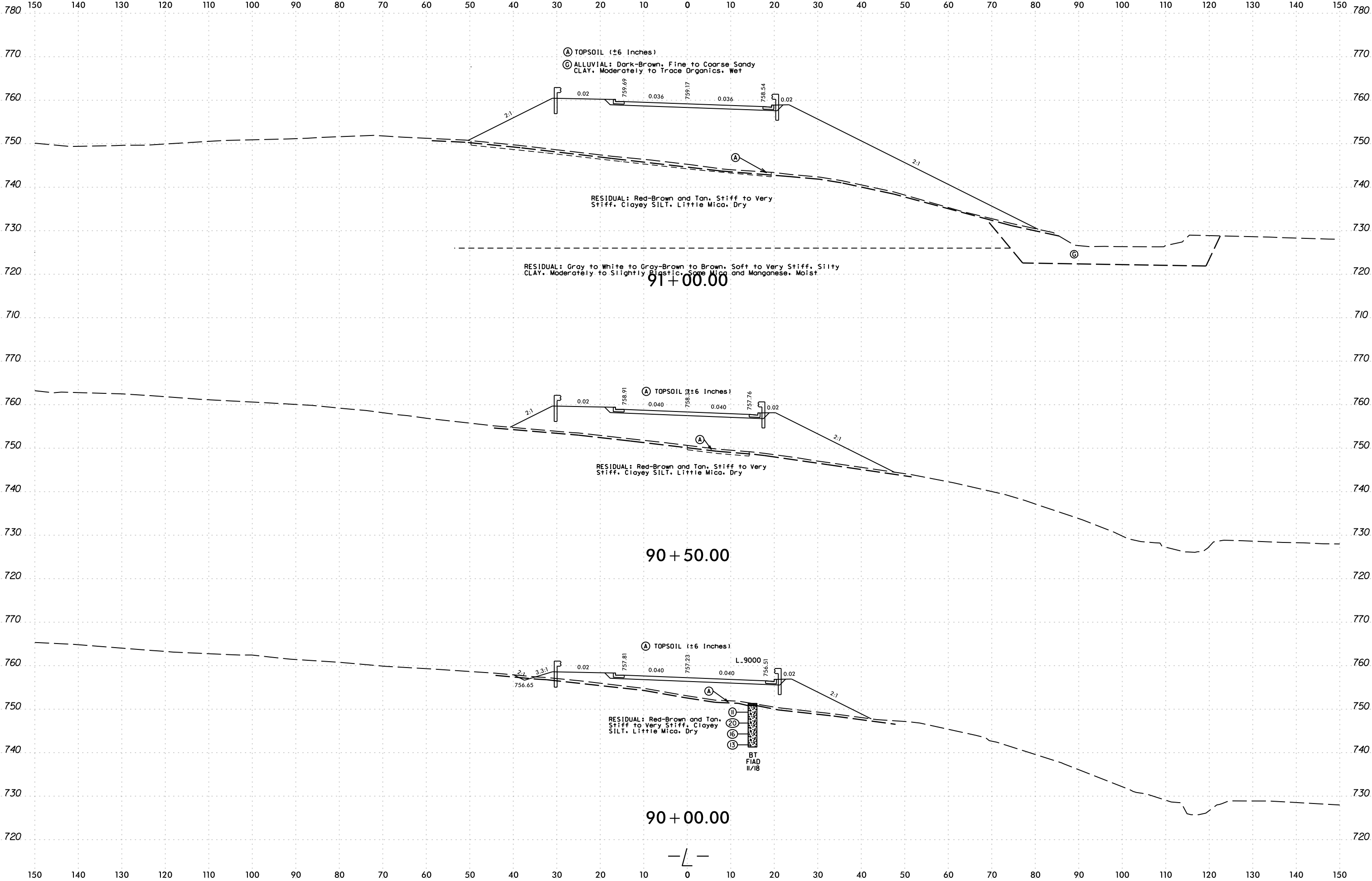




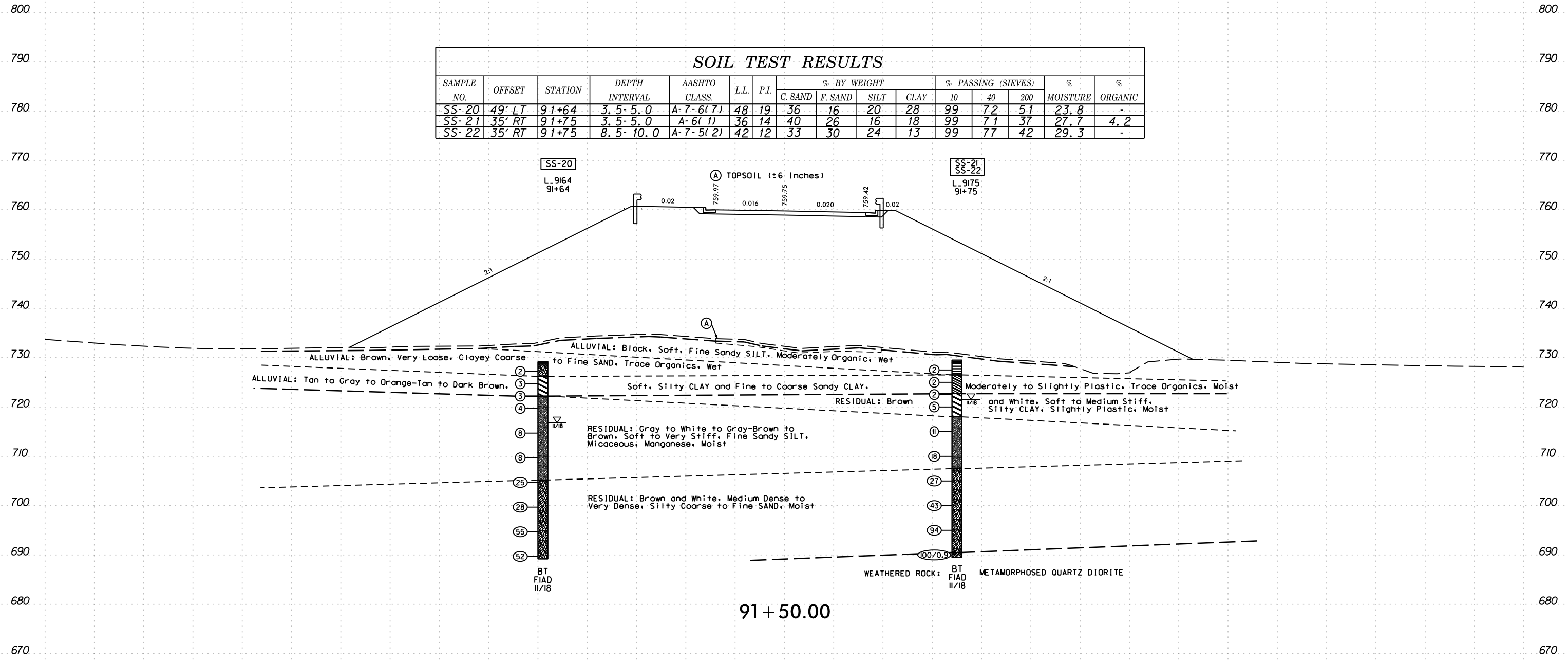
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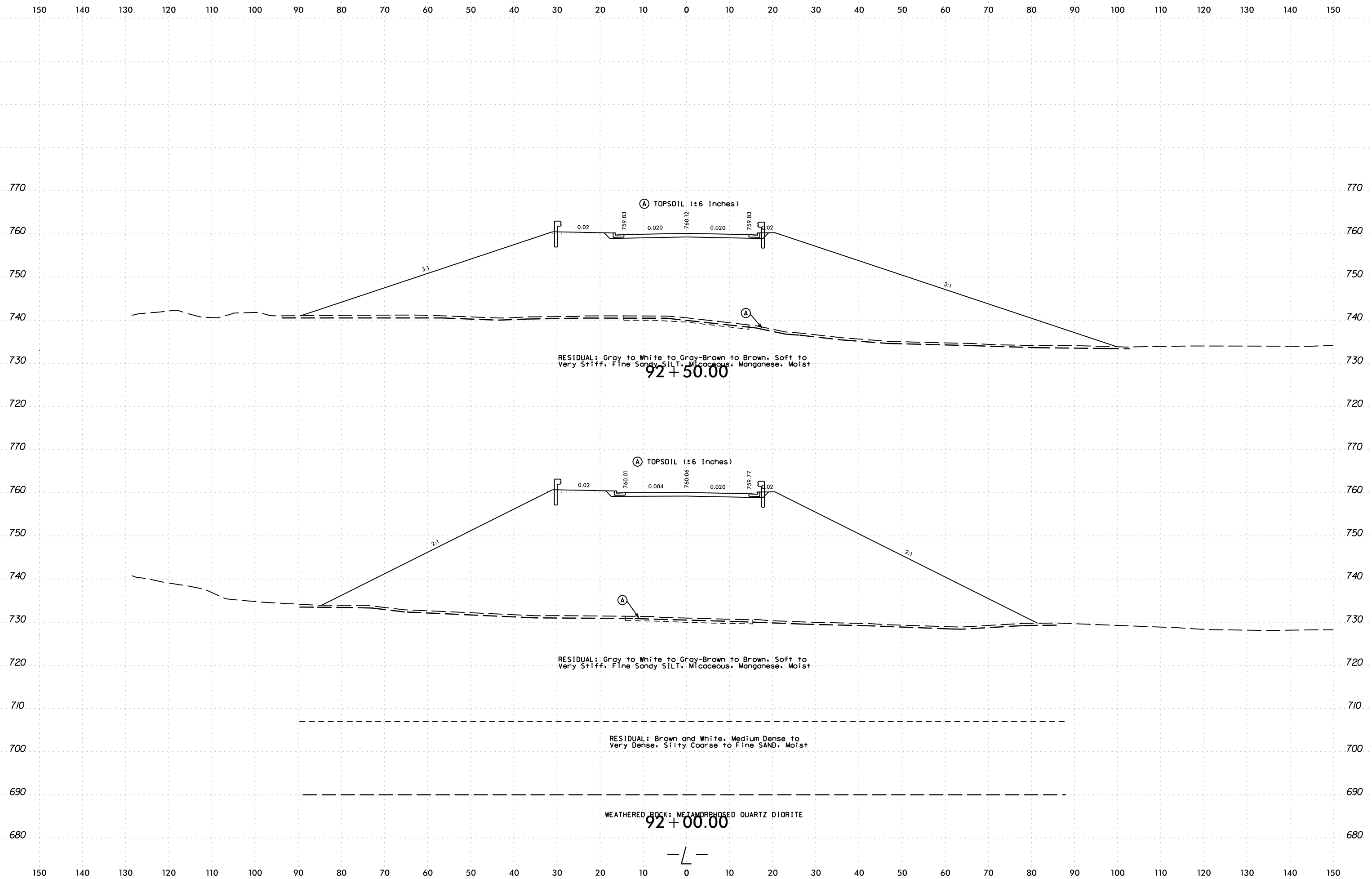


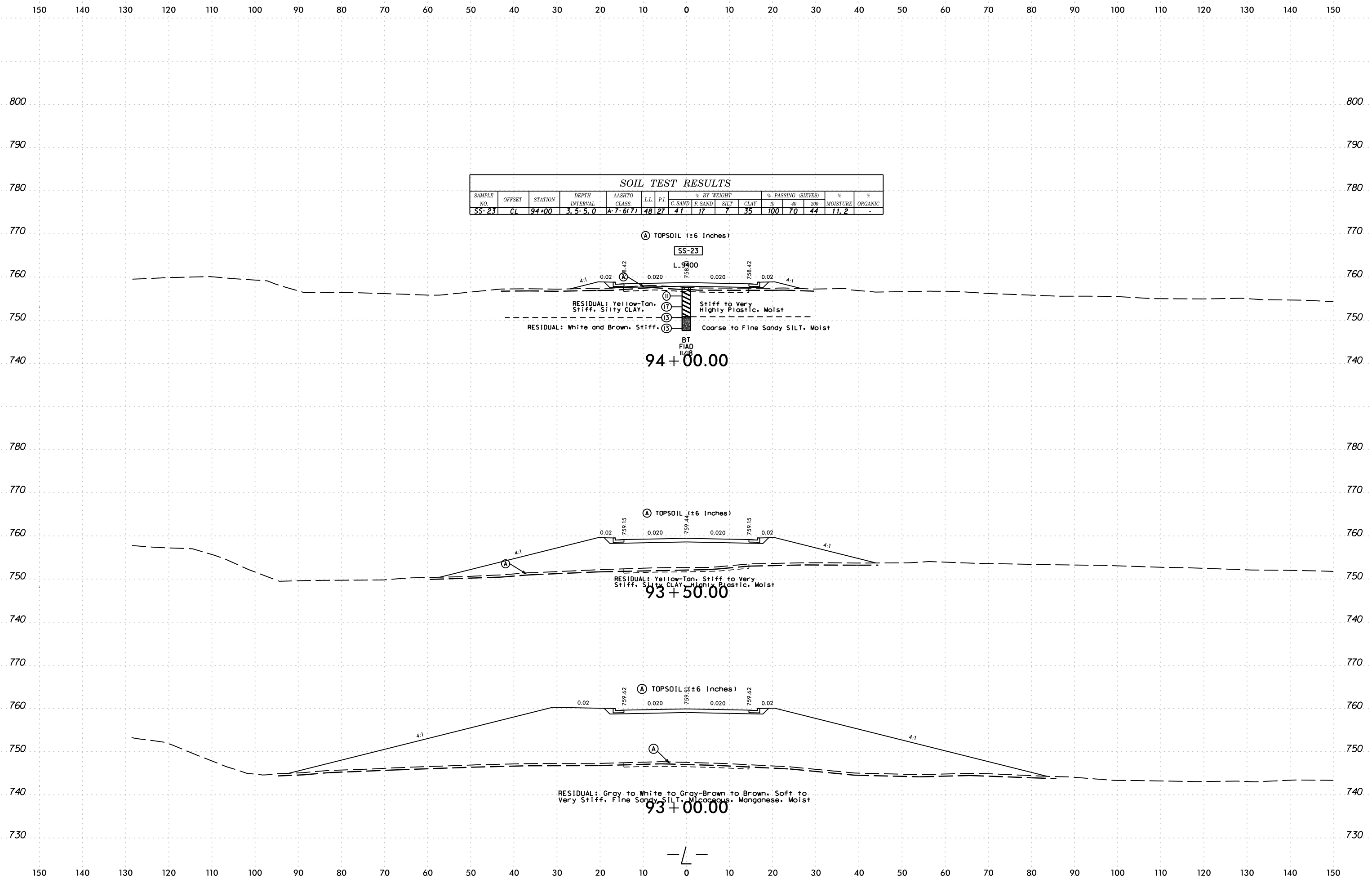
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SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
							SS-20	49' LT	91+64	3.5-5.0	A-7-6(7)	48	19		
SS-21	35' RT	91+75	3.5-5.0	A-6(1)	36	14	40	26	16	18	99	71	37	27.7	4.2
SS-22	35' RT	91+75	8.5-10.0	A-7-5(2)	42	12	33	30	24	13	99	77	42	29.3	-

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 r.pastorano





SOIL TEST RESULTS

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL	PI	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-23	CL	94+00	3.5-5.0	A-7-6(7)	48.27	41	17	7	35	100	70	44	11.2	-	

(A) TOPSOIL (±6 Inches)

SS-23

L. 94+00

RESIDUAL: Yellow-Tan, Stiff, Silty CLAY.

RESIDUAL: White and Brown, Stiff, Coarse to Fine Sandy SILT, Moist

BT FIAD 11/18

94 + 00.00

(A) TOPSOIL (±6 Inches)

RESIDUAL: Yellow-Tan, Stiff to Very Stiff, Silty CLAY, Highly Plastic, Moist

93 + 50.00

(A) TOPSOIL (±6 Inches)

RESIDUAL: Gray to White to Gray-Brown to Brown, Soft to Very Stiff, Fine Sandy SILT, Micaceous, Manganese, Moist

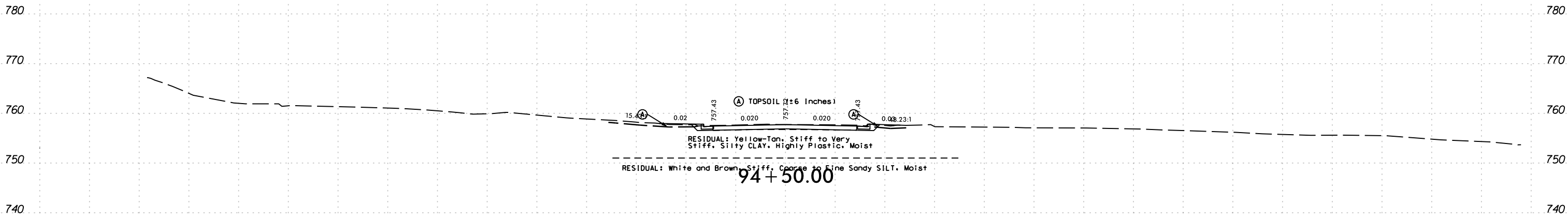
93 + 00.00

6/23/16

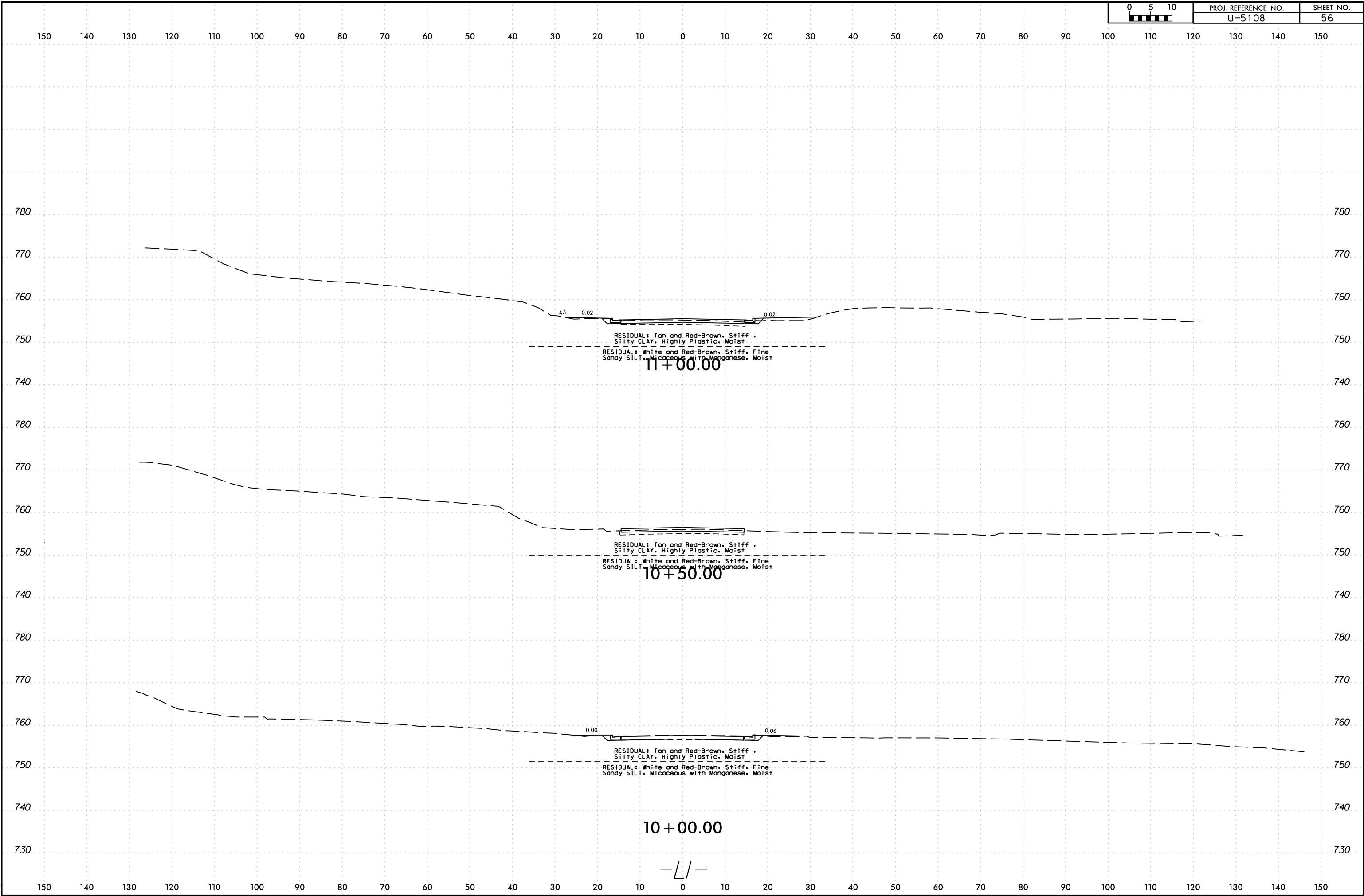


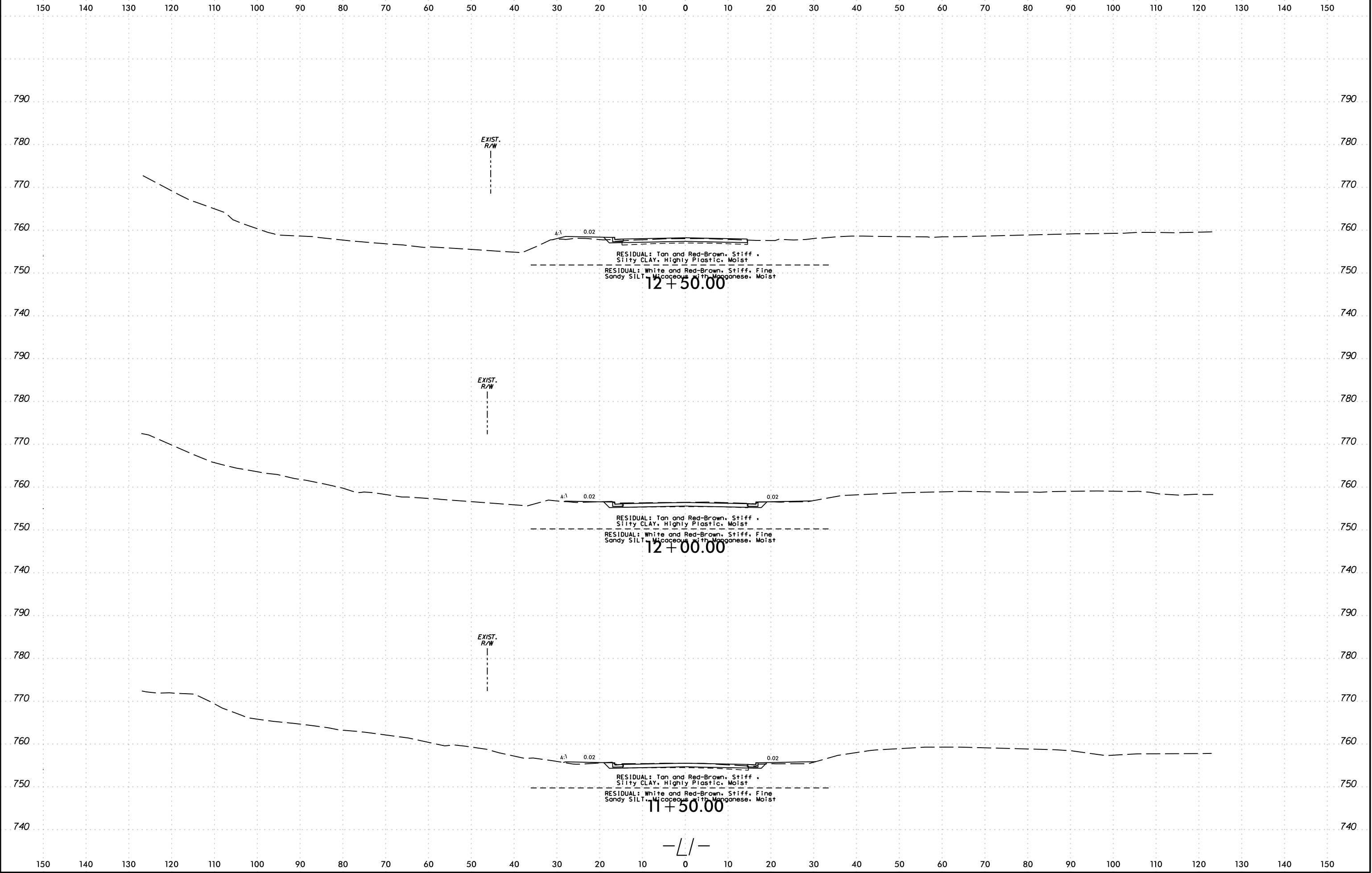
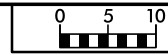
PROJ. REFERENCE NO.	SHEET NO.
U-5108	55

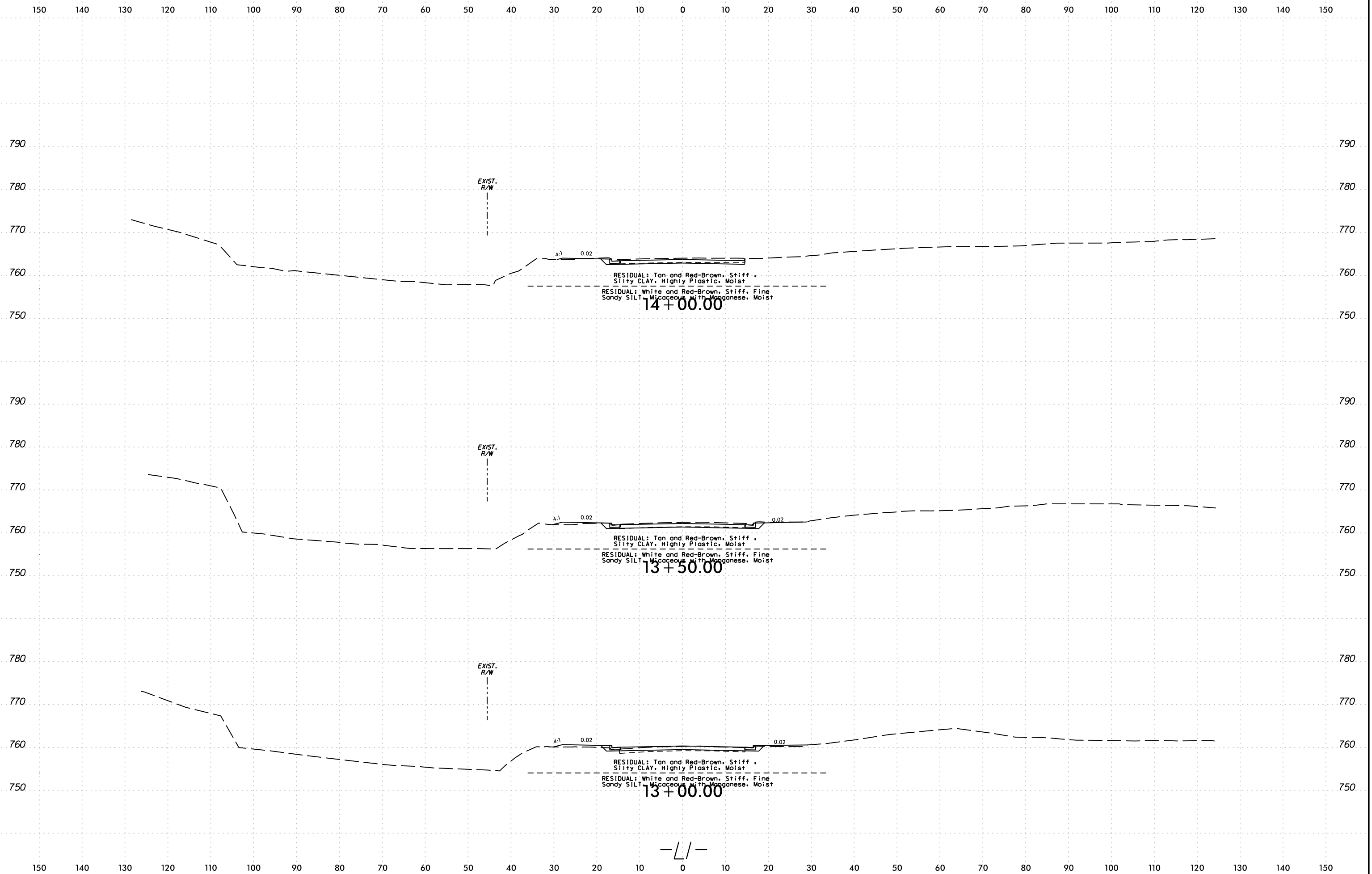
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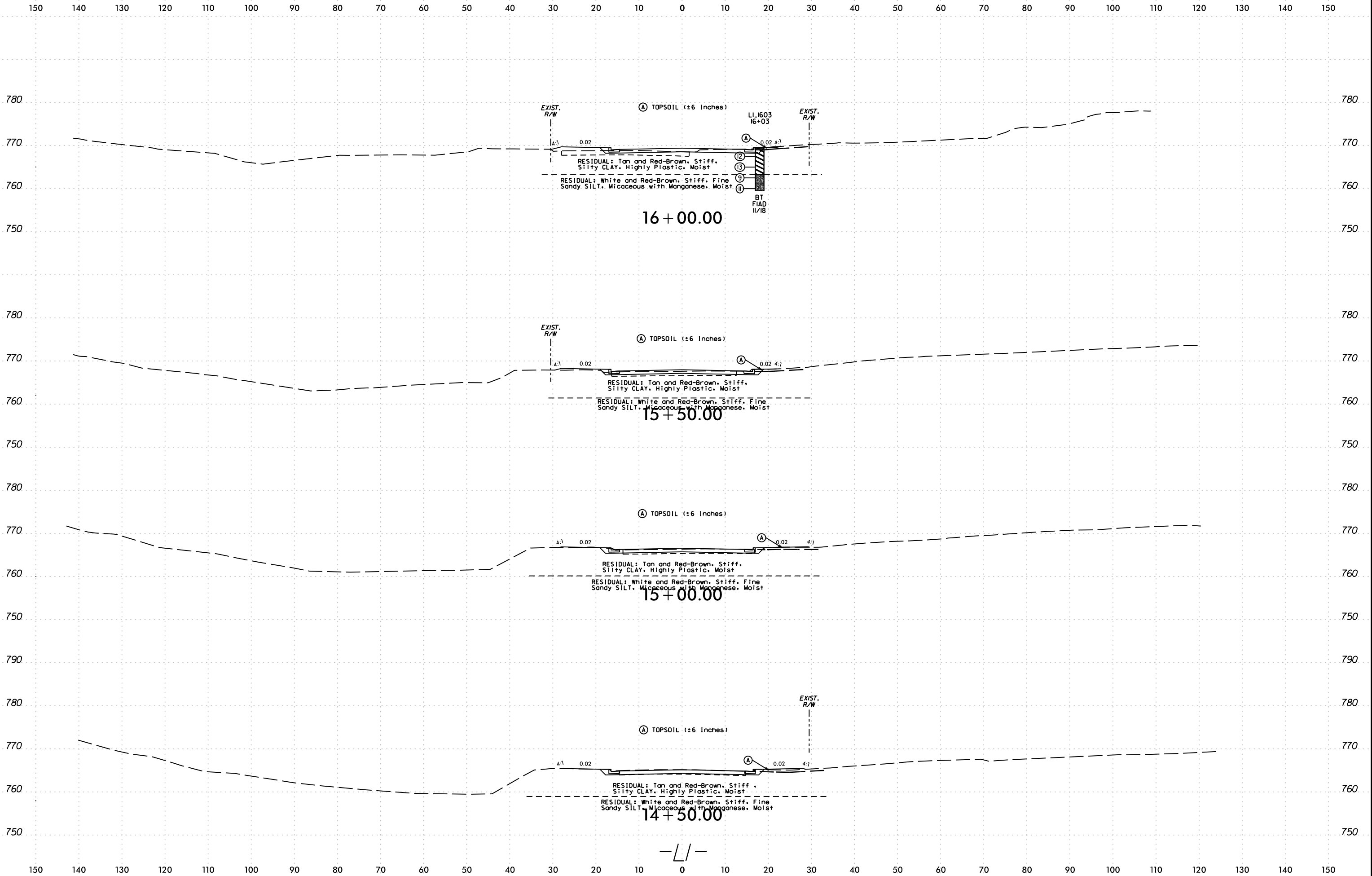
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 rps@u-5108





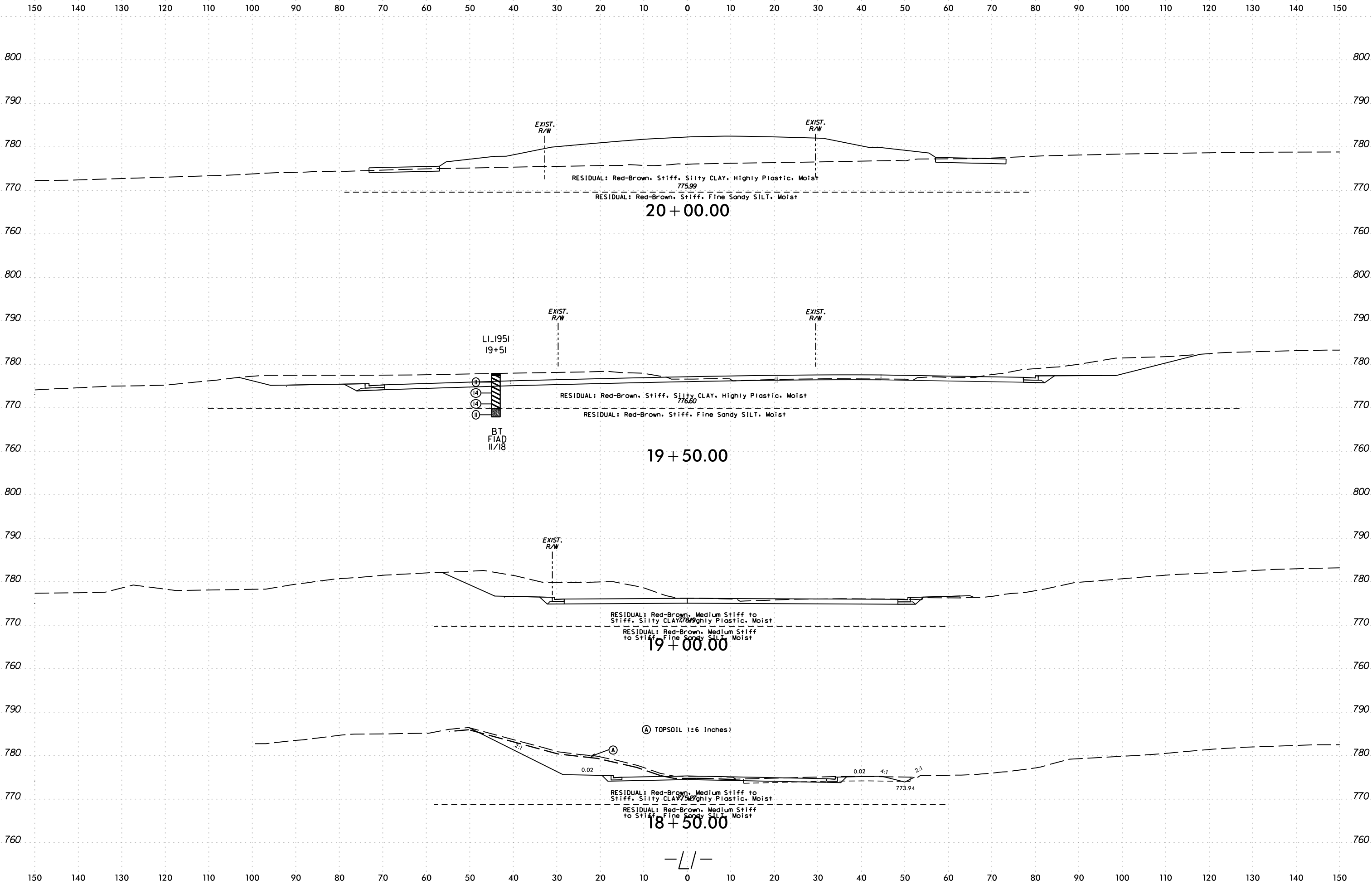


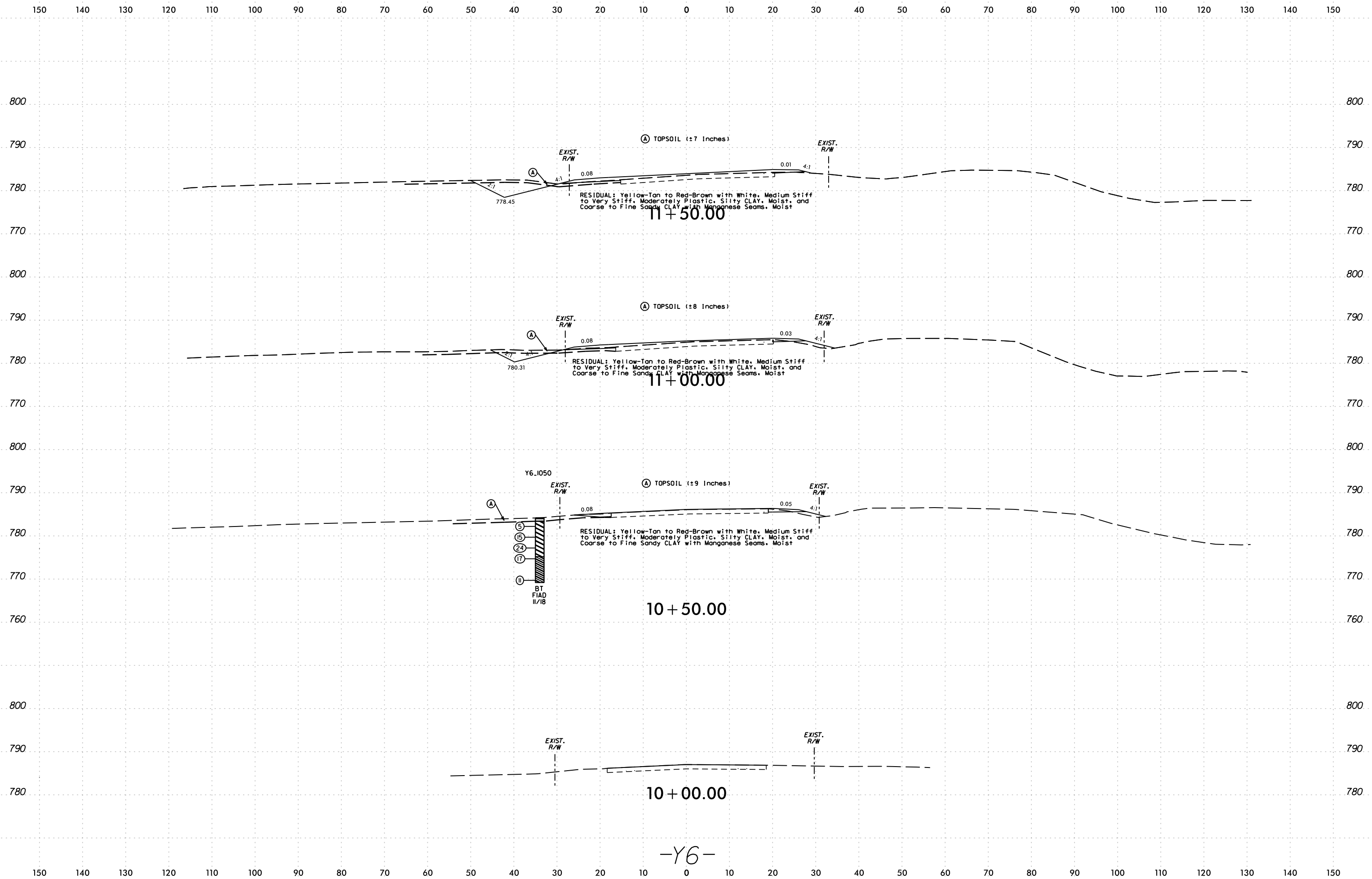
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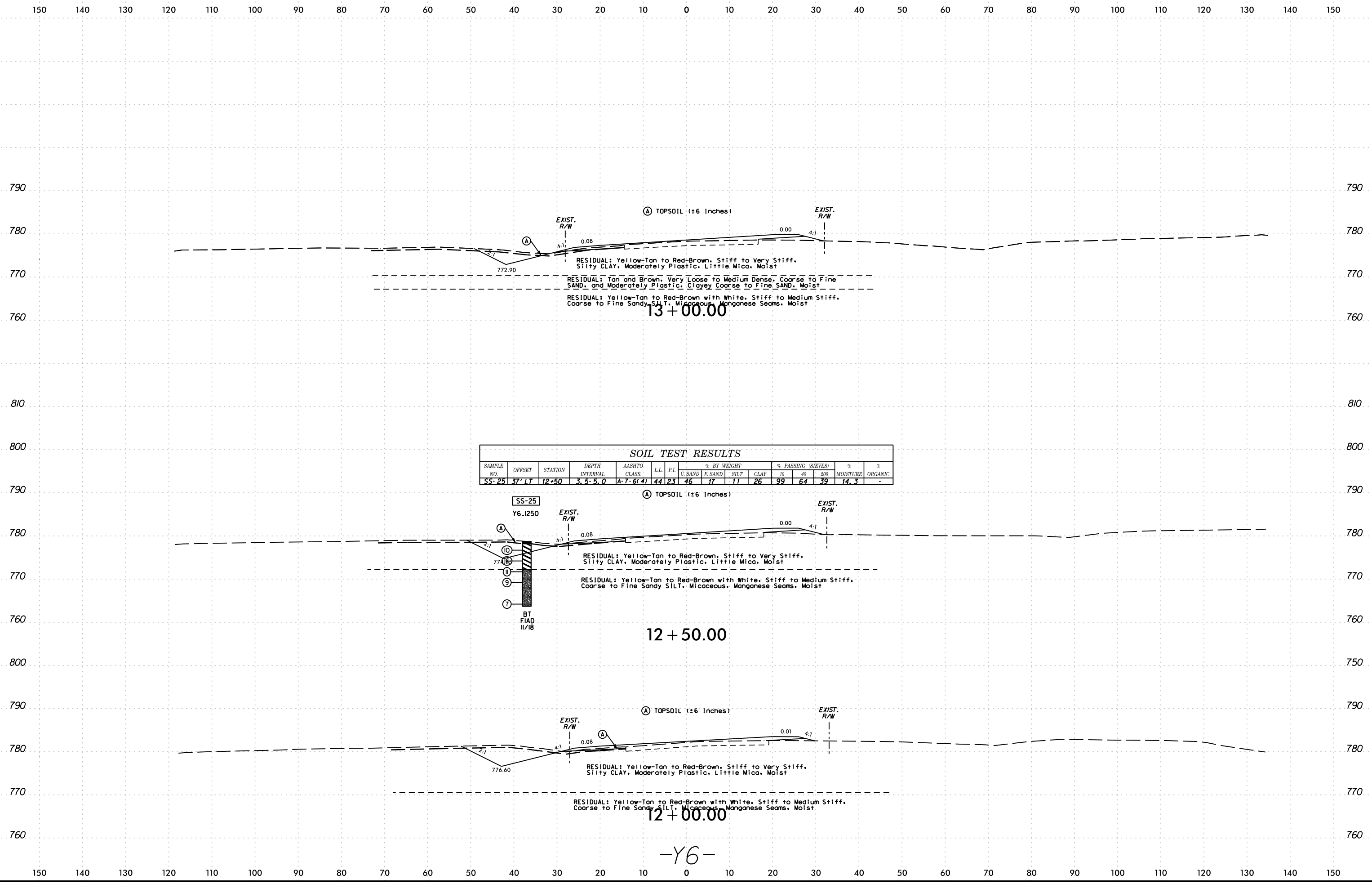
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-Y6-



SOIL TEST RESULTS														
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)		% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	#10	#200		
SS-25	37' LT	12+50	3.5-5.0	A-7-6(4)	44	23	46	17	11	26	99	64	39	14.3

12/6/2019 10:47:01 AM
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 r.pastorano

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

800 800

790 790

780 780

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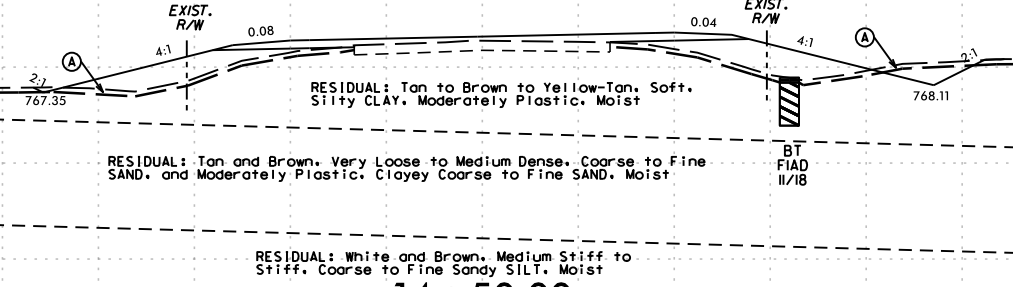
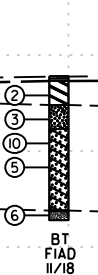
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SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-26	6' LT	14+50	8.5-10.0	A-2-7(2)	41	24	50	20	10	20	99	63	32	15.0	-

SS-26
Y6.I450LT

(A) TOPSOIL (±6 Inches)

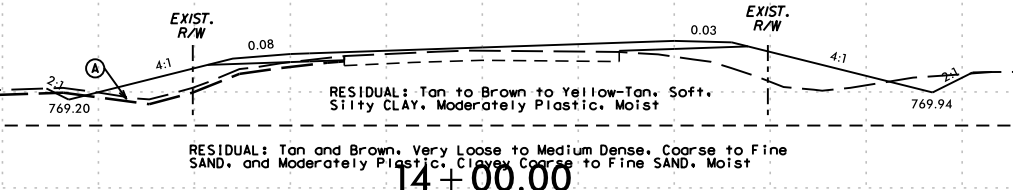
Y6.I450RT



14 + 50.00

(A) TOPSOIL (±6 Inches)

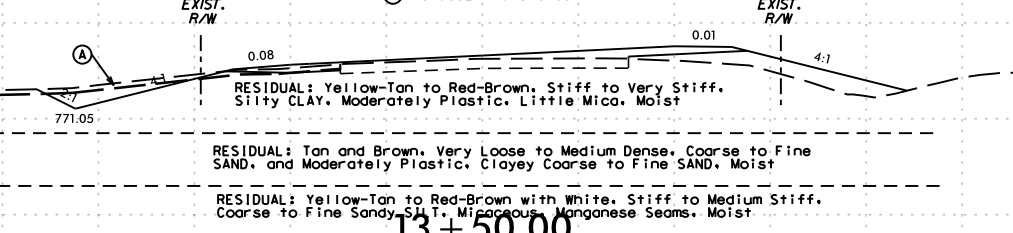
EXIST. R/W



14 + 00.00

(A) TOPSOIL (±6 Inches)

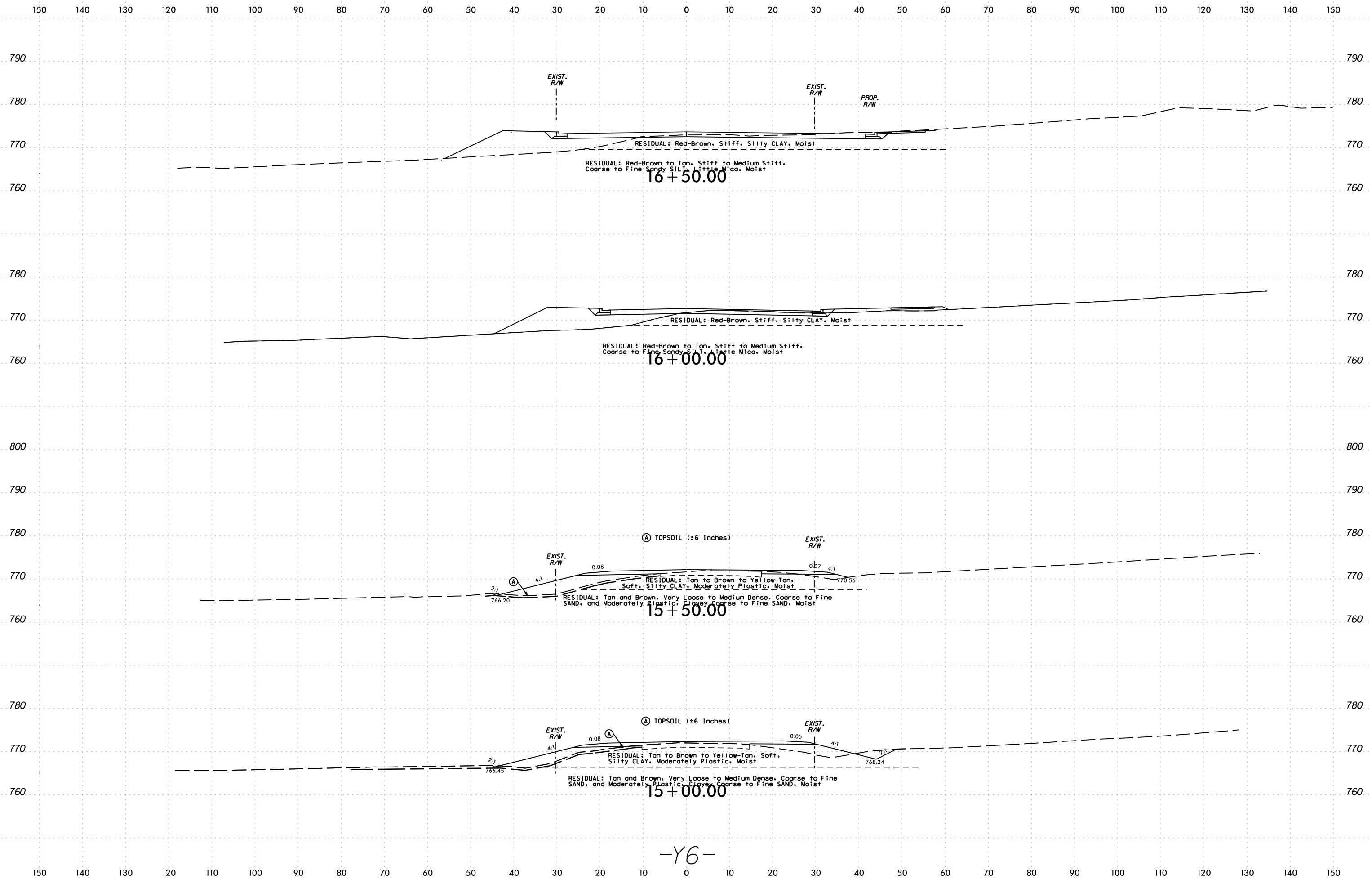
EXIST. R/W



13 + 50.00

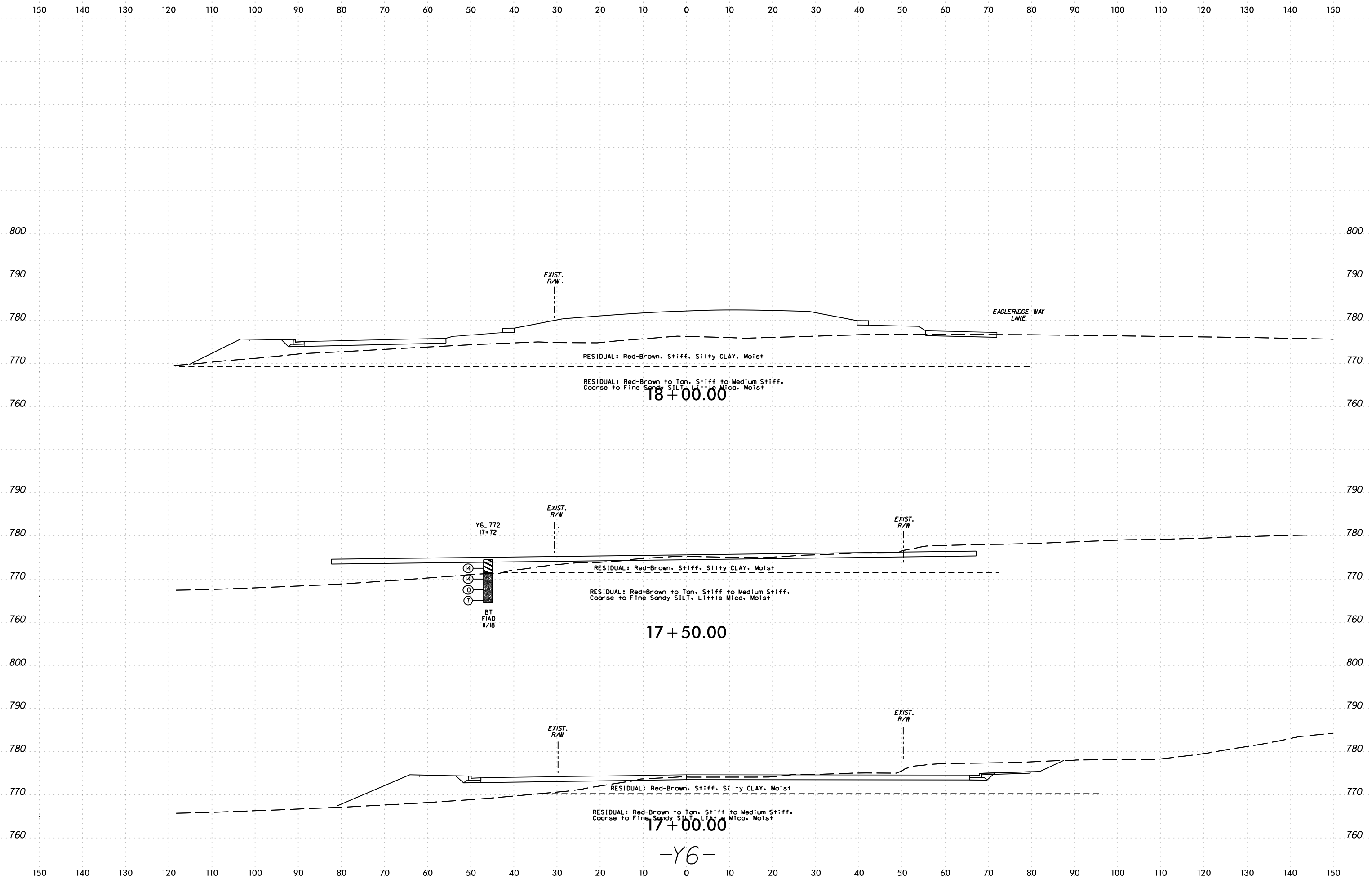
-Y6-

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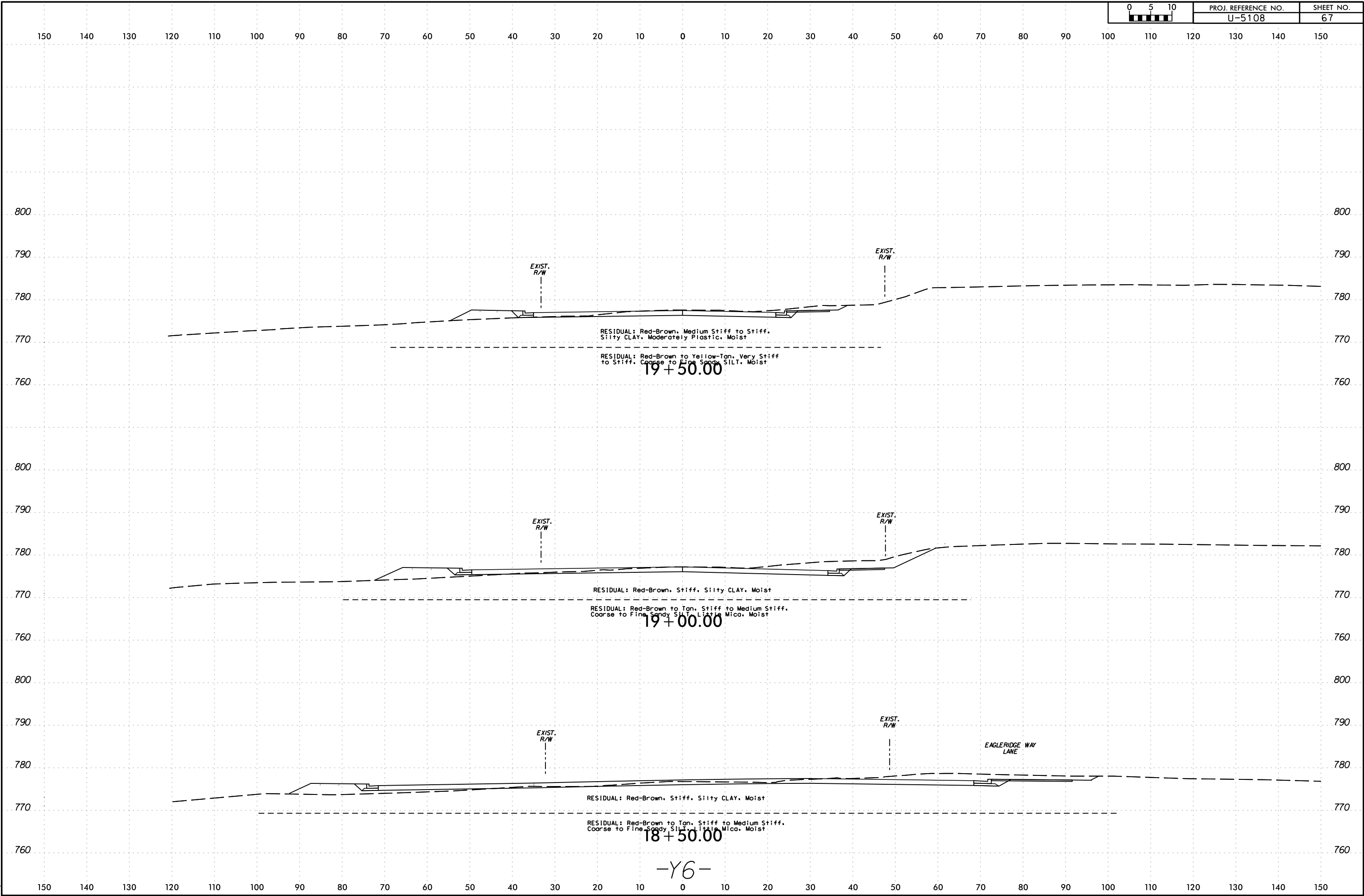
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rps:ana

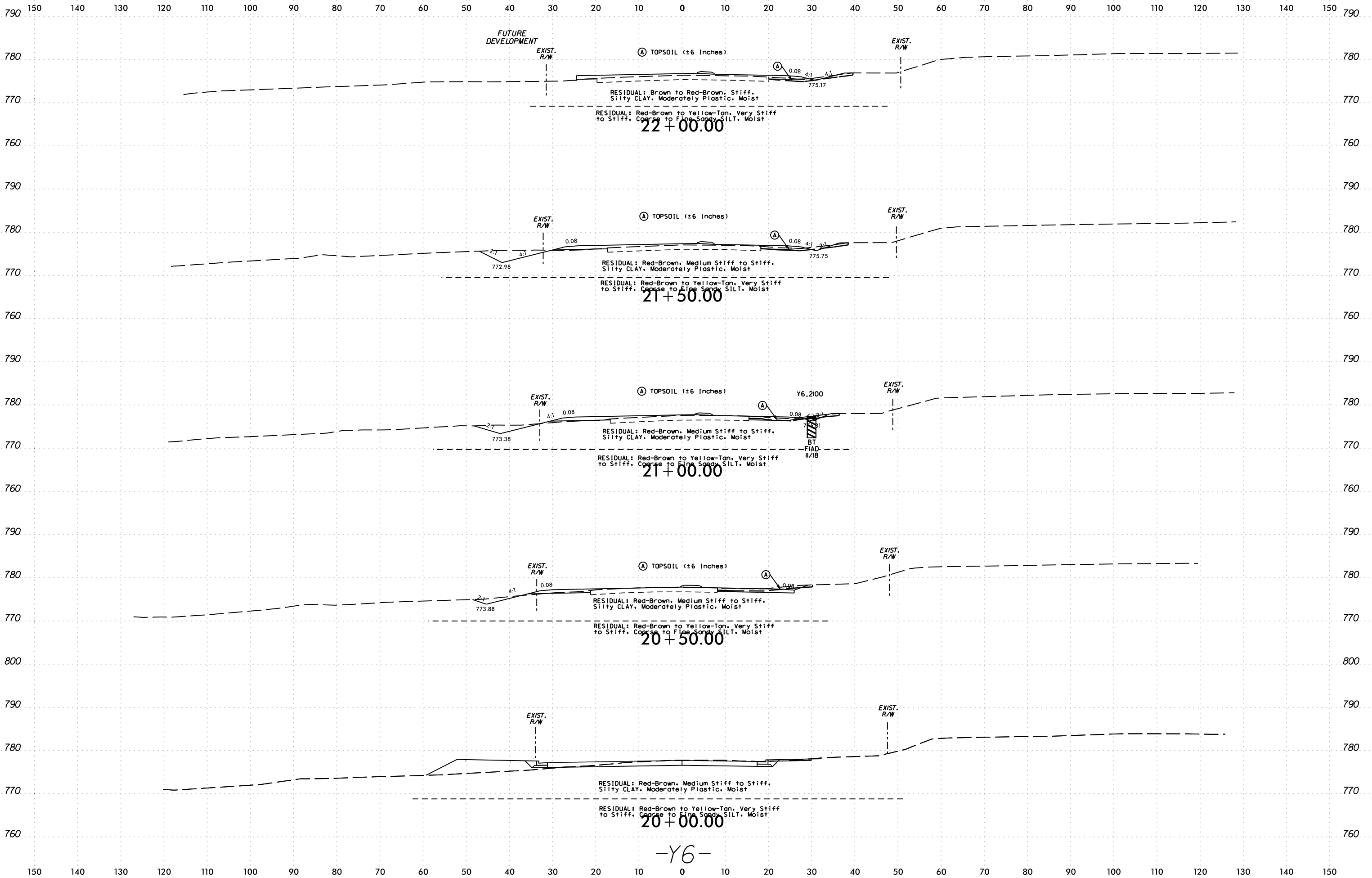
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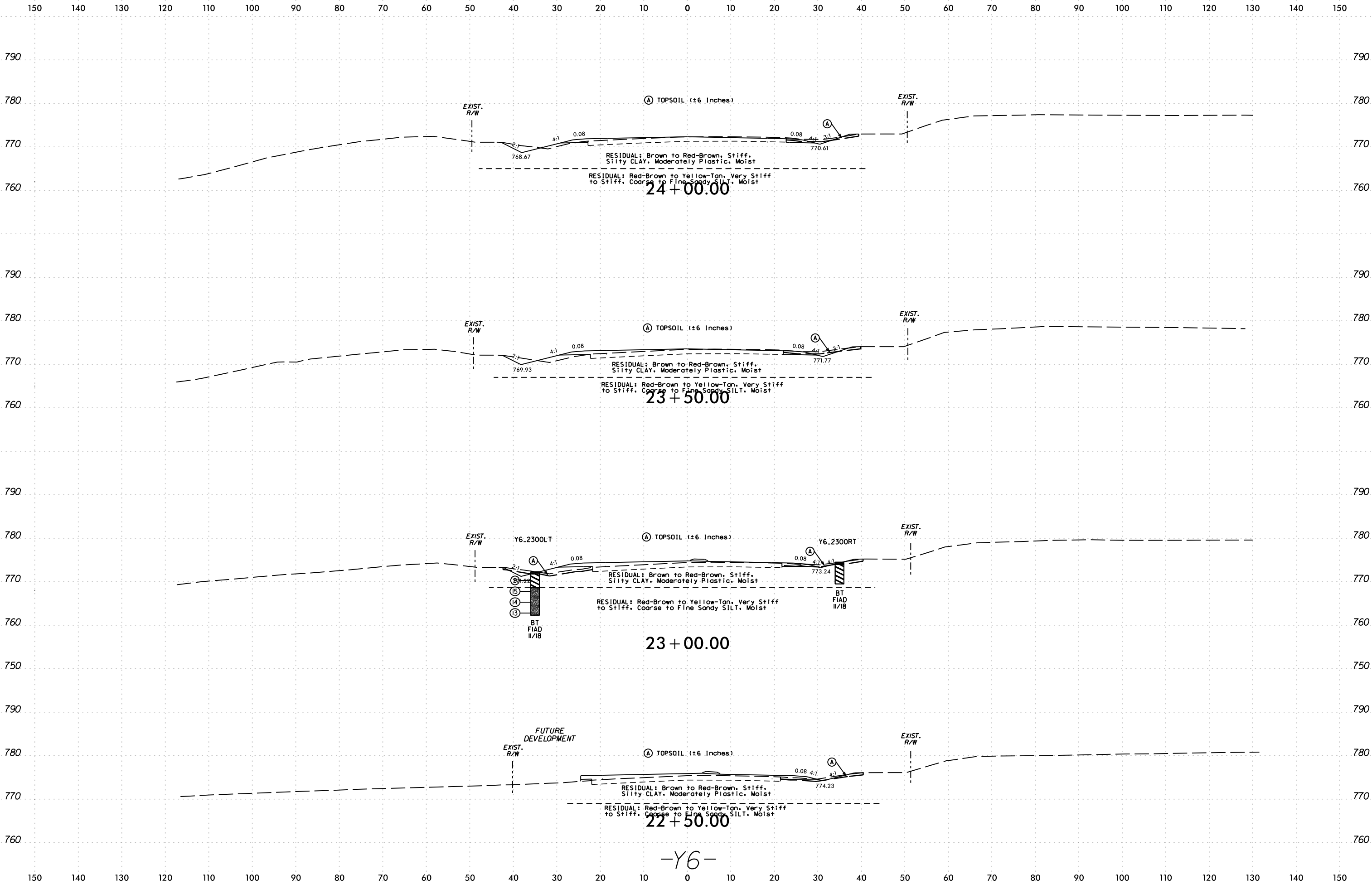
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 rps@unb.ca

-Y6-





-Y6-



I:\E\2019\04\17\04 AM 2\Projects\2018\01\GV05.300.U-5108 (Northcross)\US108_GEO_RDWY\CADD_GEO\RDWY\CADD_GEO\U-5108_Geo_xsi_Y6.dgn rps:one

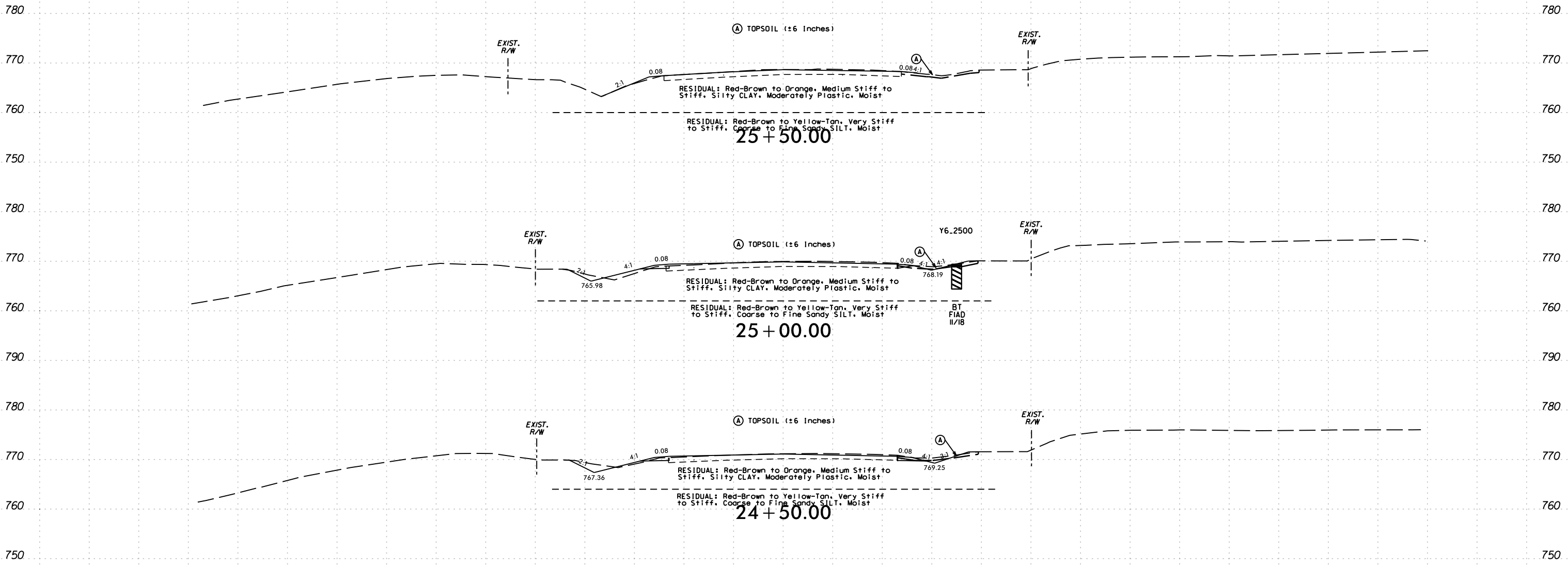
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PROJ. REFERENCE NO.
U-5108

SHEET NO.
70

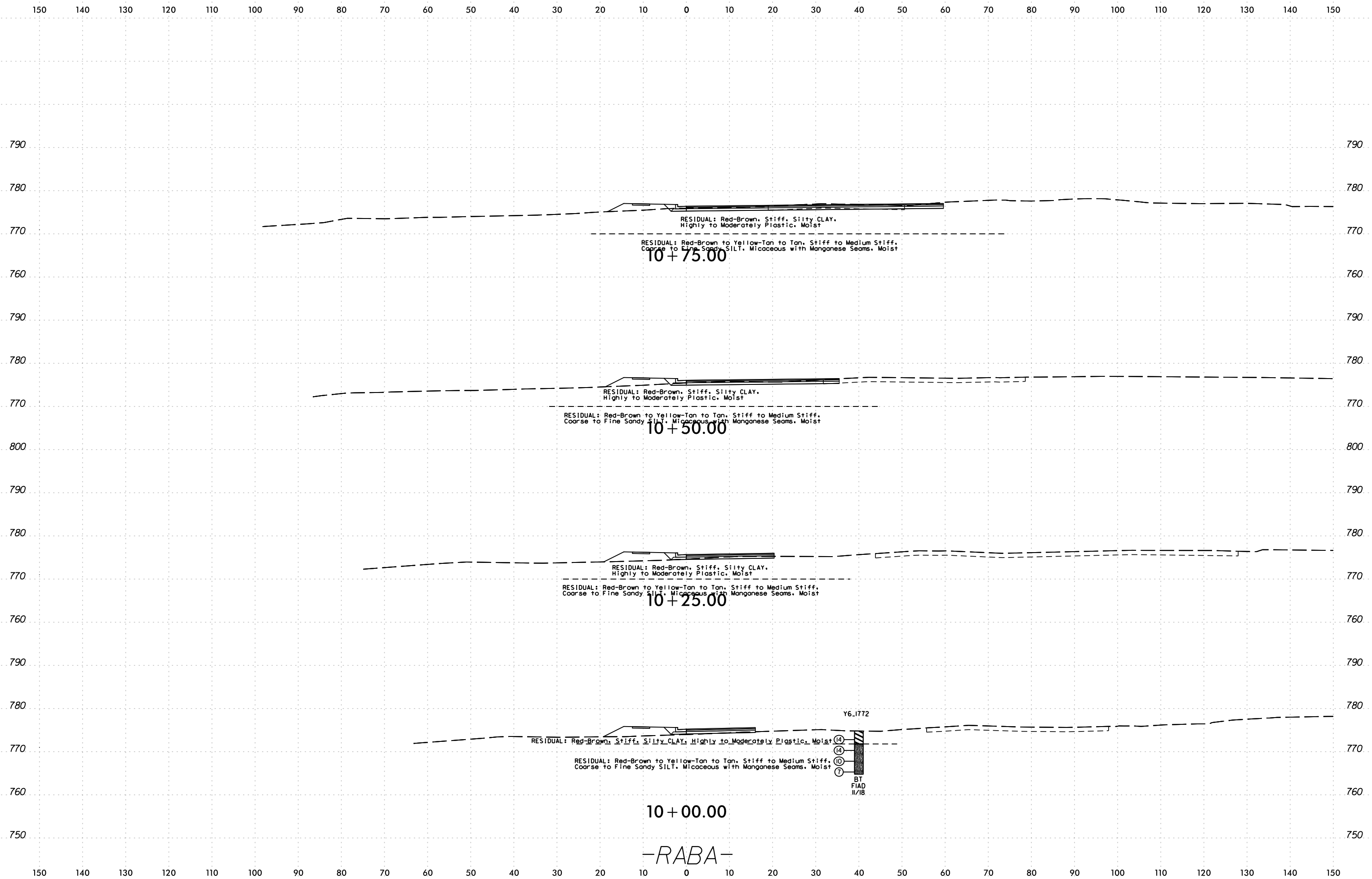
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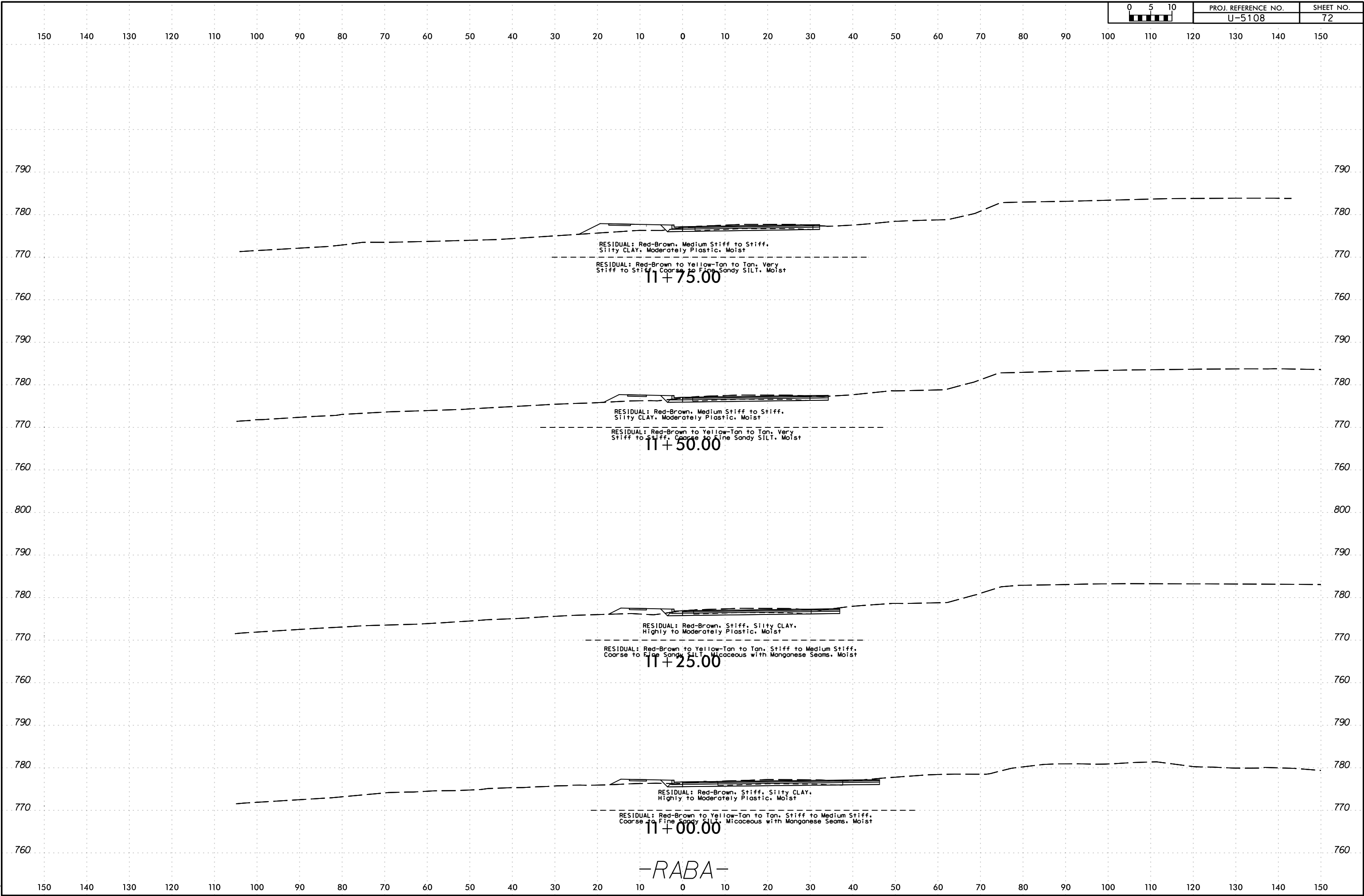


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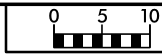
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rps@un





-RABA-



150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

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RESIDUAL: Red-Brown, Medium Stiff to Stiff,
Silty CLAY, Moderately Plastic, Moist

RESIDUAL: Red-Brown to Yellow-Tan to Tan, Very
Stiff to Stiff, Coarse to Fine Sandy SILT, Moist

12+25.00

RESIDUAL: Red-Brown, Medium Stiff to Stiff,
Silty CLAY, Moderately Plastic, Moist

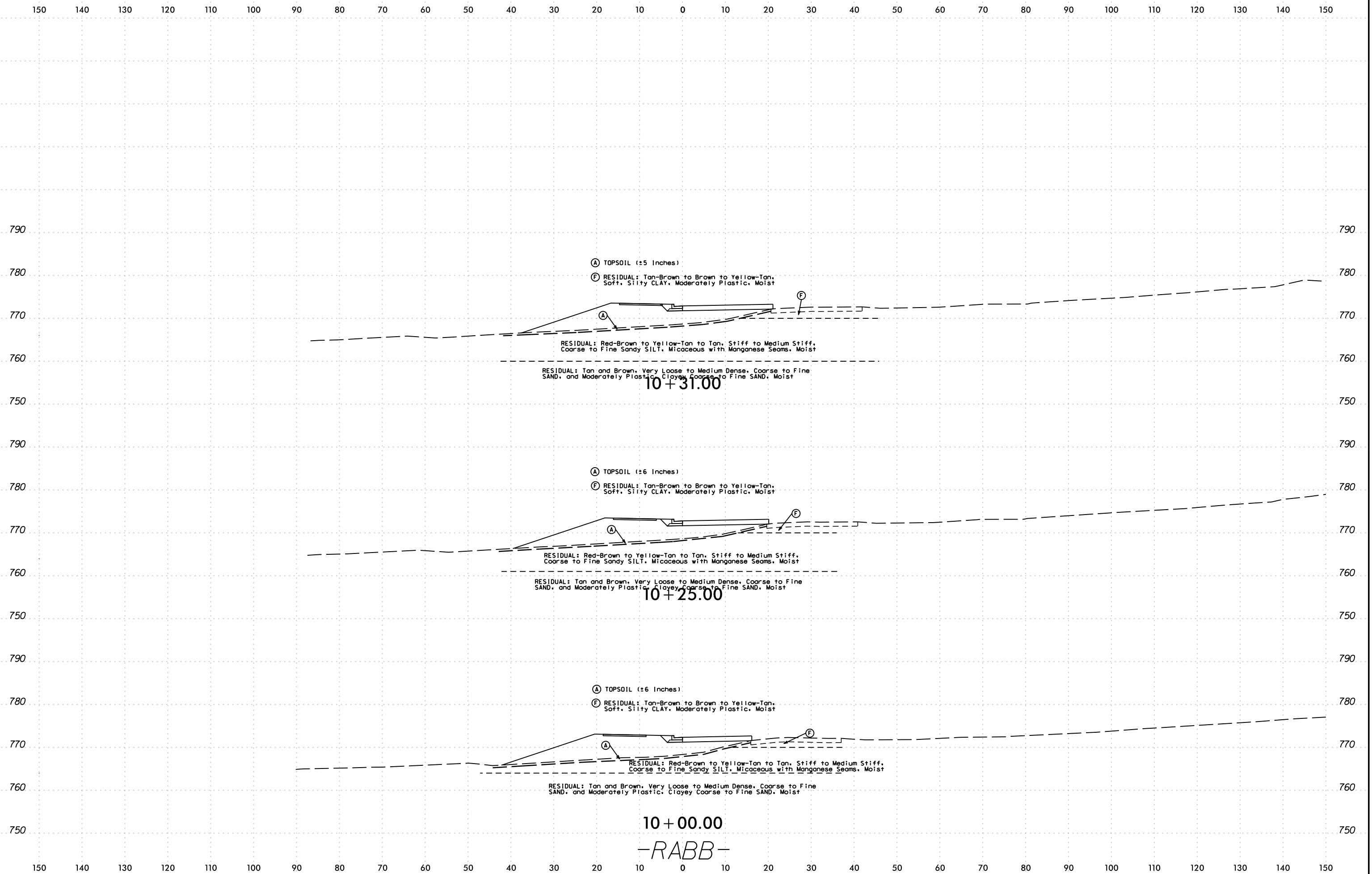
RESIDUAL: Red-Brown to Yellow-Tan to Tan, Very
Stiff to Stiff, Coarse to Fine Sandy SILT, Moist

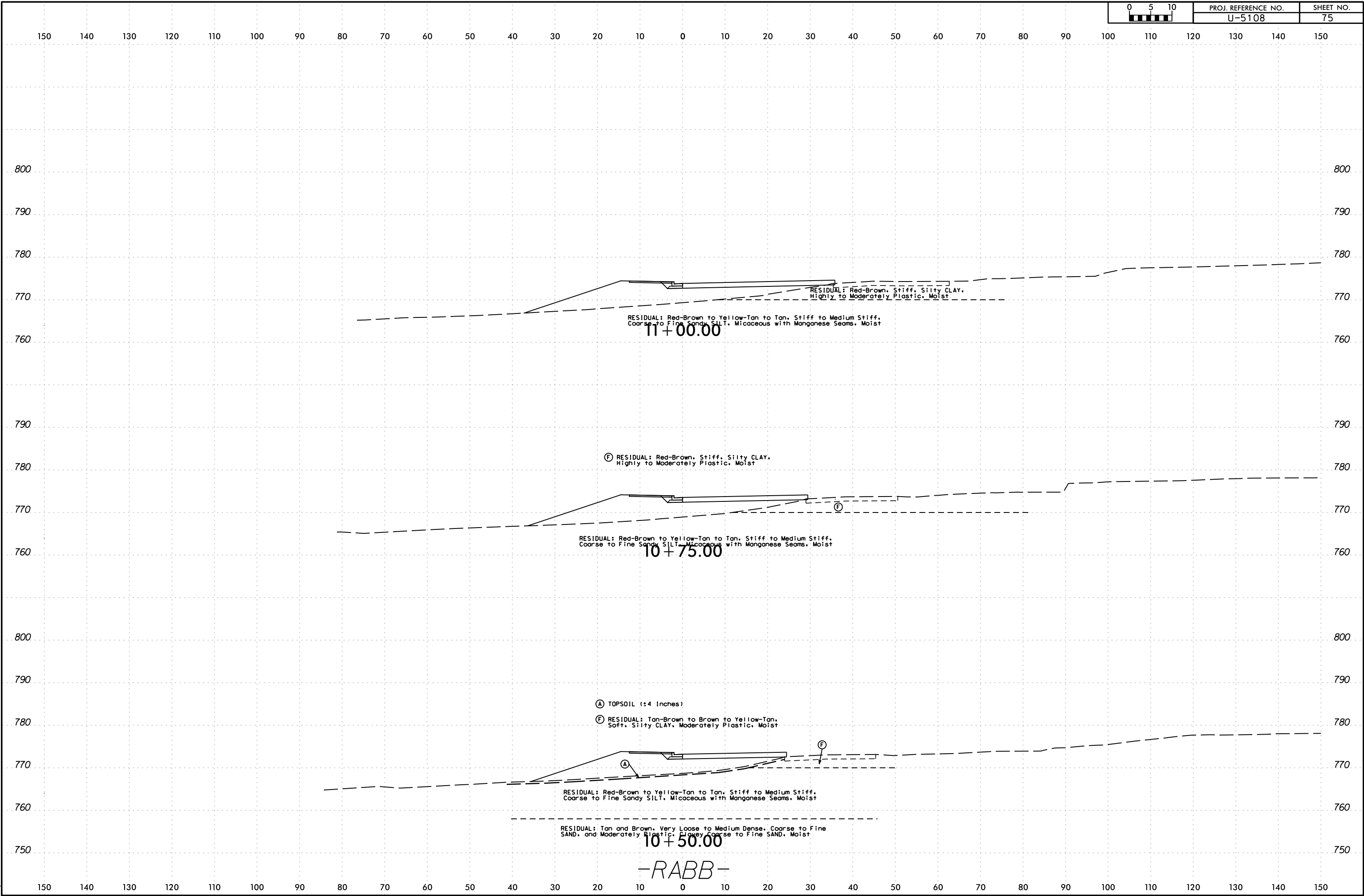
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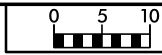
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r.pastorano



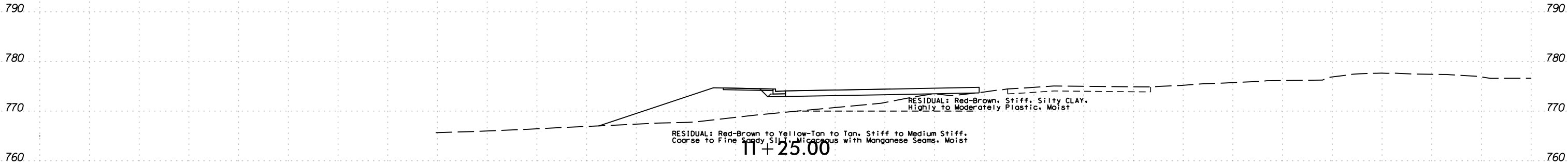


6/23/16



PROJ. REFERENCE NO.	SHEET NO.
U-5108	76

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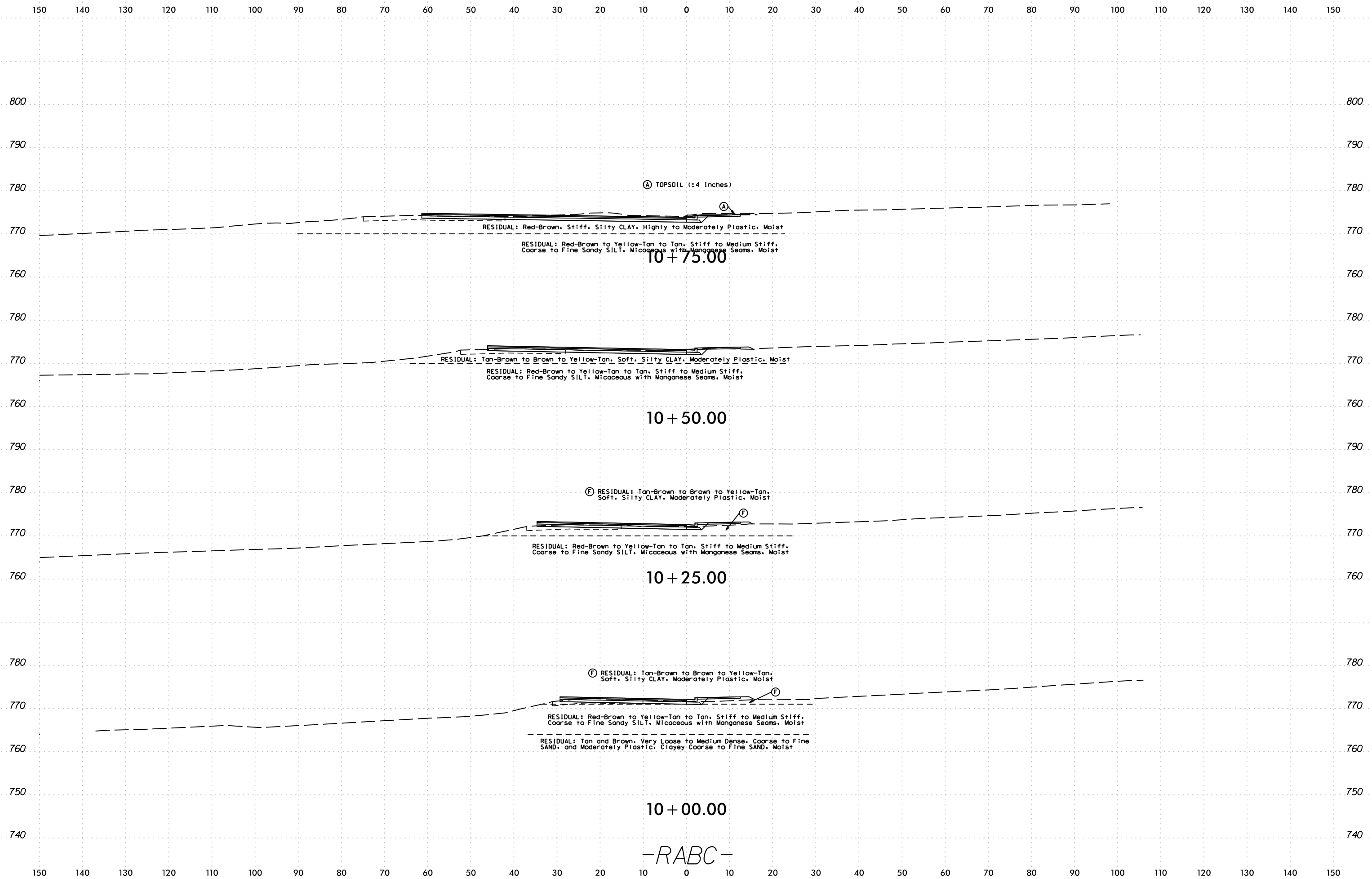
RESIDUAL: Red-Brown, Stiff, Silty CLAY, Highly to Moderately Plastic, Moist

RESIDUAL: Red-Brown to Yellow-Tan to Tan, Stiff to Medium Stiff, Coarse to Fine Sandy Silty Micaeous with Manganese Seams, Moist

11+25.00
-RABB-

I:\Projects\2018\GIS\G005\300_U-5108 (Northcross)\US108_GEO_RDWY\CADD_GEO\GEO\GEO\U-5108_Geo.xst_RABB.dgn

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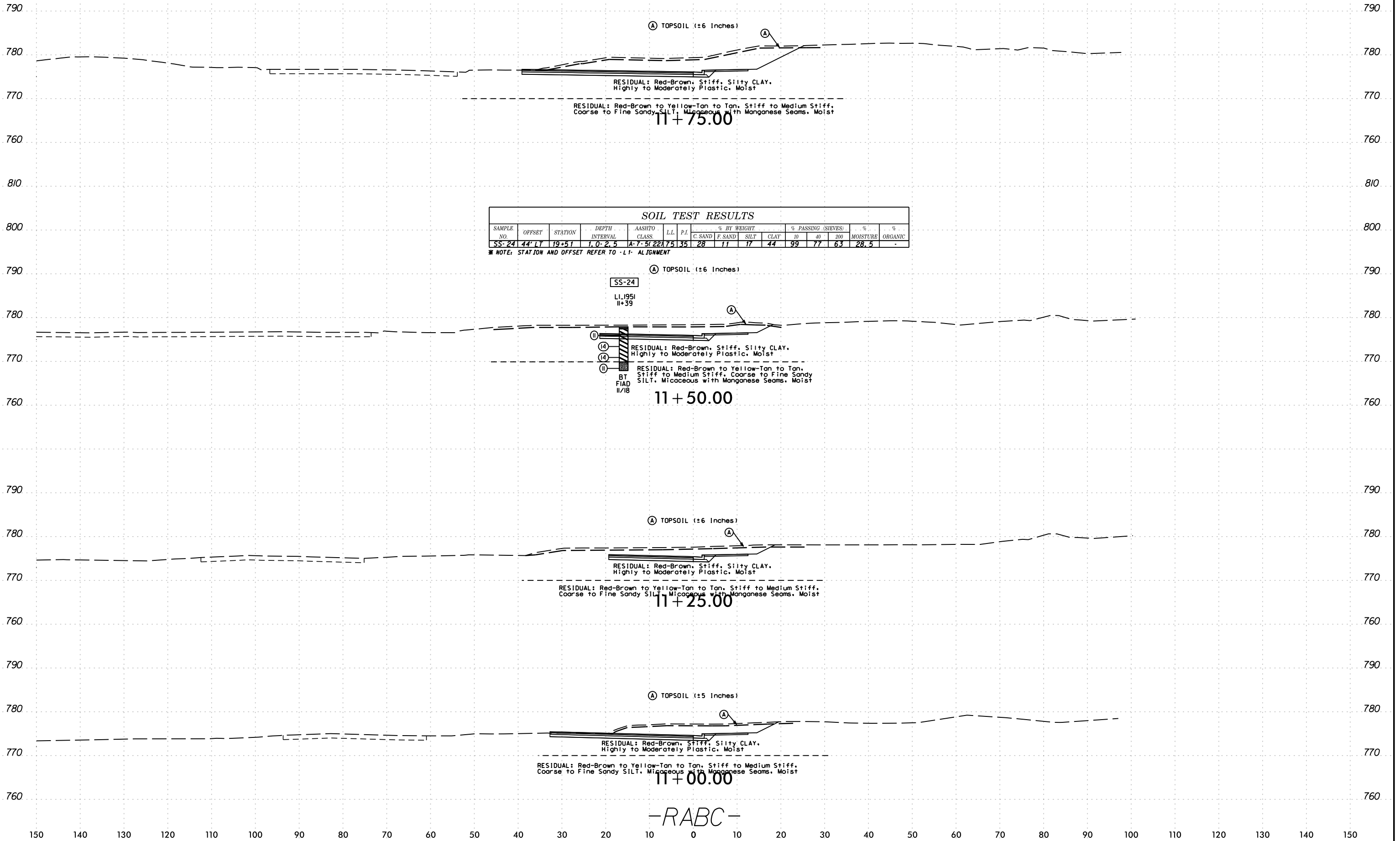


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rpastrona

-RABC-

NOTE: END -RABC- AT STA. 12+41.61
-RABC- STA. 12+41.61 = -LI- STA. 18+50/-RABD- STA. 10+00

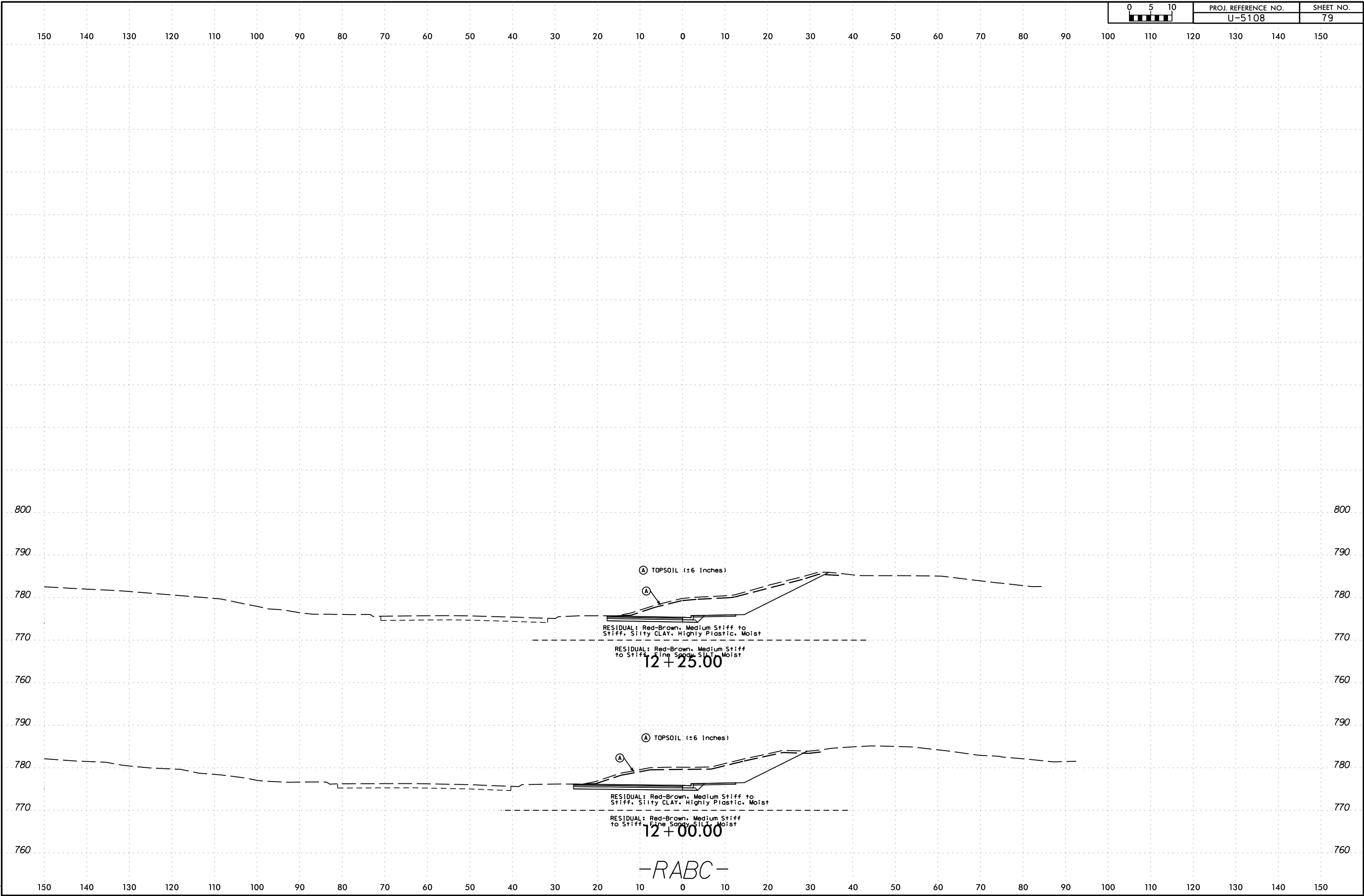
NOTE: END -RABC- AT STA. 12+41.61
-RABC- STA. 12+41.61 = -LI- STA. 18+50/-RABD- STA. 10+00

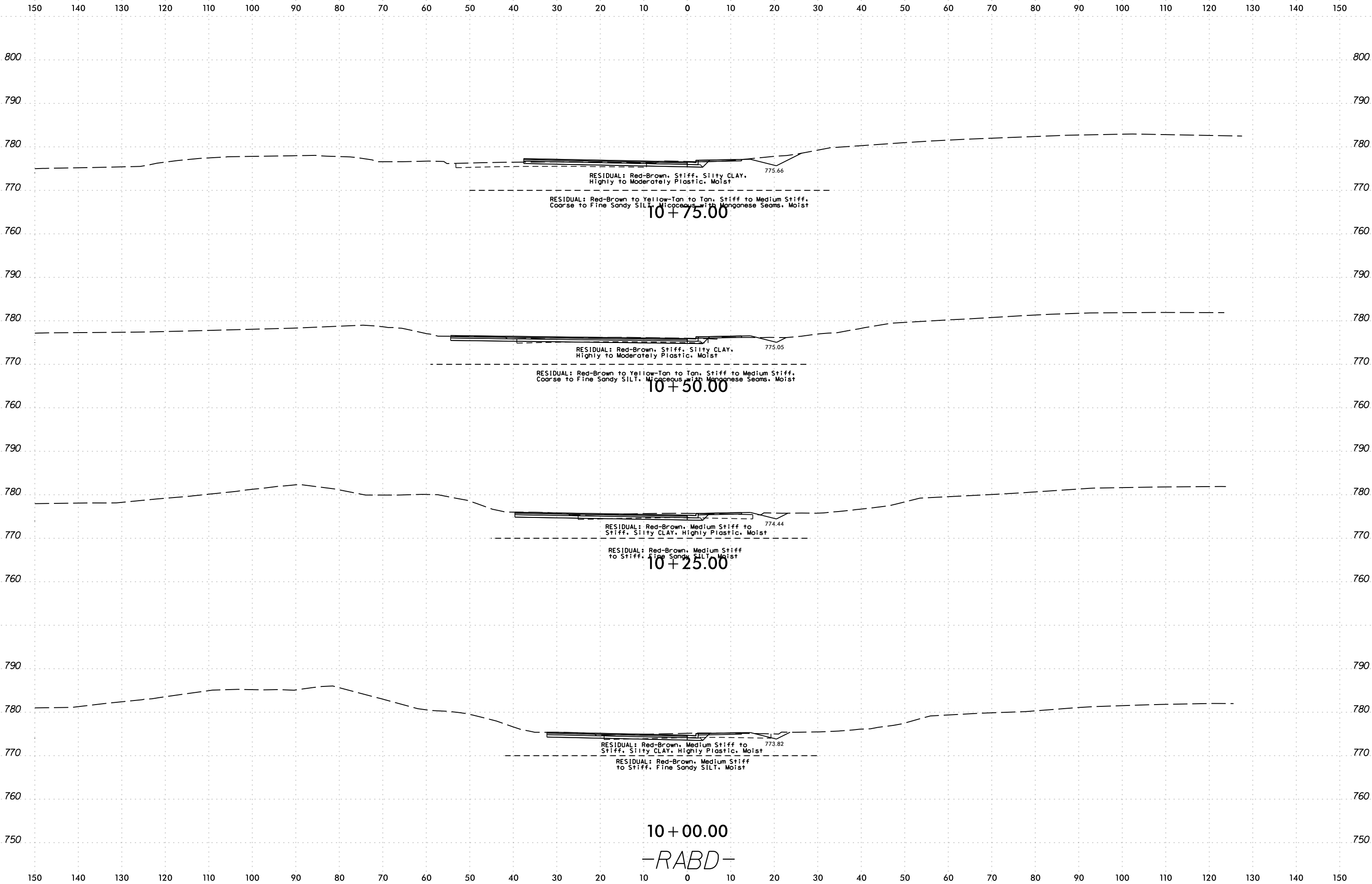


SOIL TEST RESULTS

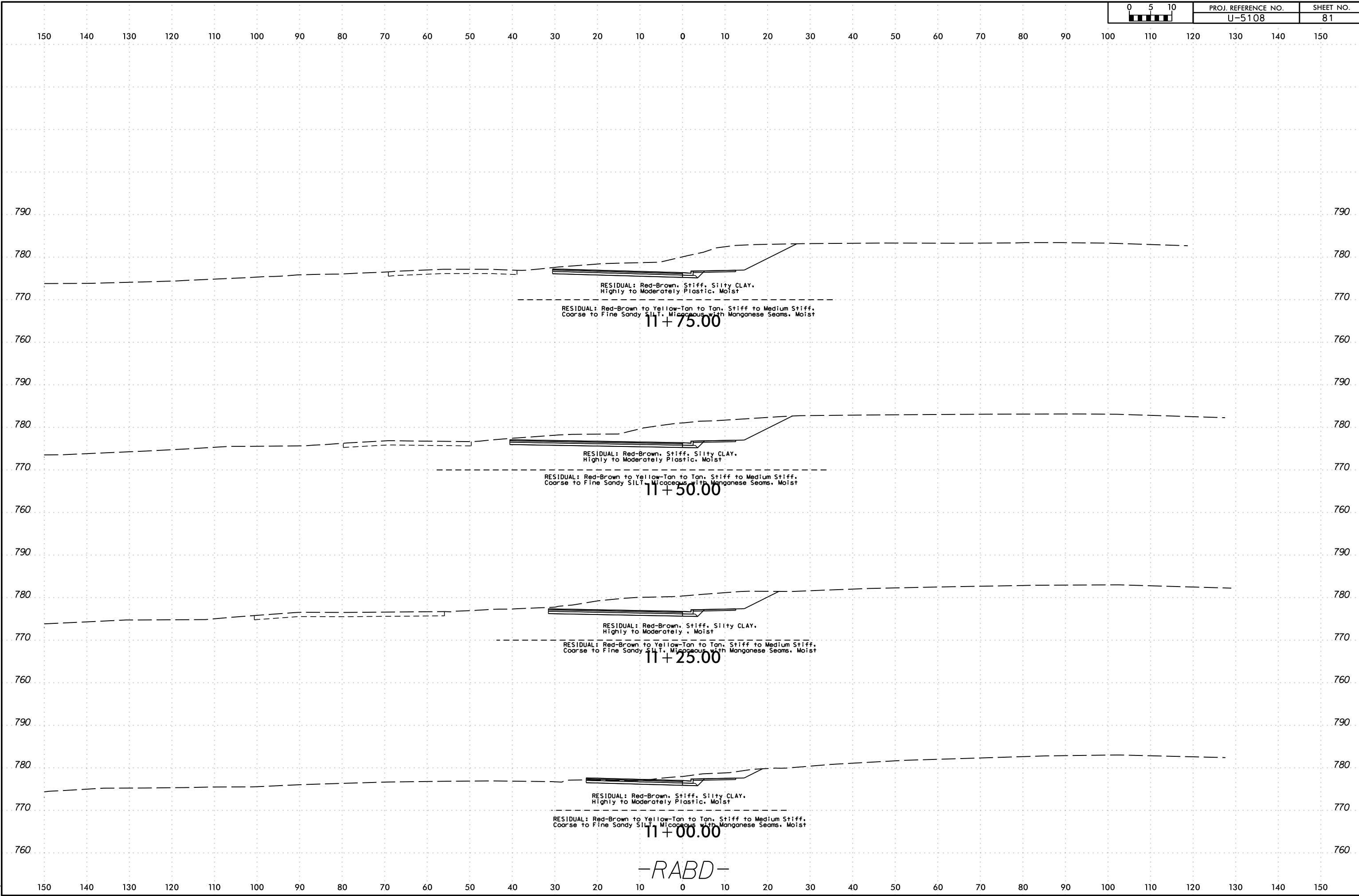
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)			MOISTURE	% ORGANIC	
							C. SAND	F. SAND	SILT	CLAY	10	40	200			
SS-24	44' LT	19+51	1.0-2.5	A-7.5	22	7.5	35	28	11	17	44	99	77	63	28.5	-

* NOTE: STATION AND OFFSET REFER TO -LI- ALIGNMENT

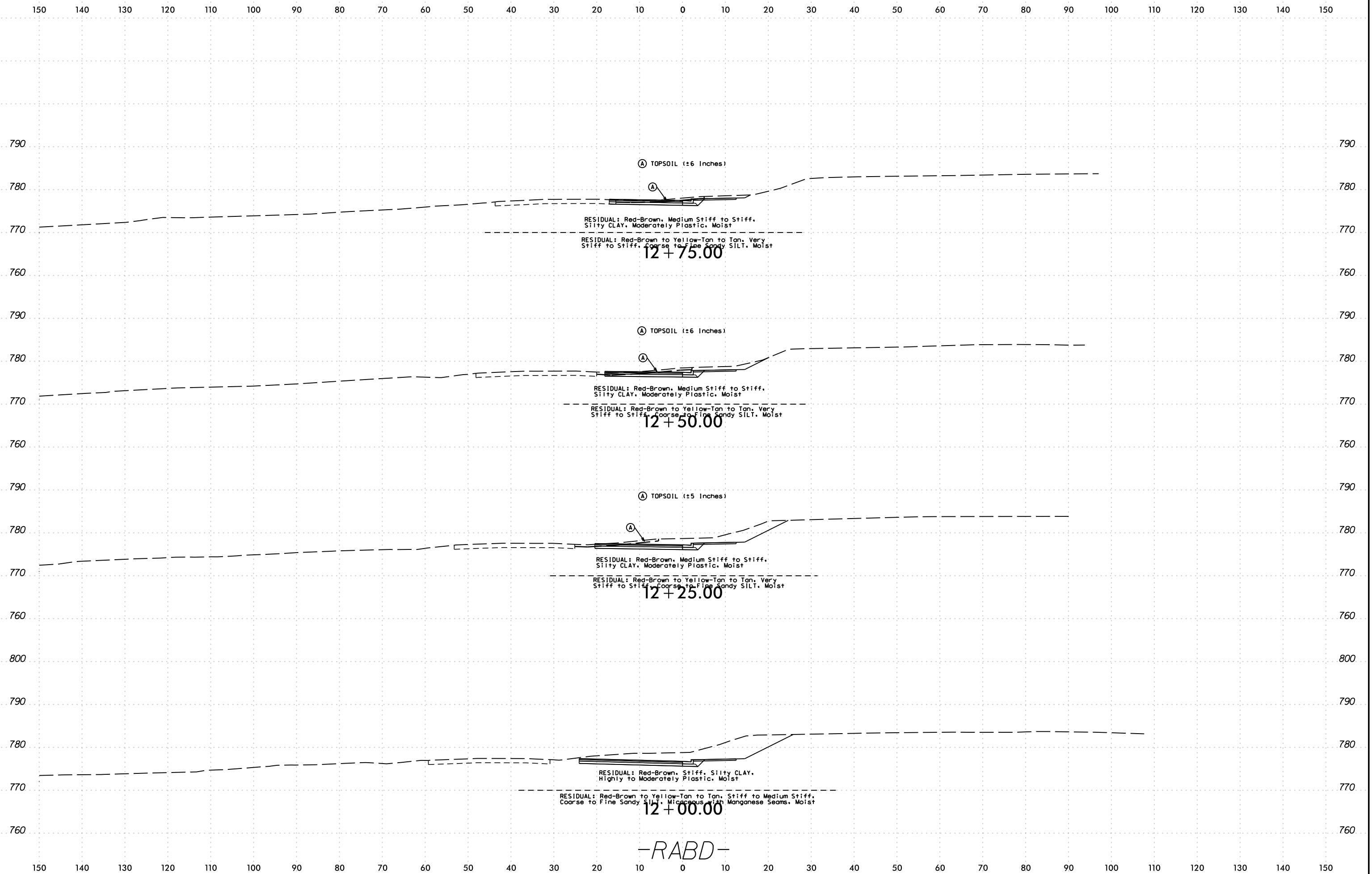




10+00.00
 -RABD-



-RABD-



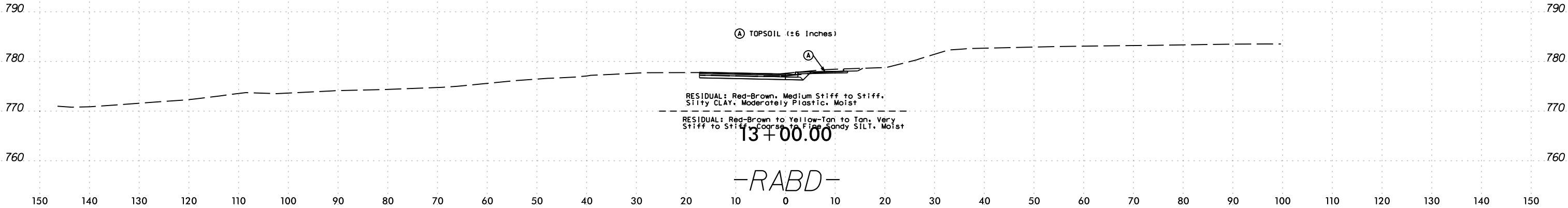
6/23/16



PROJ. REFERENCE NO.	SHEET NO.
U-5108	83

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 rps:ana



150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT
SUBSURFACE INVESTIGATION
APPENDIX A
LABORATORY TEST RESULTS

REFERENCE: U-5108

PROJECT: 42370



ESP ASSOCIATES, INC.
7011 ALBERT PICK RD
SUITE E
GREENSBORO, NC 27409
FIRM # C-0587
WWW.ESPASSOCIATES.COM

SOILS LABORATORY TESTS RESULTS

WBS NO.: 42370.1.1

TIP NO.: U-5108

COUNTY: Mecklenburg

SITE DESCRIPTION: Northcross Drive Extension From End of Northcross Drive to Westmoreland Drive

BORING NO.	SAMPLE NO.	BORING LOCATION	DEPTH INTERVAL (FT)	AASHTO CLASS	N	L.L	P.I.	% BY WEIGHT				% PASSING SIEVES			% MOISTURE	% ORGANIC
								CSE. SAND	F. SAND	SILT	CLAY	10	40	200		
EB1-A	SS-1	-L- STA. 73+46, 24' LT	3.5-5.0	A-2-4 (0)	2	NP	NP	61	26	5	8	99	57	16	22.3	-
EB2-A	SS-2	-L- STA. 74+56, 24' LT	8.7-10.2	A-4 (1)	2	31	7	19	41	21	19	100	93	49	36.6	-
EB2-B	SS-3	-L- STA. 74+56, 18' RT	8.7-10.2	A-7-6 (6)	3	41	20	28	28	17	27	95	80	47	26.2	-
L_2800	SS-4	-L-STA. 28+00, 29' RT	1.0-2.5	A-7-5 (35)	5	75	41	15	11	14	60	100	91	77	31.0	-
RWAL1-3	SS-5	-L- STA. 32+09, 13' LT	1.0-2.5	A-7-5 (27)	7	71	41	21	16	13	50	99	87	66	30.0	-
RWAL1-5	SS-6	-L- STA. 33+14, 22' LT	8.5-10.0	A-7-5 (7)	10	53	12	26	20	9	45	100	82	59	33.3	-
L_3800LT	SS-7	-L- STA. 38+00, 20' LT	1.0-2.5	A-7-5 (22)	6	68	38	33	7	9	51	100	73	61	25.8	-
L_4450	SS-8	-L- STA. 44+50, 15' LT	13.5-15.0	A-5 (3)	4	50	9	31	31	23	15	100	81	46	35.6	-
L_4600	SS-9	-L- STA. 46+00, CL	1.0-2.5	A-2-4 (0)	3	23	9	49	21	13	17	100	67	33	15.6	-
L_5600	SS-10	-L- STA. 56+00, CL	3.5-5.0	A-7-5 (11)	16	63	21	30	18	23	29	100	80	55	28.3	-
L_5700LT	SS-11	-L- STA. 57+00, 27' LT	13.5-15.0	A-7-5 (11)	13	62	22	29	19	28	24	100	80	56	17.9	-
L_5900	SS-12	-L- STA. 59+00, CL	1.0-2.5	A-7-5 (27)	17	97	55	42	5	9	44	100	65	54	31.1	-
L_6500RT	SS-13	-L- STA. 65+00, 27' RT	8.5-10.0	A-7-5 (9)	14	51	18	28	21	28	23	99	79	56	15.8	-
L_6700	SS-14	-L- STA. 67+00, 10' RT	1.0-2.5	A-7-5 (24)	8	63	33	21	10	14	55	100	84	71	30.7	-
L_7250	SS-15	-L- STA. 72+50, CL	1.0-2.5	A-4 (0)	54	NP	NP	36	32	21	11	96	72	37	15.8	-
L_7700	SS-16	-L- STA. 77+00, CL	1.0-2.5	A-7-6 (8)	9	42	25	32	21	14	33	100	79	49	16.8	-
L_7850	SS-17	-L- STA. 78+50, CL	3.5-5.0	A-7-6 (12)	9	54	30	33	18	11	38	99	76	53	22.5	-
L_8250	SS-18	-L- STA. 82+50, 20' RT	3.5-5.0	A-5 (3)	8	51	10	36	21	20	23	100	75	48	27.8	-
L_8250	SS-19	-L- STA. 82+50, 20' RT	8.5-10.0	A-5 (1)	8	52	9	37	28	22	13	100	75	42	21.2	-
L_9164	SS-20	-L- STA. 91+64, 49' LT	3.5-5.0	A-7-6 (7)	3	48	19	36	16	20	28	99	72	51	23.8	-
L_9175	SS-21	-L- STA. 91+75, 35' RT	3.5-5.0	A-6 (1)	2	36	14	40	26	16	18	99	71	37	27.7	4.2
L_9175	SS-22	-L- STA. 91+75, 35' RT	8.5-10.0	A-7-5 (2)	5	42	12	33	30	24	13	99	77	42	29.3	-
L_9400	SS-23	-L- STA. 94+00, CL	3.5-5.0	A-7-6 (7)	17	48	27	41	17	7	35	100	70	44	11.2	-
L1_1951	SS-24	-L1- STA. 19+51, 44' LT	1.0-2.5	A-7-5 (22)	11	75	35	28	11	17	44	99	77	63	28.5	-
Y6_1250	SS-25	-Y6- STA. 12+50, 37' LT	3.5-5.0	A-7-6 (4)	16	44	23	46	17	11	26	99	64	39	14.3	-
Y6_1450LT	SS-26	-Y6- STA. 14+50, 61' LT	8.5-10.0	A-2-7 (2)	5	41	24	50	20	10	20	99	63	32	15.0	-

Signed: 

NCDOT Certification No. 129-04-0411