

SEE SHEET 3 FOR PLAN SHEET LAYOUT  
AT TIME OF INVESTIGATION

STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5861	1	175

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

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INVESTIGATED BY RK&K, LLP

DRAWN BY A. BOZORGI

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SUBMITTED BY RK&K, LLP

DATE MARCH 2020

ROADWAY  
SUBSURFACE INVESTIGATION

COUNTY CHEROKEE  
PROJECT DESCRIPTION WIDENING US 19/29 FROM  
THE GEORGIA STATE LINE TO US 64/74

INVENTORY

CROSS SECTIONS

LINE	STATION	SHEETS
-DR5-	12+00	150
-DR6-	12+50	151
-DR7-	11+00 - 13+00	152 - 153
-DR8-	13+00	154
-DR9-	11+50	155
-DR10-	12+00	156
-DR11-	10+50 - 11+50	157
-DR12-	10+50	158
-DR13-	10+50	159
-DR14-	11+00	160
-DR15-	11+00	161
-DR16-	11+00	162
-DR17-	11+00 - 11+25	163
-DR18-	10+50	164
-DR19-	10+50	165
-DR20-	10+55 - 10+95	166
-DR21-	10+00 - 10+50	167 - 168
-DR22-	10+00 - 13+00	169 - 170

\* These cross sections are subsets of -L- cross sections.

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APPENDIX	TITLE	SHEETS
A	BORING LOGS	172
B	LAB RESULTS	173 - 175

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LINE	STATION	PLAN
-L_DET1-	10+00 - 40+11	4 - 5
-L_DET2-	10+00 - 39+12	6 - 7
-L_DET3-	10+00 - 23+06	8
-L_DET4-	10+00 - 42+99	9 - 11
-L_DET6-	10+00 - 31+46	12 - 13
-DET_DR18-	10+00 - 11+45	9
-DET_DR18B-	10+00 - 11+40	9
-DET_DR19-	10+06 - 11+76	9
-DET_DR22-	10+40 - 13+37	12
-DET_Y1-	10+00 - 13+24	5
-L-	10+25 - 209+47	14 - 31
-Y1-	09+97 - 16+77	15
-Y2-	10+00 - 15+55	15
-Y3-	10+00 - 13+55	17
-Y3A-	10+00 - 12+40	17
-Y4-	12+72 - 14+95	19
-Y5-	10+00 - 11+40	19
-Y6-	11+30 - 17+24	21
-Y7-	10+00 - 13+10	21
-Y8-	10+50 - 12+77	23
-Y9-	10+00 - 13+50	23
-Y10A-	11+00 - 14+04	24
-Y10B-	11+50 - 19+51	25 & 31
-Y11-	11+00 - 14+43	25
-Y11A-	10+00 - 14+29	25 - 26
-Y12-	18+67 - 35+00	21 & 31
-Y13-	10+00 - 13+70	31
-DRI-	10+00 - 11+23	14
-DR2-	10+00 - 12+64	14
-DR5-	11+20 - 12+57	16
-DR6-	12+22 - 12+98	17
-DR7-	10+00 - 13+57	16 - 17
-DR8-	12+58 - 13+80	18
-DR9-	10+00 - 11+90	19
-DR10-	11+10 - 12+40	20
-DR11-	10+00 - 11+50	20
-DR12-	10+00 - 11+35	21
-DR13-	10+00 - 11+35	21
-DR14-	10+00 - 13+00	21 - 22
-DR15-	10+00 - 13+30	22
-DR16-	10+45 - 11+99	24
-DR17-	10+00 - 11+31	24
-DR18-	10+00 - 11+45	24
-DR18B-	10+00 - 11+85	24
-DR19-	10+00 - 11+75	24
-DR20-	10+55 - 11+10	25
-DR21-	10+00 - 11+25	24
-DR22-	10+00 - 13+37	27
-DR23-	10+00 - 12+09	26
-DR24-	10+00 - 11+32	28

CROSS SECTIONS

LINE	STATION	SHEETS
-L-	10+50 - 208+00	32 - 121
-L_DET1-	10+00 - 40+00	33 - 46
-L_DET2-	10+00 - 39+12	58 - 75
-L_DET3-	10+00 - 23+06	80 - 87
-L_DET4-	10+00 - 42+99	91 - 107
-L_DET6-	10+00 - 31+46	110 - 120
-Y1-	11+00 - 16+00	122 - 123
-Y2-	11+00 - 13+00	124
-Y3-	11+00 - 13+00	125 - 126
-Y3A-	11+50	127
-Y4-	13+50 - 15+00	128 - 129
-Y5-	11+00	130
-Y6-	10+50 - 16+00	131 - 133
-Y7-	11+00 - 13+00	134
-Y8-	10+50	135
-Y9-	11+00 - 13+50	136 - 137
-Y10A-	11+00 - 13+50	138 - 140
-Y10B-	12+00 - 17+50	141 - 142
-Y11-	11+00 - 13+00	143
-Y11A-	11+00 - 13+00	144 - 145
-Y12-	21+50 - 35+00	146 - 147
-DRI-	10+50 - 11+00	148
-DR2-	12+00	149

REFERENCE: R-5861

PROJECT: 47427

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Greg Goins 3/3/2020  
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-DR2-	12+00	149


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**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT  
SUBSURFACE INVESTIGATION  
SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS**

SOIL DESCRIPTION				GRADATION				ROCK DESCRIPTION				TERMS AND DEFINITIONS			
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i>				WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.				HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:				ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS IN OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SRC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SRQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.			
SOIL LEGEND AND AASHTO CLASSIFICATION				ANGULARITY OF GRAINS				WEATHERED ROCK (WR)				NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.			
GENERAL CLASS.				MINERALOGICAL COMPOSITION				CRYSTALLINE ROCK (CR)				FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.			
GROUP CLASS.				COMPRESSIBILITY				NON-CRYSTALLINE ROCK (INCR)				FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.			
SYMBOL				PERCENTAGE OF MATERIAL				COASTAL PLAIN SEDIMENTARY ROCK (CP)				COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.			
% PASSING				GROUND WATER				FRESH				ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.			
MATERIAL PASSING #40				MISCELLANEOUS SYMBOLS				VERY SLIGHT (V SL.)				ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.			
GROUP INDEX				ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION				SLIGHT (SL.)				ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.			
USUAL TYPES OF MAJOR MATERIALS				SOIL SYMBOL				MODERATE (MOD.)				SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.			
GEN. RATING AS SUBGRADE				ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT				MODERATELY SEVERE (MOD. SEV.)				ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. IF TESTED, WOULD YIELD SPT REFUSAL			
PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30				INFERRED SOIL BOUNDARY				SEVERE (SEV.)				ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF			
CONSISTENCY OR DENSENESS				INFERRED ROCK LINE				VERY SEVERE (V SEV.)				ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF			
PRIMARY SOIL TYPE				ALLUVIAL SOIL BOUNDARY				COMPLETE				ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.			
RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)				RECOMMENDATION SYMBOLS				VERY HARD				CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.			
RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> )				UNDERCUT				HARD				CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.			
TEXTURE OR GRAIN SIZE				SHALLOW UNDERCUT				MODERATELY HARD				CAN BE SCRATCHED BY KNIFE OR PICK, GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.			
U.S. STD. SIEVE SIZE				UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE				MEDIUM				CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PEICES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.			
BOULDER (BLDR.)				UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK				HARD				CAN BE GROOVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.			
GRAIN SIZE				ABBREVIATIONS				VERY SOFT				CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGERNAIL.			
SOIL MOISTURE - CORRELATION OF TERMS				AR - AUGER REFUSAL				SOFT				FRACTURE SPACING			
SOIL MOISTURE SCALE (ATTERBERG LIMITS)				BT - BORING TERMINATED				MODERATELY SOFT				BEDDING			
FIELD MOISTURE DESCRIPTION				CL - CLAY				VERY HARD				TERM			
GUIDE FOR FIELD MOISTURE DESCRIPTION				CPT - CONE PENETRATION TEST				HARD				SPACING			
- SATURATED - (SAT.)				CSE. - COARSE				MODERATELY HARD				TERM			
USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE				DMT - DILATOMETER TEST				HARD				THICKNESS			
- WET - (W)				DPT - DYNAMIC PENETRATION TEST				MODERATELY HARD				VERY THICKLY BEDDED			
SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE				e - VOID RATIO				MODERATELY HARD				THICKLY BEDDED			
- MOIST - (M)				F - FINE				MODERATELY HARD				THINLY BEDDED			
SOLID; AT OR NEAR OPTIMUM MOISTURE				FOSS. - FOSSILIFEROUS				MODERATELY HARD				VERY THINLY BEDDED			
- DRY - (D)				FRAC. - FRACTURED, FRACTURES FRAGS. - FRAGMENTS				MODERATELY HARD				THICKLY LAMINATED			
REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE				HL. - HIGHLY				MODERATELY HARD				THINLY LAMINATED			
PLASTICITY				EQUIPMENT USED ON SUBJECT PROJECT				MODERATELY HARD				INDURATION			
PLASTICITY INDEX (PI)				DRILL UNITS:				MODERATELY HARD				TERM			
DRY STRENGTH				CME-45C				MODERATELY HARD				THICKNESS			
NON PLASTIC				CME-55				MODERATELY HARD				VERY THICKLY BEDDED			
SLIGHTLY PLASTIC				CME-550				MODERATELY HARD				THICKLY BEDDED			
MODERATELY PLASTIC				VANE SHEAR TEST				MODERATELY HARD				THINLY BEDDED			
HIGHLY PLASTIC				PORTABLE HOIST				MODERATELY HARD				VERY THINLY BEDDED			
COLOR				X DEIDRICH D-50				MODERATELY HARD				THICKLY LAMINATED			
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.				ADVANCING TOOLS:				MODERATELY HARD				THINLY LAMINATED			
				CLAY BITS				MODERATELY HARD				INDURATED			
				6" CONTINUOUS FLIGHT AUGER				MODERATELY HARD				EXTREMELY INDURATED			
				8" HOLLOW AUGERS				MODERATELY HARD							
				HARD FACED FINGER BITS				MODERATELY HARD							
				TUNG-CARBIDE INSERTS				MODERATELY HARD							
				CASING W/ ADVANCER				MODERATELY HARD							
				TRICONE STEEL TEETH				MODERATELY HARD							
				TRICONE TUNG-CARB.				MODERATELY HARD							
				CORE BIT				MODERATELY HARD							
				HAMMER TYPE:				MODERATELY HARD							
				AUTOMATIC				MODERATELY HARD							
				MANUAL				MODERATELY HARD							
				CORE SIZE:				MODERATELY HARD							
				B				MODERATELY HARD							
				H				MODERATELY HARD							
				HAND TOOLS:				MODERATELY HARD							
				POST HOLE DIGGER				MODERATELY HARD							
				HAND AUGER				MODERATELY HARD							
				SOUNDING ROD				MODERATELY HARD							
				VANE SHEAR TEST				MODERATELY HARD							



March 2, 2020

**WBS Number:** 47427.1.1

**TIP Number:** R-5861

**County:** Cherokee

**Description:** Widening US 19/129 from the Georgia State Line to US 64/74

**Subject:** Roadway Subsurface Inventory Report

## PROJECT DESCRIPTION

The project begins at the North Carolina-Georgia state line and extends approximately 4.2 miles north to US 64 in Cherokee County, North Carolina. The project consists of realigning/widening and improvements of existing US 19/129.

Two Diedrich D-50 drill rigs with automatic hammers were used for the geotechnical investigation from July to September of 2019. During this time, a total of 168 Standard Penetration Tests (SPT) borings and 8 Auger probe borings were drilled. Representative soil samples were collected for visual classification and laboratory testing. Bulk samples were collected from select proposed excavation areas for laboratory testing.

The following alignments were investigated. Selected cross sections of these alignments are included in this report.

<u>Line</u>	<u>Stations (±)</u>
-LDET1-	10+00 – 40+00
-LDET2-	10+00 – 39+12
-LDET3-	10+00 – 23+06
-LDET4-	10+00 – 42+99
-LDET6-	10+00 – 31+46
-DET_DR18-	10+00 – 11+45
-DET_DR18B-	10+00 – 11+40
-DET_DR19-	10+00 – 11+76
-DET_DR22-	10+00 – 13+37
-DET_Y1-	10+00 – 13+14
-L-	10+25 – 209+47
-Y1-	09+97 - 16+77
-Y2-	10+00 - 15+55
-Y3-	10+00 - 13+55
-Y3A-	10+00 - 12+40
-Y4-	12+72 - 14+95
-Y5-	10+00 - 11+40
-Y6-	11+30 - 17+24
-Y7-	10+00 - 13+10
-Y8-	10+50 - 12+77

R-5861: Widening US 19/129 from the Georgia State Line to US 64/74

-Y9-	10+00 - 13+50
-Y10A-	11+00 - 14+04
-Y10B-	11+50 - 19+51
-Y11-	11+00 - 14+43
-Y11A-	10+00 - 14+29
-Y12-	18+67 - 35+00
-Y13-	10+00 - 13+70
-DR1-	10+00 - 11+23
-DR2-	10+00 - 12+64
-DR5-	11+20 - 12+57
-DR6-	12+22 - 12+98
-DR7-	10+00 - 13+57
-DR8-	12+58 - 13+80
-DR9-	10+00 - 11+90
-DR10-	11+10 - 12+40
-DR11-	10+00 - 11+50
-DR12-	10+00 - 11+35
-DR13-	10+00 - 11+35
-DR14-	10+00 - 13+00
-DR15-	10+00 - 13+30
-DR16-	10+45 - 11+99
-DR17-	10+00 - 11+31
-DR18-	10+00 - 11+45
-DR18B-	10+00 - 11+85
-DR19-	10+00 - 11+75
-DR20-	10+55 - 11+10
-DR21-	10+00 - 11+25
-DR22-	10+00 - 13+37
-DR23-	10+00 - 12+09
-DR24-	10+00 - 11+32

## PHYSIOGRAPHY AND GEOLOGY

The proposed project is located within the Blue Ridge Physiographic Province, along the existing US 19/129 corridor from the Georgia state line to the intersection with US-64/US-74, and passes through a populated rural area. Terrain within the proposed project corridor consists of large hills to mountains separated by mountain streams. The proposed project passes along and between steeply sloping hillsides.

The bedrock underlying the proposed project consists of members of the Ocoee Supergroup and Murphy Belt (Geologic Map of North Carolina, 1985). These rocks include schist, phyllite, slate, quartzite, and assorted slightly metamorphosed sedimentary rocks (metagraywacke, metasilstone, metasandstone, and metaconglomerate), several of which were encountered and identified during the investigation. Some existing cut slopes within the project have exposed underlying bedrock. The overlying residual soils are a result of physical and chemical weathering of the underlying bedrock.





**SOIL PROPERTIES**

Soils encountered during the geotechnical investigation are separated into four (4) categories based on soil origin. The origins consist of roadway embankment, artificial fill, alluvial soils, and residual soils.

**Roadway Embankment:** Materials interpreted as roadway embankment were encountered within the limits of the existing US 19/129 alignment. The roadway embankment generally consisted of loose to dense, sandy GRAVEL (A-1-b) and silty to clayey SAND (A-2-4, A-2-5, A-2-6, A-2-7) and medium stiff to very stiff, sandy to clayey SILT (A-4 and A-5) to sandy silty CLAY (A-6). The thickness of the encountered roadway embankment varied up to 11.5 feet.

**Artificial Fill:** Artificial fill was found in the proposed project area where land had been graded for construction of businesses and in the parking lots. The fill consists of stiff sandy CLAY (A-6). The thickness of the encountered artificial fill varied up to 2.0 feet.

**Alluvial Soils:** Alluvial soils were typically associated with drainage features or areas where creeks previously crossed or are adjacent to the proposed alignment. Alluvial soils generally consisted very soft to stiff sandy SILT (A-4) and sandy silty CLAY (A-6, A-7-5, and A-7-6), and very loose silty clayey SAND (A-2-5). The thickness of the encountered alluvial soils varied up to 12.0 feet.

**Residual Soils:** Soils classified as residual soils generally consisted of very loose to very dense, clayey and silty fine to coarse SAND (A-1-b, A-2-4, A-2-5, A-2-6, A-2-7.) and very soft to hard, sandy SILT (A-4, A-5) and slightly to highly plastic silty CLAY (A-6, A-7-5, A-7-6). Varying amounts of mica and rock fragments were noted within soils interpreted as residual soils.

**ROCK PROPERTIES**

**Weathered Rock:** Weathered rock was encountered in sixty-eight (68) borings. Weathered rock was encountered at the following locations above or within six (6) feet of proposed grade:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	19+50 – 21+25	LT
-L-	42+00 – 43+50	LT & RT
-L-	44+50 – 49+00	LT & RT
-L-	53+50 – 55+50	LT & RT
-L-	78+50 – 81+50	LT & RT
-L-	85+50 – 95+00	LT & RT
-L-	103+00 – 107+00	LT & RT
-L-	113+00 – 119+00	LT & RT
-L-	121+00 – 123+50	LT & RT
-L-	149+00 – 152+00	LT & RT
-L-	159+50 – 178+50	LT & RT
-L-	185+00 – 190+00	LT & RT
-L_DET2-	18+75 – 24+75	LT & RT
-L_DET3-	10+00 – 12+00	LT & RT
-L_DET4-	19+00 – 22+20	LT & RT
-L_DET4-	31+25 – 32+50	LT & RT

-L_DET4-	35+00 – 39+50	LT & RT
-L_DET6-	14+00 – 22+25	LT & RT
-L_DET6-	23+25 – 26+00	LT & RT
-Y6-	15+00 – 16+75	LT & RT
-Y10B-	13+00 – 15+00	LT & RT
-Y10B-	17+00 – 19+00	LT & RT
-DR9-	10+50 – 12+50	LT & RT
-DR14-	10+00 – 12+00	LT & RT
-DR15-	10+75 – 11+75	LT & RT
-DR22-	10+25 – 11+25	LT & RT
-DR23-	10+75 – 11+25	LT & RT

**Crystalline Rock:** Crystalline rock is defined as auger refusal or SPT refusal with penetration by split spoon of less than or equal to 0.1 feet per 60 blows. Crystalline rock was encountered in twenty-three (23) borings. Crystalline rock was encountered at the following locations above or within six (6) feet of proposed grade:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	18+25 – 19+50	LT
-L-	43+50 – 45+50	LT & RT
-L-	88+25 – 89+25	LT
-L-	90+25 – 92+75	LT
-L-	117+00 – 118+75	RT
-L-	165+50 – 167+50	LT & RT
-L_DET2-	18+40 – 19+40	LT & RT
-L_DET2-	20+50 – 23+00	LT & RT
-L_DET4-	19+20 – 20+75	LT & RT
-L_DET4-	35+00 – 36+90	LT & RT

**GROUNDWATER**

Groundwater was encountered during drilling operations (0-hr reading) within thirty-one (31) borings at elevations ranging from 1613.8 to 1759.6. Static (24-hr reading) measurements were recorded within forty-three (43) borings at elevations ranging from 1624.0 to 1766.2.

**Ponds:** Five (5) ponds are located within or in close proximity of right of way on this project. They are noted at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	82+24 – 86+61	RT
-L-	99+98 – 102+30	RT
-L-	102+81 – 105+11	RT
-Y9-	12+00 – 13+17	RT
-DR9-	10+04 – 10+79	LT

**Water wells:** Two water wells are located within right of way on this project. They are noted at the following locations:



-DR21- 10+00 – 10+95 LT &amp; RT

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	107+43	LT
-L-	158+74	LT
-Y6-	12+64	LT
-Y10B-	17+32	LT

**Groundwater:** Groundwater was encountered at the following locations above or within six (6) feet of the proposed grade:

#### AREAS OF SPECIAL GEOTECHNICAL INTEREST

**Alluvial Soils:** Alluvial soils were encountered along the proposed alignments at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	33+00 – 34+46	LT
-L-	35+96 – 37+19	LT
-L-	56+00 – 58+80	RT
-L-	71+21 – 73+64	LT & RT
-L-	83+90 – 86+26	LT & RT
-L-	126+57 – 128+25	LT & RT
-L_DET3-	14+40 – 16+55	LT & RT

**Artificial Fill:** Artificial fill was encountered along the proposed alignments at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-DR7-	10+64 – 11+55	LT & RT
-L-	108+19 – 110+30	LT

**Soft, Loose and/or Wet Soils:** Relatively soft or loose and/or wet soils were encountered along the proposed alignments at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L_DET3-	14+43 – 15+13	RT
-L_DET3-	15+75 – 16+55	RT
-L-	126+90 – 128+25	LT
-Y9-	12+60 – 13+20	RT

**Highly Plastic Soils:** Highly plastic soils with plasticity indices (PI) greater than 25 and within proposed cut sections or PI greater than 35 and/or high liquid limit within 3-ft of subgrade were encountered at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	21+75 – 26+75	LT & RT
-L-	137+25 – 139+25	LT
-L-	158+75 – 160+75	LT & RT
-L-	170+75 – 172+75	LT & RT
-L-	190+75 – 192+25	LT & RT
-DR17-	10+20 – 11+40	LT & RT

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	17+75 – 18+75	LT & RT
-L-	23+50 – 29+50	LT & RT
-L-	43+50 – 45+50	LT & RT
-L-	73+50 – 75+50	LT & RT
-L-	88+25 – 88+75	LT & RT
-L-	105+00 – 111+00	LT & RT
-L-	149+25 – 151+00	LT & RT
-L-	163+00 – 165+00	LT & RT
-L_DET2-	18+40 – 18+90	LT & RT
-L_DET4-	18+70 – 20+80	LT & RT
-Y1-	15+00 – 16+77	LT & RT
-Y2-	10+00 – 11+50	LT & RT
-Y6-	15+00 – 17+24	LT & RT
-Y9-	13+20 – 13+50	LT & RT
-Y10B-	16+30 – 19+51	LT & RT

The following areas contain groundwater above or within three (3) feet of the existing grade:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	17+75 – 18+75	LT & RT
-L-	23+50 – 29+50	LT & RT
-L-	43+50 – 45+50	LT & RT
-L-	107+00 – 111+00	LT & RT
-L-	149+25 – 151+00	LT & RT
-L-	163+00 – 165+00	LT & RT
-L_DET4-	18+70 – 20+80	LT & RT
-Y1-	15+00 – 16+77	LT & RT
-Y2-	10+00 – 11+50	LT & RT
-Y6-	15+00 – 17+24	LT & RT
-Y10B-	16+30 – 19+51	LT & RT



Prepared by,



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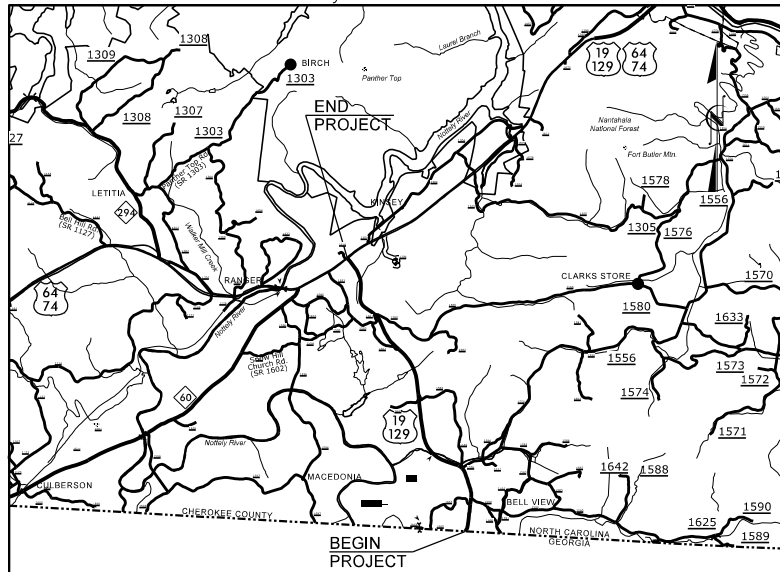
### Appendix A

#### Bulk Samples

The following bulk samples were collected from cut sections for laboratory testing:

Sample No.	Line	Station	Offset	Depth (ft)	Test(s) Performed
S-225	-L-	90+00	90' LT	1.0 – 8.5	Standard Proctor, California Bearing Ratio
S-1159	-L-	172+00	0	2.0 – 8.0	Standard Proctor, California Bearing Ratio
S-1041	-L_DET6-	191+99	20' RT	0.0 – 8.5	Standard Proctor, California Bearing Ratio

See Sheet 1-A For Index of Sheets  
See Sheet 1-B For Conventional Symbols



VICINITY MAP (NTS)

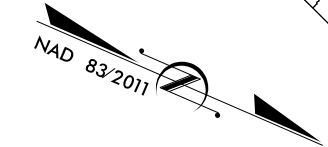
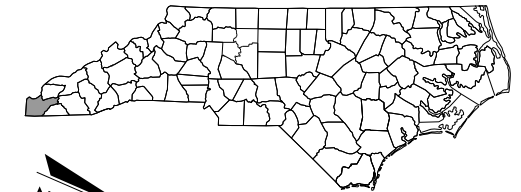
STATE OF NORTH CAROLINA  
DIVISION OF HIGHWAYS

**CHEROKEE COUNTY**

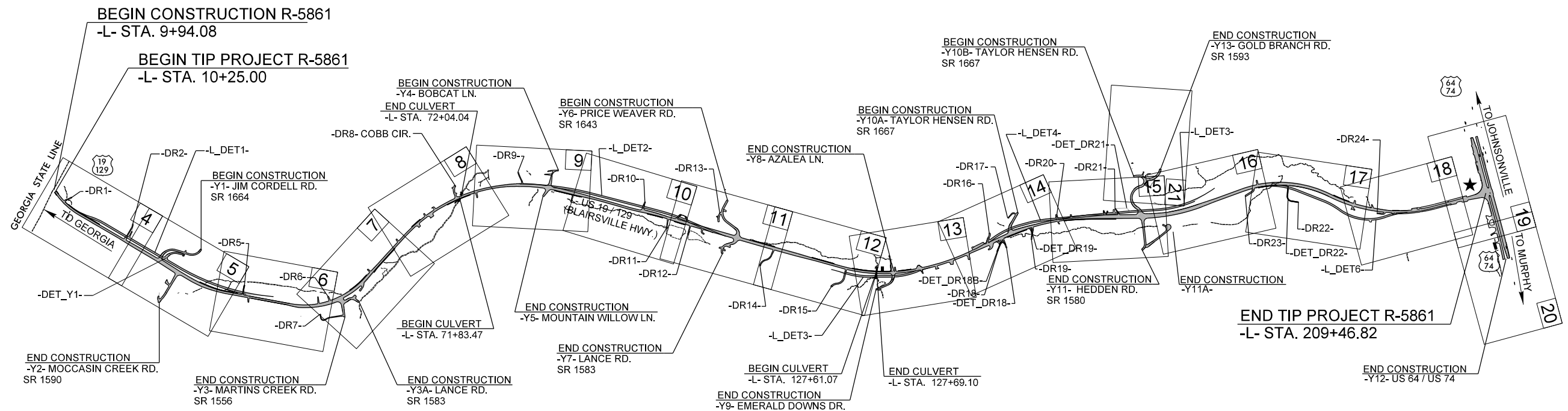
**LOCATION: WIDENING US 19 /129 FROM THE GEORGIA STATE LINE TO US 64 /74.**

**TYPE OF WORK: GRADING, PAVING, WIDENING, DRAINAGE, CULVERTS, SIGNING, SIGNALS, & UTILITIES**

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5861	3	
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
47427.1.1	NHP - 0019 (058)	PE	
47427.2.1	NHP - 0019 (058)	UTILITIES & RW	



**TIP PROJECT: R-5861**

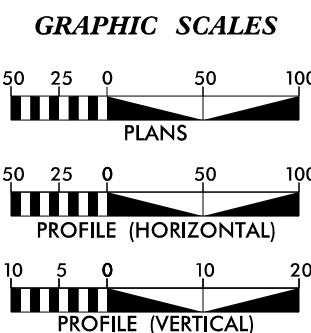


- NOTES:**
1. THIS PROJECT IS NOT WITHIN A MUNICIPAL BOUNDARY.
  2. CLEARING ON THIS PROJECT SHALL BE PERFORMED TO THE LIMITS ESTABLISHED BY METHOD III (EXCEPT IN PARALLEL STREAM LOCATIONS CLEAR ONLY TO THE SLOPE STAKE LINE.)
  3. DESIGN EXCEPTION FOR MINIMUM HORIZONTAL CURVE RADIUS, SAG VERTICAL CURVE, AND VERTICAL STOPPING SIGHT DISTANCE.

★ UPGRADE TRAFFIC SIGNAL

**INCOMPLETE PLANS**  
DO NOT USE FOR R/W ACQUISITION  
DOCUMENT NOT CONSIDERED FINAL  
UNLESS ALL SIGNATURES COMPLETED

**CONTRACT:**



**DESIGN DATA**  
ADT 2020 = 9,000  
ADT 2050 = 11,122  
V = 60 MPH  
DHV = 8%  
D = 55%  
T = 4% \*  
(\* TTST = 2% /\* DUAL = 2%)  
FUNC CLASS = RURAL ARTERIAL  
STATEWIDE TIER  
DESIGN EXCEPTIONS AS NOTED ON PLANS

**PROJECT LENGTH**

LENGTH ROADWAY TIP PROJECT R-5861.....3.767 miles  
LENGTH STRUCTURE TIP PROJECT R-5861.....0.000 miles  
TOTAL LENGTH OF PROJECT R-5861.....3.767 miles

**PLANS PREPARED BY:**  
**RK&K**  
900 RIDGEFIELD DRIVE, SUITE 350  
RALEIGH, NORTH CAROLINA 27609  
NC LICENSE NO. F-0112  
1-888-521-4455 OR 919-878-9560  
FOR NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
2018 STANDARD SPECIFICATIONS

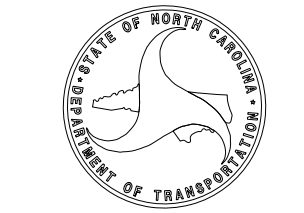
**RIGHT OF WAY DATE:** August 30, 2019  
**LETTING DATE:** December 15, 2020

**NCDOT CONTACT:** Kenneth J. McDowell  
DIVISION 14

**PROJECT ENGINEER:** Brandon McInnis, P.E.  
**PROJECT DESIGN ENGINEER:** Jillian Hinson, E.I.

**HYDRAULICS ENGINEER**  
SIGNATURE: \_\_\_\_\_ P.E.

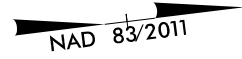
**ROADWAY DESIGN ENGINEER**  
SIGNATURE: \_\_\_\_\_ P.E.





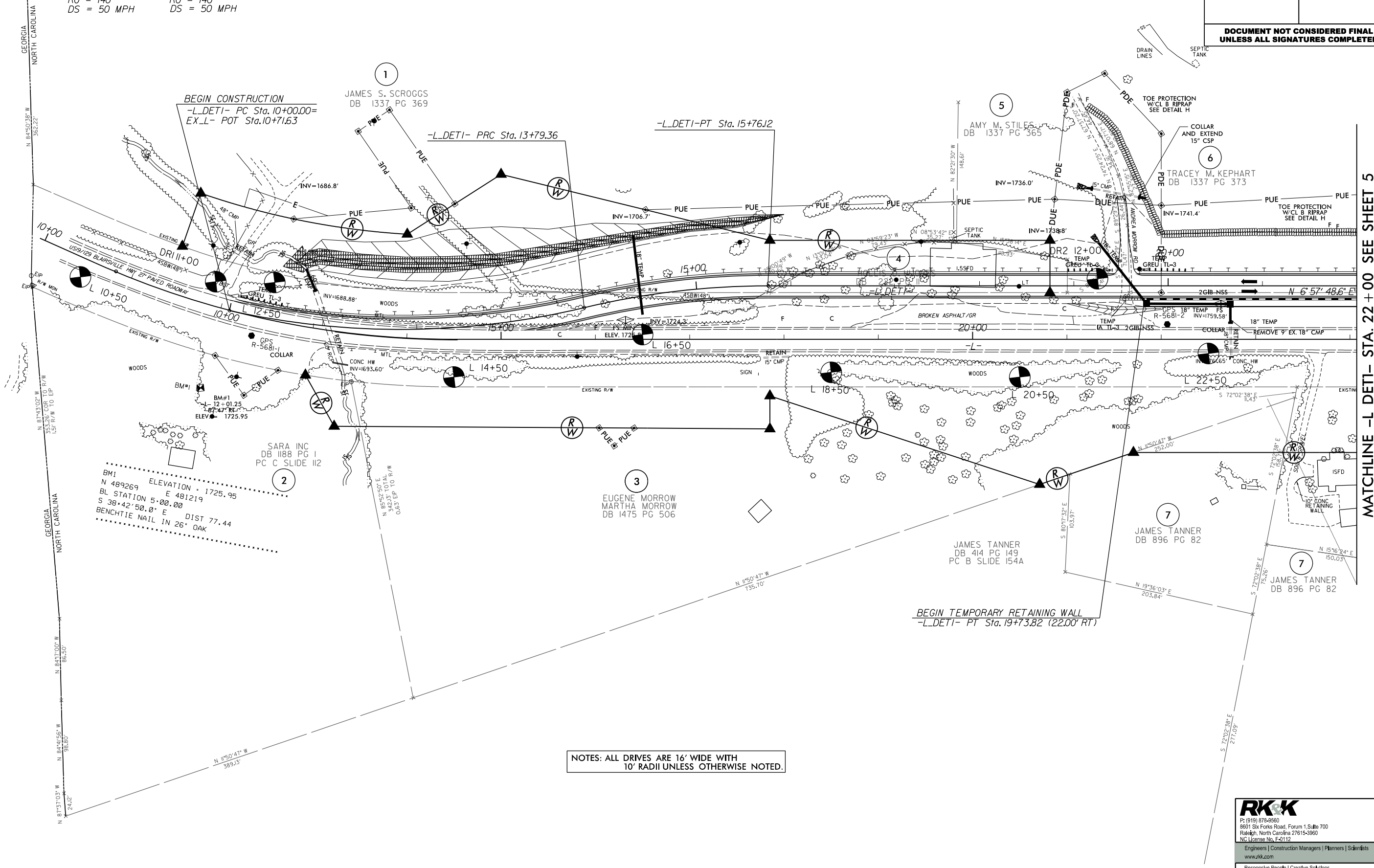
# -L\_DET1-

PROJECT REFERENCE NO. <i>R-586I</i>	SHEET NO. <b>4</b>
R/W SHEET NO. <b>2B-1</b>	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



**-L\_DET1-**

PI Sta 11+93.13	PI Sta 14+78.25
$\Delta = 26^{\circ}02'45.8''$ (LT)	$\Delta = 13^{\circ}30'33.5''$ (RT)
D = 6' 51" 57.2"	D = 6' 51" 57.2"
L = 379.36'	L = 196.76'
T = 193.13'	T = 98.90'
R = 835.00'	R = 835.00'
SE=0.06	SE=0.06
RO = 140	RO = 140
DS = 50 MPH	DS = 50 MPH



BM1 ELEVATION = 1725.95  
 N 489269 E 481219  
 BL STATION 5+00.00  
 S 38°42'50.0" E DIST 77.44  
 BENCHTIE NAIL IN 26" OAK

NOTES: ALL DRIVES ARE 16' WIDE WITH  
 10' RADII UNLESS OTHERWISE NOTED.

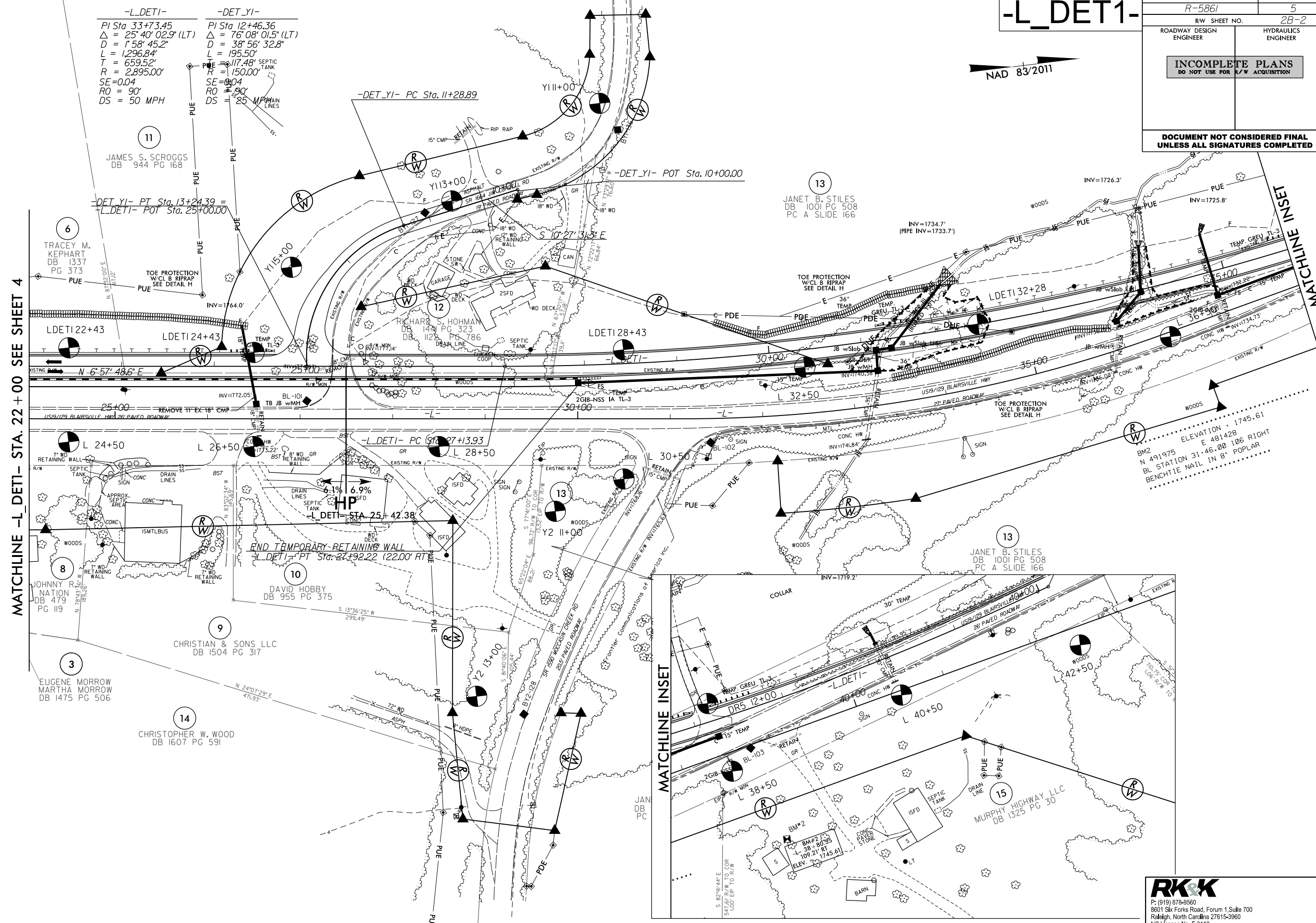
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MATCHLINE -L\_DET1- STA. 22+00 SEE SHEET 5

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# -L\_DET1-

PROJECT REFERENCE NO. R-5861	SHEET NO. 5
R/W SHEET NO. 2B-2	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



MATCHLINE -L\_DET1- STA. 22+00 SEE SHEET 4

MATCHLINE INSET

MATCHLINE INSET

**-L\_DET1-**  
 PI Sta 33+73.45  
 $\Delta = 25^\circ 40' 02.9''$  (LT)  
 $D = 1'58'' 45.2''$   
 $L = 1,296.84'$   
 $T = 659.52'$   
 $R = 2,895.00'$   
 $SE = 0.04$   
 $RO = 90'$   
 $DS = 50$  MPH

**-DET\_Y1-**  
 PI Sta 12+46.36  
 $\Delta = 76^\circ 08' 01.5''$  (LT)  
 $D = 38^\circ 56' 32.8''$   
 $L = 195.50'$   
 $R = 150.00'$   
 $SE = 0.04$   
 $RO = 90'$   
 $DS = 25$  MPH

**-DET\_Y1-** PT Sta. 13+24.39 =  
**-L\_DET1-** POT Sta. 25+00.00

**-DET\_Y1-** PC Sta. 11+28.89

**-DET\_Y1-** POT Sta. 10+00.00

**-L\_DET1-** PC Sta. 27+13.93

**-L\_DET1-** STA. 25+42.38

**-L\_DET1-** PT Sta. 27+92.22 (22.00' RT)

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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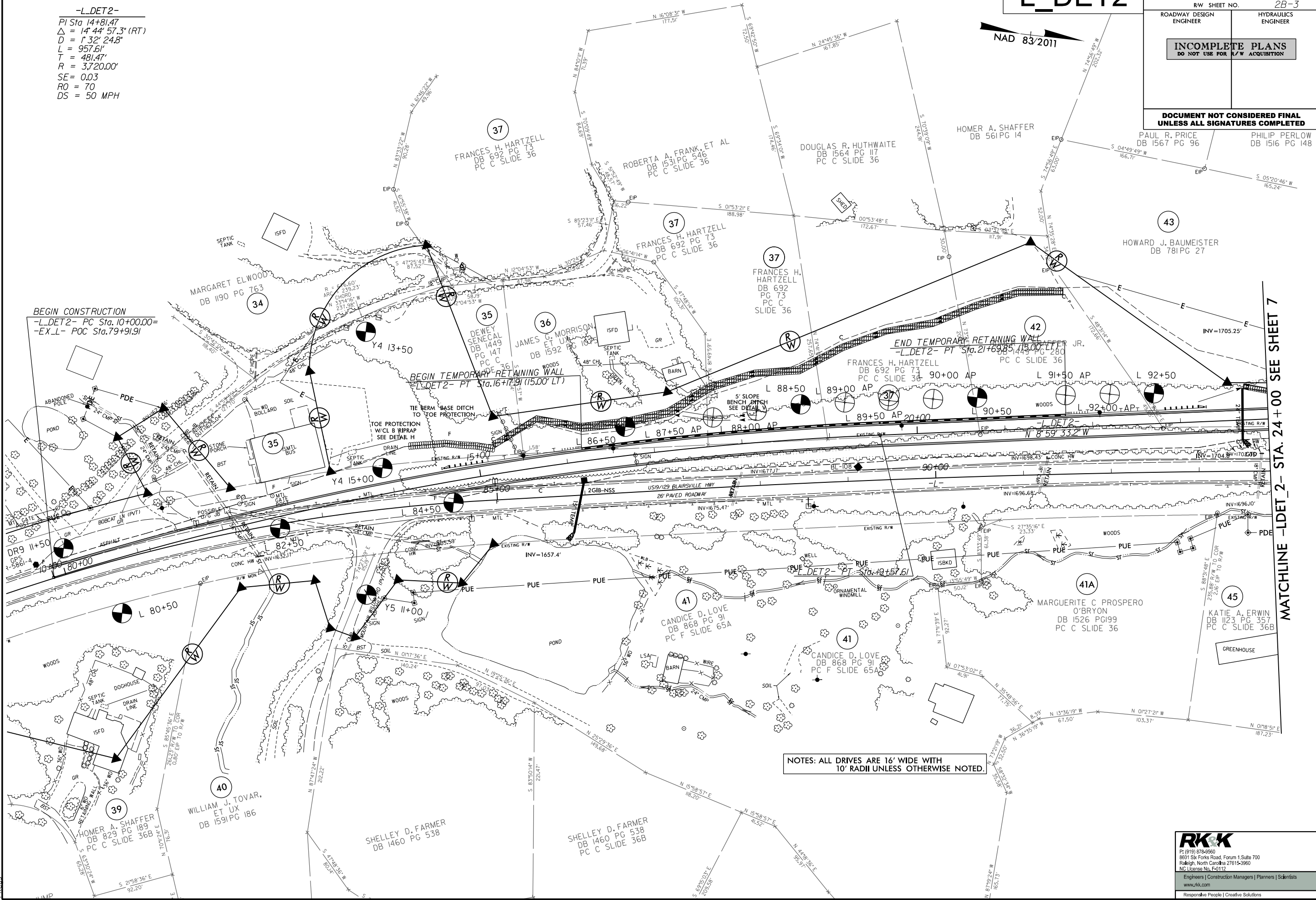


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2/26/2020  
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**-L\_DET2-**  
PI Sta 14+81.47  
 $\Delta = 14' 44" 57.3" (RT)$   
 $D = 1' 32" 24.8"$   
 $L = 957.61'$   
 $T = 481.47'$   
 $R = 3,720.00'$   
 $SE = 0.03$   
 $RO = 70$   
 $DS = 50 MPH$

# -L\_DET2-

PROJECT REFERENCE NO. <i>R-5861</i>	SHEET NO. <i>6</i>
R/W SHEET NO. <i>2B-3</i>	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	
PAUL R. PRICE DB 1567 PG 96	PHILIP PERLOW DB 1516 PG 148



**BEGIN CONSTRUCTION**  
-L\_DET2- PC Sta. 10+00.00=  
-EX\_L- POC Sta. 79+91.91

**BEGIN TEMPORARY RETAINING WALL**  
-L\_DET2- PT Sta. 16+17.91 (15.00' LT)

**END TEMPORARY RETAINING WALL**  
-L\_DET2- PT Sta. 21+69.85 (13.00' RT)

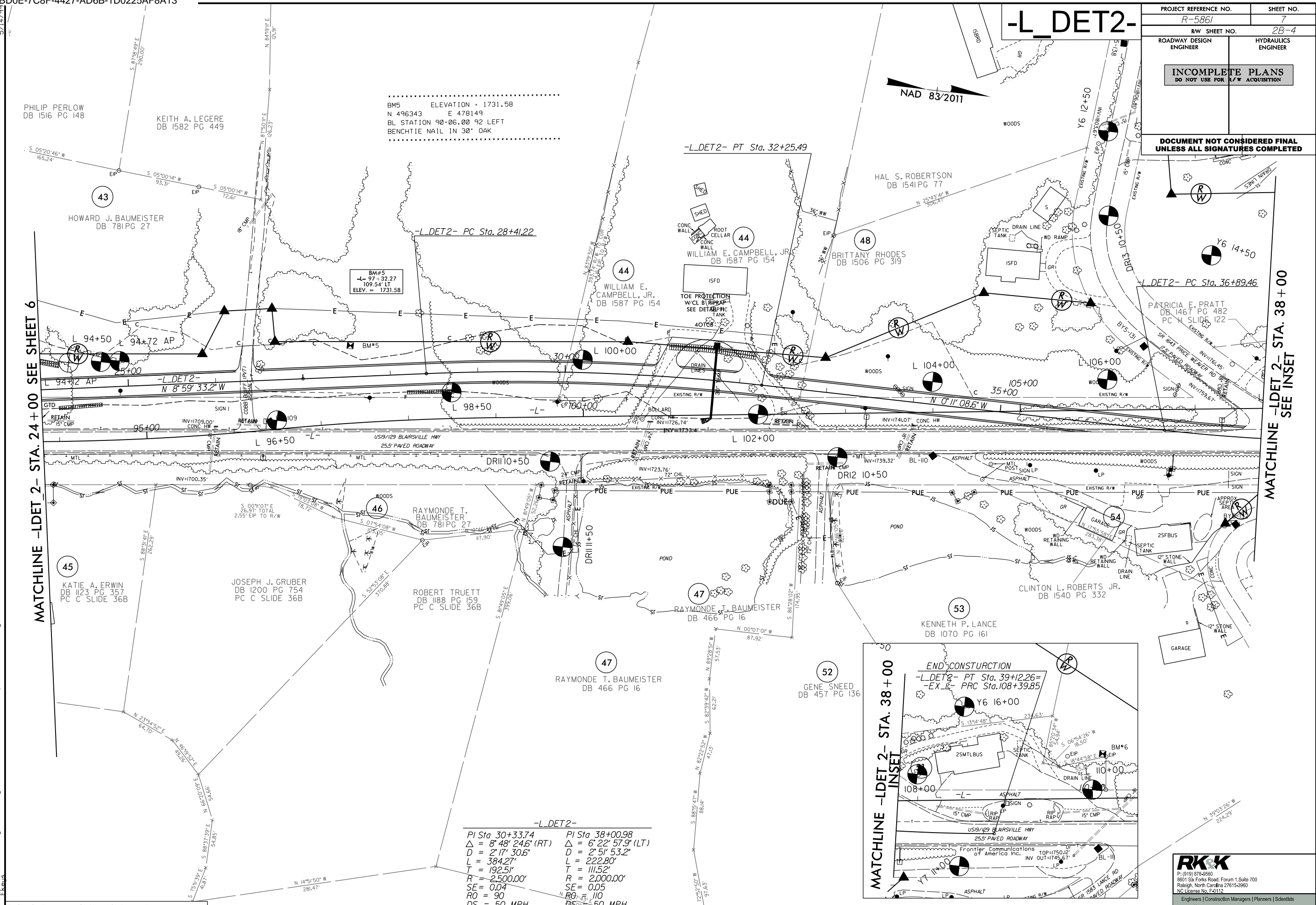
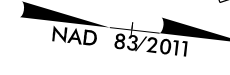
**NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.**

MATCHLINE -LDET\_2- STA. 24 + 00 SEE SHEET 7

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PROJECT REFERENCE NO.	SHEET NO.
R-5861	7
R/W SHEET NO.	2B-4
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	

# -L\_DET2-



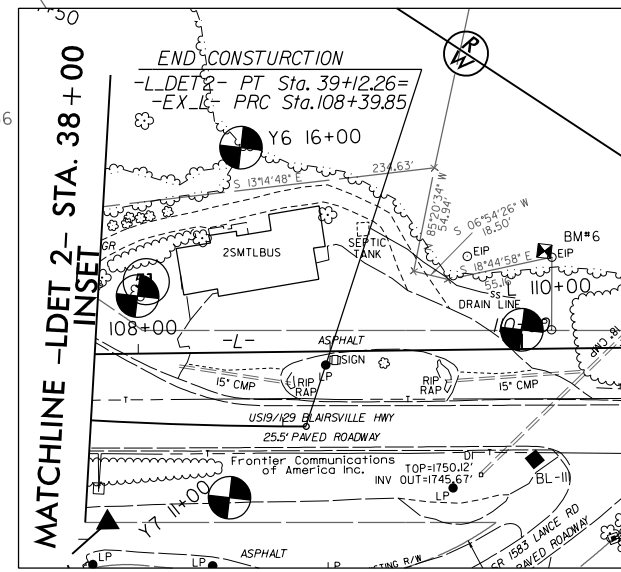
MATCHLINE -LDET 2- STA. 24+00 SEE SHEET 6

MATCHLINE -LDET 2- STA. 38+00 SEE INSET

BM5 ELEVATION = 1731.58  
 N 496343 E 478149  
 BL STATION 90+06.00 92 LEFT  
 BENCHTIE NAIL IN 30' OAK

BM#5  
 -L- 97+32.27  
 109.54' LT  
 ELEV. = 1731.58

-L_DET2-	
PI Sta 30+33.74	PI Sta 38+00.98
Δ = 8' 48" 24.6" (RT)	Δ = 6' 22" 57.9" (LT)
D = 2' 17" 30.6"	D = 2' 51" 53.2"
L = 384.27'	L = 222.80'
T = 192.51'	T = 111.52'
R = 2,500.00'	R = 2,000.00'
SE = 0.04	SE = 0.05
RO = 90	RO = 110
DS = 50 MPH	DS = 50 MPH



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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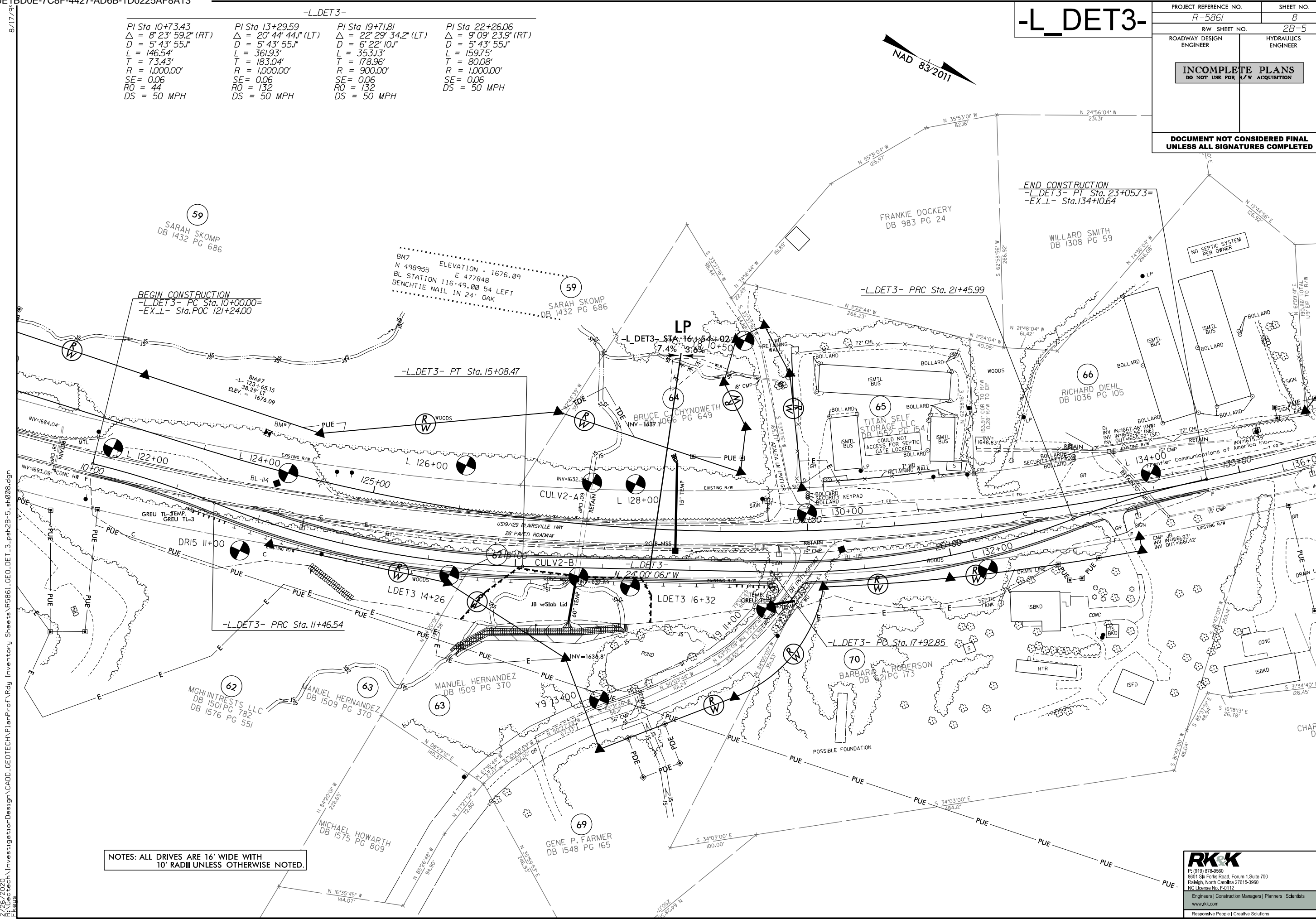


-L\_DET3-

PI Sta 10+73.43 Δ = 8° 23' 59.2" (RT) D = 5' 43' 55.1" L = 146.54' T = 73.43' R = 1,000.00' SE = 0.06 RO = 44 DS = 50 MPH	PI Sta 13+29.59 Δ = 20° 44' 44.1" (LT) D = 5' 43' 55.1" L = 361.93' T = 183.04' R = 1,000.00' SE = 0.06 RO = 132 DS = 50 MPH	PI Sta 19+71.81 Δ = 22° 29' 34.2" (LT) D = 6' 22' 10.1" L = 353.13' T = 178.96' R = 900.00' SE = 0.06 RO = 132 DS = 50 MPH	PI Sta 22+26.06 Δ = 9° 09' 23.9" (RT) D = 5' 43' 55.1" L = 159.75' T = 80.08' R = 1,000.00' SE = 0.06 RO = 132 DS = 50 MPH
---	--	--	--

-L\_DET3-

PROJECT REFERENCE NO. R-5861	SHEET NO. 8
R/W SHEET NO. 2B-5	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

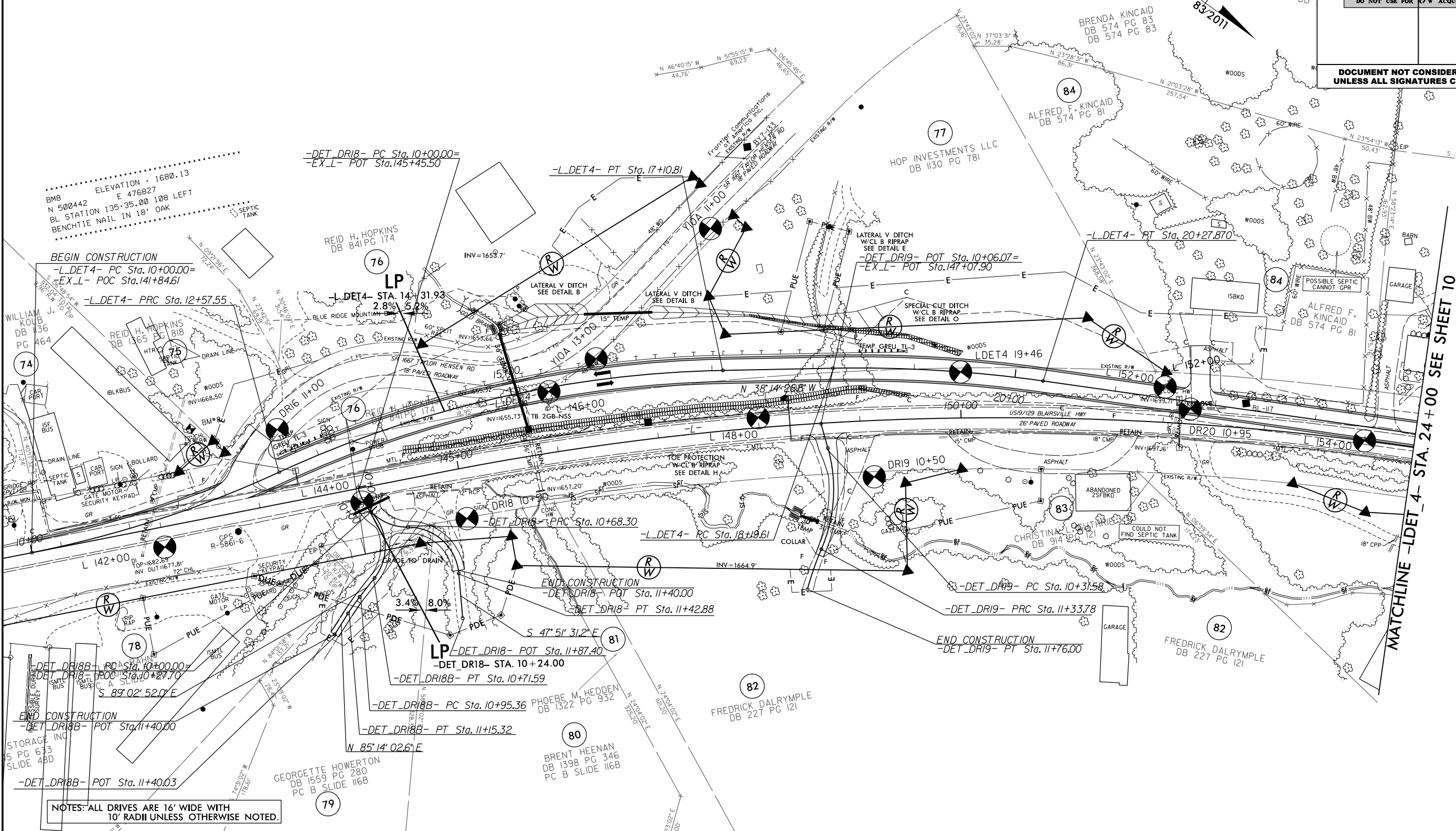
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# -L\_DET4-

PROJECT REFERENCE NO.	SHEET NO.
R-5861	9
R/W SHEET NO.	2B-6
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

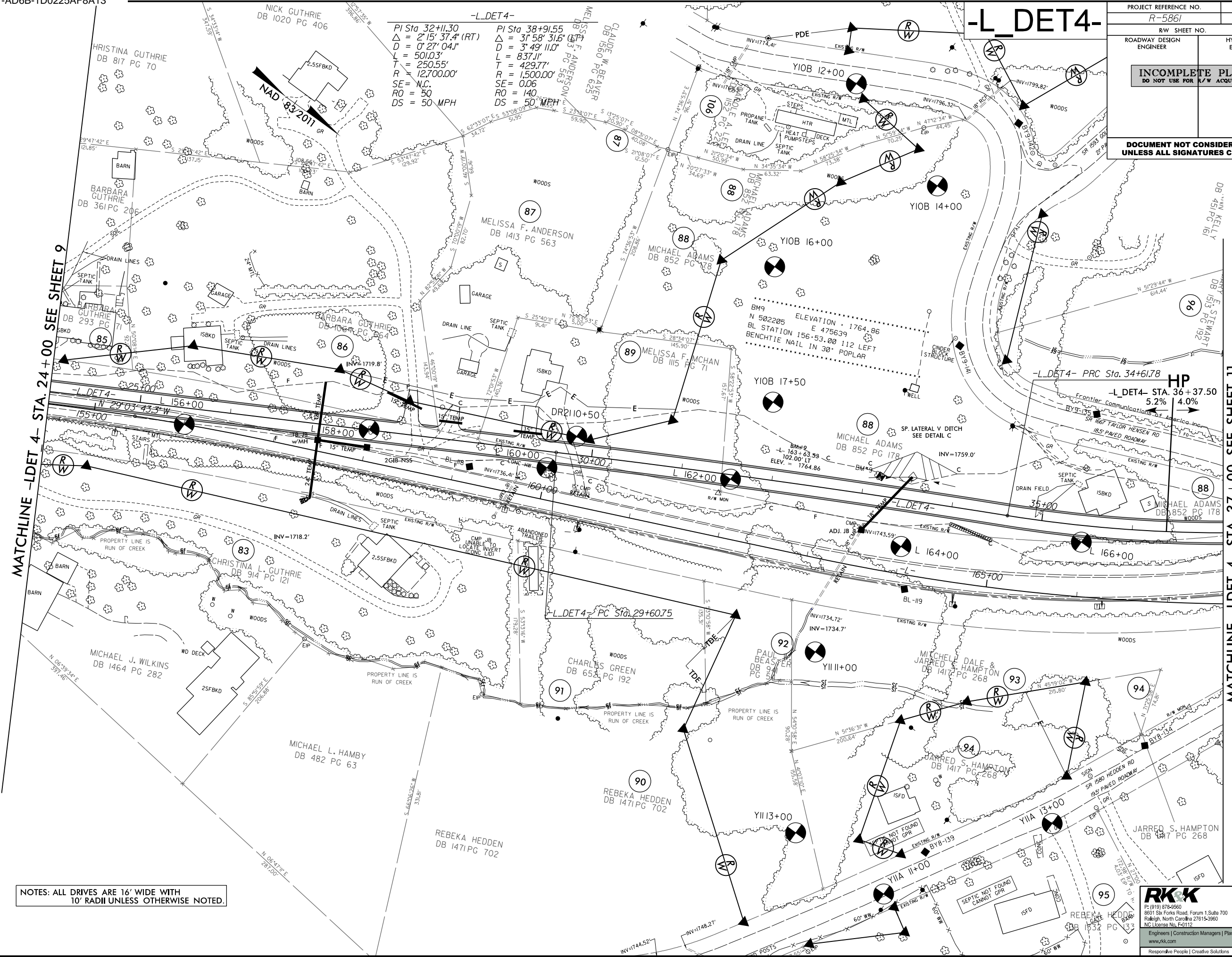
-L_DET4-		-DET_DR18-		-DET_DR18B-		-DET_DR19-	
PI Sta 11+29.41	PI Sta 14+87.52	PI Sta 10+40.68	PI Sta 11+4.49	PI Sta 10+43.49	PI Sta 11+05.35	PI Sta 10+84.76	PI Sta 11+54.93
$\Delta = 13' 25" 10.6" (LT)$	$\Delta = 23' 37" 01.0" (RT)$	$\Delta = 78' 15" 52.3" (LT)$	$\Delta = 85' 28" 02.8" (RT)$	$\Delta = 82' 02" 03.8" (RT)$	$\Delta = 5' 43" 05.5" (LT)$	$\Delta = 39' 02" 18.7" (RT)$	$\Delta = 8' 03" 46.2" (LT)$
D = 5' 12" 37.8"	D = 5' 12" 37.8"	D = 114' 35" 29.6"	D = 114' 35" 29.6"	D = 114' 35" 29.6"	D = 28' 38" 52.4"	D = 38' 11" 49.9"	D = 19' 05" 54.9"
L = 257.55'	L = 453.26'	L = 208.26'	L = 68.30'	L = 74.58'	L = 71.59'	L = 102.20'	L = 42.22'
T = 129.48'	T = 229.97'	T = 104.35'	T = 40.68'	T = 46.19'	T = 9.99'	T = 53.17'	T = 21.14'
R = 100.00'	R = 1,100.00'	R = 1,300.00'	R = 50.00'	R = 50.00'	R = 200.00'	R = 150.00'	R = 300.00'
	SE = 0.06	SE = 0.06					
	RO = 140	RO = 140					
	DS = 50 MPH	DS = 50 MPH					

MATCHLINE -LDET\_4- STA. 24+00 SEE SHEET 10





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2/26/2020  
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**-L\_DET4-**

PI Sta 32+11.30	PI Sta 38+91.55
$\Delta = 2' 15' 37.4'' (RT)$	$\Delta = 3' 58' 31.6''$
$D = 0' 27' 04.1''$	$D = 3' 49' 11.0''$
$L = 501.03'$	$L = 837.11'$
$T = 250.55'$	$T = 429.77'$
$R = 12,700.00'$	$R = 15,000.00'$
SE = N.C.	SE = 0.06
RO = 50	RO = 140
DS = 50 MPH	DS = 50 MPH

**-L\_DET4-**

PROJECT REFERENCE NO. R-5861	SHEET NO. 10
R/W SHEET NO. 2B-7	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	

**INCOMPLETE PLANS**  
DO NOT USE FOR R/W ACQUISITION

**DOCUMENT NOT CONSIDERED FINAL**  
UNLESS ALL SIGNATURES COMPLETED

MATCHLINE -LDET 4- STA. 24+00 SEE SHEET 9

MATCHLINE -LDET 4- STA. 37+00 SEE SHEET 11

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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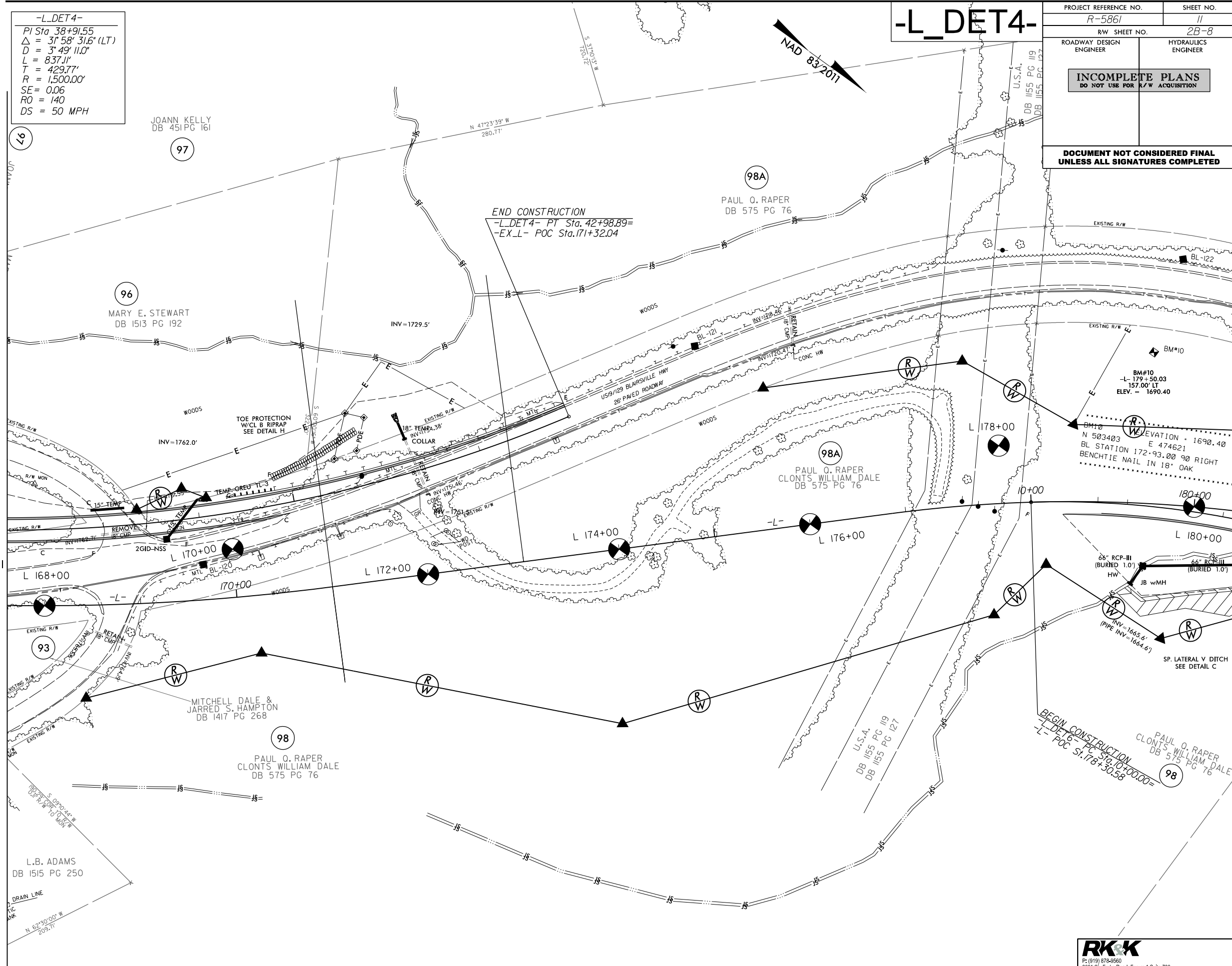
**-L\_DET4-**  
 PI Sta 38+91.55  
 $\Delta = 31^{\circ} 58' 31.6" (LT)$   
 $D = 3^{\circ} 49' 11.0"$   
 $L = 837.11'$   
 $T = 429.77'$   
 $R = 1500.00'$   
 $SE = 0.06$   
 $RO = 140$   
 $DS = 50 MPH$

# -L\_DET4-

PROJECT REFERENCE NO. R-5861	SHEET NO. 11
R/W SHEET NO. 2B-8	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	

**DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED**

MATCHLINE -LDET 4- STA. 37+00 SEE SHEET 10



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

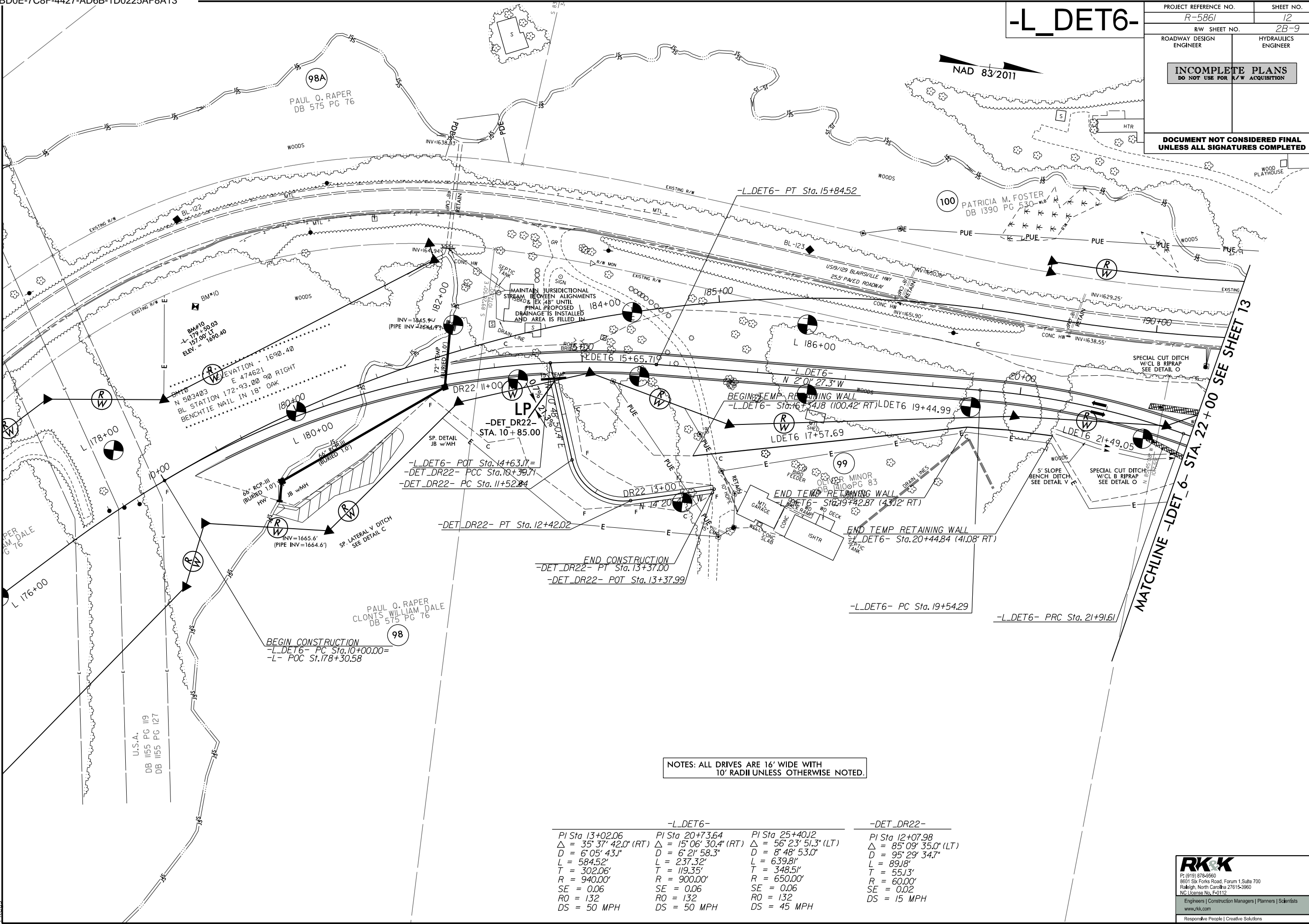
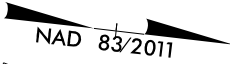
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# -L\_DET6-

PROJECT REFERENCE NO. R-586I	SHEET NO. 12
R/W SHEET NO. 2B-9	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

-L_DET6-			-DET_DR22-		
PI Sta 13+02.06	PI Sta 20+73.64	PI Sta 25+40.12	PI Sta 12+07.98		
$\Delta = 35^\circ 37' 42.0''$ (RT)	$\Delta = 15^\circ 06' 30.4''$ (RT)	$\Delta = 56^\circ 23' 51.3''$ (LT)	$\Delta = 85^\circ 09' 35.0''$ (LT)		
D = 6' 05' 43.1"	D = 6' 21' 58.3"	D = 8' 48' 53.0"	D = 95' 29' 34.7"		
L = 584.52'	L = 237.32'	L = 639.81'	L = 89.18'		
T = 302.06'	T = 119.35'	T = 348.51'	T = 55.13'		
R = 940.00'	R = 900.00'	R = 650.00'	R = 60.00'		
SE = 0.06	SE = 0.06	SE = 0.06	SE = 0.02		
RO = 132	RO = 132	RO = 132	DS = 15 MPH		
DS = 50 MPH	DS = 50 MPH	DS = 45 MPH			



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 8/17/09  
 PER M. DALE G 76  
 U.S.A. DB 1155 PG 119 DB 1155 PG 127  
 PAUL O. RAPER CLONTS WILLIAM DALE DB 575 PG 76  
 PATRICIA M. FOSTER DB 1390 PG 530  
 MATCHLINE -LDET\_6- STA. 22+00 SEE SHEET 13

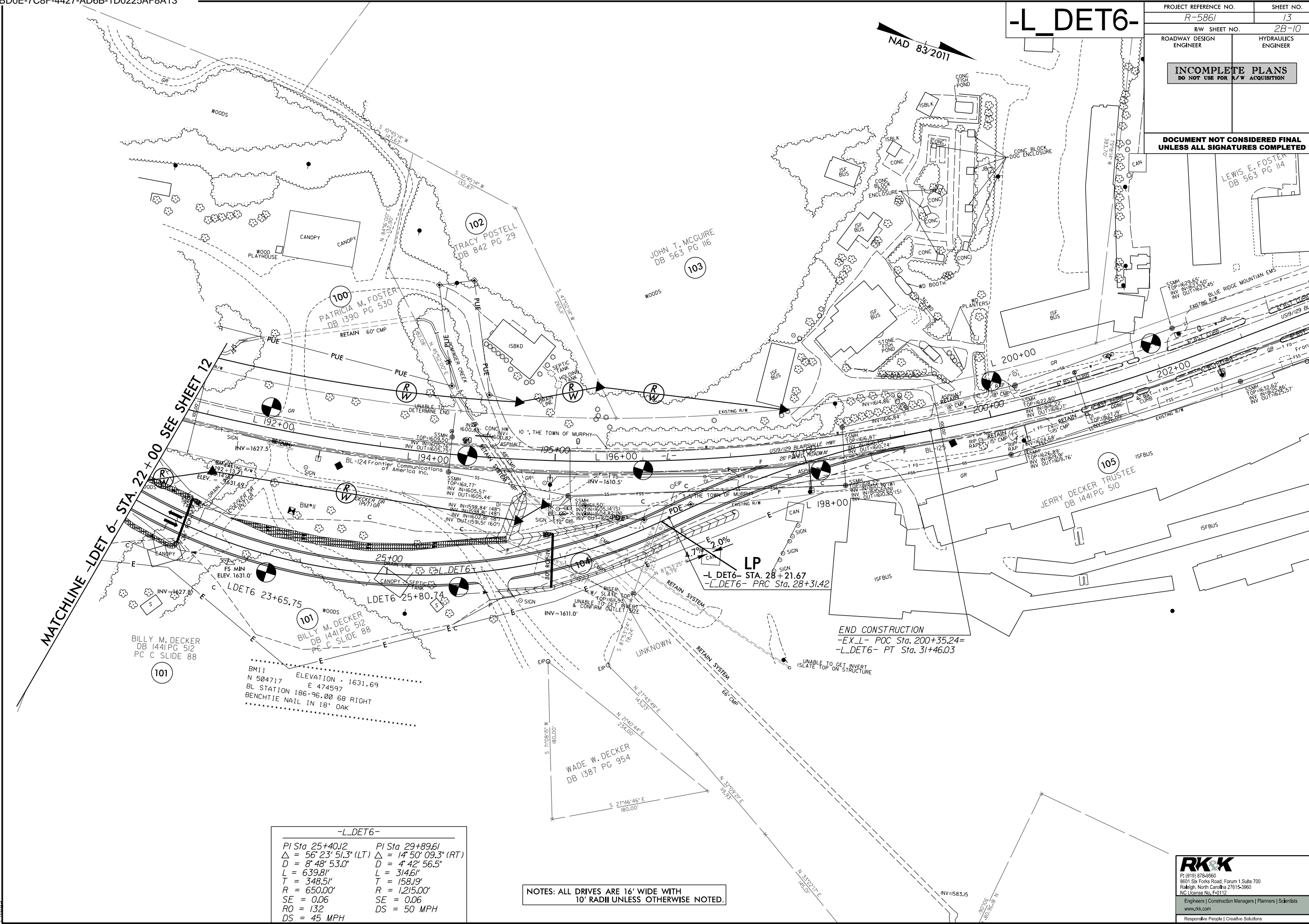
8/17/09

# -L\_DET6-

PROJECT REFERENCE NO. <i>R-5861</i>	SHEET NO. <i>13</i>
R/W SHEET NO. <i>2B-10</i>	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	

**DOCUMENT NOT CONSIDERED FINAL  
UNLESS ALL SIGNATURES COMPLETED**

LEWIS E. FOSTER  
DB 563 PG 14



MATCHLINE -LDET 6- STA. 22+00 SEE SHEET 12

-L_DET6-	
PI Sta 25+40.12	PI Sta 29+89.61
$\Delta = 56^{\circ} 23' 51.3" (LT)$	$\Delta = 14^{\circ} 50' 09.3" (RT)$
$D = 8' 48" 53.0"$	$D = 4' 42" 56.5"$
$L = 639.81'$	$L = 314.61'$
$T = 348.51'$	$T = 158.19'$
$R = 650.00'$	$R = 1,215.00'$
$SE = 0.06$	$SE = 0.06$
$RO = 132$	$DS = 50 MPH$
$DS = 45 MPH$	

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

END CONSTRUCTION  
 -EX\_L- POC Sta. 200+35.24=  
 -L\_DET6- PT Sta. 31+46.03

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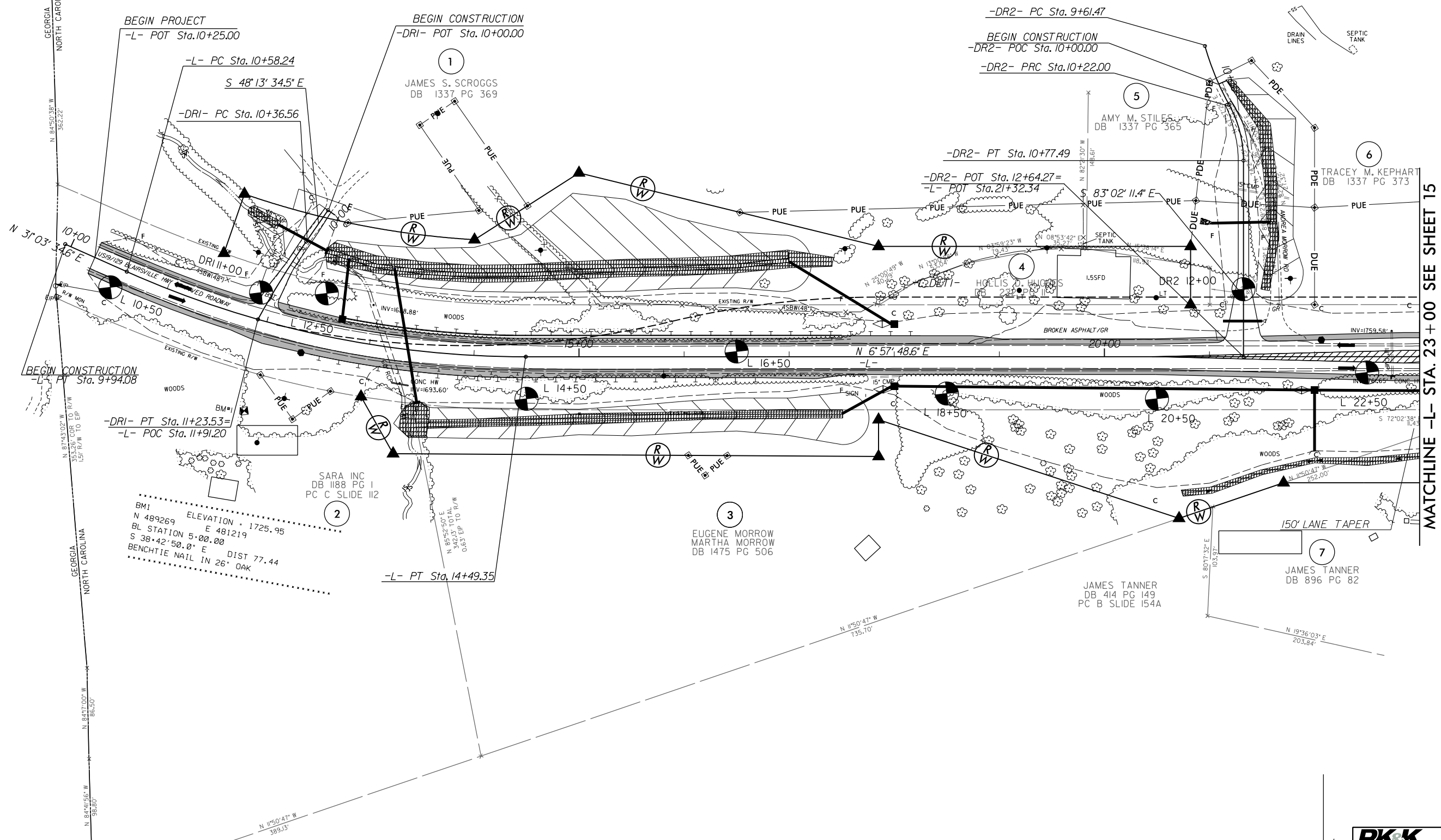


8/17/09

-L-	-DRI-	-DR2-	
PI Sta 12+56.73	PI Sta 10+80.09	PI Sta 9+91.87	PI Sta 10+50.35
$\Delta = 24^{\circ} 05' 46.1" (LT)$	$\Delta = 6^{\circ} 06' 49.5" (LT)$	$\Delta = 13^{\circ} 05' 15.7" (LT)$	$\Delta = 28^{\circ} 53' 59.0" (RT)$
D = 6' 09' 39.0"	D = 7' 01' 48.6"	D = 21' 37' 15.8"	D = 52' 05' 13.5"
L = 391.12'	L = 86.96'	L = 60.53'	L = 55.48'
T = 198.49'	T = 43.52'	T = 30.40'	T = 28.35'
R = 930.00'	R = 815.00'	R = 265.00'	R = 110.00'
SE = 0.06	SE = 0.02	SE = 0.02	SE = 0.02
RO = 150'	DS = 15 MPH	DS = 15 MPH	DS = 15 MPH

NAD 83/2011

PROJECT REFERENCE NO. R-5861	SHEET NO. 14
RW SHEET NO. 4	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



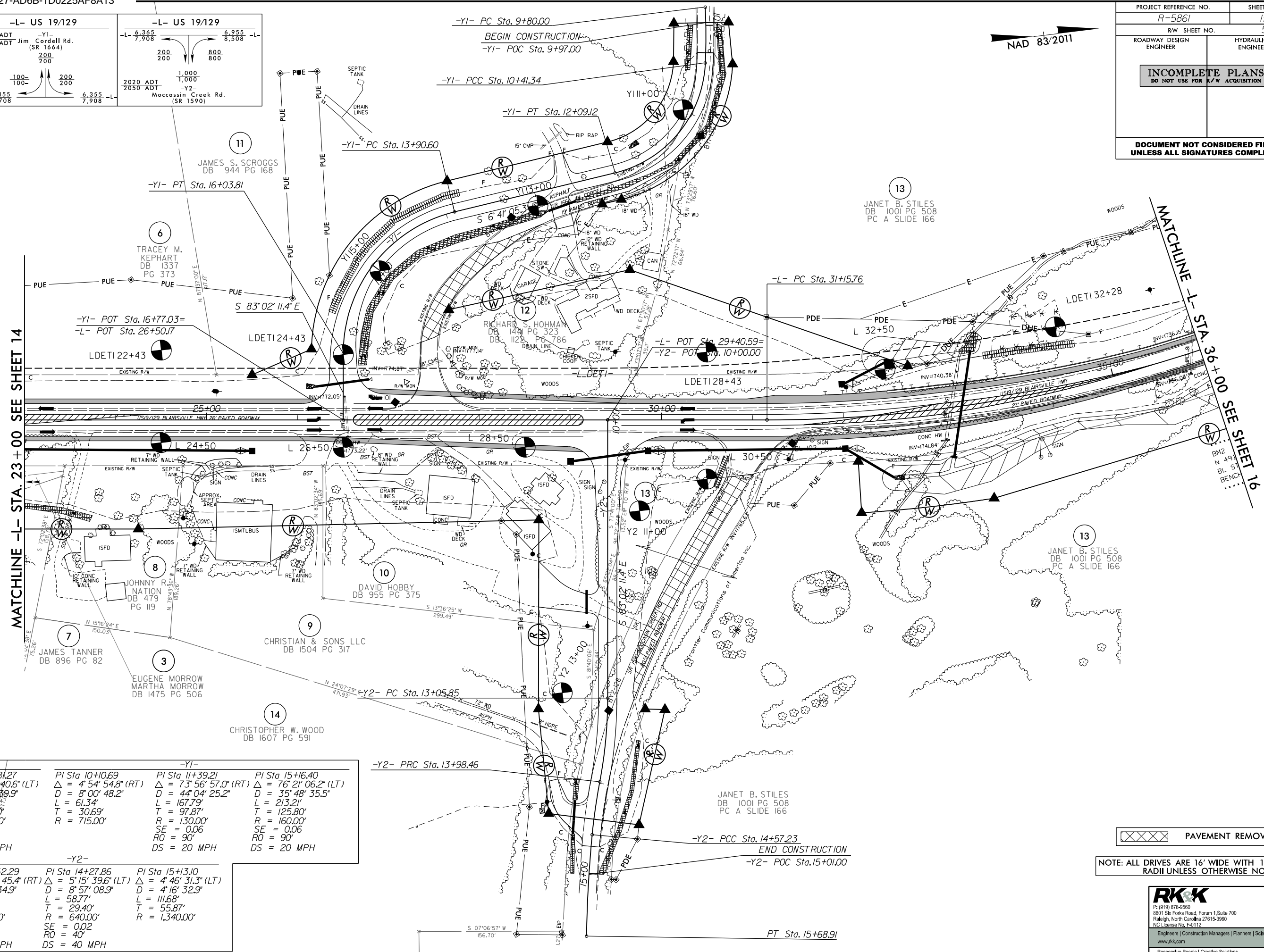
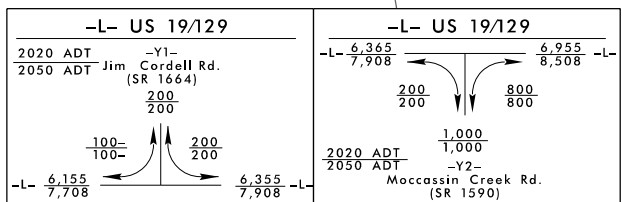
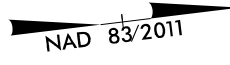
BM1  
N 489269 E 481219  
BL STATION 5+00.00  
S 38°42'50.0" E DIST 77.44  
BENCHTIE NAIL IN 26" OAK

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

2/26/2020  
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PROJECT REFERENCE NO. R-5861	SHEET NO. 15
R/W SHEET NO. 5	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



-L-		-Y1-	
PI Sta 33+81.27	PI Sta 10+10.69	PI Sta 11+39.21	PI Sta 15+16.40
$\Delta = 19^\circ 56' 40.6''$ (LT)	$\Delta = 4^\circ 54' 54.8''$ (RT)	$\Delta = 73^\circ 56' 57.0''$ (RT)	$\Delta = 76^\circ 21' 06.2''$ (LT)
D = 3' 47' 39.9"	D = 8' 00' 48.2"	D = 44' 04' 25.2"	D = 35' 48' 35.5"
L = 525.63'	L = 61.34'	L = 167.79'	L = 213.21'
T = 265.50'	T = 30.69'	T = 97.87'	T = 125.80'
R = 1,510.00'	R = 715.00'	R = 130.00'	R = 160.00'
SE = 0.06	SE = 0.06	SE = 0.06	SE = 0.06
RO = 210'	RO = 90'	RO = 90'	RO = 90'
DS = 60 MPH	DS = 20 MPH	DS = 20 MPH	DS = 20 MPH

-Y2-		
PI Sta 13+52.29	PI Sta 14+27.86	PI Sta 15+13.10
$\Delta = 10^\circ 49' 45.4''$ (RT)	$\Delta = 5^\circ 15' 39.6''$ (LT)	$\Delta = 4^\circ 46' 31.3''$ (LT)
D = 11' 41' 34.9"	D = 8' 57' 08.9"	D = 4' 16' 32.9"
L = 92.61'	L = 58.77'	L = 111.68'
T = 46.44'	T = 29.40'	T = 55.87'
R = 490.00'	R = 640.00'	R = 1,340.00'
SE = NC	SE = 0.02	
RO = 40'	RO = 40'	
DS = 40 MPH	DS = 40 MPH	

PAVEMENT REMOVAL

NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

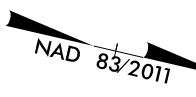
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8/17/09  
 2/26/2020  
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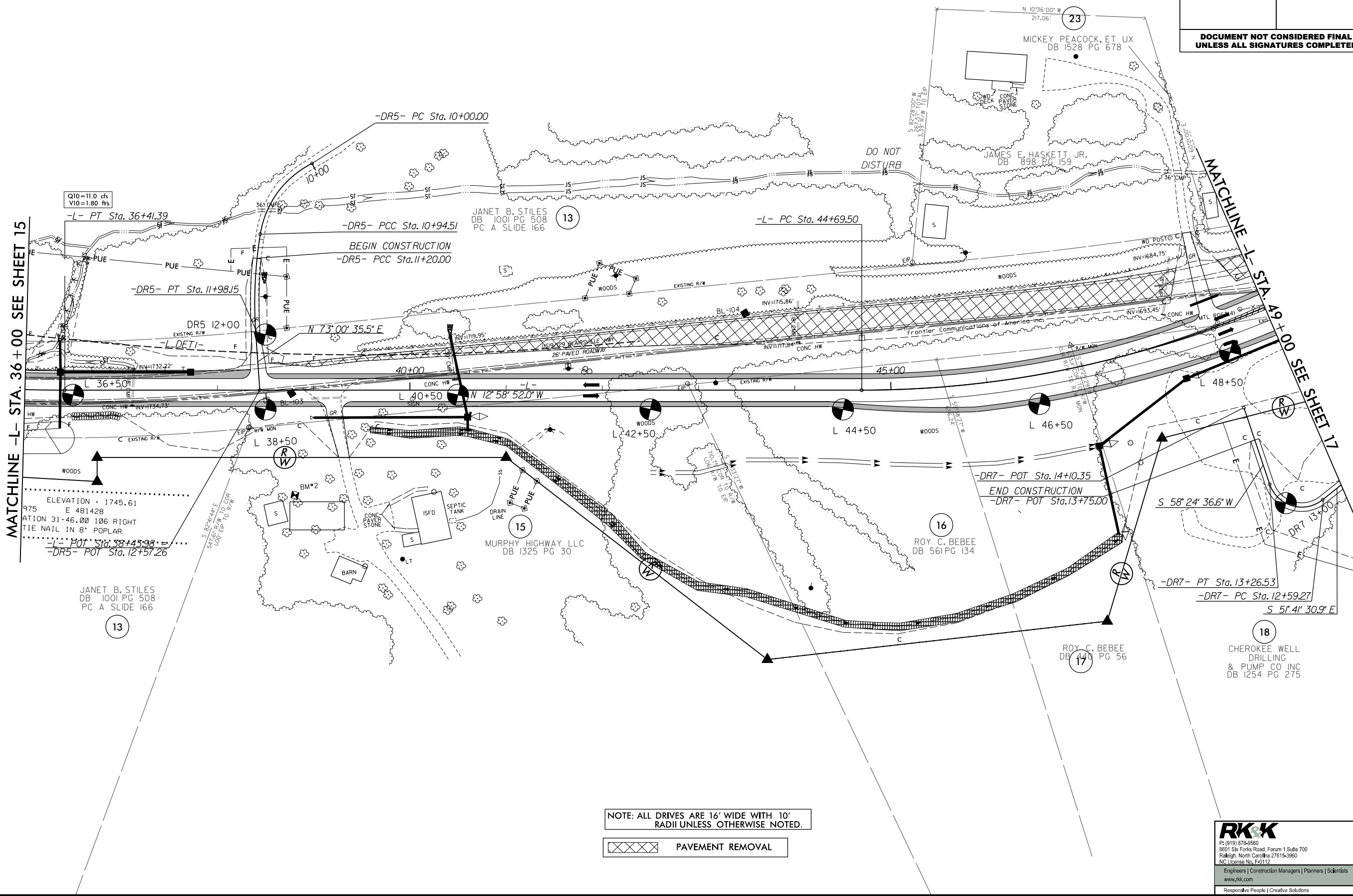


8/17/09

-L-		-DR5-		-DR7-	
PI Sta 33+81.27	PI Sta 50+66.87	PI Sta 10+51.11	PI Sta 11+46.56	PI Sta 13+09.35	
$\Delta = 19^\circ 56' 40.6" (LT)$	$\Delta = 58^\circ 48' 26.3" (LT)$	$\Delta = 54^\circ 08' 51.5" (LT)$	$\Delta = 13^\circ 11' 45.2" (LT)$	$\Delta = 110^\circ 06' 07.5" (RT)$	
$D = 3^\circ 47' 39.9"$	$D = 5^\circ 24' 18.9"$	$D = 57^\circ 17' 44.8"$	$D = 12^\circ 43' 56.6"$	$D = 163^\circ 42' 08.0"$	
$L = 525.63'$	$L = 1,087.96'$	$L = 94.51'$	$L = 103.64'$	$L = 67.26'$	
$T = 265.50'$	$T = 597.37'$	$T = 51.11'$	$T = 52.05'$	$T = 50.08'$	
$R = 1,510.00'$	$R = 1,060.00'$	$R = 100.00'$	$R = 450.00'$	$R = 35.00'$	
$SE = 0.06$	$SE = 0.06$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$	
$RO = 210^\circ$	$RO = 195^\circ$	$DS = 15 \text{ MPH}$	$DS = 15 \text{ MPH}$	$DS = 15 \text{ MPH}$	



PROJECT REFERENCE NO. R-5861	SHEET NO. 16
R/W SHEET NO. 6	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



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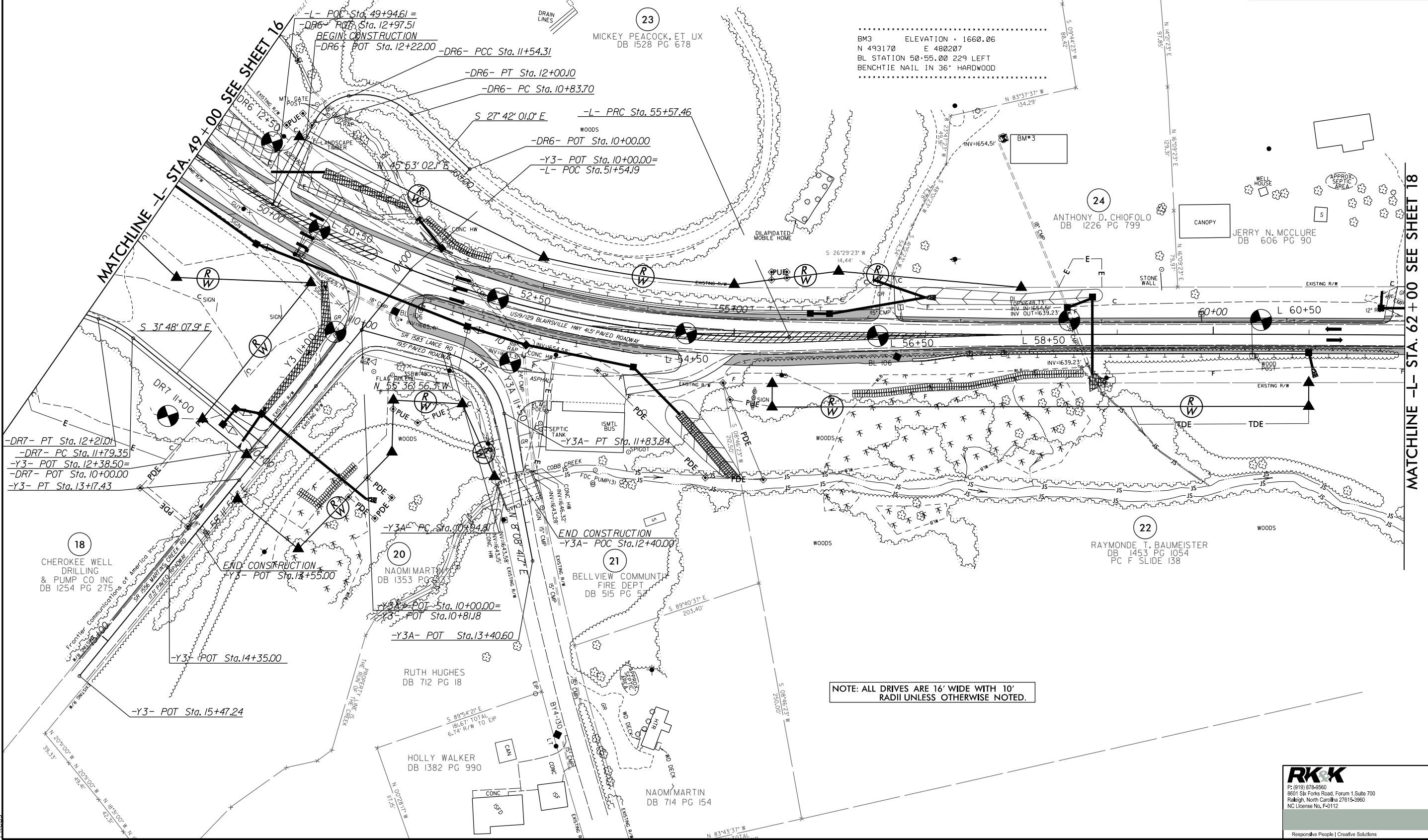
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2/26/2020  
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-L-		-Y3A-		-DR6-		-DR7-	
PI Sta 50+66.87	PI Sta 59+39.36	PI Sta 11+44.57	PI Sta 11+21.86	PI Sta 11+78.95	PI Sta 12+00.39		
$\Delta = 58^\circ 48' 26.3" (LT)$	$\Delta = 1^\circ 27' 31.2" (RT)$	$\Delta = 63^\circ 45' 38.0" (RT)$	$\Delta = 53^\circ 56' 30.0" (LT)$	$\Delta = 52^\circ 28' 26.9" (LT)$	$\Delta = 19^\circ 53' 23.0" (LT)$		
D = 5' 24' 18.9"	D = 0' 11' 27.5"	D = 71' 37' 11.0"	D = 76' 23' 39.7"	D = 114' 35' 29.6"	D = 47' 44' 47.3"		
L = 1,087.96'	L = 763.75'	L = 89.03'	L = 70.61'	L = 45.79'	L = 41.66'		
T = 597.37'	T = 381.90'	T = 49.76'	T = 38.17'	T = 24.64'	T = 21.04'		
R = 1,060.00'	R = 30,000.00'	R = 80.00'	R = 75.00'	R = 50.00'	R = 120.00'		
SE = 0.06	SE = 0.02	SE = 0.06	SE = 0.02	SE = 0.02	SE = 0.02		
RO = 195'	RO = 70'	RO = 90'	RO = 15 MPH	RO = 15 MPH	RO = 15 MPH		
DS = 55 MPH	DS = 60 MPH	DS = 15 MPH					

DESIGN EXCEPTION  
REQUIRED FOR  
MINIMUM HORIZONTAL  
CURVE RADIUS.

PROJECT REFERENCE NO. R-5861	SHEET NO. 17
R/W SHEET NO. 7	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



MATCHLINE -L- STA. 49+00 SEE SHEET 16

MATCHLINE -L- STA. 62+00 SEE SHEET 18

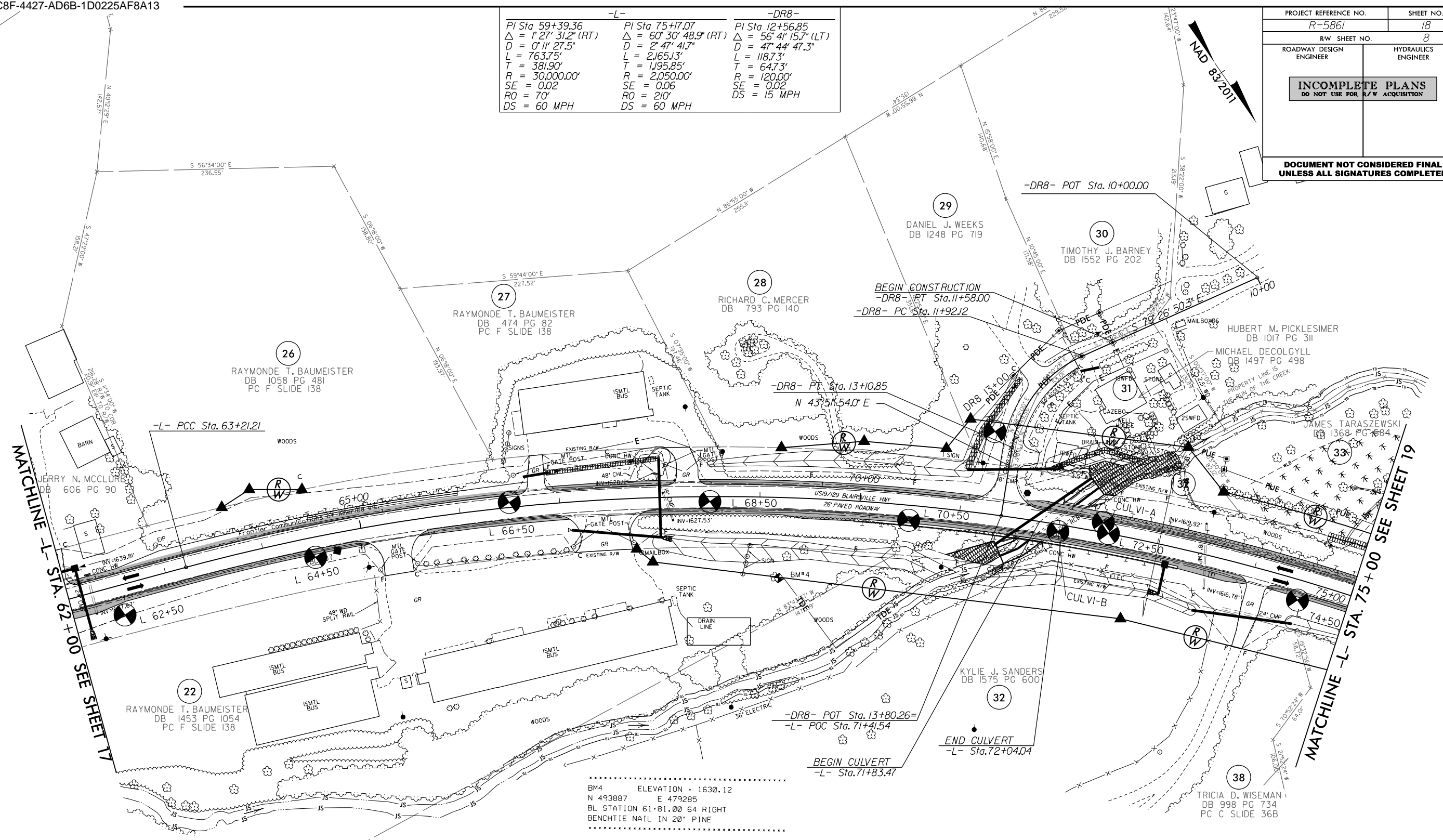
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-L-		-DR8-	
PI Sta 59+39.36	PI Sta 75+17.07	PI Sta 12+56.85	
$\Delta = 1^{\circ}27'31.2''$ (RT)	$\Delta = 60^{\circ}30'48.9''$ (RT)	$\Delta = 56^{\circ}41'15.7''$ (LT)	
D = 0'11'27.5"	D = 2'47'41.7"	D = 47'44'47.3"	
L = 763.75'	L = 2,165.13'	L = 118.73'	
T = 381.90'	T = 1,195.85'	T = 64.73'	
R = 30,000.00'	R = 2,050.00'	R = 120.00'	
SE = 0.02	SE = 0.06	SE = 0.02	
RO = 70'	RO = 210'	DS = 15 MPH	
DS = 60 MPH	DS = 60 MPH		

PROJECT REFERENCE NO. R-5861	SHEET NO. 18
R/W SHEET NO. 8	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



.....  
 BM4 ELEVATION = 1630.12  
 N 493887 E 479285  
 BL STATION 61+81.00 64 RIGHT  
 BENCHTIE NAIL IN 20' PINE  
 .....

CULVERT #1  
TWO BARRELS

	NORTH	EAST	ELEV.
CUL1	493988.22	479006.62	1618.40
CUL2	493995.76	478999.21	1618.39
CUL3	493996.70	478998.62	1618.33
CUL4	494003.99	478990.66	1618.43
CE1	493994.78	479000.15	1626.44
HW1	494000.61	478995.60	1628.15
CUL5	493990.38	479066.33	1618.45
CUL6	493998.30	479058.53	1618.40
CUL7	493999.27	479057.78	1618.37
CUL8	494005.81	479049.69	1618.54
CE2	493999.96	479055.77	1626.49
HW2	493997.29	479057.40	1628.27

NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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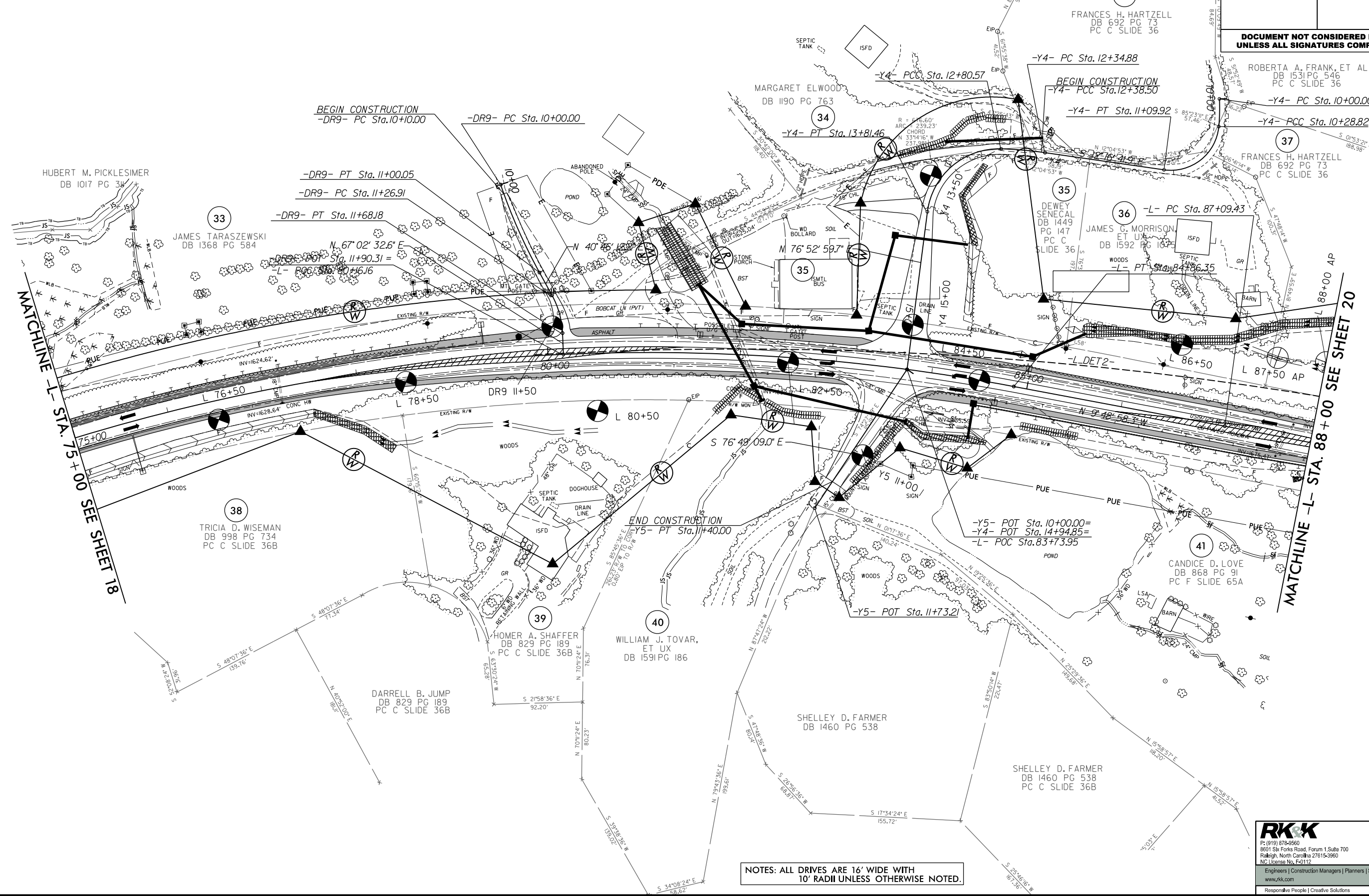


8/17/09

-DR9-		-L-		-Y4-			
PI Sta 10+50.15	PI Sta 11+47.91	PI Sta 75+17.07	PI Sta 90+43.98	PI Sta 10+14.44	PI Sta 10+81.45	PI Sta 12+57.81	PI Sta 13+48.53
$\Delta = 9^{\circ} 53' 01.0" (LT)$	$\Delta = 26^{\circ} 16' 20.4" (RT)$	$\Delta = 60^{\circ} 30' 48.9" (RT)$	$\Delta = 2^{\circ} 47' 40.83" (RT)$	$\Delta = 7^{\circ} 51' 52.2" (RT)$	$\Delta = 92^{\circ} 55' 38.0" (RT)$	$\Delta = 6^{\circ} 28' 50.8" (LT)$	$\Delta = 84^{\circ} 21' 27.6" (LT)$
$D = 9^{\circ} 52' 42.9"$	$D = 63^{\circ} 39' 43.1"$	$D = 2^{\circ} 47' 41.7"$	$D = 0^{\circ} 25' 03.9"$	$D = 27^{\circ} 17' 01.3"$	$D = 114^{\circ} 35' 29.6"$	$D = 14^{\circ} 10' 59.9"$	$D = 83^{\circ} 37' 14.3"$
$L = 100.05'$	$L = 41.27'$	$L = 2,165.13'$	$L = 668.97'$	$L = 28.82'$	$L = 81.09'$	$L = 45.69'$	$L = 100.88'$
$T = 50.15'$	$T = 21.00'$	$T = 1,195.85'$	$T = 334.55'$	$T = 14.44'$	$T = 52.62'$	$T = 22.93'$	$T = 67.96'$
$R = 580.00'$	$R = 90.00'$	$R = 2,050.00'$	$R = 13,715.00'$	$R = 210.00'$	$R = 50.00'$	$R = 405.00'$	$R = 75.00'$
$SE = 0.02$	$SE = 0.02$	$SE = 0.06$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$
$DS = 15 MPH$	$DS = 15 MPH$	$RO = 210'$	$RO = 70'$	$DS = 15 MPH$	$DS = 15 MPH$	$RO = 30'$	$RO = 30'$



PROJECT REFERENCE NO. R-5861	SHEET NO. 19
R/W SHEET NO. 9	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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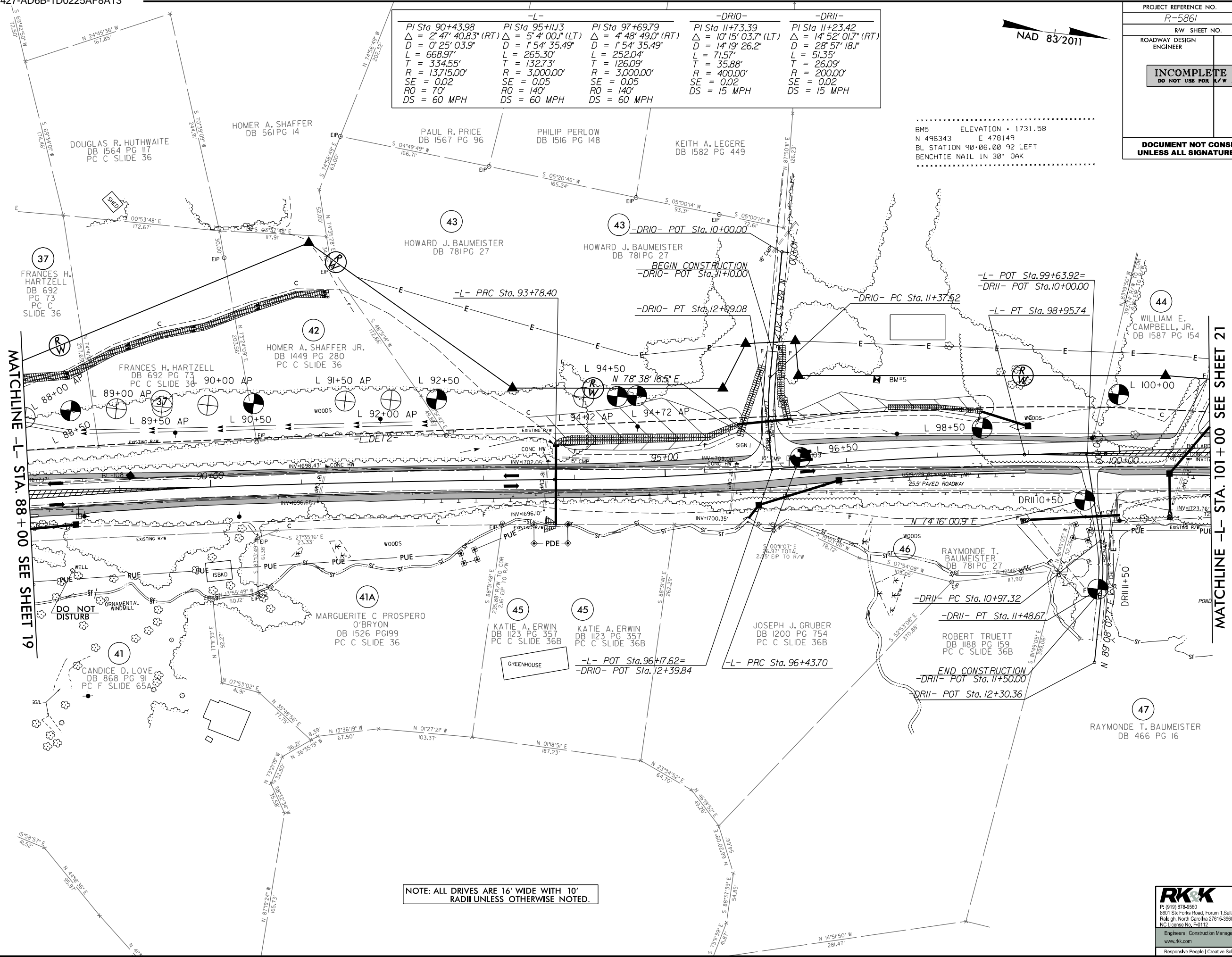
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 R5861

PROJECT REFERENCE NO. R-5861		SHEET NO. 20	
RW SHEET NO. 10		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION			
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED			

-L-			-DRIO-		-DRII-	
PI Sta 90+43.98	PI Sta 95+111.3	PI Sta 97+69.79	PI Sta 11+73.39	PI Sta 11+23.42	PI Sta 11+23.42	PI Sta 11+23.42
$\Delta = 2' 47" 40.83" (RT)$	$\Delta = 5' 4" 00.1" (LT)$	$\Delta = 4' 48" 49.0" (RT)$	$\Delta = 10' 15" 03.7" (LT)$	$\Delta = 14' 52" 01.7" (RT)$	$\Delta = 14' 52" 01.7" (RT)$	$\Delta = 14' 52" 01.7" (RT)$
D = 0' 25' 03.9"	D = 1' 54' 35.49"	D = 1' 54' 35.49"	D = 14' 19' 26.2"	D = 28' 57' 18.1"	D = 28' 57' 18.1"	D = 28' 57' 18.1"
L = 668.97'	L = 265.30'	L = 252.04'	L = 71.57'	L = 51.35'	L = 51.35'	L = 51.35'
T = 334.55'	T = 132.73'	T = 126.09'	T = 35.88'	T = 26.09'	T = 26.09'	T = 26.09'
R = 13,715.00'	R = 3,000.00'	R = 3,000.00'	R = 400.00'	R = 200.00'	R = 200.00'	R = 200.00'
SE = 0.02	SE = 0.05	SE = 0.05	SE = 0.02	SE = 0.02	SE = 0.02	SE = 0.02
RO = 70'	RO = 140'	RO = 140'	DS = 15 MPH	DS = 15 MPH	DS = 15 MPH	DS = 15 MPH
DS = 60 MPH	DS = 60 MPH	DS = 60 MPH				

NAD 83/2011

.....  
 BMS ELEVATION + 1731.58  
 N 496343 E 478149  
 BL STATION 90+06.00 92 LEFT  
 BENCHMARK NAIL IN 30" OAK  
 .....



MATCHLINE -L- STA. 88 + 00 SEE SHEET 19

MATCHLINE -L- STA. 101 + 00 SEE SHEET 21

NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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<p>PI Sta 11+20.71  <math>\Delta = 0' 38" 52.86"</math> (LT)  <math>D = 0' 15" 37.57"</math>  <math>L = 248.82'</math>  <math>T = 124.41'</math>  <math>R = 22,000.00'</math>  <math>SE = NC</math>  <math>RO = 70'</math>  <math>DS = 60</math> MPH</p>	<p>PI Sta 13+60.37  <math>\Delta = 8' 00" 06.6"</math> (LT)  <math>D = 39' 30" 51.6"</math>  <math>L = 204.99'</math>  <math>T = 123.85'</math>  <math>R = 145.00'</math>  <math>SE = 0.06</math>  <math>RO = 100'</math>  <math>DS = 25</math> MPH</p>	<p>PI Sta 16+47.26  <math>\Delta = 66' 29" 36.7"</math> (RT)  <math>D = 67' 24" 24.5"</math>  <math>L = 98.65'</math>  <math>T = 55.72'</math>  <math>R = 85.00'</math>  <math>SE = 0.05</math>  <math>RO = 75'</math>  <math>DS = 20</math> MPH</p>
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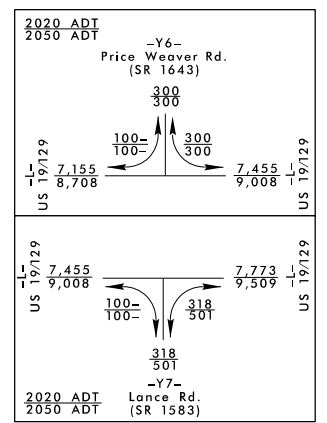
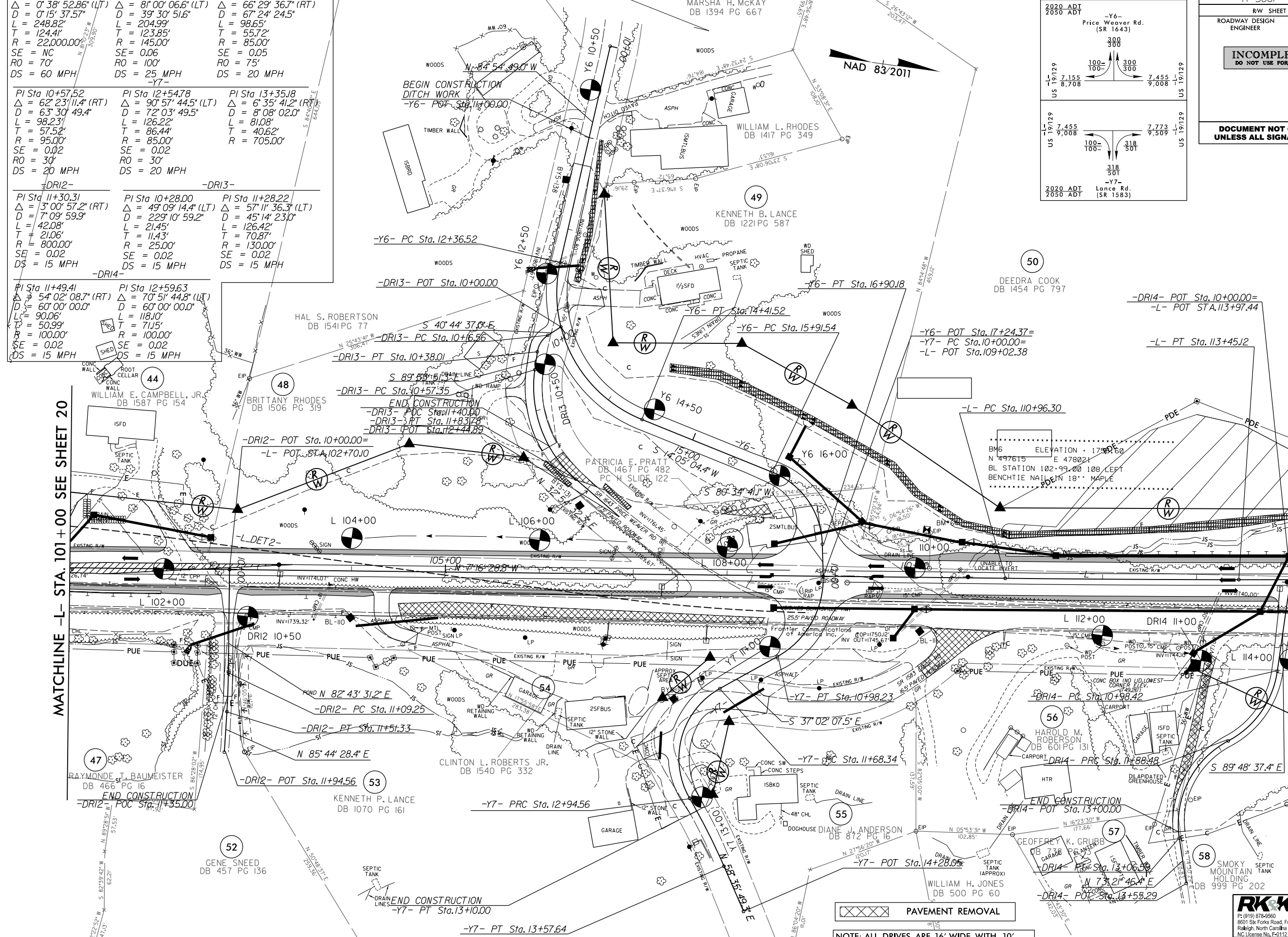
<p>PI Sta 10+57.52  <math>\Delta = 62' 23" 11.4"</math> (RT)  <math>D = 63' 30" 49.4"</math>  <math>L = 98.23'</math>  <math>T = 57.52'</math>  <math>R = 95.00'</math>  <math>SE = 0.02</math>  <math>RO = 30'</math>  <math>DS = 20</math> MPH</p>	<p>PI Sta 12+54.78  <math>\Delta = 90' 57" 44.5"</math> (LT)  <math>D = 72' 03" 49.5"</math>  <math>L = 126.22'</math>  <math>T = 86.44'</math>  <math>R = 85.00'</math>  <math>SE = 0.02</math>  <math>RO = 30'</math>  <math>DS = 20</math> MPH</p>	<p>PI Sta 13+35.18  <math>\Delta = 6' 35" 41.2"</math> (RT)  <math>D = 8' 08" 02.0"</math>  <math>L = 81.08'</math>  <math>T = 40.62'</math>  <math>R = 705.00'</math>  <math>SE = 0.02</math>  <math>RO = 75'</math>  <math>DS = 20</math> MPH</p>
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<p>PI Sta 11+30.31  <math>\Delta = 3' 00" 57.2"</math> (RT)  <math>D = 7' 09" 59.9"</math>  <math>L = 42.08'</math>  <math>T = 21.06'</math>  <math>R = 800.00'</math>  <math>SE = 0.02</math>  <math>DS = 15</math> MPH</p>	<p>PI Sta 10+28.00  <math>\Delta = 49' 09" 14.4"</math> (LT)  <math>D = 229' 10" 59.2"</math>  <math>L = 21.45'</math>  <math>T = 11.43'</math>  <math>R = 25.00'</math>  <math>SE = 0.02</math>  <math>DS = 15</math> MPH</p>	<p>PI Sta 11+28.22  <math>\Delta = 57' 11" 36.3"</math> (LT)  <math>D = 45' 14" 23.0"</math>  <math>L = 126.42'</math>  <math>T = 70.87'</math>  <math>R = 130.00'</math>  <math>SE = 0.02</math>  <math>DS = 15</math> MPH</p>
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<p>PI Sta 11+49.41  <math>\Delta = 54' 02" 08.7"</math> (RT)  <math>D = 60' 00" 00.0"</math>  <math>L = 90.06'</math>  <math>T = 50.99'</math>  <math>R = 100.00'</math>  <math>SE = 0.02</math>  <math>DS = 15</math> MPH</p>	<p>PI Sta 12+59.63  <math>\Delta = 70' 51" 44.8"</math> (LT)  <math>D = 60' 00" 00.0"</math>  <math>L = 118.10'</math>  <math>T = 71.15'</math>  <math>R = 100.00'</math>  <math>SE = 0.02</math>  <math>DS = 15</math> MPH</p>
--	---

MATCHLINE -L- STA. 101+00 SEE SHEET 20

MATCHLINE -L- STA. 114+00 SEE SHEET 22



PROJECT REFERENCE NO. R-5861	SHEET NO. 21
R/W SHEET NO. II	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

**INCOMPLETE PLANS**  
DO NOT USE FOR R/W ACQUISITION

**DOCUMENT NOT CONSIDERED FINAL**  
UNLESS ALL SIGNATURES COMPLETED

XXXXX PAVEMENT REMOVAL

NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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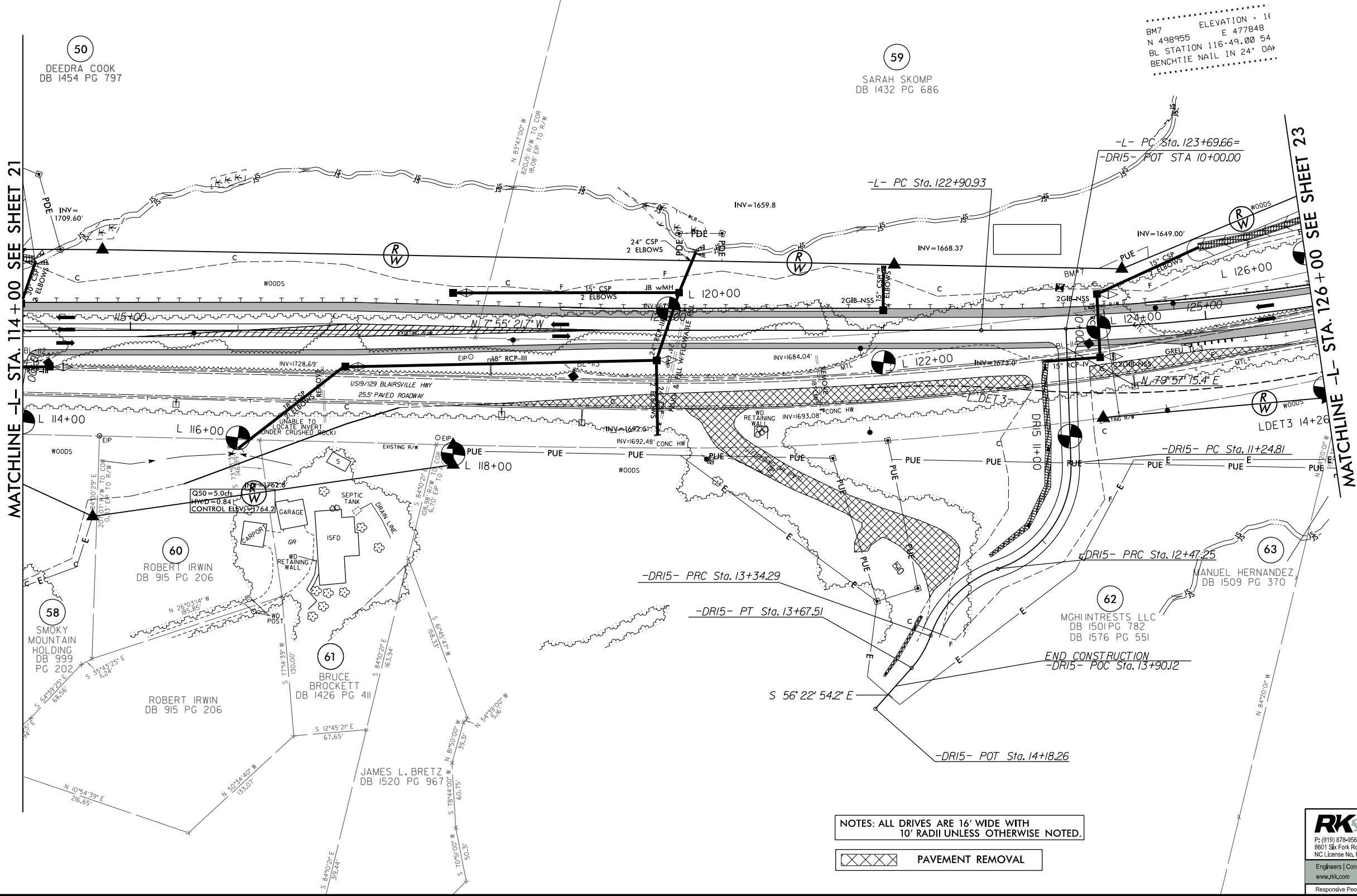
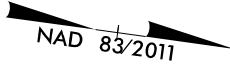
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 2/26/2020  
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8/17/09

-L-		-DRI5-	
PI Sta 127+30.02	PI Sta 11+99.43	PI Sta 12+96.26	PI Sta 13+52.13
$\Delta = 23^{\circ} 20' 58.3" (LT)$	$\Delta = 73^{\circ} 27' 47.3" (RT)$	$\Delta = 52^{\circ} 13' 28.3" (LT)$	$\Delta = 22^{\circ} 25' 31.3" (RT)$
D = 2' 41' 46.6"	D = 60' 00' 00.0"	D = 60' 00' 00.0"	D = 67' 29' 52.7"
L = 865.99'	L = 122.44'	L = 87.04'	L = 33.22'
T = 439.09'	T = 74.62'	T = 49.02'	T = 17.84'
R = 2125.00'	R = 100.00'	R = 100.00'	R = 90.00'
SE = 0.06	SE = 0.02	SE = 0.02	SE = 0.02
RO = 165'	DS = 15 MPH	DS = 15 MPH	DS = 15 MPH

PROJECT REFERENCE NO. R-5861	SHEET NO. 22
RW SHEET NO. 12	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



ELEVATION + 1ft  
 BM7 N 498955 E 477848  
 BL STATION 116+49.00 54  
 BENCHTIE NAIL IN 24" OAH

MATCHLINE -L- STA. 114+00 SEE SHEET 21

MATCHLINE -L- STA. 126+00 SEE SHEET 23

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

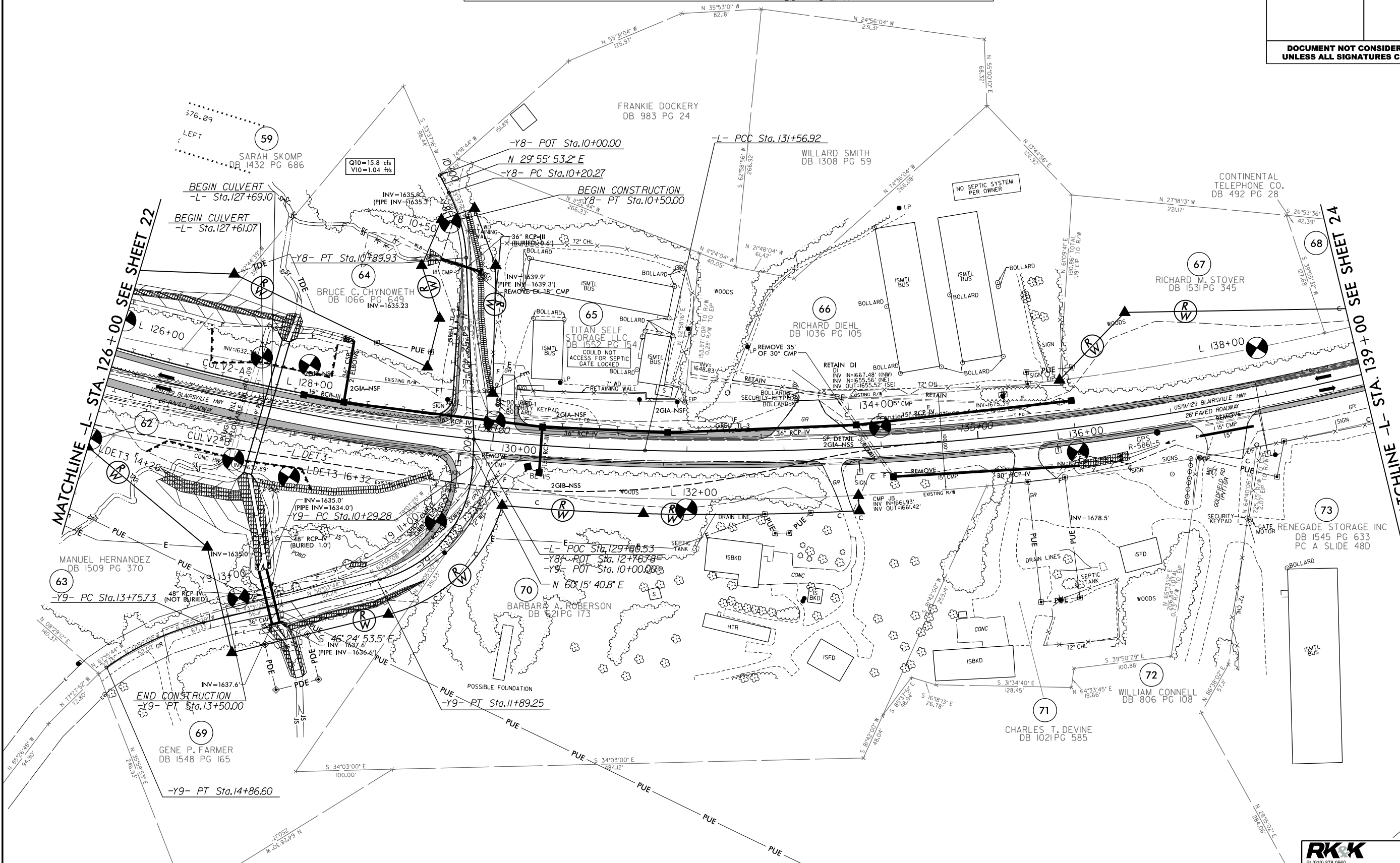
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PROJECT REFERENCE NO. R-5861		SHEET NO. 23	
RW SHEET NO. 13		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION			
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED			

-L-	-Y8-	-Y9-
PI Sta 127+30.02 $\Delta = 23^\circ 20' 58.3" (LT)$ $D = 2' 41' 46.6"$ $L = 865.99'$ $R = 439.09'$ $SE = 0.06$ $DS = 60 MPH$	PI Sta 135+82.23 $\Delta = 16^\circ 58' 31.5" (LT)$ $D = 2' 00' 37.4"$ $L = 844.39'$ $R = 425.31'$ $SE = 0.05$ $DS = 60 MPH$	PI Sta 10+55.66 $\Delta = 24^\circ 56' 46.9" (RT)$ $D = 35' 48' 35.5"$ $L = 696.6'$ $R = 35.39'$ $SE = 0.03$ $RO = 45'$ $DS = 15 MPH$
PI Sta 11+22.32 $\Delta = 73^\circ 19' 25.7" (RT)$ $D = 45' 50' 11.8"$ $L = 159.97'$ $R = 125.00'$ $SE = 0.05$ $RO = 75'$ $DS = 15 MPH$	PI Sta 14+31.88 $\Delta = 22^\circ 17' 24.8" (LT)$ $D = 20' 06' 13.6"$ $L = 110.88'$ $R = 285.00'$	



NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

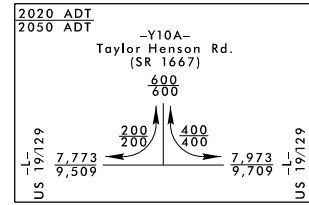
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 k.e.k.



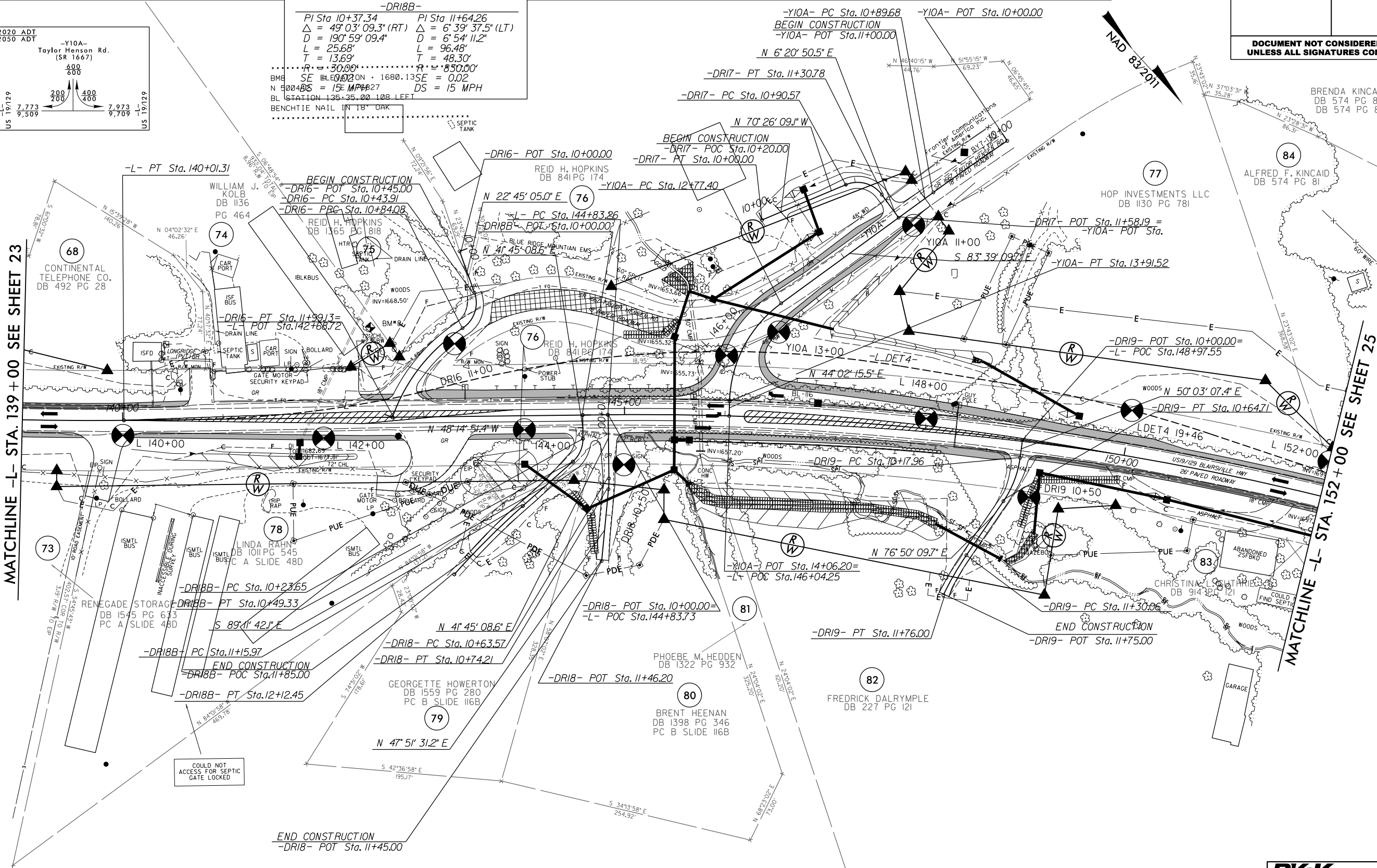
PROJECT REFERENCE NO. R-5861		SHEET NO. 24	
RW SHEET NO. 14		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION			
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED			

PI Sta 135+82.23 $\Delta = 16' 58" 31.5" (LT)$ $D = 2' 00" 37.4"$ $L = 844.39'$ $T = 425.31'$ $R = 2,850.00'$ $SE = 0.05$ $DS = 60 MPH$	PI Sta 151+02.43 $\Delta = 24' 25" 52.3" (RT)$ $D = 2' 00" 12.1"$ $L = 1,219.52'$ $T = 619.17'$ $R = 2,869.00'$ $SE = 0.05$ $DS = 60 MPH$	PI Sta 10+44.85 $\Delta = 2' 20" 08.2" (LT)$ $D = 2' 36" 15.7"$ $L = 89.68'$ $T = 44.85'$ $R = 2,200.00'$	PI Sta 13+38.78 $\Delta = 52' 18" 34.8" (LT)$ $D = 45' 50" 11.8"$ $L = 114.12'$ $T = 61.39'$ $R = 125.00'$ $SE = 0.03$ $DS = 20 MPH$	PI Sta 10+67.65 $\Delta = 76' 43" 07.2" (RT)$ $D = 190' 59" 09.4"$ $L = 40.17'$ $T = 23.74'$ $R = 30.00'$ $SE = 0.02$ $DS = 15 MPH$	PI Sta 11+43.77 $\Delta = 37' 40" 05.5" (LT)$ $D = 32' 44" 25.6"$ $L = 115.05'$ $T = 59.69'$ $R = 175.00'$ $SE = 0.02$ $DS = 15 MPH$	PI Sta 11+44.34 $\Delta = 76' 46" 59.6" (RT)$ $D = 190' 59" 09.4"$ $L = 40.20'$ $T = 23.77'$ $R = 30.00'$ $SE = 0.02$ $DS = 15 MPH$	PI Sta 10+68.89 $\Delta = 6' 05" 49.0" (RT)$ $D = 57' 17" 44.8"$ $L = 10.64'$ $T = 5.33'$ $R = 100.00'$ $SE = 0.02$ $DS = 15 MPH$	PI Sta 10+41.77 $\Delta = 26' 47" 02.3" (RT)$ $D = 57' 17" 44.8"$ $L = 46.75'$ $T = 23.81'$ $R = 100.00'$ $SE = 0.02$ $DS = 15 MPH$	PI Sta 11+53.07 $\Delta = 8' 46" 24.5" (LT)$ $D = 19' 05" 54.9"$ $L = 45.94'$ $T = 23.01'$ $R = 300.00'$ $SE = 0.02$ $DS = 15 MPH$
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MATCHLINE -L- STA. 139+00 SEE SHEET 23

MATCHLINE -L- STA. 152+00 SEE SHEET 25



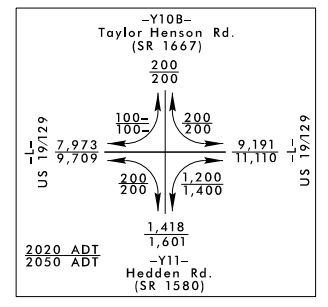
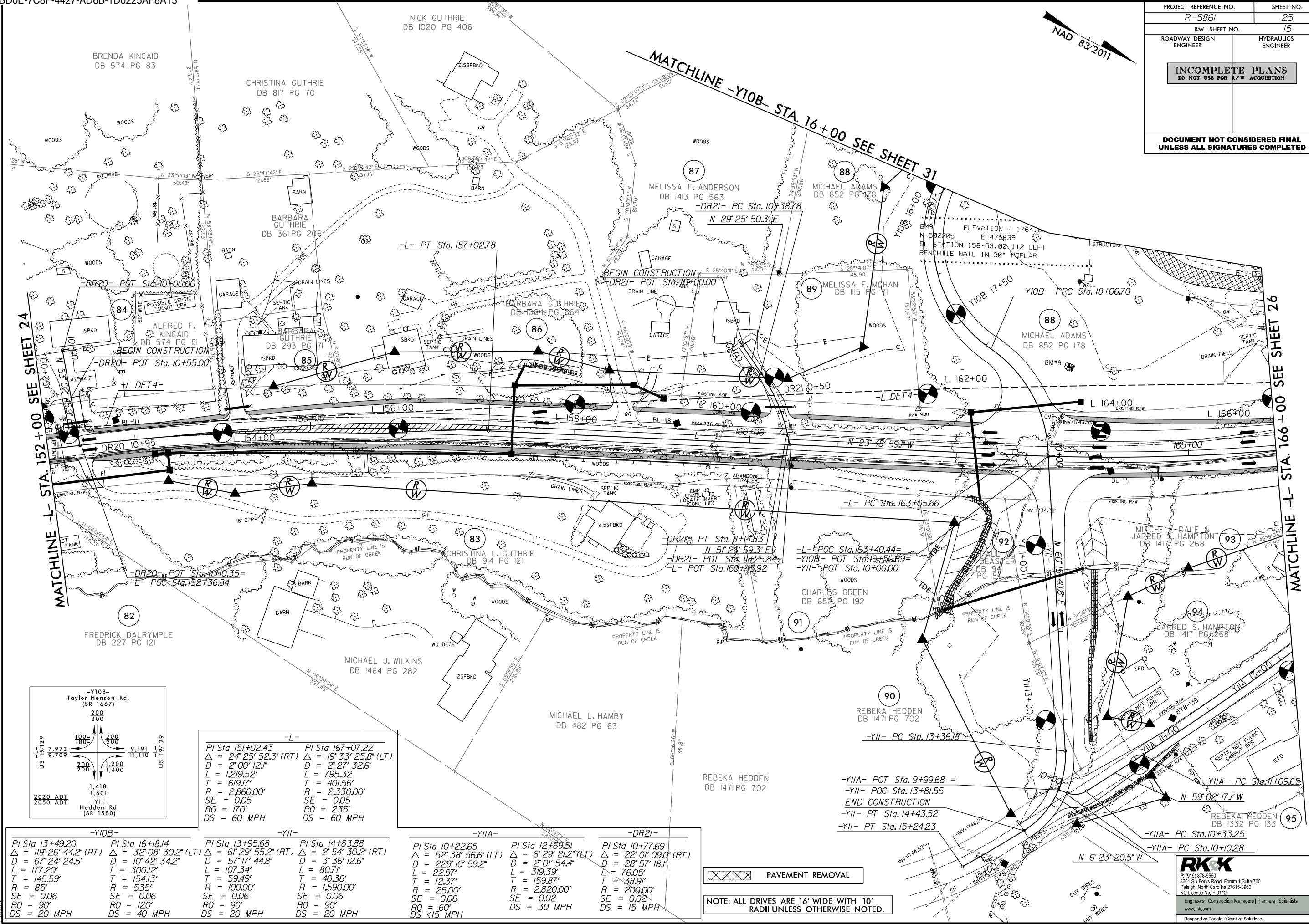
PAVEMENT REMOVAL  
 NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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 kkeis



PROJECT REFERENCE NO. R-5861		SHEET NO. 25	
RW SHEET NO. 15		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION			
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED			



-L-	
PI Sta 151+02.43 Δ = 24° 25' 52.3" (RT) D = 2' 00" 12.1" L = 1,219.52' T = 619.17' R = 2,860.00' SE = 0.05 RO = 170' DS = 60 MPH	PI Sta 167+07.22 Δ = 19° 33' 25.8" (LT) D = 2' 27' 32.6" L = 795.32' T = 401.56' R = 2,330.00' SE = 0.05 RO = 235' DS = 60 MPH

-Y10B-	
PI Sta 13+49.20 Δ = 119° 26' 44.2" (RT) D = 67° 24' 24.5" L = 177.20' T = 145.59' R = 85' SE = 0.06 RO = 90' DS = 20 MPH	PI Sta 16+18.14 Δ = 32° 08' 30.2" (LT) D = 10° 42' 34.2" L = 300.12' T = 154.13' R = 535' SE = 0.06 RO = 120' DS = 40 MPH

-Y11-	
PI Sta 13+95.68 Δ = 61° 29' 55.2" (RT) D = 57° 17' 44.8" L = 107.34' T = 59.49' R = 100.00' SE = 0.06 RO = 90' DS = 20 MPH	PI Sta 14+83.88 Δ = 2° 54' 30.2" (RT) D = 3° 36' 12.6" L = 80.71' T = 40.36' R = 1,590.00' SE = 0.06 RO = 90' DS = 20 MPH

-Y11A-	
PI Sta 10+22.65 Δ = 52° 38' 56.6" (LT) D = 22° 10' 59.2" L = 22.97' T = 12.37' R = 25.00' SE = 0.06 RO = 60' DS <15 MPH	PI Sta 12+69.51 Δ = 6° 29' 21.2" (LT) D = 2° 01' 54.4" L = 319.39' T = 159.87' R = 2,820.00' SE = 0.02 DS = 30 MPH

-DR21-	
PI Sta 10+77.69 Δ = 22° 01' 09.0" (RT) D = 28° 57' 18.1" L = 76.05' T = 38.91' R = 200.00' SE = 0.02 DS = 15 MPH	



NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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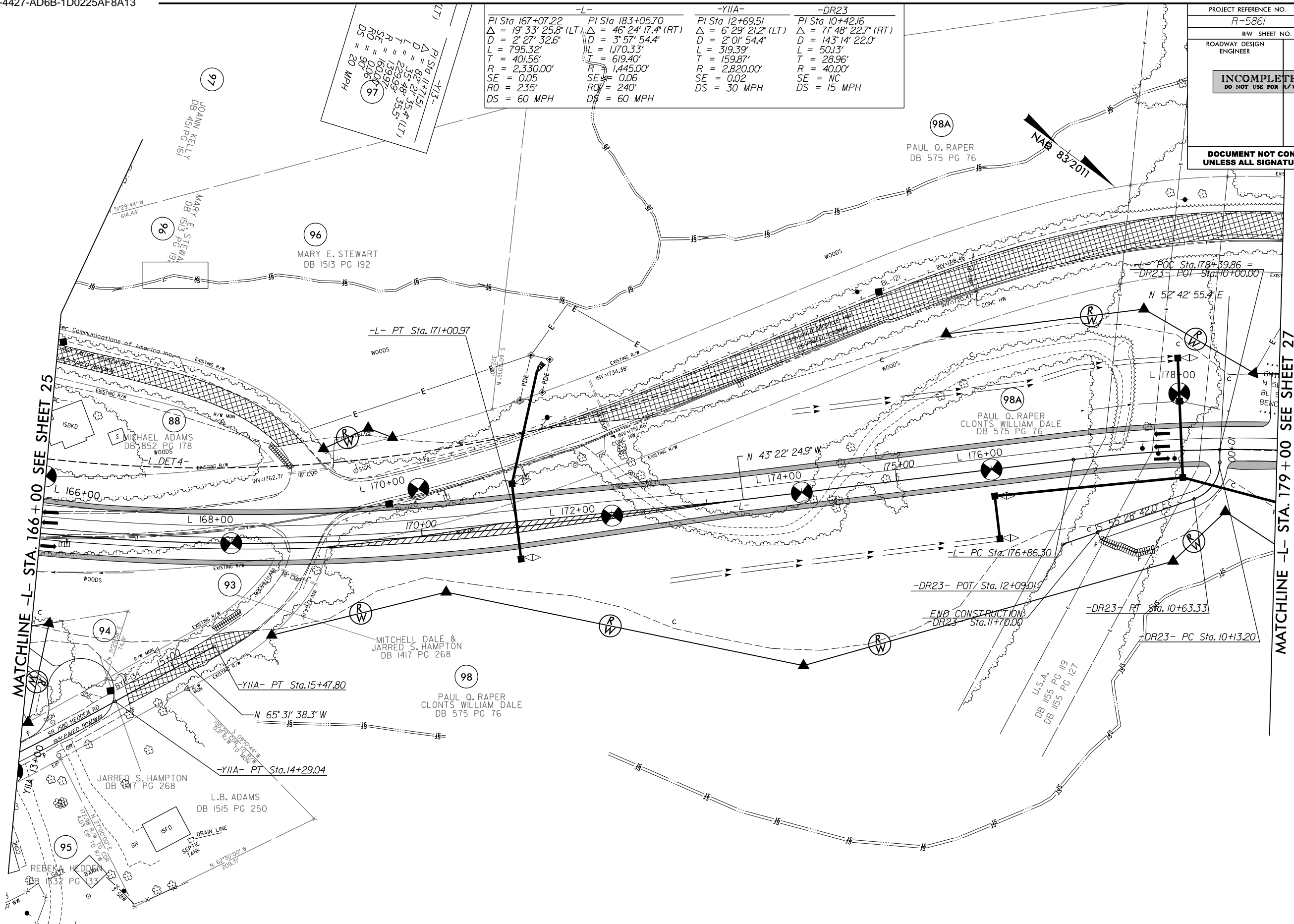
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 k.klaus

8/17/09

PROJECT REFERENCE NO. R-5861		SHEET NO. 26	
RW SHEET NO. 16		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION			
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED			

-L-	-YIIA-	-DR23-
PI Sta 167+07.22	PI Sta 183+05.70	PI Sta 12+69.51
$\Delta = 19' 33" 25.8" (LT)$	$\Delta = 46' 24" 17.4" (RT)$	$\Delta = 6' 29' 21.2" (LT)$
$D = 2' 27' 32.6"$	$D = 3' 57' 54.4"$	$D = 2' 01' 54.4"$
$L = 795.32'$	$L = 1,170.33'$	$L = 319.39'$
$T = 401.56'$	$T = 619.40'$	$T = 159.87'$
$R = 2,330.00'$	$R = 1,445.00'$	$R = 2,820.00'$
$SE = 0.05$	$SE = 0.06$	$SE = 0.02$
$RO = 235'$	$RO = 240'$	$RO = 30'$
$DS = 60$ MPH	$DS = 60$ MPH	$DS = 15$ MPH

-YI3-
PI Sta 11+71.51
$\Delta = 82' 17' 15.1"$
$D = 35' 27' 35.4" (LT)$
$L = 229.97'$
$T = 159.97'$
$R = 1,601.00'$
$SE = 0.06$
$RO = 90'$
$DS = 20$ MPH



MATCHLINE -L- STA. 166+00 SEE SHEET 25

MATCHLINE -L- STA. 179+00 SEE SHEET 27

NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

PAVEMENT REMOVAL

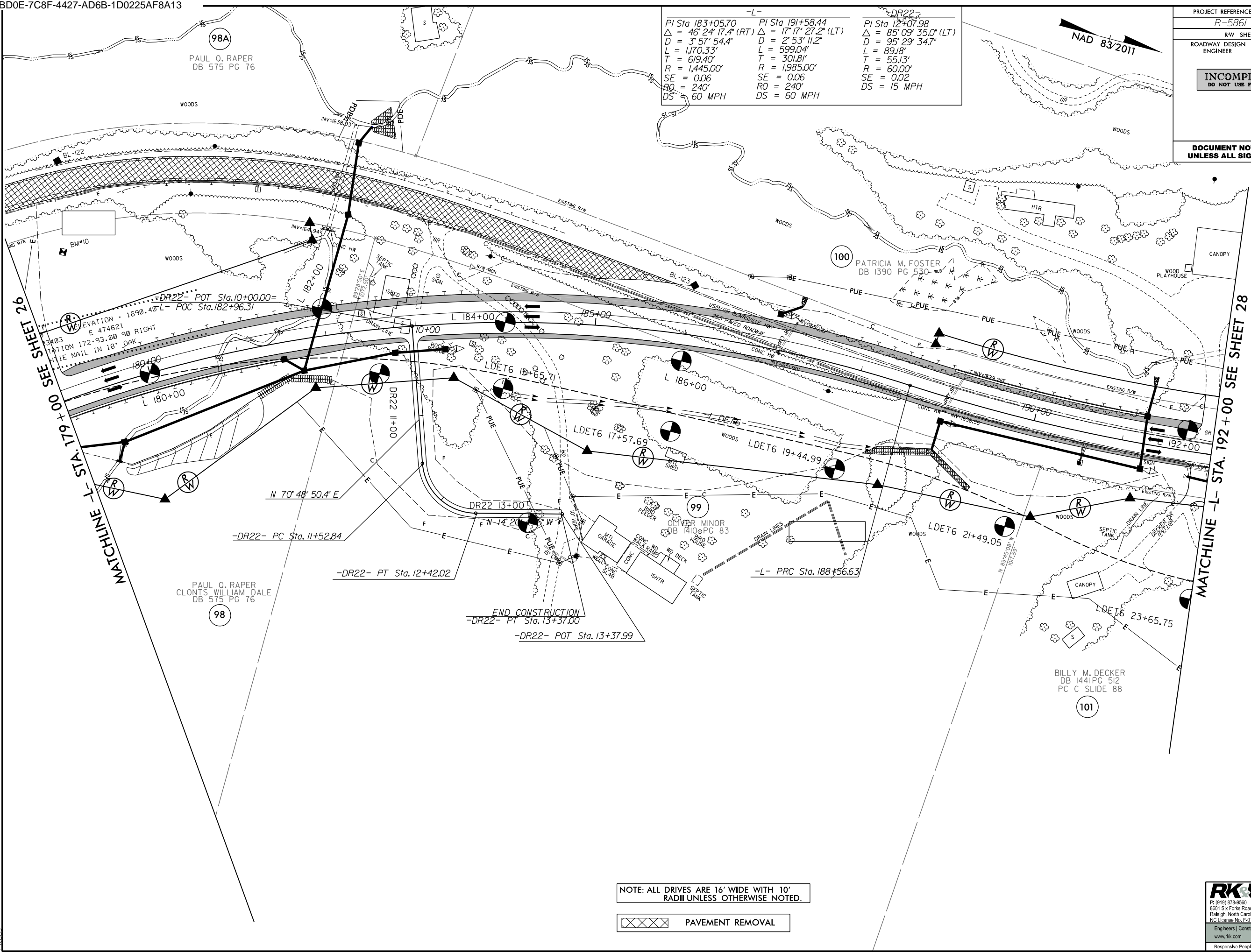
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PROJECT REFERENCE NO. R-5861		SHEET NO. 27	
RW SHEET NO. 17		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION			
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED			

-L-		DR22
PI Sta 183+05.70	PI Sta 191+58.44	PI Sta 12+07.98
$\Delta = 46^\circ 24' 17.4" (RT)$	$\Delta = 17^\circ 17' 27.2" (LT)$	$\Delta = 85^\circ 09' 35.0" (LT)$
D = 3' 57' 54.4"	D = 2' 53' 11.2"	D = 95' 29' 34.7"
L = 1,170.33'	L = 599.04'	L = 89.18'
T = 619.40'	T = 301.81'	T = 55.13'
R = 1,445.00'	R = 1,985.00'	R = 60.00'
SE = 0.06	SE = 0.06	SE = 0.02
RO = 240'	RO = 240'	DS = 15 MPH
DS = 60 MPH	DS = 60 MPH	



NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

PAVEMENT REMOVAL

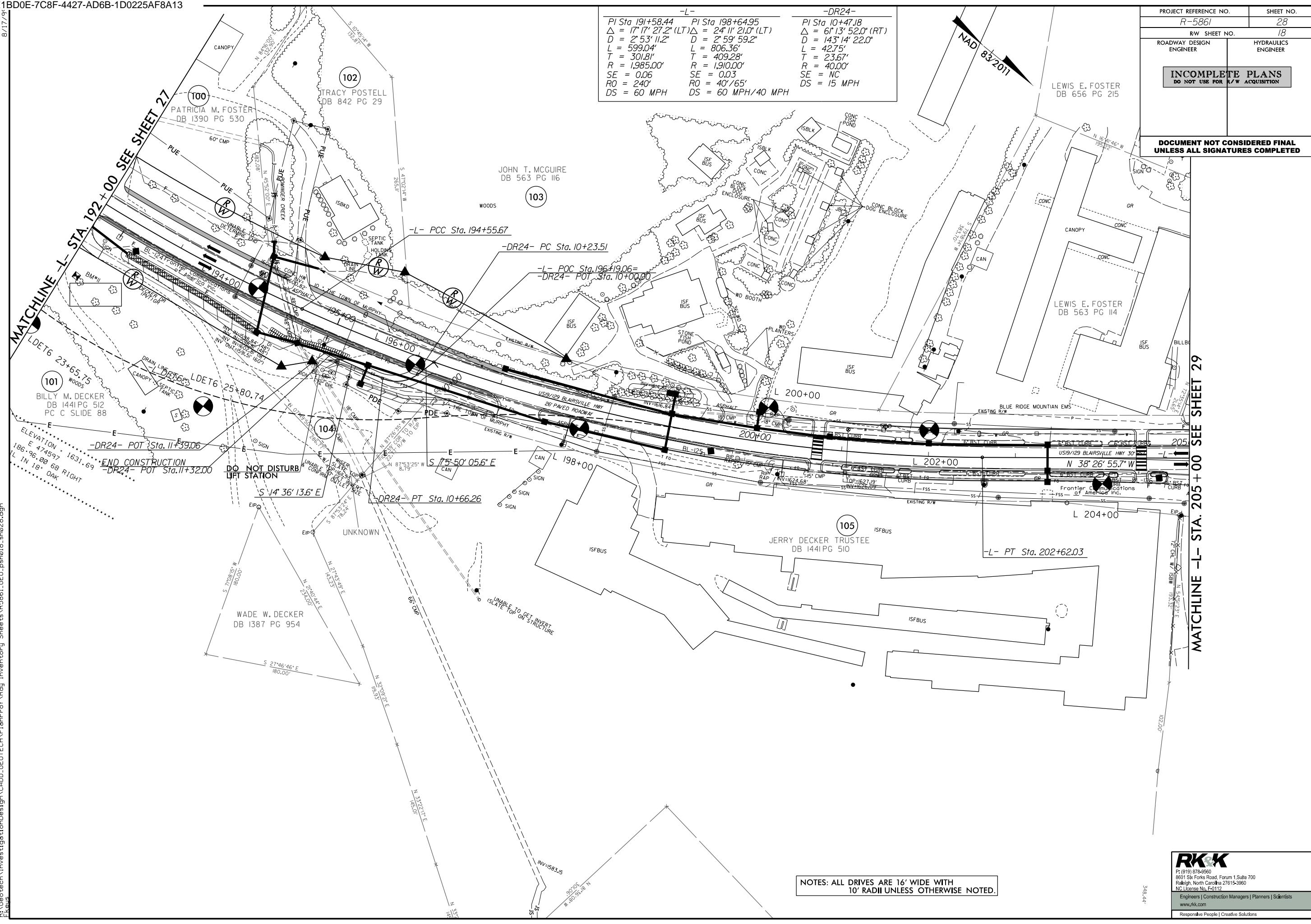
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PROJECT REFERENCE NO.	SHEET NO.
R-5861	28
R/W SHEET NO.	18
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	

-L-	-DR24-
PI Sta 191+58.44	PI Sta 198+64.95
$\Delta = 17' 17" 27.2" (LT)$	$\Delta = 24' 11" 21.0" (LT)$
$D = 2' 53' 11.2"$	$D = 2' 59' 59.2"$
$L = 599.04'$	$L = 806.36'$
$T = 301.81'$	$T = 409.28'$
$R = 1,985.00'$	$R = 1,910.00'$
$SE = 0.06$	$SE = 0.03$
$RO = 240'$	$RO = 40' / 65'$
$DS = 60 MPH$	$DS = 60 MPH / 40 MPH$
PI Sta 10+47.18	PI Sta 10+47.18
$\Delta = 6' 13' 52.0" (RT)$	$\Delta = 6' 13' 52.0" (RT)$
$D = 143' 14' 22.0"$	$D = 143' 14' 22.0"$
$L = 42.75'$	$L = 42.75'$
$T = 23.67'$	$T = 23.67'$
$R = 40.00'$	$R = 40.00'$
$SE = NC$	$SE = NC$
$DS = 15 MPH$	$DS = 15 MPH$

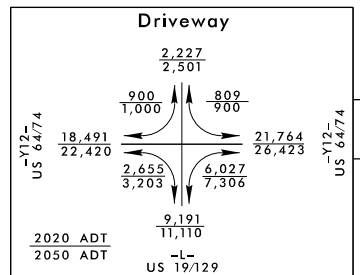


NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

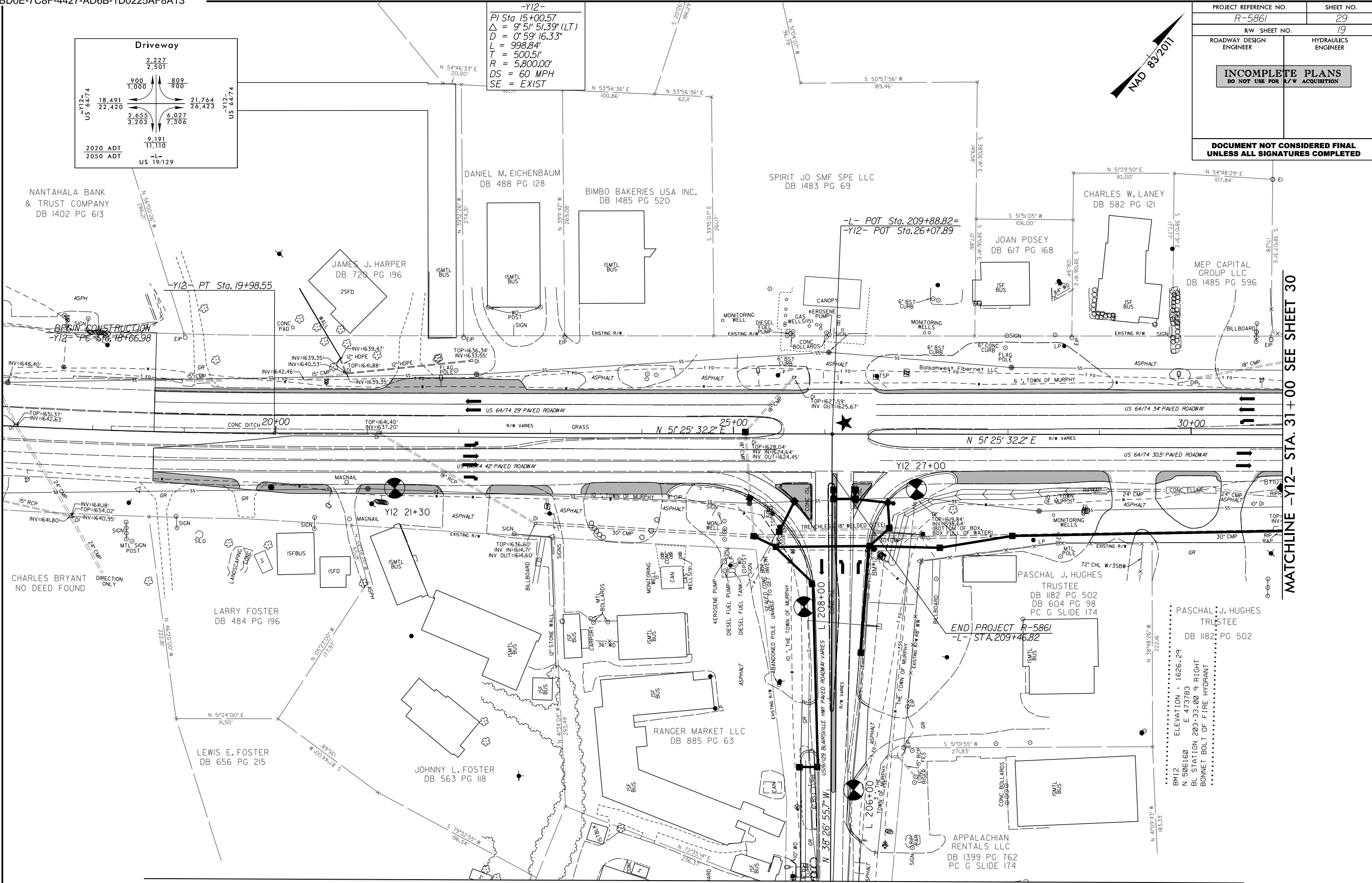
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PROJECT REFERENCE NO. <i>R-5861</i>		SHEET NO. <i>29</i>	
RW SHEET NO. <i>19</i>		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION			
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED			



*-Y12-*  
 PI Sta 15+00.57  
 $\Delta = 9^{\circ} 51' 51.39''$  (LT)  
 $D = 0^{\circ} 59' 16.33''$   
 $L = 998.84'$   
 $T = 500.51'$   
 $R = 5,800.00'$   
 $DS = 60$  MPH  
 $SE = EXIST$



MATCHLINE -Y12- STA. 31+00 SEE SHEET 30

MATCHLINE -L- STA. 205+00 SEE SHEET 28

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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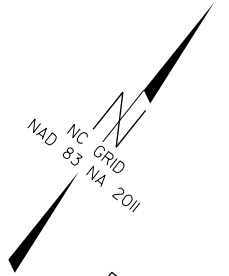
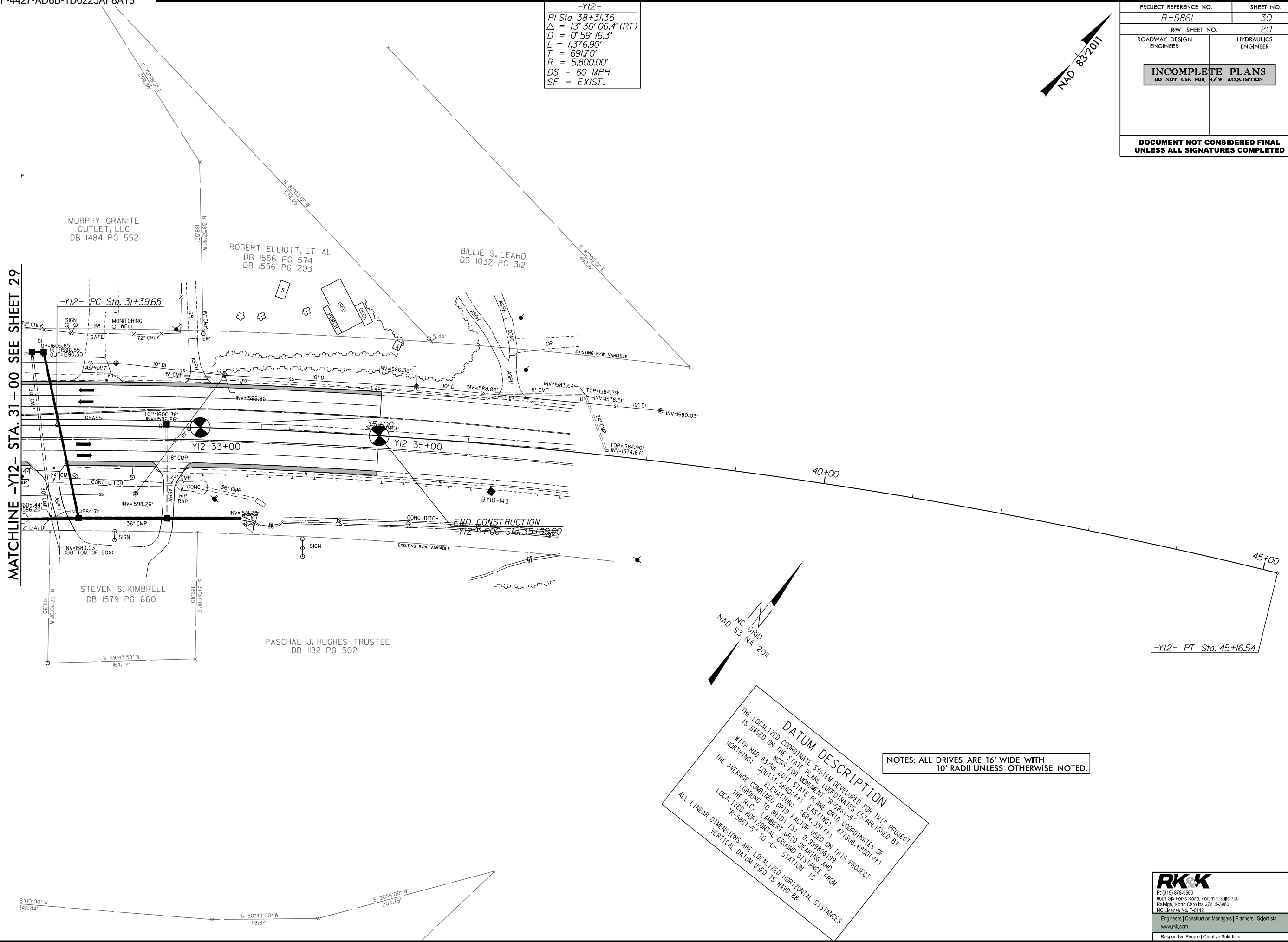
-Y12-

PI Sta 38+31.35  
 $\Delta = 13^{\circ} 36' 06.4" (RT)$   
 $D = 0^{\circ} 59' 16.3"$   
 $L = 1,376.90'$   
 $T = 691.70'$   
 $R = 5,800.00'$   
 $DS = 60 \text{ MPH}$   
 $SF = \text{EXIST.}$



PROJECT REFERENCE NO. <i>R-5861</i>	SHEET NO. <i>30</i>
R/W SHEET NO. <i>20</i>	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	

MATCHLINE -Y12- STA. 31+00 SEE SHEET 29



**DATUM DESCRIPTION**

THE LOCALIZED COORDINATE SYSTEM DEVELOPED FOR THIS PROJECT IS BASED ON THE STATE PLANE COORDINATES ESTABLISHED BY NCGS FOR MONUMENT "R-5861-S".

NORTHING: 500131.5640(F+)  
 EASTING: 417308.6800(F+)  
 ELEVATION: 1684.35(F+)

THE AVERAGE COMBINED GRID FACTOR USED ON THIS PROJECT (GROUND TO GRID) IS: 0.999806199

THE N.C. LAMBERT GRID BEARING AND LOCALIZED HORIZONTAL GROUND DISTANCE FROM "R-5861-S" TO "L" STATION IS

ALL LINEAR DIMENSIONS ARE LOCALIZED HORIZONTAL DISTANCES. VERTICAL DATUM USED IS NAVD 88

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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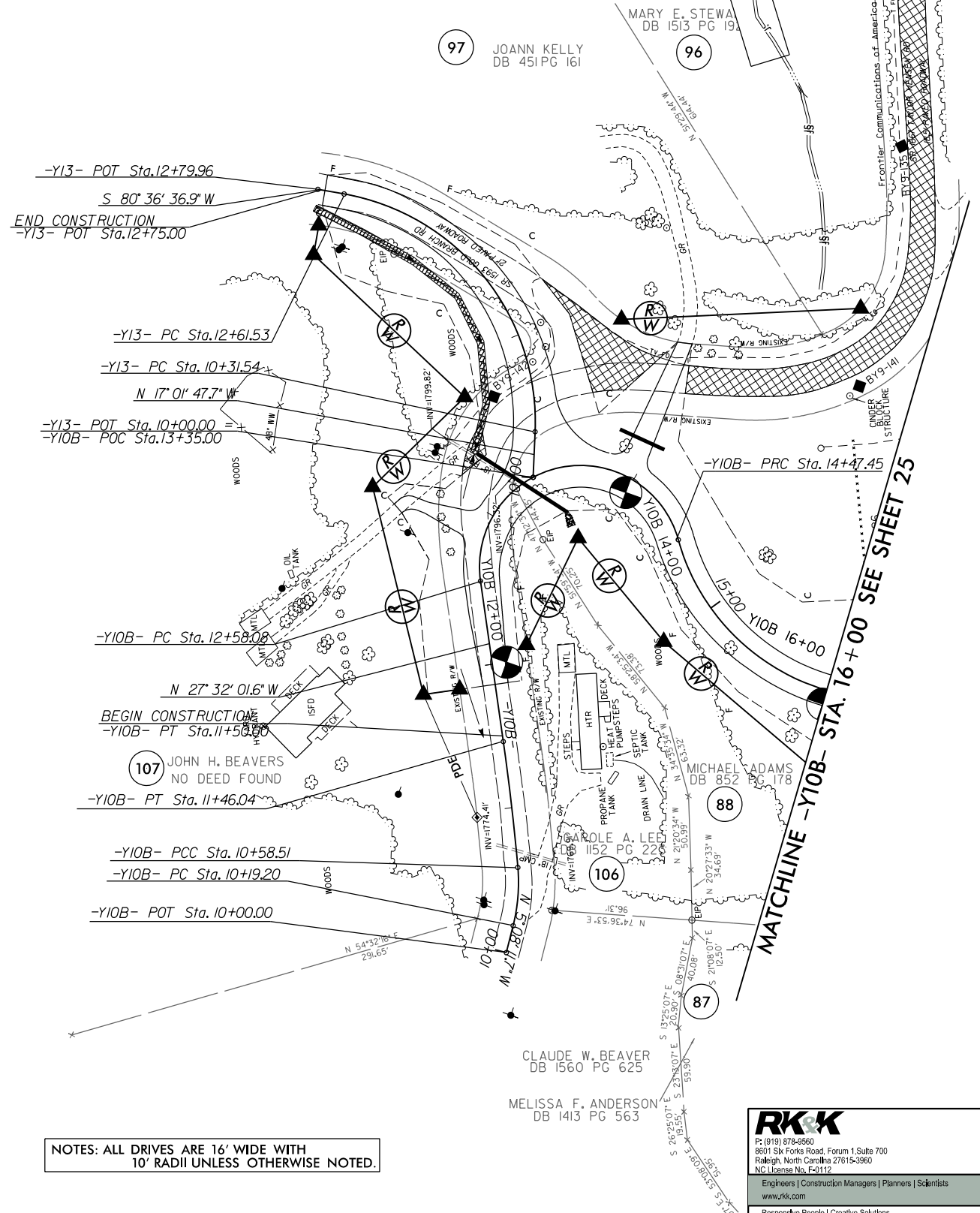
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REVISIONS

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-Y10B-		-Y13-		
PI Sta 10+39.67	PI Sta 11+02.29	PI Sta 13+52.77	PI Sta 18+30.42	PI Sta 11+71.51
$\Delta = 19^{\circ} 21' 25.9" (LT)$	$\Delta = 3^{\circ} 02' 24.0" (LT)$	$\Delta = 172^{\circ} 38' 45.0" (RT)$	$\Delta = 137^{\circ} 13' 19.0" (LT)$	$\Delta = 82^{\circ} 21' 35.4" (LT)$
$D = 49' 14' 55.1"$	$D = 3' 28' 22.8"$	$D = 91' 10' 09.8"$	$D = 38' 11' 49.9"$	$D = 35' 48' 35.5"$
$L = 39.31'$	$L = 87.53'$	$L = 189.37'$	$L = 359.25'$	$L = 229.99'$
$T = 20.47'$	$T = 43.78'$	$T = 1089.23'$	$T = 382.97'$	$T = 139.97'$
$R = 120.00'$	$R = 1650.00'$	$R = 70.00'$	$R = 150.00'$	$R = 160.00'$
		$SE = 0.06$	$SE = 0.06$	$SE = 0.06$
		$RO = 120'$	$RO = 100'$	$RO = 90'$
		$DS = 15 MPH$	$DS = 25 MPH$	$DS = 20 MPH$

PROJECT REFERENCE NO. R-5861	SHEET NO. 31
R/W SHEET NO. 21	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
<b>INCOMPLETE PLANS</b> DO NOT USE FOR R/W ACQUISITION	
<b>DOCUMENT NOT CONSIDERED FINAL</b> UNLESS ALL SIGNATURES COMPLETED	



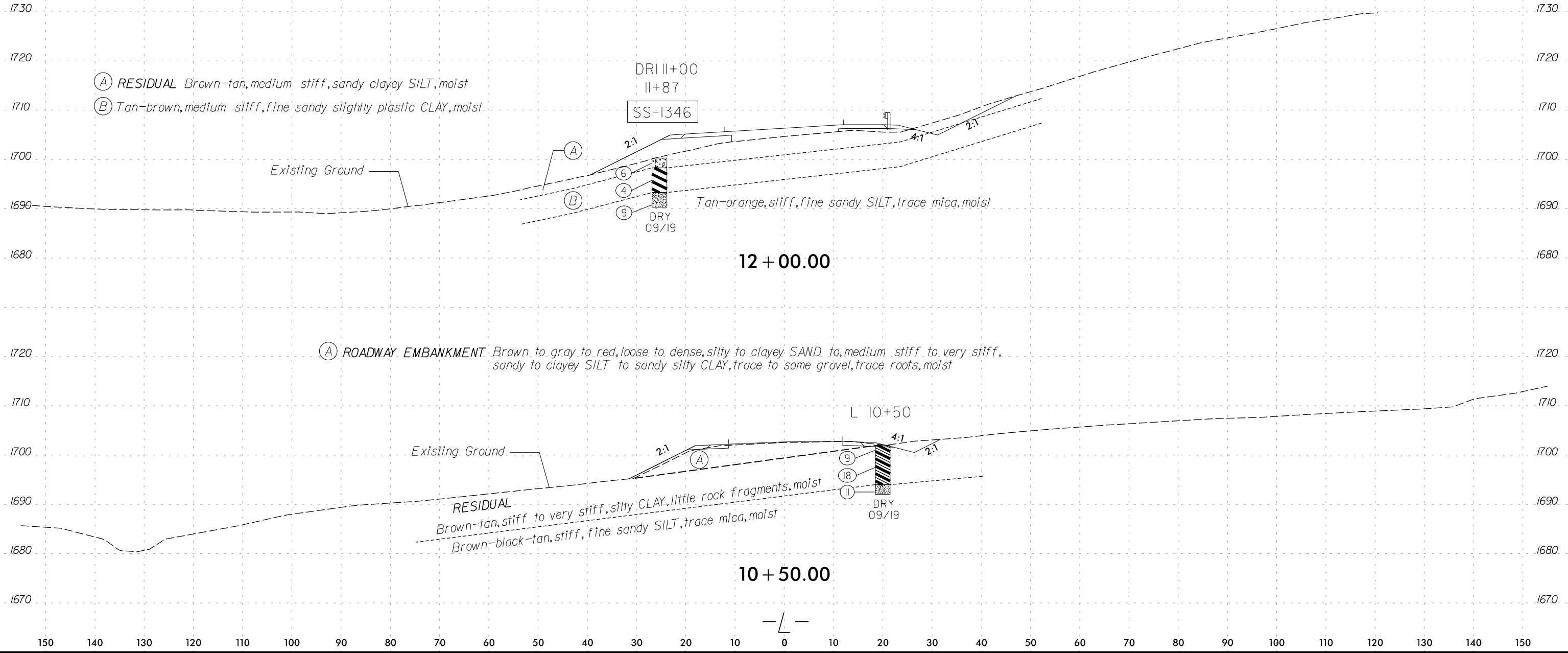
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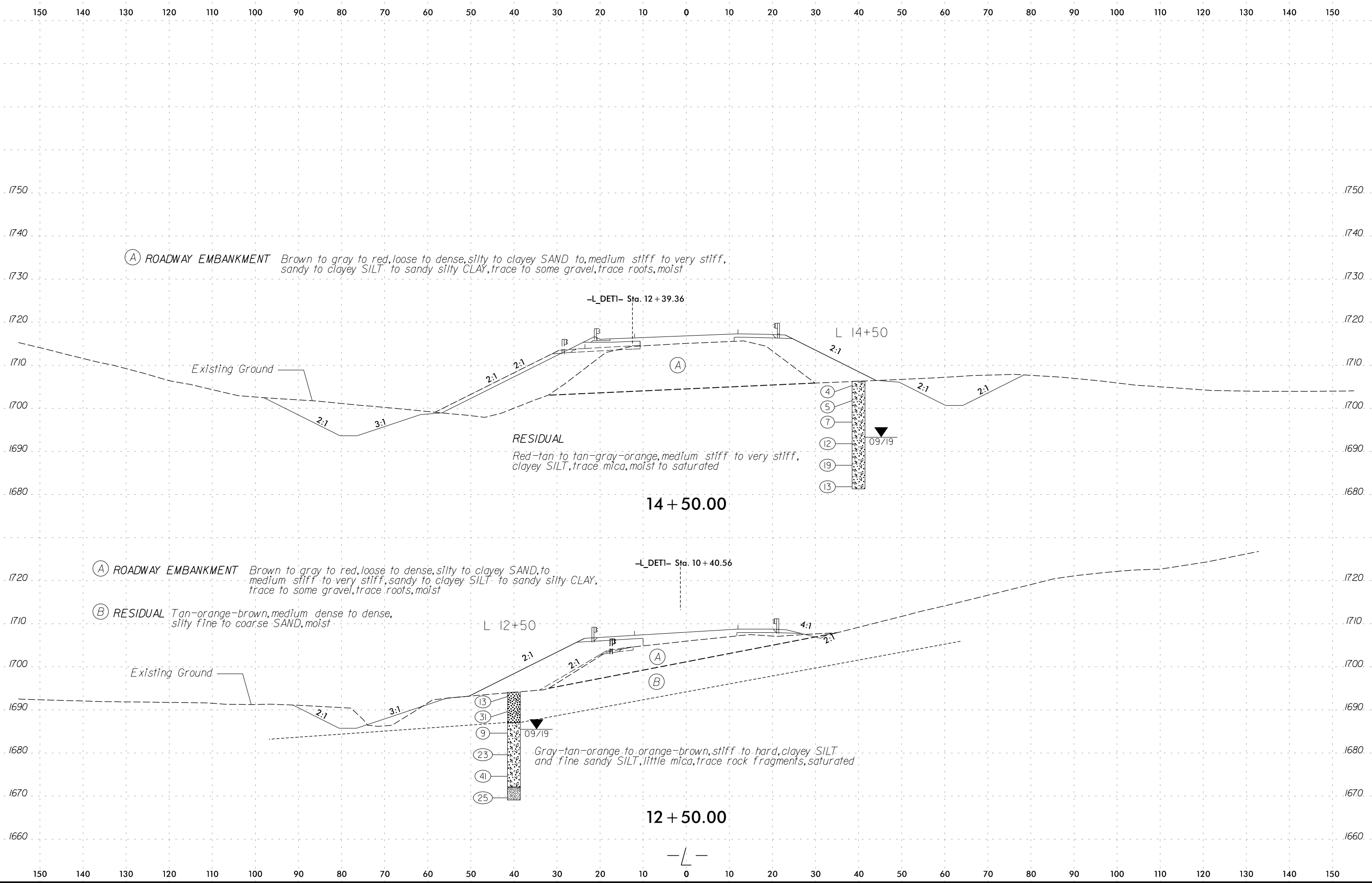


150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1346	11+87	25' LT	3.5-5.0	A-7-6 (7)	41	12	8	37	19	36	98	94	62.3	24.3	-

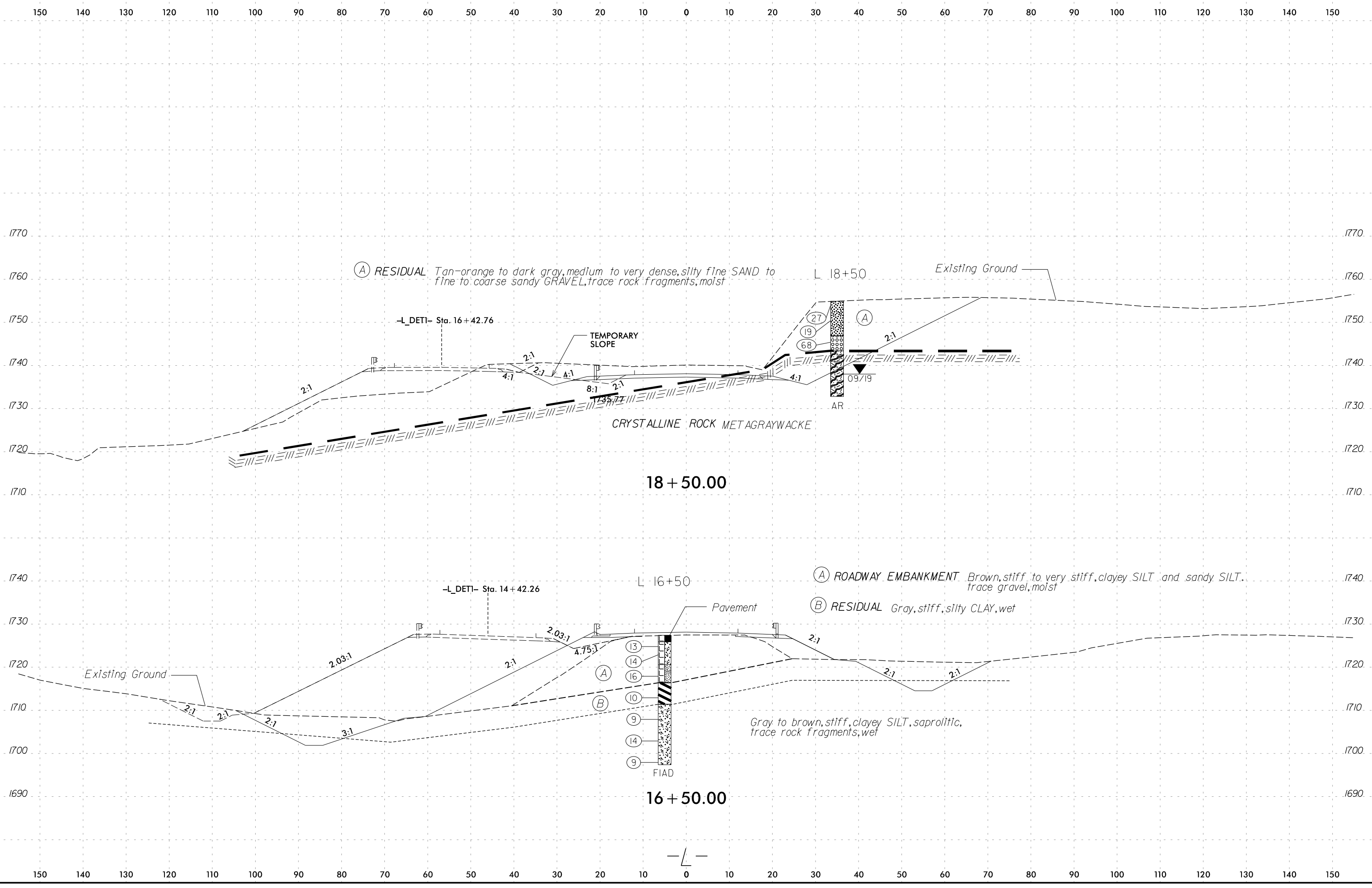


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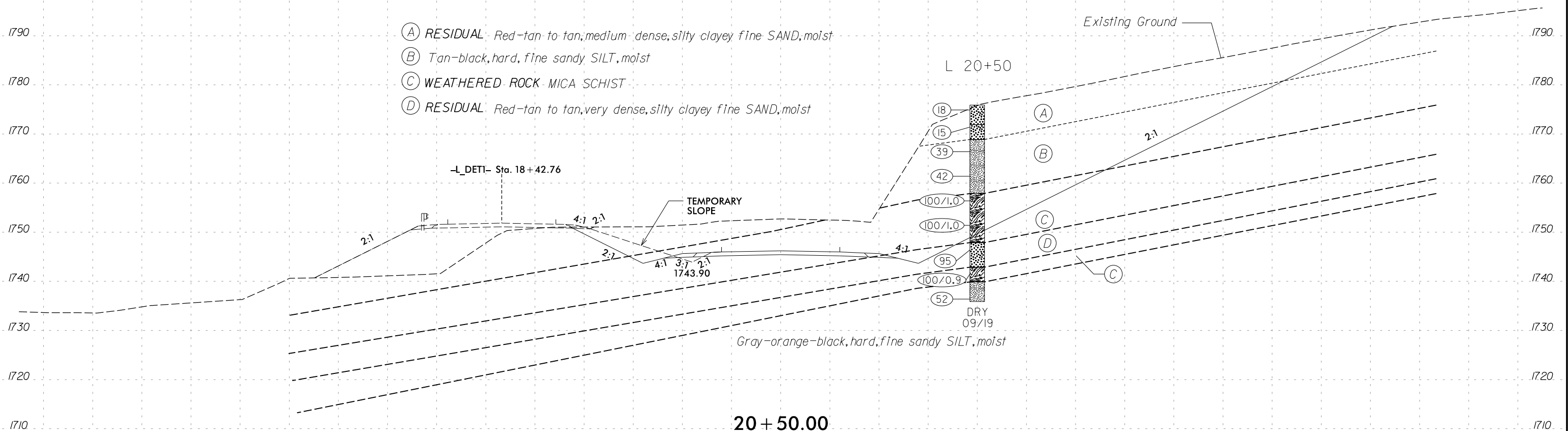
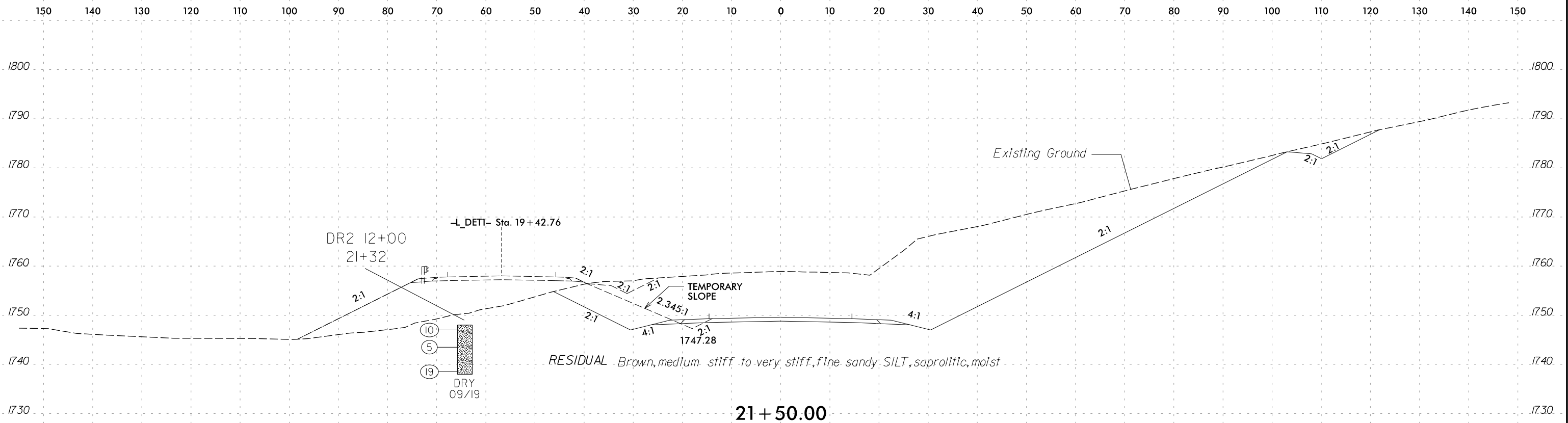


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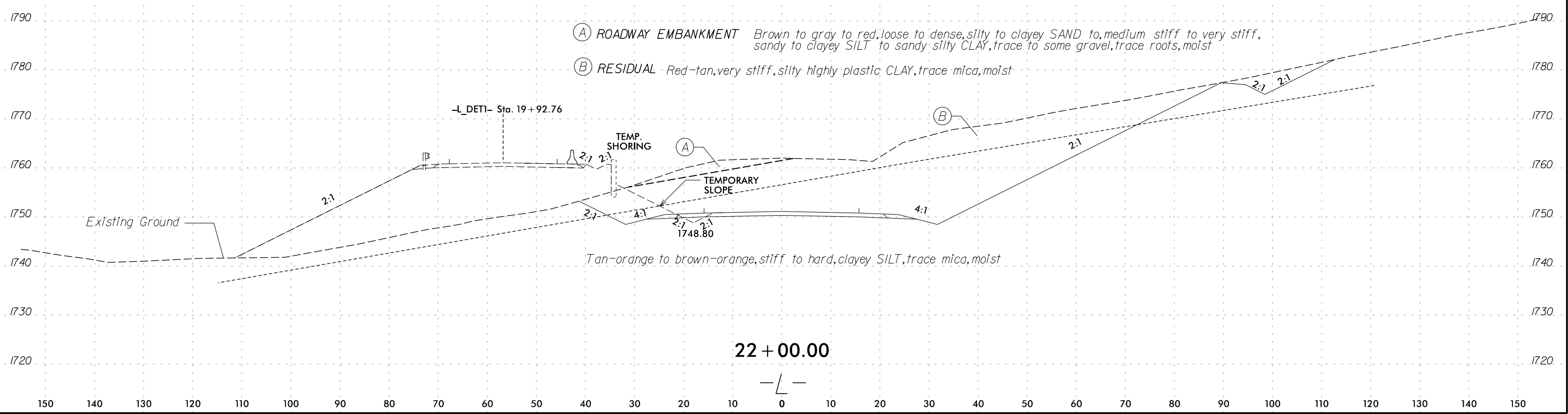
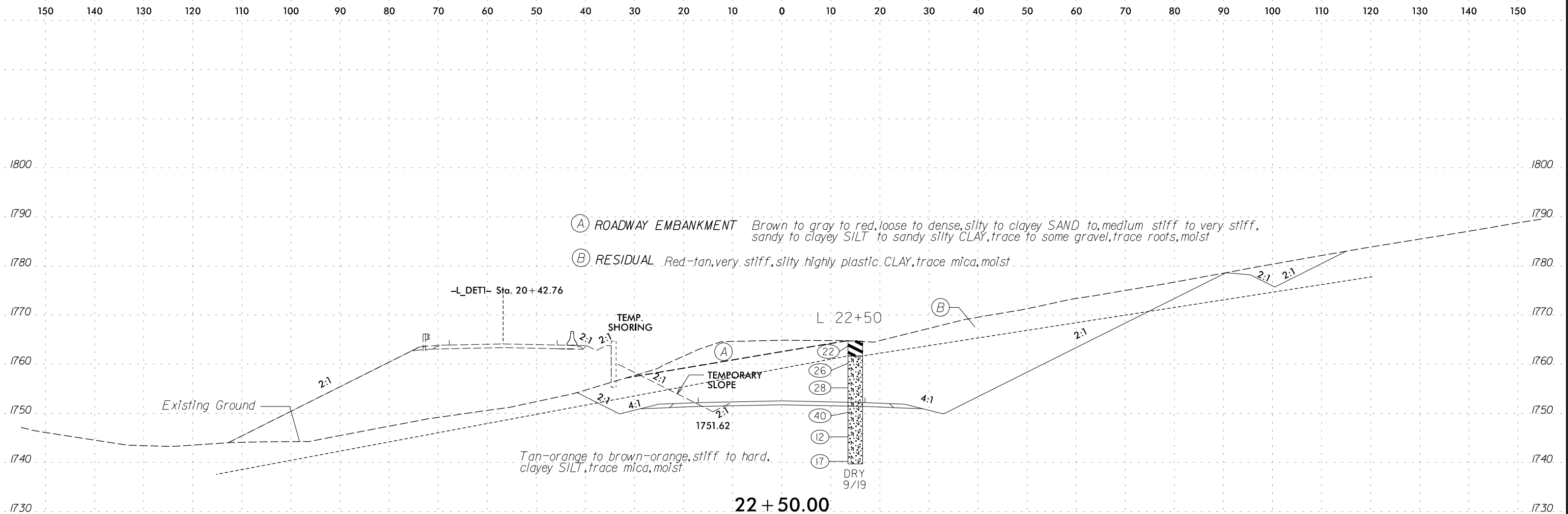


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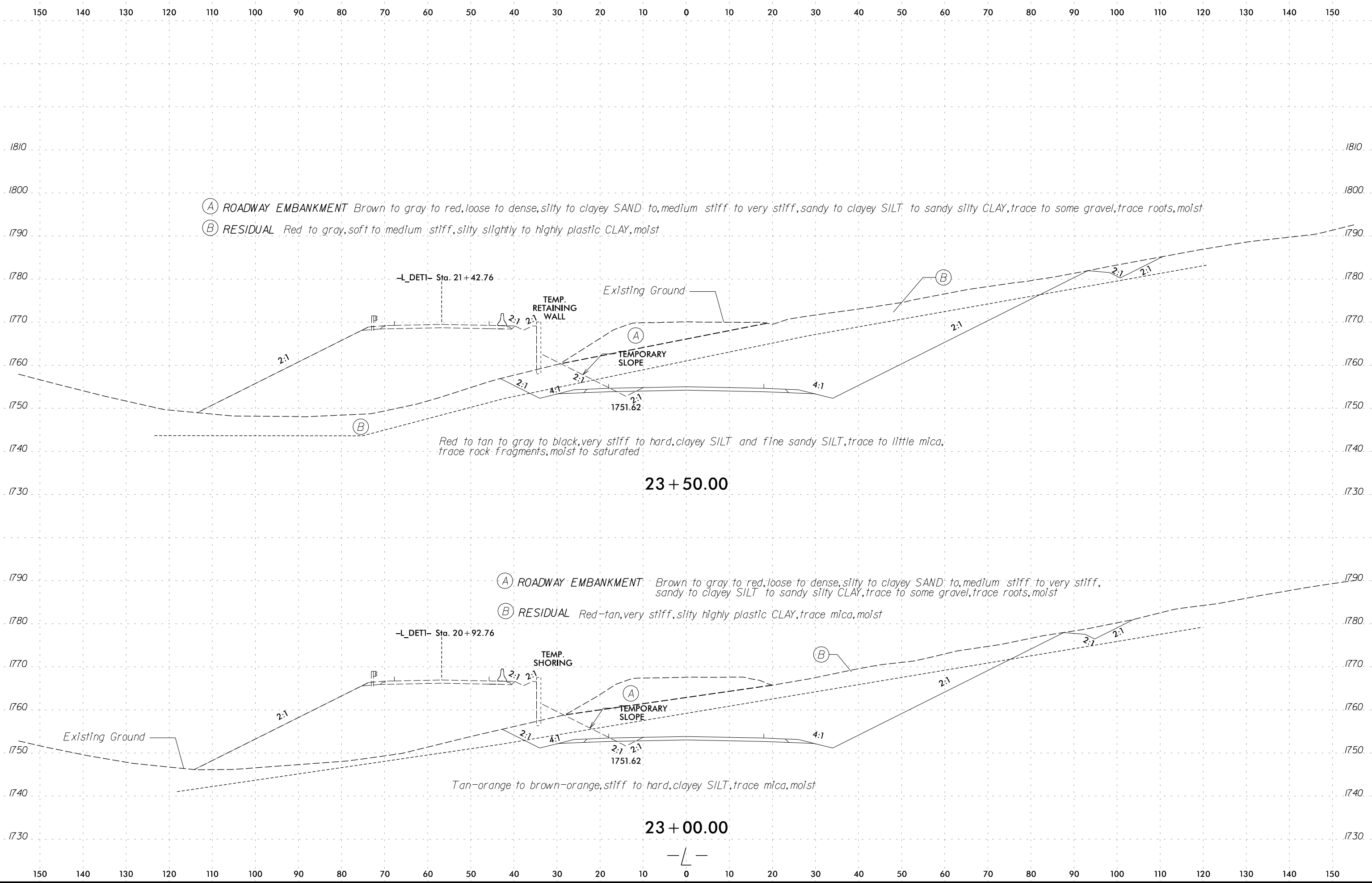


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(A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*  
 (B) RESIDUAL *Red to gray, soft to medium stiff, silty slightly to highly plastic CLAY, moist*

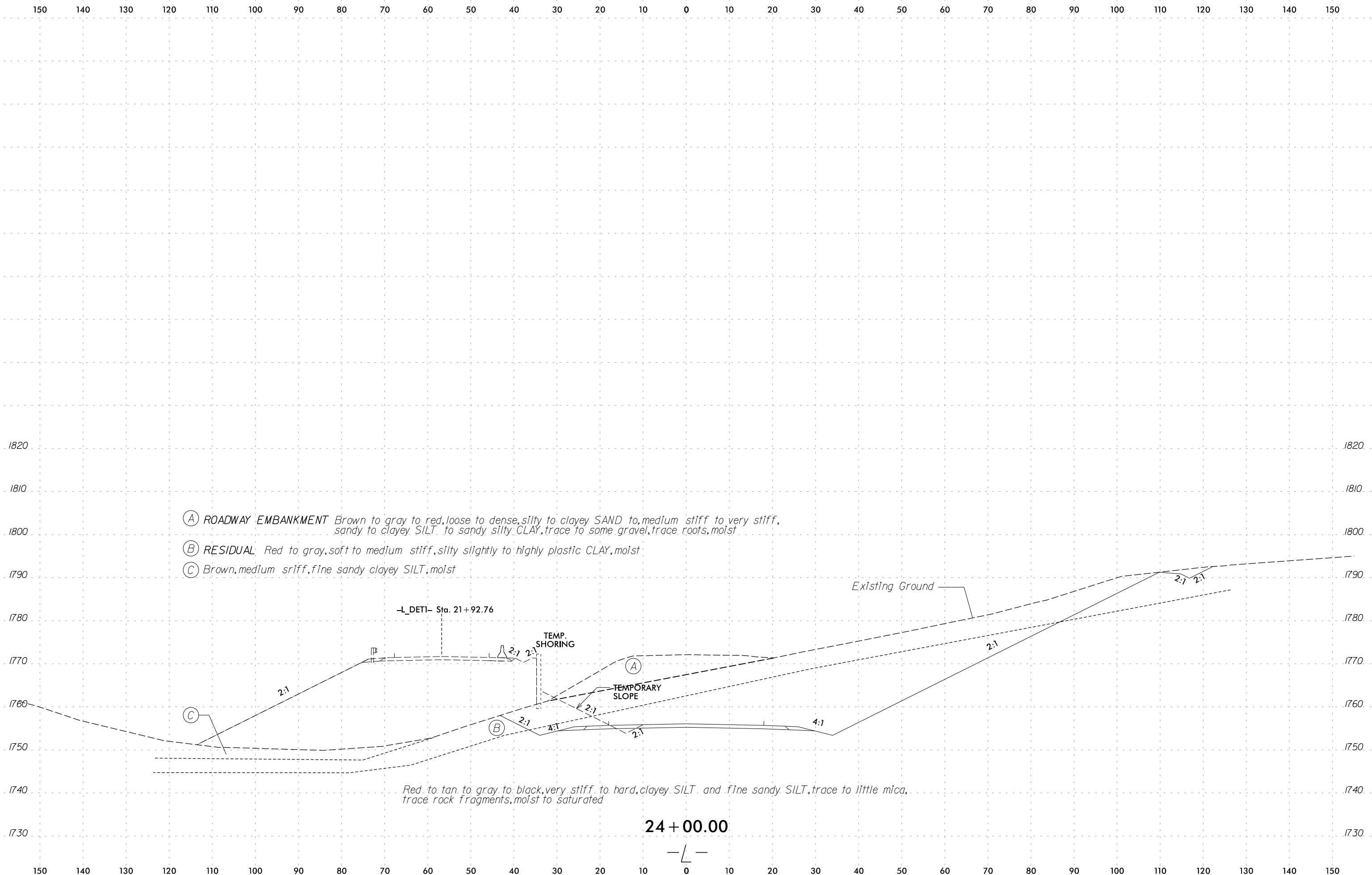
*Red to tan to gray to black, very stiff to hard, clayey SILT and fine sandy SILT, trace to little mica, trace rock fragments, moist to saturated*

(A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*  
 (B) RESIDUAL *Red-tan, very stiff, silty highly plastic CLAY, trace mica, moist*

*Tan-orange to brown-orange, stiff to hard, clayey SILT, trace mica, moist*

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- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Red to gray, soft to medium stiff, silty slightly to highly plastic CLAY, moist*
- (C) *Brown, medium stiff, fine sandy clayey SILT, moist*

-L DETI- Sta. 21+92.76

TEMP. SHORING

TEMPORARY SLOPE

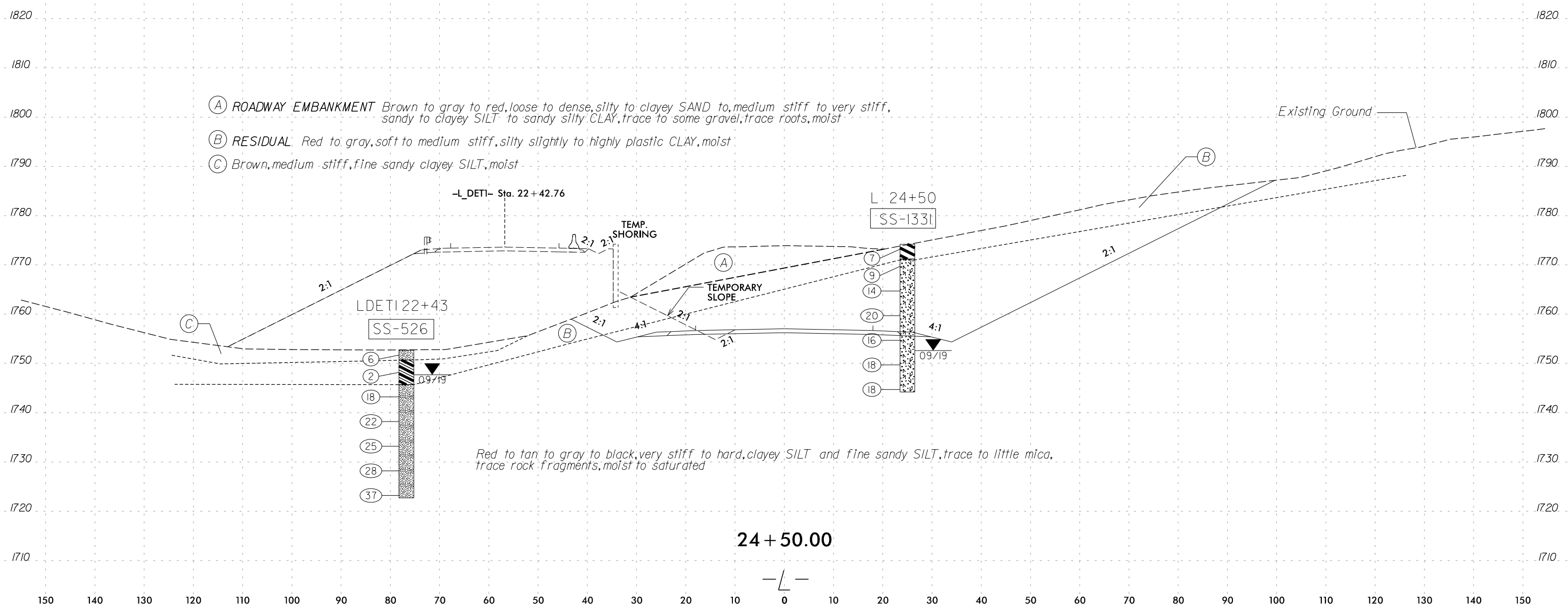
Existing Ground

24+00.00

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150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1331	24+50	25' RT	0.0-1.5	A-7-5 (26)	64	30	3	26	16	55	100	99	77.9	33	-
SS-526	24+50	77' LT	3.5-5.0	A-6 (5)	35	11	7	42	17	34	100	98	61.2	29.2	-

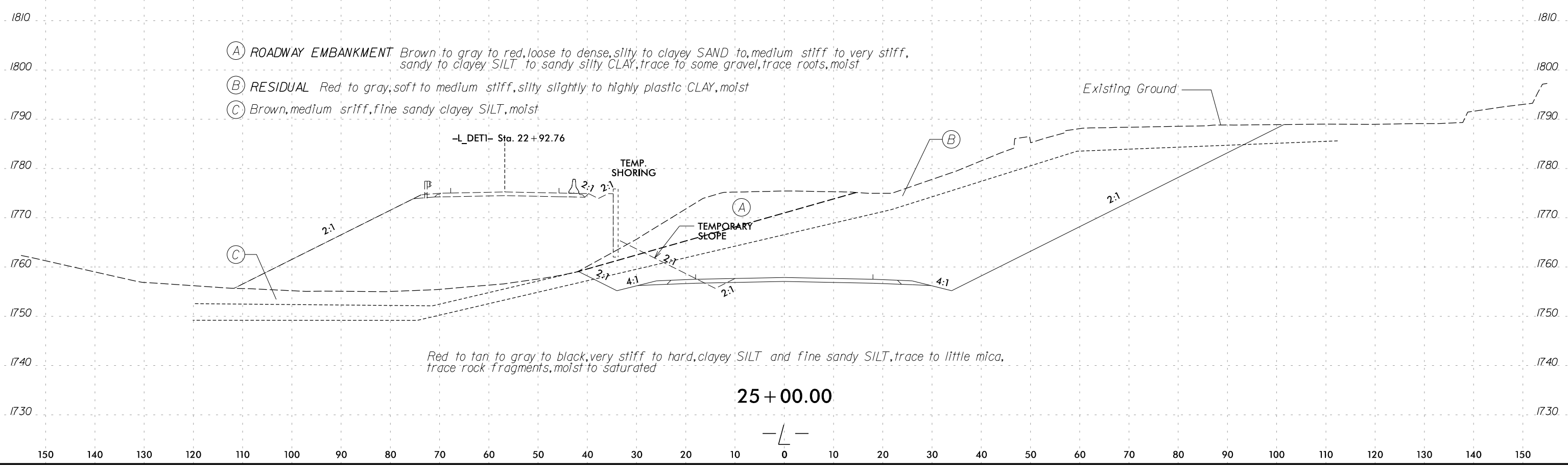
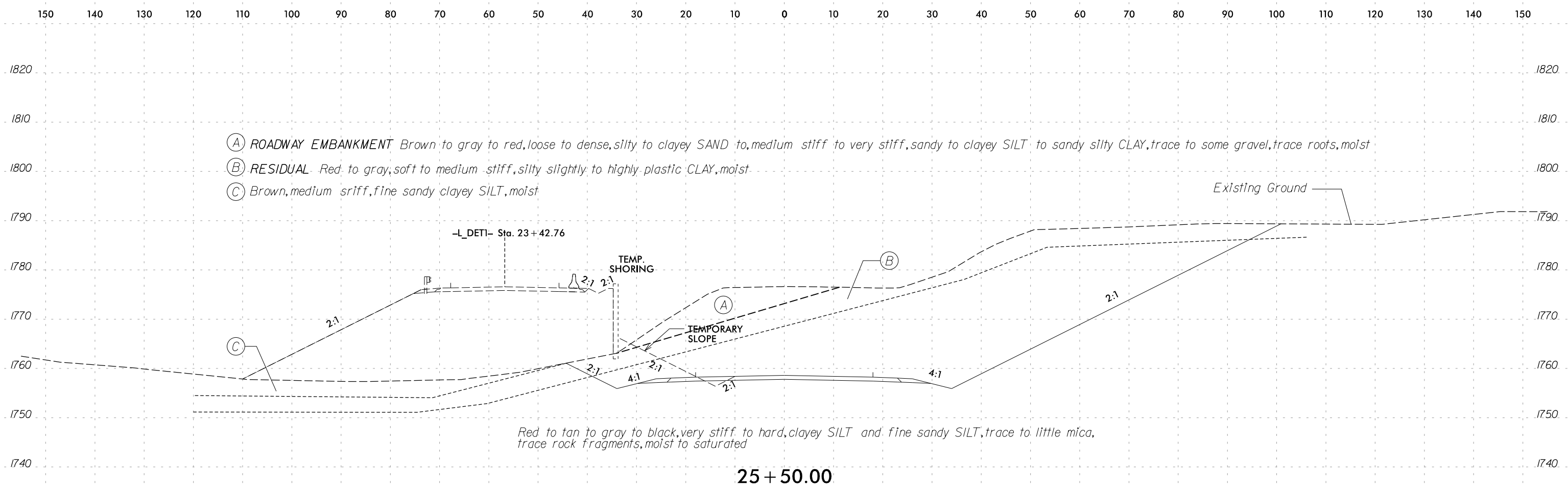


- (A) ROADWAY EMBANKMENT Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist
- (B) RESIDUAL Red to gray, soft to medium stiff, silty slightly to highly plastic CLAY, moist
- (C) Brown, medium stiff, fine sandy clayey SILT, moist

Red to tan to gray to black, very stiff to hard, clayey SILT and fine sandy SILT, trace to little mica, trace rock fragments, moist to saturated

24 + 50.00

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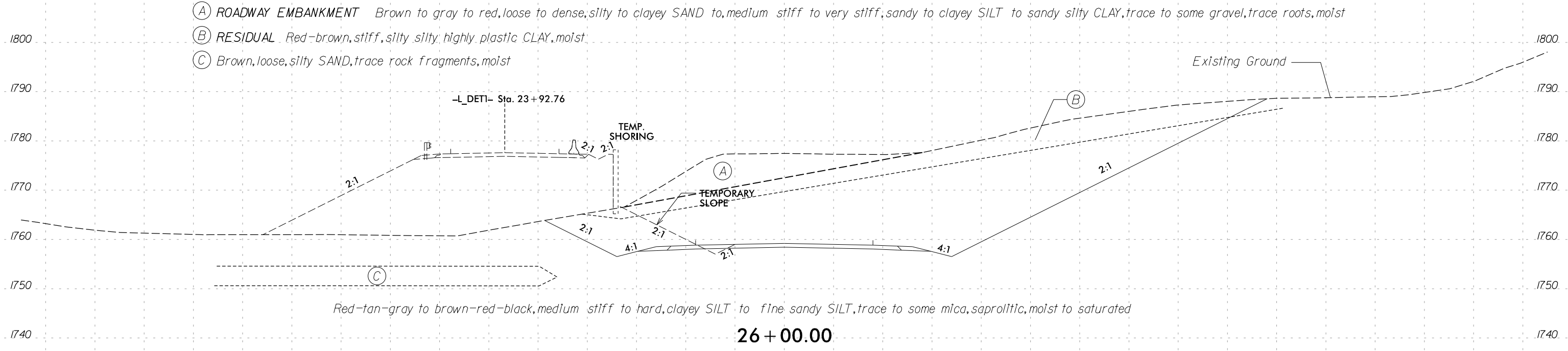
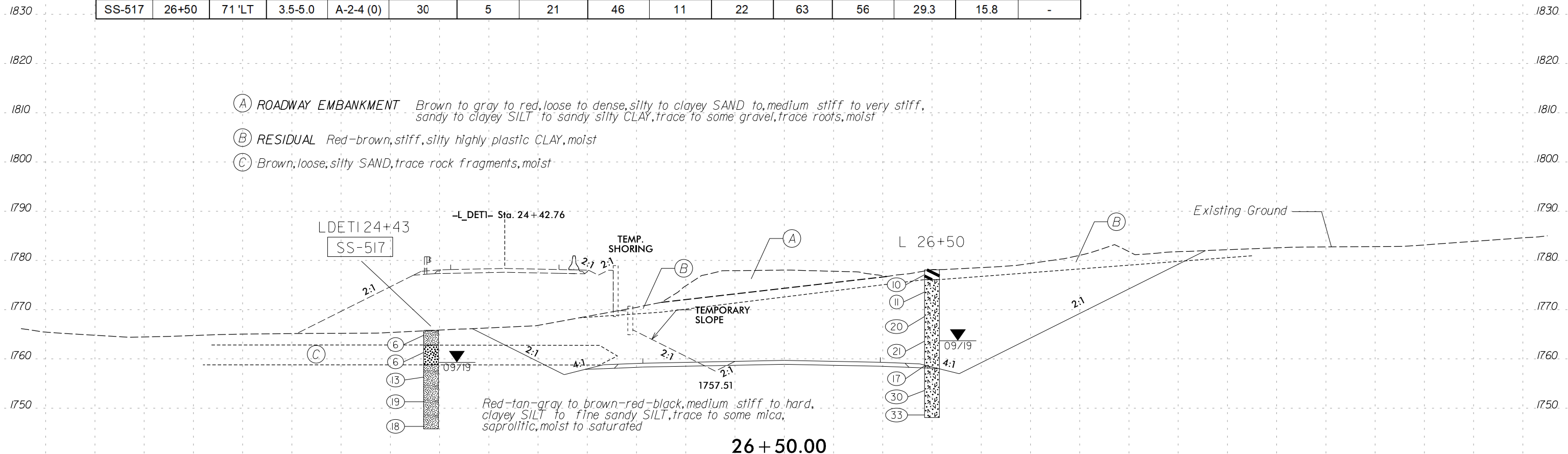


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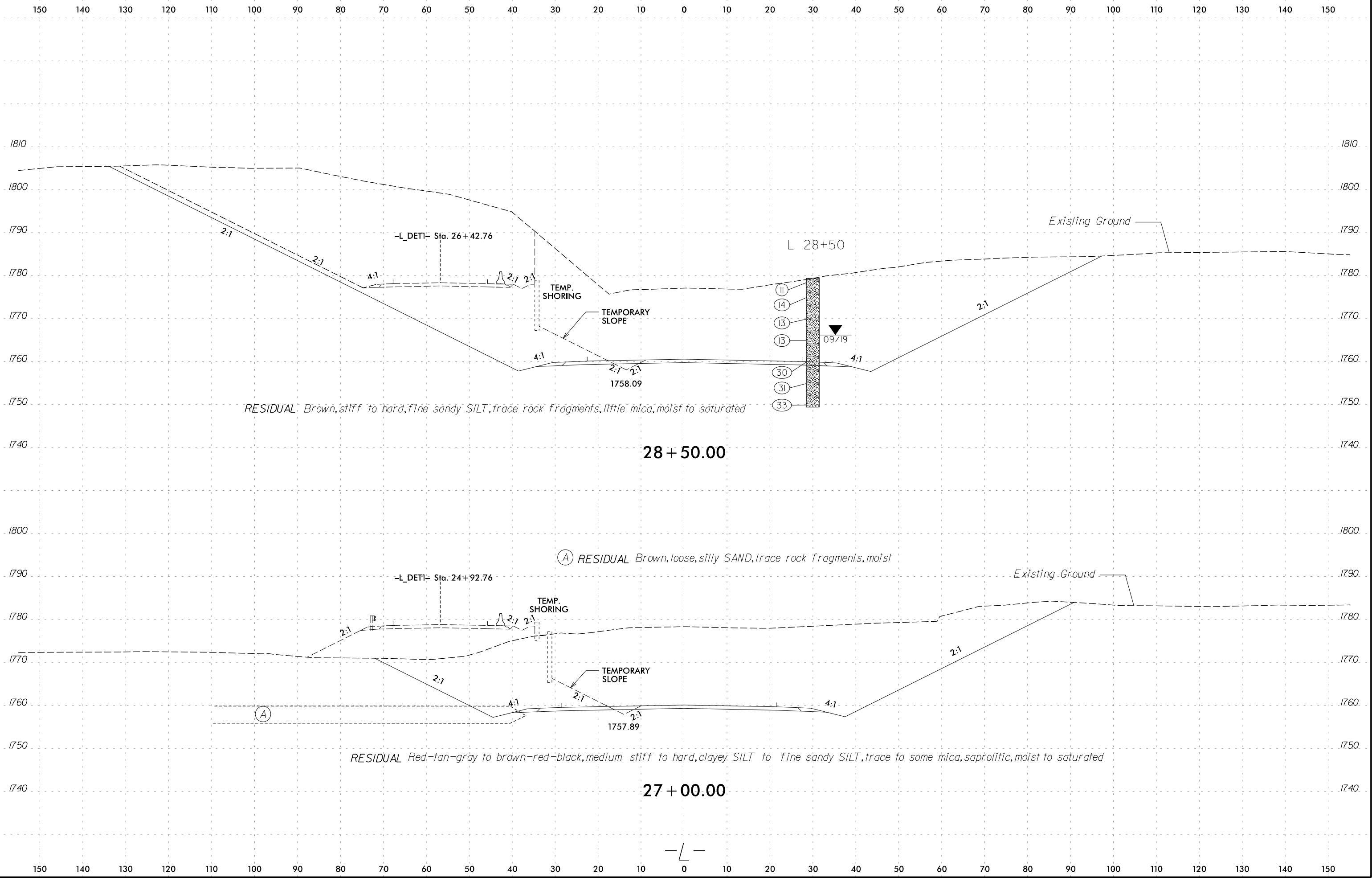


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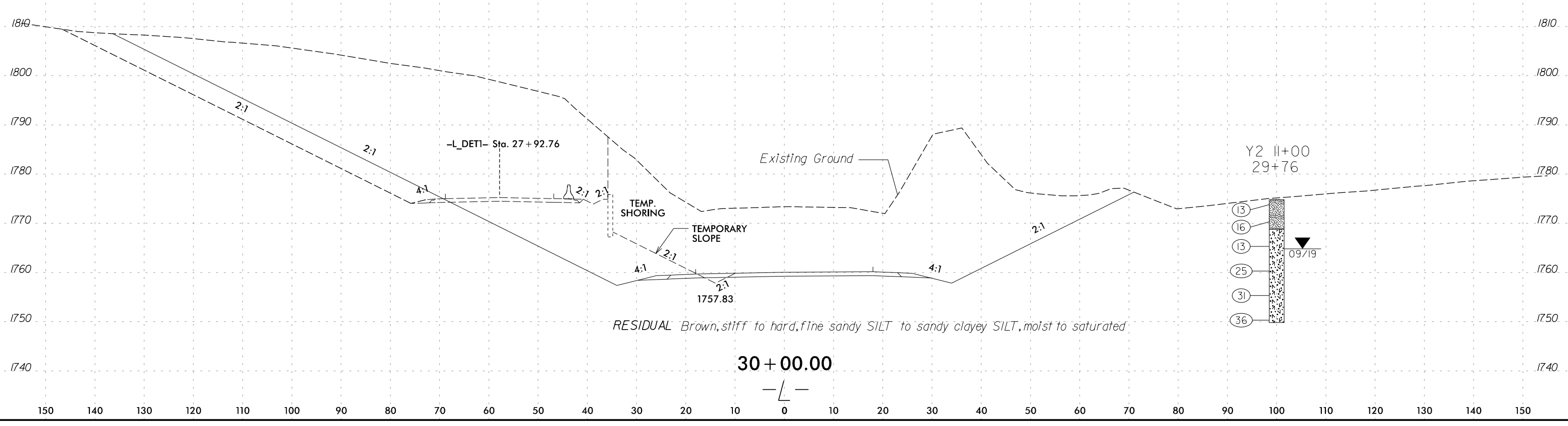
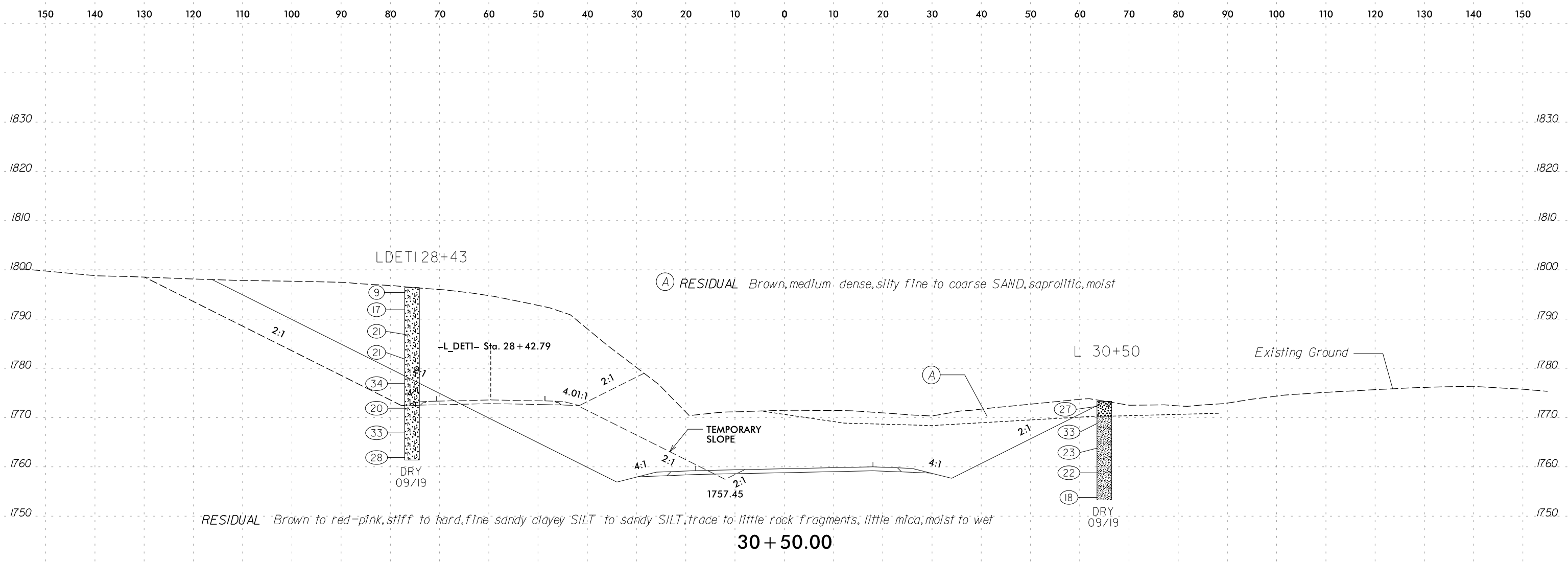
<b>SOIL TEST RESULTS</b>															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-517	26+50	71 'LT	3.5-5.0	A-2-4 (0)	30	5	21	46	11	22	63	56	29.3	15.8	-



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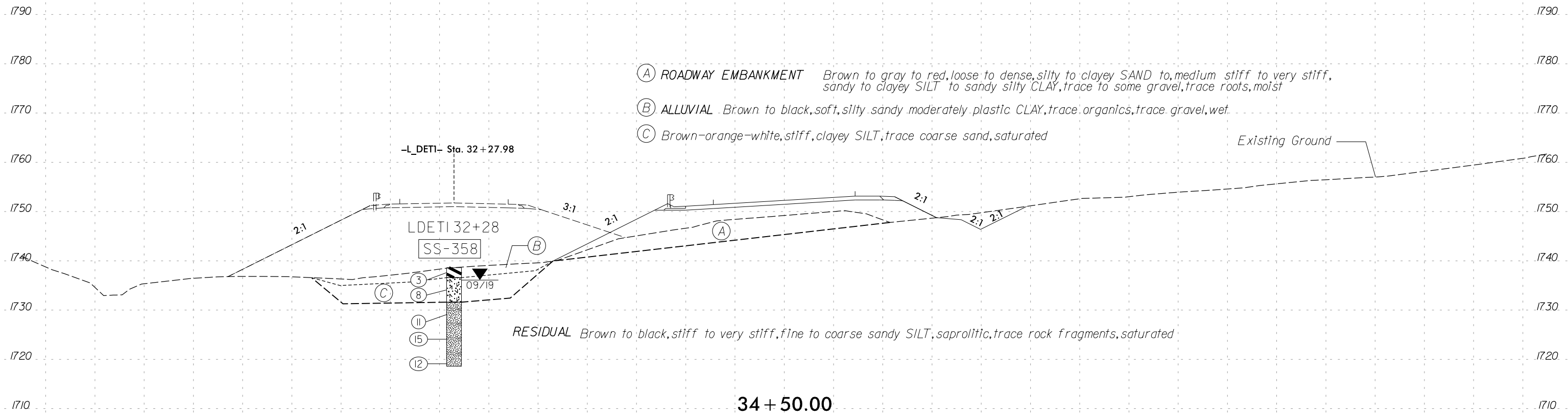


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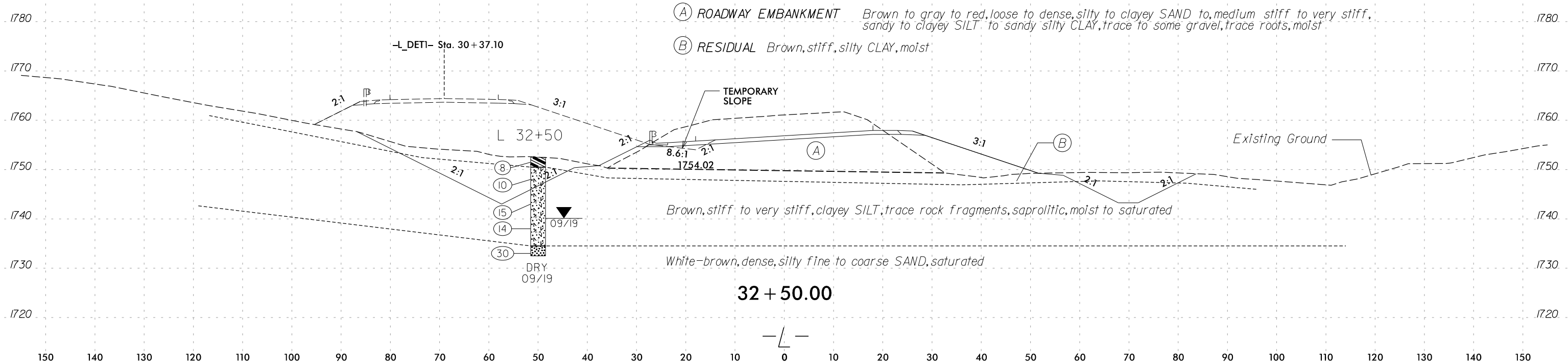


SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-358	34+50	67' LT	0.0-1.5	A-7-5 (6)	58	17	19	37	23	21	90	80	47.1	44.2	-

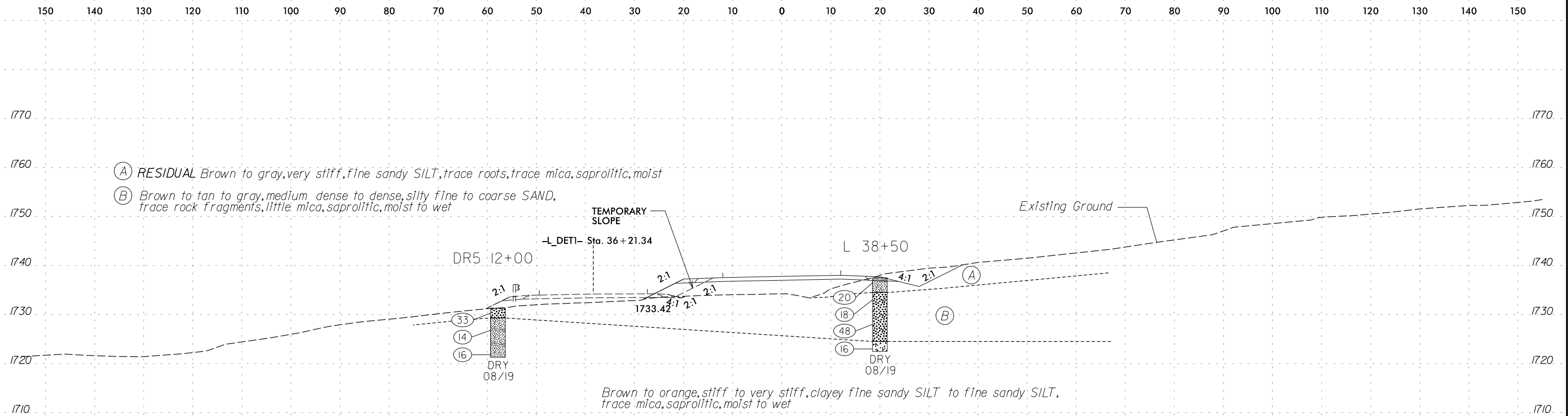
- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) ALLUVIAL *Brown to black, soft, silty sandy moderately plastic CLAY, trace organics, trace gravel, wet*
- (C) *Brown-orange-white, stiff, clayey SILT, trace coarse sand, saturated*



- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown, stiff, silty CLAY, moist*

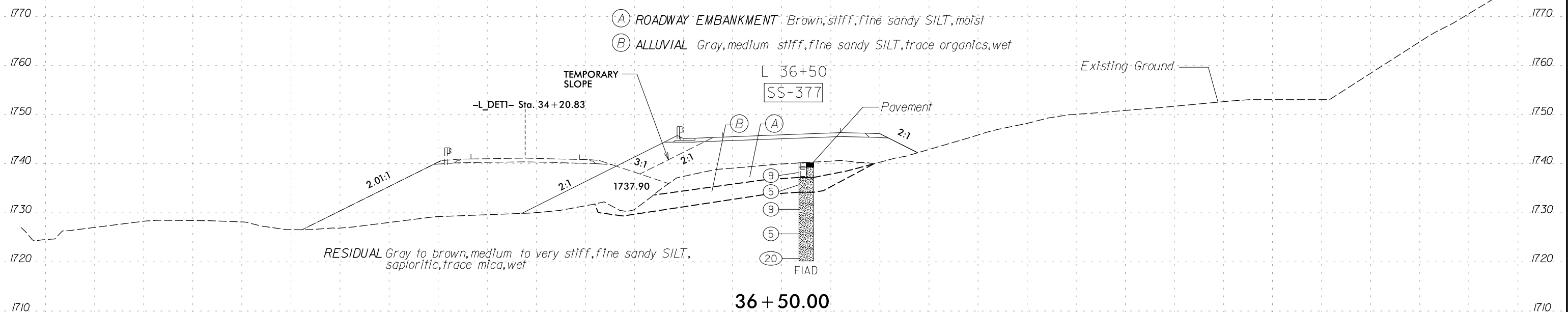


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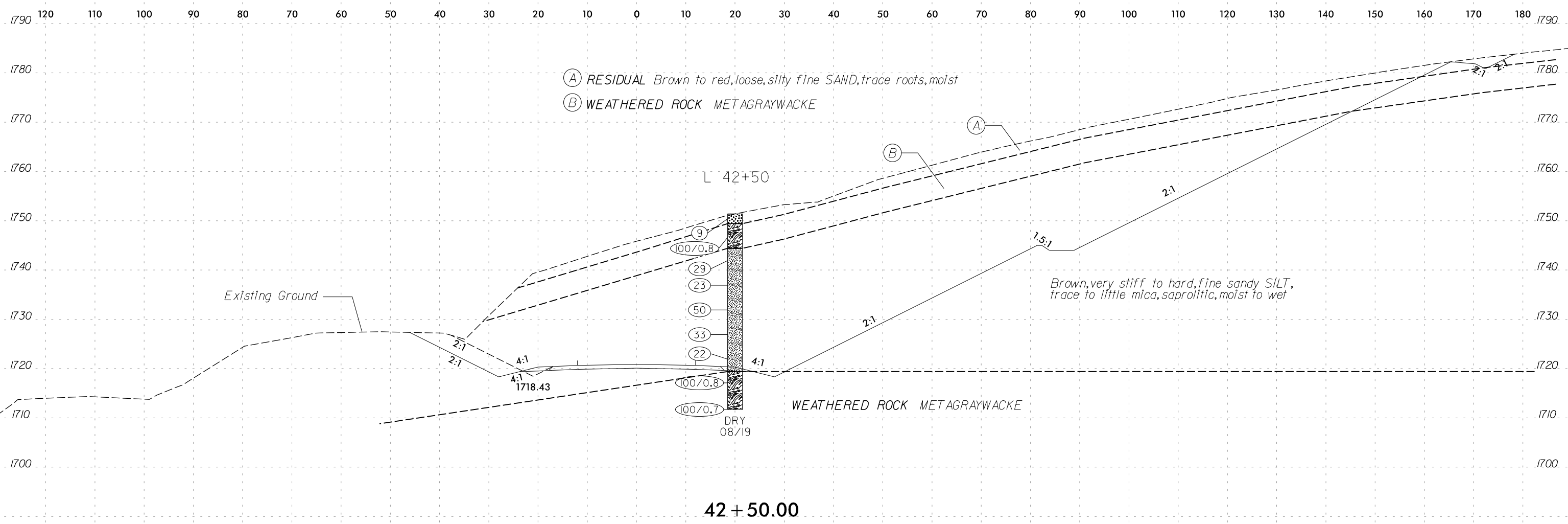
38 + 50.00

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-377	36+50	5' RT	3.5-5.0	A-4 (0)	24	3	16	54	10	20	100	95	41	17.7	-



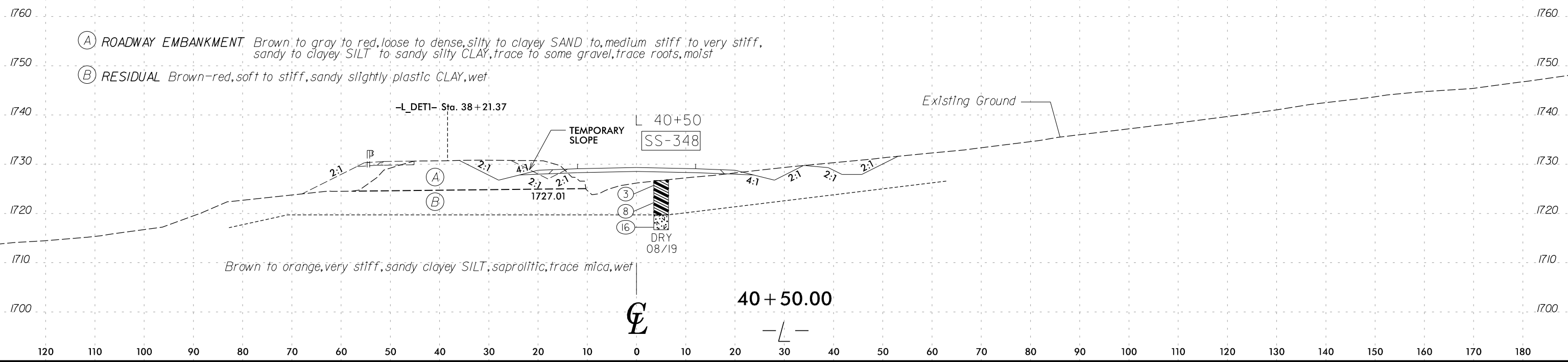
36 + 50.00

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42 + 50.00

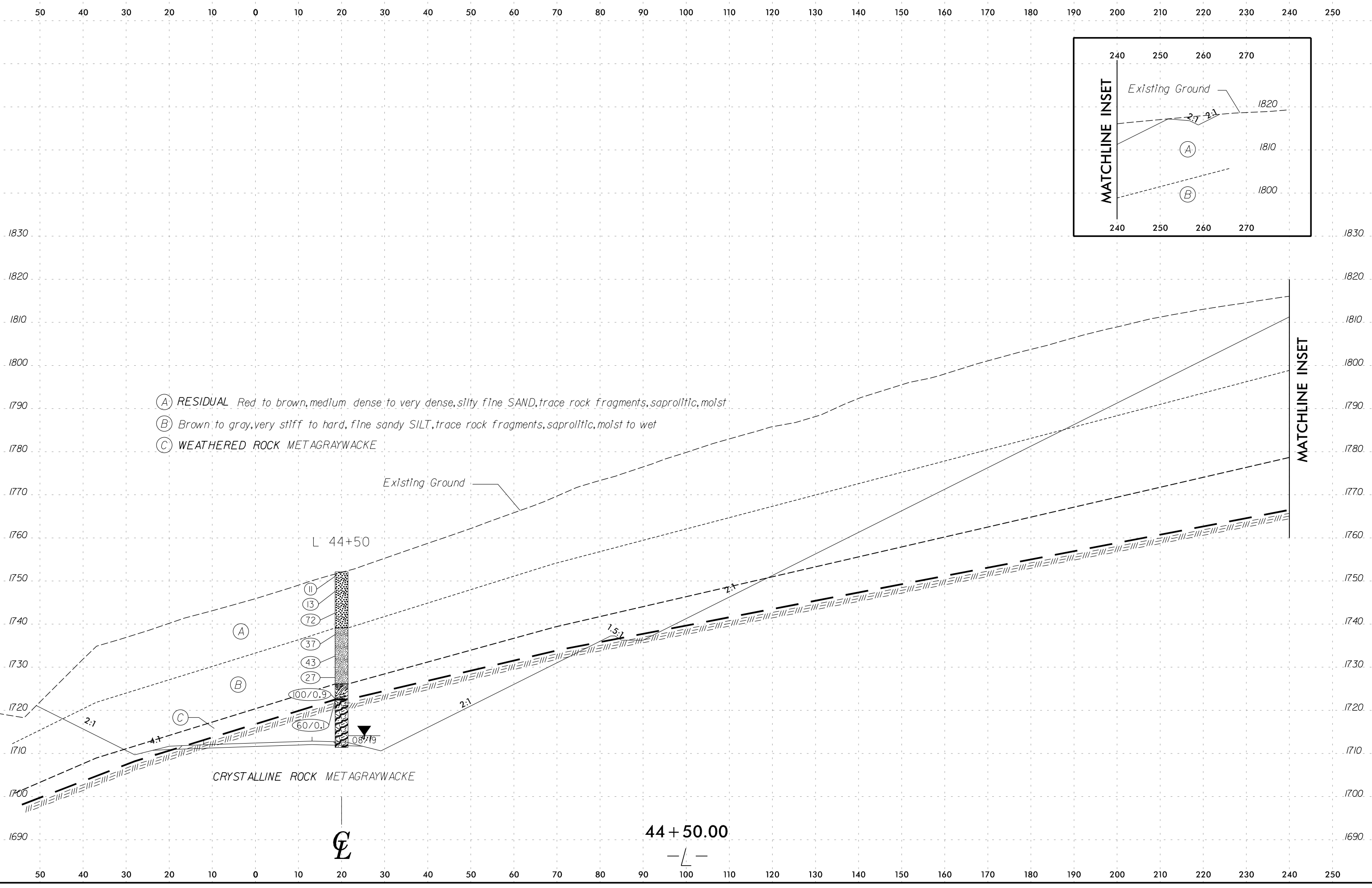
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-348	40+50	5' RT	0.0-1.5	A-6 (6)	37	14	11	35	21	33	93	88	56.7	25.3	-



40 + 50.00

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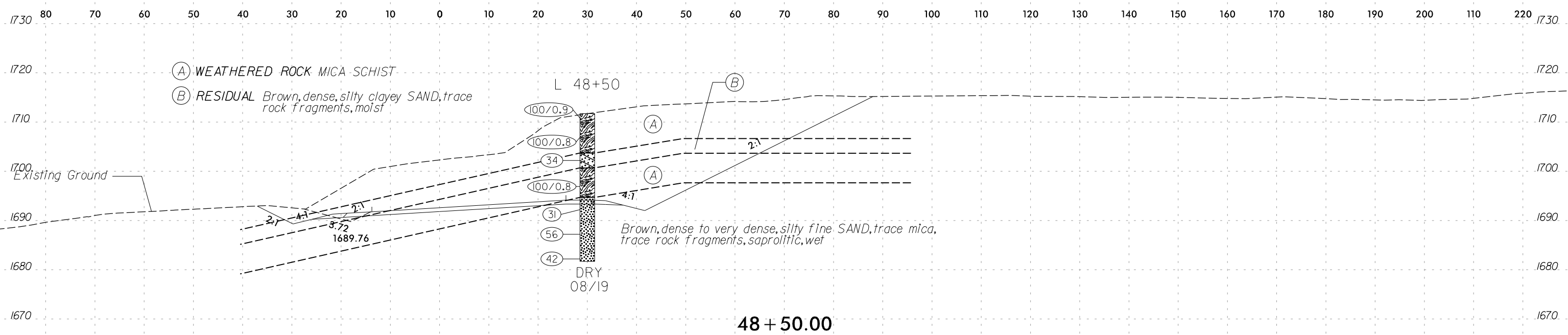
- (A) RESIDUAL Red to brown, medium dense to very dense, silty fine SAND, trace rock fragments, saprolitic, moist
- (B) Brown to gray, very stiff to hard, fine sandy SILT, trace rock fragments, saprolitic, moist to wet
- (C) WEATHERED ROCK METAGRAYWACKE

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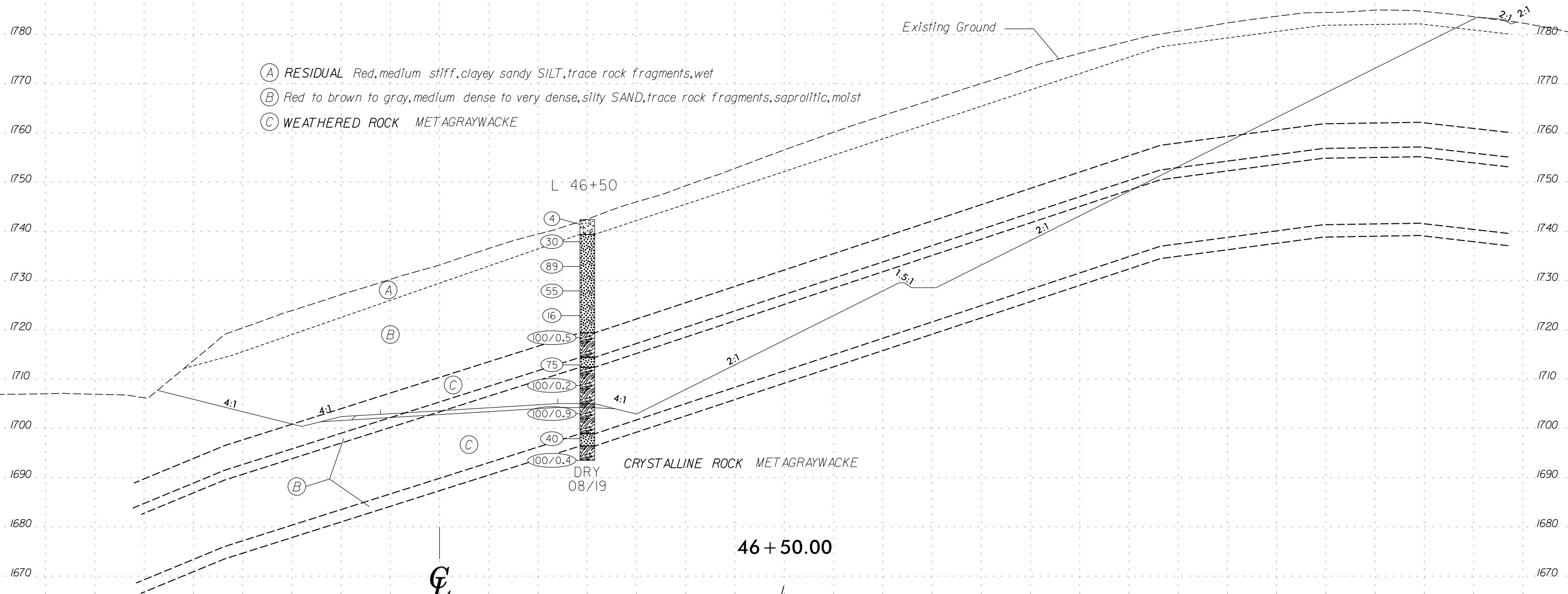
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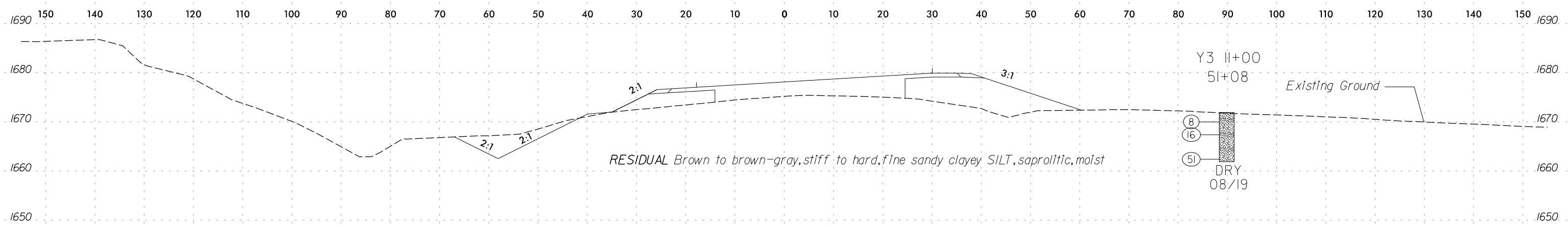


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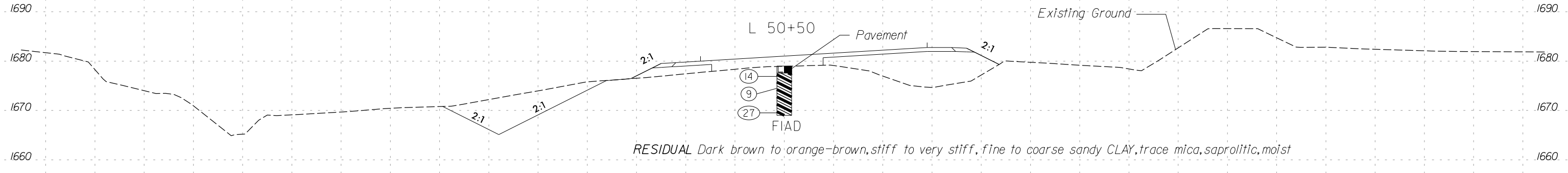


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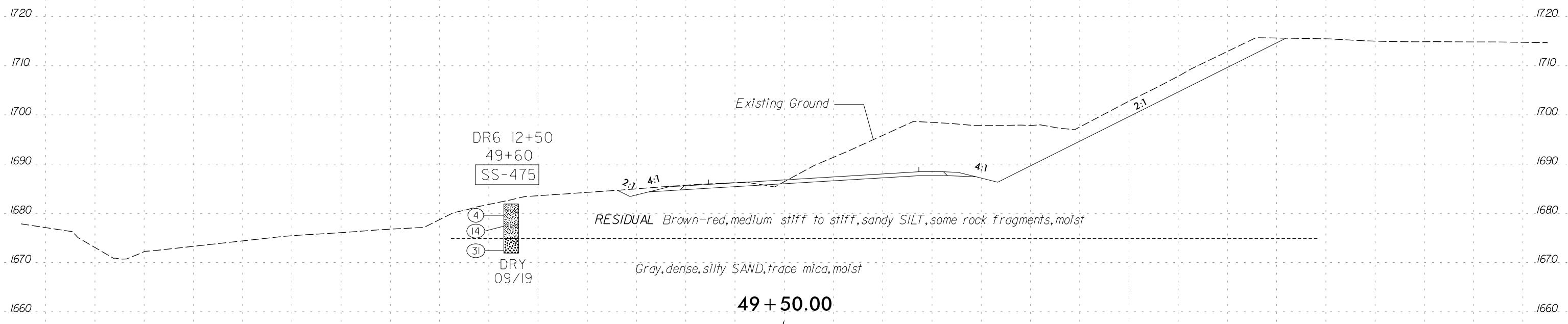


51 + 00.00



50 + 50.00

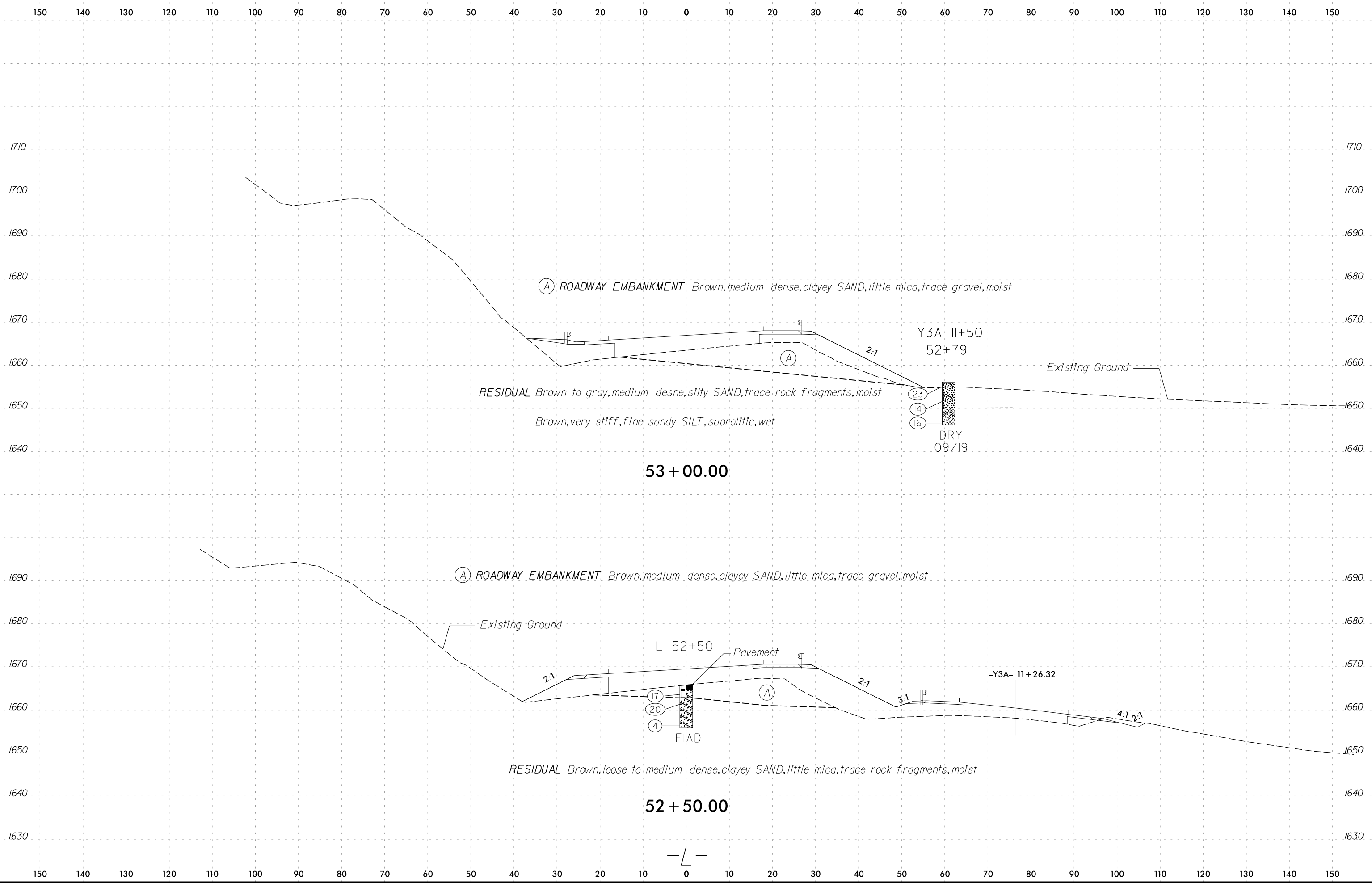
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-475	49+60	55' LT	1.3-2.8	A-4 (4)	32	10	13	32	21	34	97	91	58.5	18	-



49 + 50.00

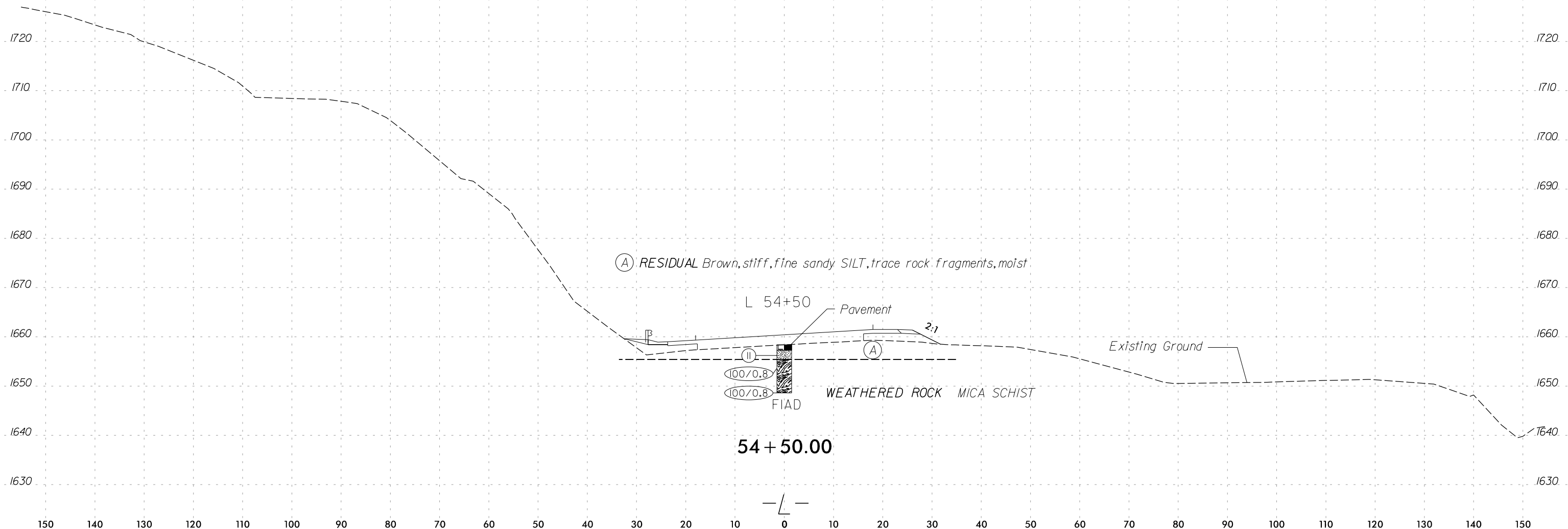
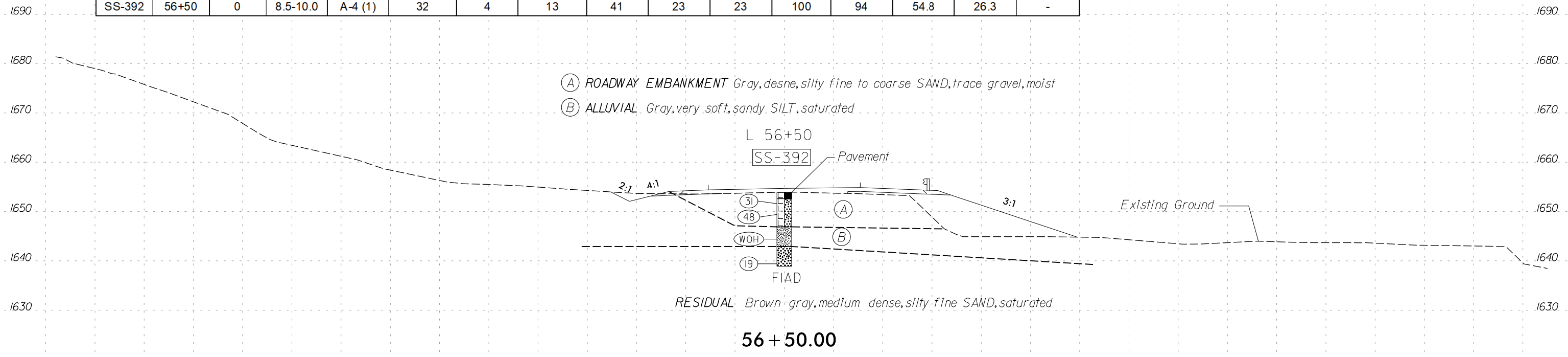
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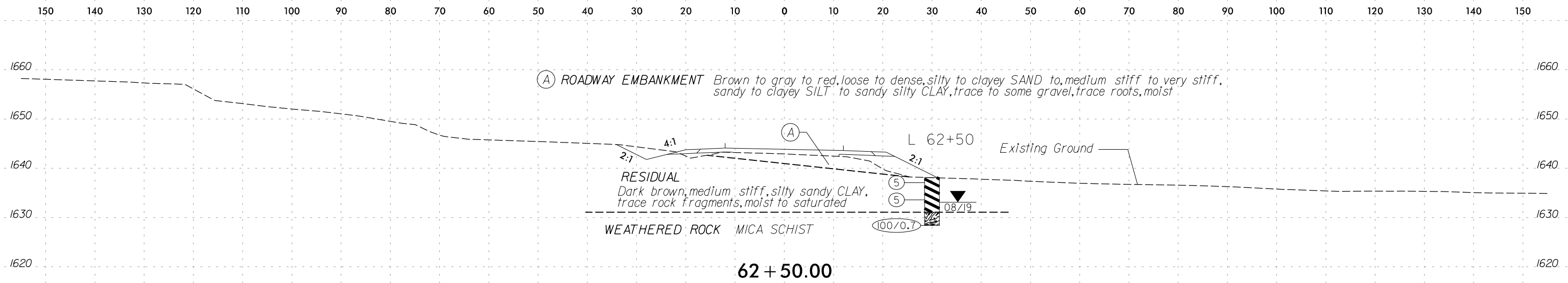


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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-392	56+50	0	8.5-10.0	A-4 (1)	32	4	13	41	23	23	100	94	54.8	26.3	-



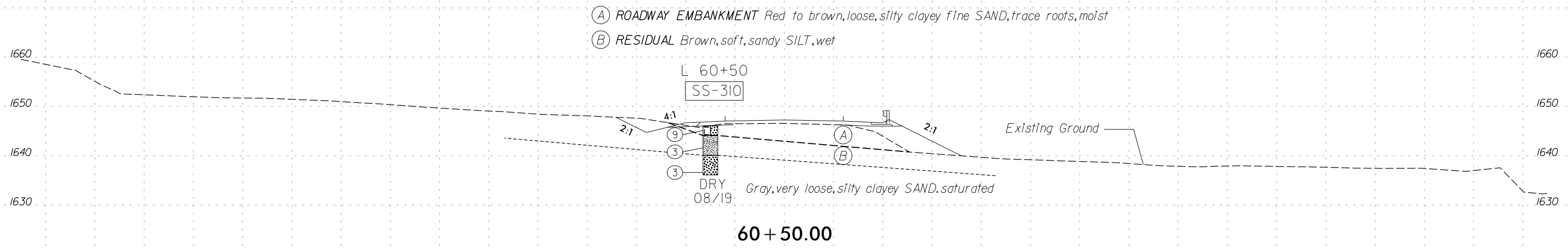
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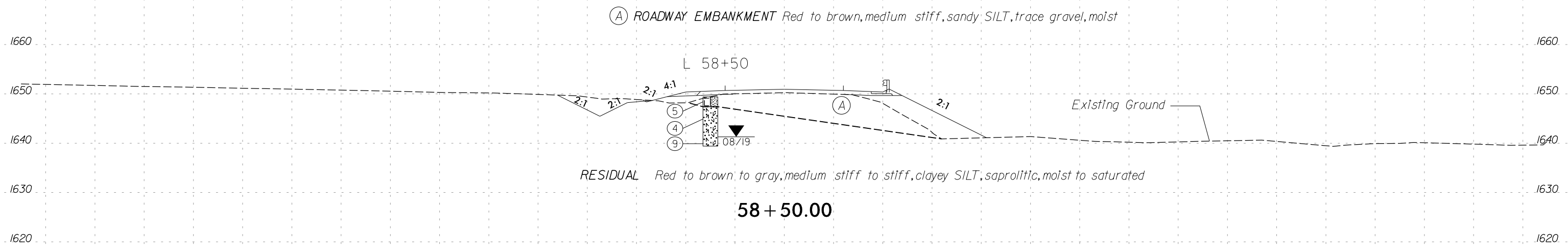
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**SOIL TEST RESULTS**

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-310	60+50	15' LT	3.5-5.0	A-4 (0)	25	6	16	48	11	25	98	92	43.4	19.5	-



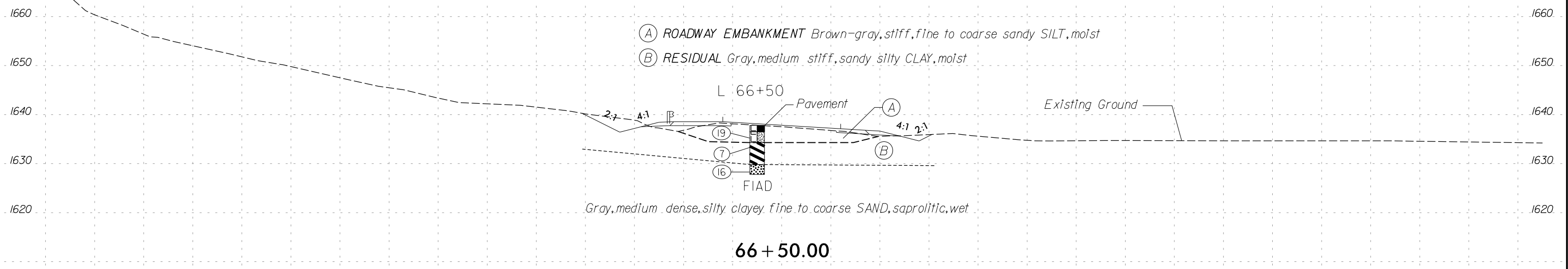
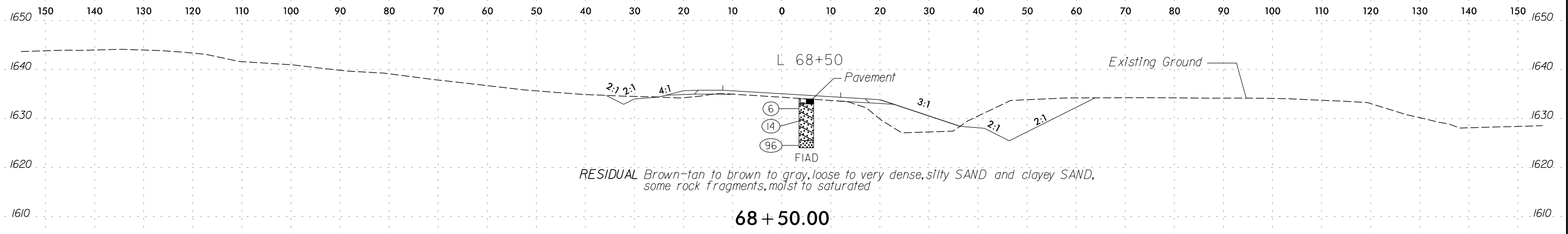
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58 + 50.00

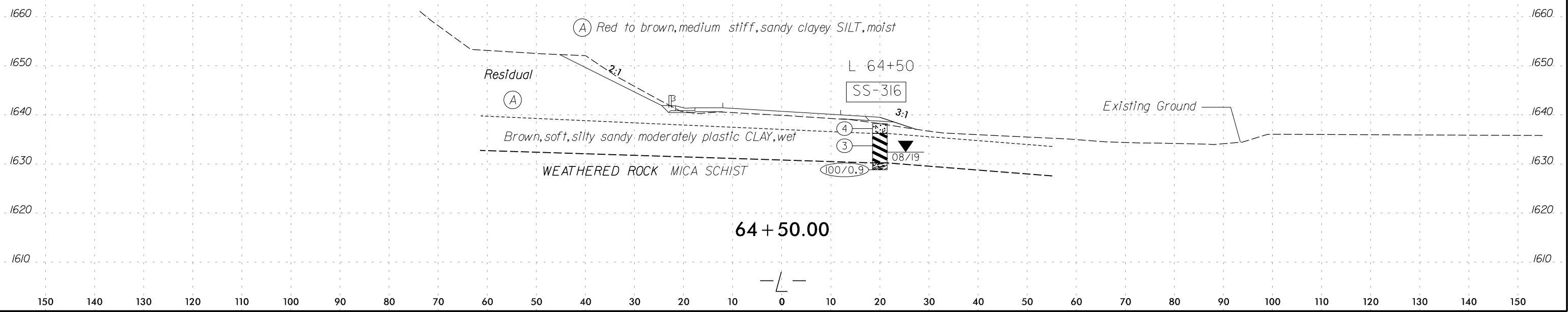
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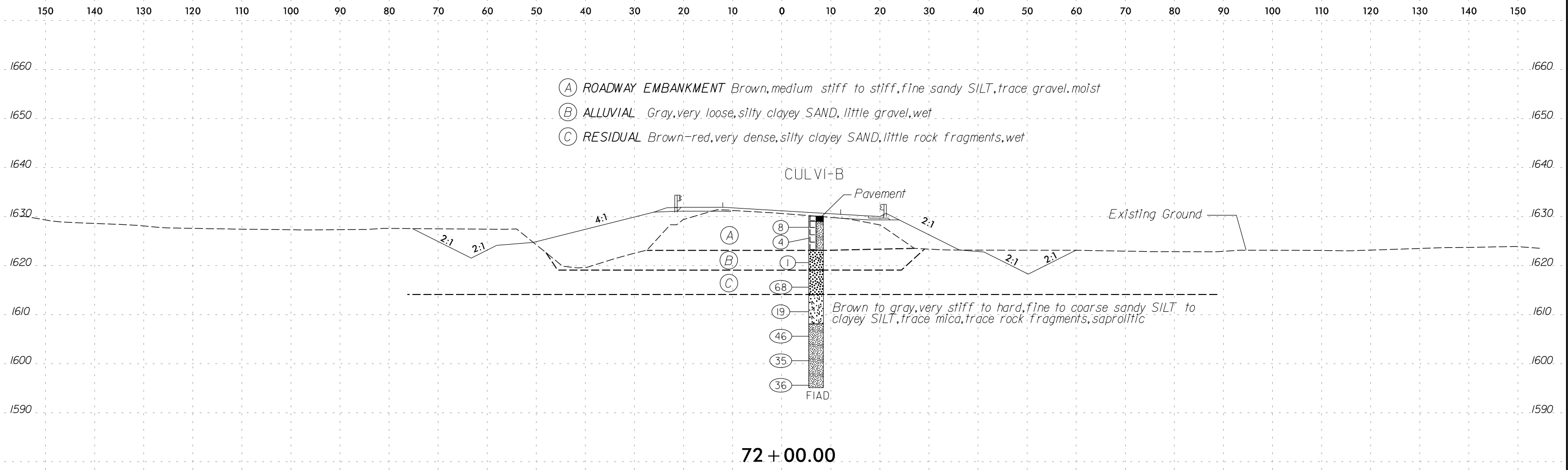


**SOIL TEST RESULTS**

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-316	64+50	20' RT	3.5-5.0	A-7-6 (13)	46	19	6	31	24	39	100	98	70.2	30.7	-

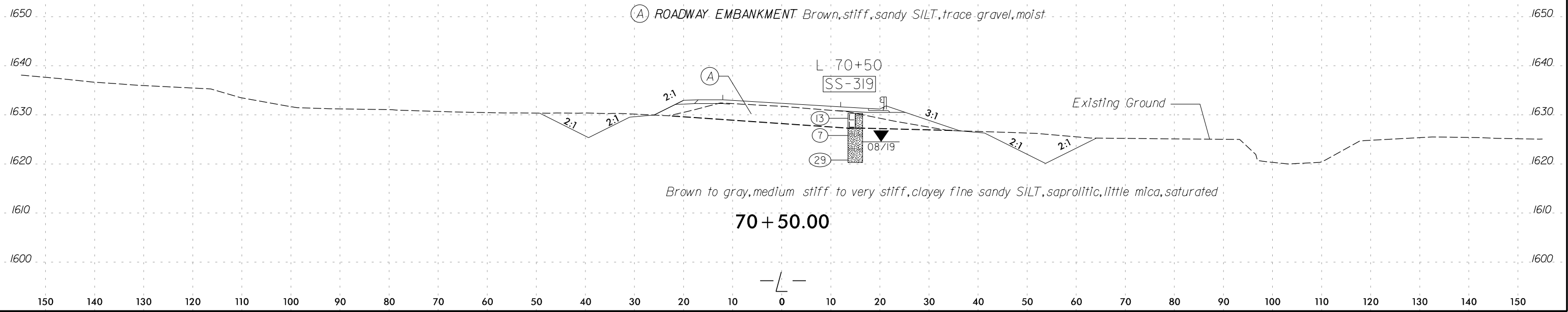


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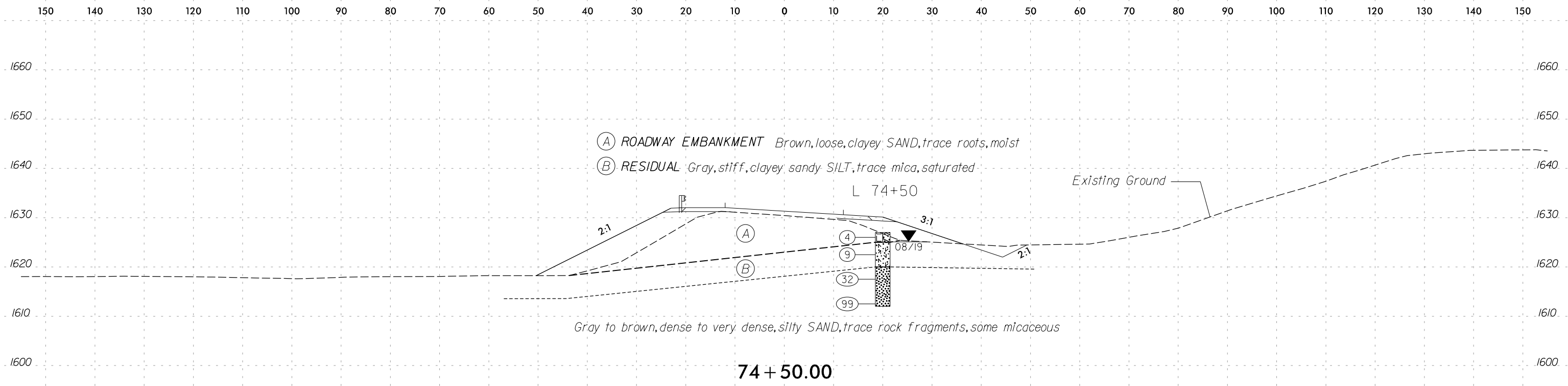


**SOIL TEST RESULTS**

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-319	70+50	50' RT	3.5-5.0	A-4 (0)	27	5	8	51	17	24	100	98	51.5	18.3	-

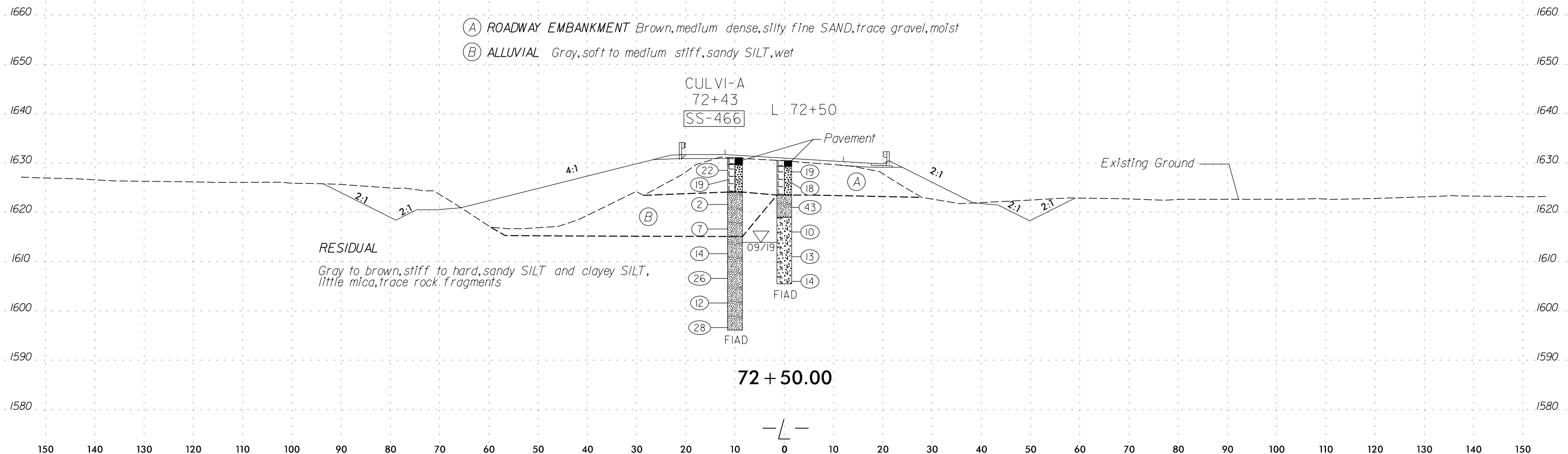


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**SOIL TEST RESULTS**

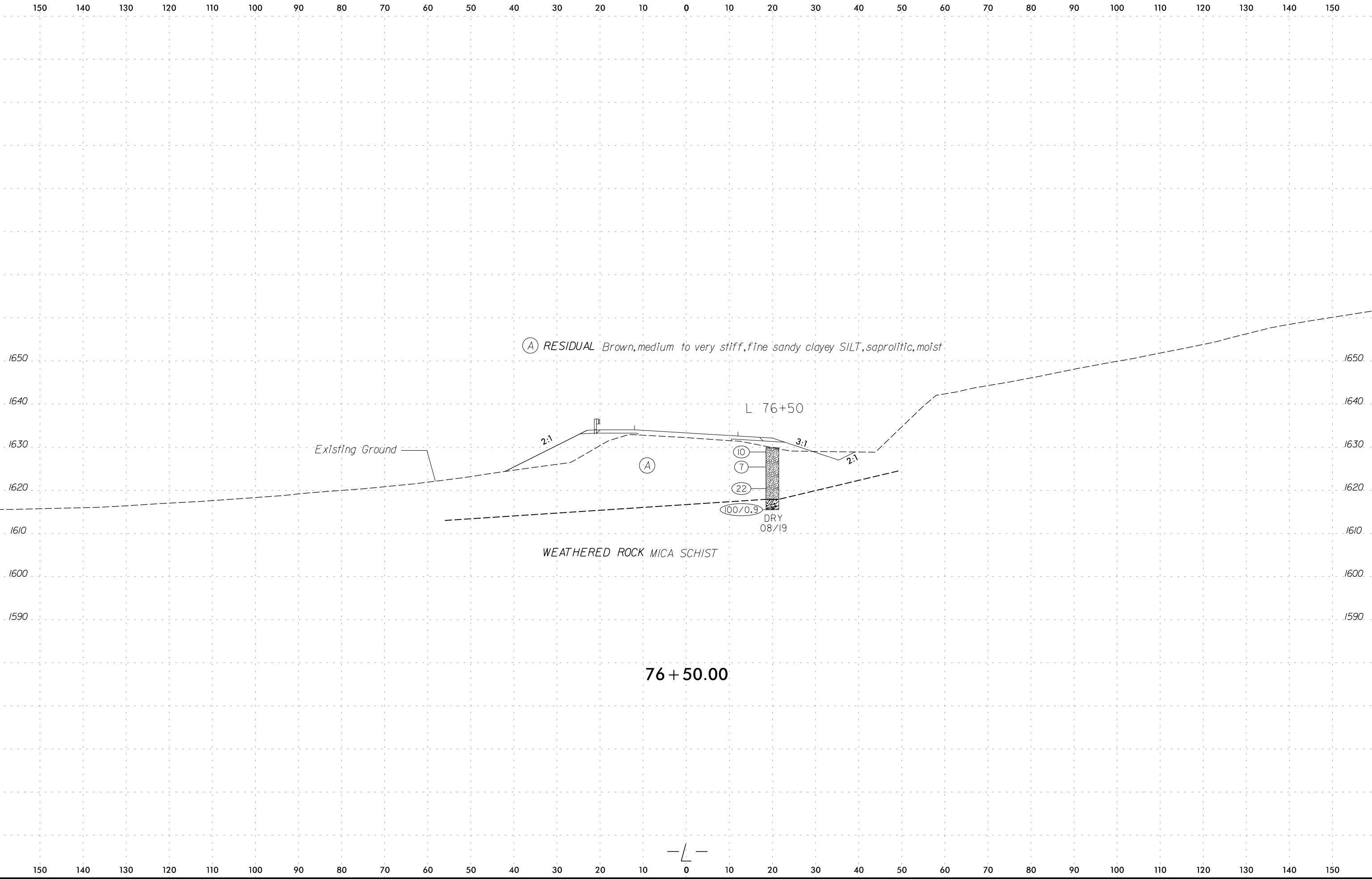
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-466	72+43	10' LT	8.5-10.0	A-4 (3)	31	8	8	36	22	34	99	97	63.5	29.2	-



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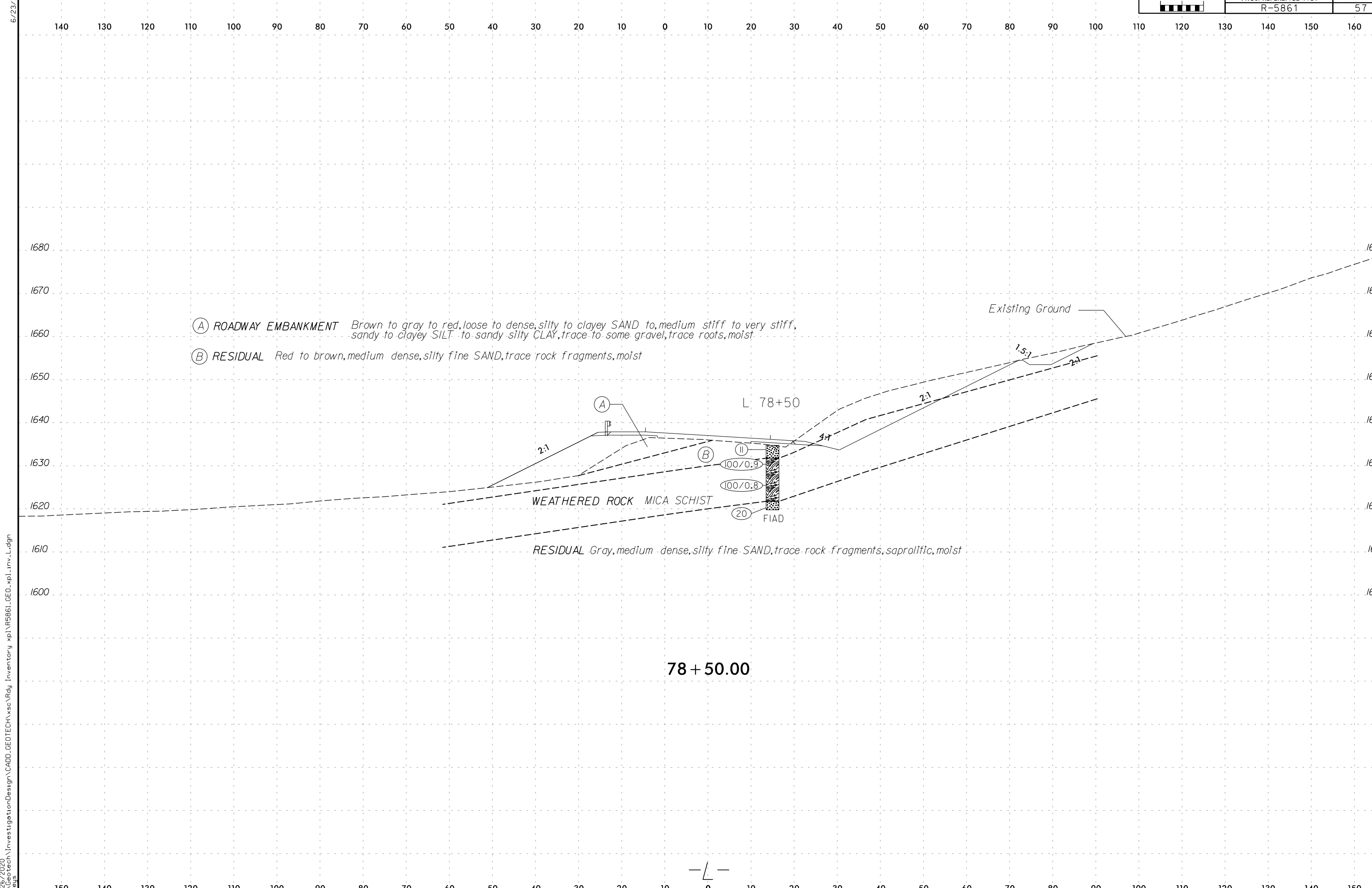


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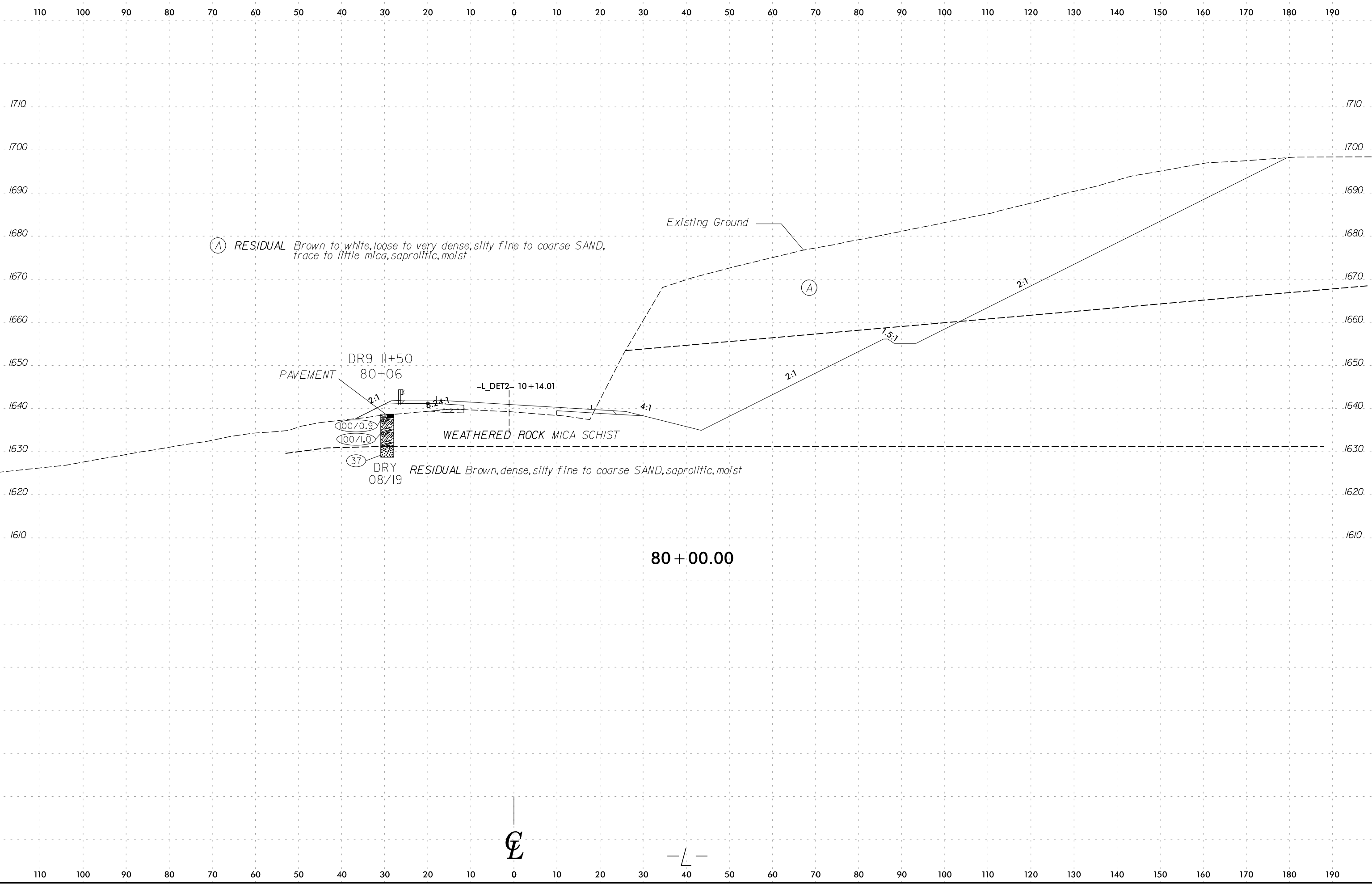
- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Red to brown, medium dense, silty fine SAND, trace rock fragments, moist*

WEATHERED ROCK MICA SCHIST

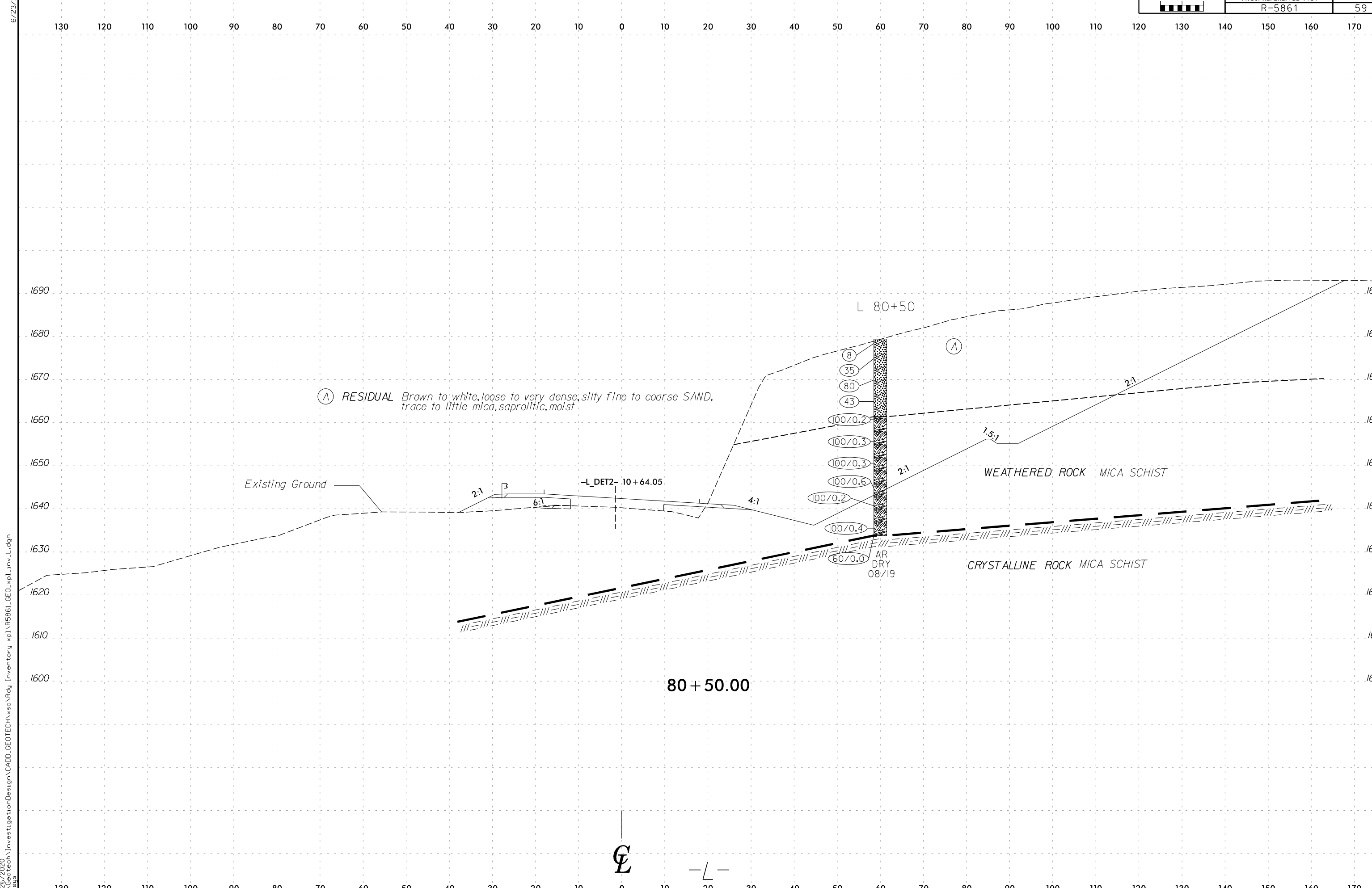
RESIDUAL *Gray, medium dense, silty fine SAND, trace rock fragments, saprolitic, moist*

78 + 50.00

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(A) RESIDUAL Brown to white, loose to very dense, silty fine to coarse SAND, trace to little mica, saprolitic, moist

Existing Ground

-L\_DET2- 10 + 64.05

L 80+50

WEATHERED ROCK MICA SCHIST

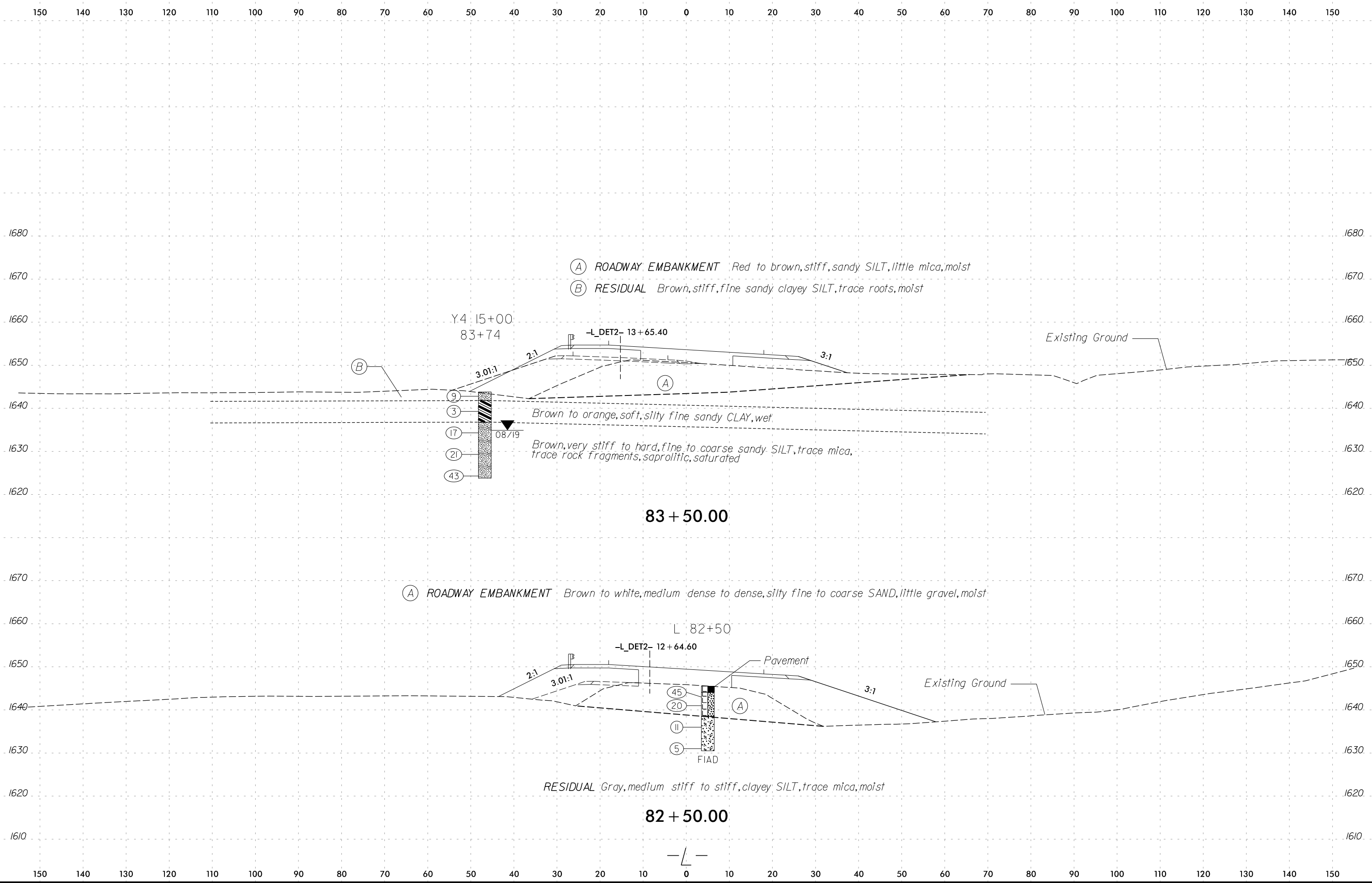
CRYSTALLINE ROCK MICA SCHIST

AR  
DRY  
08/19

80 + 50.00

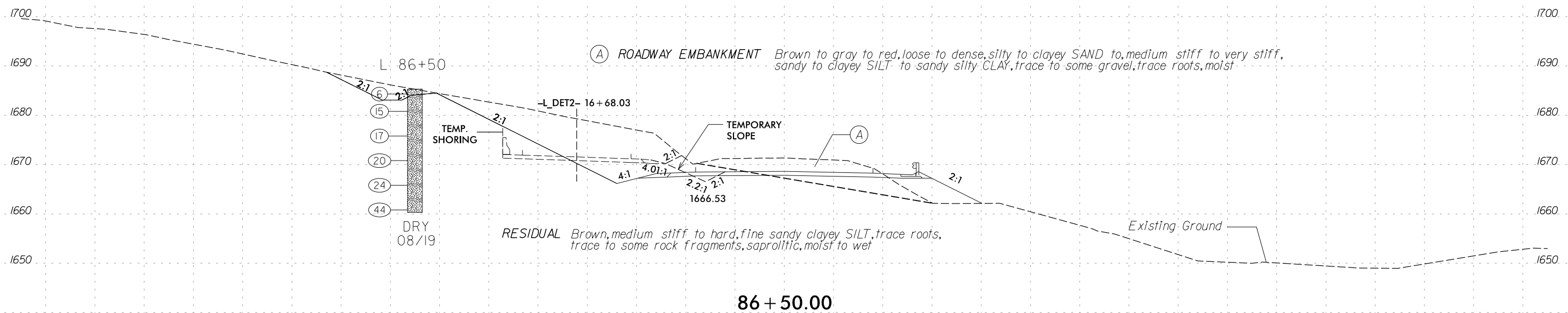


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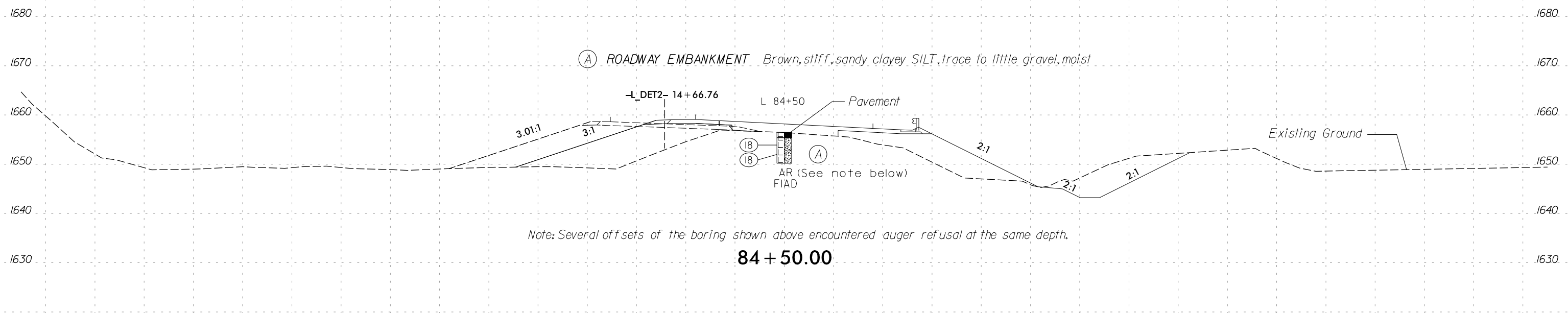


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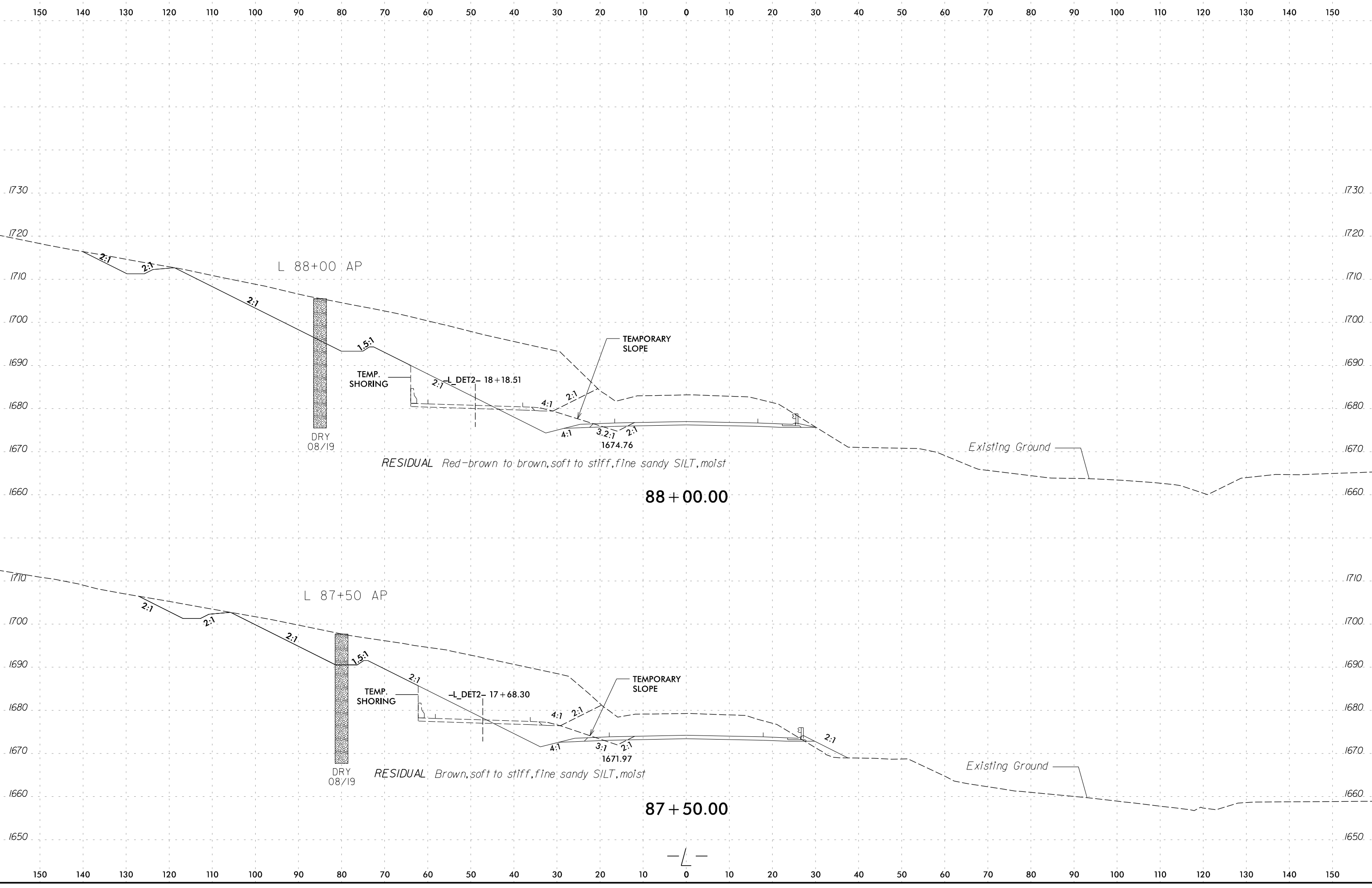
86 + 50.00



84 + 50.00

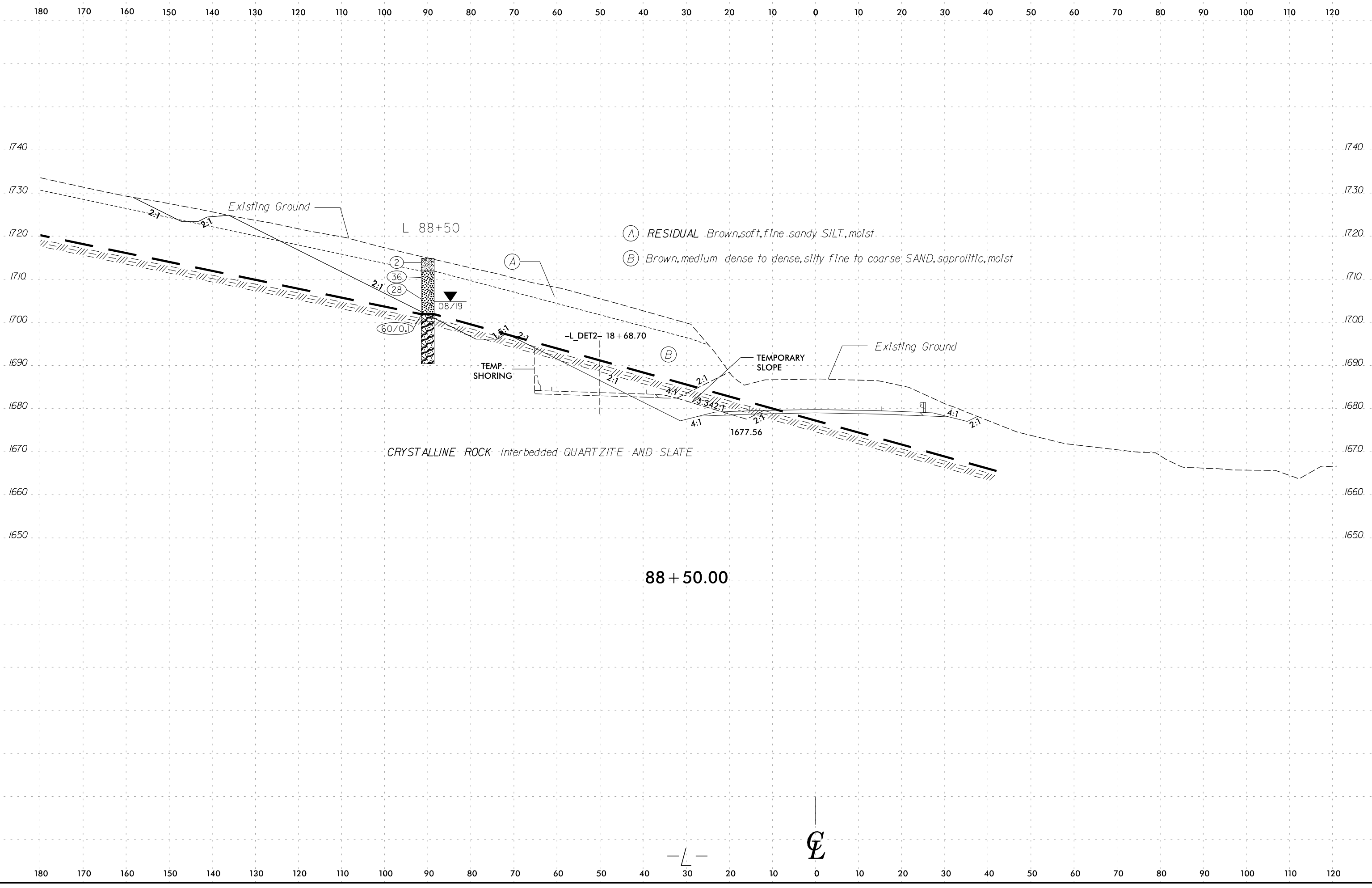
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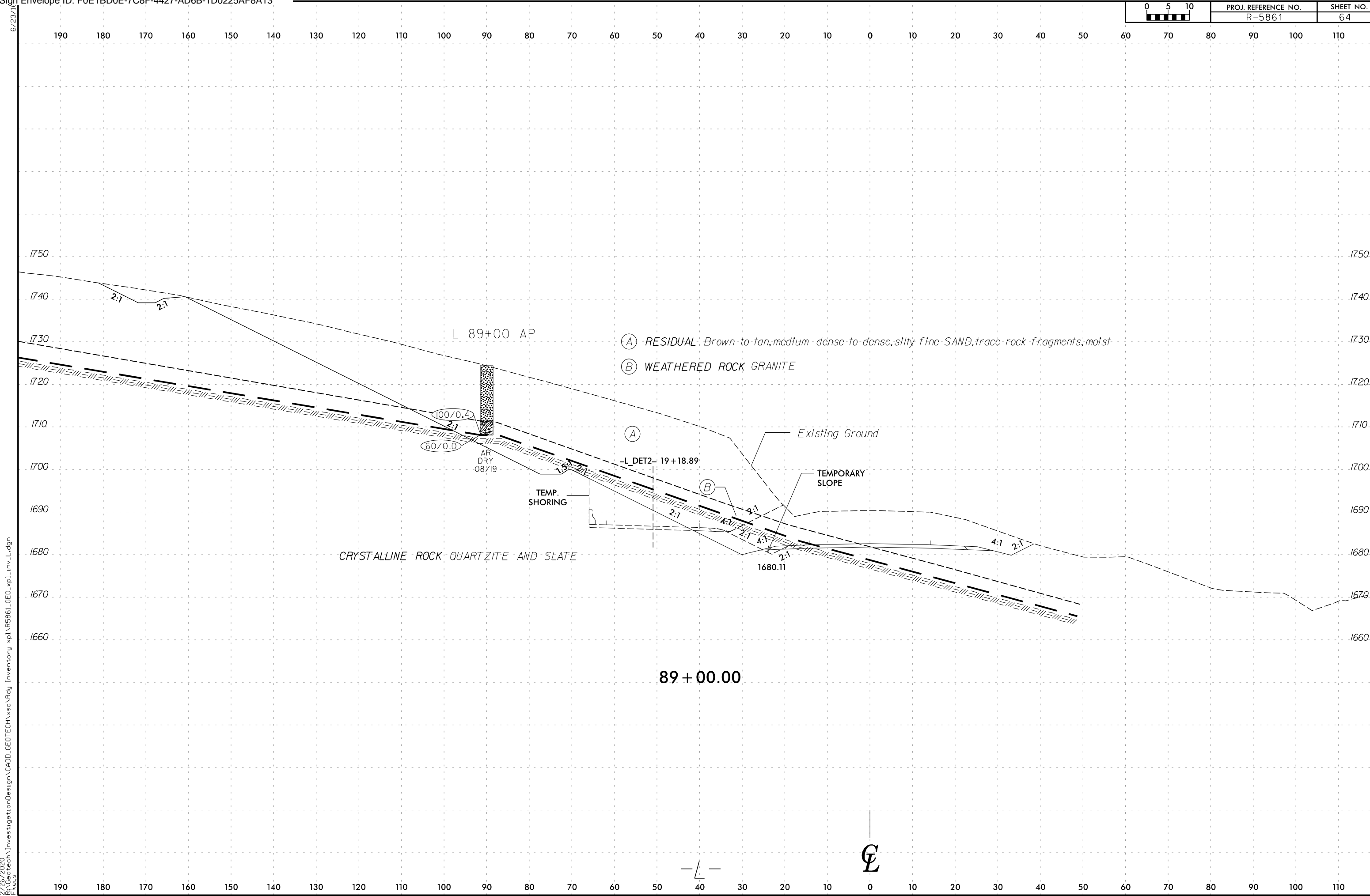


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- (A) RESIDUAL: Brown to tan, medium dense to dense, silty fine SAND, trace rock fragments, moist
- (B) WEATHERED ROCK GRANITE

L 89+00 AP

100/0.4

60/0.0

AR DRY 08/19

-L DET2- 19+18.89

Existing Ground

TEMPORARY SLOPE

TEMP. SHORING

CRYSTALLINE ROCK QUARTZITE AND SLATE

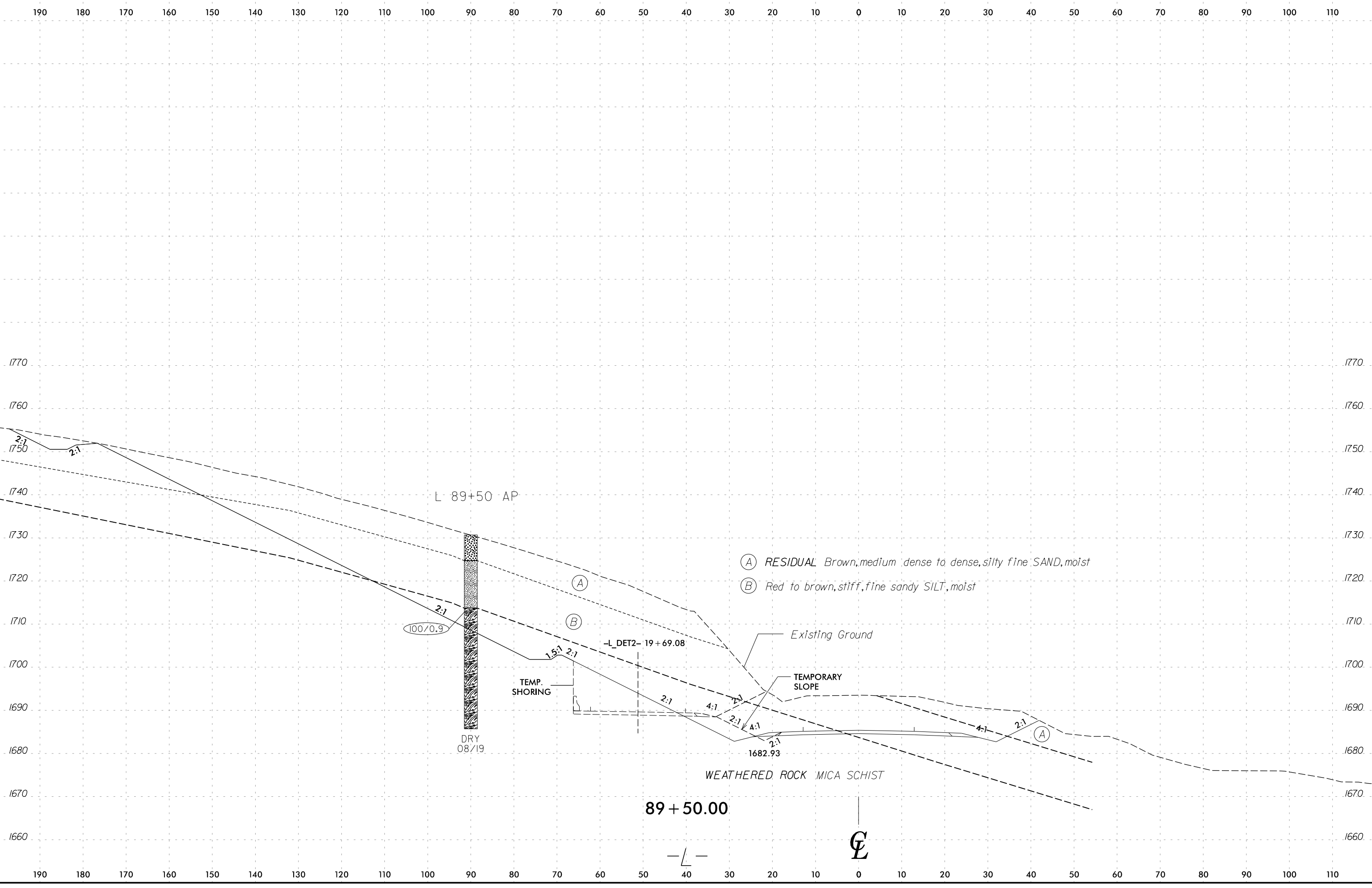
1680.11

89 + 00.00

Ⓞ

-L-

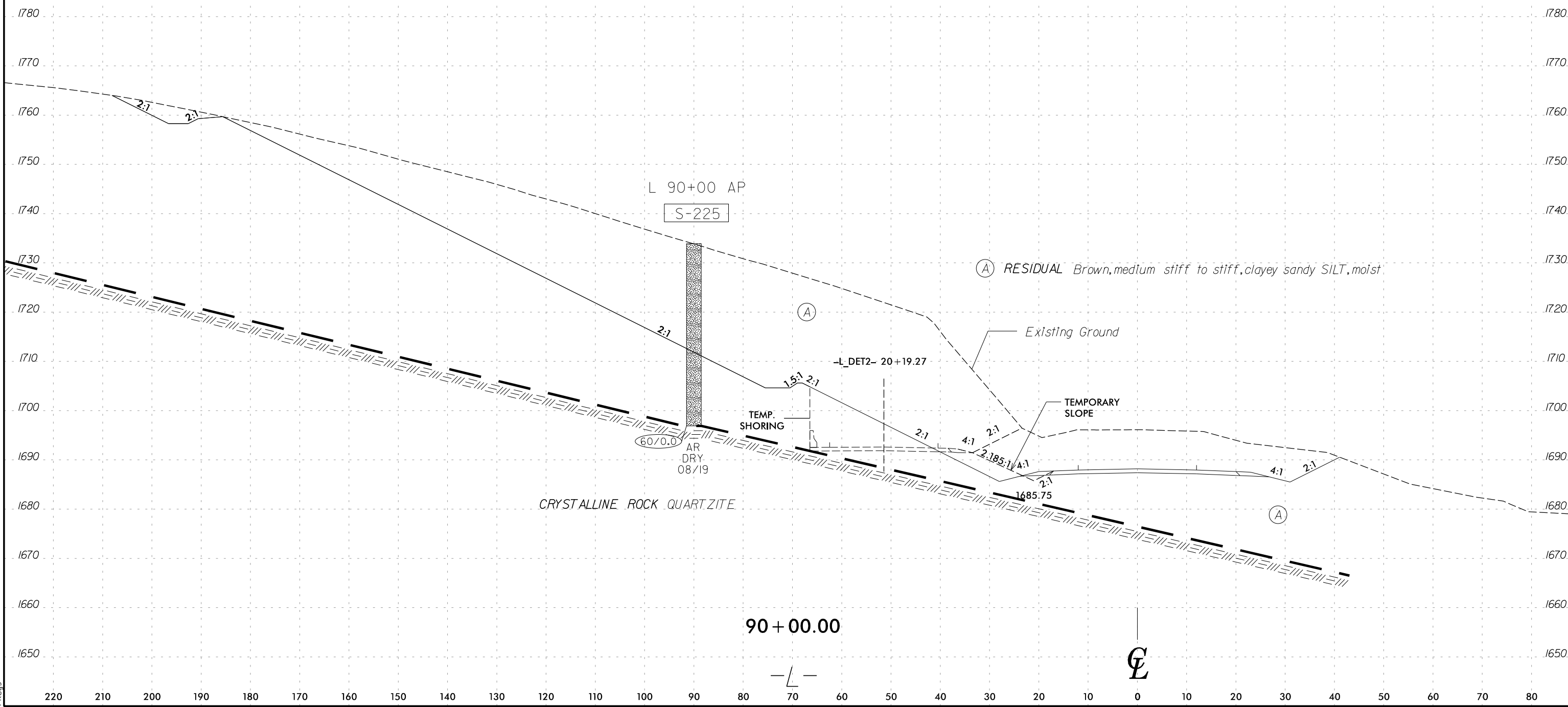
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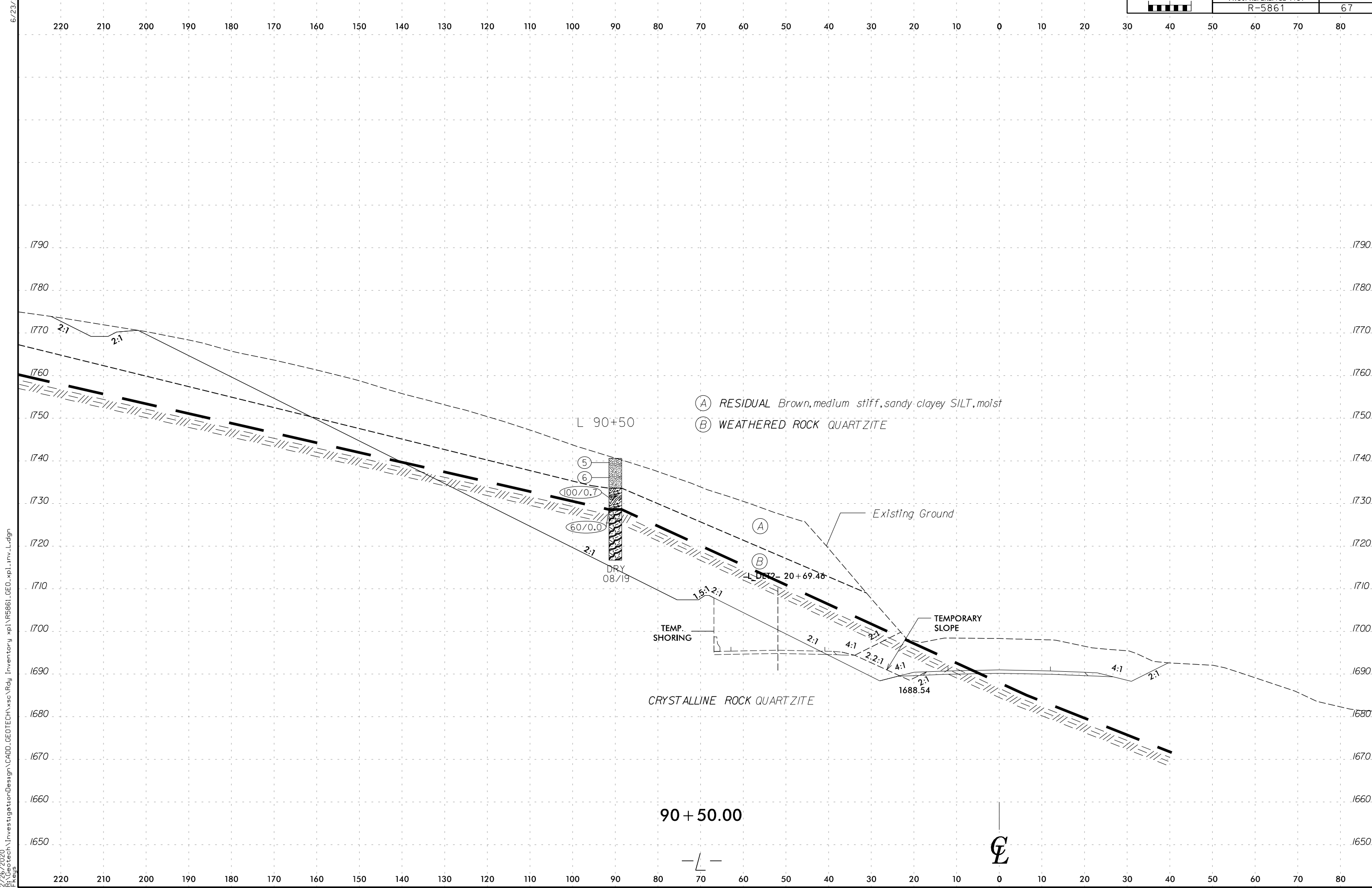
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
S-225	90+00	90' LT	1.0-8.5	A-4 (0)	29	5	10	51	17	22	96	92	46.2	ND	-



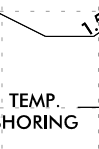
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- (A) RESIDUAL Brown, medium stiff, sandy clayey SILT, moist
- (B) WEATHERED ROCK QUARTZITE

L 90+50

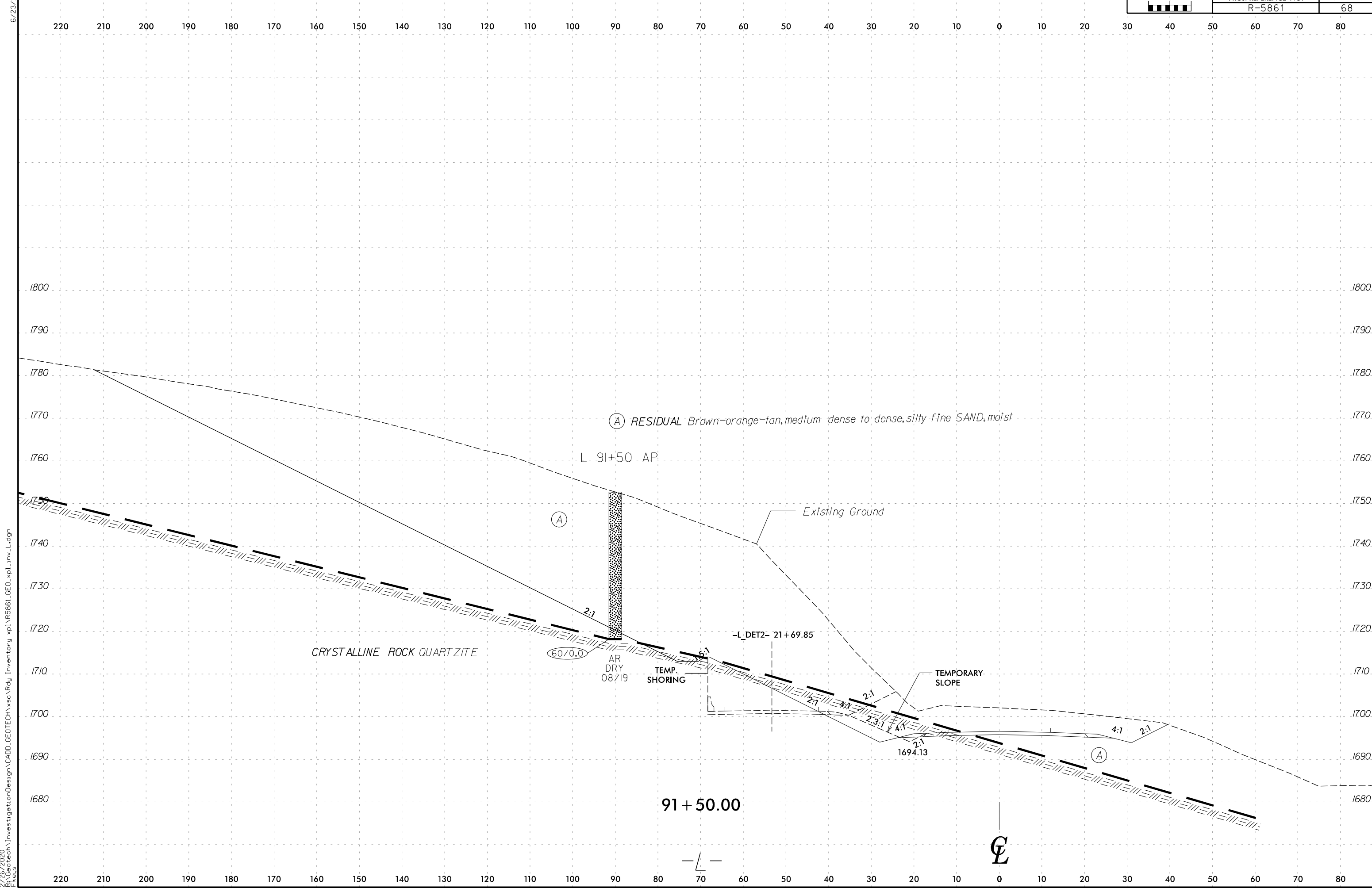


CRYSTALLINE ROCK QUARTZITE

90 + 50.00



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(A) RESIDUAL Brown-orange-tan, medium dense to dense, silty fine SAND, moist

L 91+50 AP

Existing Ground

CRYSTALLINE ROCK QUARTZITE

60/0.0

AR DRY 08/19

TEMP. SHORING

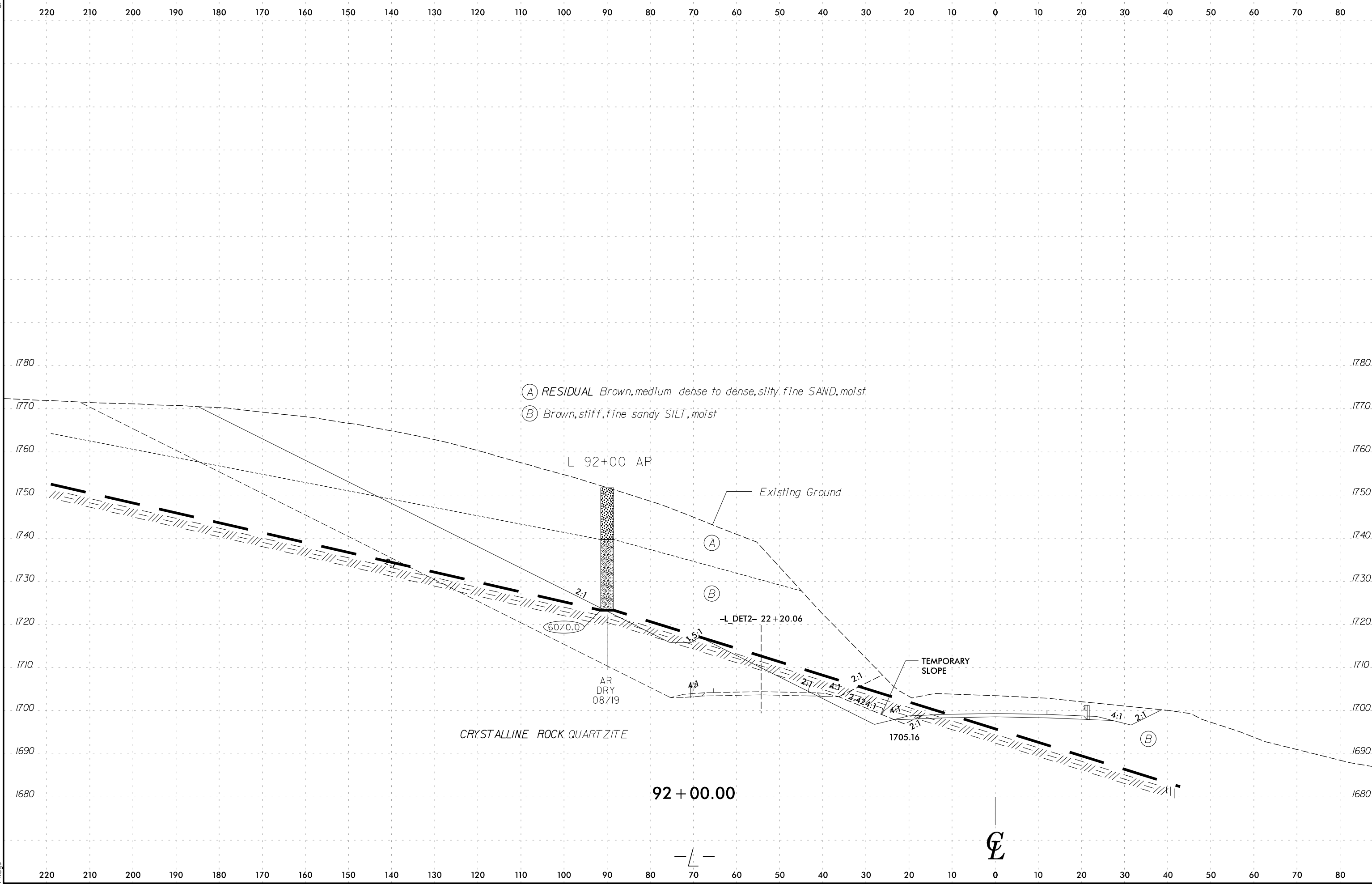
-L\_DET2- 21+69.85

TEMPORARY SLOPE

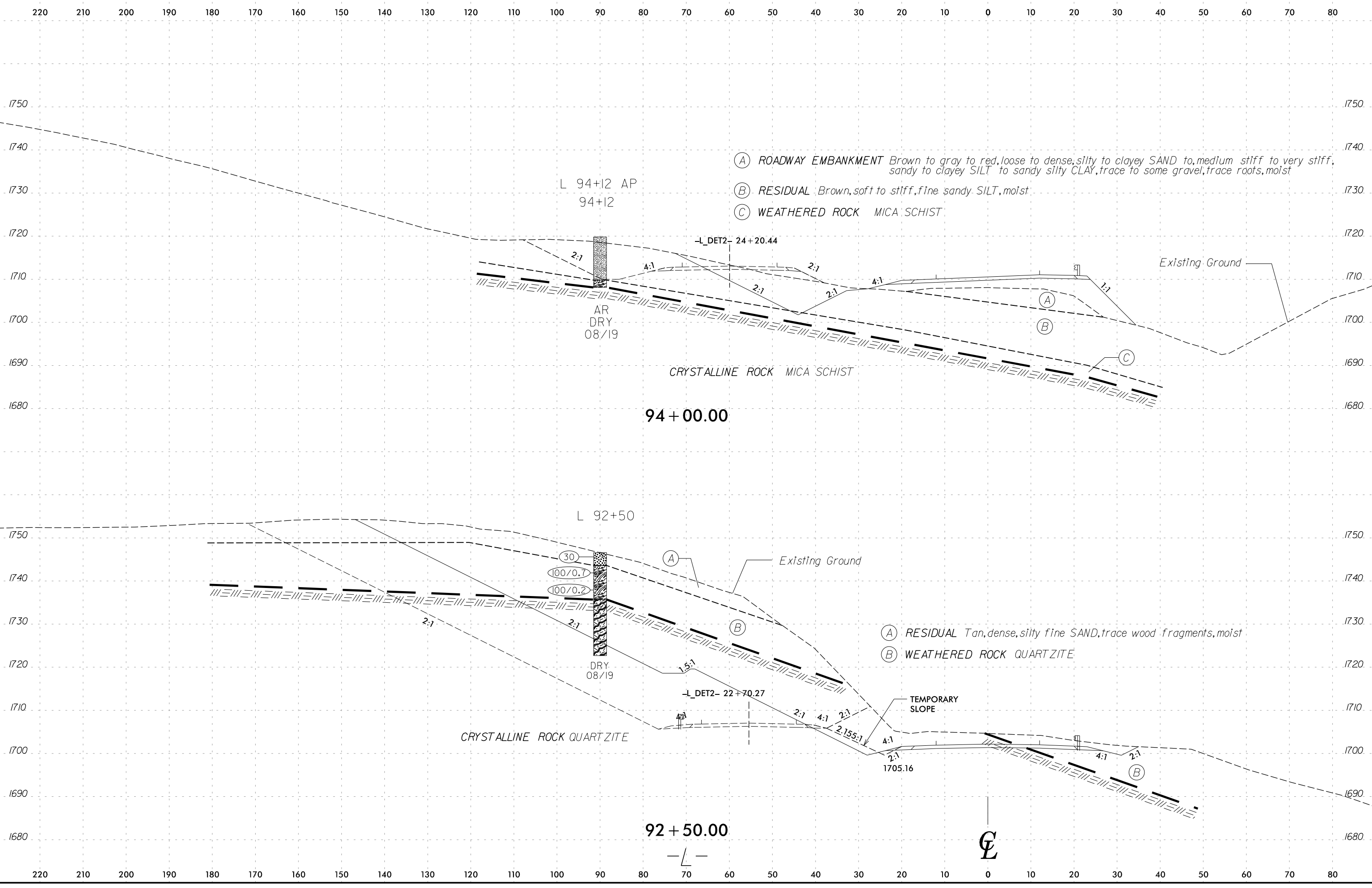
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91+50.00

CL



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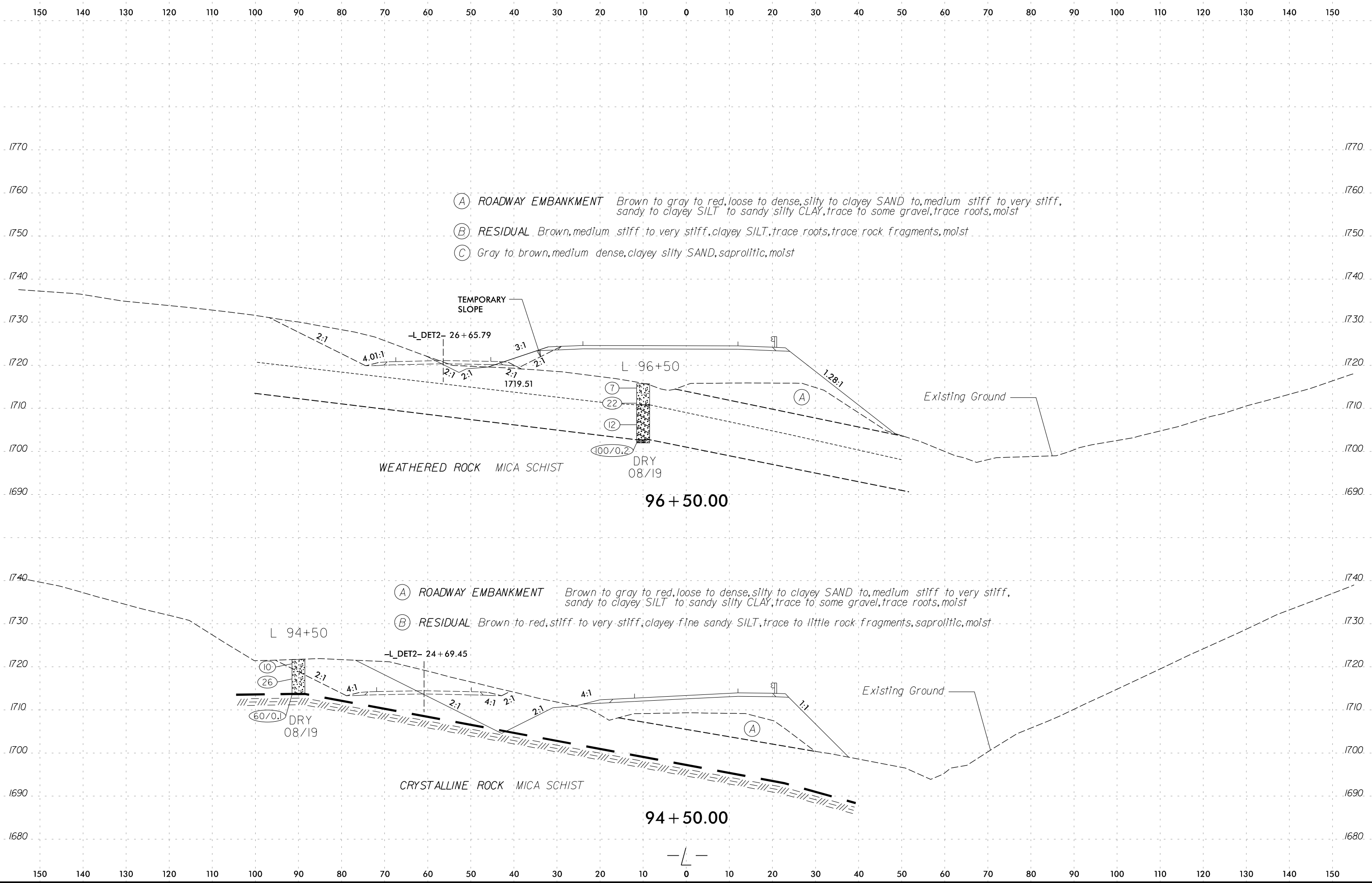


- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown, soft to stiff, fine sandy SILT, moist*
- (C) WEATHERED ROCK *MICA SCHIST*

- (A) RESIDUAL *Tan, dense, silty fine SAND, trace wood fragments, moist*
- (B) WEATHERED ROCK *QUARTZITE*

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- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown, medium stiff to very stiff, clayey SILT, trace roots, trace rock fragments, moist*
- (C) *Gray to brown, medium dense, clayey silty SAND, saprolitic, moist*

WEATHERED ROCK MICA SCHIST

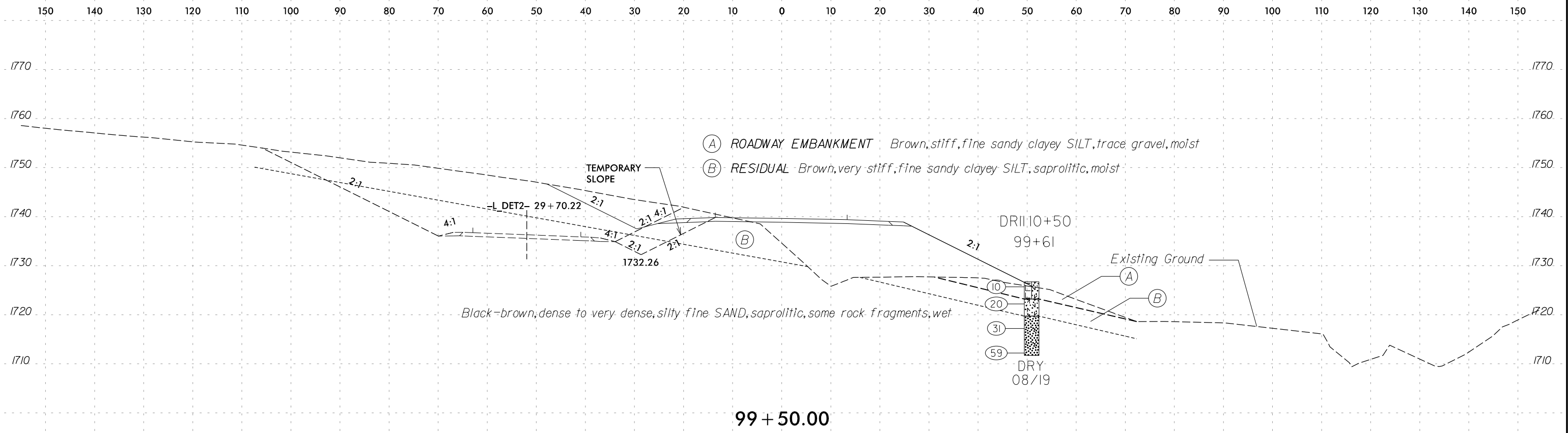
96 + 50.00

- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown to red, stiff to very stiff, clayey fine sandy SILT, trace to little rock fragments, saprolitic, moist*

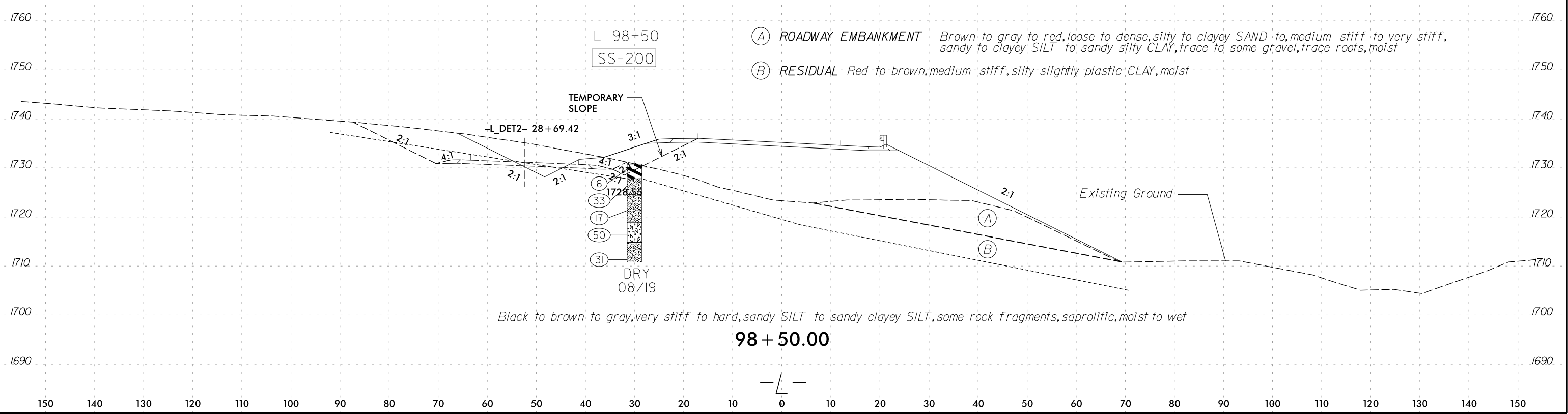
CRYSTALLINE ROCK MICA SCHIST

94 + 50.00

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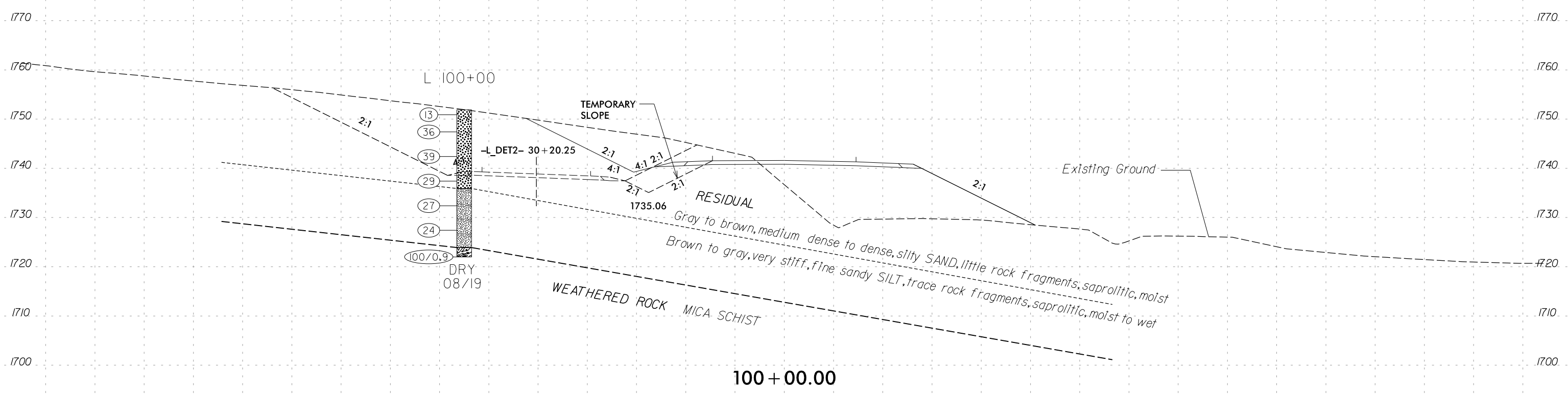
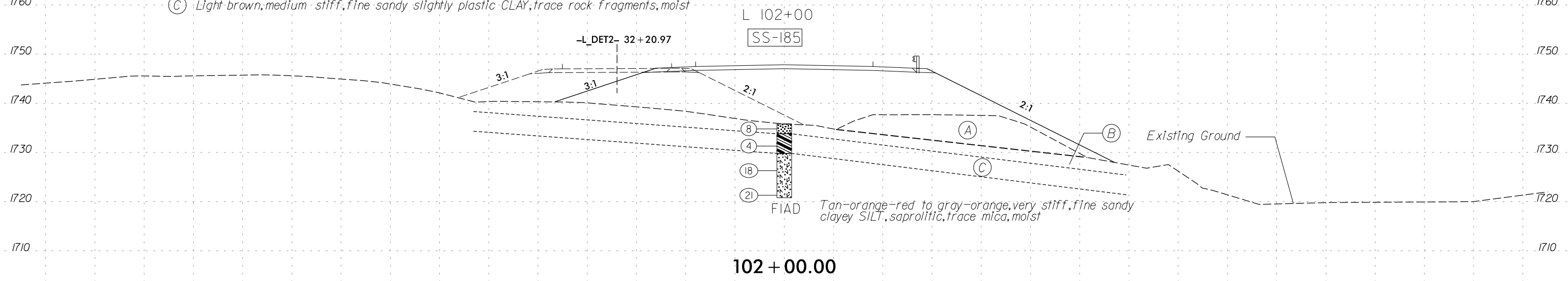
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-200	98+50	30' LT	0.0-1.5	A-7-6 (10)	41	15	17	22	23	38	100	87	68.5	23.2	-



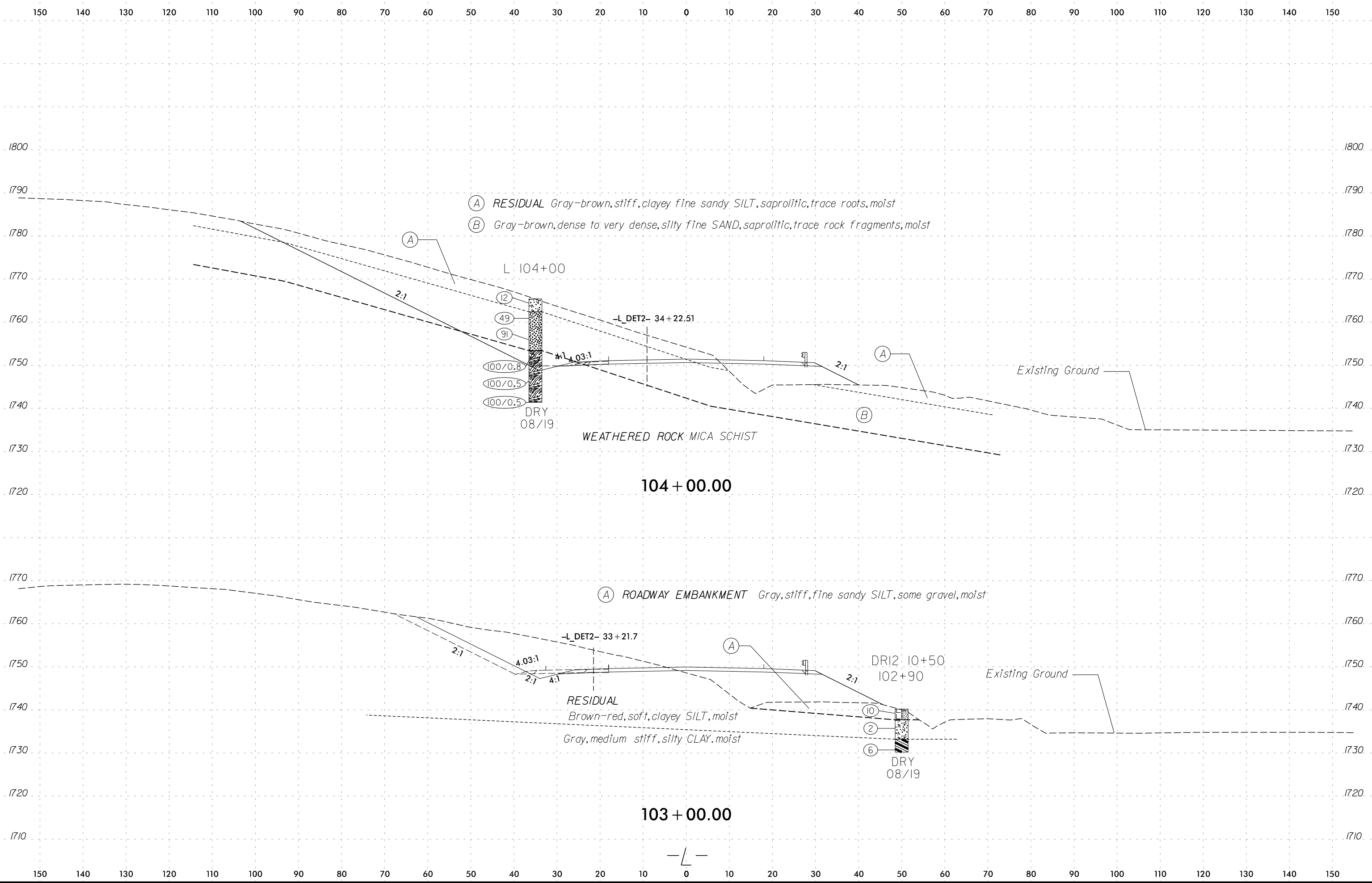
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-185	102+00	0	3.5-5.0	A-6 (9)	37	14	8	20	31	41	93	88	71.8	19.8	-

- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Tan to brown, loose, silty fine SAND, dry*
- (C) *Light brown, medium stiff, fine sandy slightly plastic CLAY, trace rock fragments, moist*



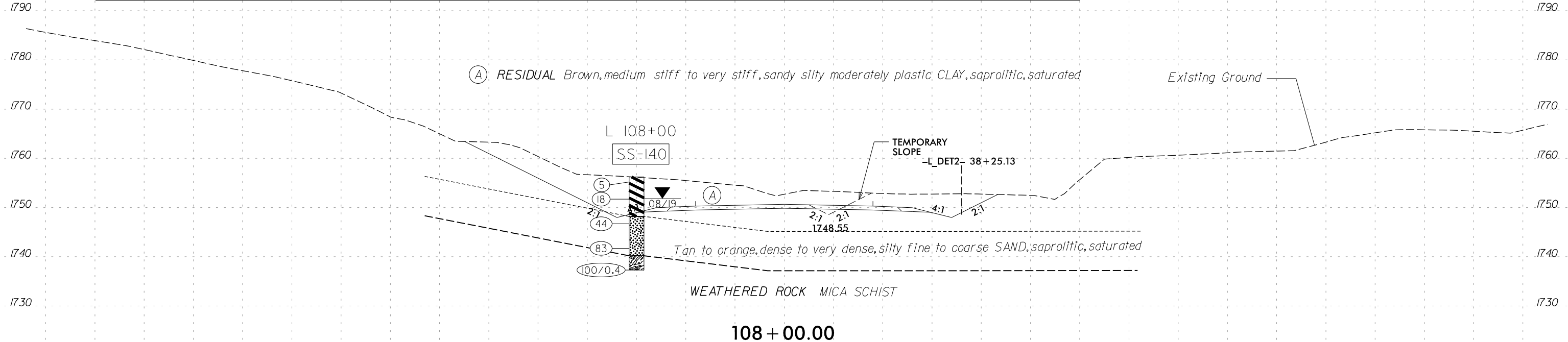
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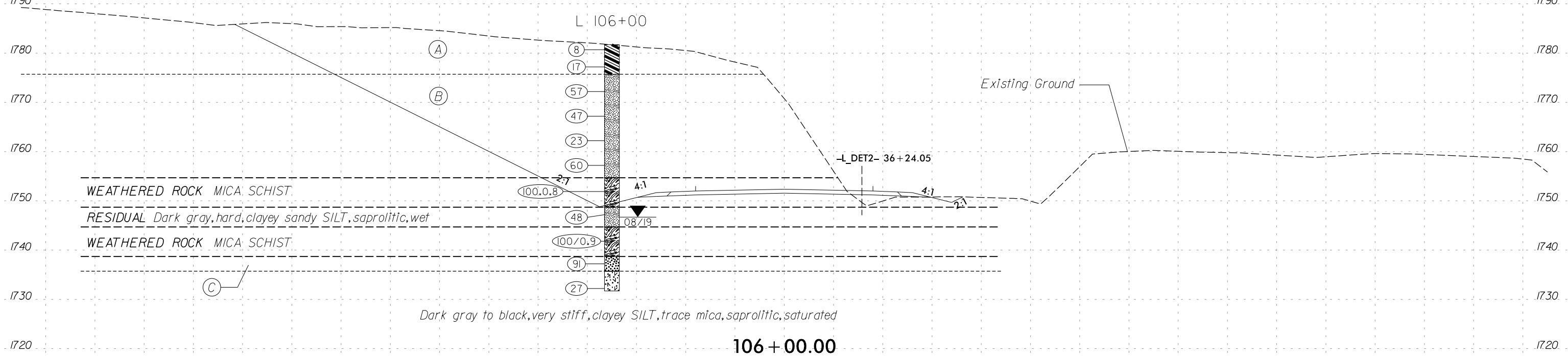
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-140	108+00	30' LT	0.0-1.5	A-7-6 (18)	44	19	2	16	31	51	100	99	86.9	27.4	-

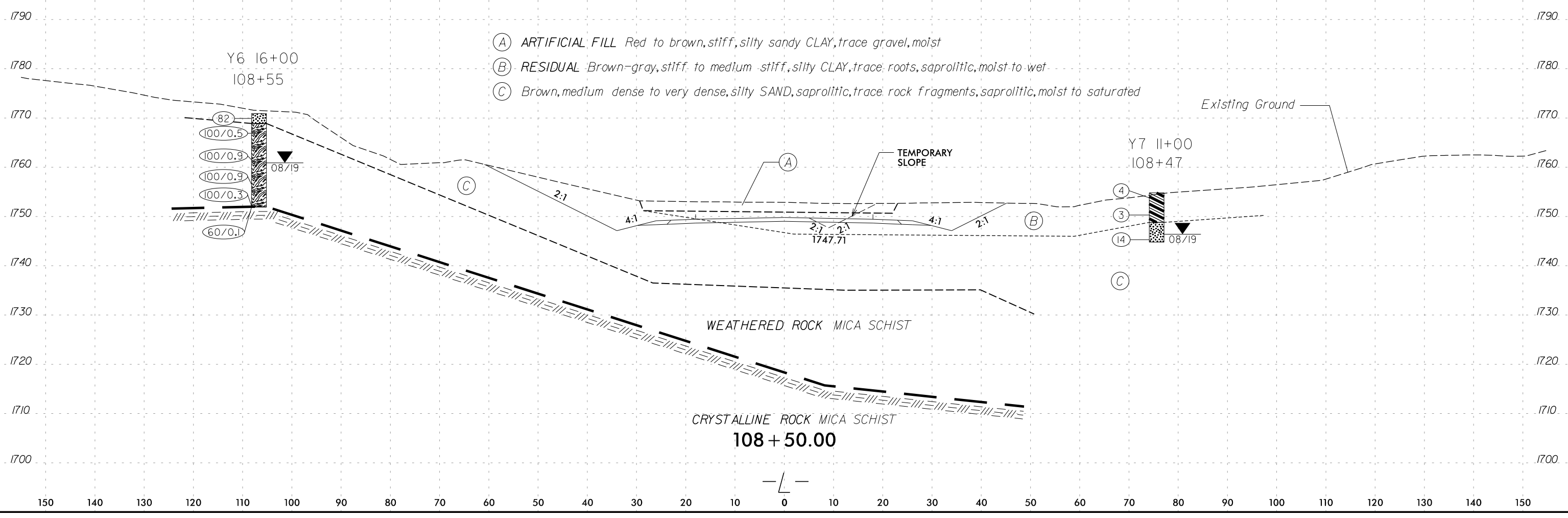
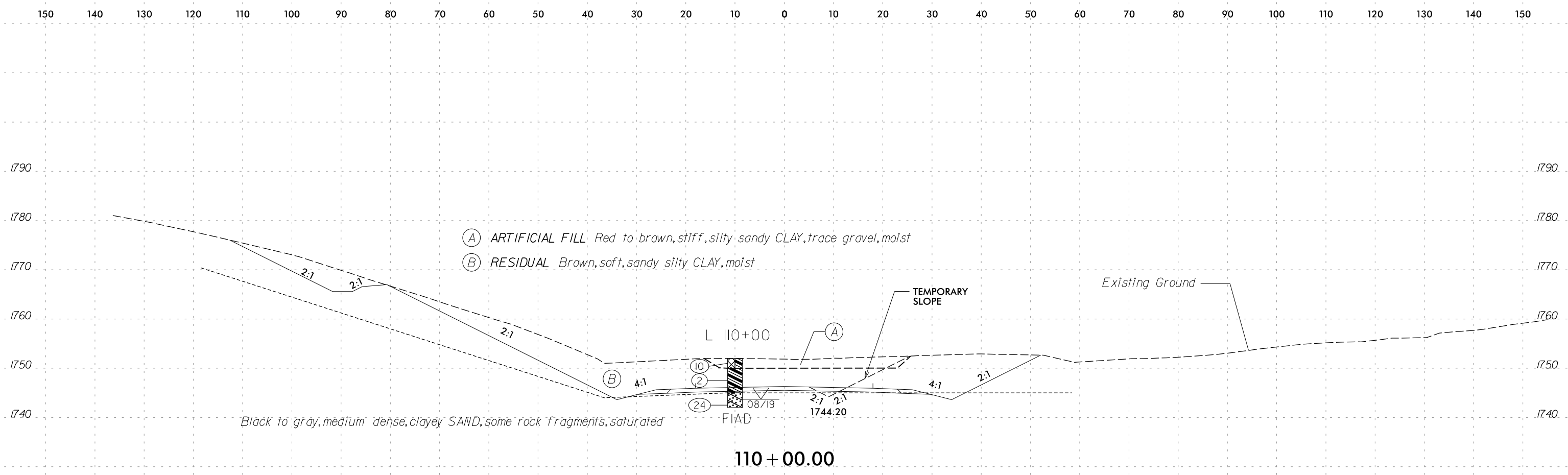


- (A) RESIDUAL Gray to brown, stiff to very stiff, sandy CLAY, saprolitic, moist
- (B) Gray to brown, very stiff to hard, sandy SILT, moist to wet
- (C) RESIDUAL Black, very dense, silty SAND, some rock fragments, saprolitic, saturated

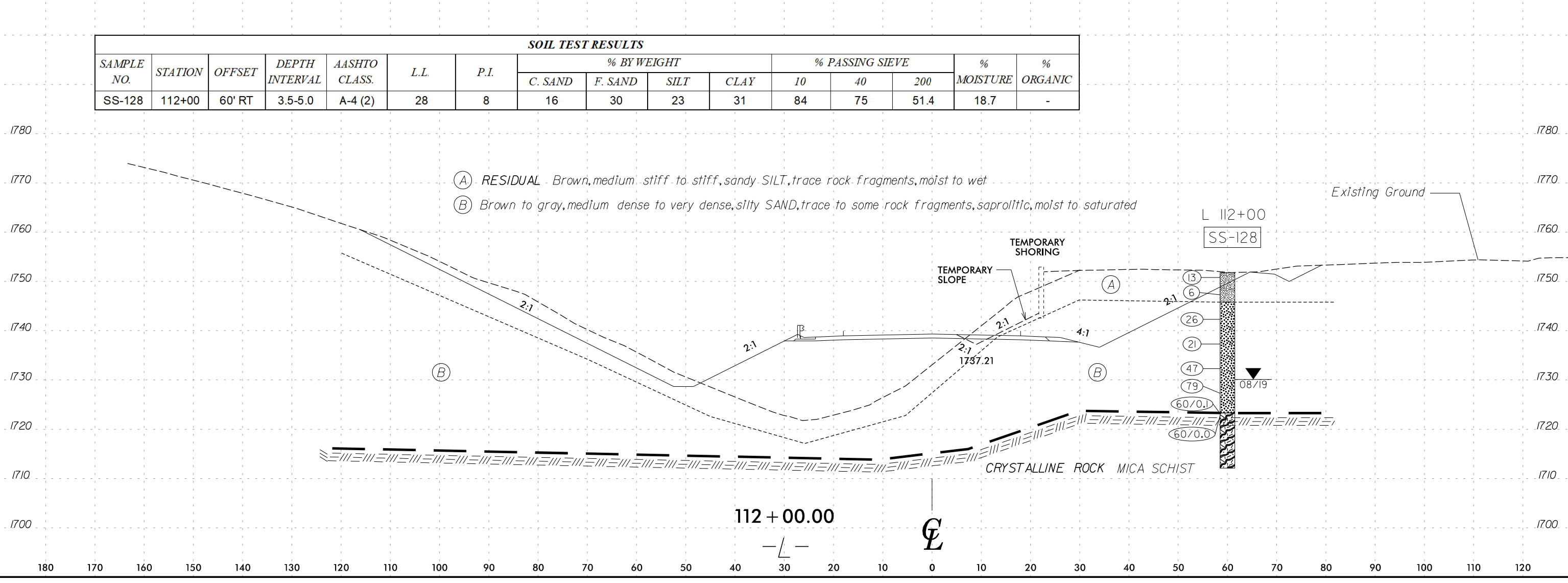
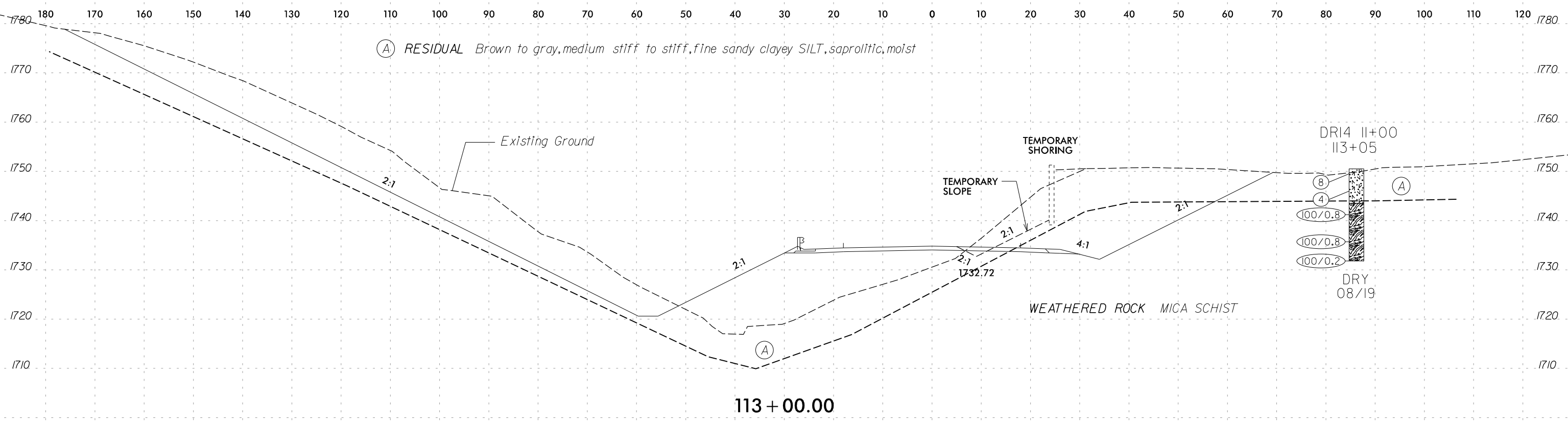


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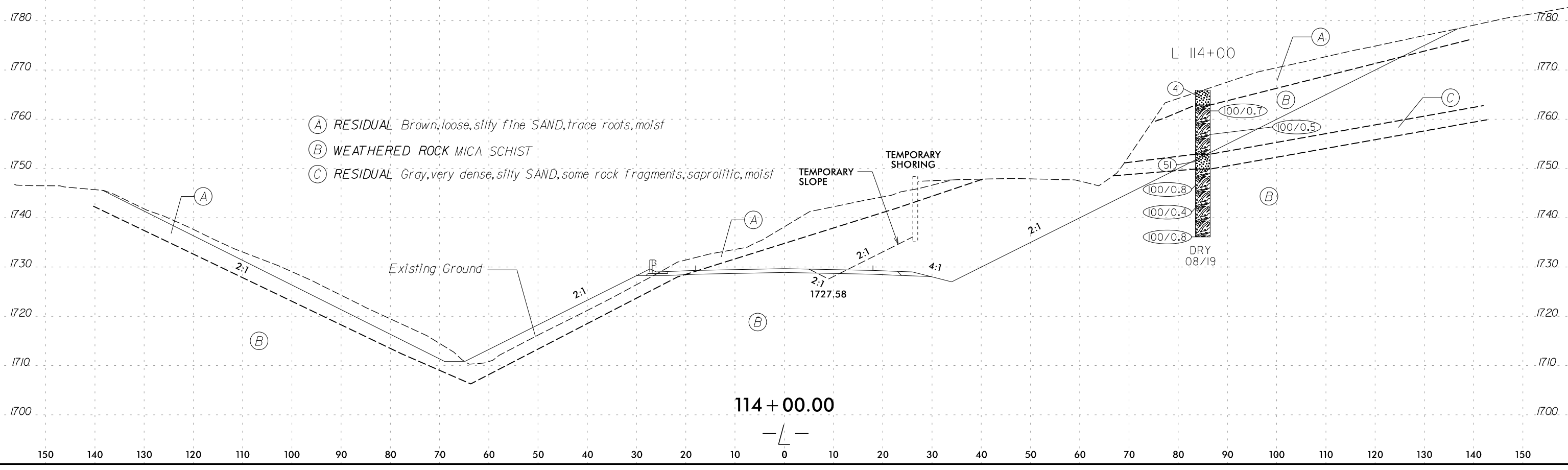
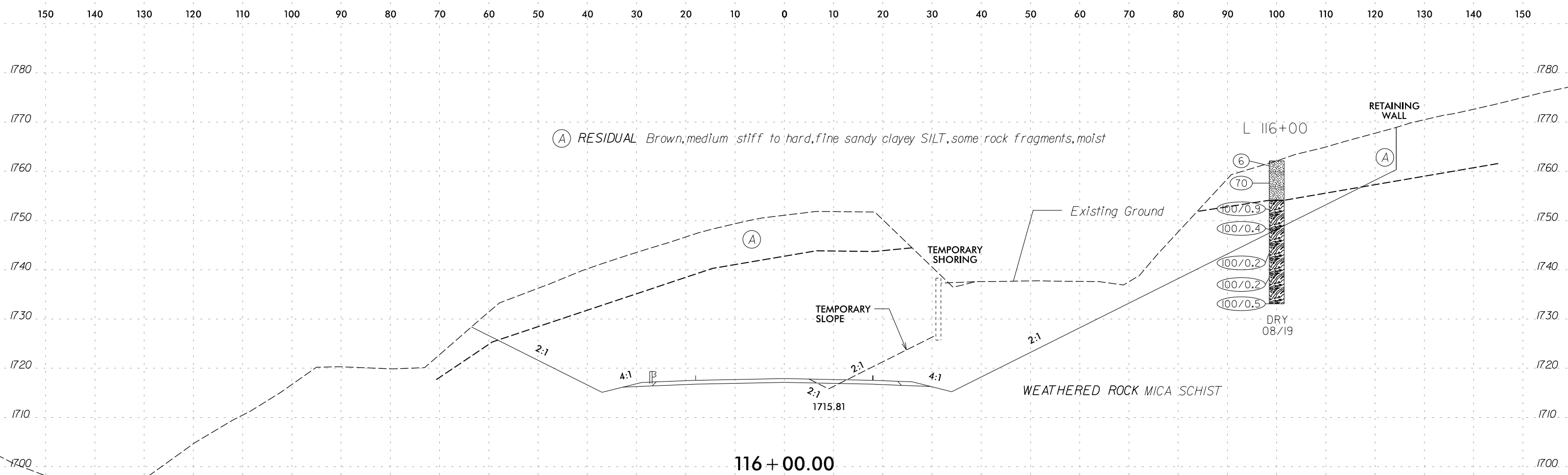




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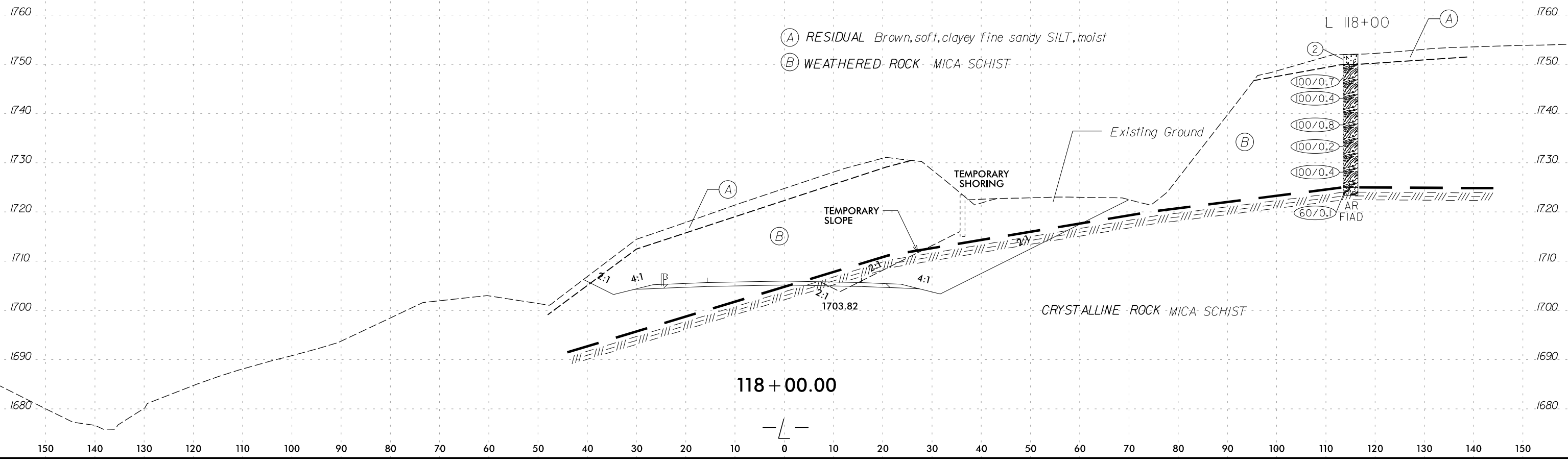
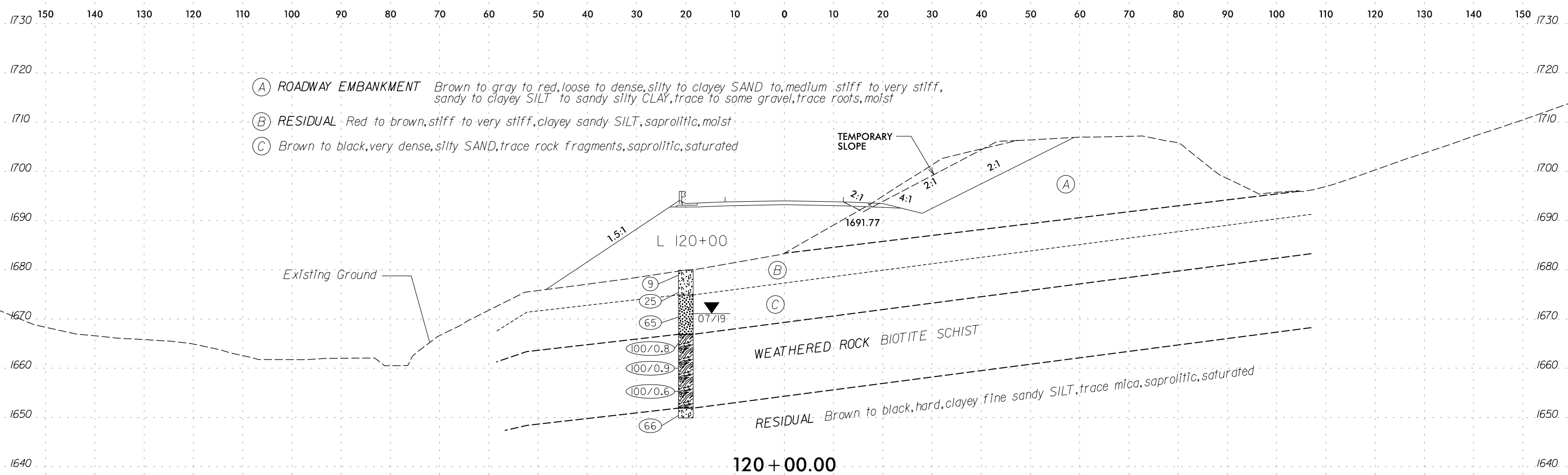


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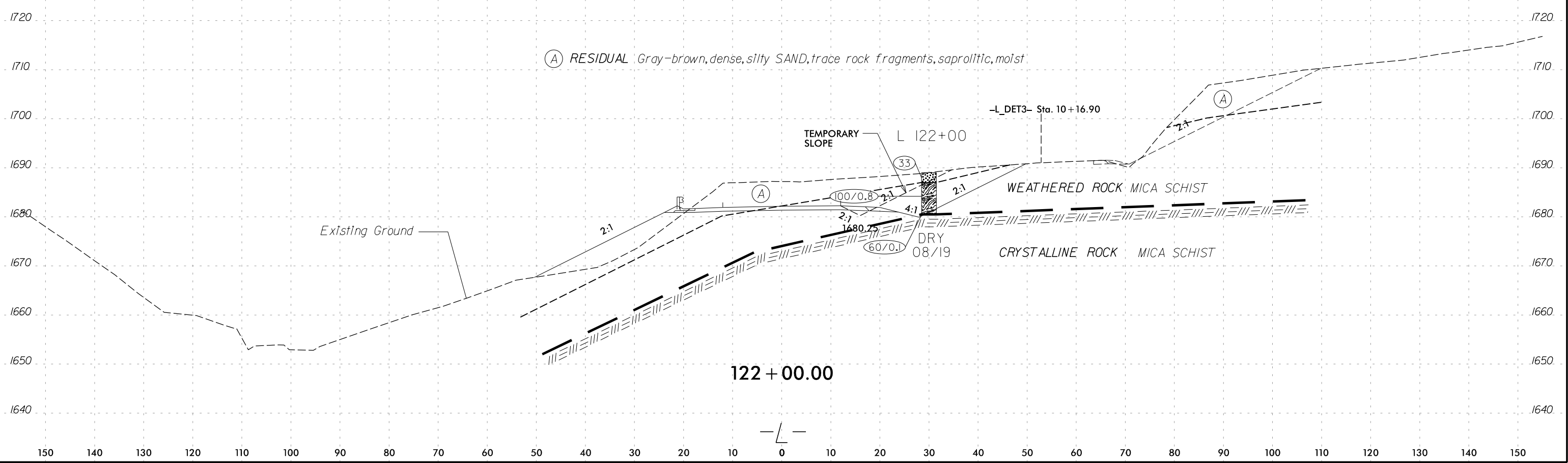
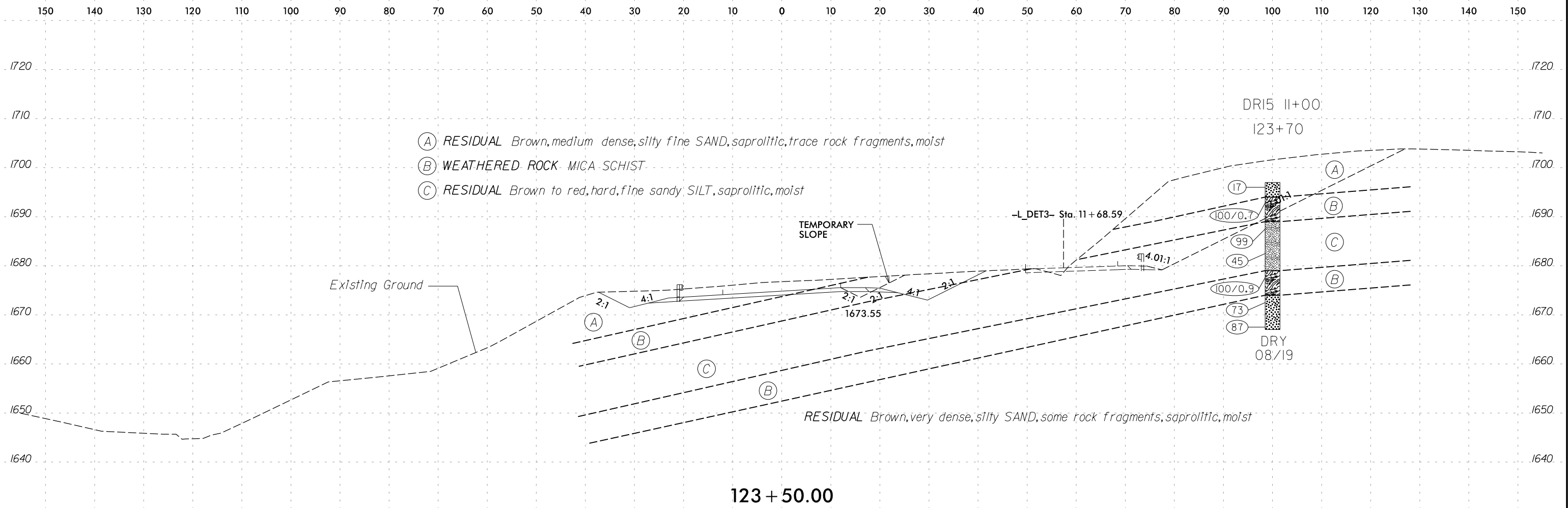


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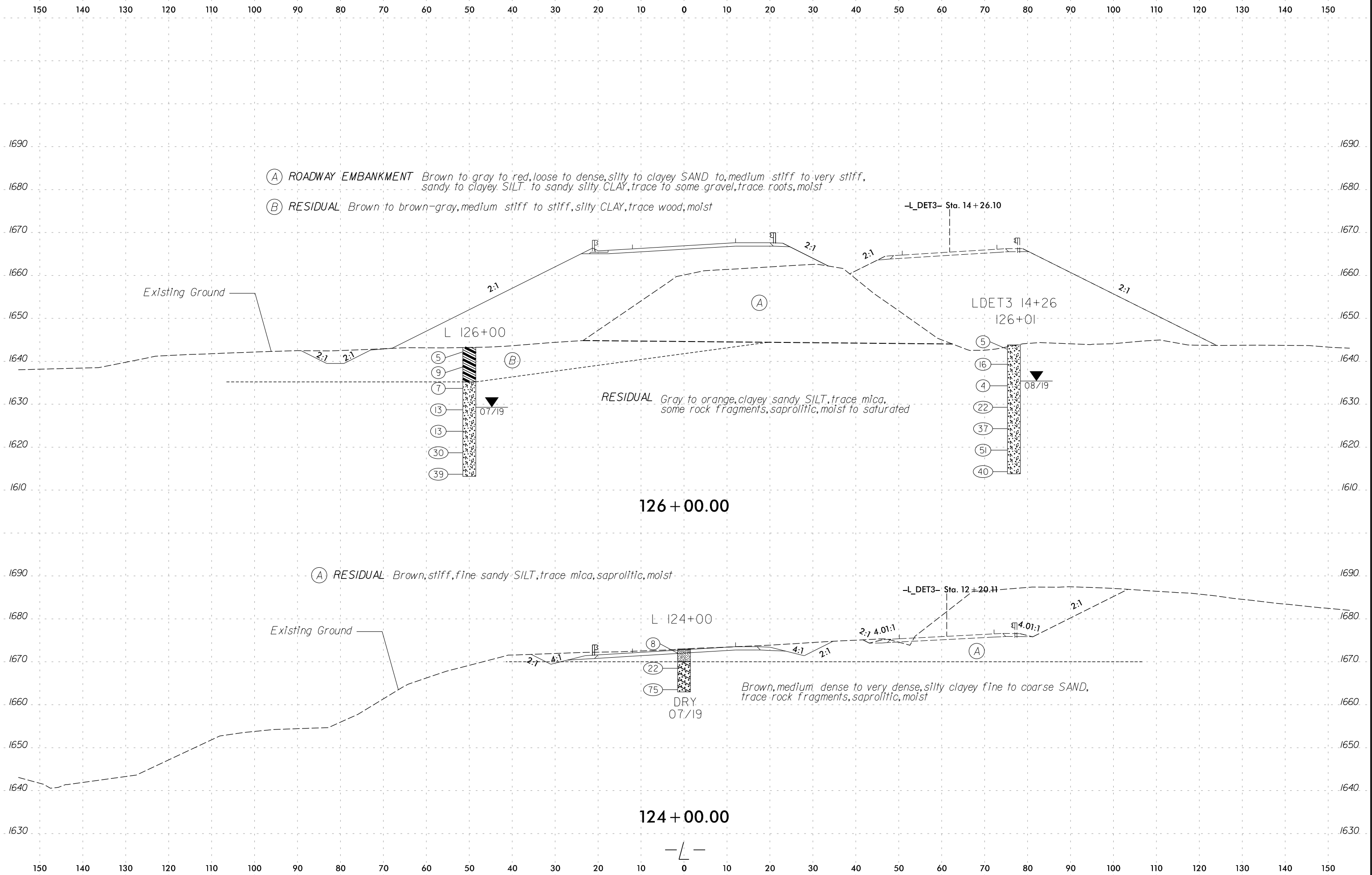




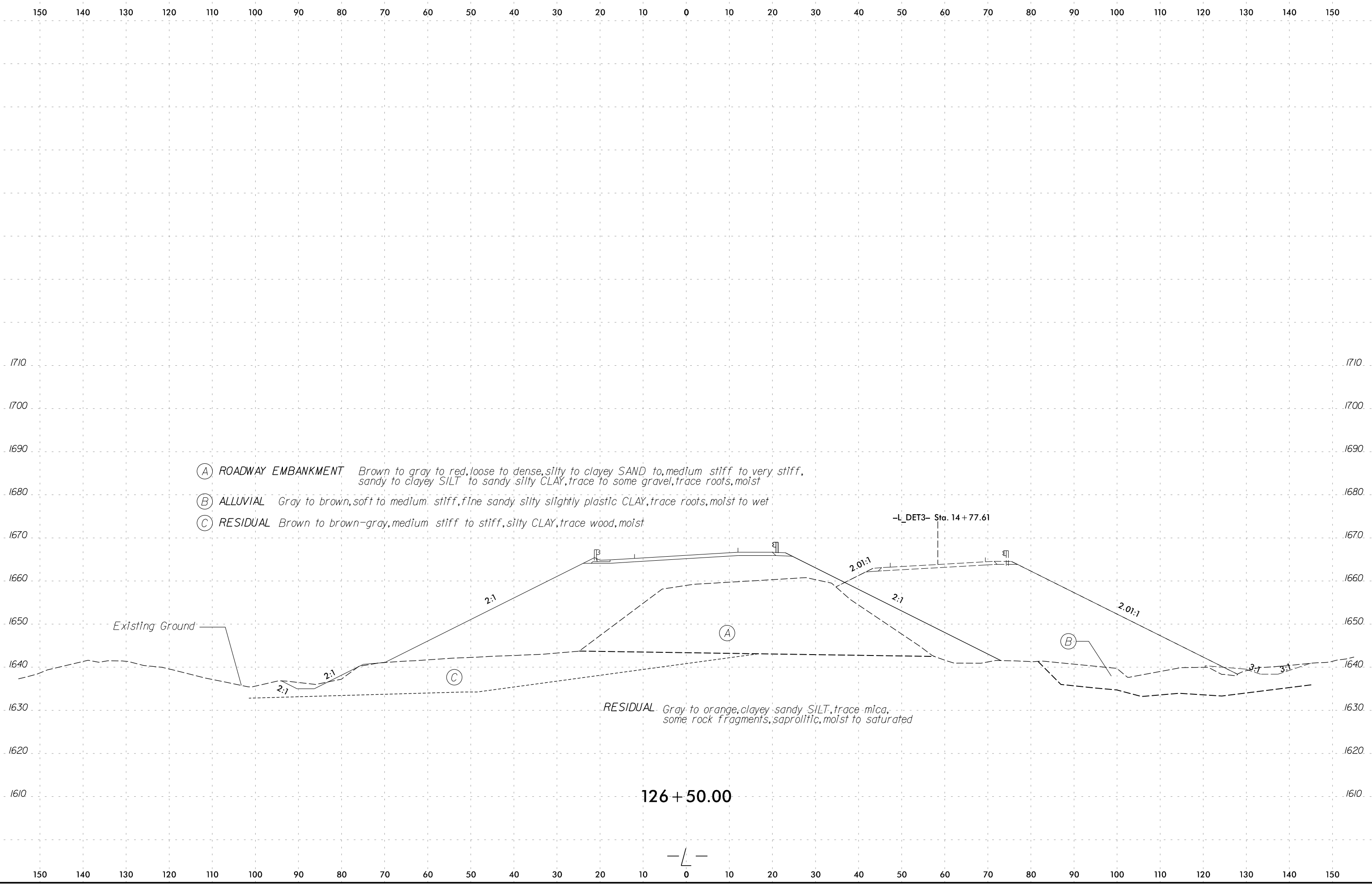
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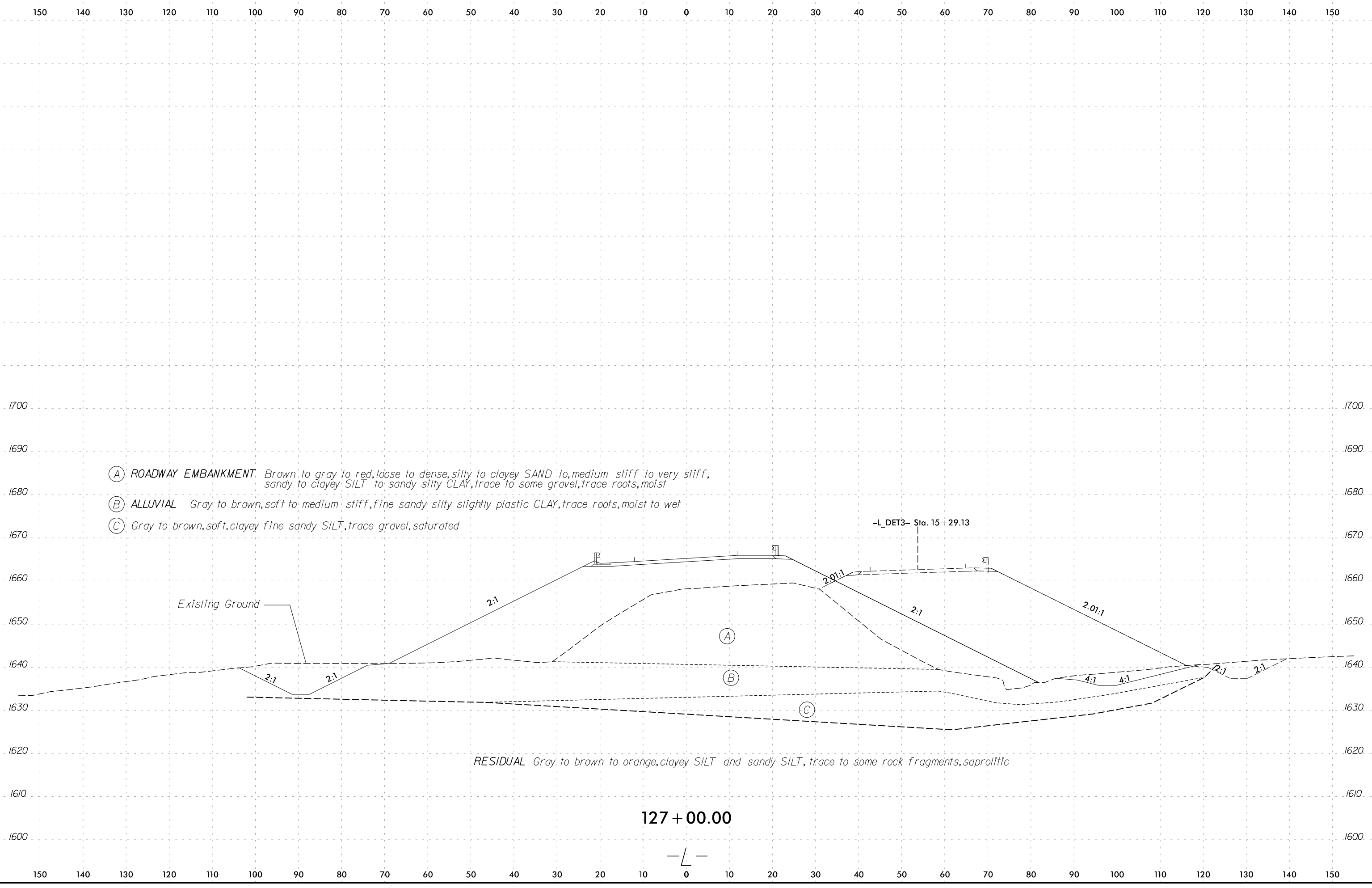
- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) ALLUVIAL *Gray to brown, soft to medium stiff, fine sandy silty slightly plastic CLAY, trace roots, moist to wet*
- (C) RESIDUAL *Brown to brown-gray, medium stiff to stiff, silty CLAY, trace wood, moist*

RESIDUAL *Gray to orange, clayey sandy SILT, trace mica, some rock fragments, saprolitic, moist to saturated*

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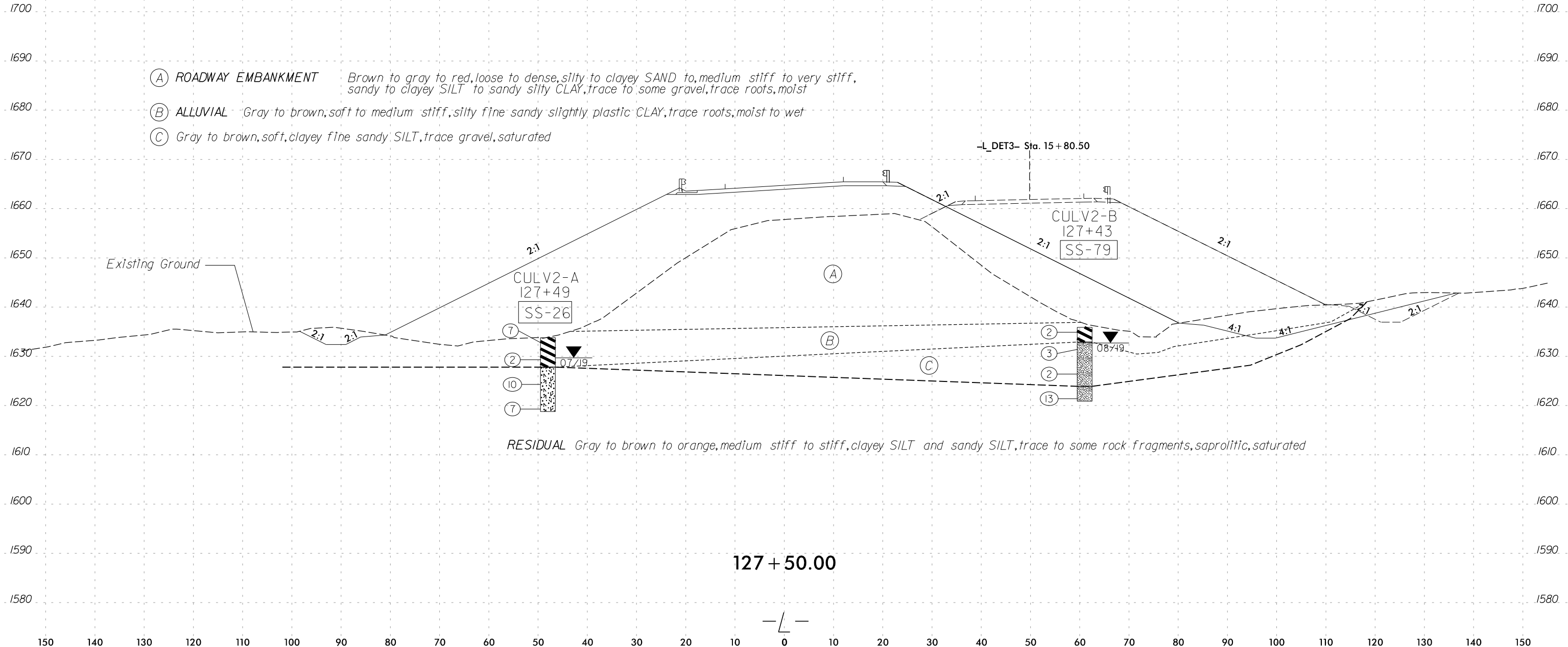


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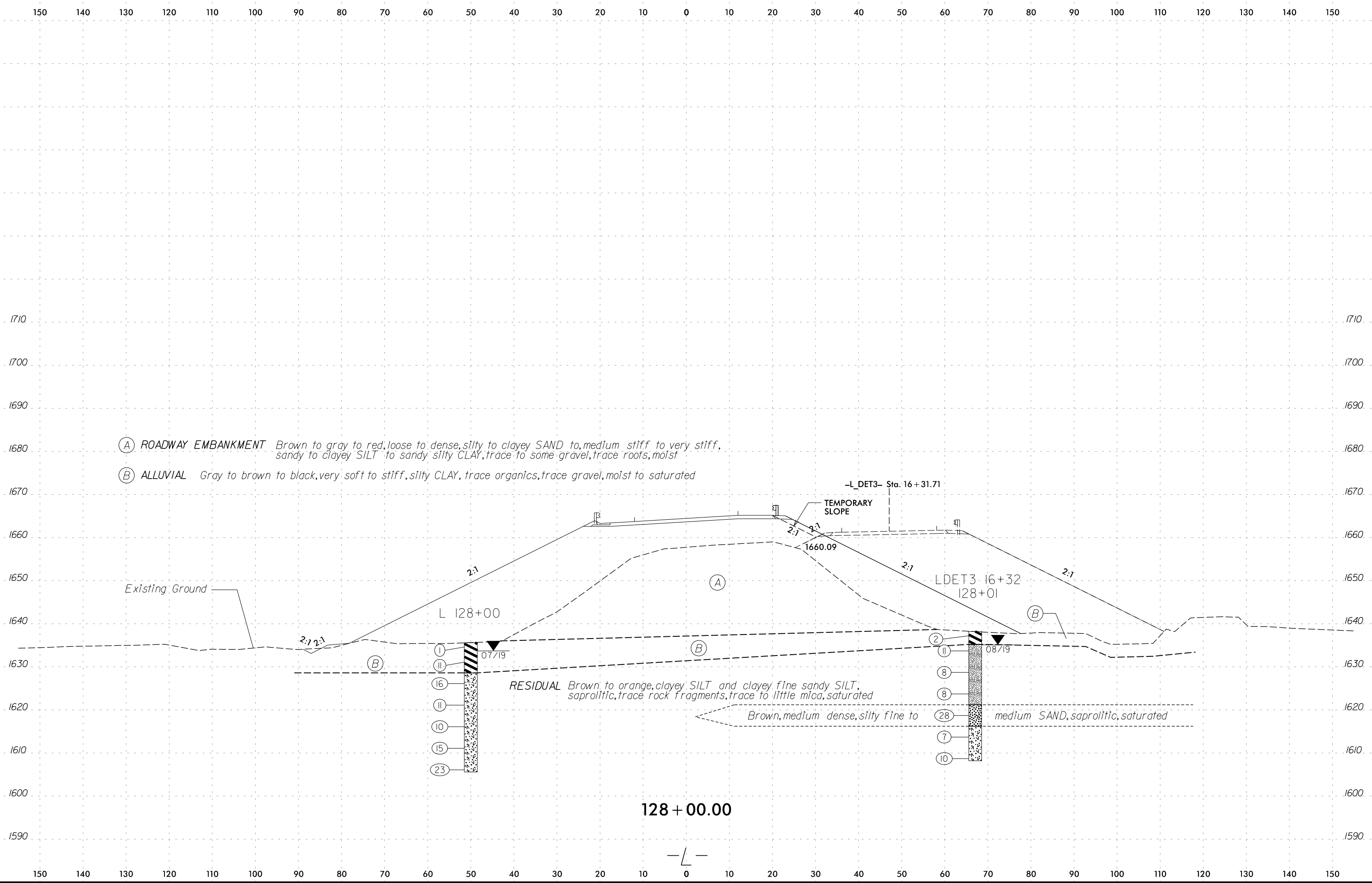


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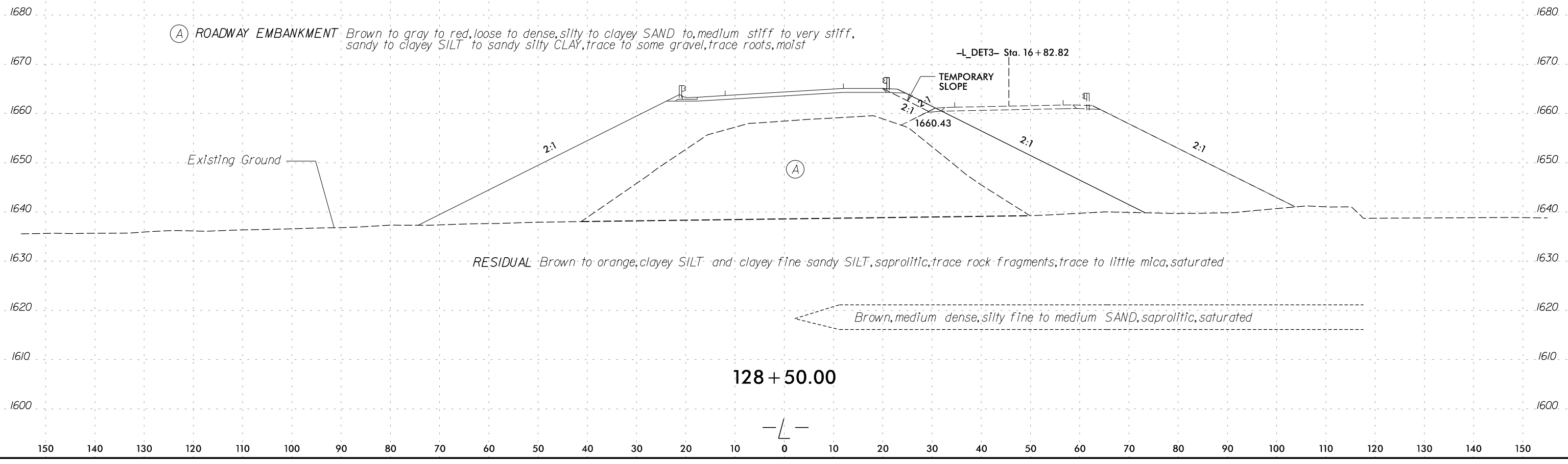
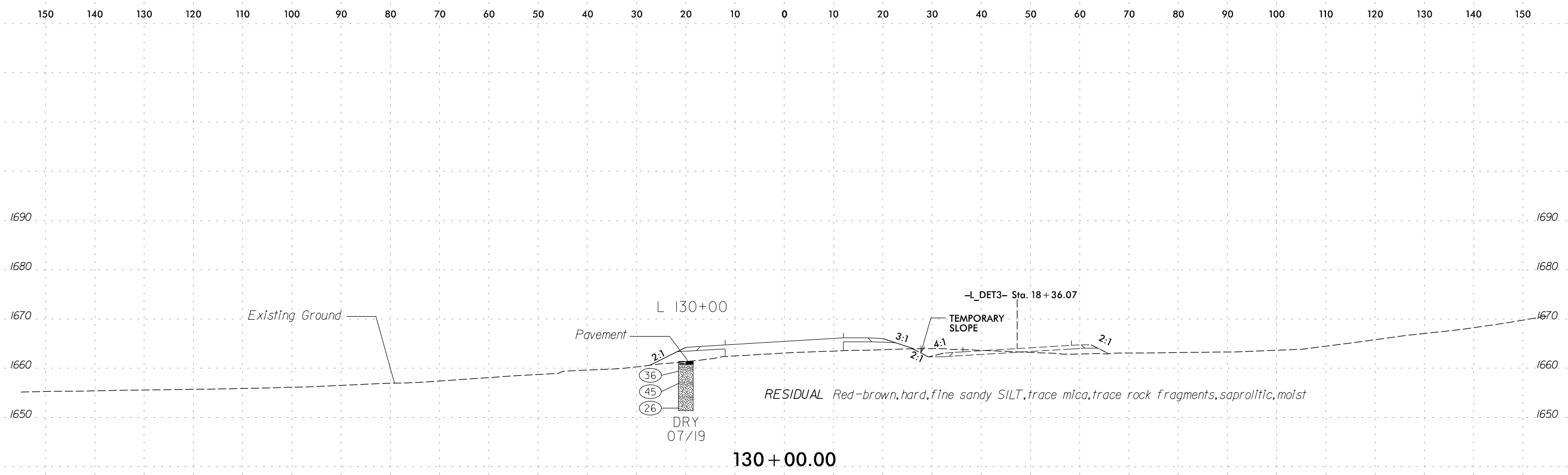
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-26	127+49	48' LT	3.5-5.0	A-7-5 (10)	55	14	9	37	34	20	98	93	63.9	45.8	-
SS-79	127+43	61' RT	3.5-5.0	A-4 (1)	34	7	19	39	18	24	91	82	48	27.5	-



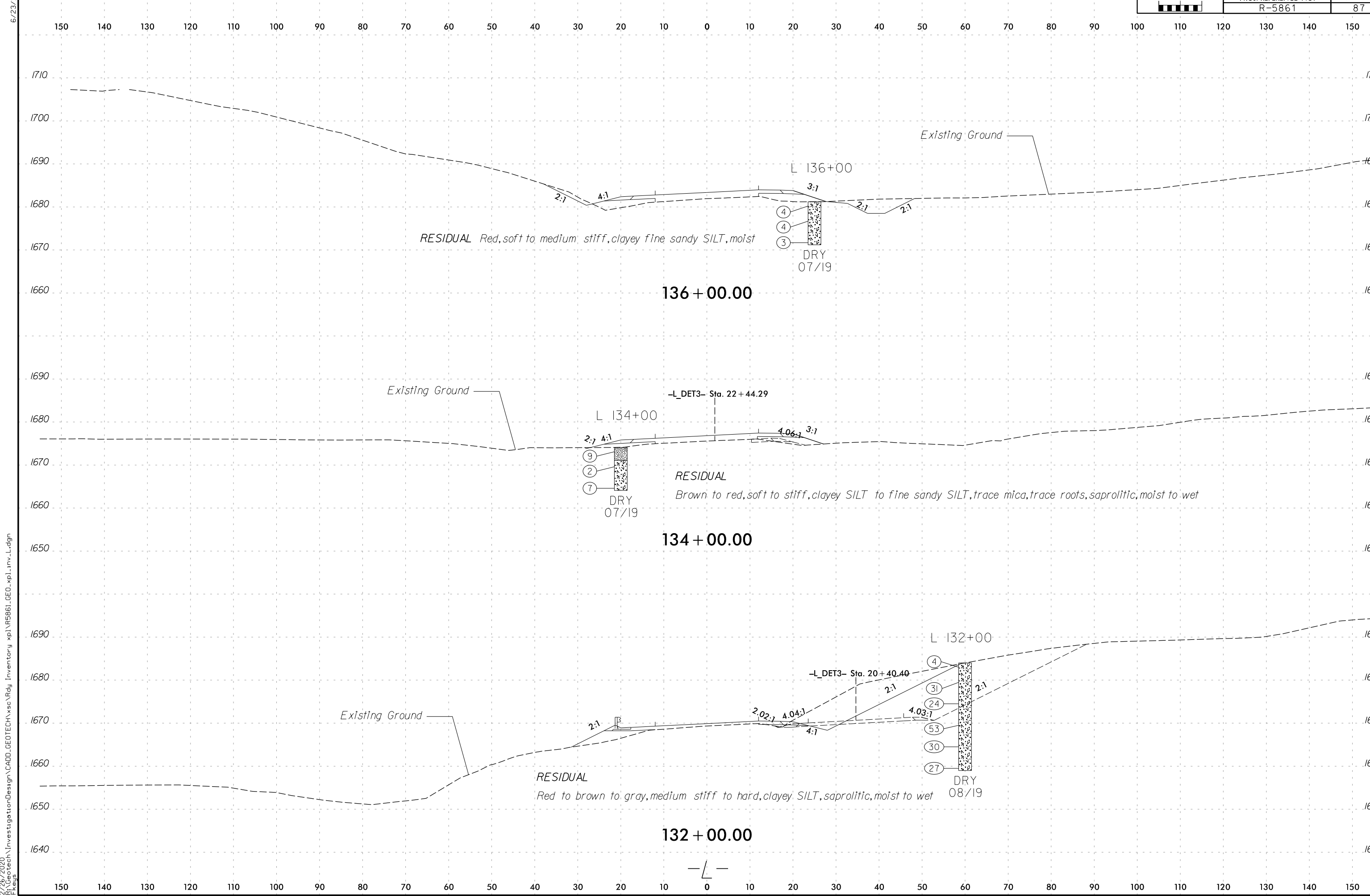
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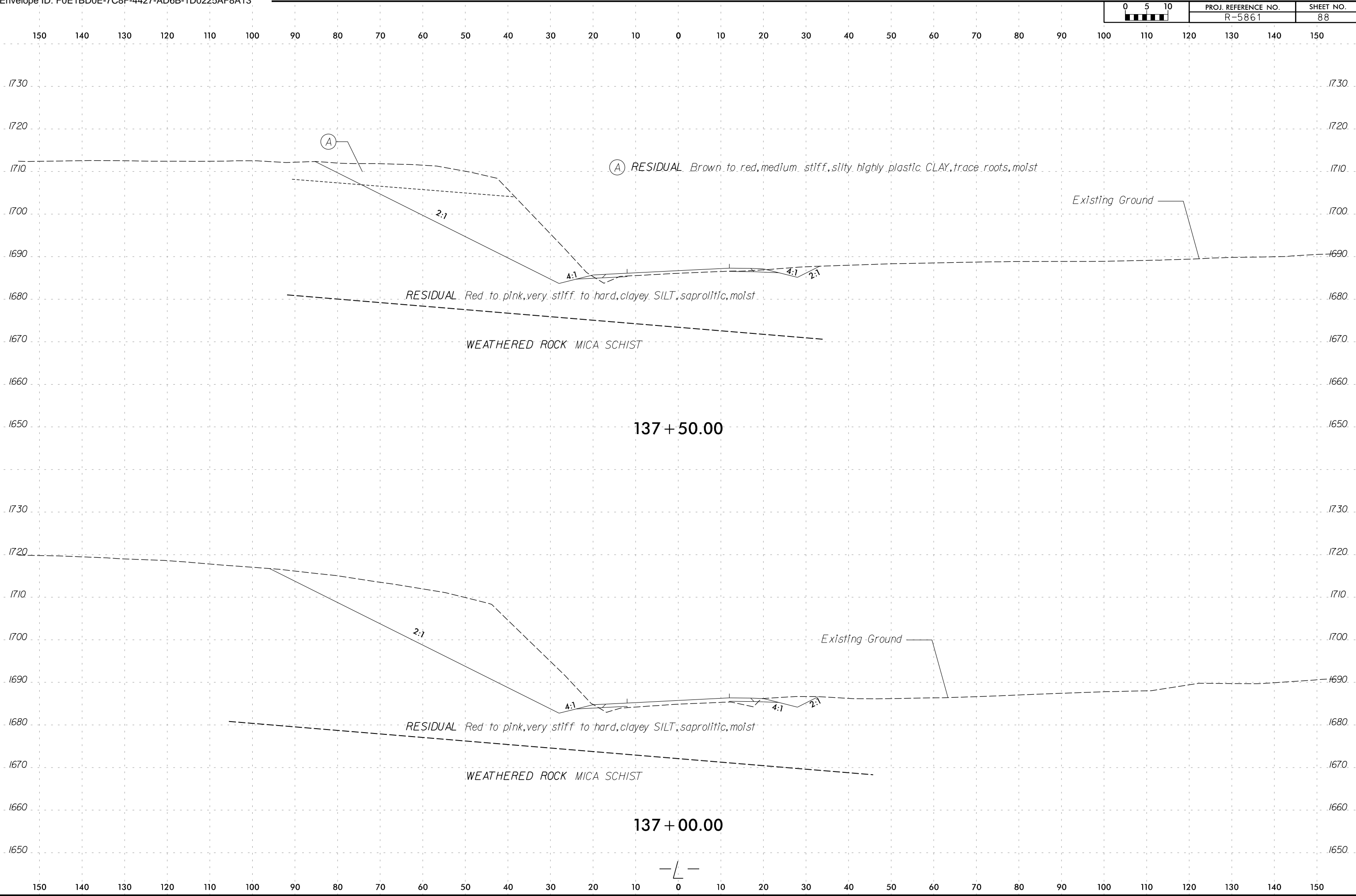
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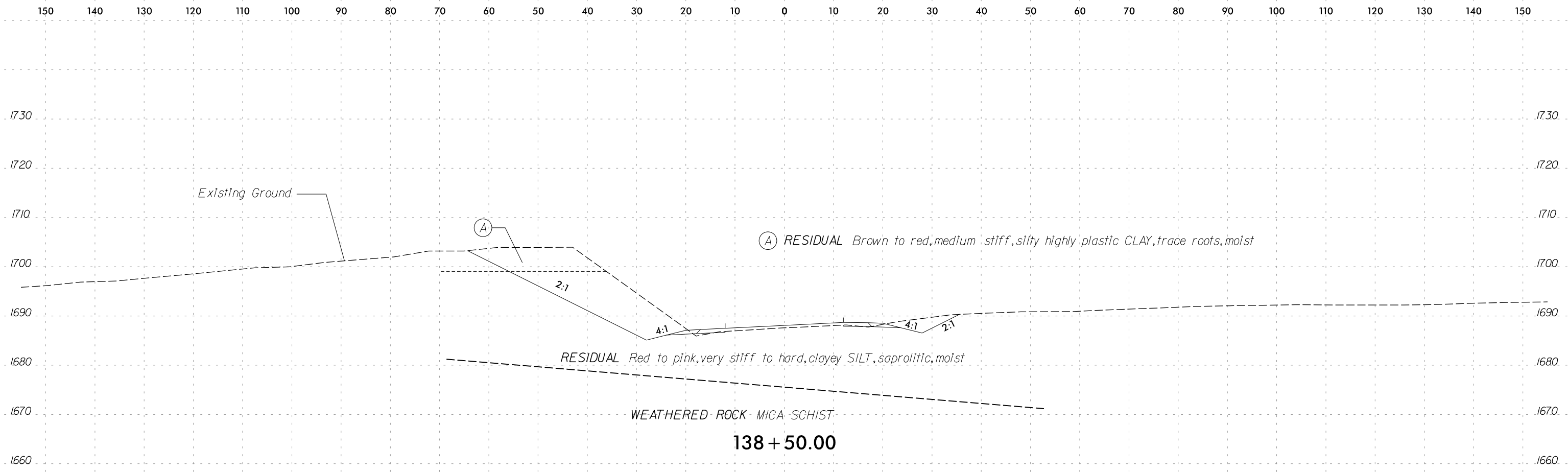


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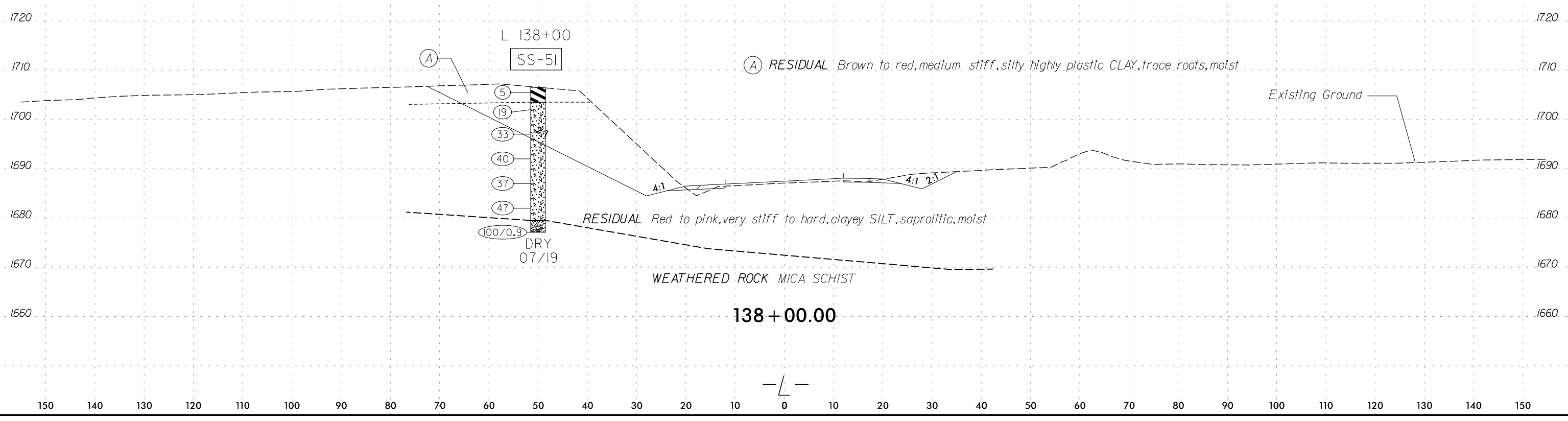


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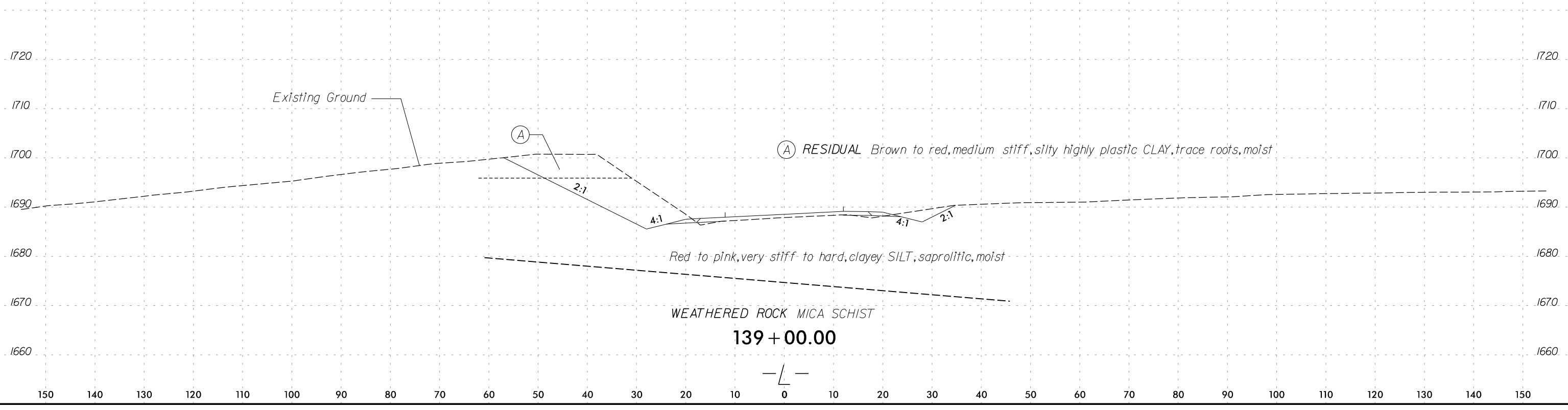
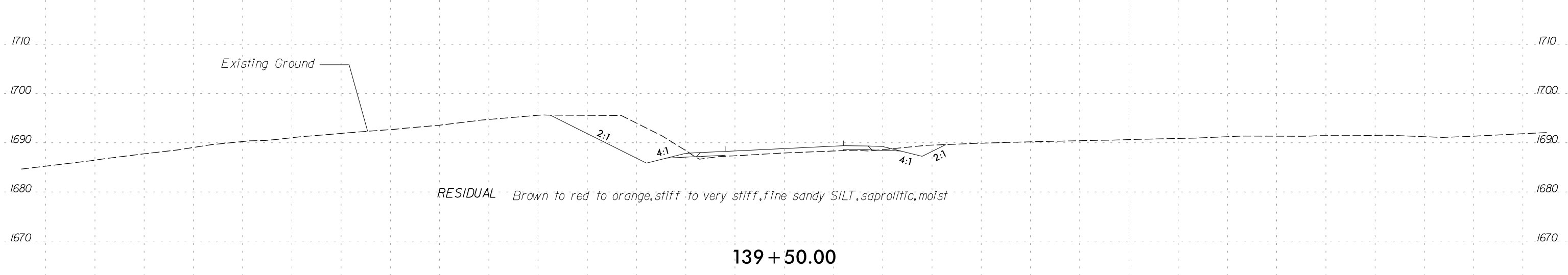
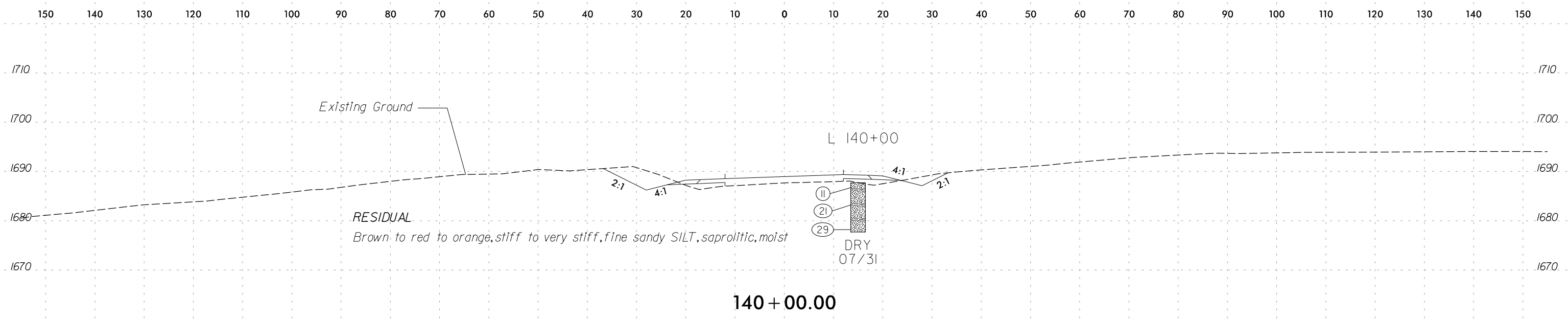




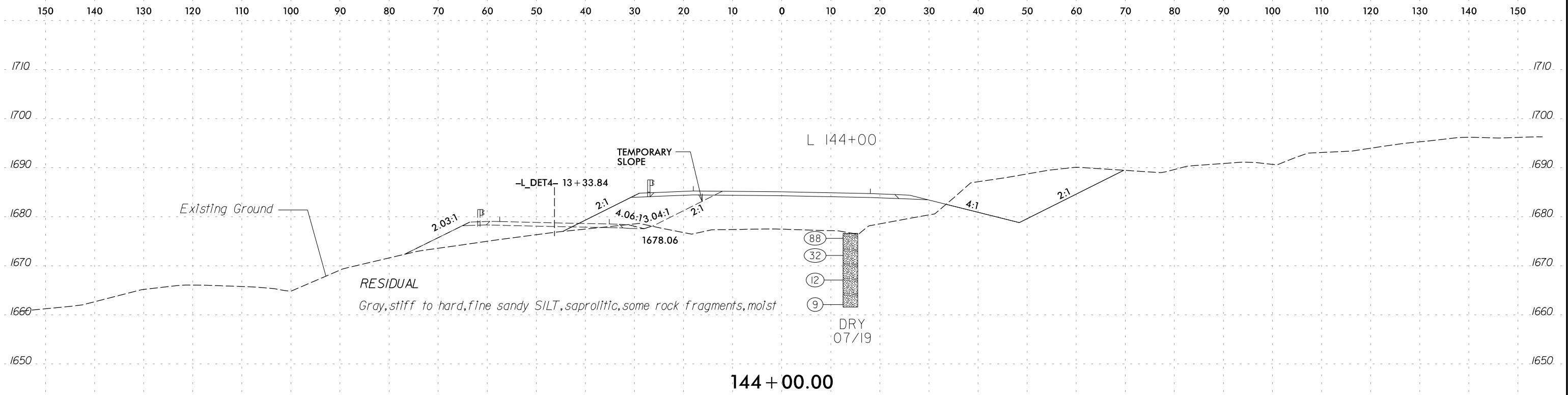
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-51	138+00	50' LT	0.0-1.5	A-7-5 (29)	57	26	1	12	33	54	99	99	93.8	30	-



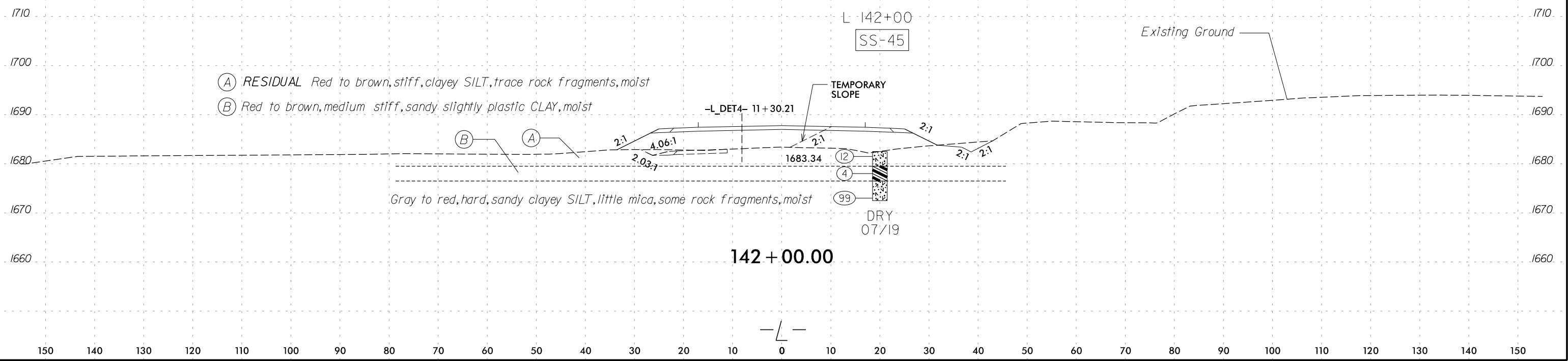
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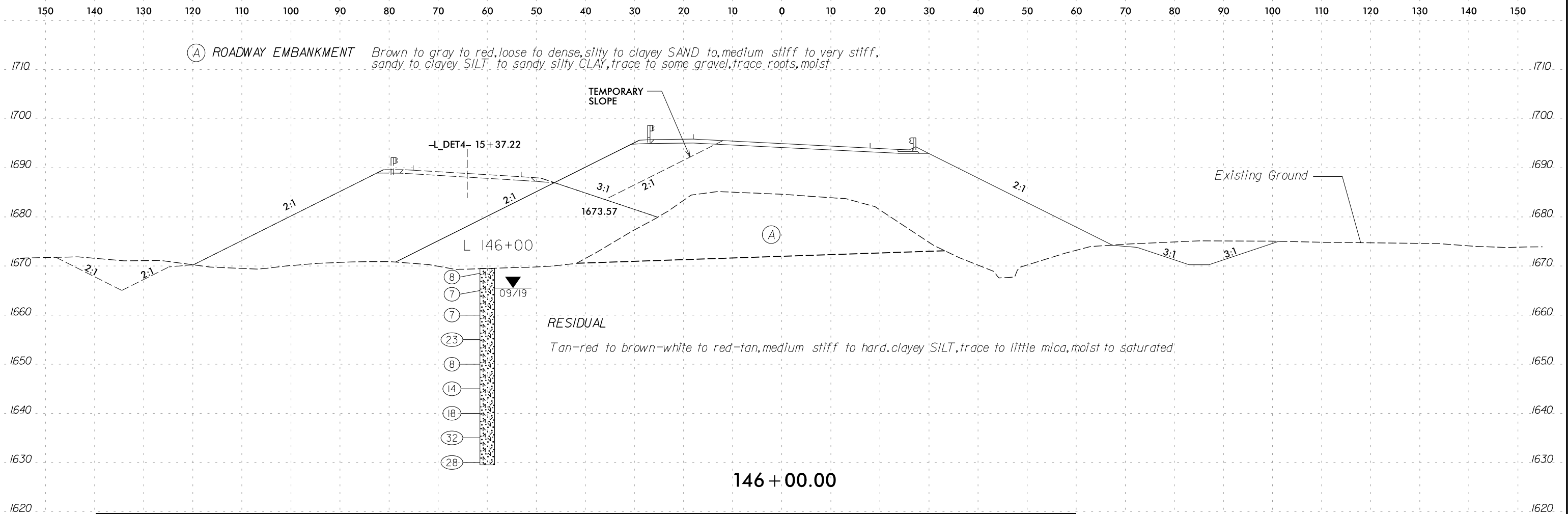
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-45	142+00	20' RT	3.5-5.0	A-6 (4)	38	11	26	17	30	27	85	67	53	20.5	-

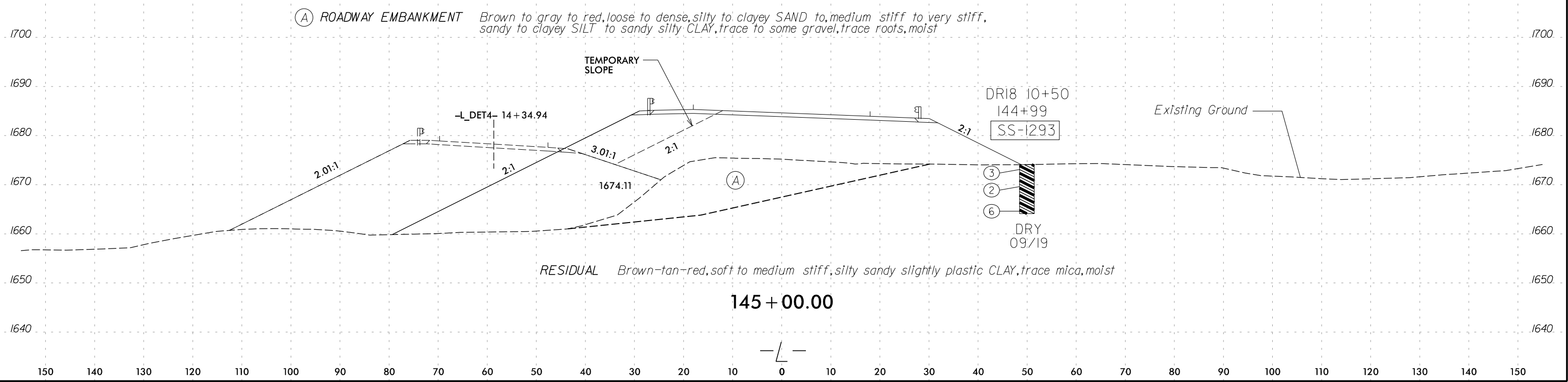


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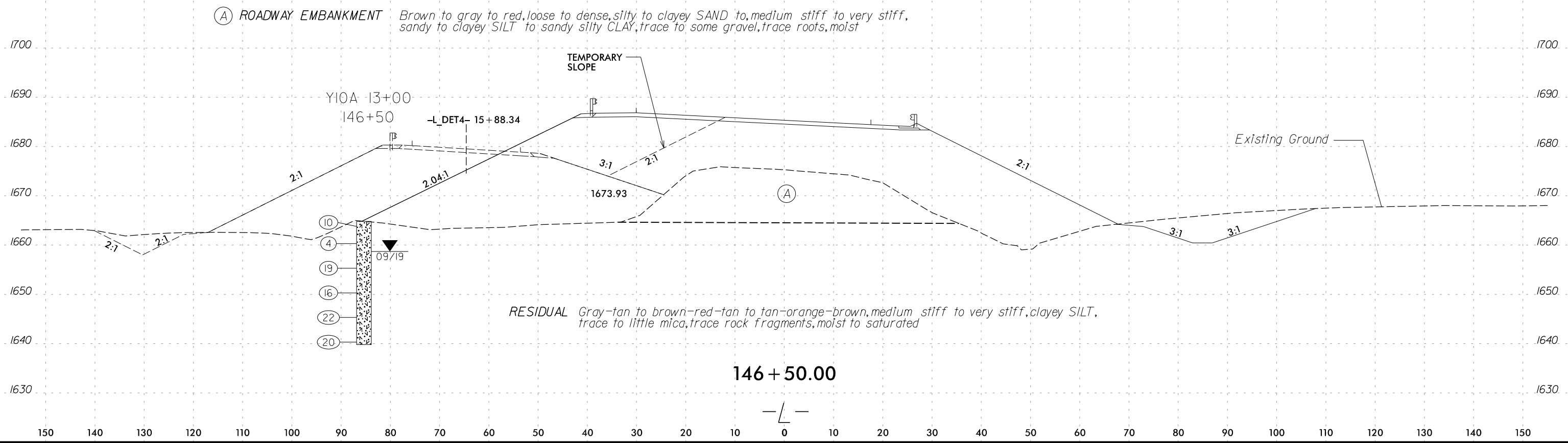
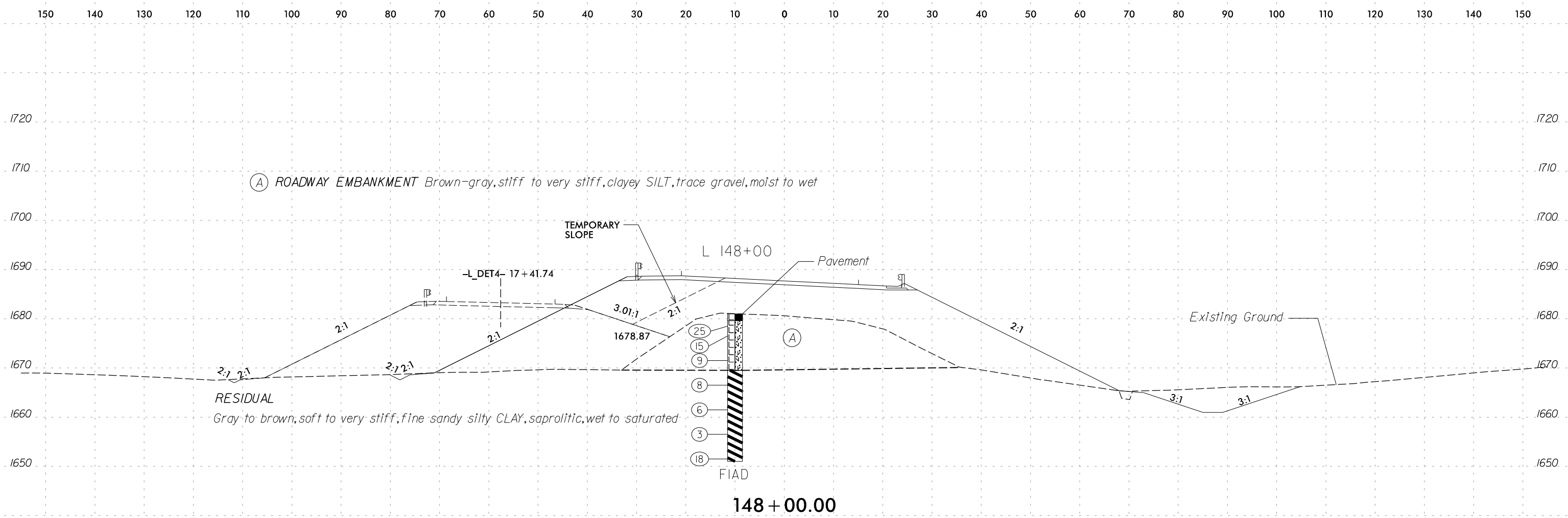
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1293	144+99	50' RT	3.5-5.0	A-6 (3)	40	11	22	12	32	34	69	57	47.4	24.6	-



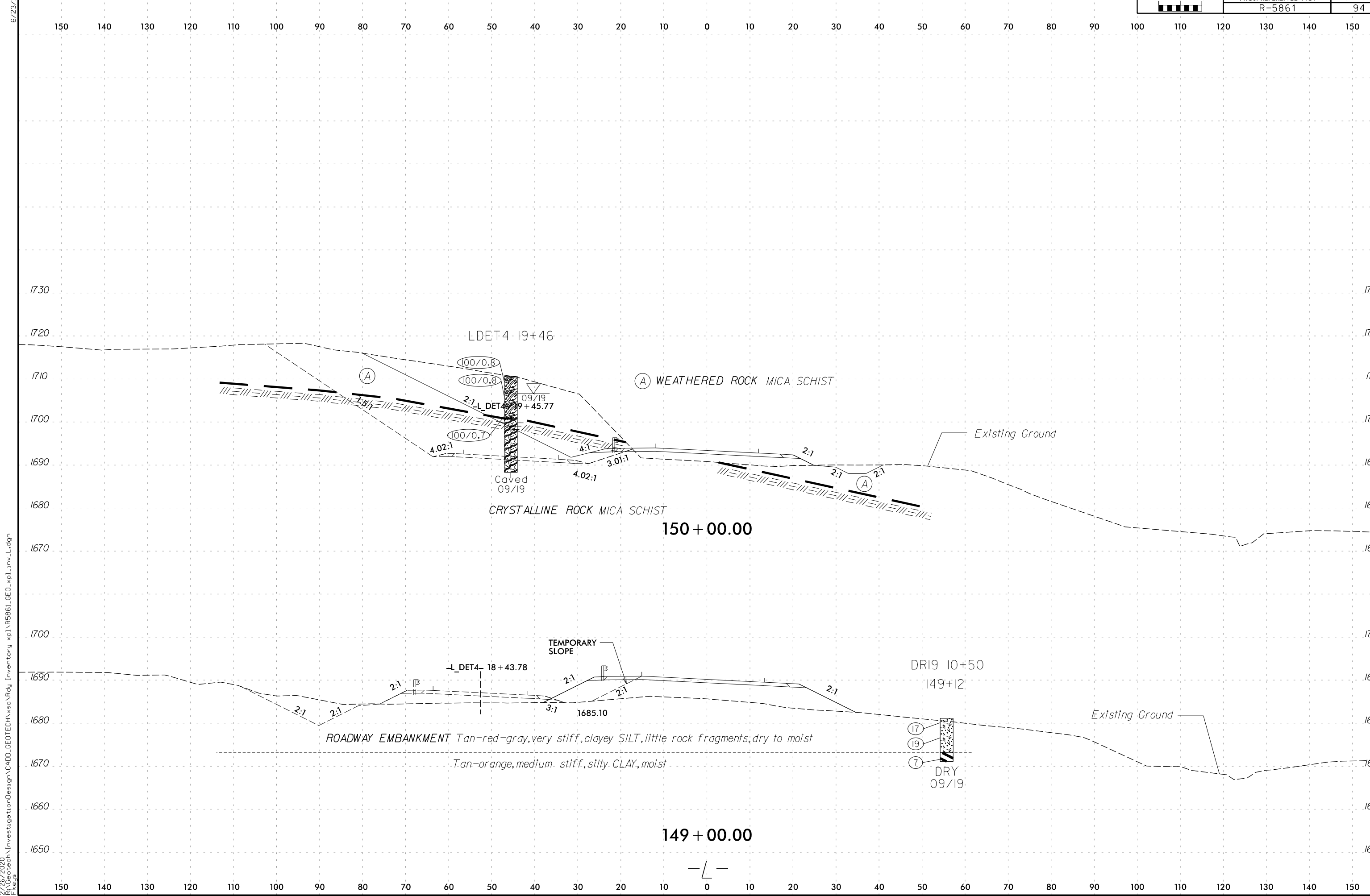
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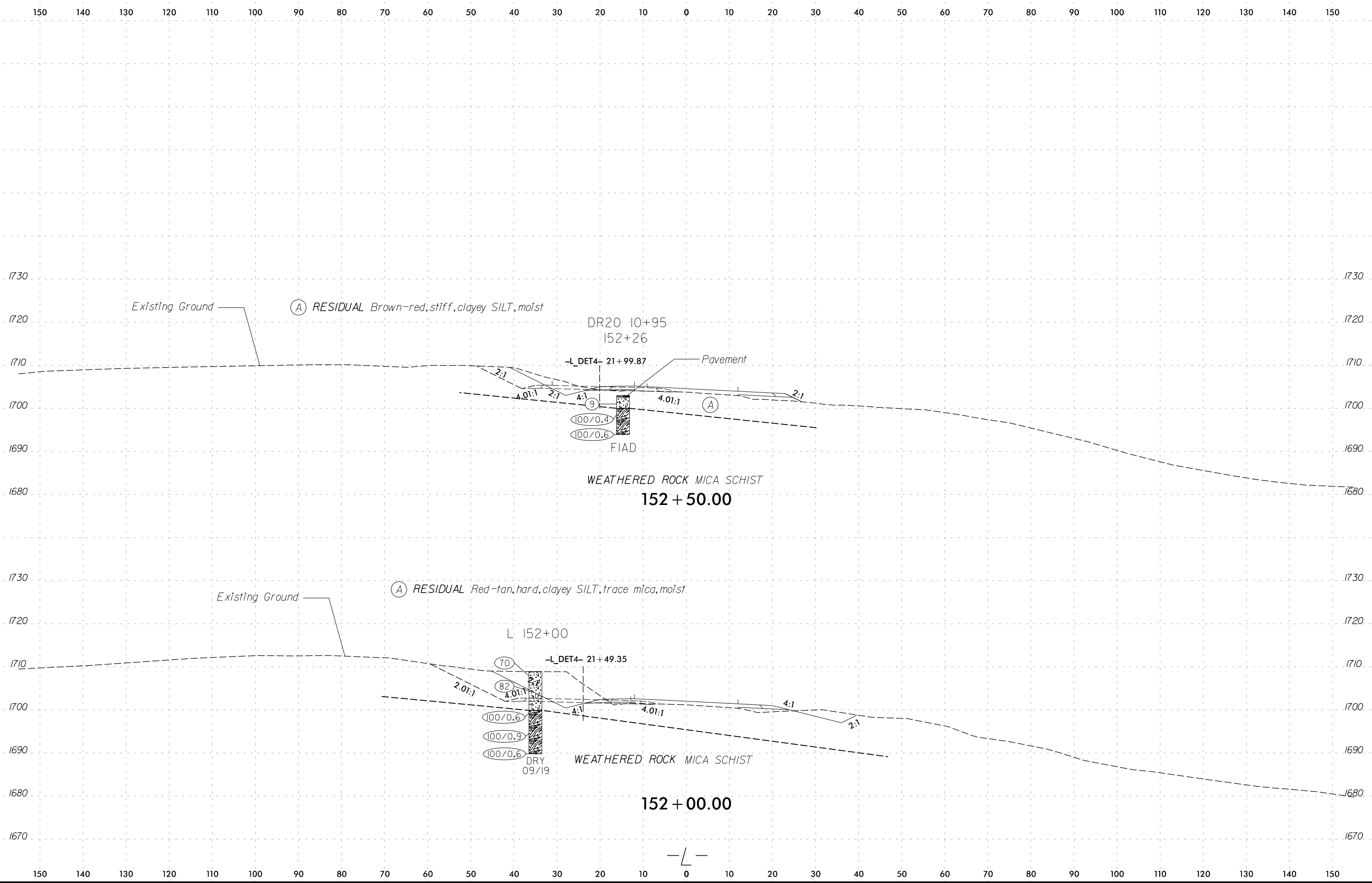




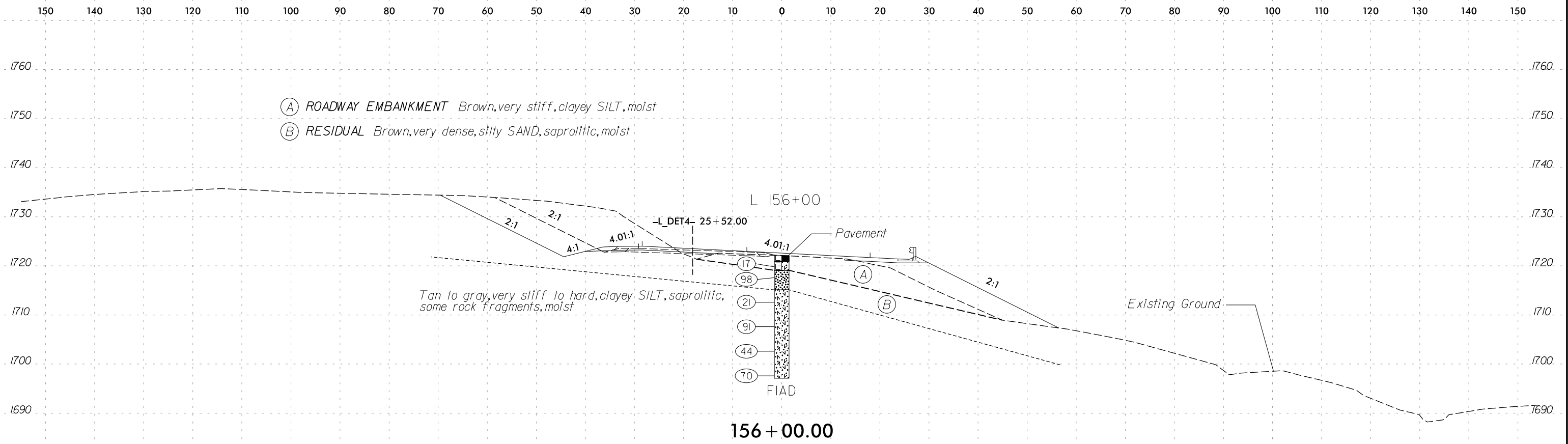
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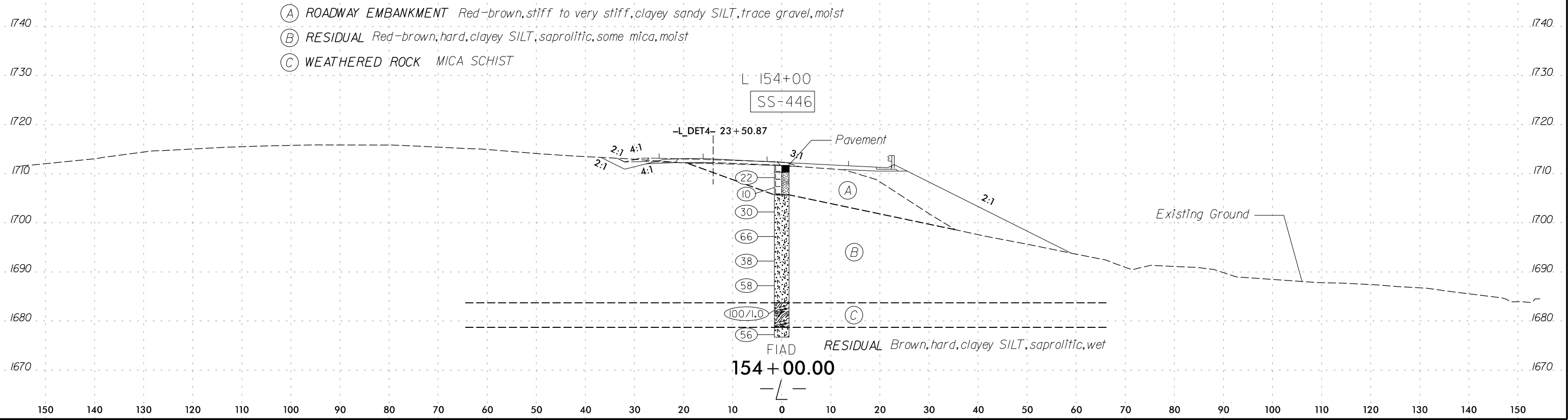
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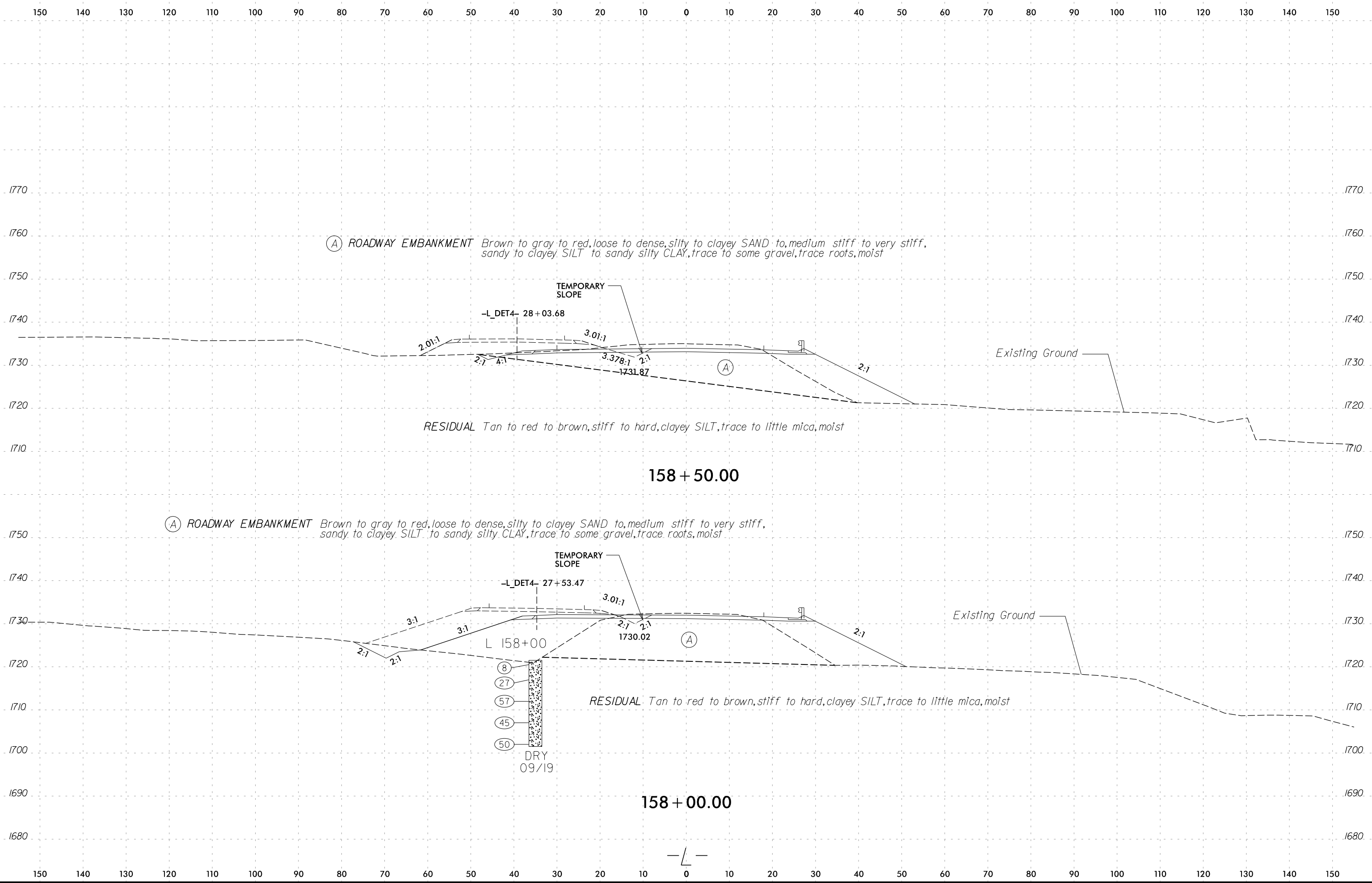
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-446	154+00	0	1.5-3.0	A-4 (0)	33	3	34	21	27	18	92	68	46.5	13.1	-

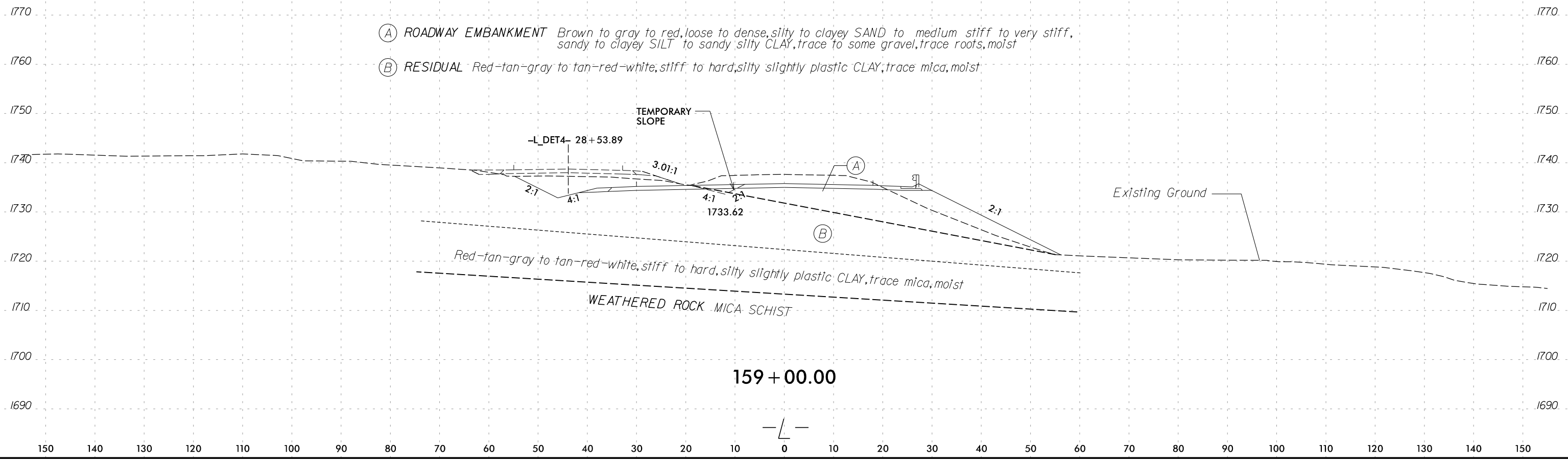
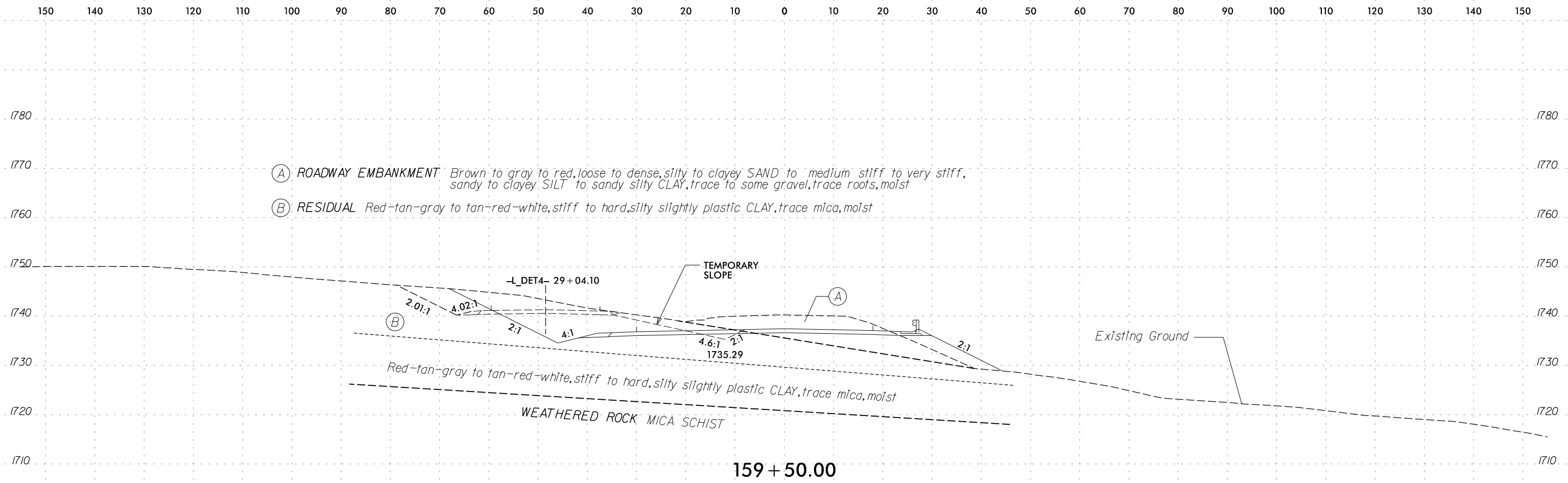


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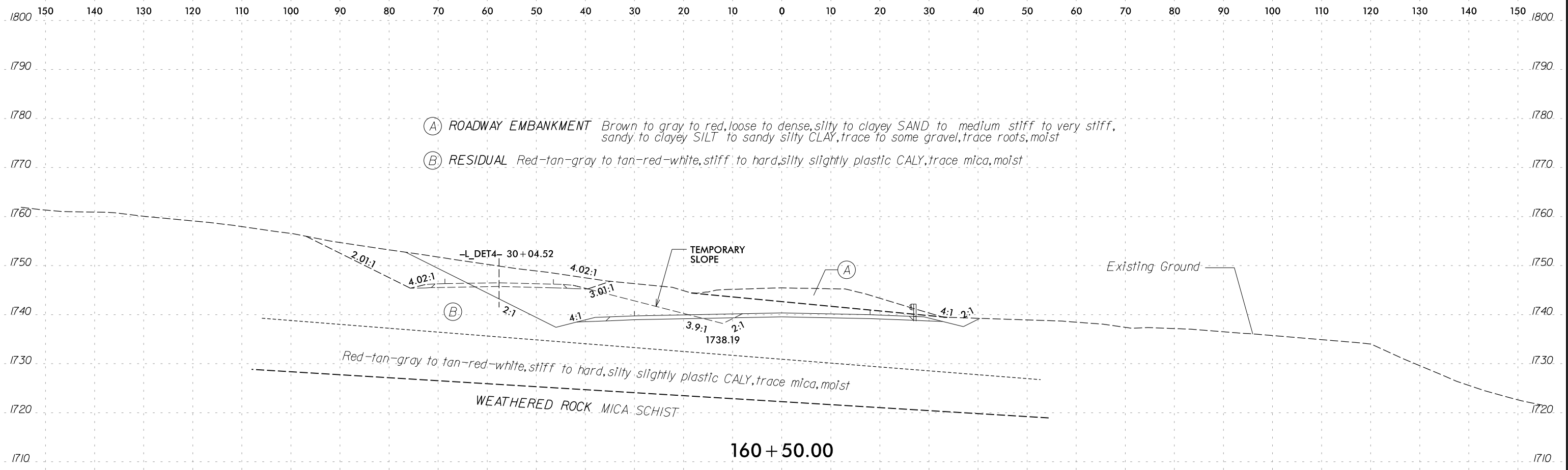


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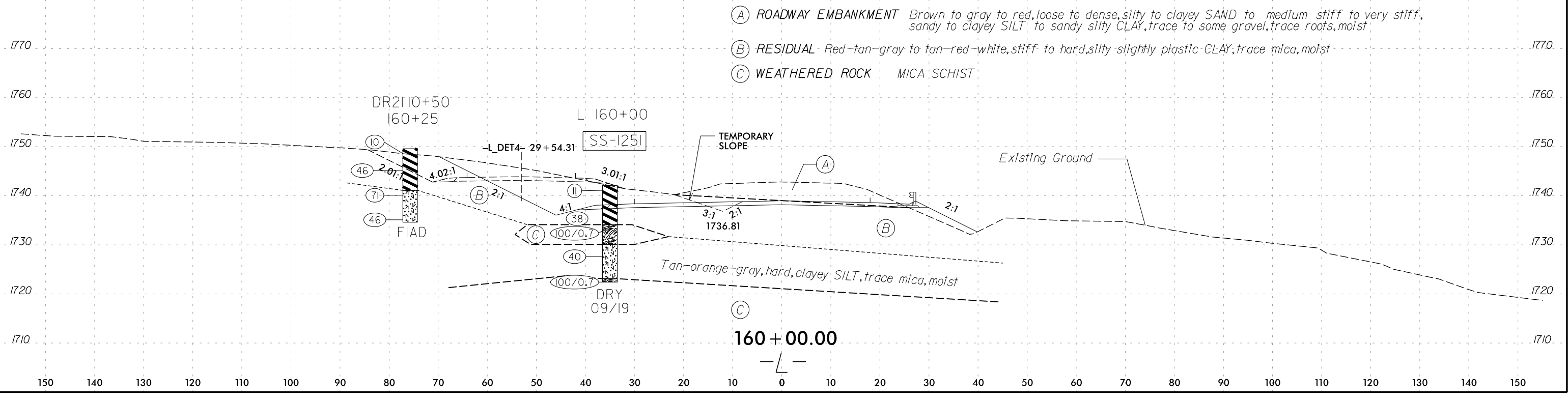




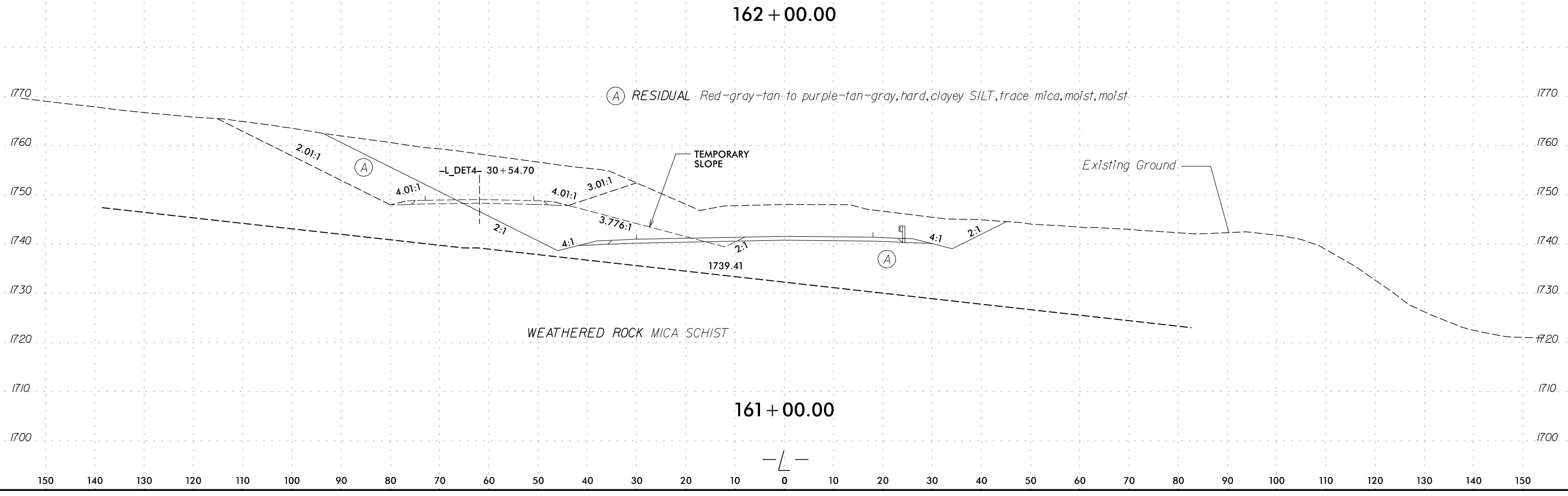
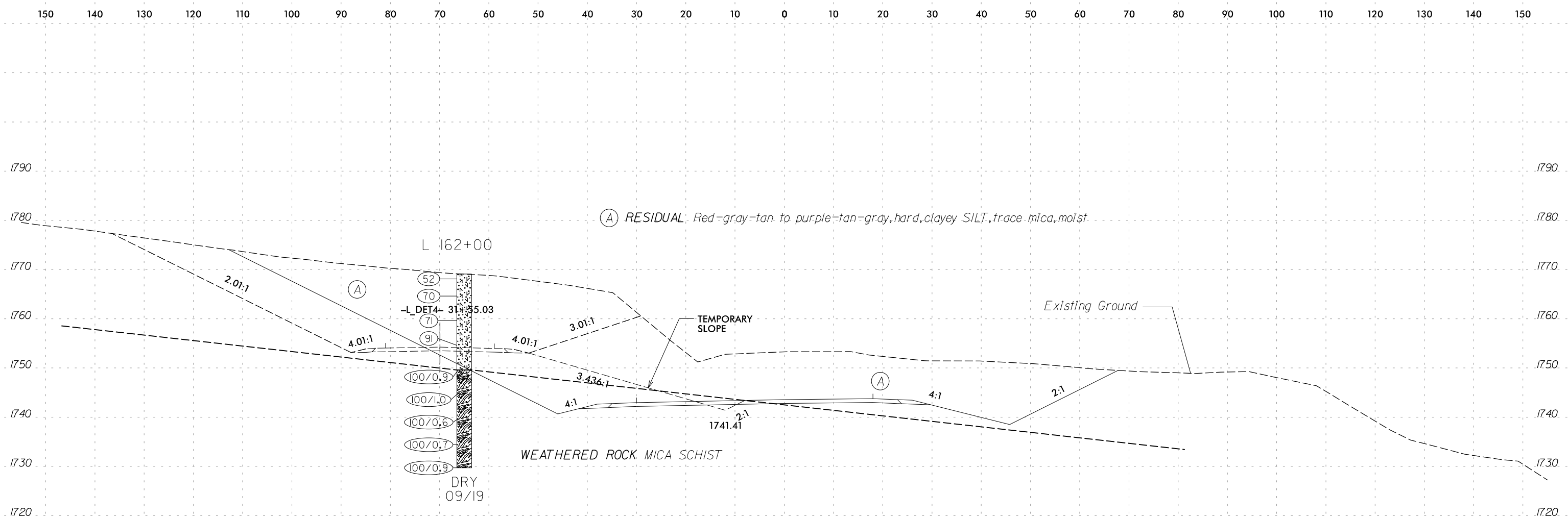
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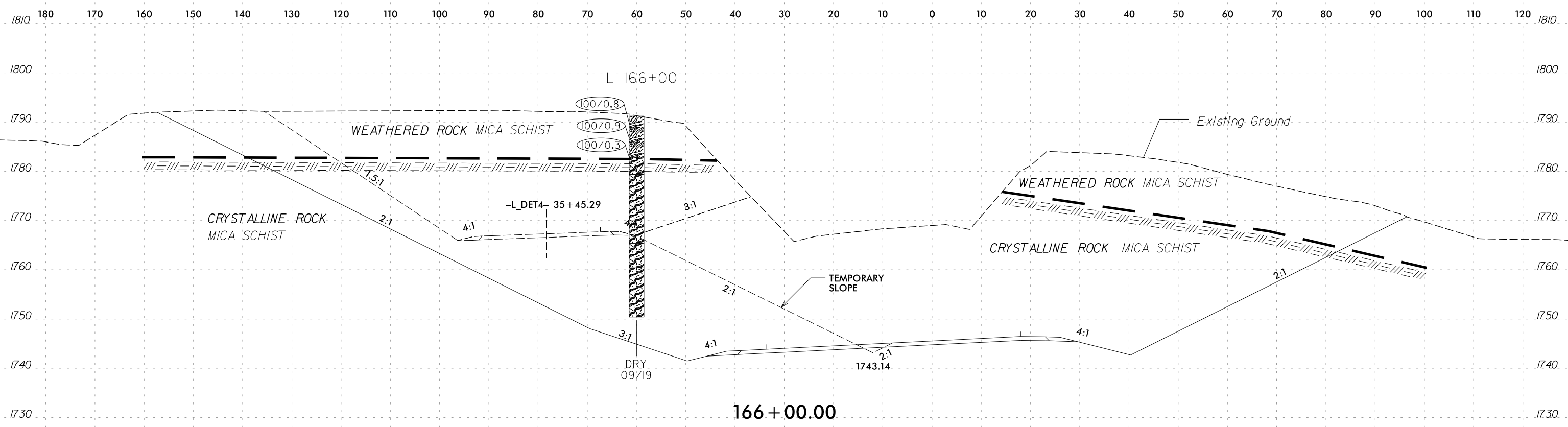
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SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1251	160+00	35' LT	0.0-1.5	A-7-5 (14)	44	11	1	15	52	32	100	100	94.3	12.3	-



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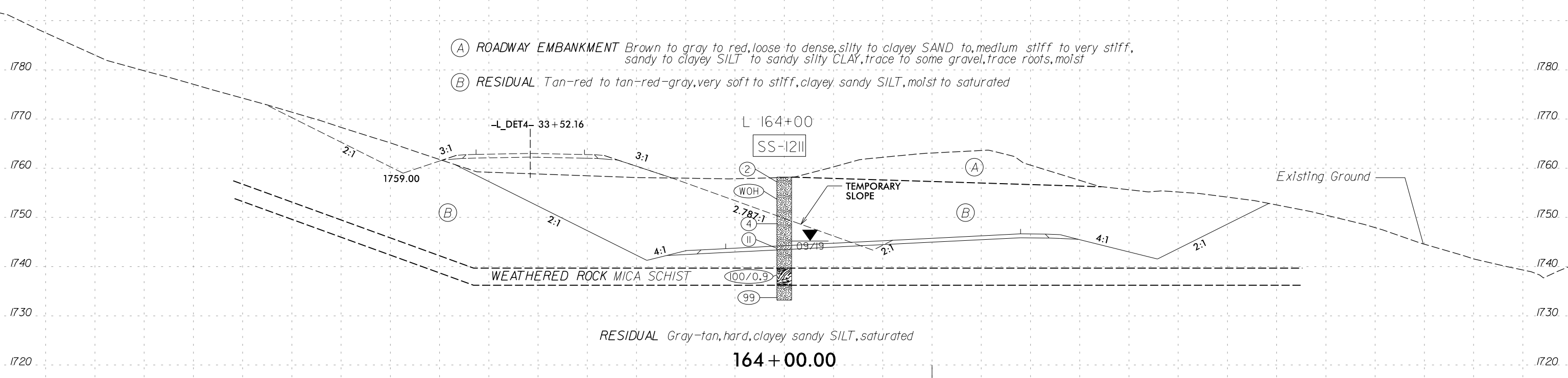


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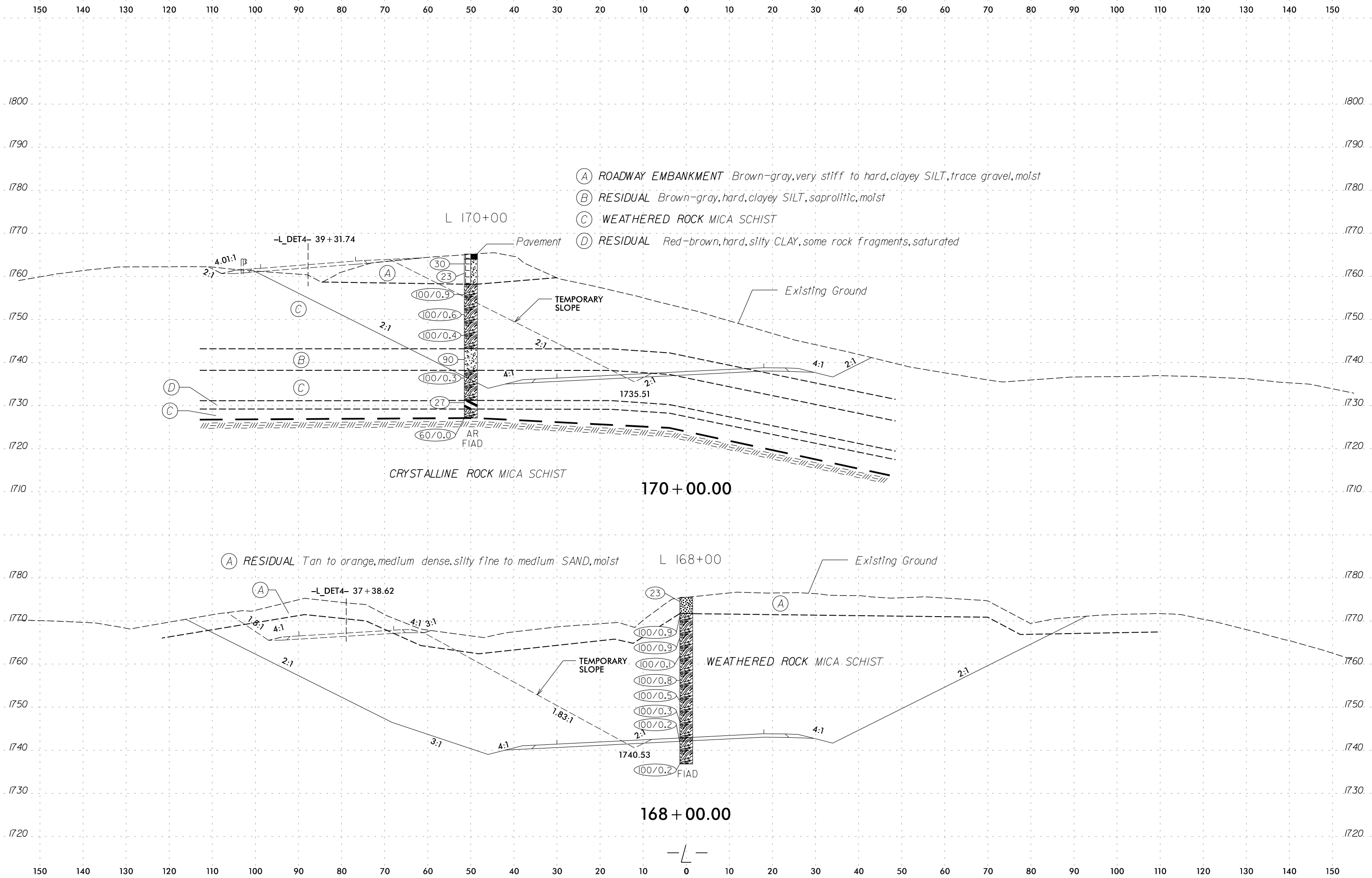
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1211	164+00	30' LT	3.5-5.0	A-4 (2)	40	6	13	28	39	20	78	71	54.5	21.9	-

- (A) ROADWAY EMBANKMENT Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist
- (B) RESIDUAL Tan-red to tan-red-gray, very soft to stiff, clayey sandy SILT, moist to saturated



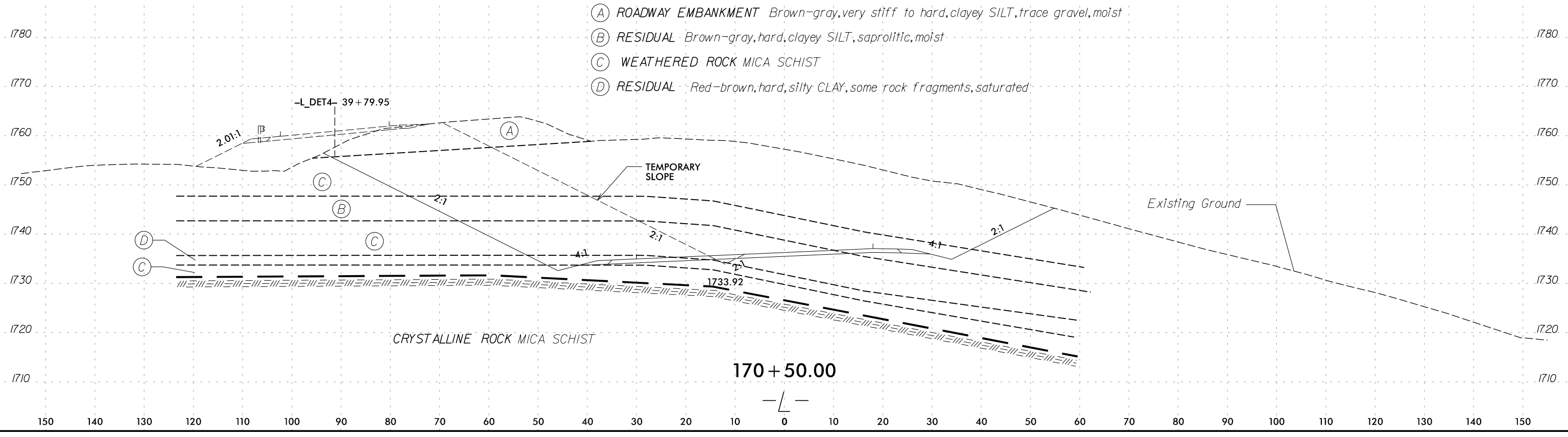
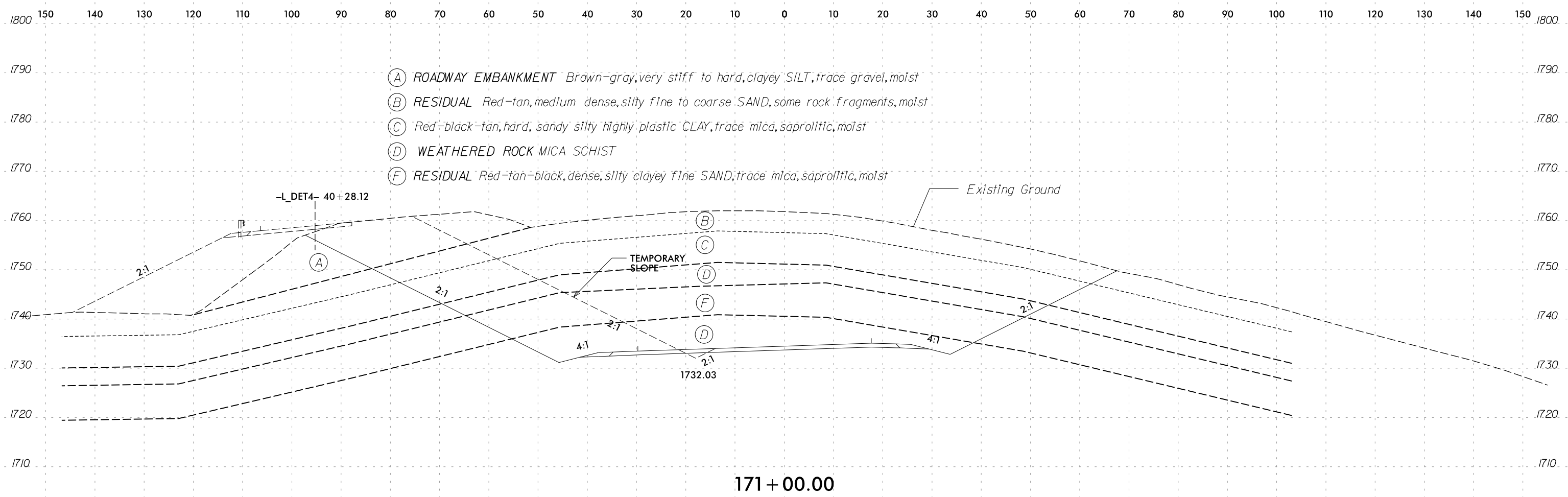
RESIDUAL Gray-tan, hard, clayey sandy SILT, saturated

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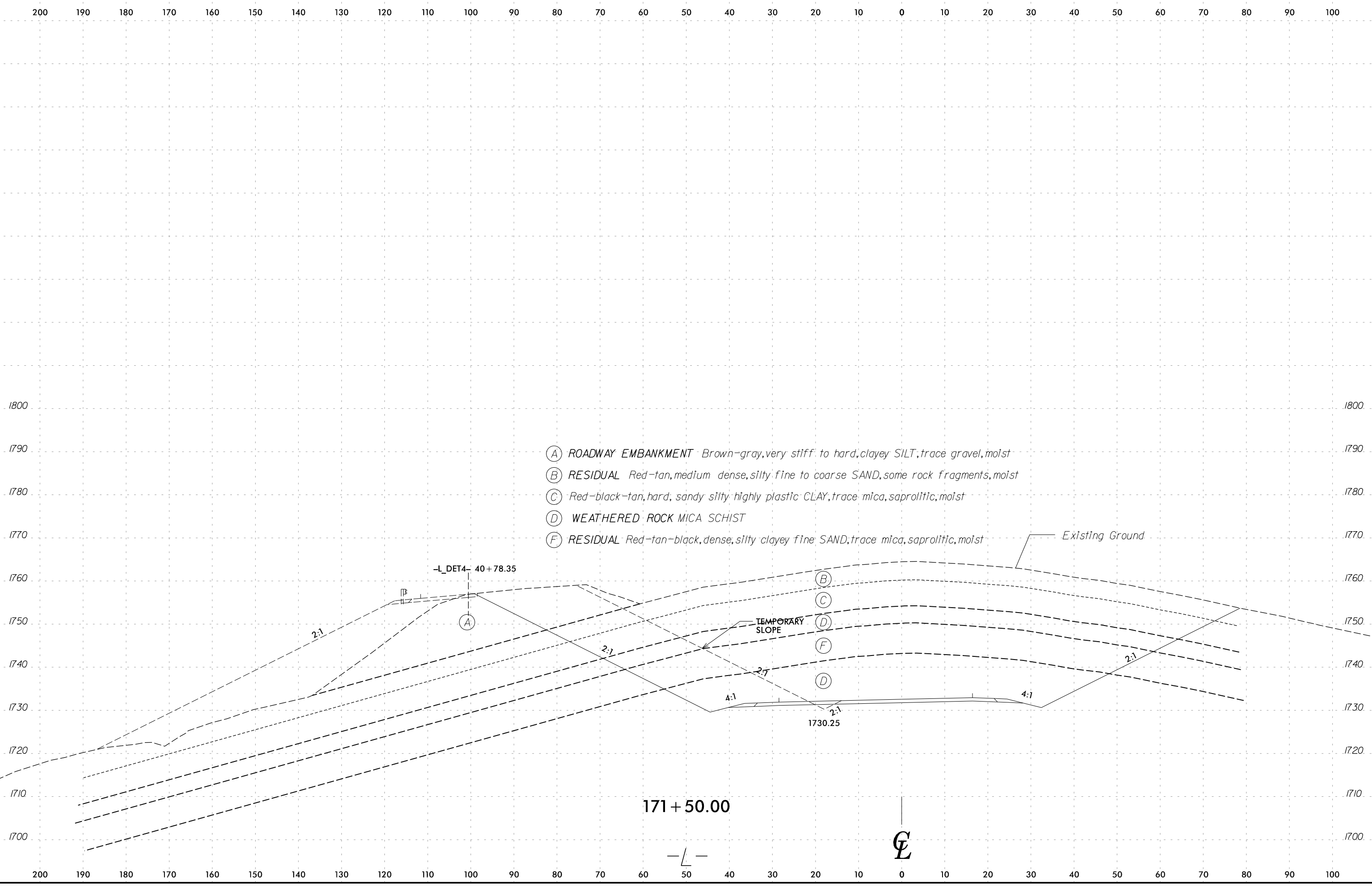


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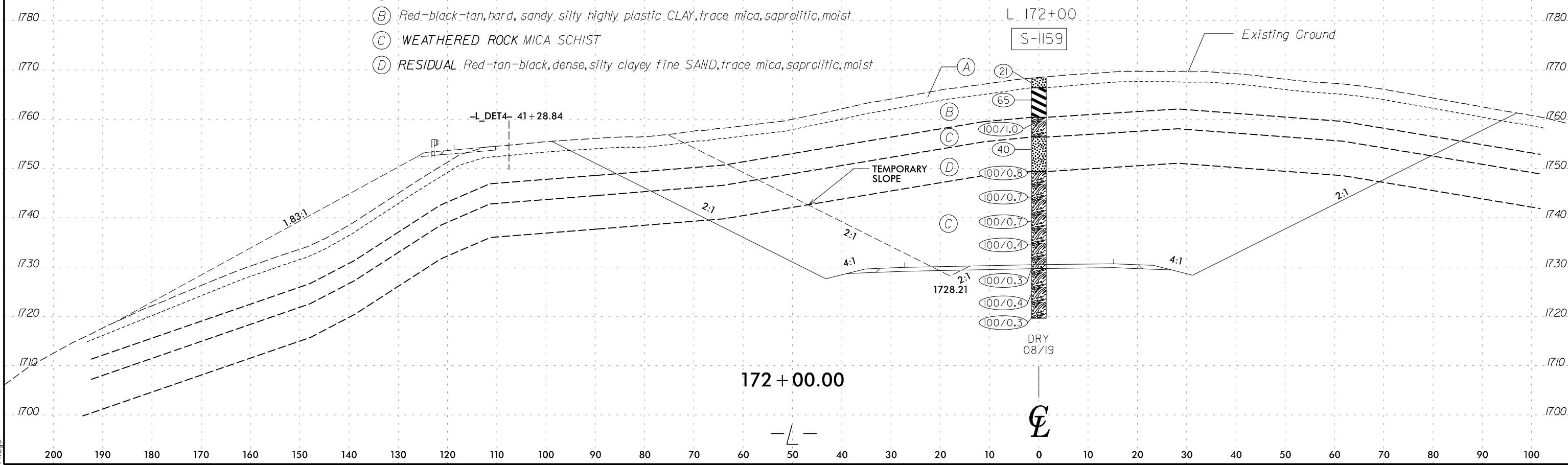
- (A) ROADWAY EMBANKMENT Brown-gray, very stiff to hard, clayey SILT, trace gravel, moist
- (B) RESIDUAL Red-tan, medium dense, silty fine to coarse SAND, some rock fragments, moist
- (C) Red-black-tan, hard, sandy silty highly plastic CLAY, trace mica, saprolitic, moist
- (D) WEATHERED ROCK MICA SCHIST
- (F) RESIDUAL Red-tan-black, dense, silty clayey fine SAND, trace mica, saprolitic, moist

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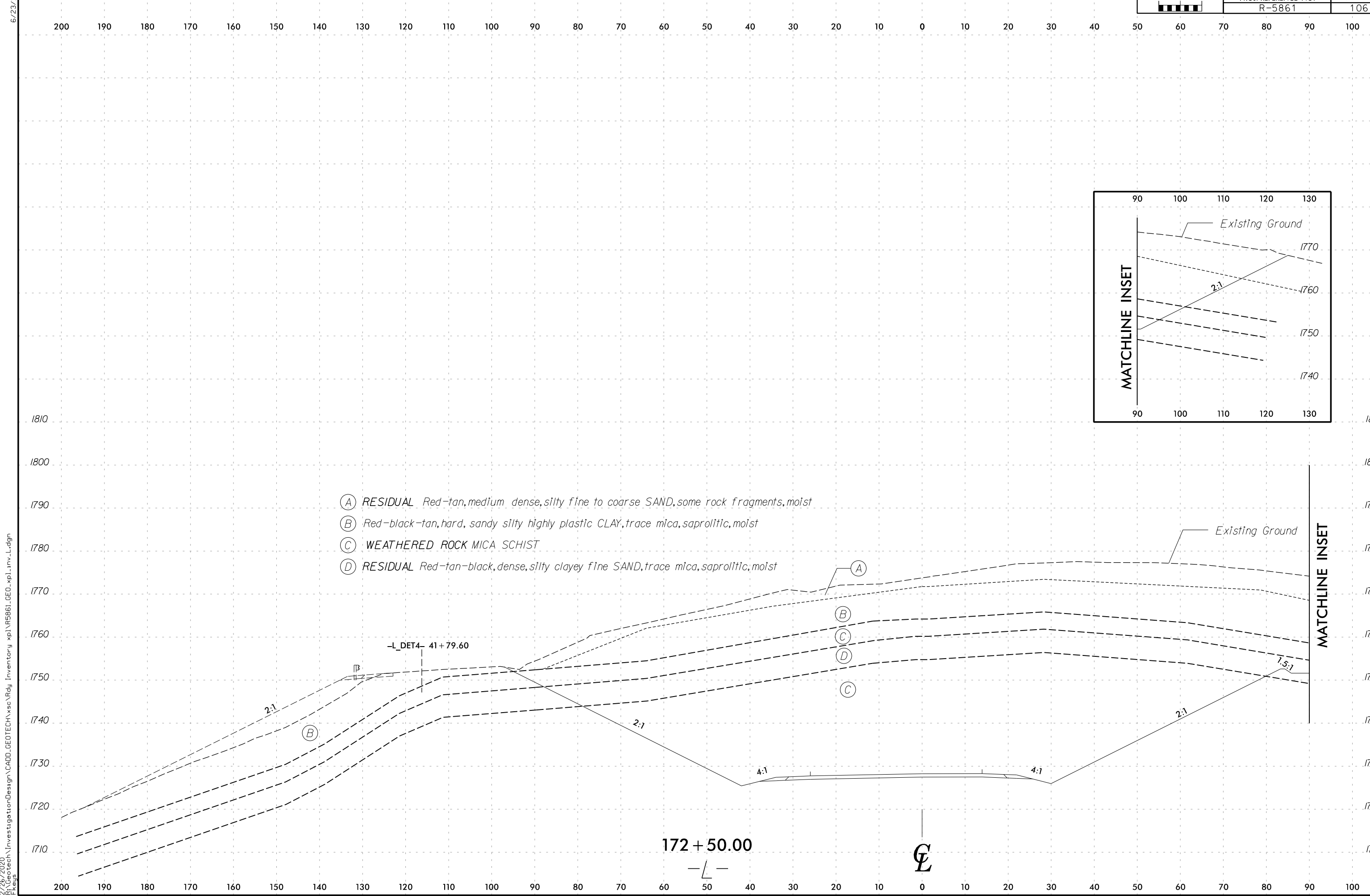
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
S-1159	172+00	0	2.0-8.0	A-7-5 (23)	64	31	12	32	31	25	97	89	70.8	ND	-

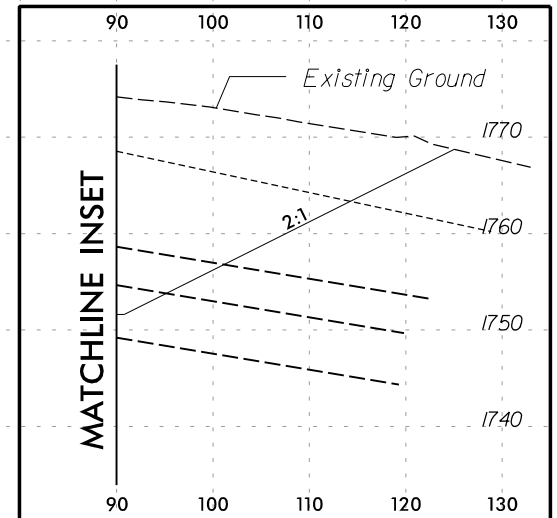
- (A) RESIDUAL Red-tan, medium dense, silty fine to coarse SAND, some rock fragments, moist
- (B) Red-black-tan, hard, sandy silty highly plastic CLAY, trace mica, saprolitic, moist
- (C) WEATHERED ROCK MICA SCHIST
- (D) RESIDUAL Red-tan-black, dense, silty clayey fine SAND, trace mica, saprolitic, moist



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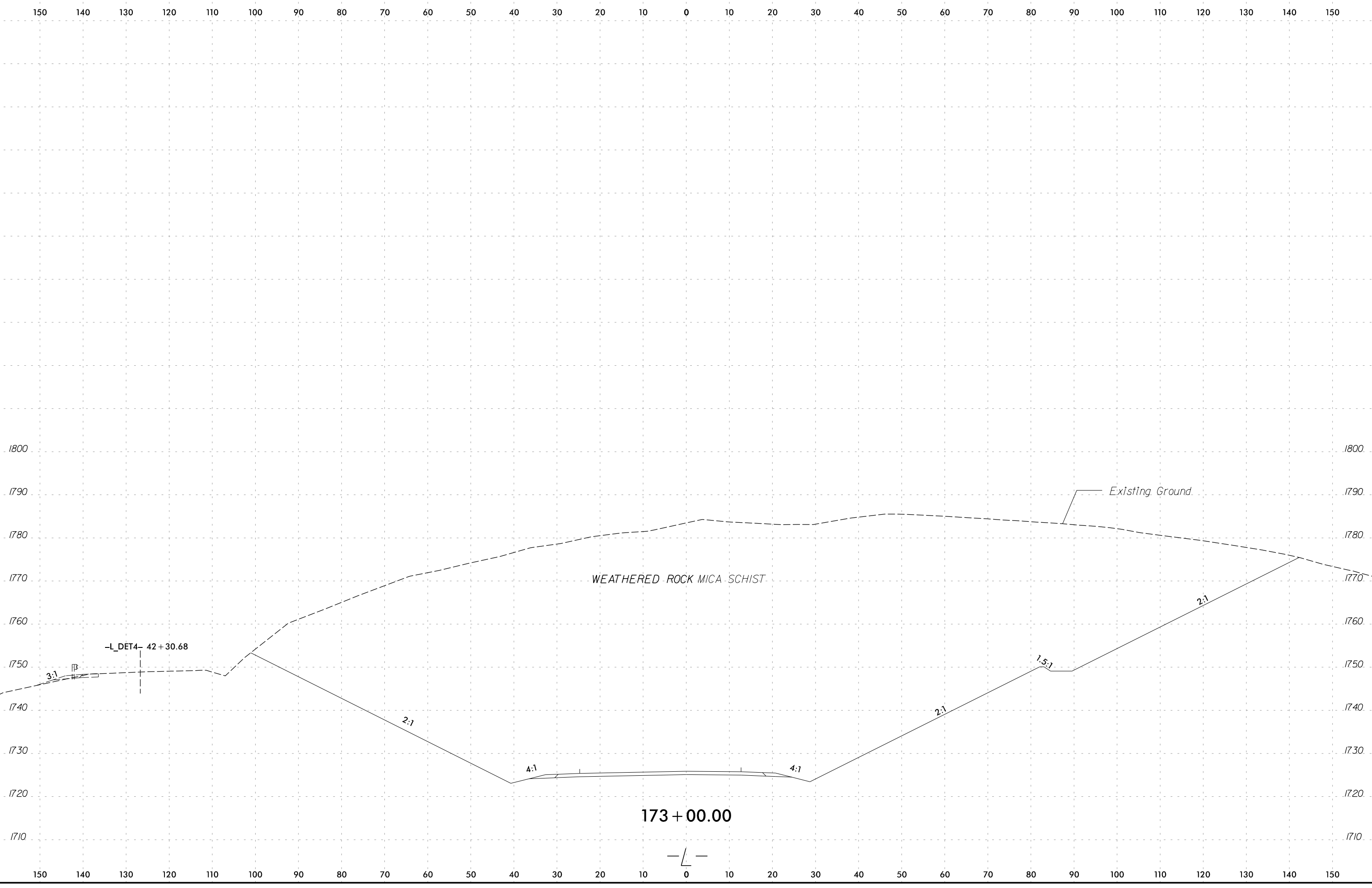


- (A) RESIDUAL Red-tan, medium dense, silty fine to coarse SAND, some rock fragments, moist
- (B) Red-black-tan, hard, sandy silty highly plastic CLAY, trace mica, saprolitic, moist
- (C) WEATHERED ROCK MICA SCHIST
- (D) RESIDUAL Red-tan-black, dense, silty clayey fine SAND, trace mica, saprolitic, moist



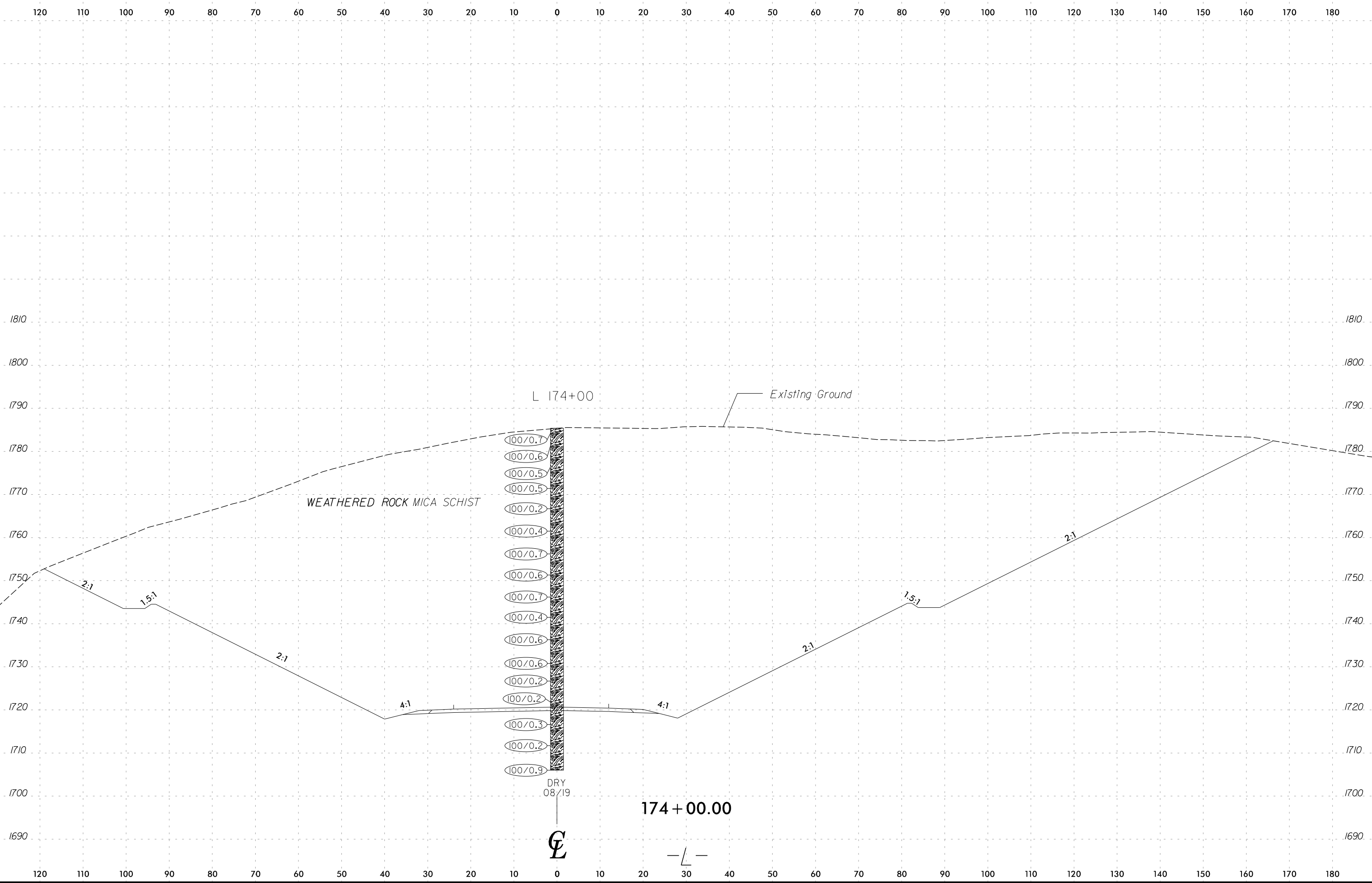
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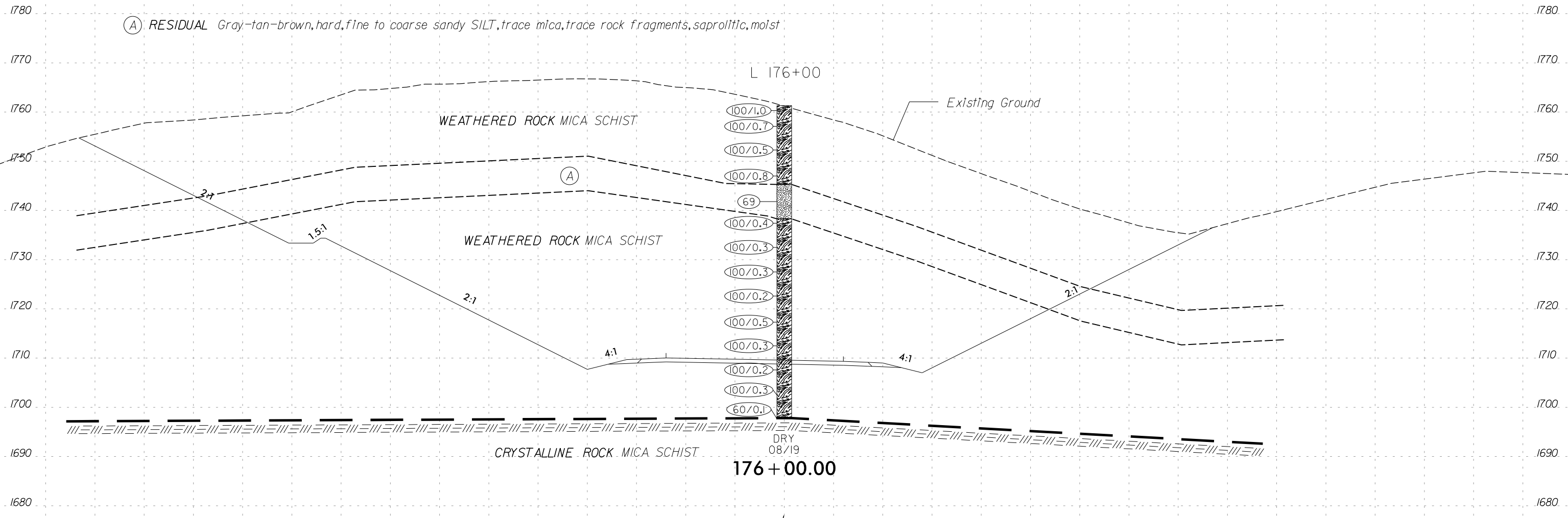
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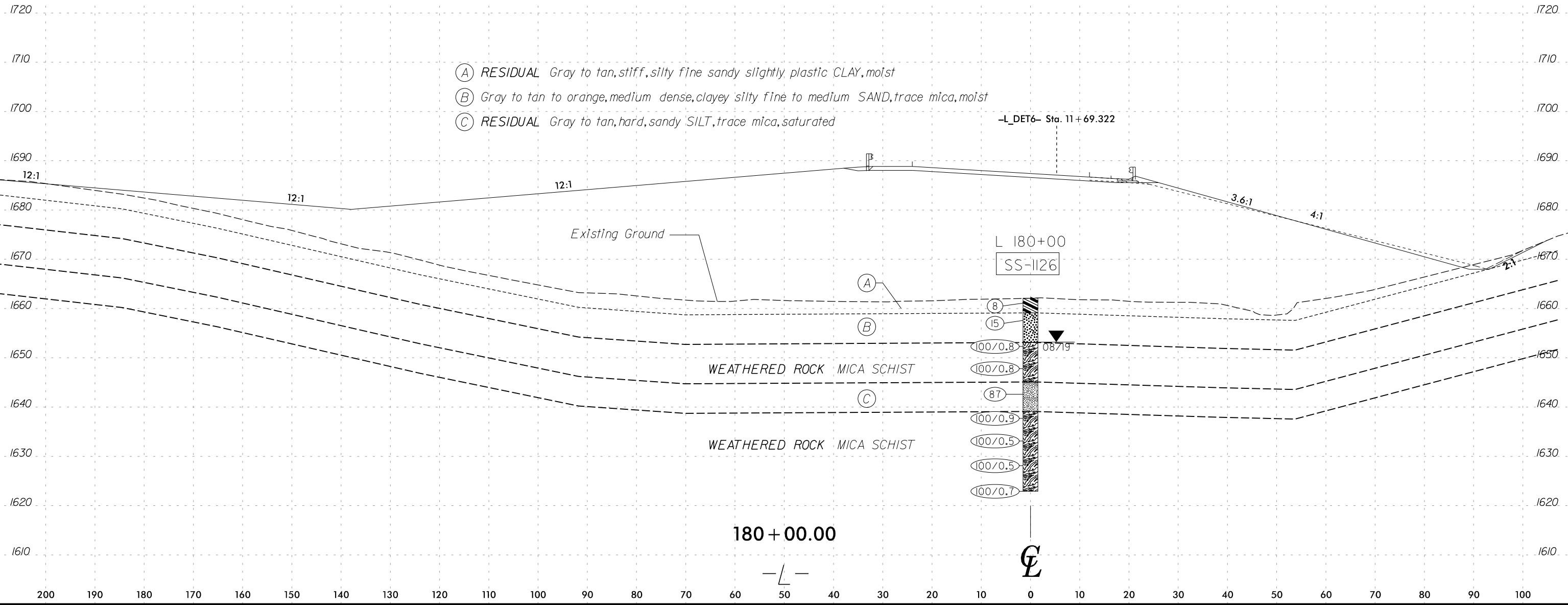


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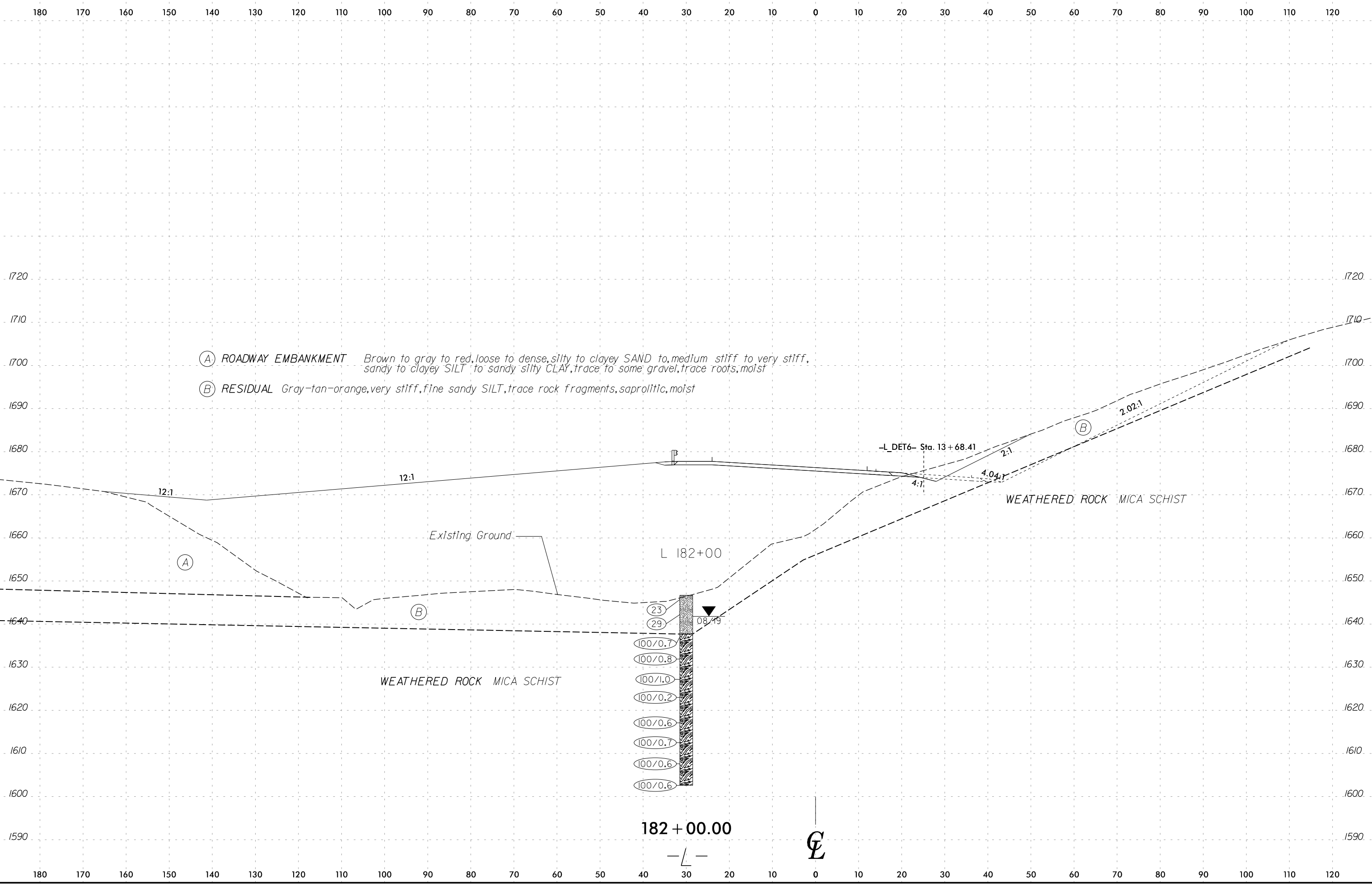
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1126	180+00	0	0.0-1.5	A-6 (8)	38	11	6	27	33	34	96	92	73.9	23	-

- (A) RESIDUAL Gray to tan, stiff, silty fine sandy slightly plastic CLAY, moist
- (B) Gray to tan to orange, medium dense, clayey silty fine to medium SAND, trace mica, moist
- (C) RESIDUAL Gray to tan, hard, sandy SILT, trace mica, saturated



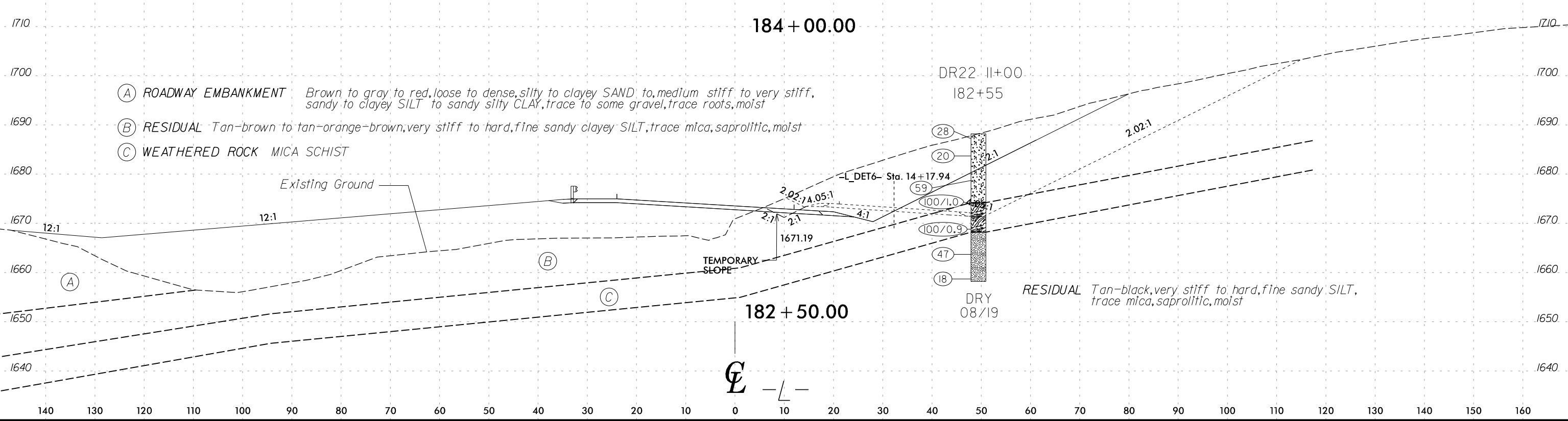
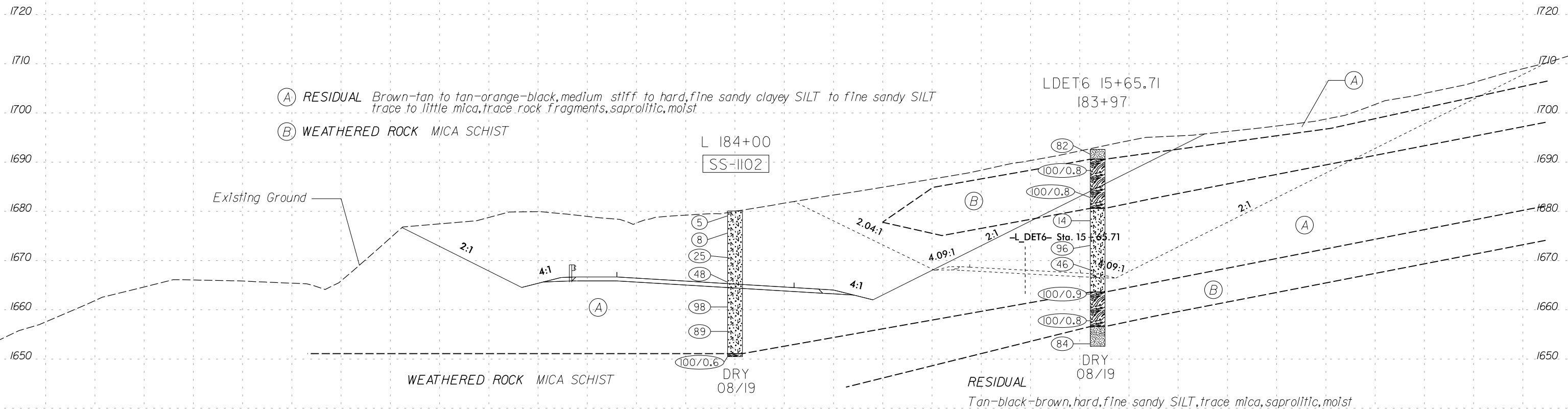
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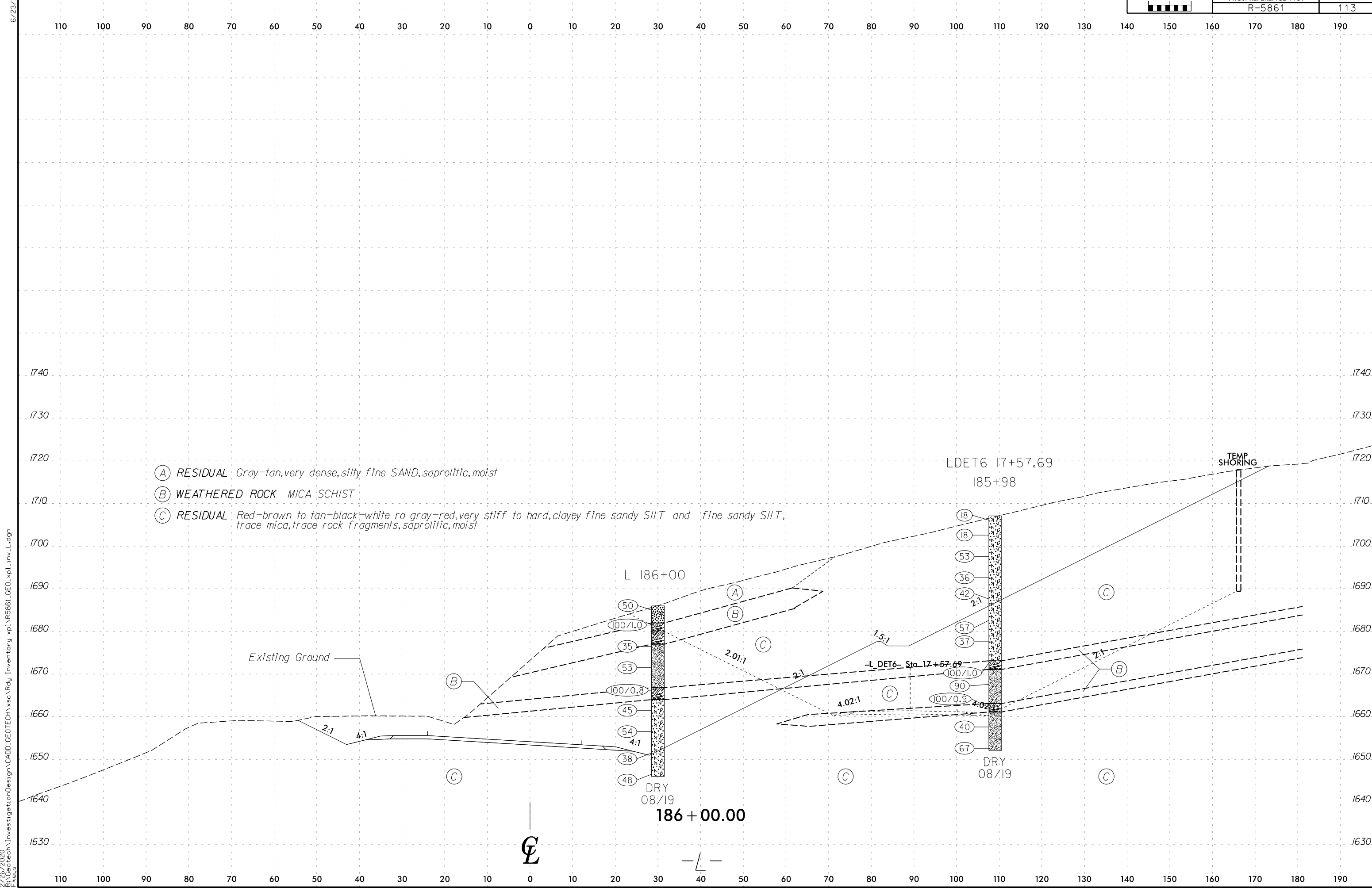
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SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1102	184+00	0	0.0-1.5	A-5 (5)	41	7	15	26	31	28	93	82	64.8	21.4	-



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- (A) RESIDUAL Gray-tan, very dense, silty fine SAND, saprolitic, moist
- (B) WEATHERED ROCK MICA SCHIST
- (C) RESIDUAL Red-brown to tan-black-white to gray-red, very stiff to hard, clayey fine sandy SILT and fine sandy SILT, trace mica, trace rock fragments, saprolitic, moist

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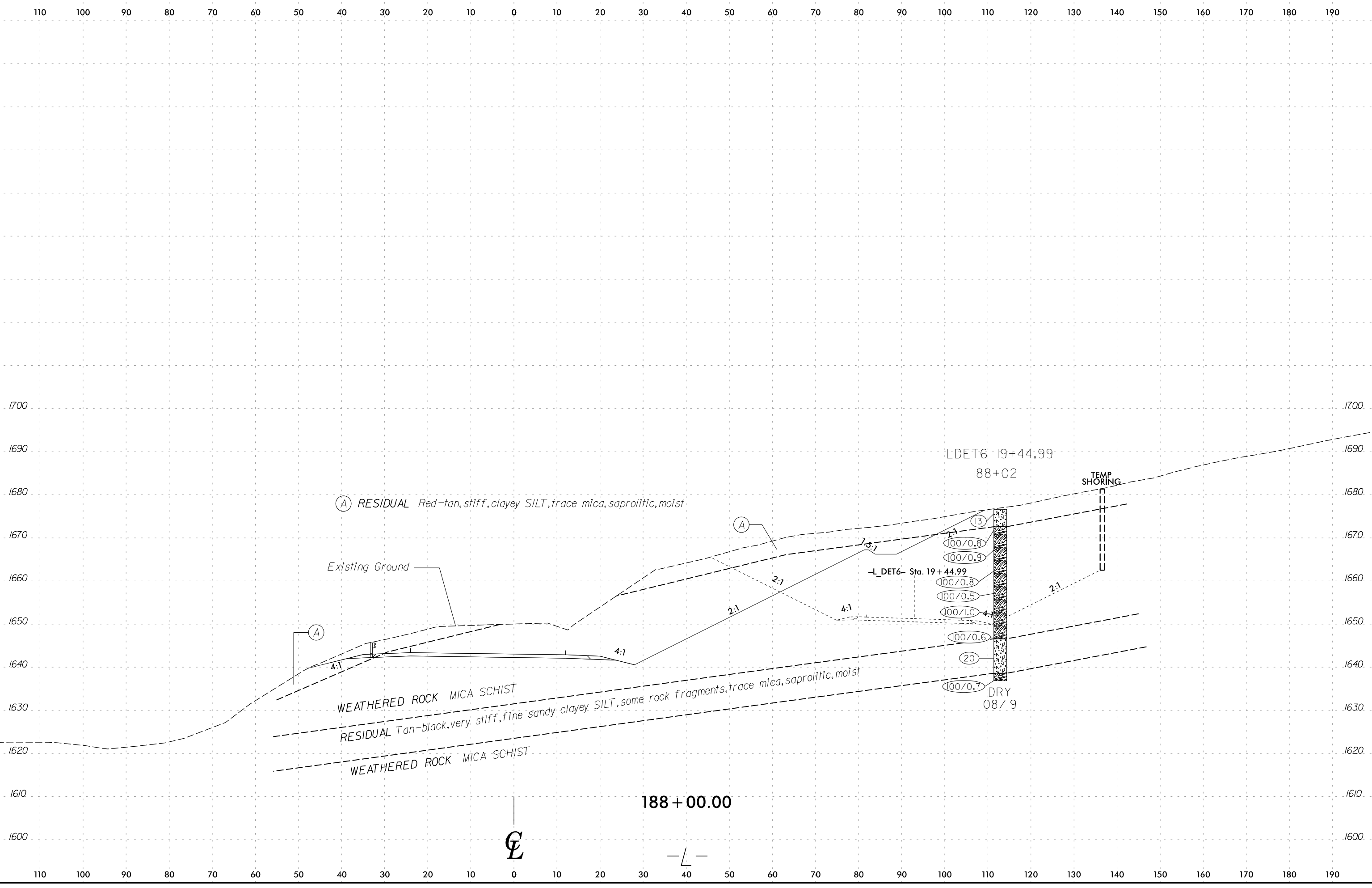
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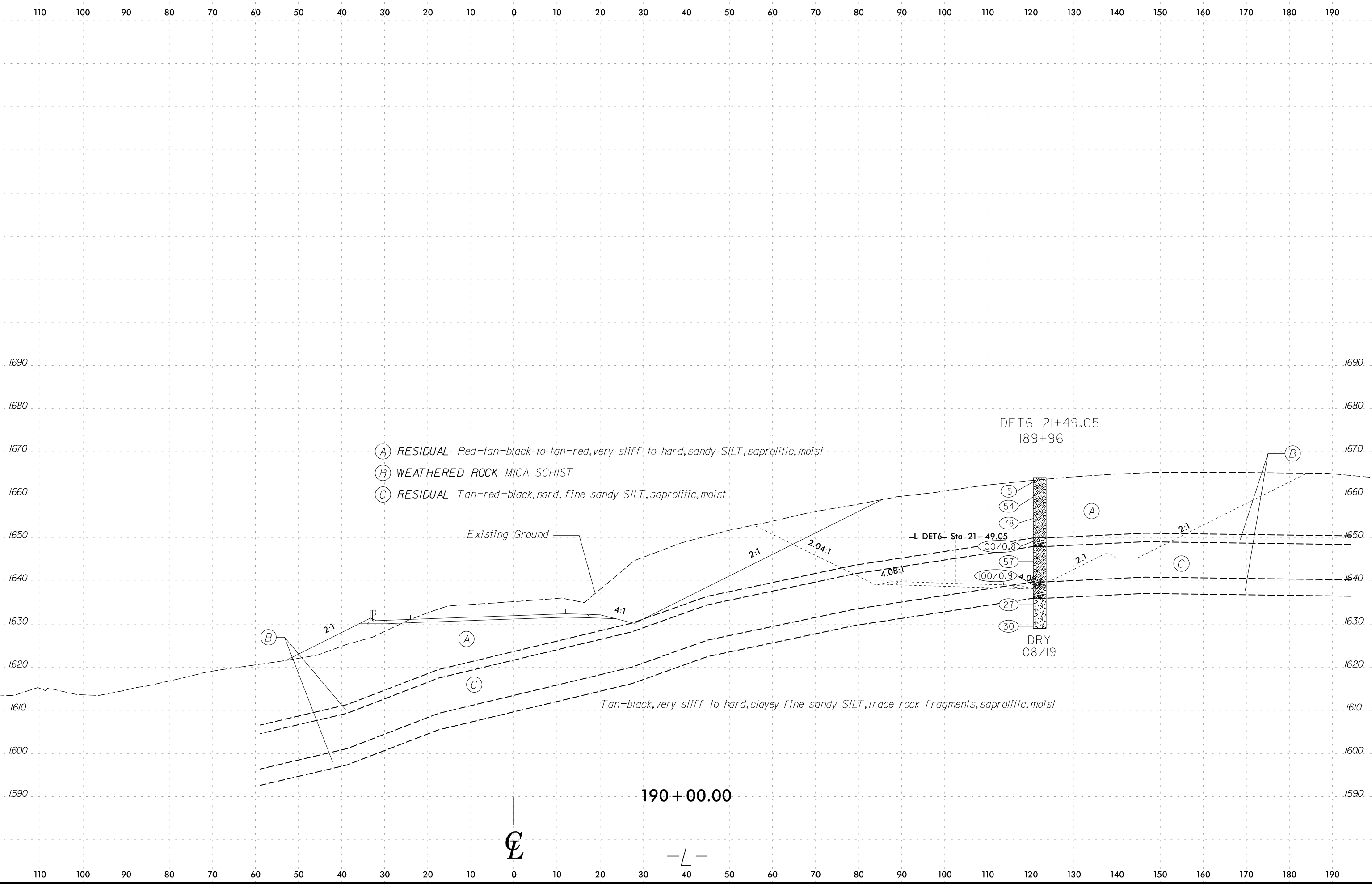
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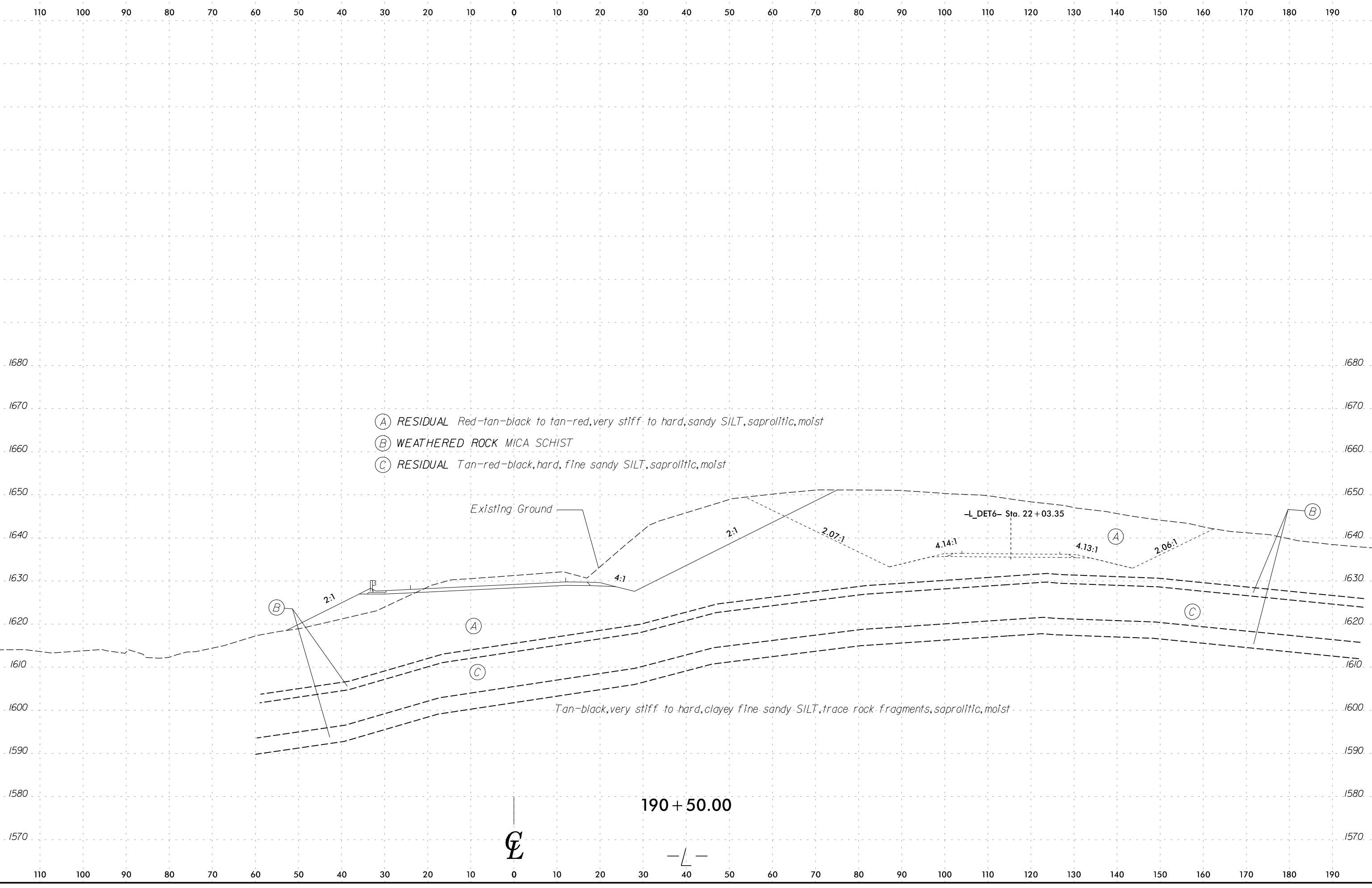
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- (A) RESIDUAL Red-tan-black to tan-red, very stiff to hard, sandy SILT, saprolitic, moist
- (B) WEATHERED ROCK MICA SCHIST
- (C) RESIDUAL Tan-red-black, hard, fine sandy SILT, saprolitic, moist

Existing Ground

-L\_DET6- Sta. 22+03.35

Tan-black, very stiff to hard, clayey fine sandy SILT, trace rock fragments, saprolitic, moist

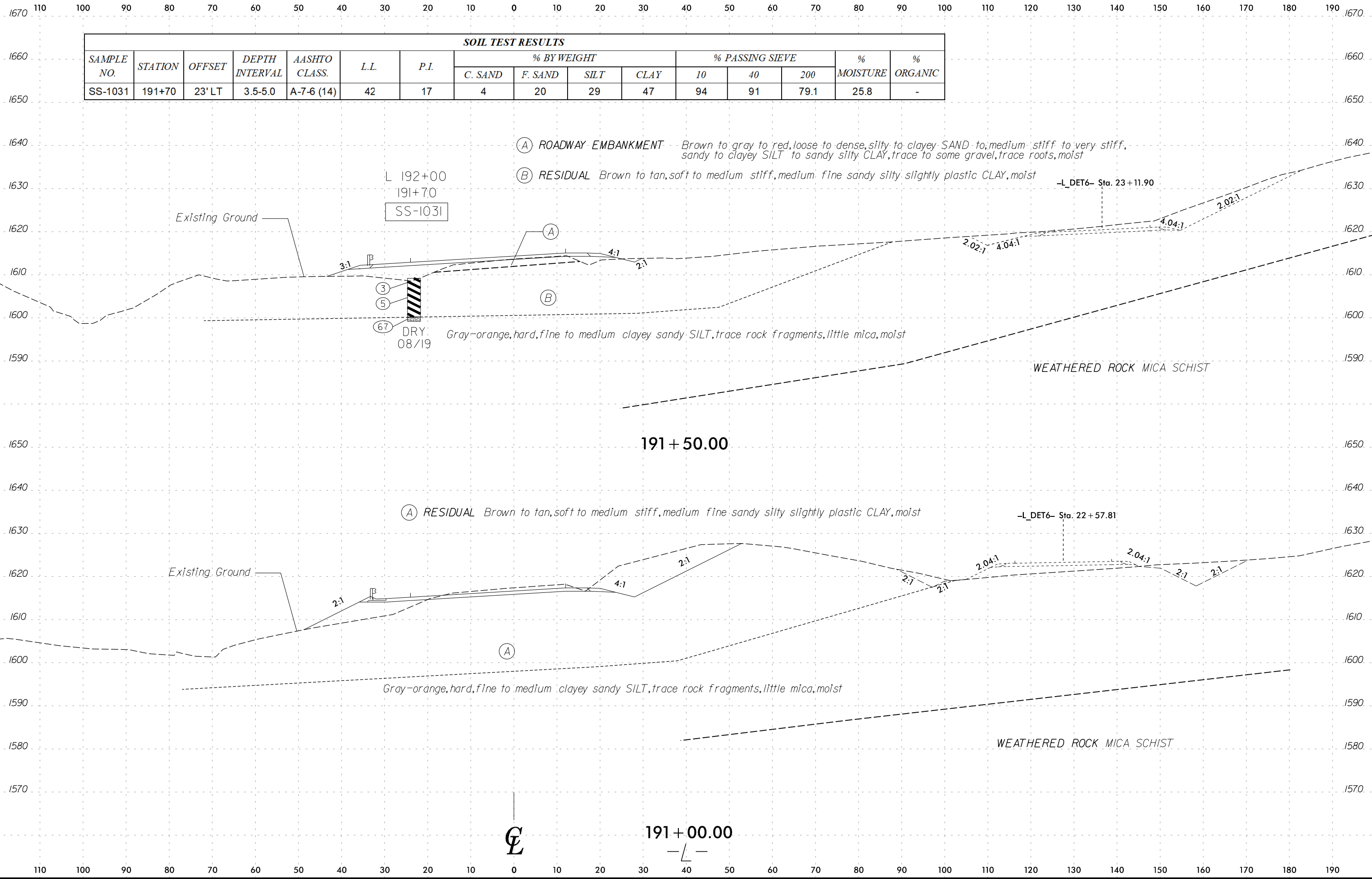
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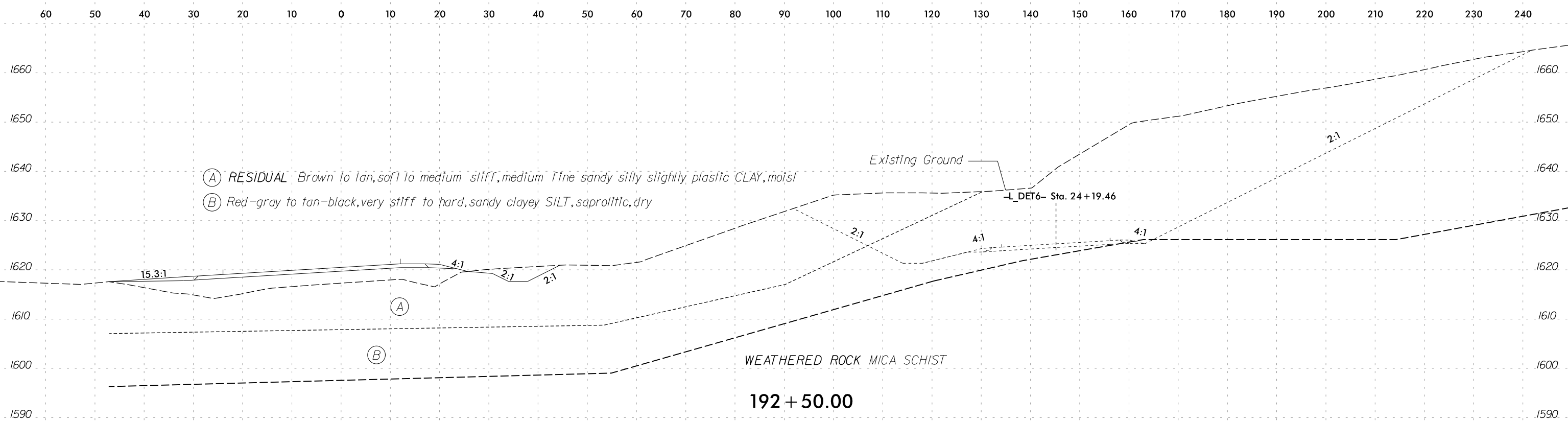
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1031	191+70	23' LT	3.5-5.0	A-7-6 (14)	42	17	4	20	29	47	94	91	79.1	25.8	-

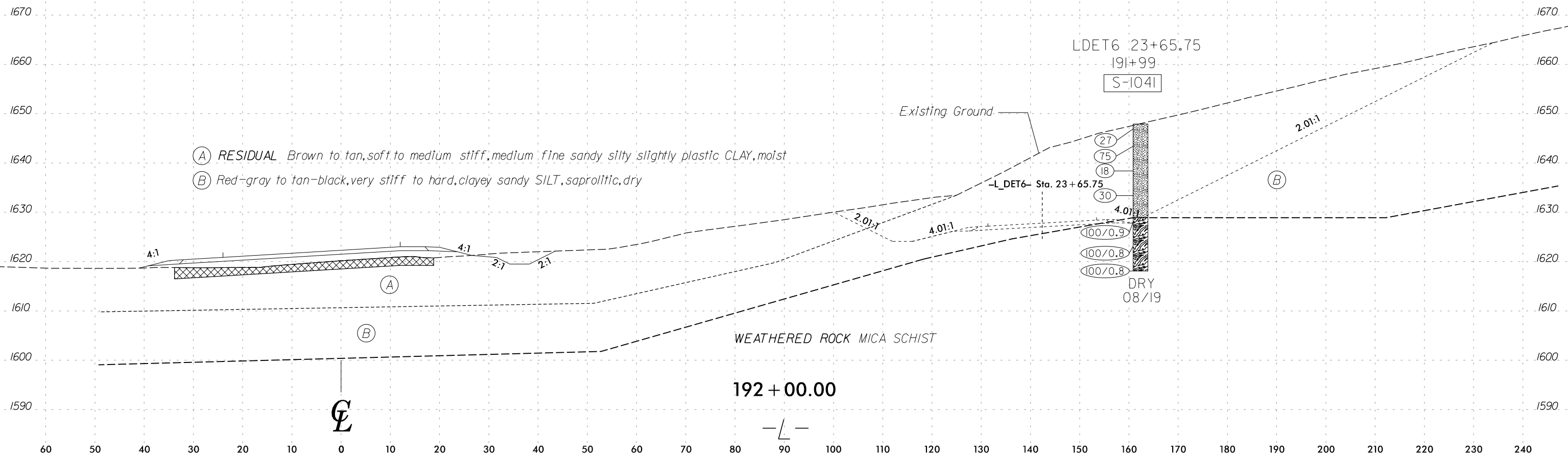


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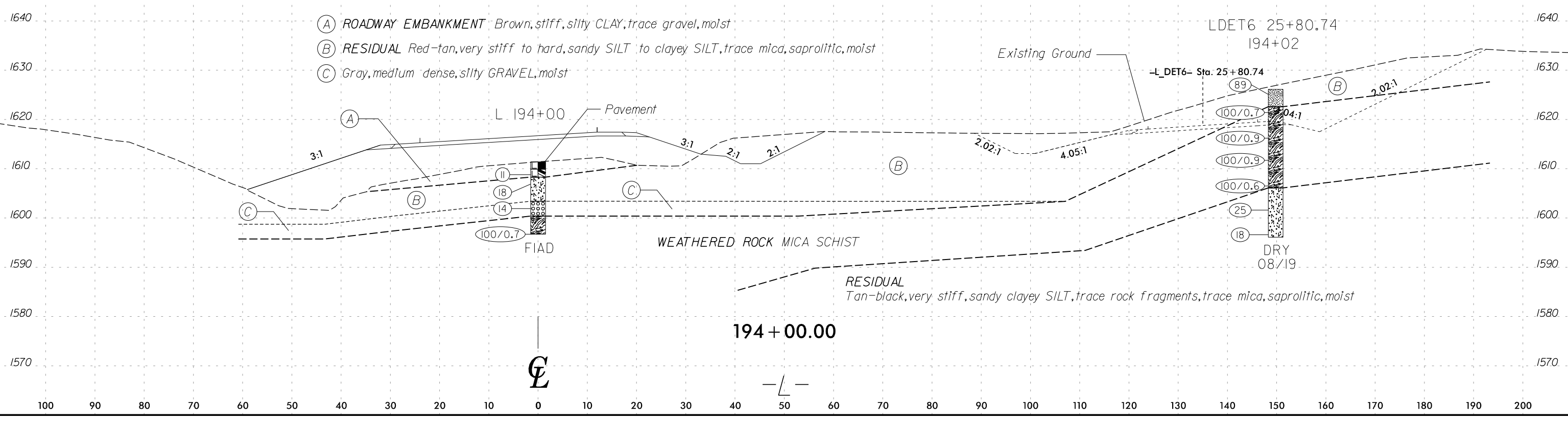
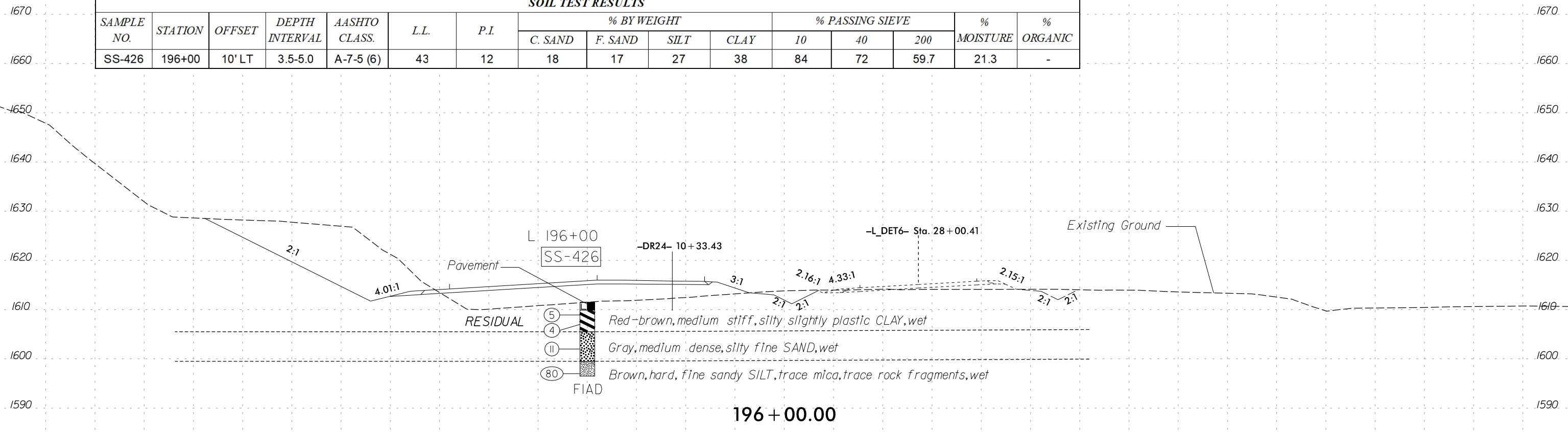
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
S-1041	191+99	162' RT	0.0-8.5	A-4 (8)	39	10	3	31	36	30	99	97	78.3	ND	-



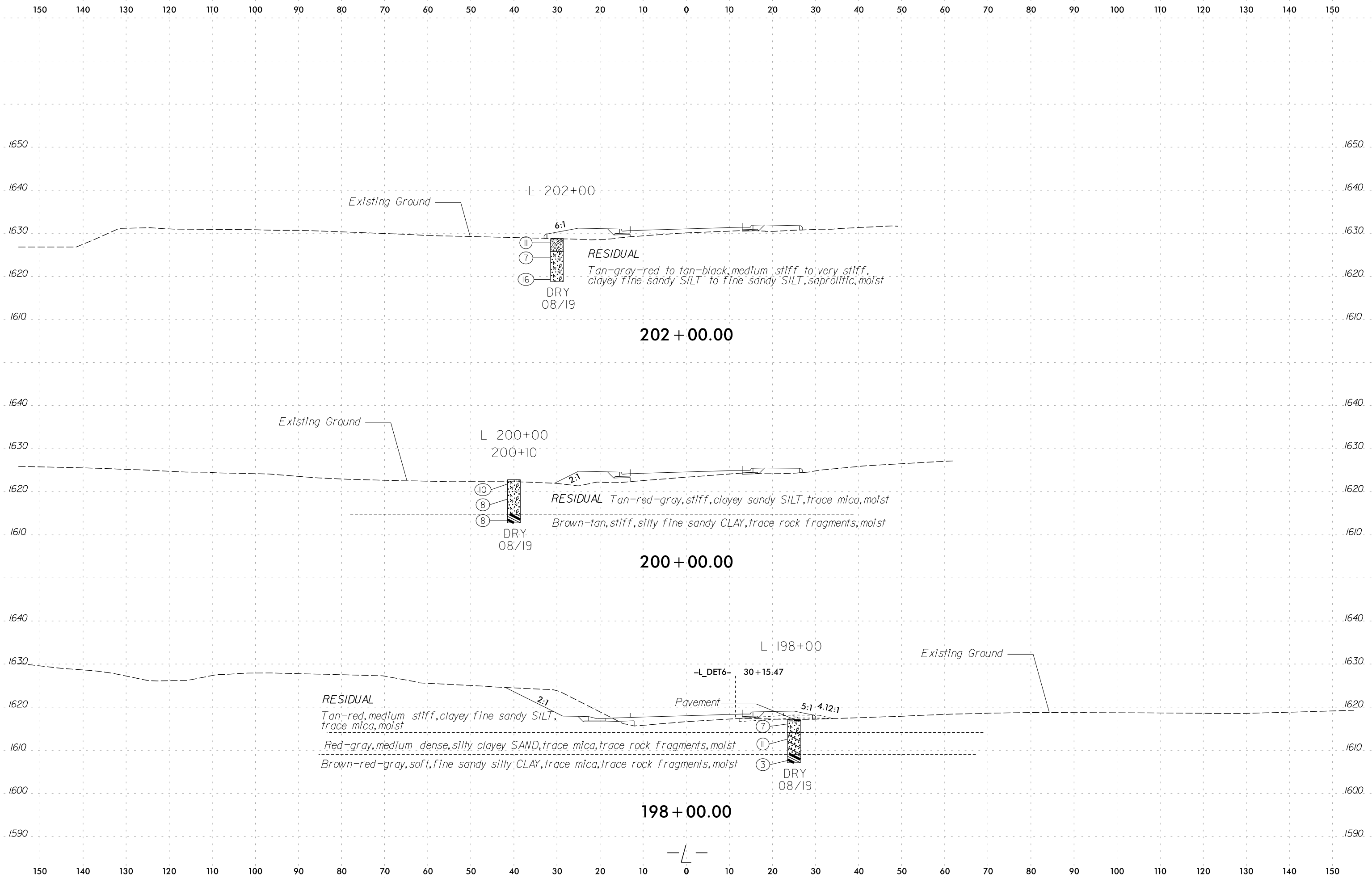
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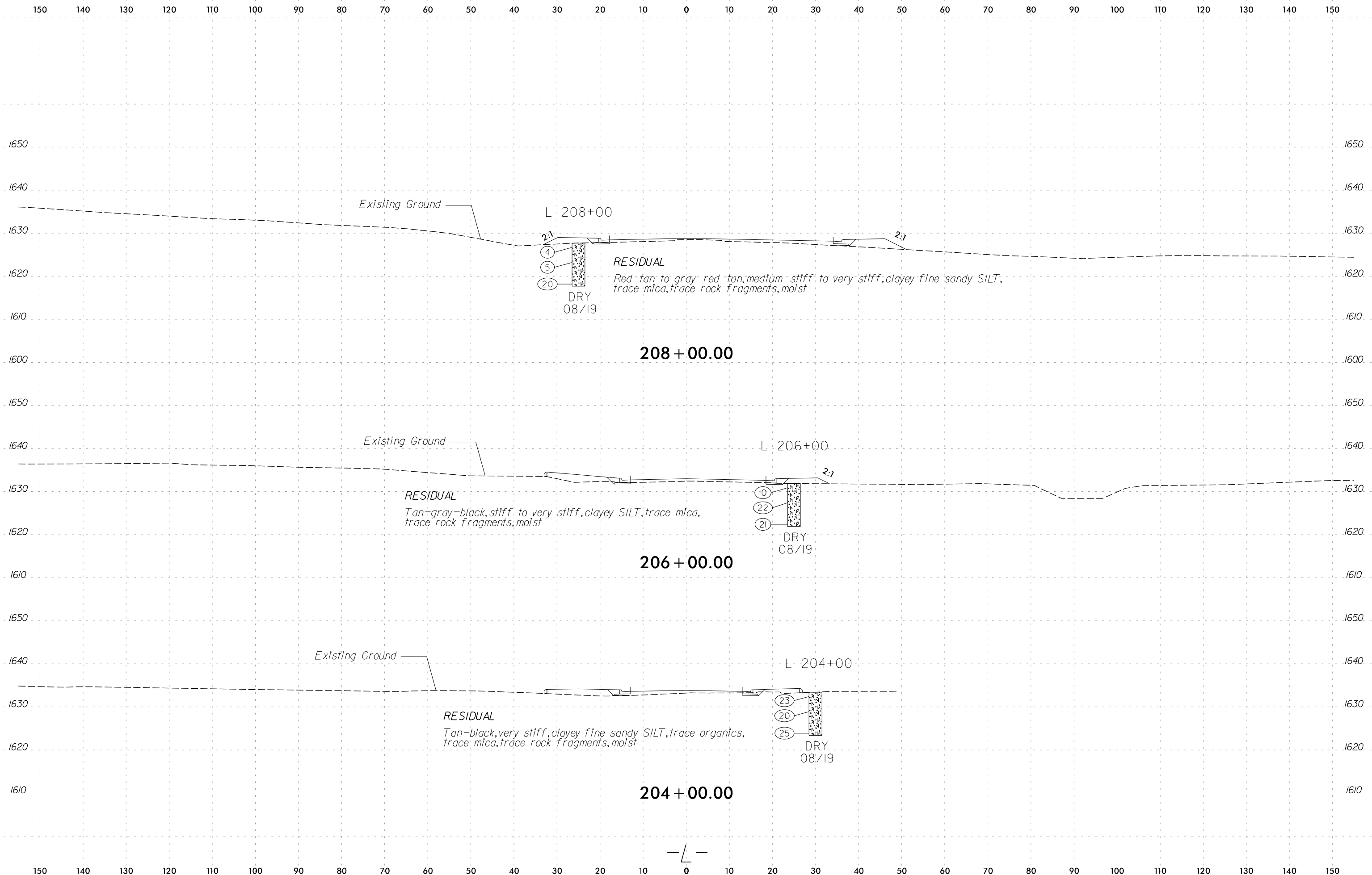
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SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-426	196+00	10' LT	3.5-5.0	A-7-5 (6)	43	12	18	17	27	38	84	72	59.7	21.3	-



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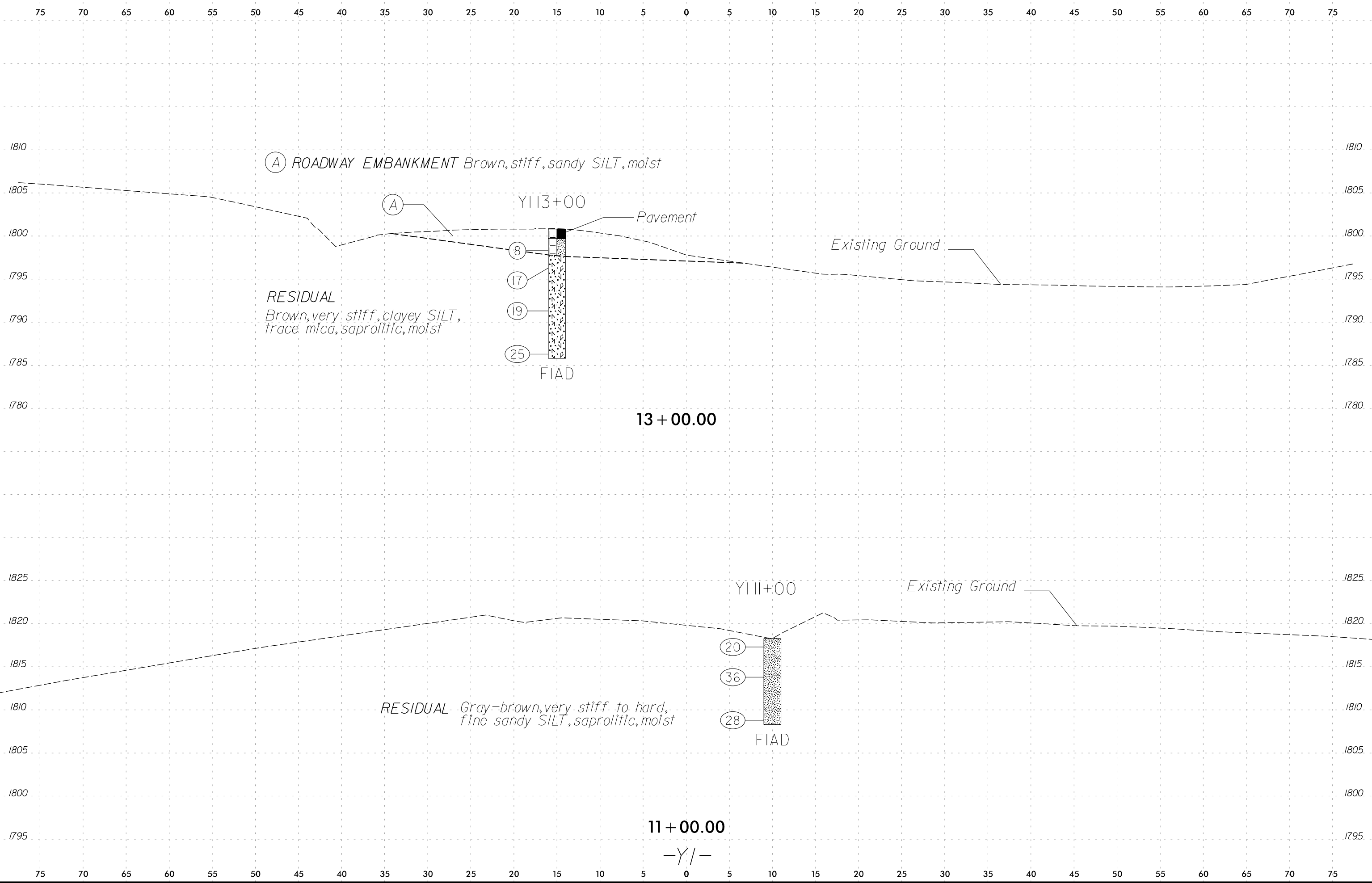


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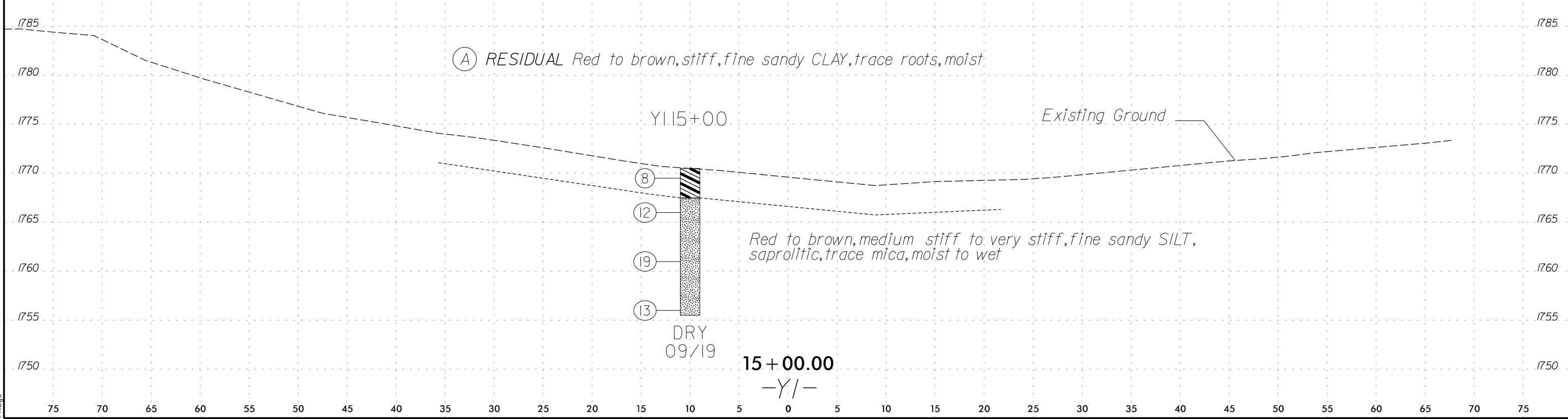
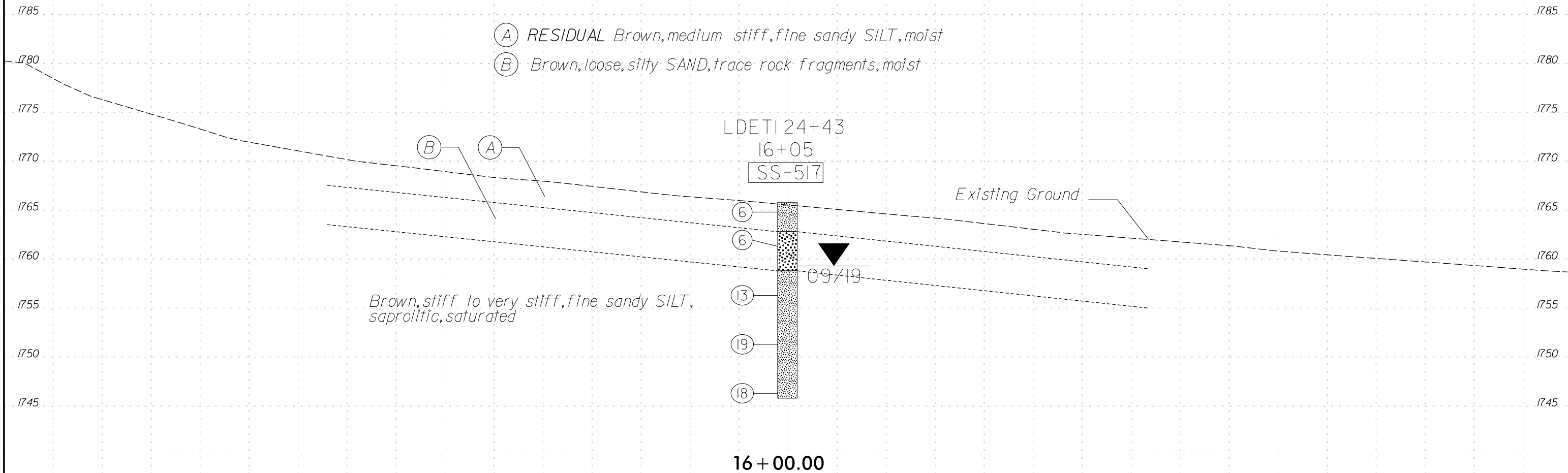
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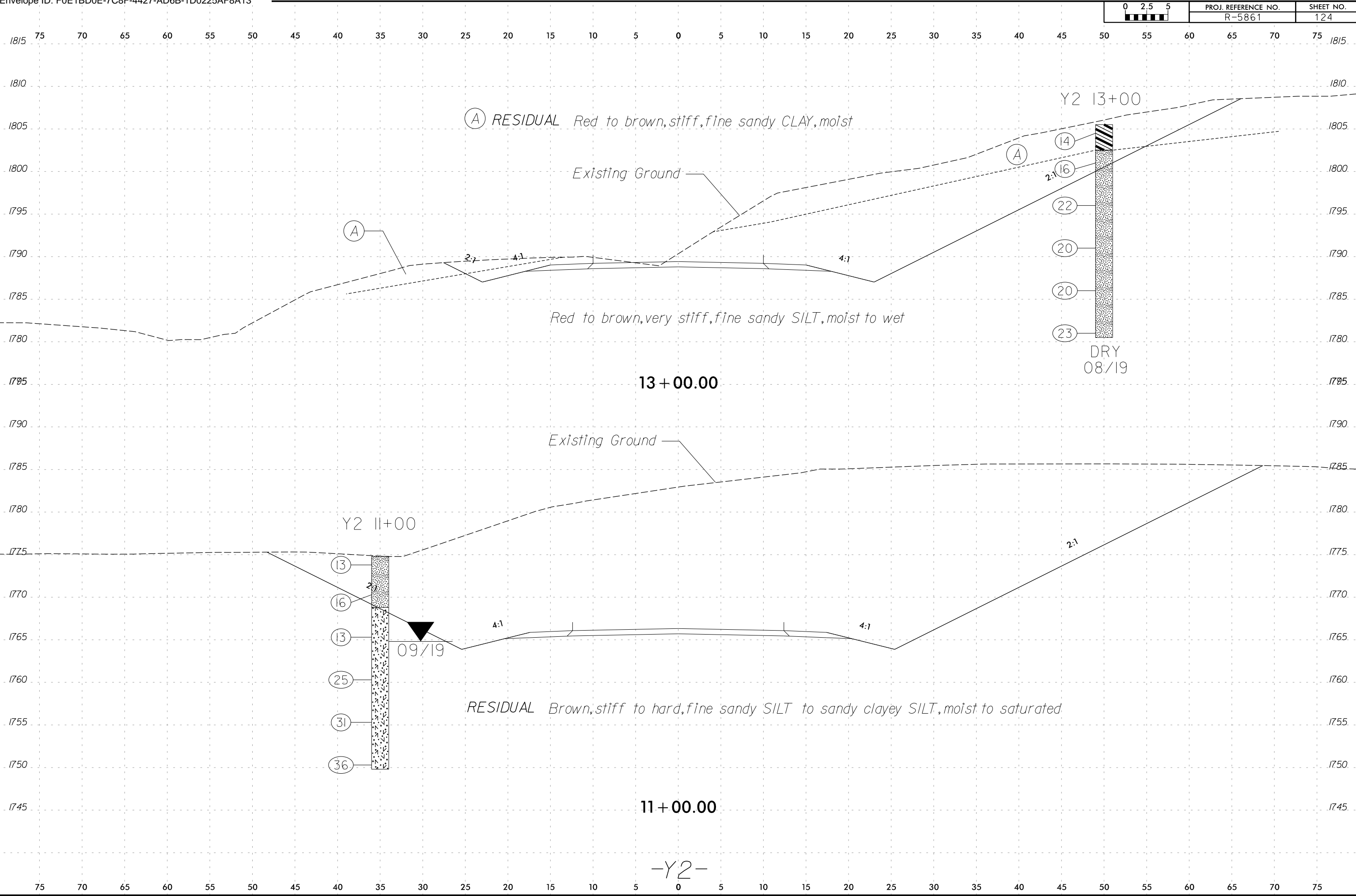
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SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-517	16+05	0	3.5-5.0	A-2-4 (0)	30	5	21	46	11	22	63	56	29.3	15.8	-



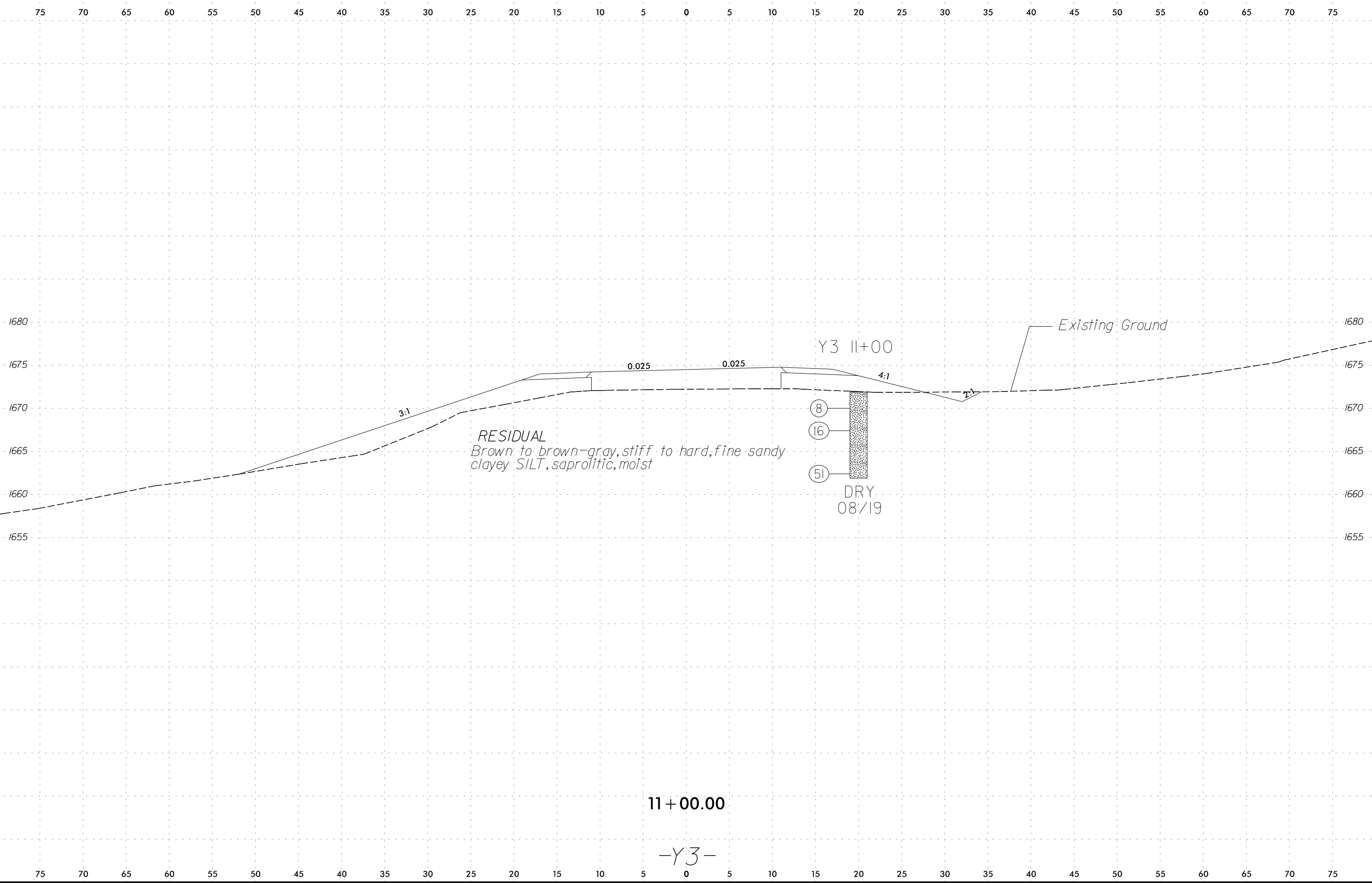
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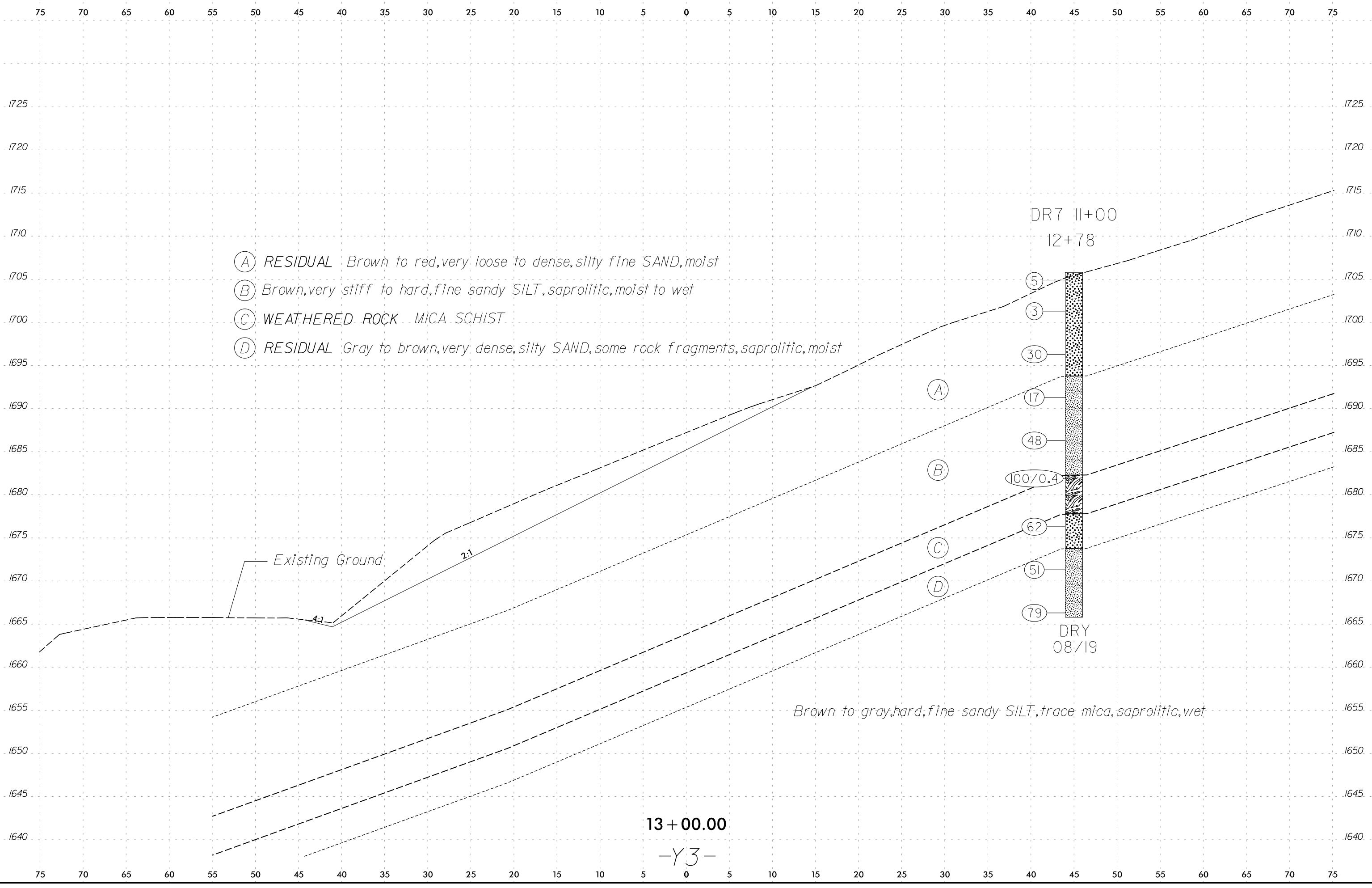


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- (A) RESIDUAL Brown to red, very loose to dense, silty fine SAND, moist
- (B) Brown, very stiff to hard, fine sandy SILT, saprolitic, moist to wet
- (C) WEATHERED ROCK MICA SCHIST
- (D) RESIDUAL Gray to brown, very dense, silty SAND, some rock fragments, saprolitic, moist

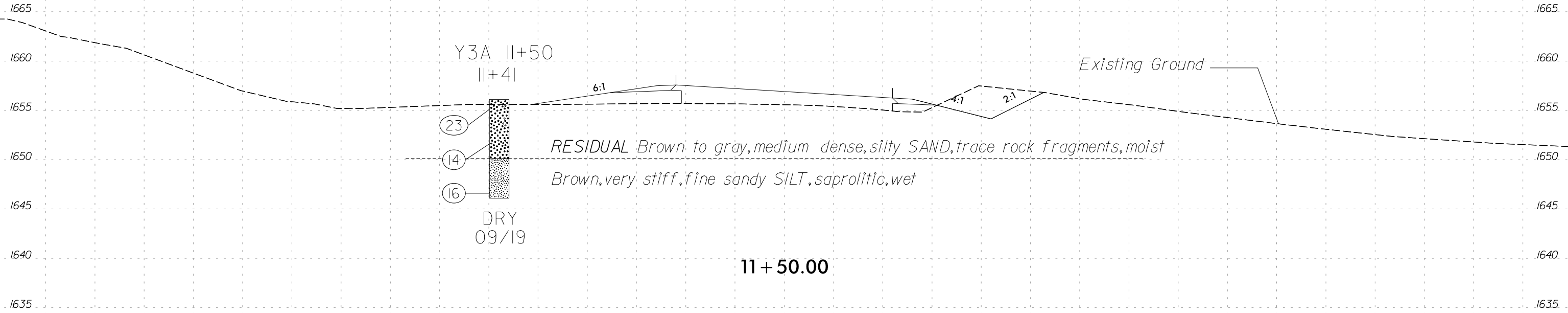
- (5)
- (3)
- (30)
- (17)
- (48)
- (100/0.4)
- (62)
- (51)
- (79)

- (A)
- (B)
- (C)
- (D)

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75 70 65 60 55 50 45 40 35 30 25 20 15 10 5 0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75



Y3A II+50  
II+41

(23)  
(14)  
(16)

RESIDUAL Brown to gray, medium dense, silty SAND, trace rock fragments, moist  
Brown, very stiff, fine sandy SILT, saprolitic, wet

DRY  
09/19

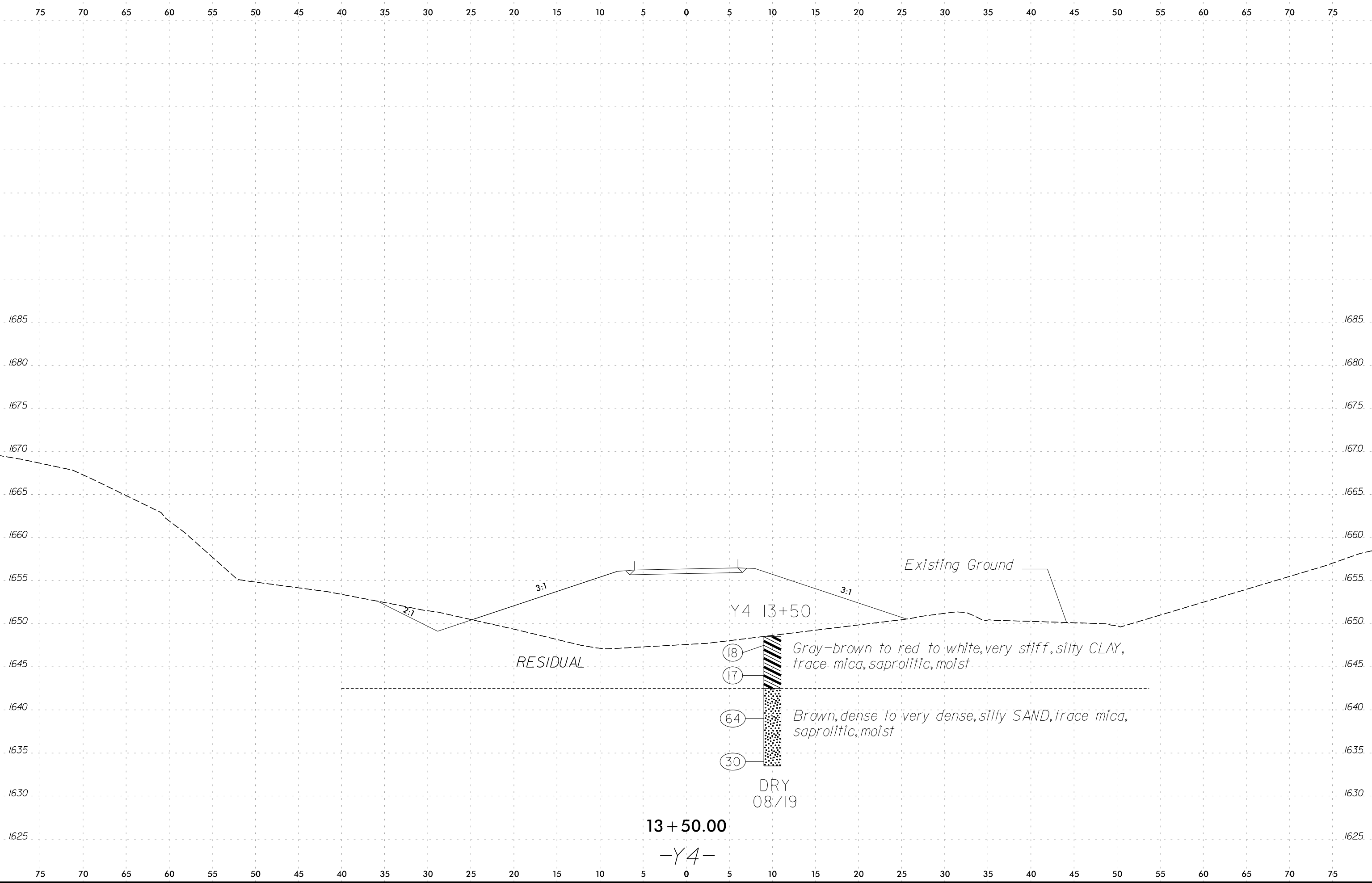
Existing Ground

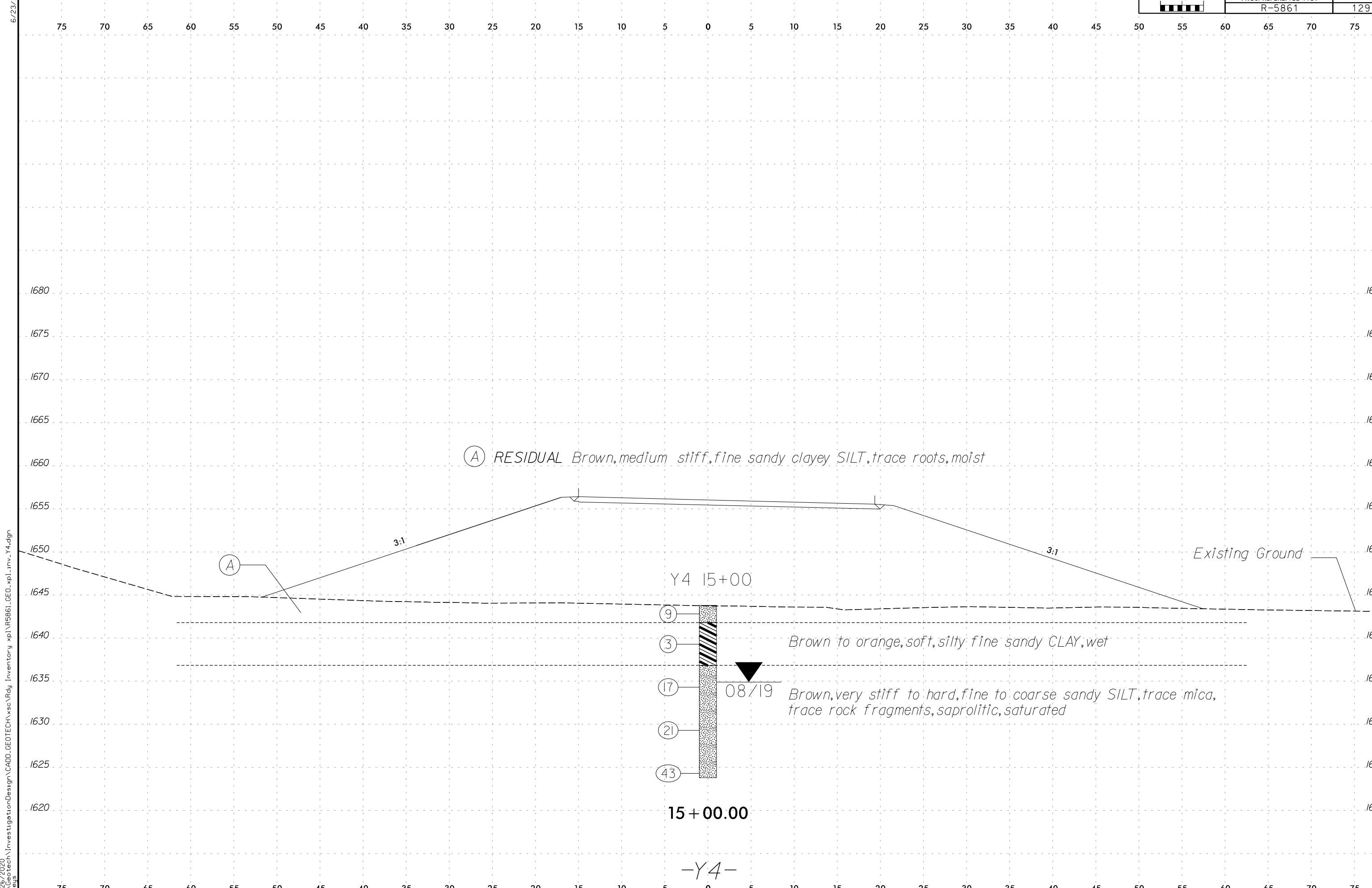
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(A) RESIDUAL *Brown, medium stiff, fine sandy clayey SILT, trace roots, moist*

(A)

Y4 15+00

(9)

(3)

*Brown to orange, soft, silty fine sandy CLAY, wet*

(17)

08/19

*Brown, very stiff to hard, fine to coarse sandy SILT, trace mica, trace rock fragments, saprolitic, saturated*

(21)

(43)

15+00.00

-Y4-

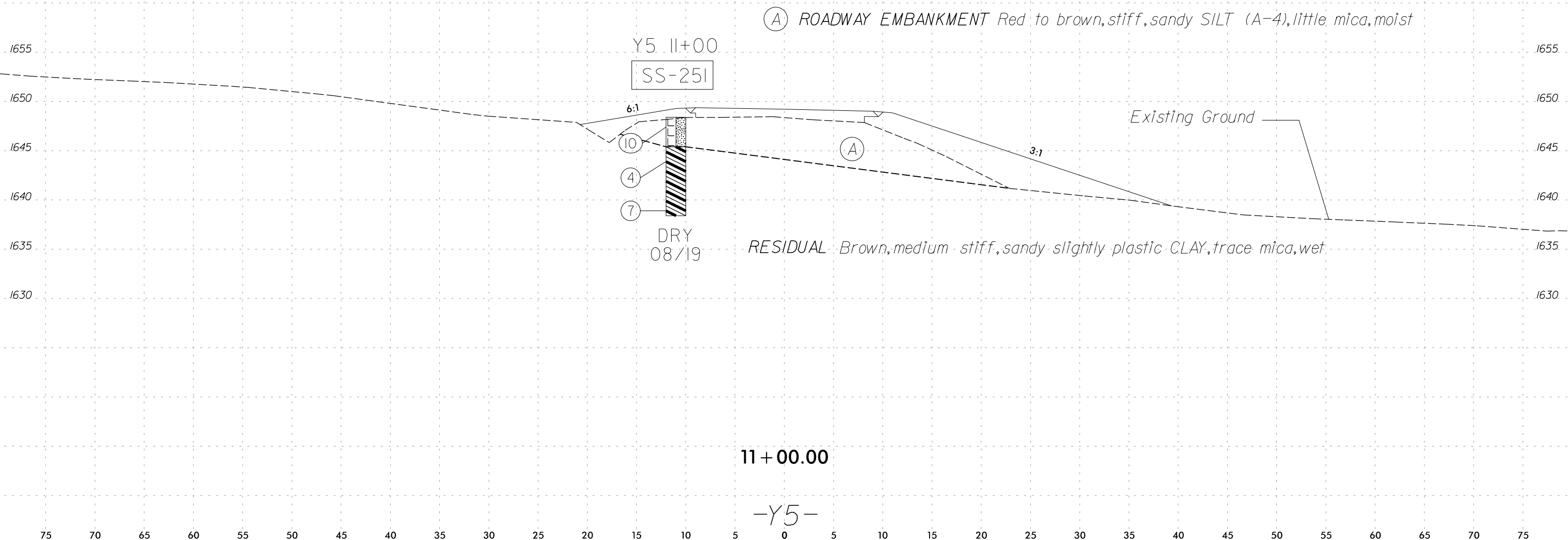
*Existing Ground*

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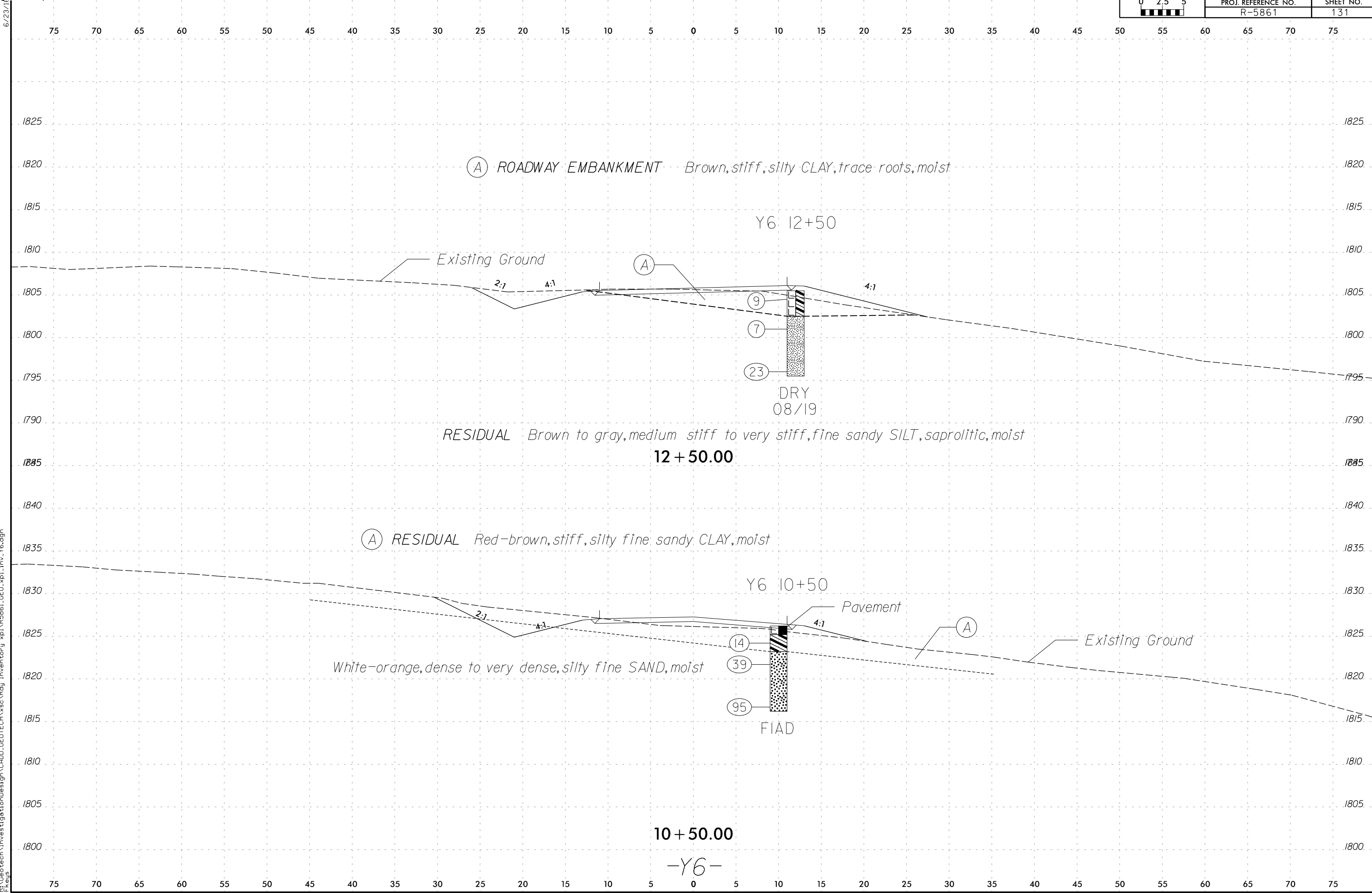
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-251	11+00	11' LT	3.5-5.0	A-6 (4)	37	12	18	33	16	33	96	85	52.6	23.3	-

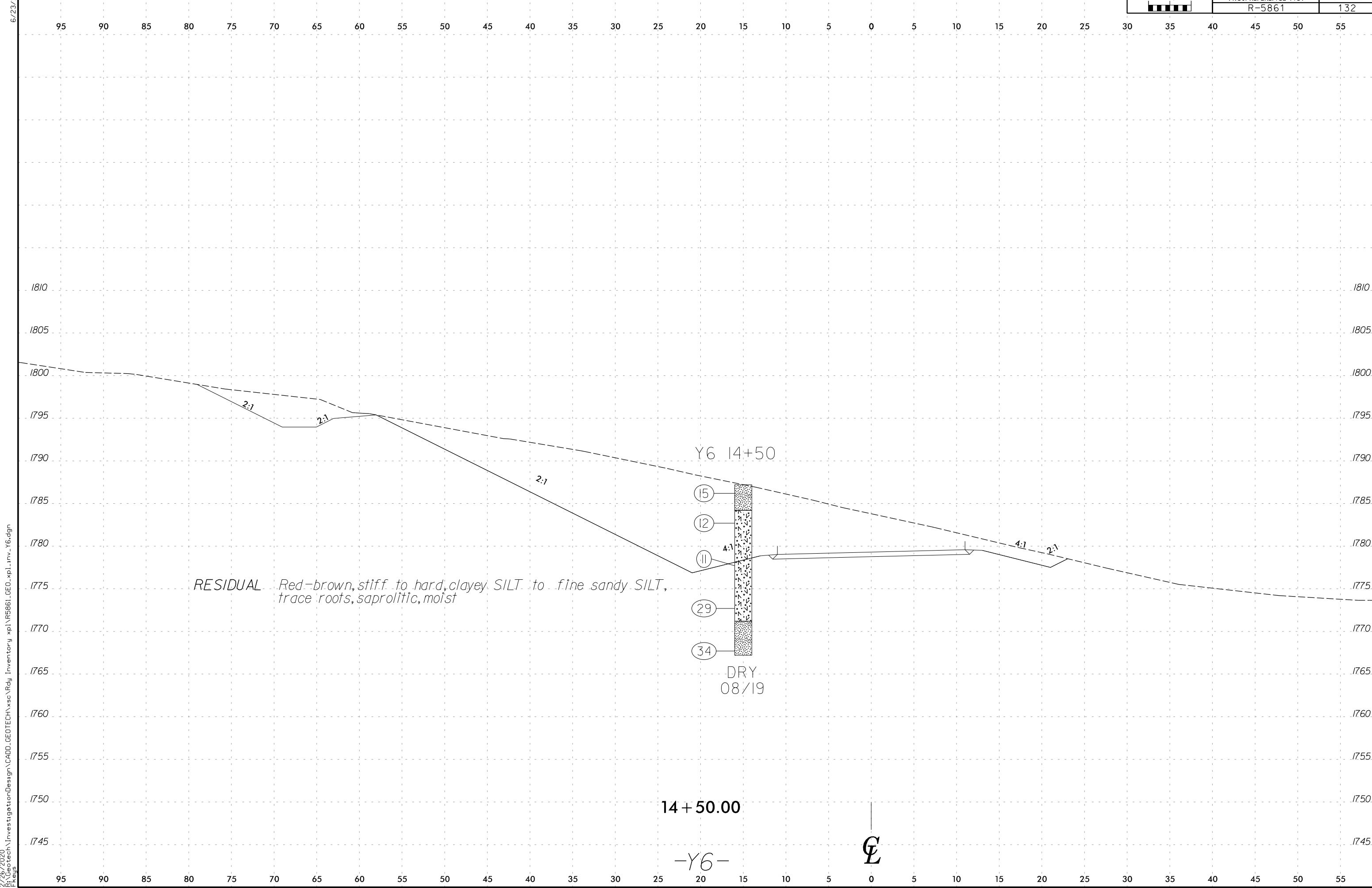


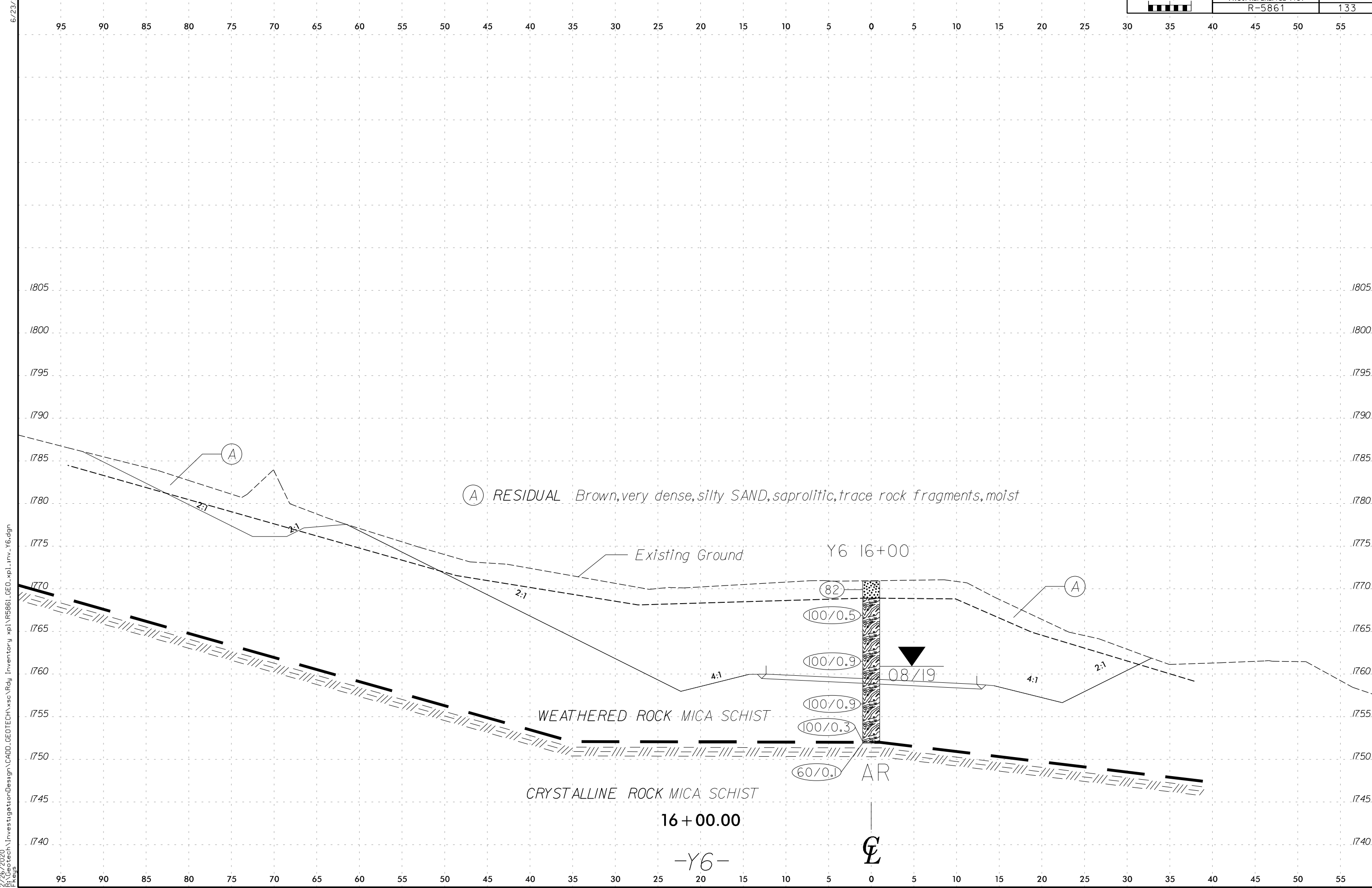
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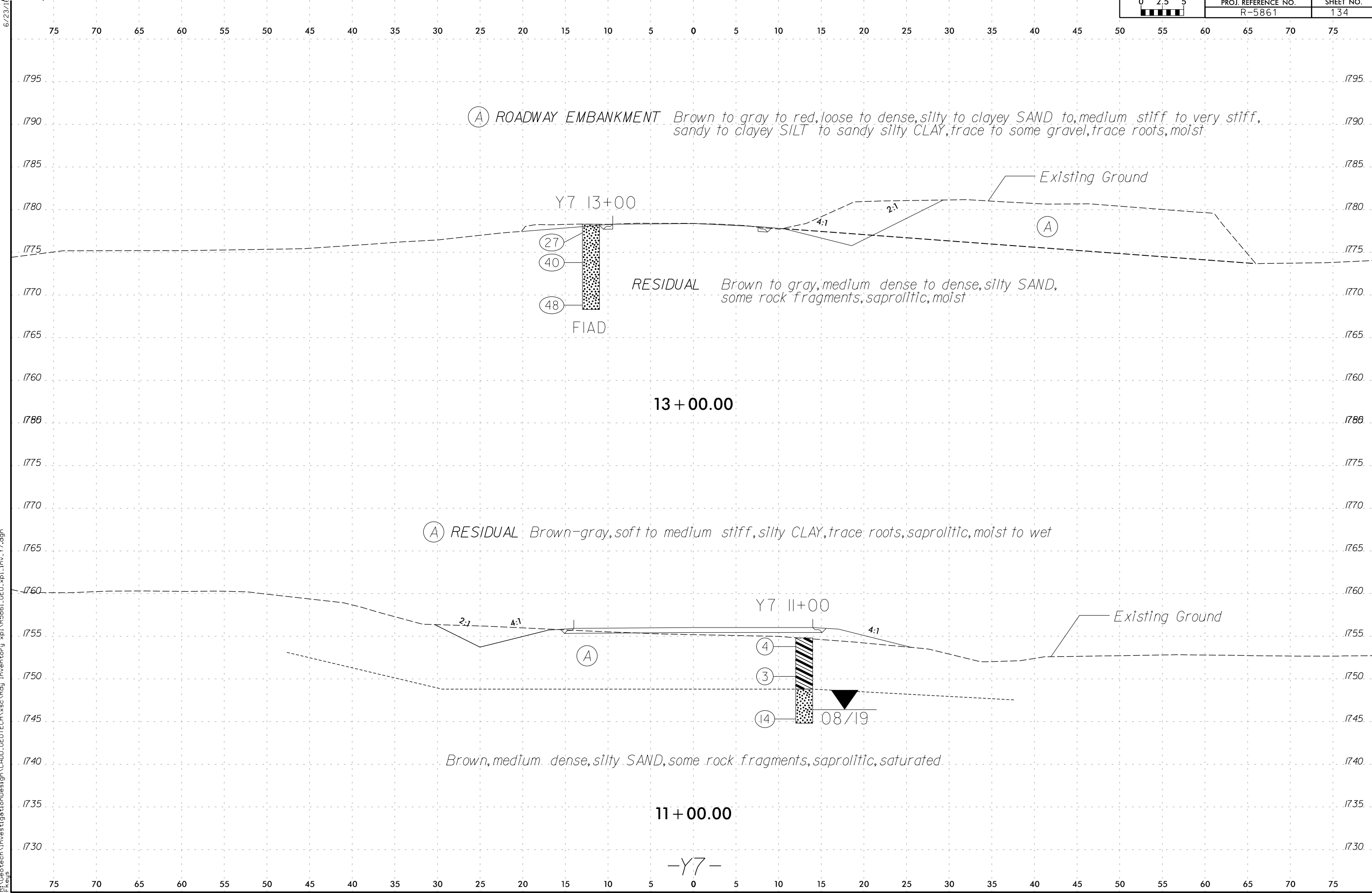


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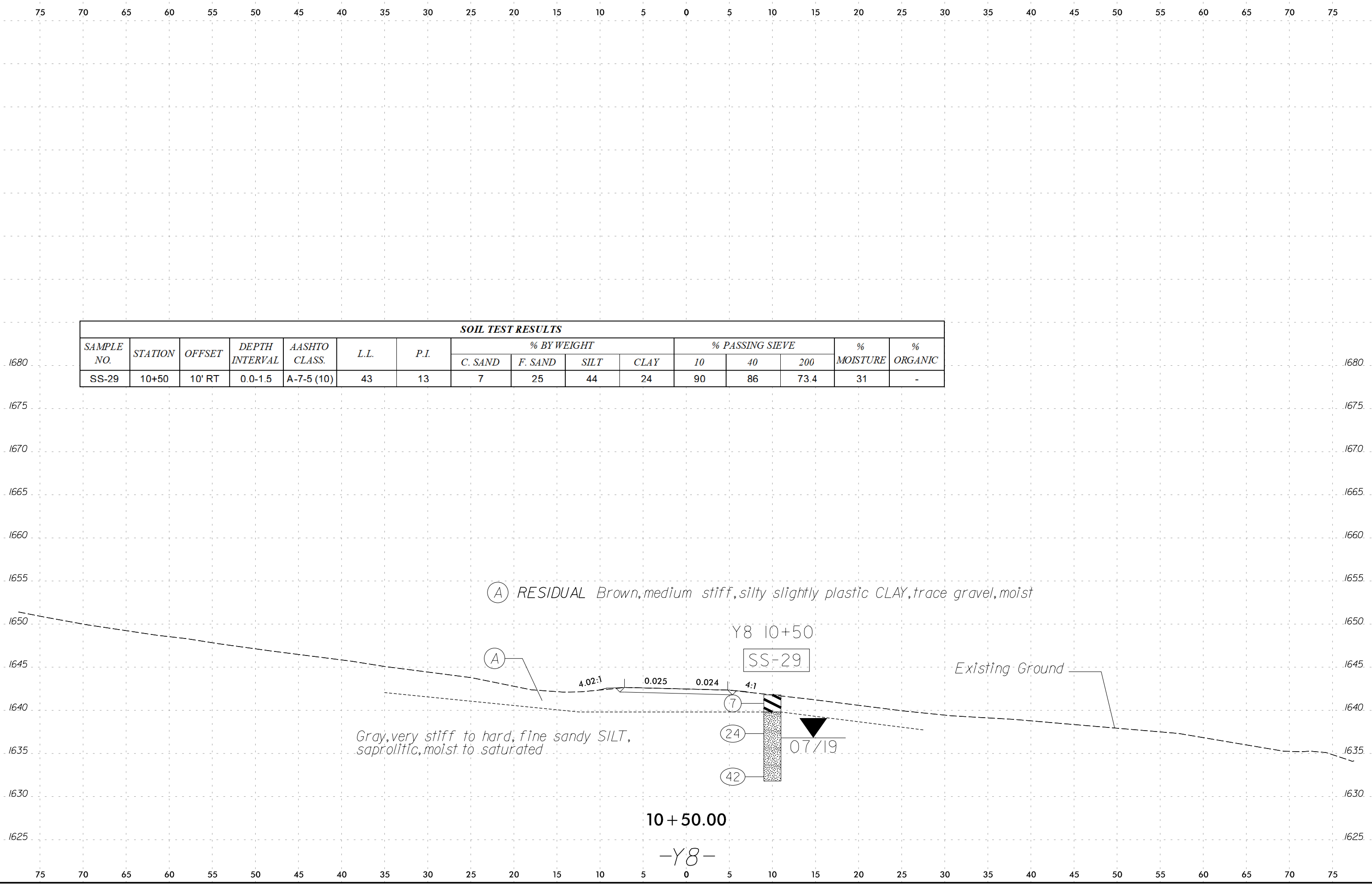


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-Y7-



**SOIL TEST RESULTS**

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-29	10+50	10' RT	0.0-1.5	A-7-5 (10)	43	13	7	25	44	24	90	86	73.4	31	-

(A) RESIDUAL Brown, medium stiff, silty slightly plastic CLAY, trace gravel, moist

Gray, very stiff to hard, fine sandy SILT, saprolitic, moist to saturated

Y8 10+50

SS-29

Existing Ground

07/19

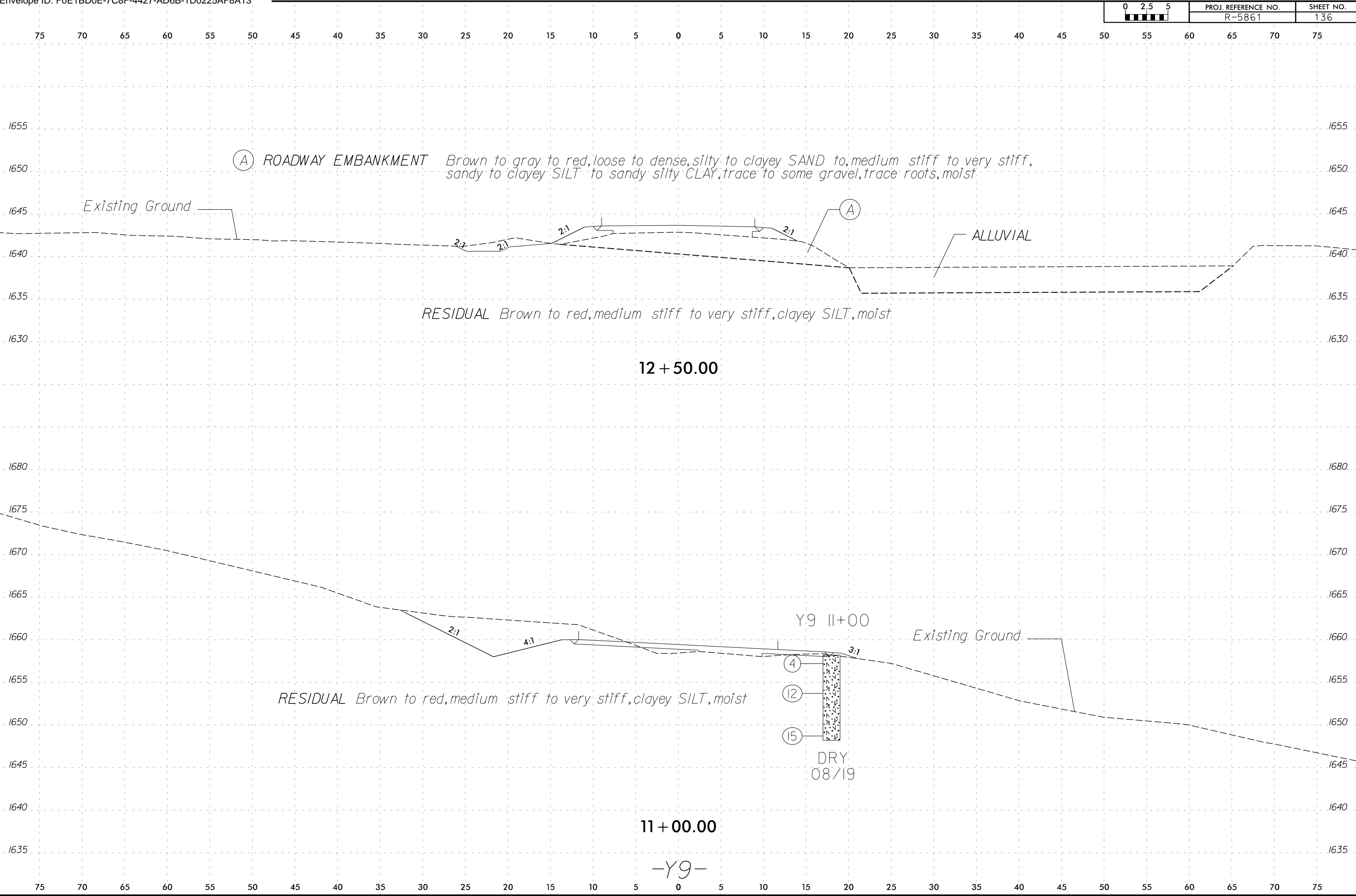
10 + 50.00

-Y8-

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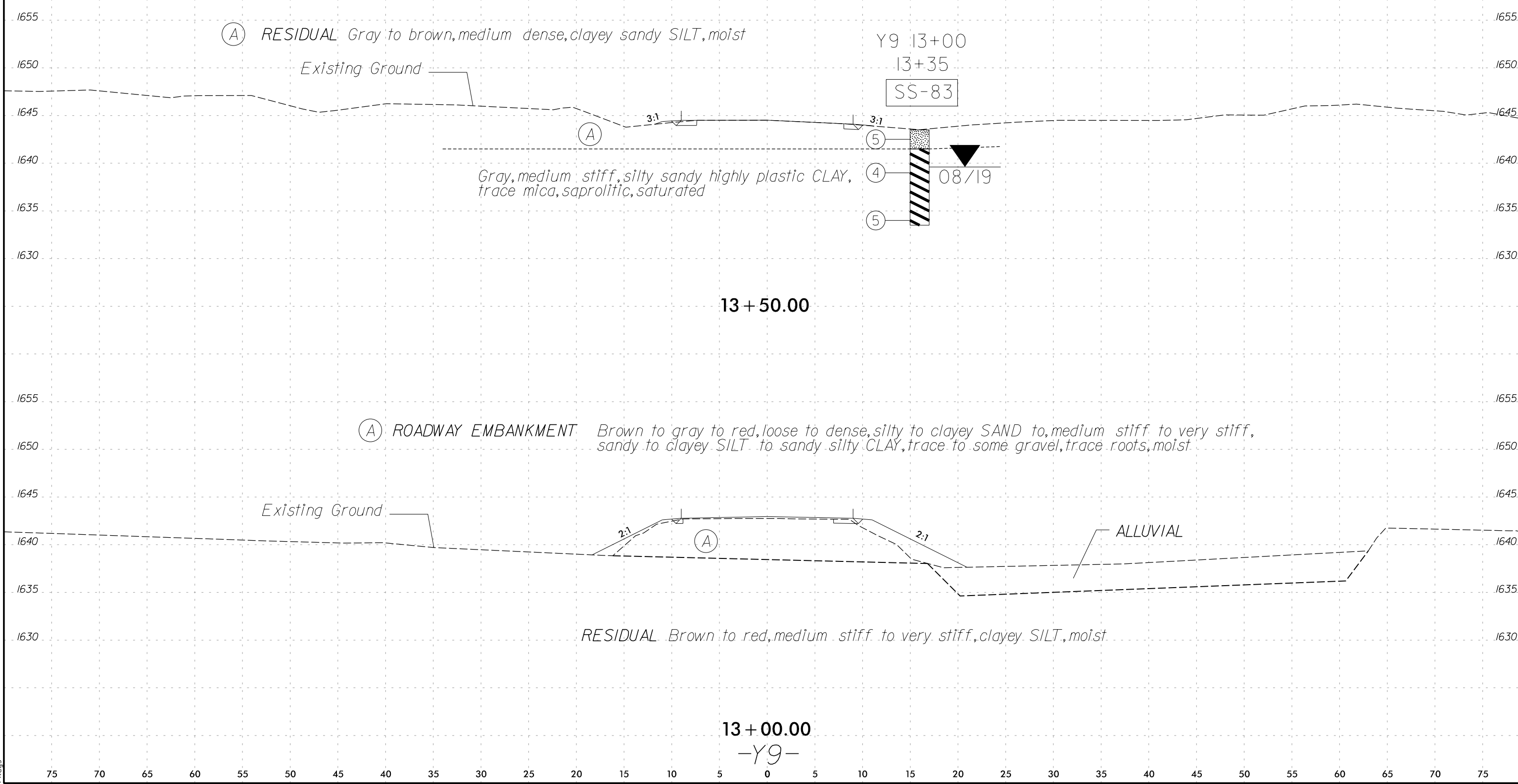


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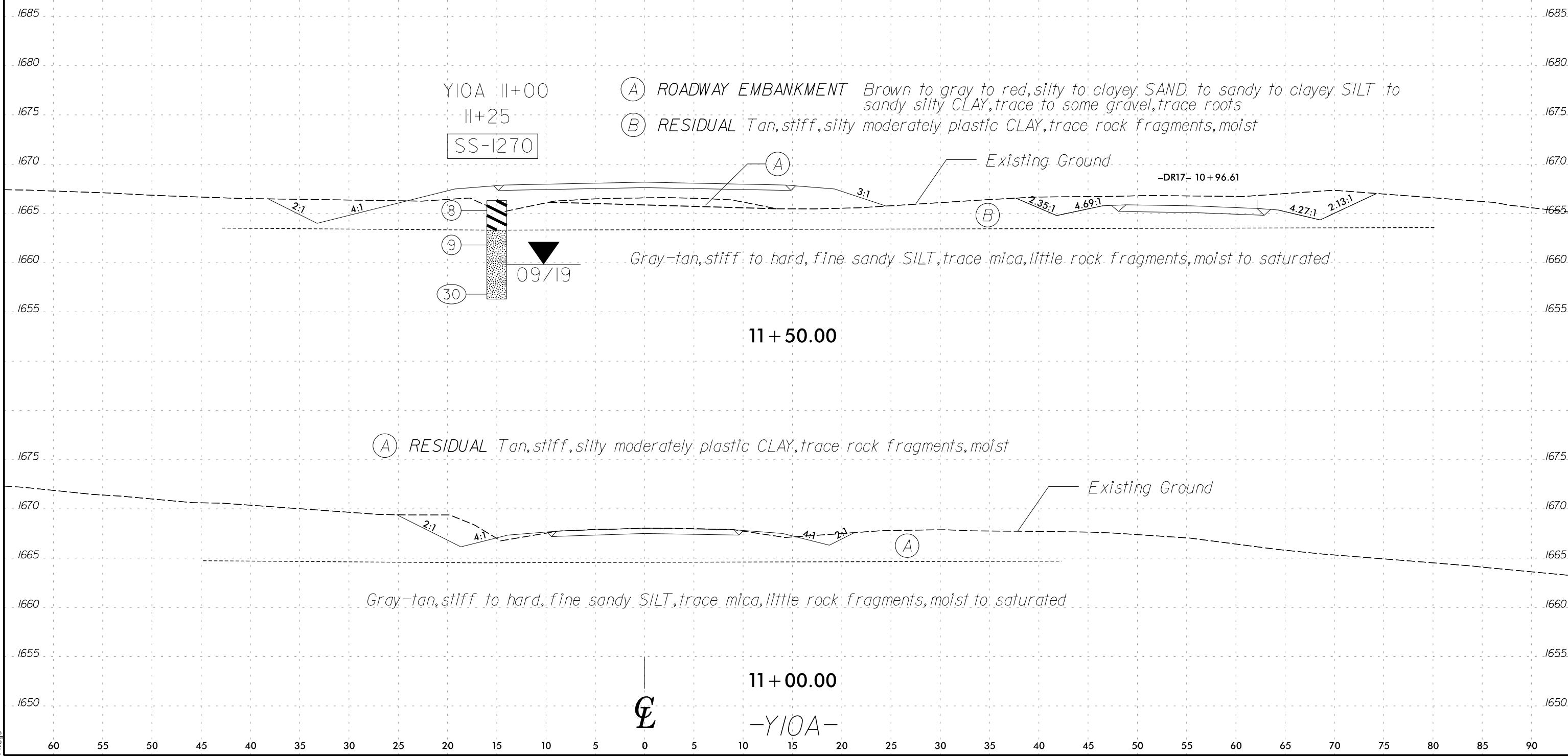
-Y9-

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-83	13+00	16' RT	3.5-5.0	A-7-5 (25)	64	33	5	37	24	34	100	97	71.3	43.3	-

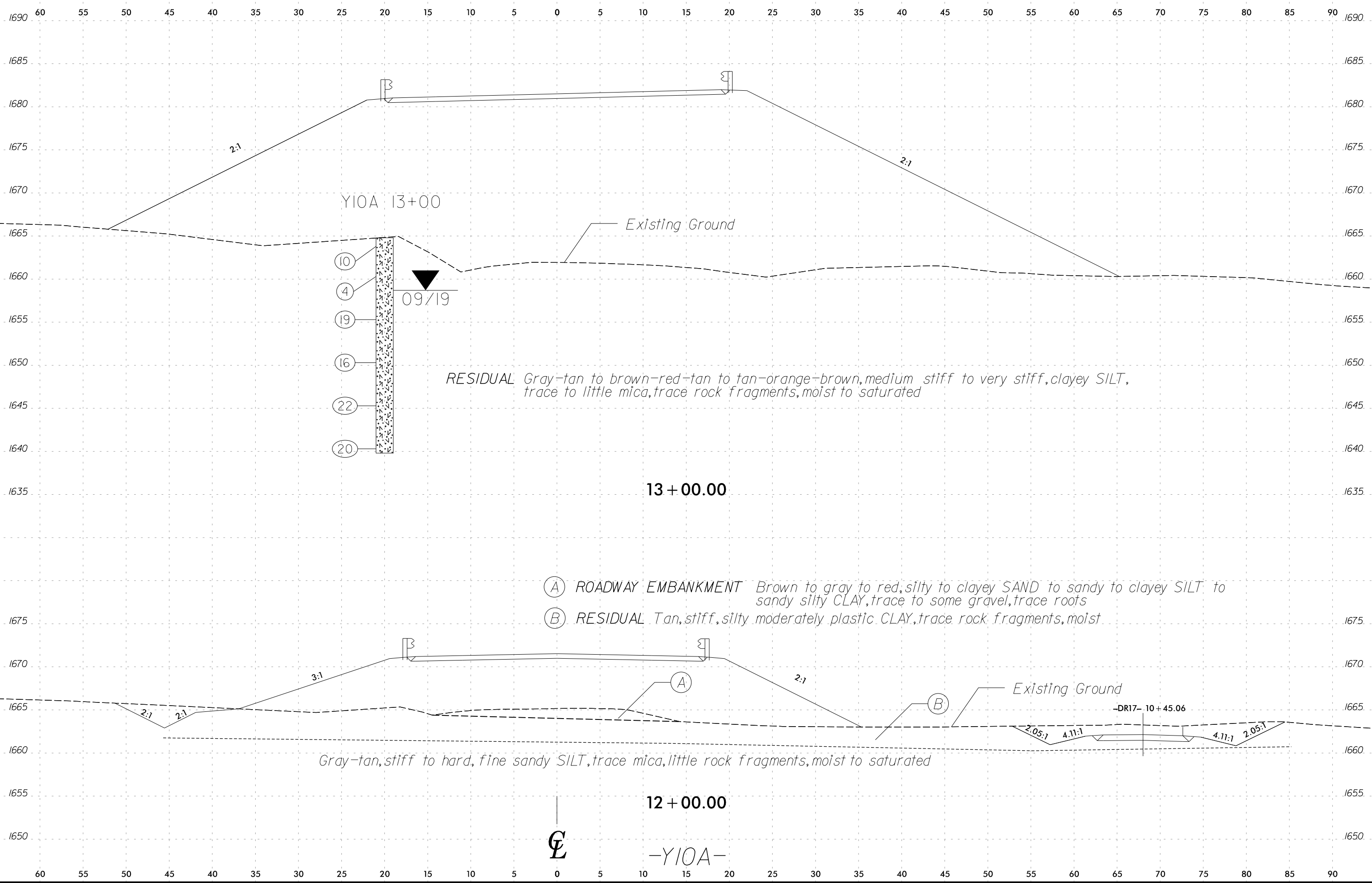


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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1270	11+25	15' LT	0.0-1.5	A-7-6 (23)	51	23	4	9	37	50	98	95	88.9	22.5	-



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Y10A 13+00

Existing Ground

09/19

RESIDUAL Gray-tan to brown-red-tan to tan-orange-brown, medium stiff to very stiff, clayey SILT, trace to little mica, trace rock fragments, moist to saturated

13 + 00.00

(A) ROADWAY EMBANKMENT Brown to gray to red, silty to clayey SAND to sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots

(B) RESIDUAL Tan, stiff, silty moderately plastic CLAY, trace rock fragments, moist

Existing Ground

Gray-tan, stiff to hard, fine sandy SILT, trace mica, little rock fragments, moist to saturated

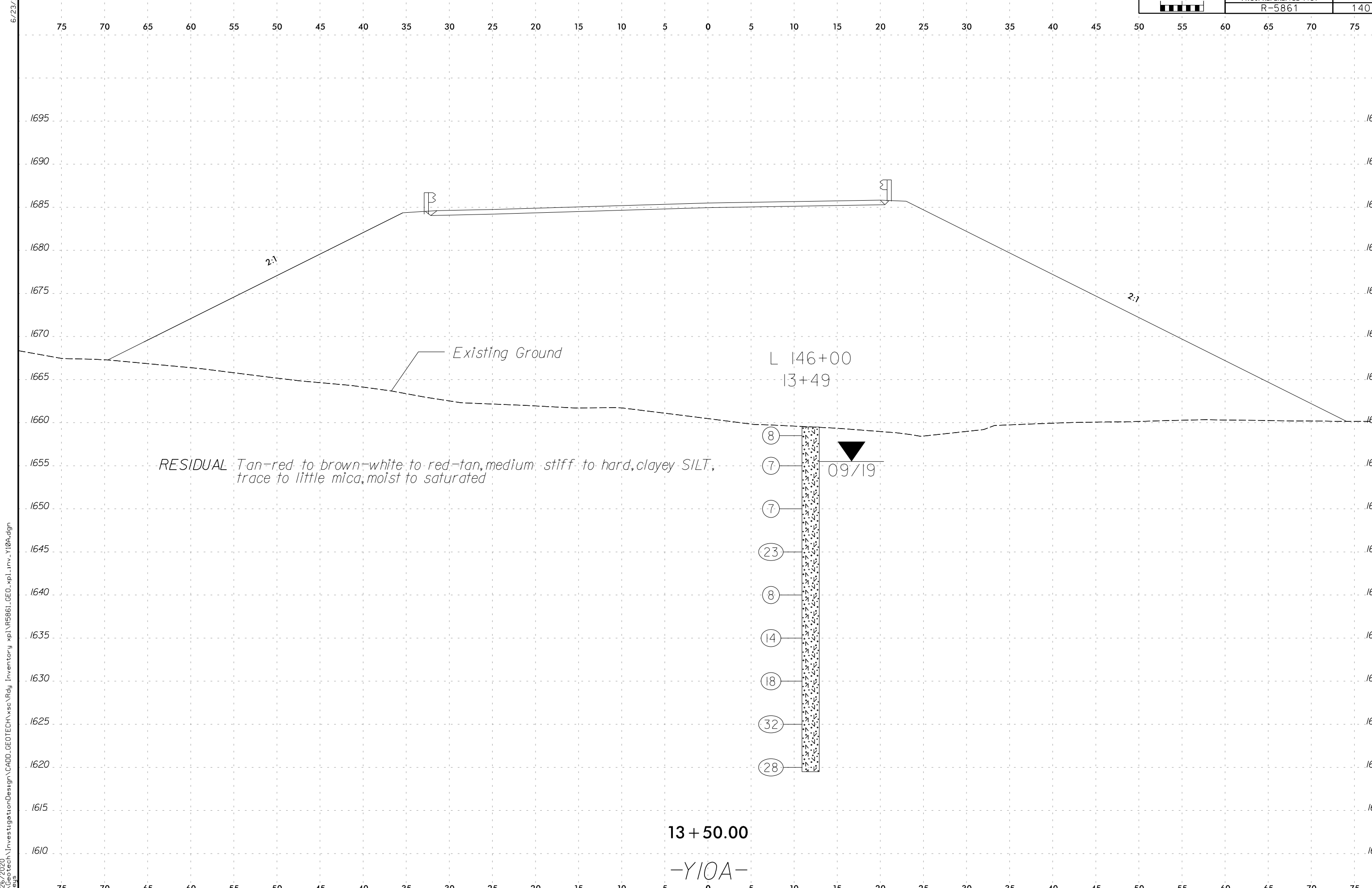
12 + 00.00

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-Y10A-

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*RESIDUAL Tan-red to brown-white to red-tan, medium stiff to hard, clayey SILT, trace to little mica, moist to saturated*

*Existing Ground*

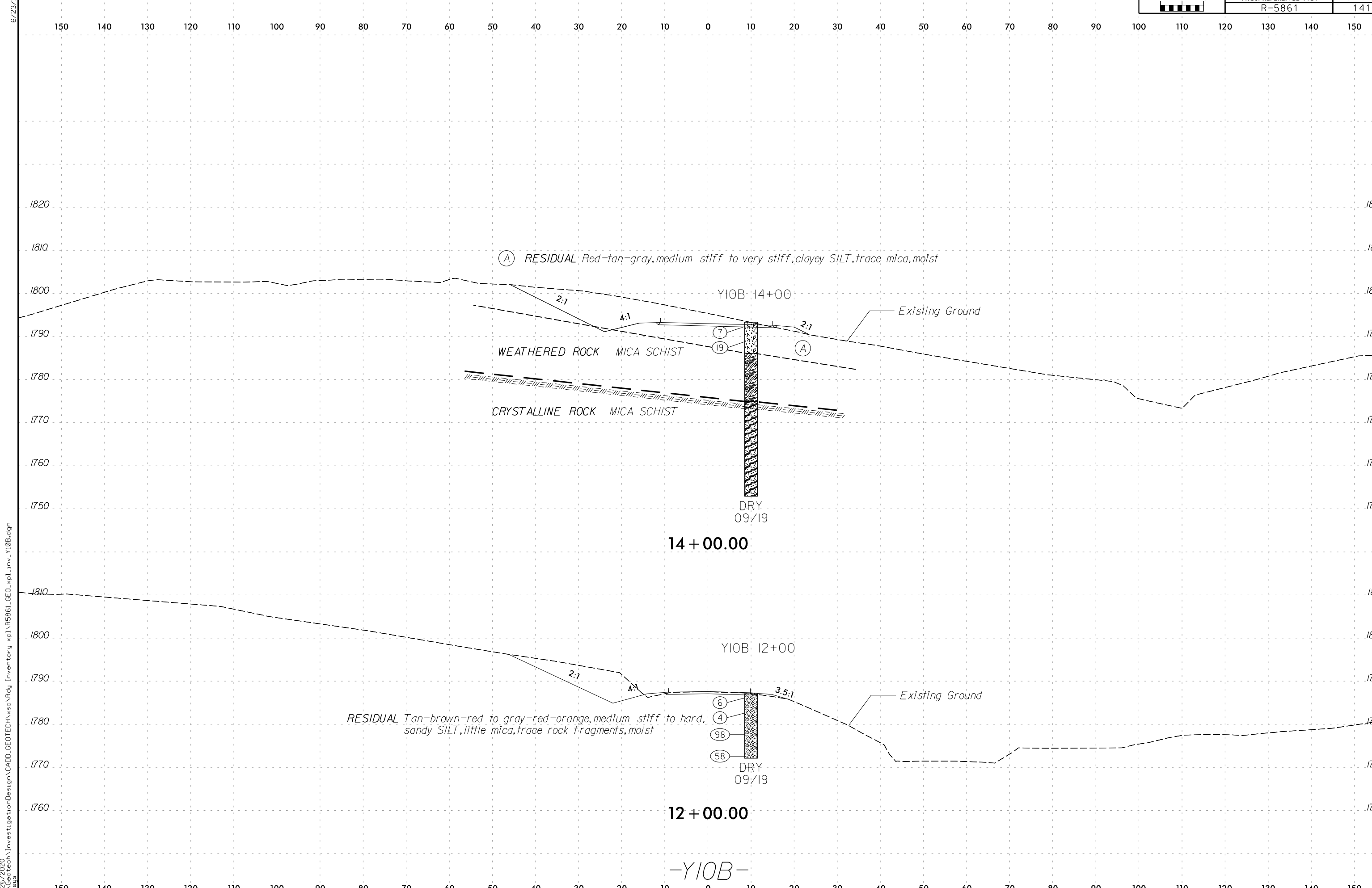
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13+49

09/19

13 + 50.00

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(A) RESIDUAL Red-tan-gray, medium stiff to very stiff, clayey SILT, trace mica, moist

Y10B 14+00

Existing Ground

WEATHERED ROCK MICA SCHIST

CRYSTALLINE ROCK MICA SCHIST

DRY 09/19

14 + 00.00

RESIDUAL Tan-brown-red to gray-red-orange, medium stiff to hard, sandy SILT, little mica, trace rock fragments, moist

Y10B 12+00

Existing Ground

DRY 09/19

12 + 00.00

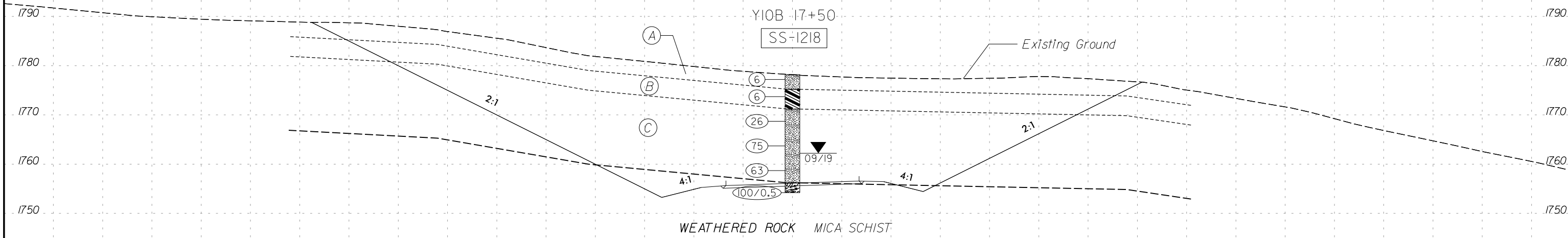
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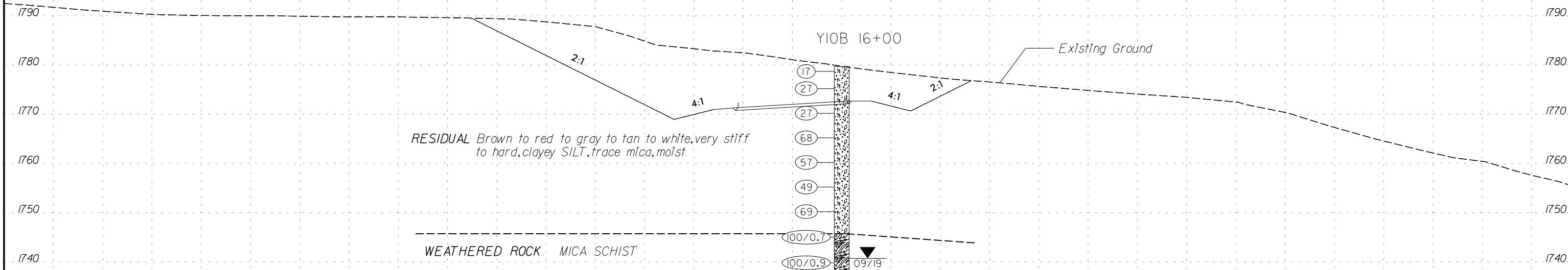


SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1218	17+50	0	8.5-10.0	A-4 (5)	38	6	8	28	50	14	100	95	75.2	20.9	-

- (A) RESIDUAL Tan-gray-red, medium stiff, sandy SILT, moist
- (B) Brown-gray-tan, medium stiff, fine sandy silty CLAY, moist
- (C) Red-tan to orange-black-red, hard, fine sandy SILT, trace to little mica, moist to saturated



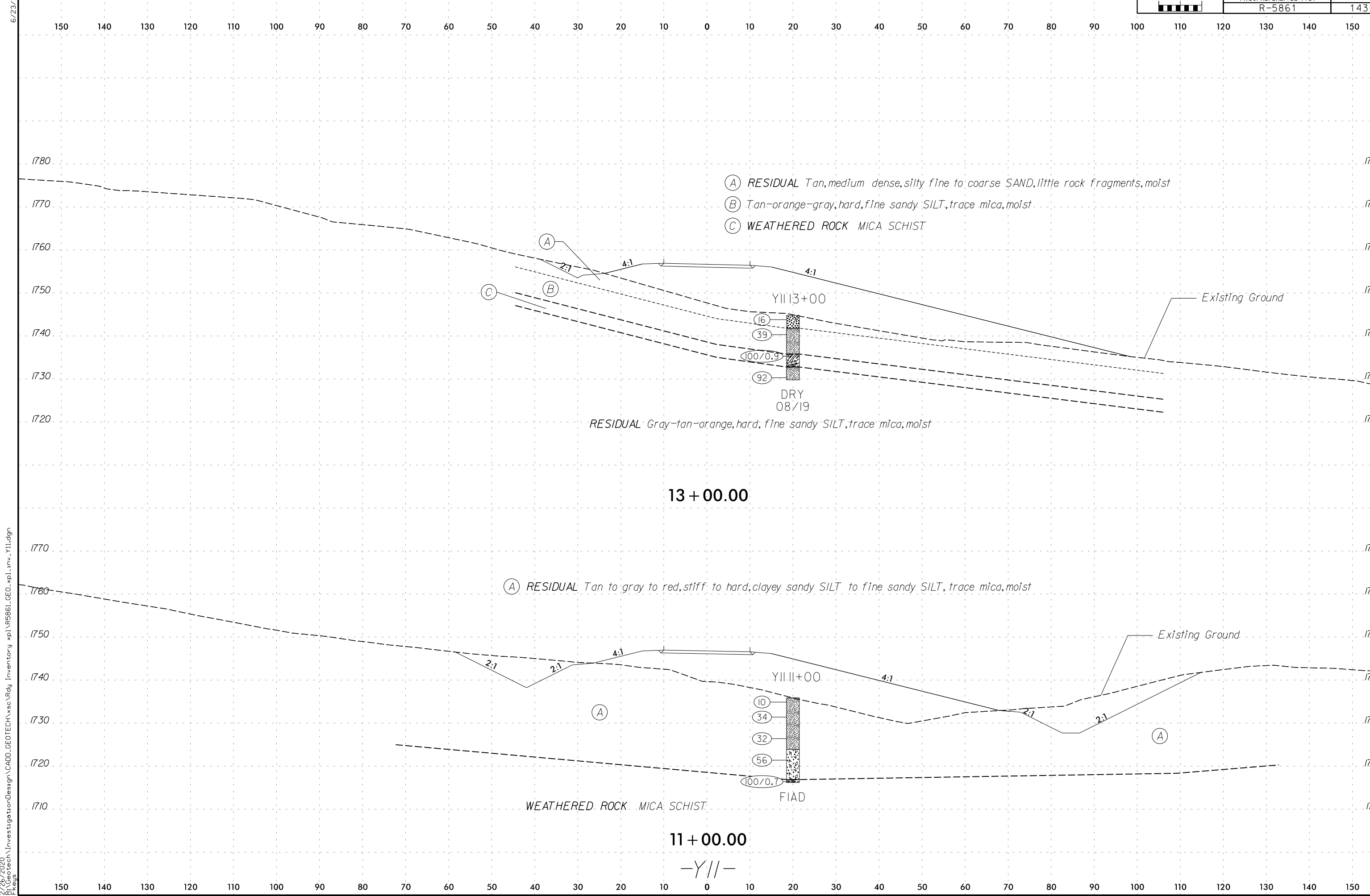
17 + 50.00



16 + 00.00

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- (A) RESIDUAL Tan, medium dense, silty fine to coarse SAND, little rock fragments, moist
- (B) Tan-orange-gray, hard, fine sandy SILT, trace mica, moist
- (C) WEATHERED ROCK MICA SCHIST

RESIDUAL Gray-tan-orange, hard, fine sandy SILT, trace mica, moist

(A) RESIDUAL Tan to gray to red, stiff to hard, clayey sandy SILT to fine sandy SILT, trace mica, moist

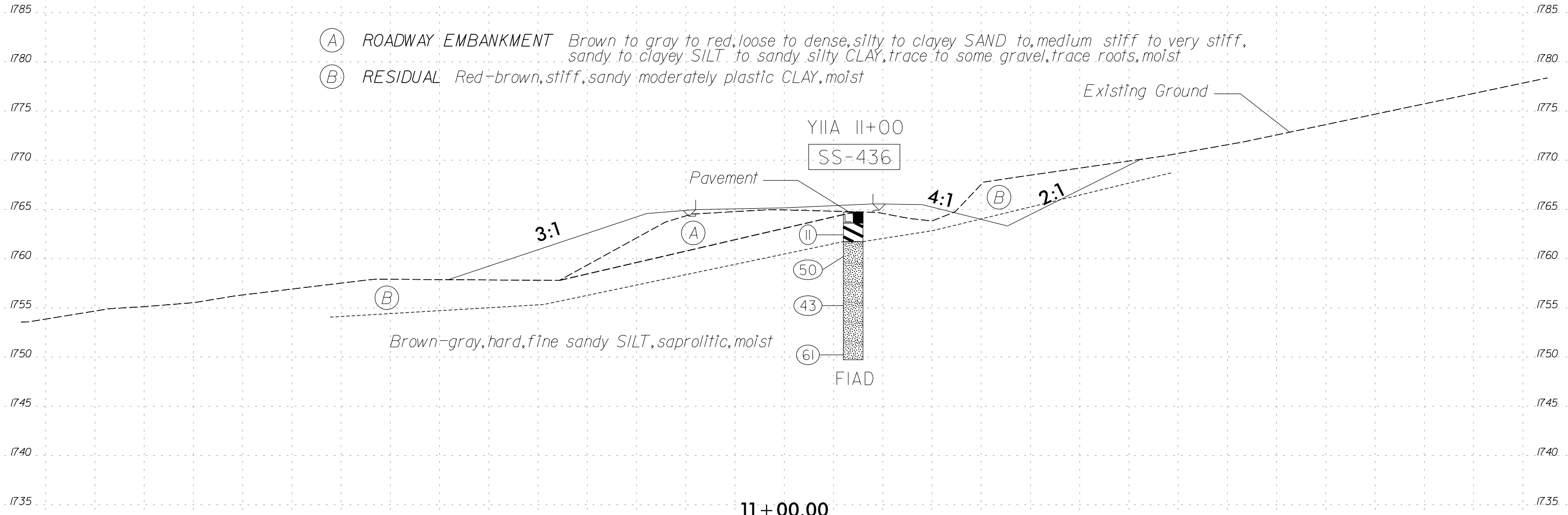
WEATHERED ROCK MICA SCHIST

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75 70 65 60 55 50 45 40 35 30 25 20 15 10 5 0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-436	11+00	7' RT	1.3-2.8	A-7-6 (9)	44	17	16	25	23	36	87	77	59.5	19.5	-

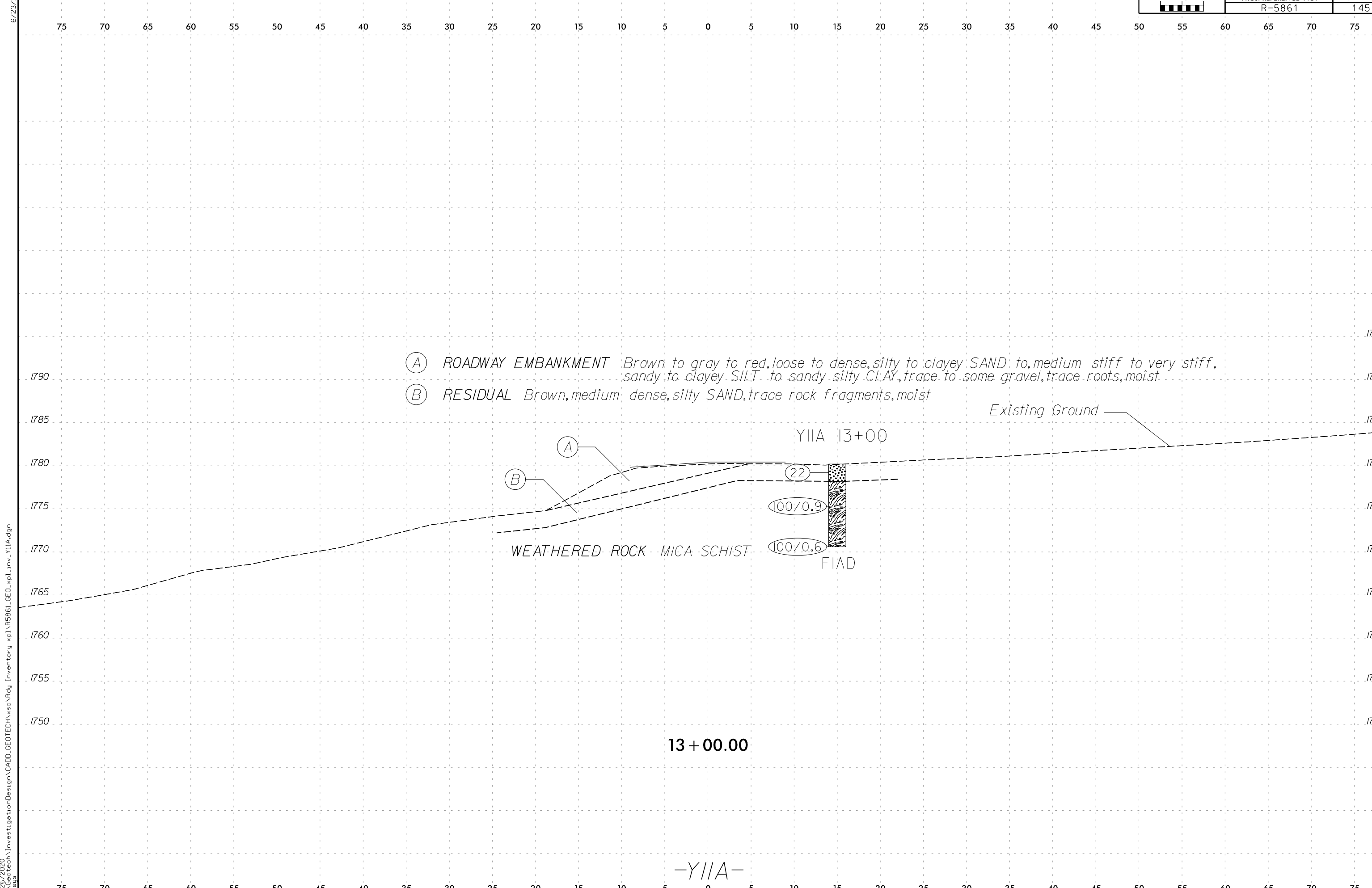
- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Red-brown, stiff, sandy moderately plastic CLAY, moist*



11 + 00.00

-Y//A-

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- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown, medium dense, silty SAND, trace rock fragments, moist*

Existing Ground

Y11A 13+00

22

100/0.9

100/0.6

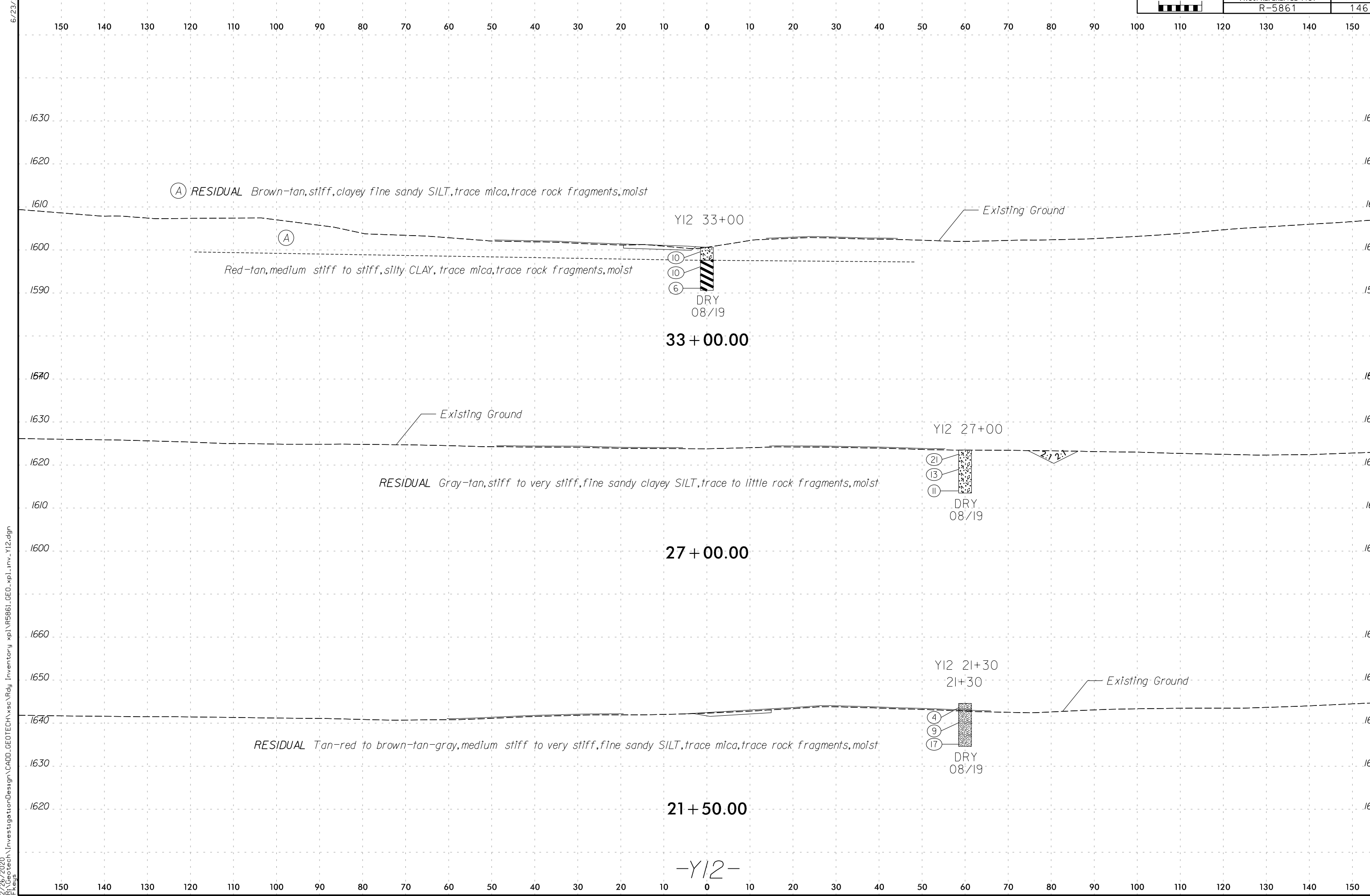
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WEATHERED ROCK MICA SCHIST

13 + 00.00

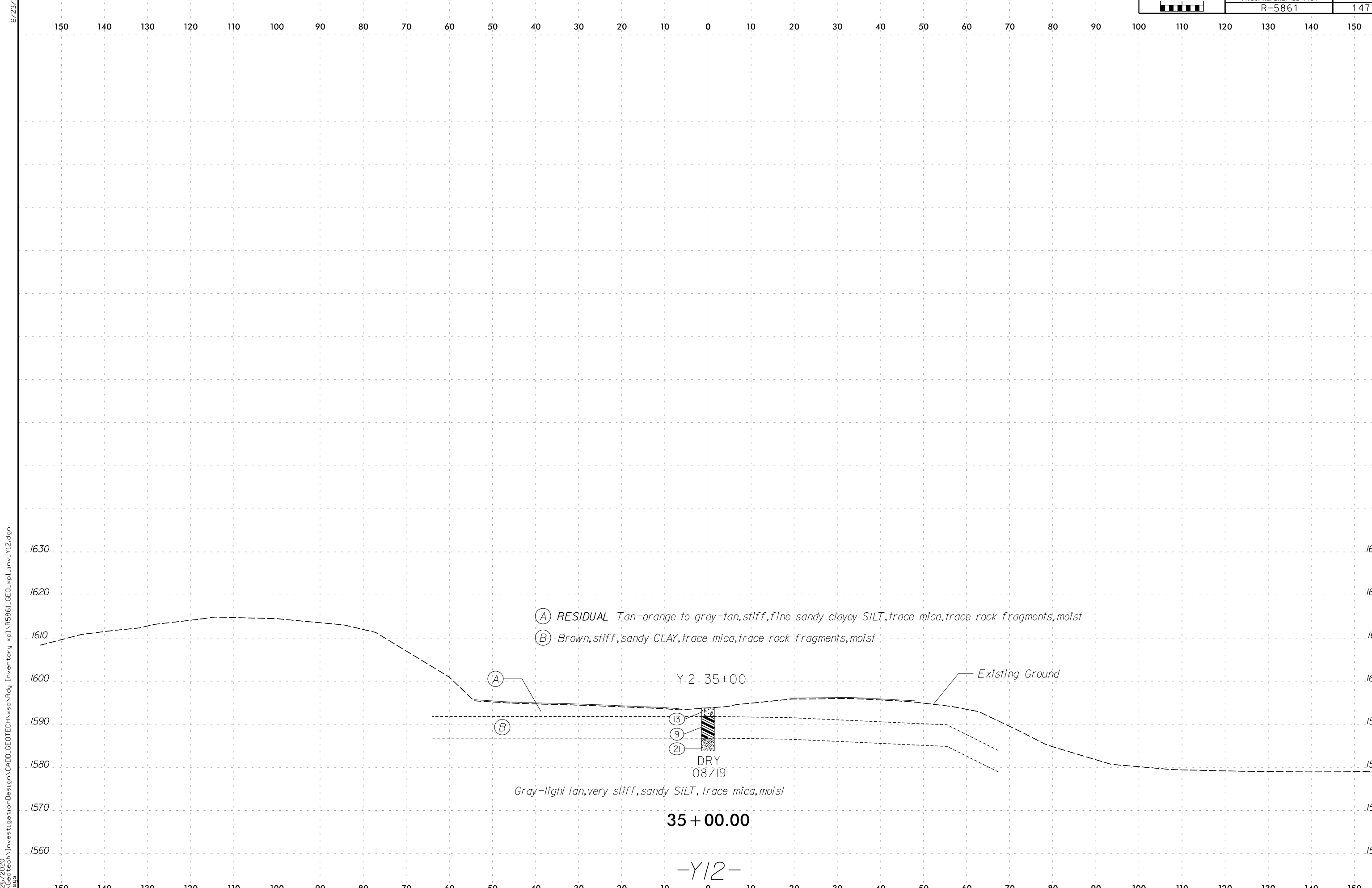
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-Y12-

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P.Keijs



(A) RESIDUAL Tan-orange to gray-tan, stiff, fine sandy clayey SILT, trace mica, trace rock fragments, moist  
 (B) Brown, stiff, sandy CLAY, trace mica, trace rock fragments, moist

(A) Existing Ground  
 (B) Existing Ground  
 Y12 35+00  
 DRY 08/19

Gray-light tan, very stiff, sandy SILT, trace mica, moist

35 + 00.00

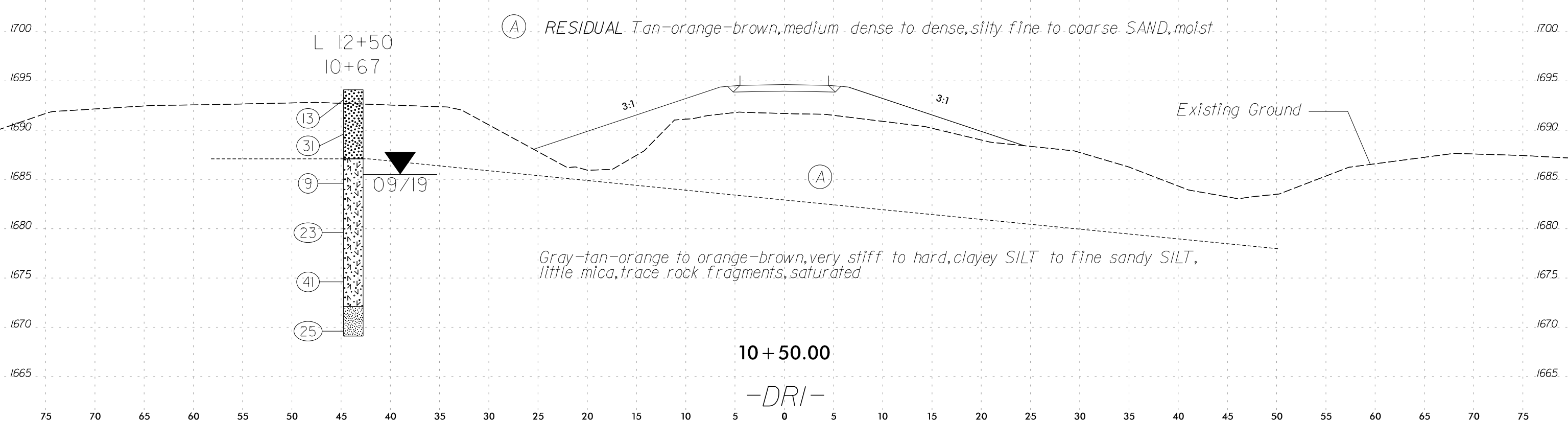
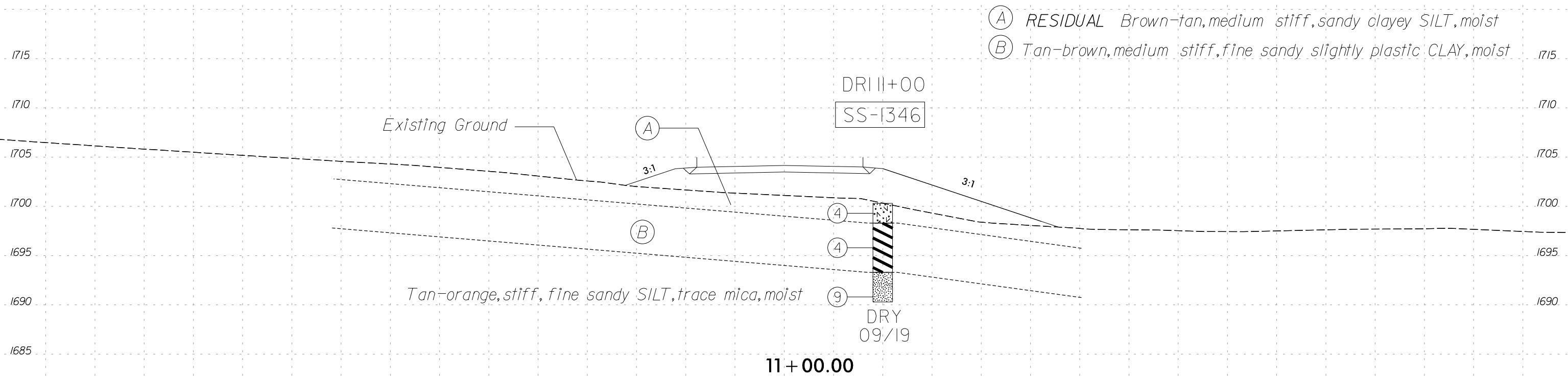
-Y12-

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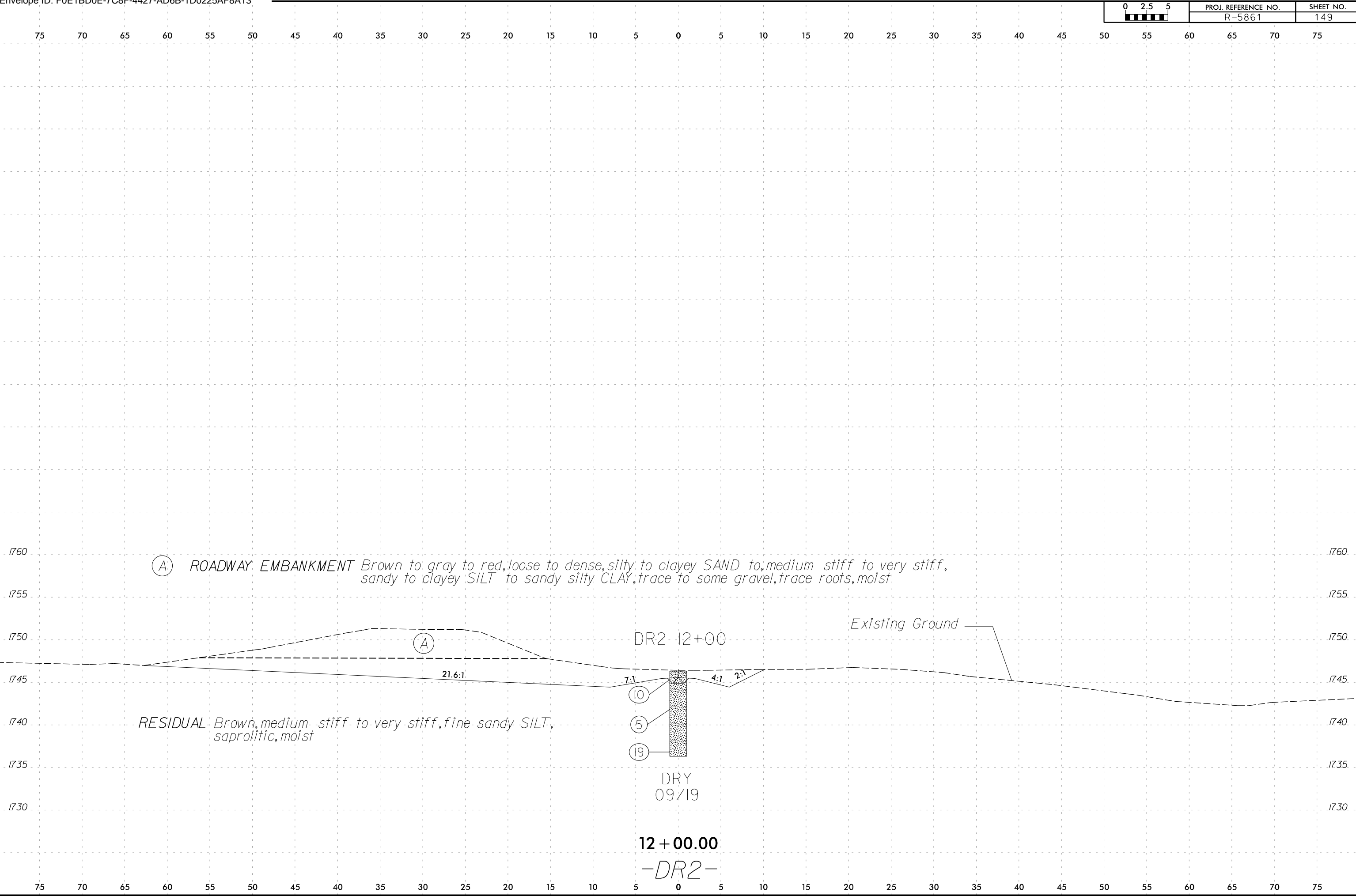
75 70 65 60 55 50 45 40 35 30 25 20 15 10 5 0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1346	11+00	20' RT	3.5-5.0	A-7-6 (7)	41	12	8	37	19	36	98	94	62.3	24.3	-

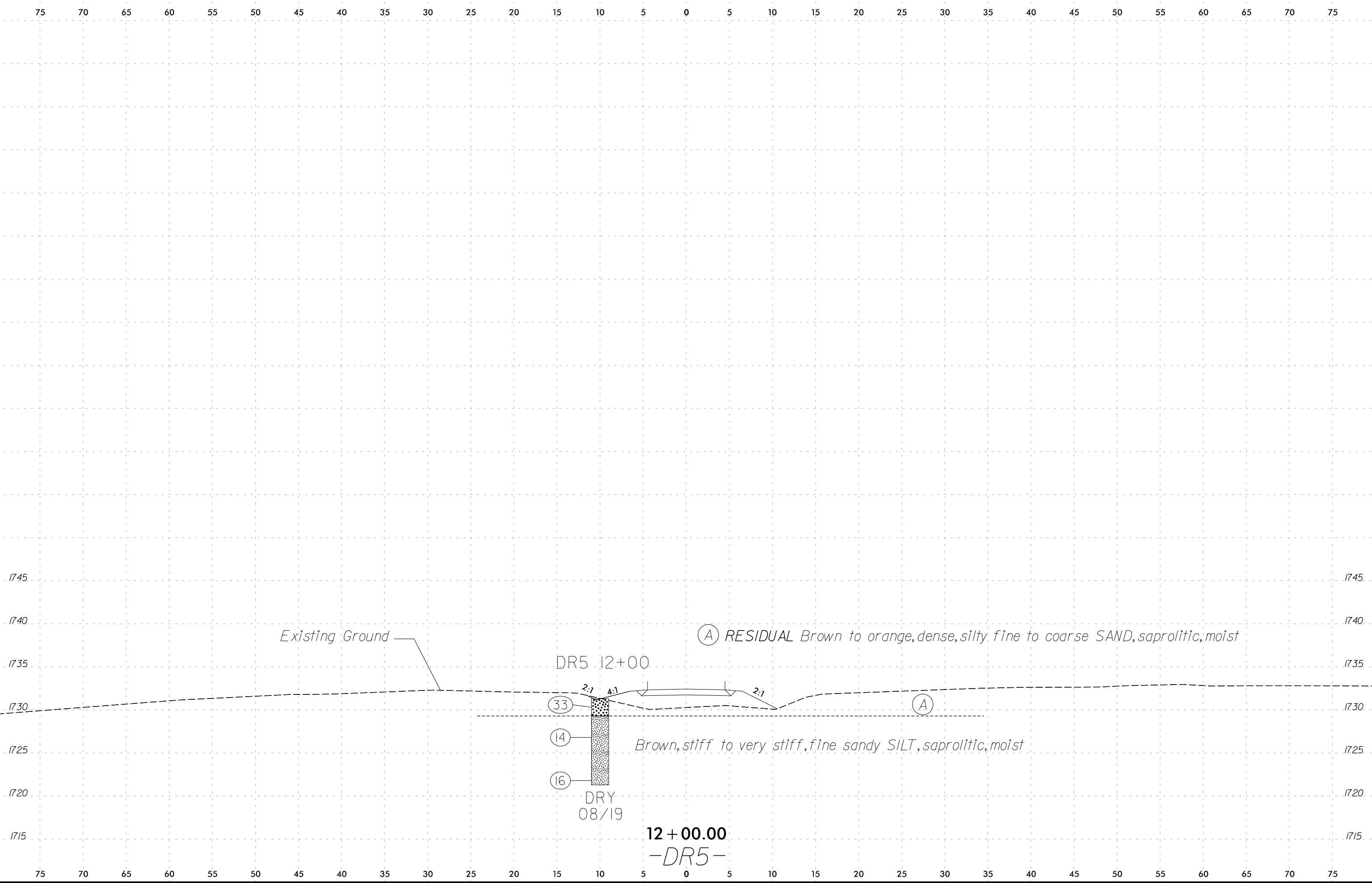


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2/26/2020  
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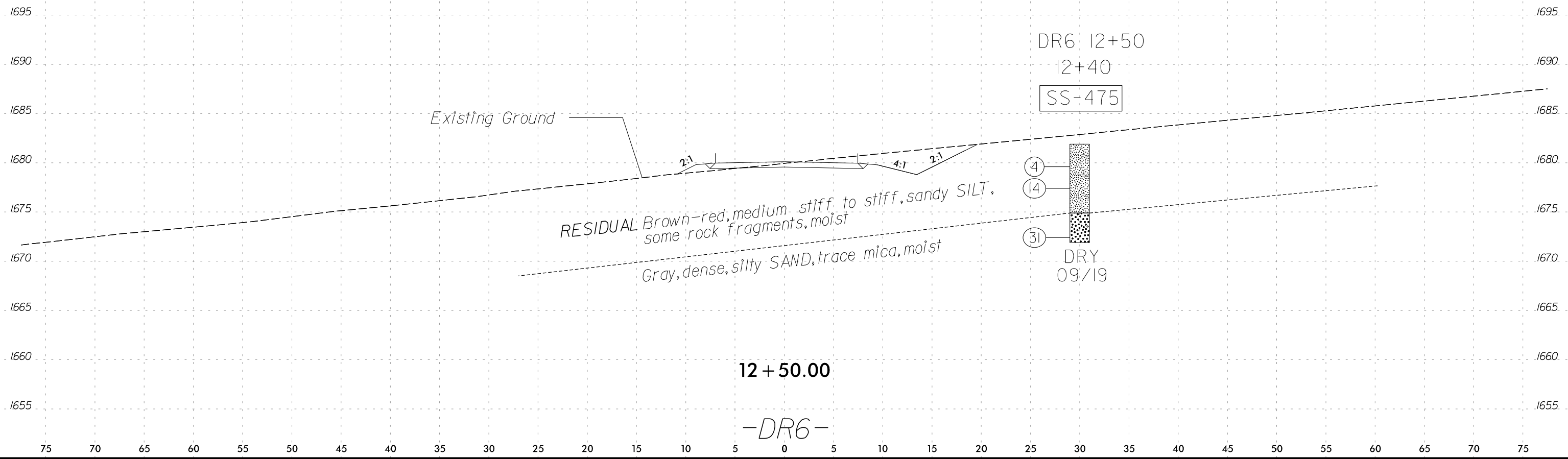


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P.Keja

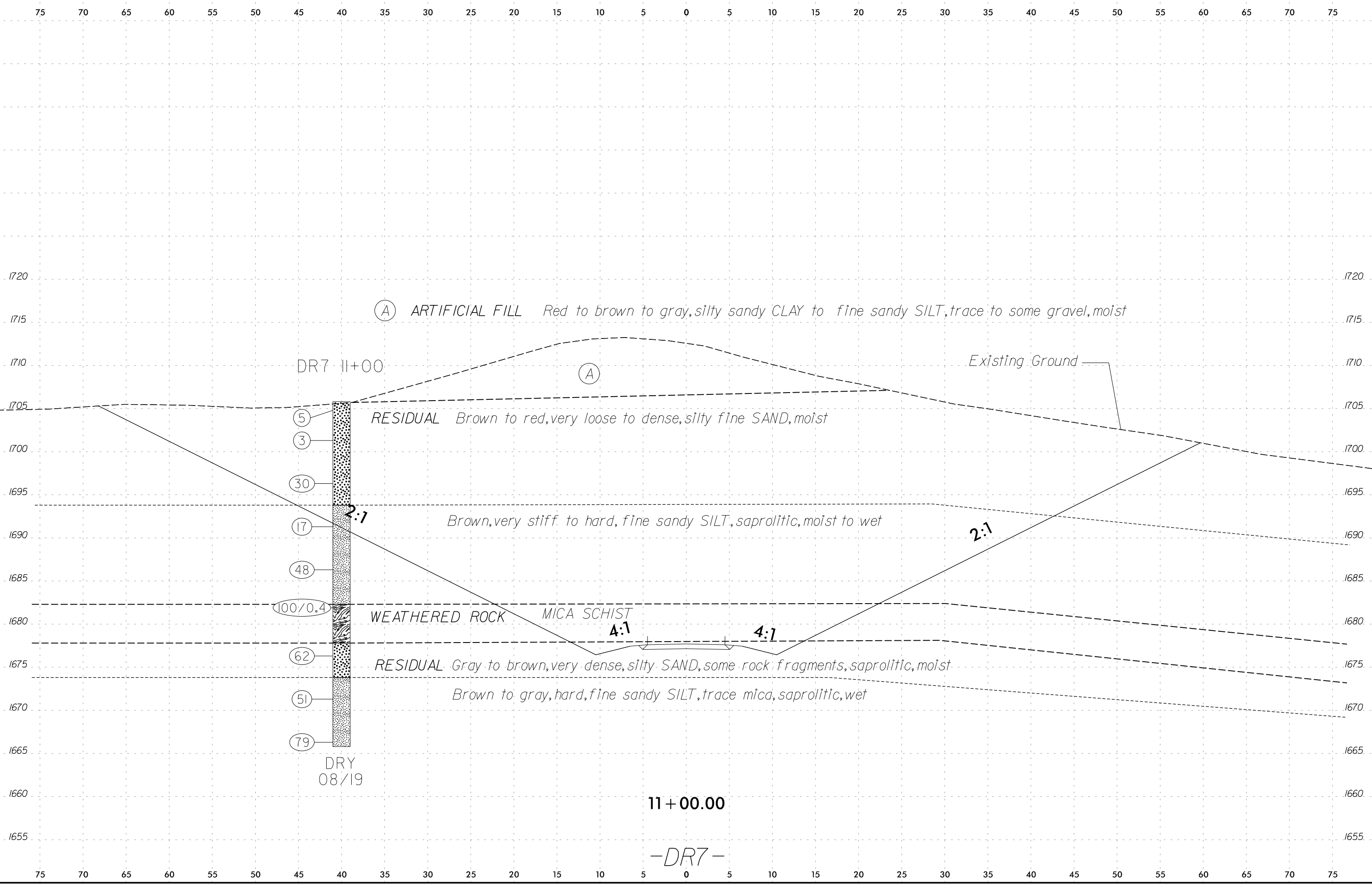


75 70 65 60 55 50 45 40 35 30 25 20 15 10 5 0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-475	12+40	30' RT	1.3-2.8	A-4 (4)	32	10	13	32	21	34	97	91	58.5	18	-



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DR7 11+00

Existing Ground

2:1

2:1

4:1

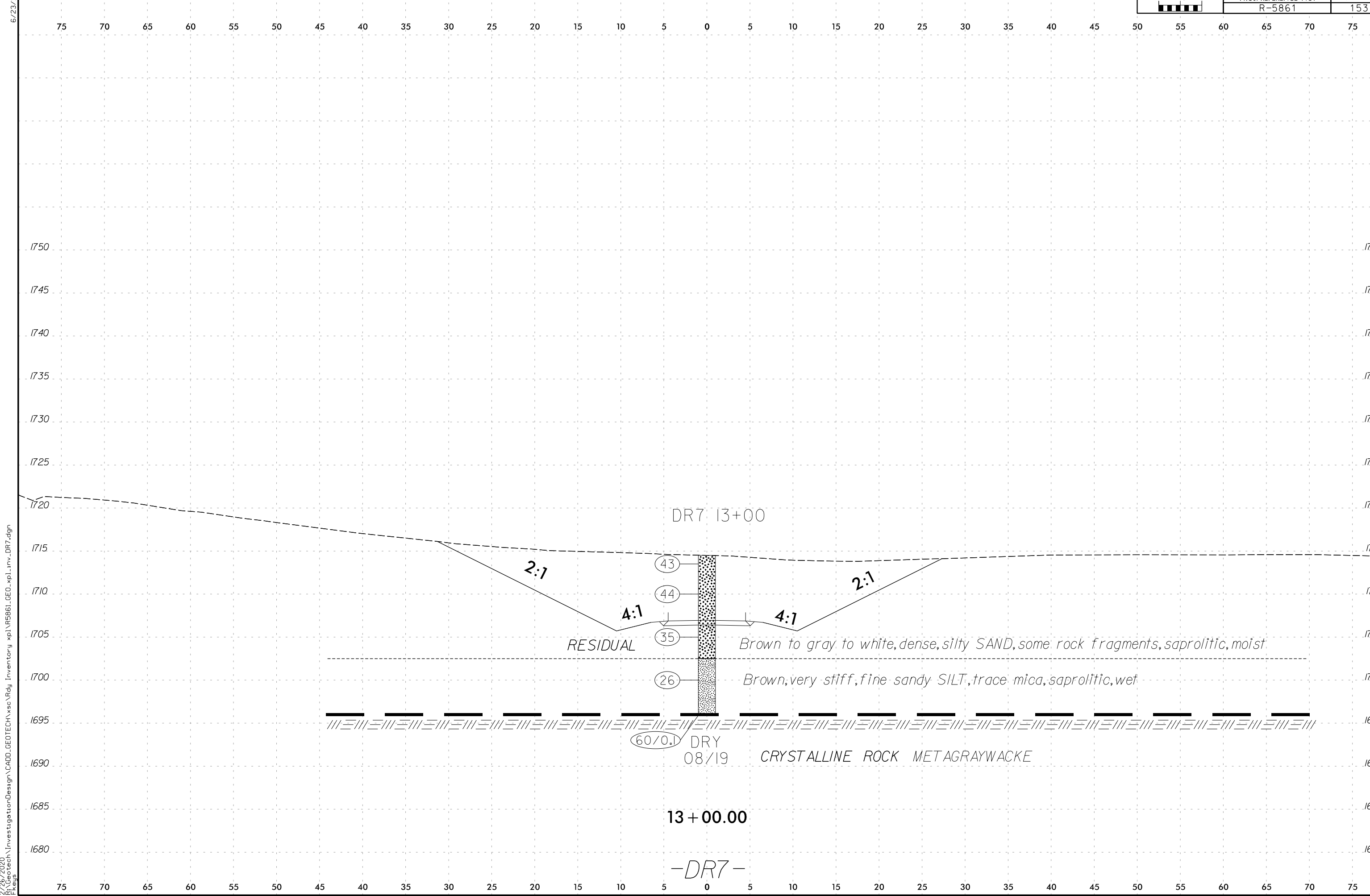
4:1

DRY  
08/19

11 + 00.00

-DR7-

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DR7: 13+00

2:1

4:1

2:1

4:1

RESIDUAL

Brown to gray to white, dense, silty SAND, some rock fragments, saprolitic, moist

Brown, very stiff, fine sandy SILT, trace mica, saprolitic, wet

60/0.1

DRY  
08/19

CRYSTALLINE ROCK METAGRAYWACKE

13 + 00.00

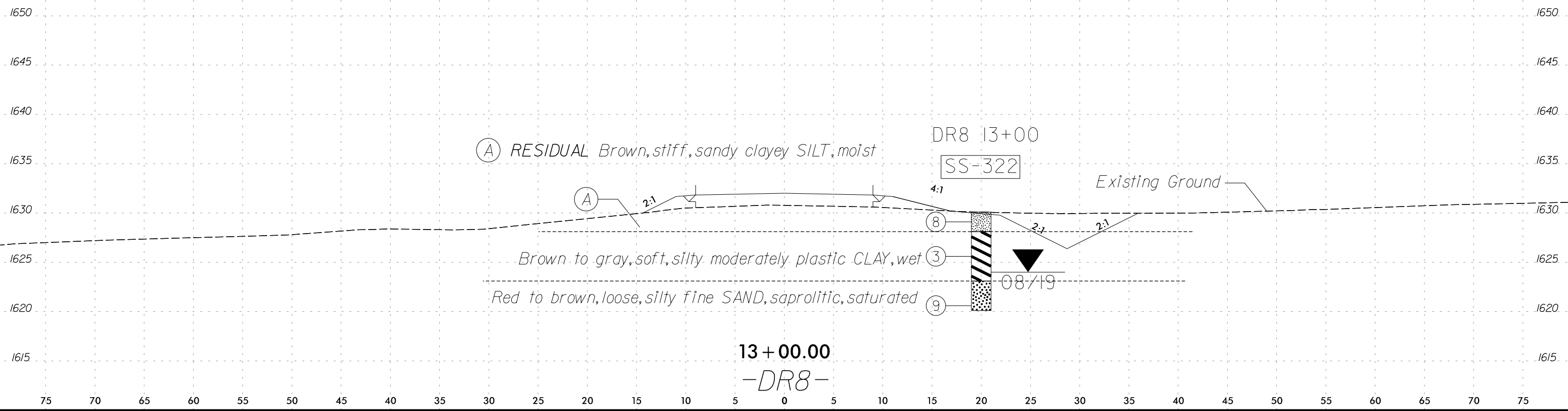
-DR7-



75 70 65 60 55 50 45 40 35 30 25 20 15 10 5 0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-322	13+00	20' RT	3.5-5.0	A-7-6 (19)	47	23	3	24	23	50	100	99	79.9	32.4	-

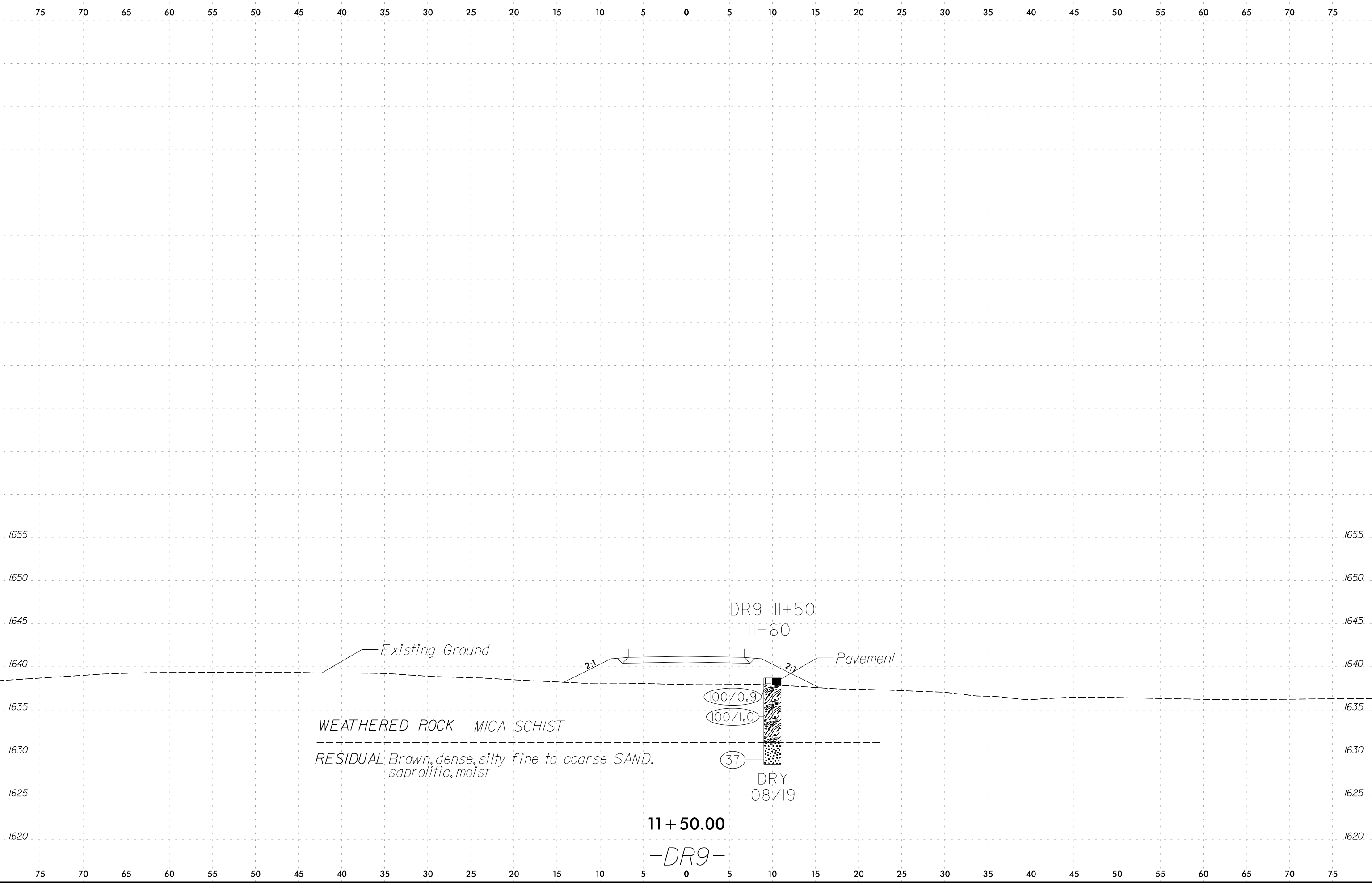
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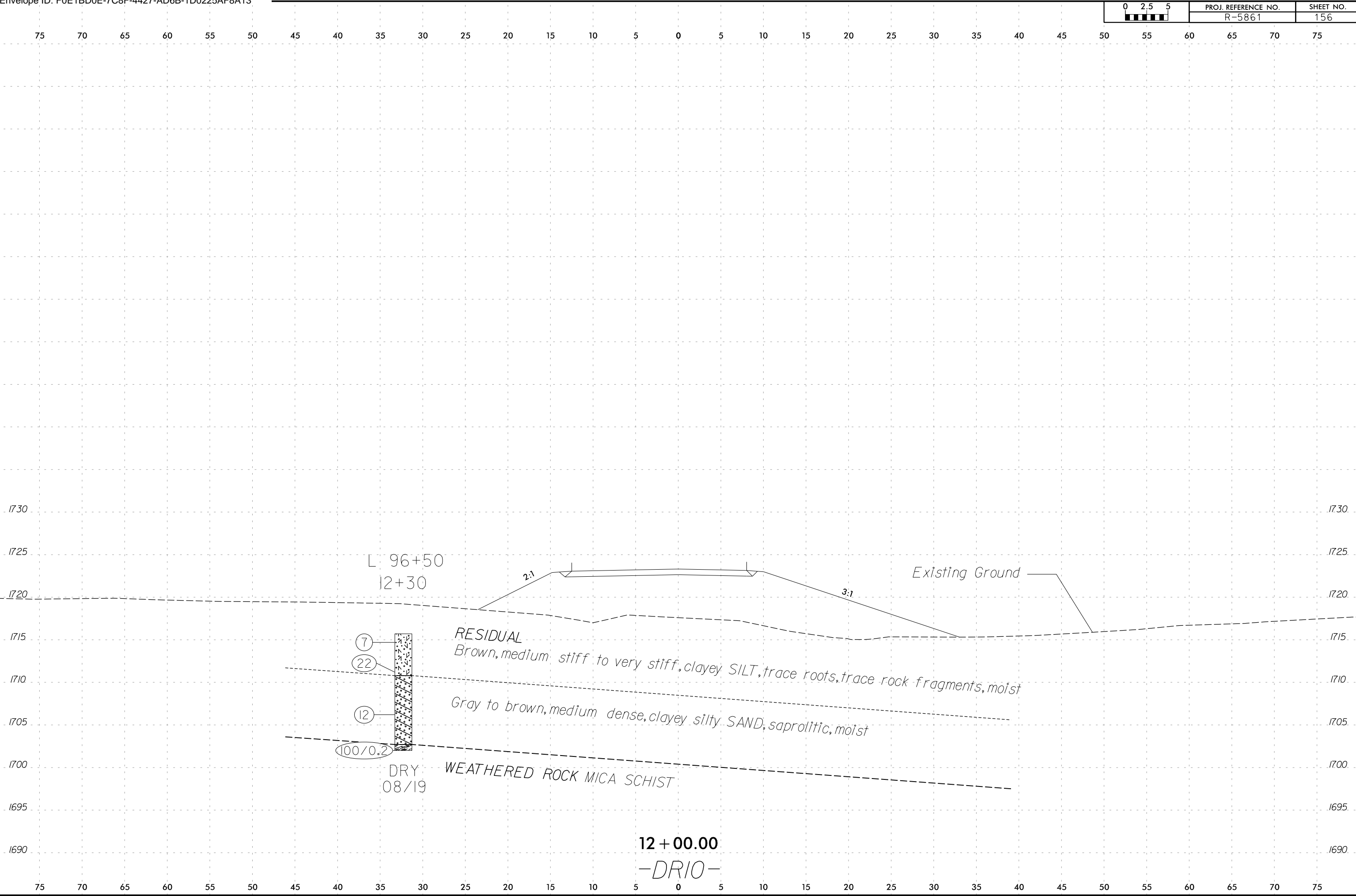
13 + 00.00  
-DR8-

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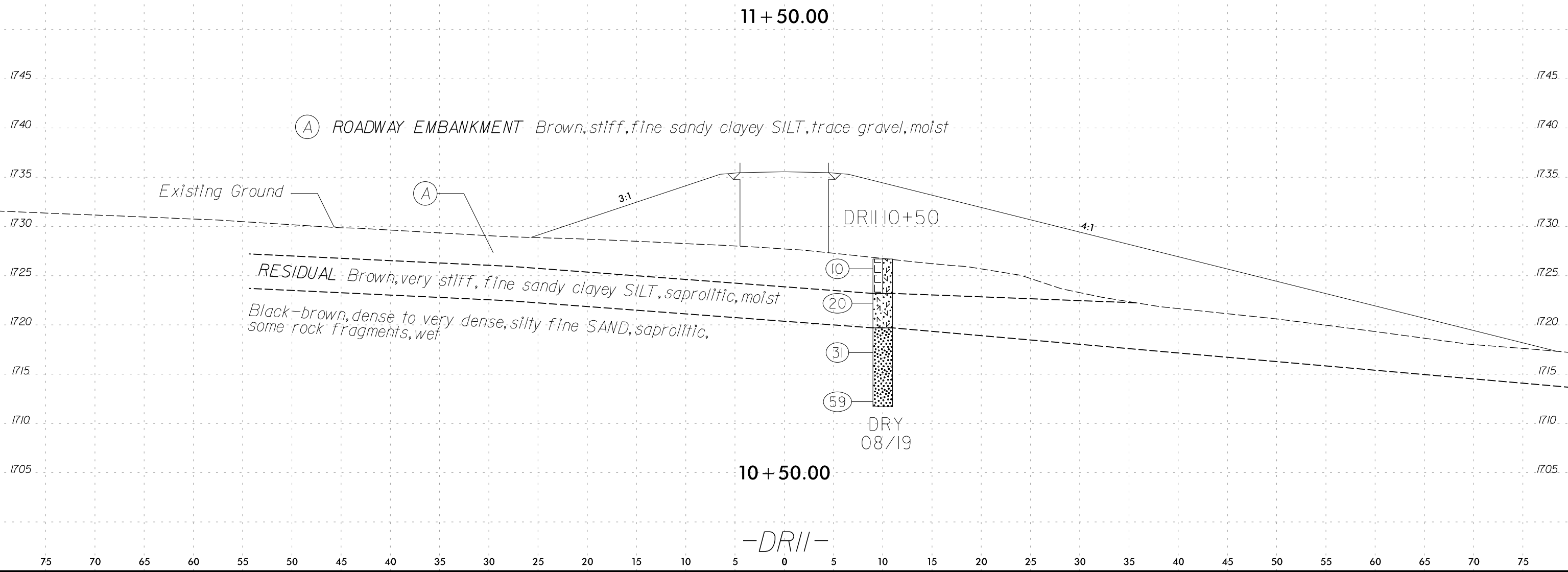
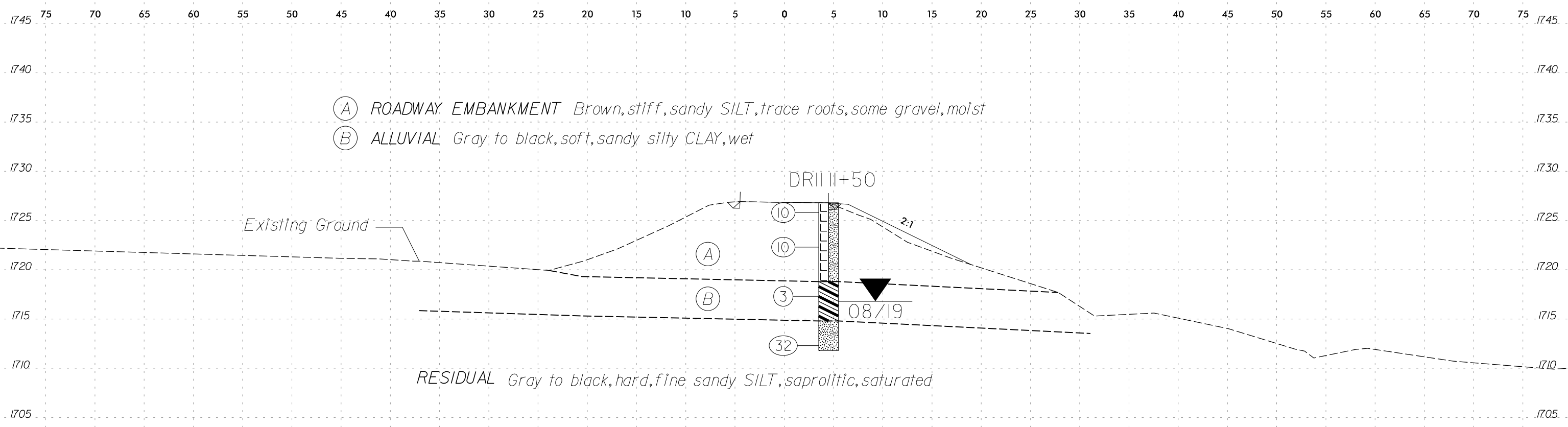
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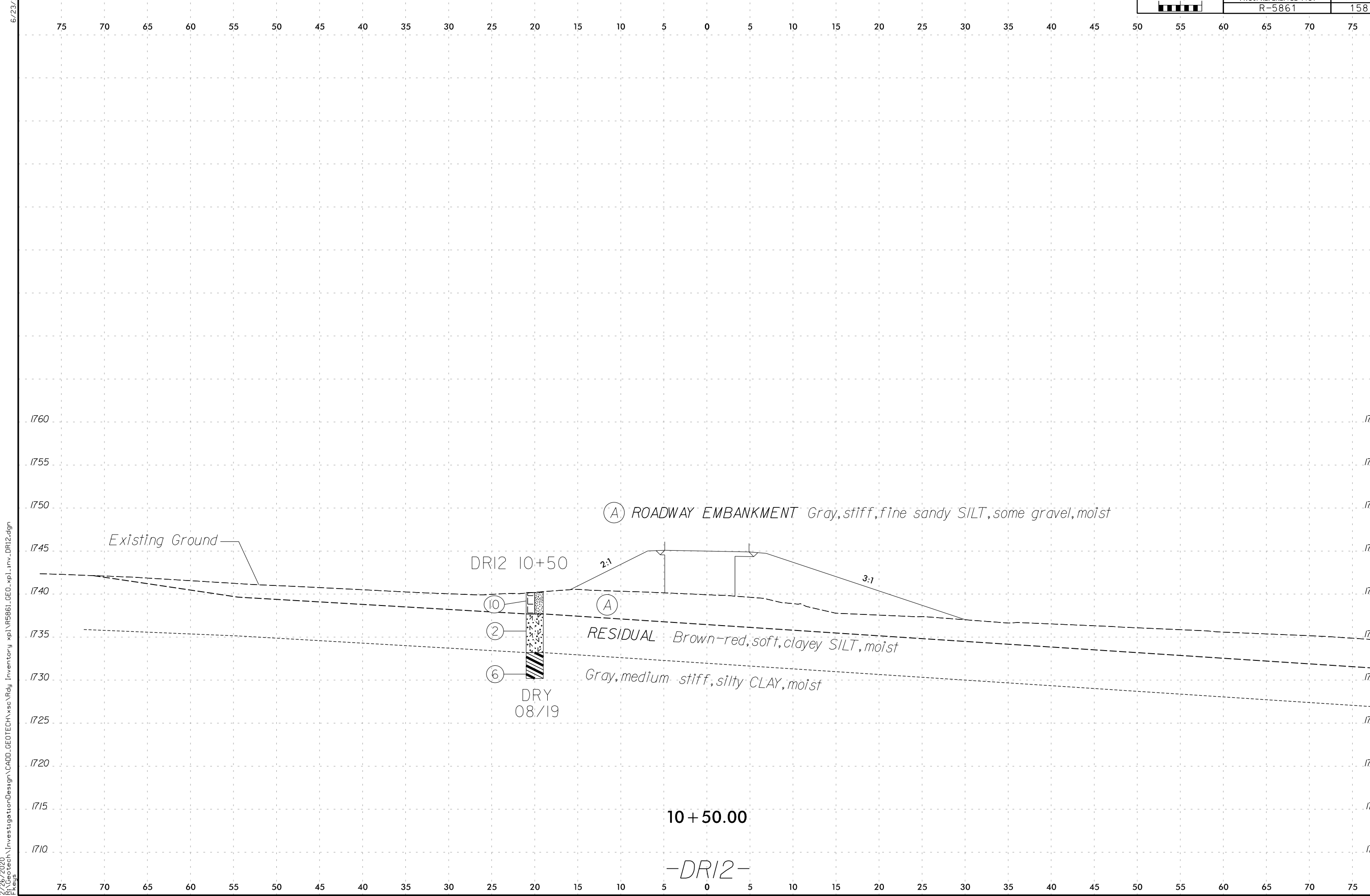


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P.Keijs



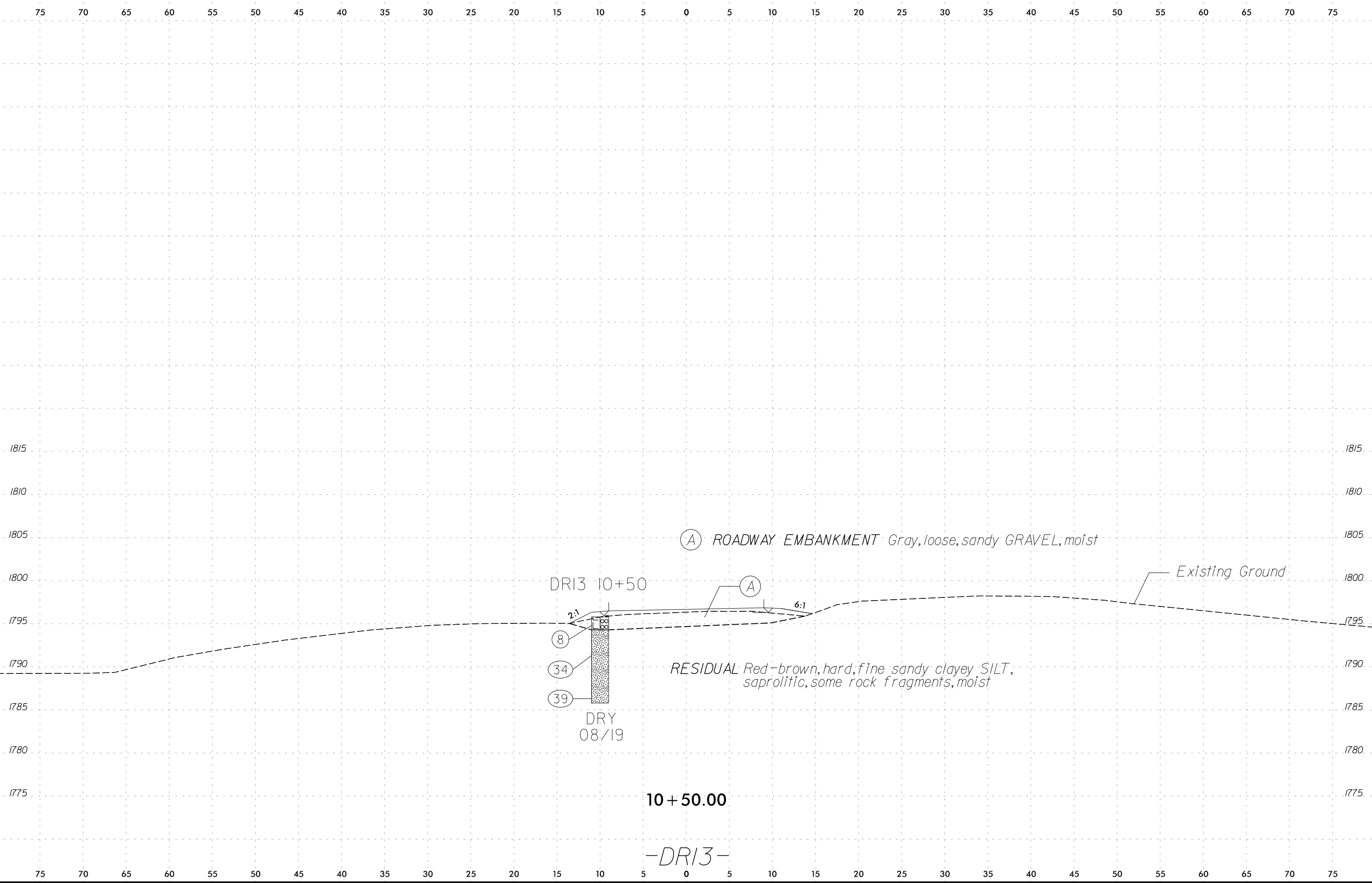
12 + 00.00  
-DR10-





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P. Keijs



DR13 10+50

(A) ROADWAY EMBANKMENT Gray, loose, sandy GRAVEL, moist

Existing Ground

(8)  
(34)  
(39)

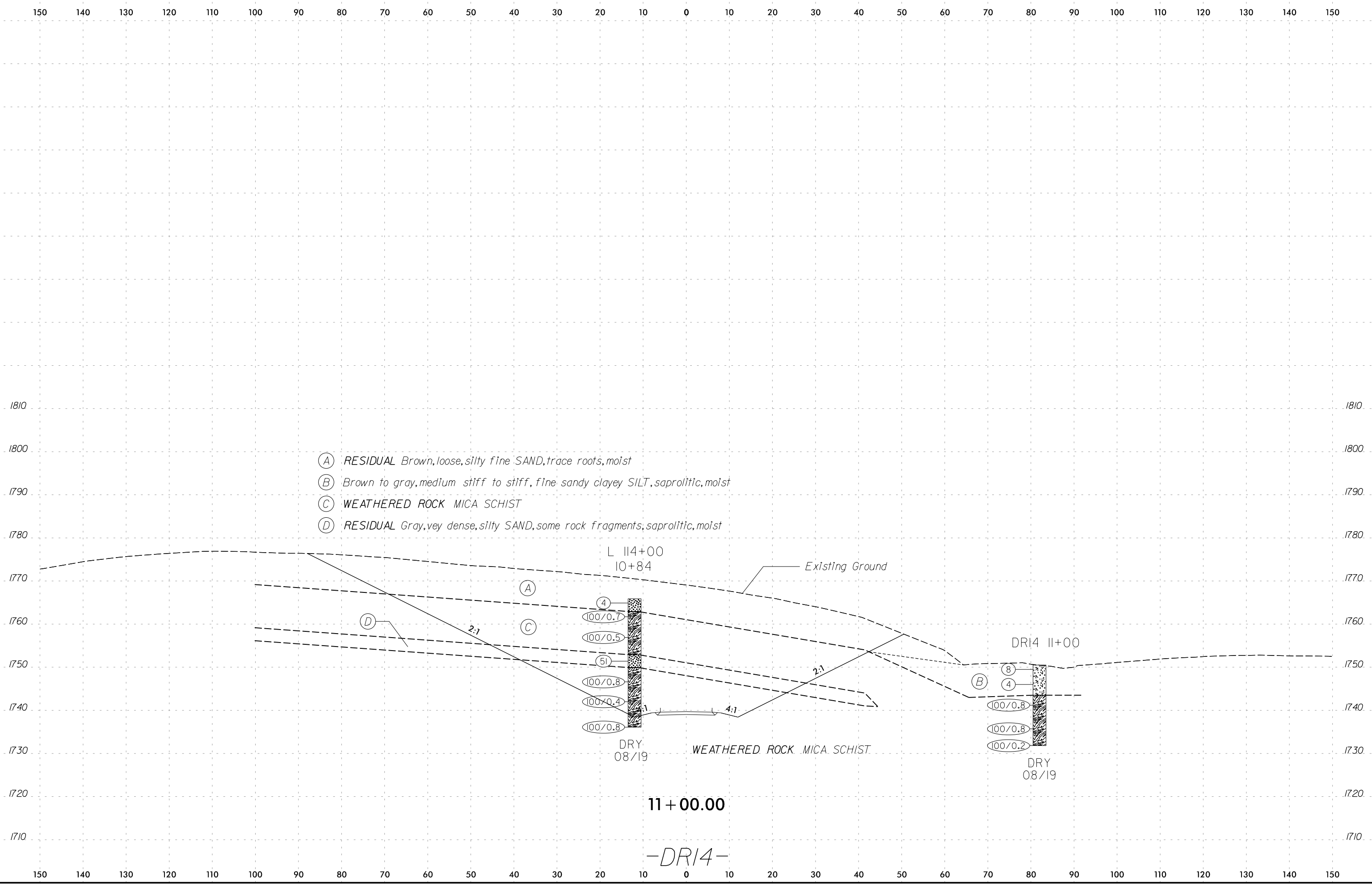
DRY  
08/19

RESIDUAL Red-brown, hard, fine sandy clayey SILT,  
saprolitic, some rock fragments, moist

10 + 50.00

-DR13-





- (A) RESIDUAL Brown, loose, silty fine SAND, trace roots, moist
- (B) Brown to gray, medium stiff to stiff, fine sandy clayey SILT, saprolitic, moist
- (C) WEATHERED ROCK MICA SCHIST
- (D) RESIDUAL Gray, very dense, silty SAND, some rock fragments, saprolitic, moist

L 11+00  
10+84

Existing Ground

DRI4 11+00

DRY  
08/19

WEATHERED ROCK MICA SCHIST

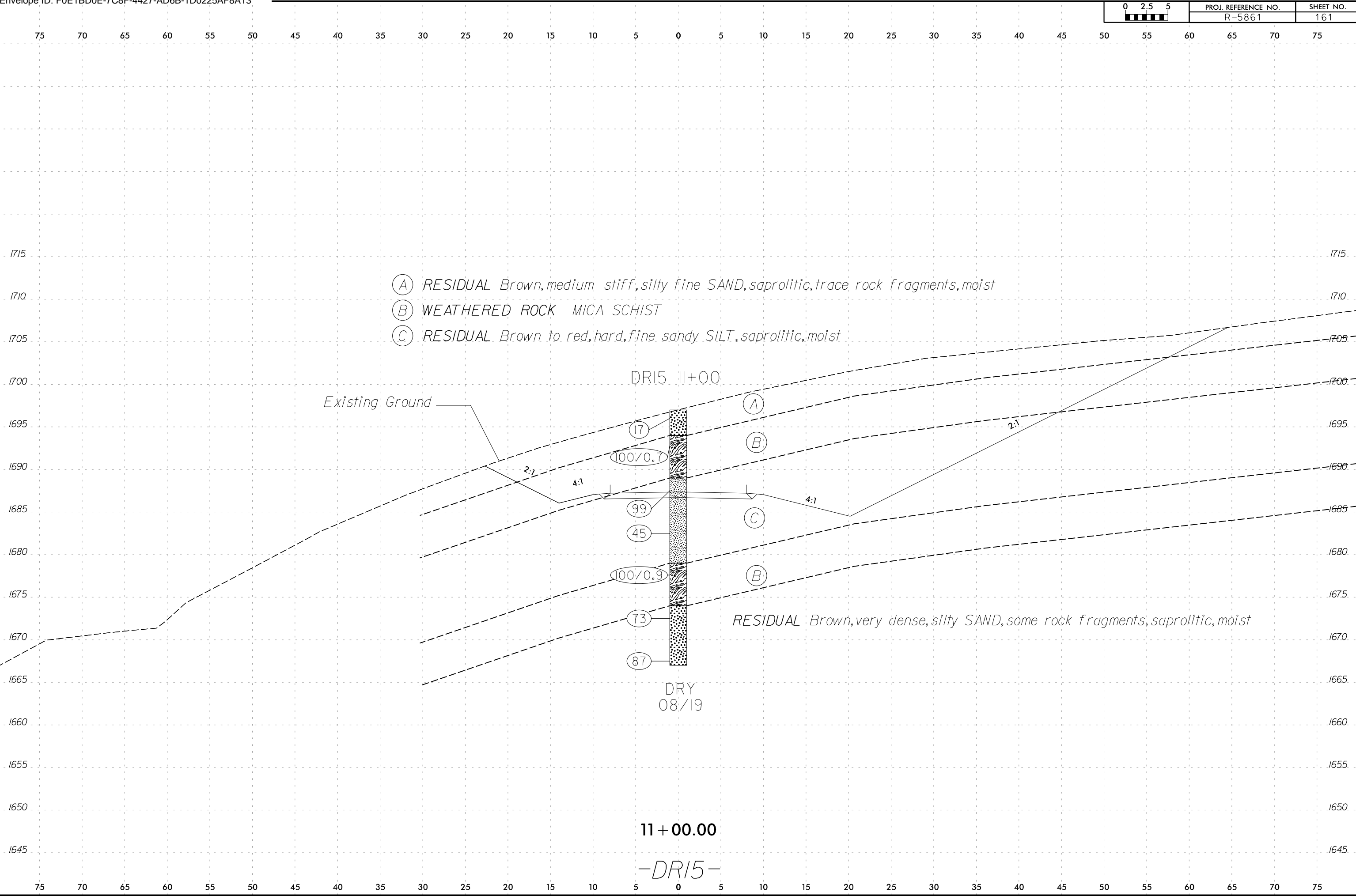
DRY  
08/19

11 + 00.00

-DRI4-

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- (A) RESIDUAL Brown, medium stiff, silty fine SAND, saprolitic, trace rock fragments, moist
- (B) WEATHERED ROCK MICA SCHIST
- (C) RESIDUAL Brown to red, hard, fine sandy SILT, saprolitic, moist

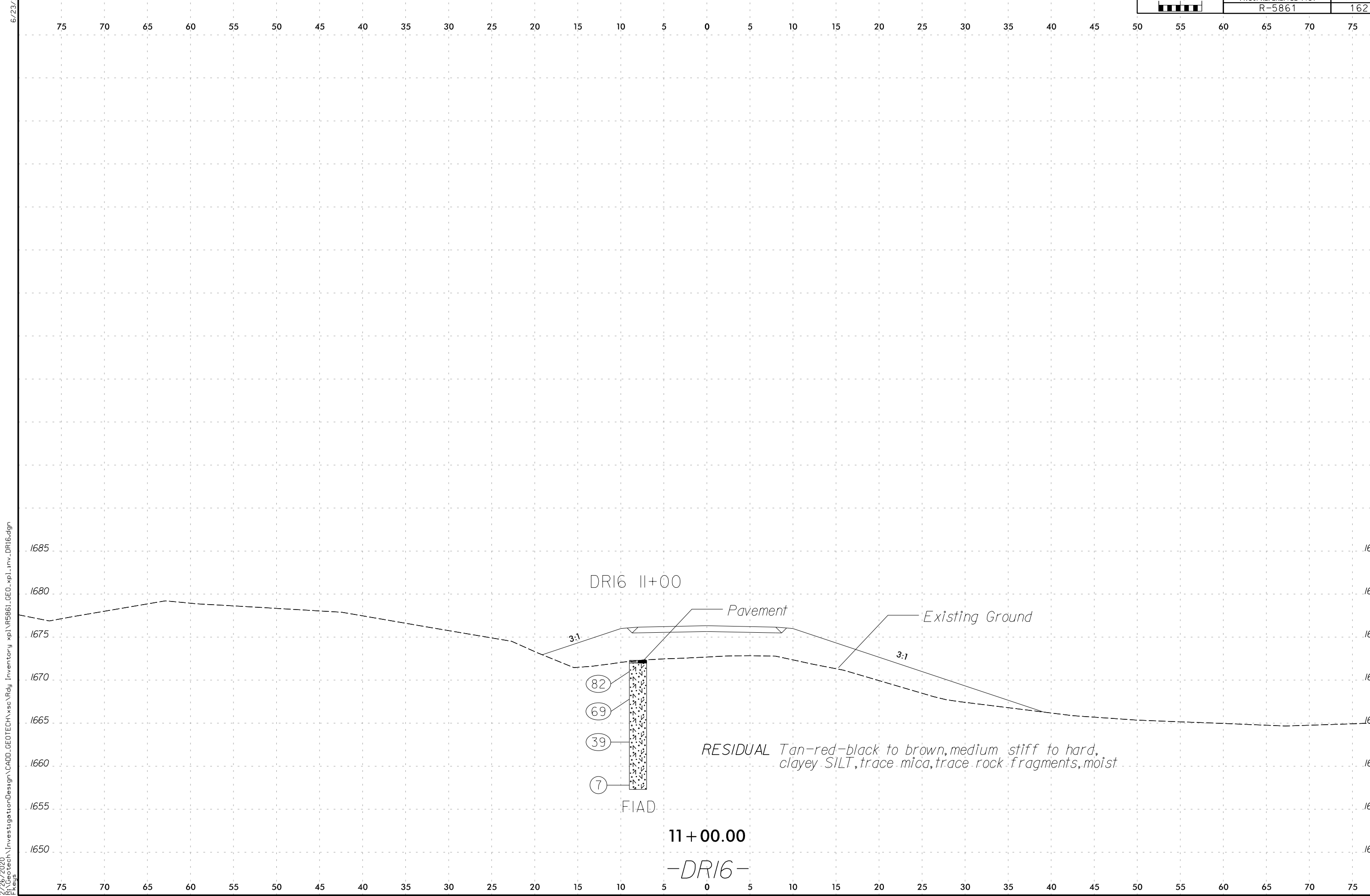
RESIDUAL Brown, very dense, silty SAND, some rock fragments, saprolitic, moist

DR15 11+00

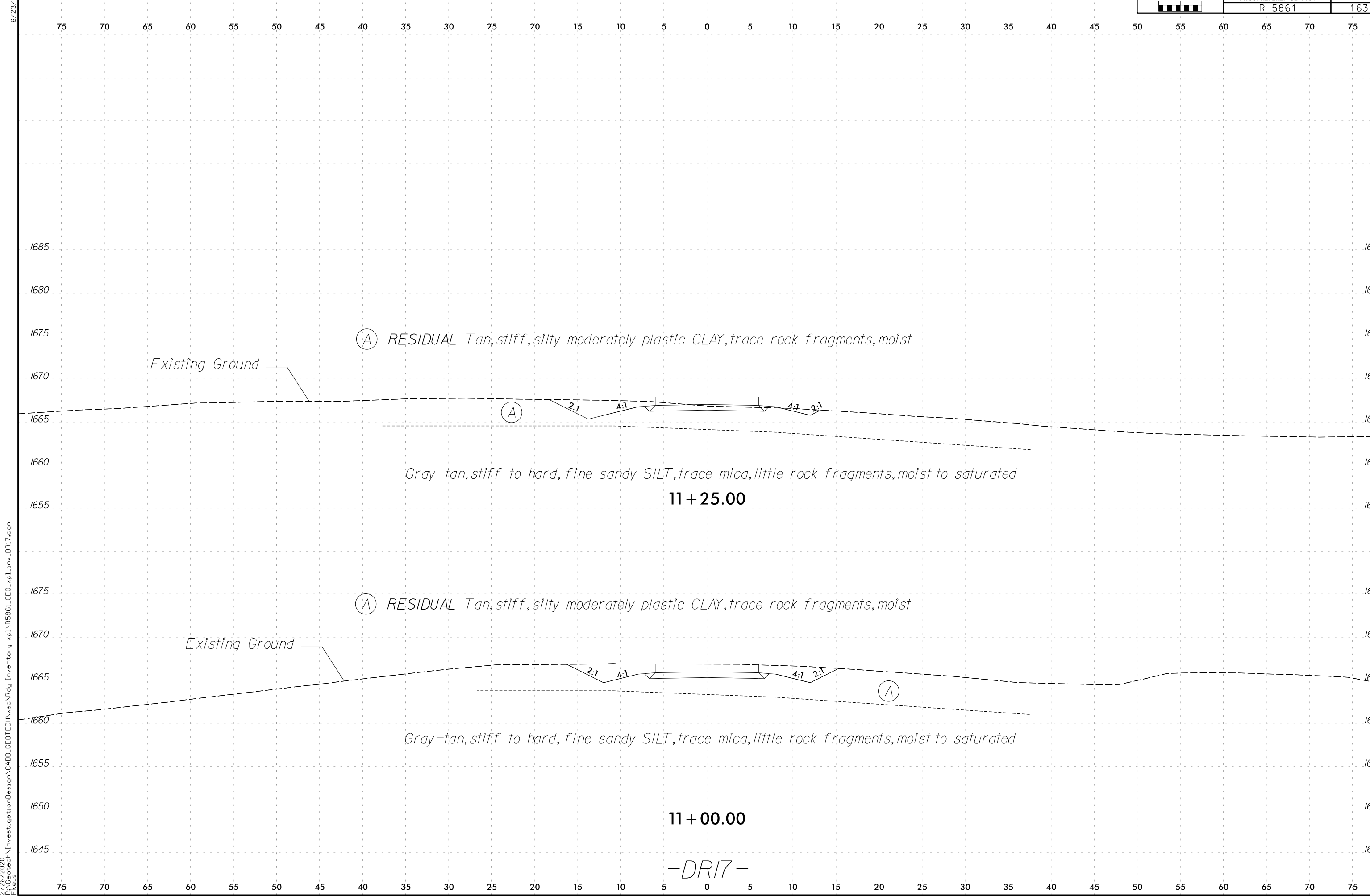
DRY  
08/19

11 + 00.00

—DR15—



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 P:\Geotech\



(A) RESIDUAL Tan, stiff, silty moderately plastic CLAY, trace rock fragments, moist

Existing Ground

(A)

2:1

4:1

4:1

2:1

Gray-tan, stiff to hard, fine sandy SILT, trace mica, little rock fragments, moist to saturated

11 + 25.00

(A) RESIDUAL Tan, stiff, silty moderately plastic CLAY, trace rock fragments, moist

Existing Ground

(A)

2:1

4:1

4:1

2:1

Gray-tan, stiff to hard, fine sandy SILT, trace mica, little rock fragments, moist to saturated

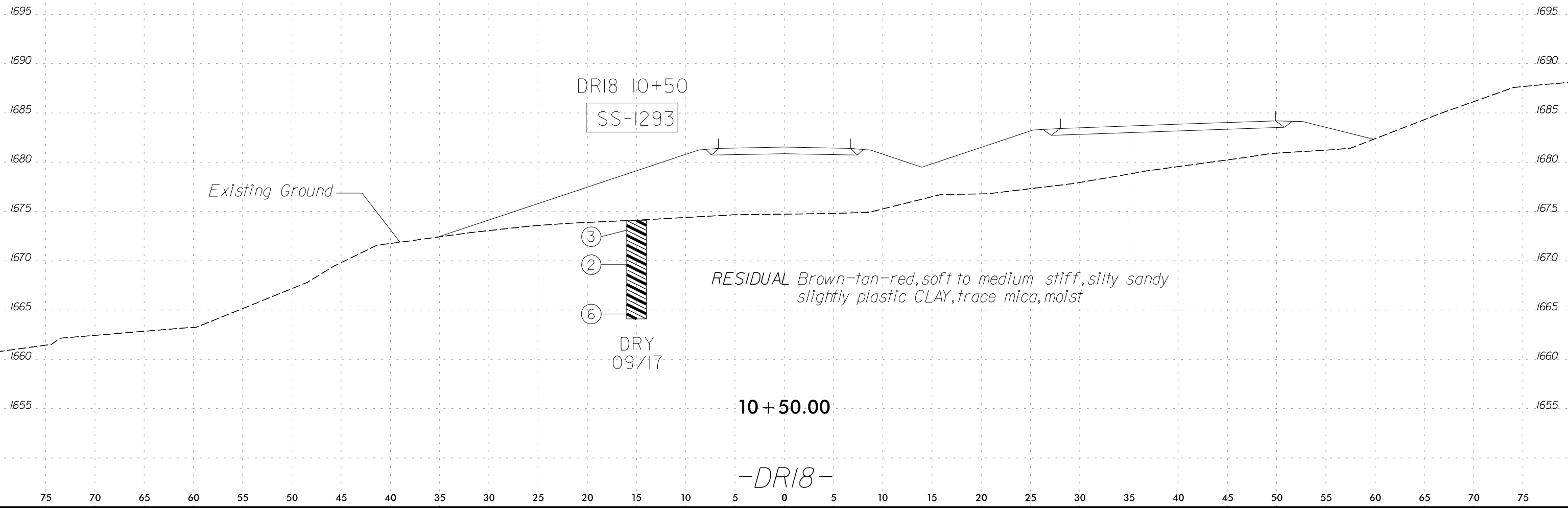
11 + 00.00

-DR17-

2/26/2020  
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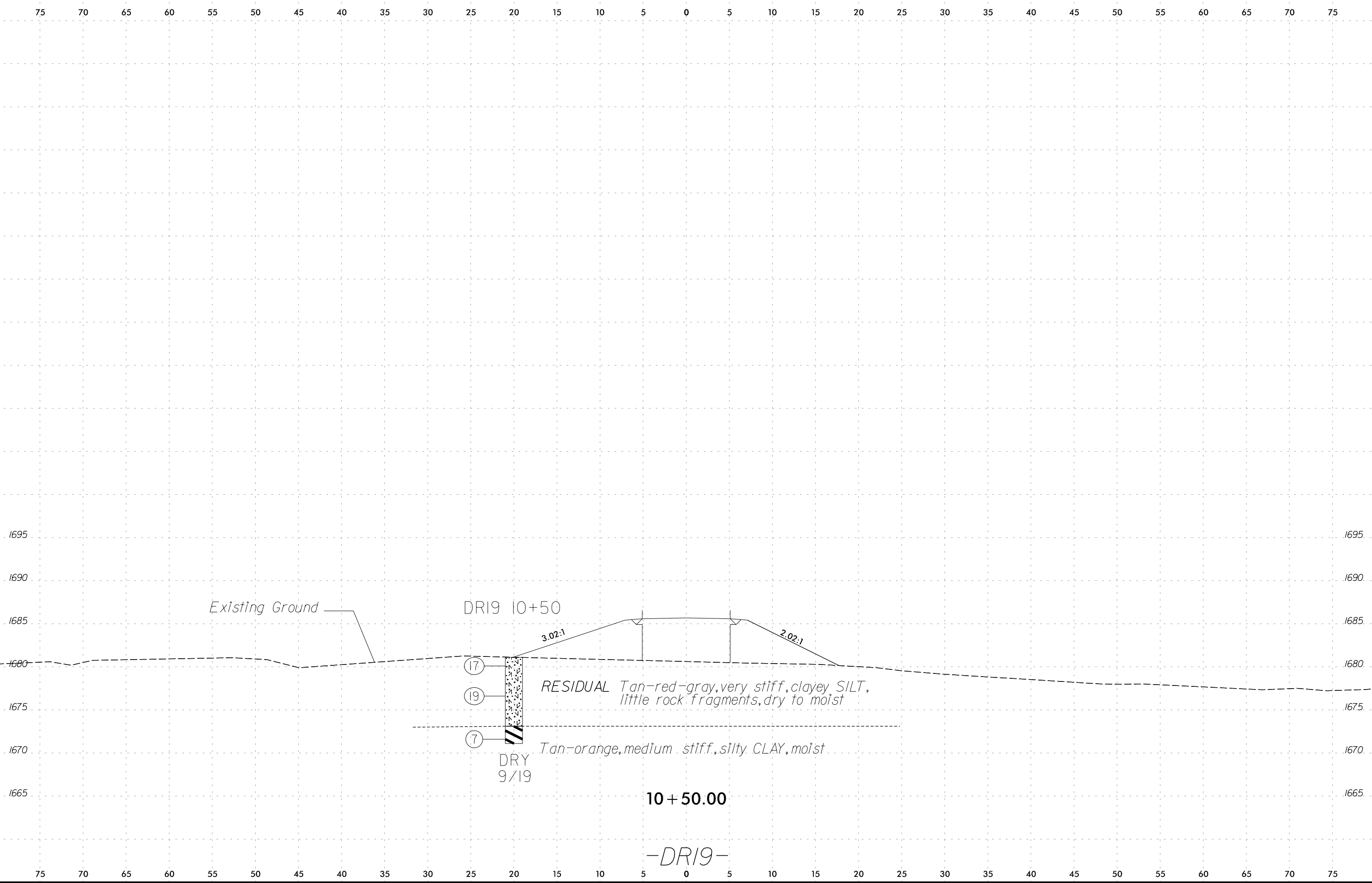
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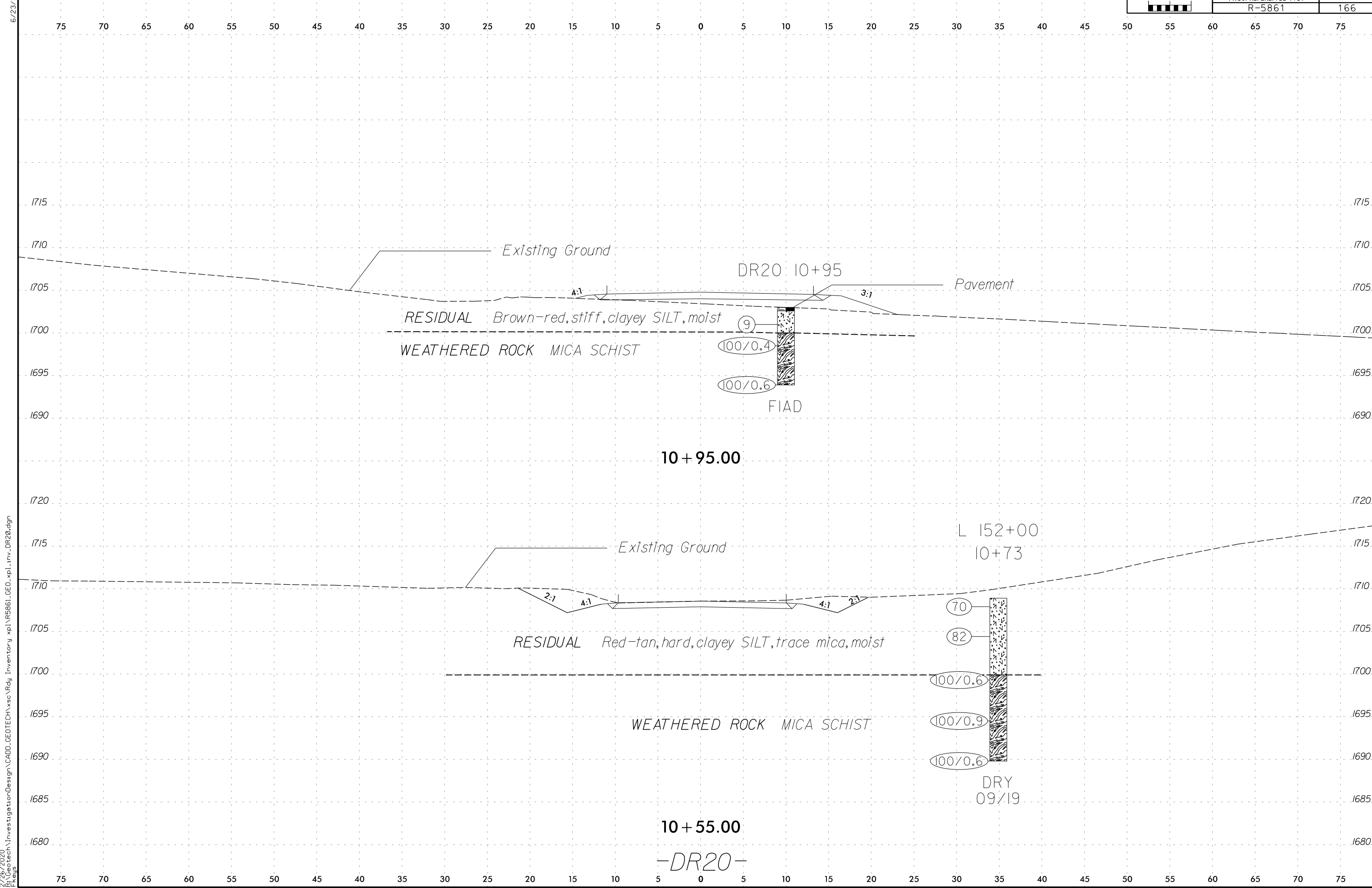
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1293	10+50	15' LT	3.5-5.0	A-6 (3)	40	11	22	12	32	34	69	57	47.4	24.6	-



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P.Keijs

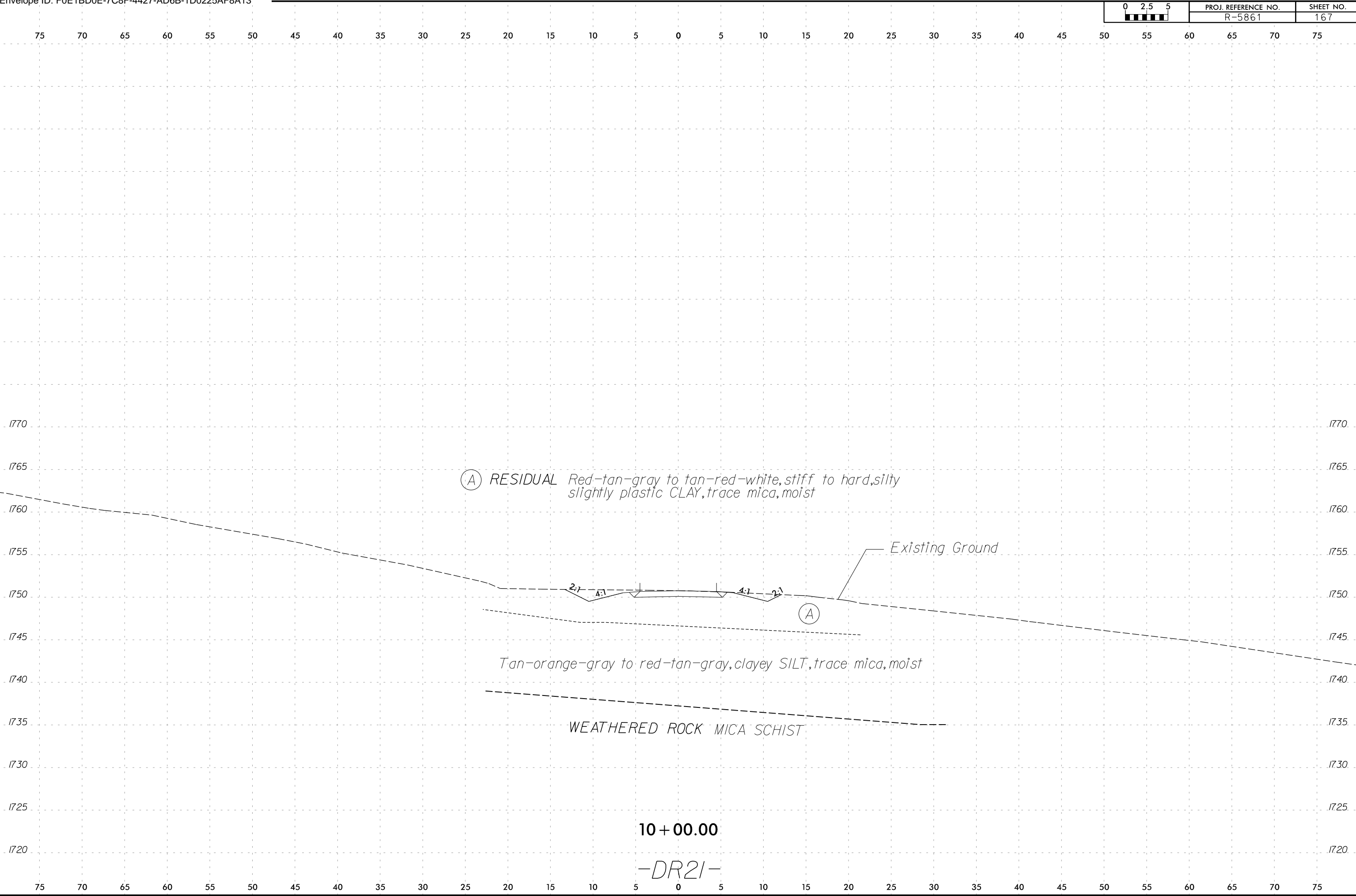


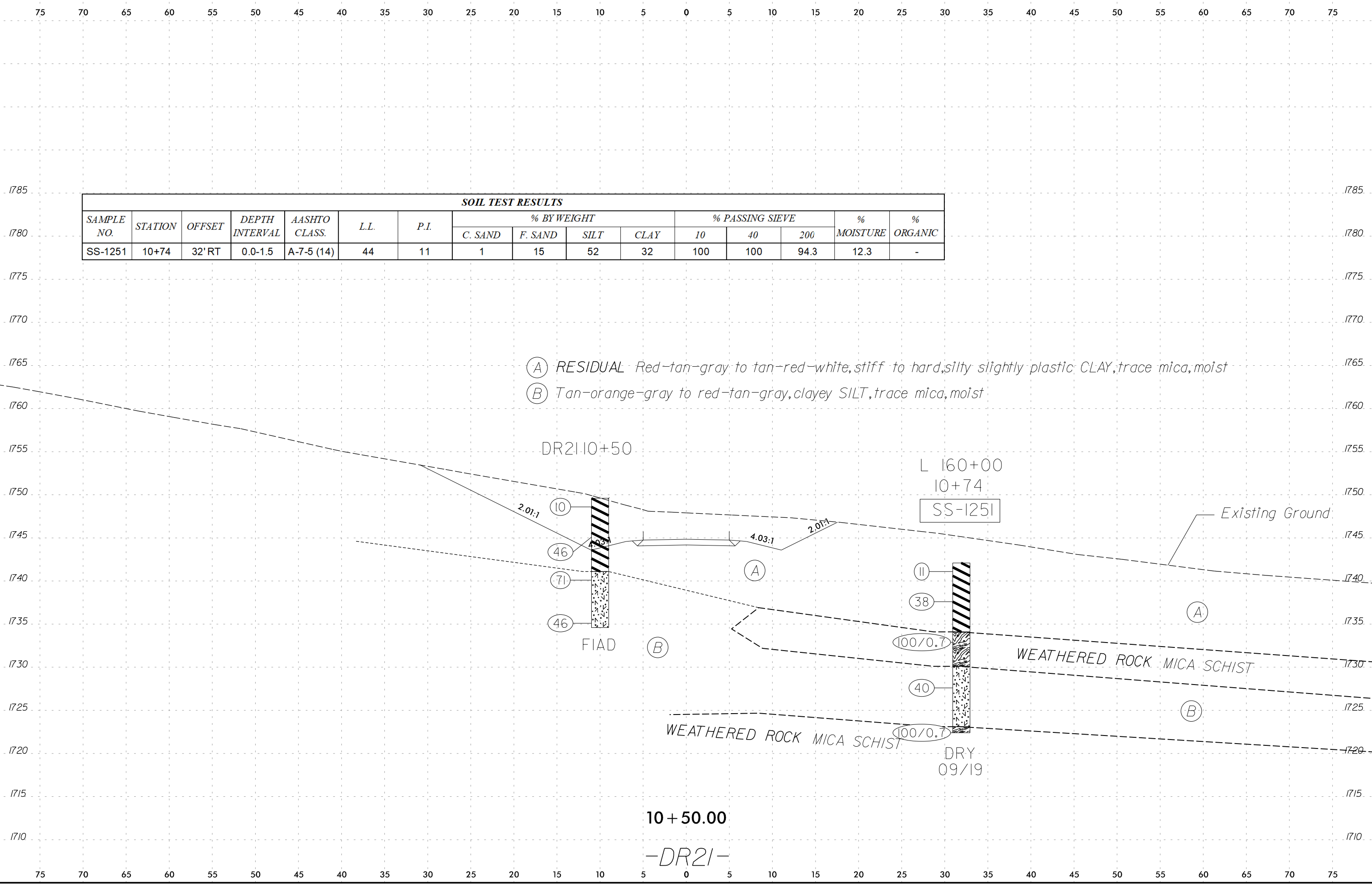


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P\_kleja



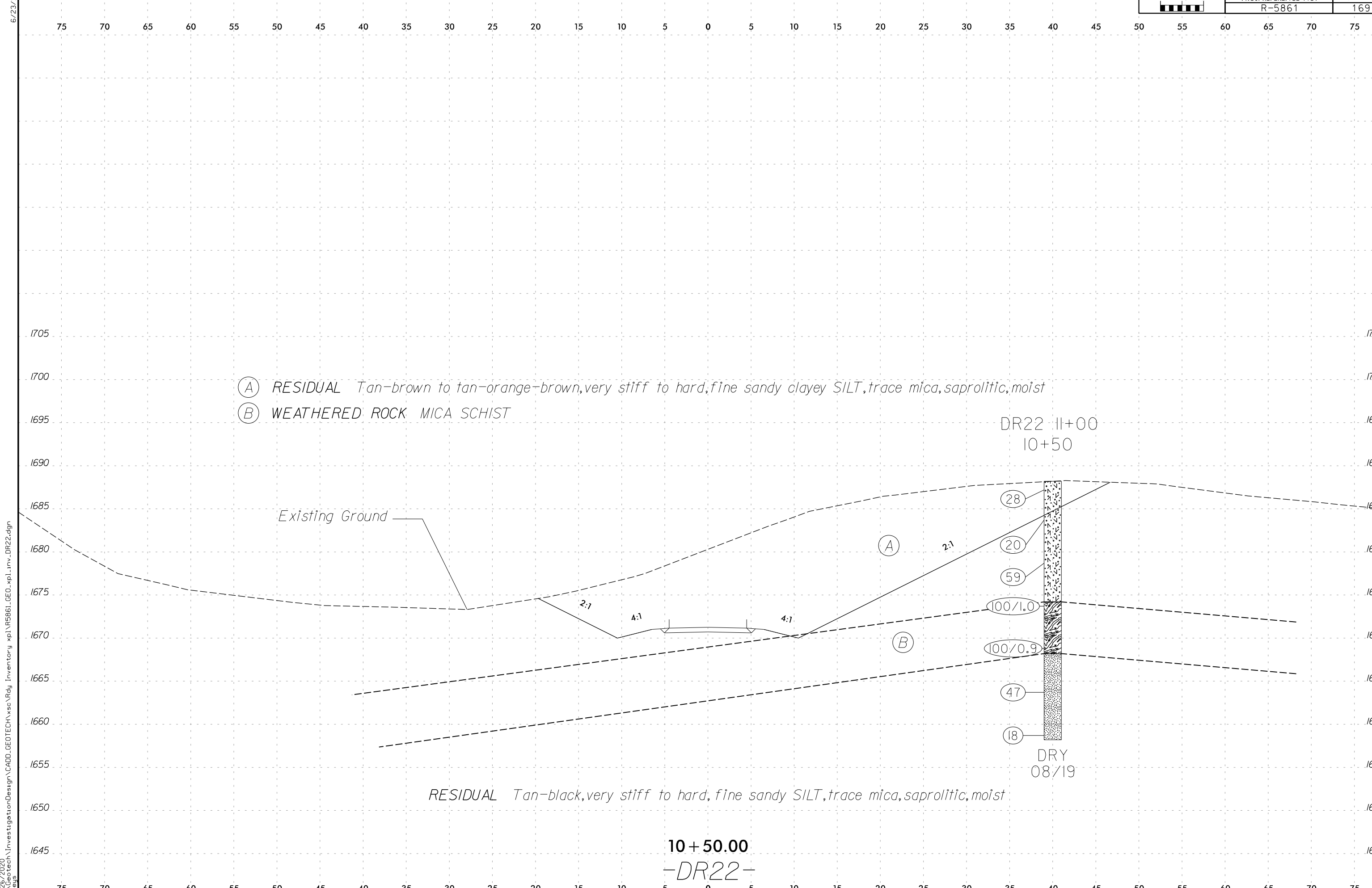


**SOIL TEST RESULTS**

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1251	10+74	32' RT	0.0-1.5	A-7-5 (14)	44	11	1	15	52	32	100	100	94.3	12.3	-

- (A) RESIDUAL Red-tan-gray to tan-red-white, stiff to hard, silty slightly plastic CLAY, trace mica, moist
- (B) Tan-orange-gray to red-tan-gray, clayey SILT, trace mica, moist

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(A) RESIDUAL Tan-brown to tan-orange-brown, very stiff to hard, fine sandy clayey SILT, trace mica, saprolitic, moist  
 (B) WEATHERED ROCK MICA SCHIST

DR22 11+00  
10+50

Existing Ground

2:1

4:1

4:1

(A)

(B)

(28)

(20)

(59)

100/1.0

100/0.9

(47)

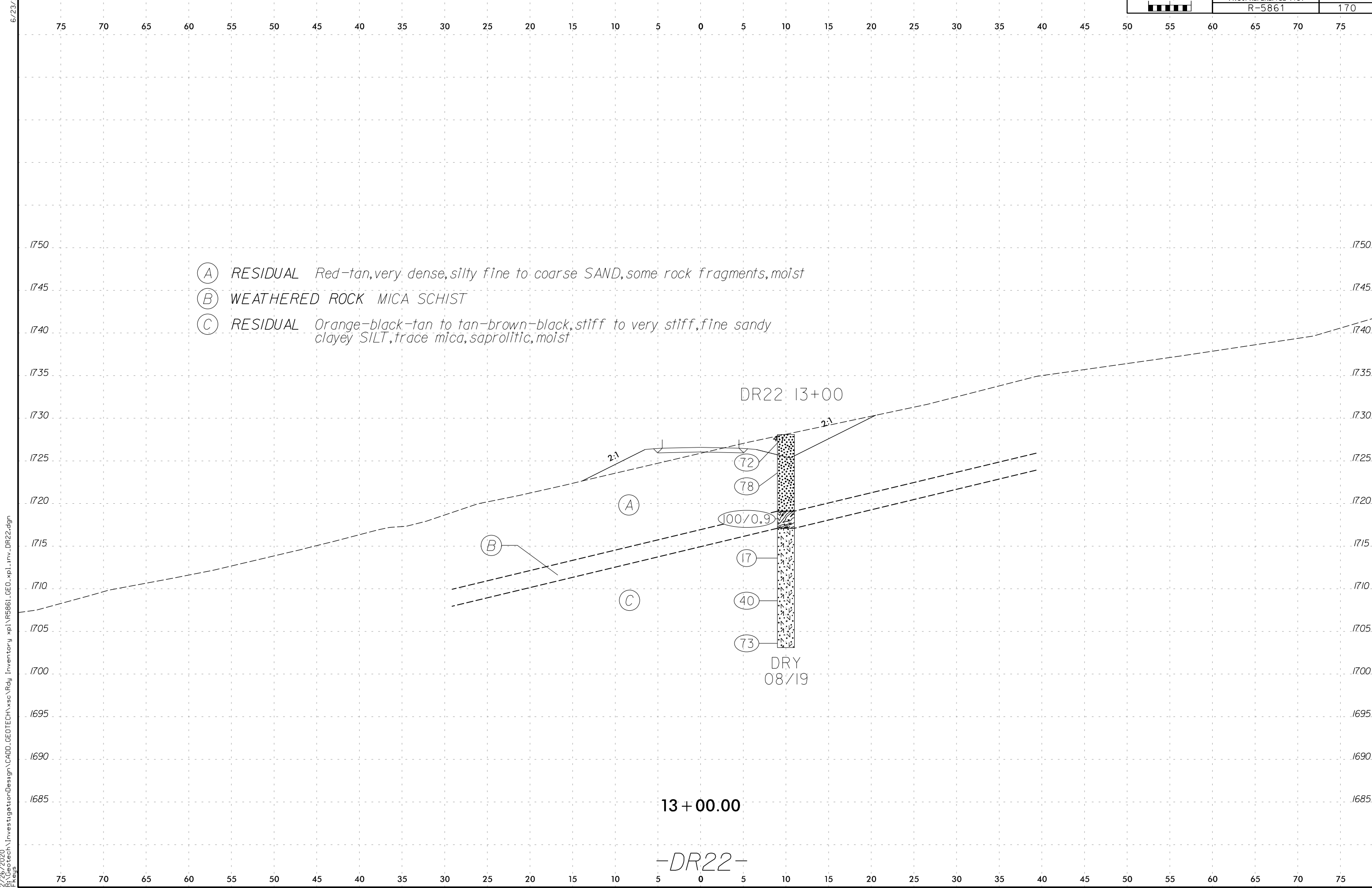
(18)

DRY  
08/19

RESIDUAL Tan-black, very stiff to hard, fine sandy SILT, trace mica, saprolitic, moist

10 + 50.00  
-DR22-

2/26/2020  
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- (A) RESIDUAL Red-tan, very dense, silty fine to coarse SAND, some rock fragments, moist
- (B) WEATHERED ROCK MICA SCHIST
- (C) RESIDUAL Orange-black-tan to tan-brown-black, stiff to very stiff, fine sandy clayey SILT, trace mica, saprolitic, moist

DR22 13+00

2:1

2:1

72

78

100/0.9

17

40

73

DRY  
08/19

(A)

(B)

(C)

13 + 00.00

-DR22-

2/26/2020  
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P.kujala

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5861	1	171

**STATE OF NORTH CAROLINA**  
**DEPARTMENT OF TRANSPORTATION**  
**DIVISION OF HIGHWAYS**  
**GEOTECHNICAL ENGINEERING UNIT**

**ROADWAY**  
**SUBSURFACE INVESTIGATION**  
**APPENDICES**

**REFERENCE: R-5861**

**PROJECT: 47427**



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# GEOTECHNICAL BORING REPORT

## BORE LOG

<b>WBS</b> 47427.1.1		<b>TIP</b> R-5861		<b>COUNTY</b> CHEROKEE		<b>GEOLOGIST</b> Mize, J.										
<b>SITE DESCRIPTION</b> Widening US 19/129 from the Georgia State Line to US 64/74							<b>GROUND WTR (ft)</b>									
<b>BORING NO.</b> L 94+72 AP		<b>STATION</b> 94+72		<b>OFFSET</b> 90 ft LT		<b>ALIGNMENT</b> L	0 HR. Dry									
<b>COLLAR ELEV.</b> 1,722.2 ft		<b>TOTAL DEPTH</b> 17.7 ft		<b>NORTHING</b> 496,083		<b>EASTING</b> 478,197	24 HR. Dry									
<b>DRILL RIG/HAMMER EFF./DATE</b> SME267 DIEDRICH D-50 74% 10/20/2017				<b>DRILL METHOD</b> H.S. Augers		<b>HAMMER TYPE</b> Automatic										
<b>DRILLER</b> Blizzard, B.		<b>START DATE</b> 08/13/19		<b>COMP. DATE</b> 08/13/19		<b>SURFACE WATER DEPTH</b> N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft)	DEPTH (ft)		
1725														1,722.2	0.0	GROUND SURFACE
1720																<b>RESIDUAL</b> Brown, sandy SILT (A-4)
1715																
1710	1,711.0	11.2												1,713.2	9.0	<b>WEATHERED ROCK</b> MICA SCHIST
	1,708.7	13.5	100/0.4													
1705	1,704.5	17.7	44	40	60/0.2											
			60/0.0											1,704.5	17.7	Boring Terminated BY AUGER REFUSAL at Elevation 1,704.5 ft on Crystalline Rock: MICA SCHIST

NCDOT BORE DOUBLE R-5861.GPJ NC\_DOT.GDT 2/23/20

**CBR (CALIFORNIA BEARING RATIO)  
OF LABORATORY COMPACTED SOIL**



AASHTO T 193

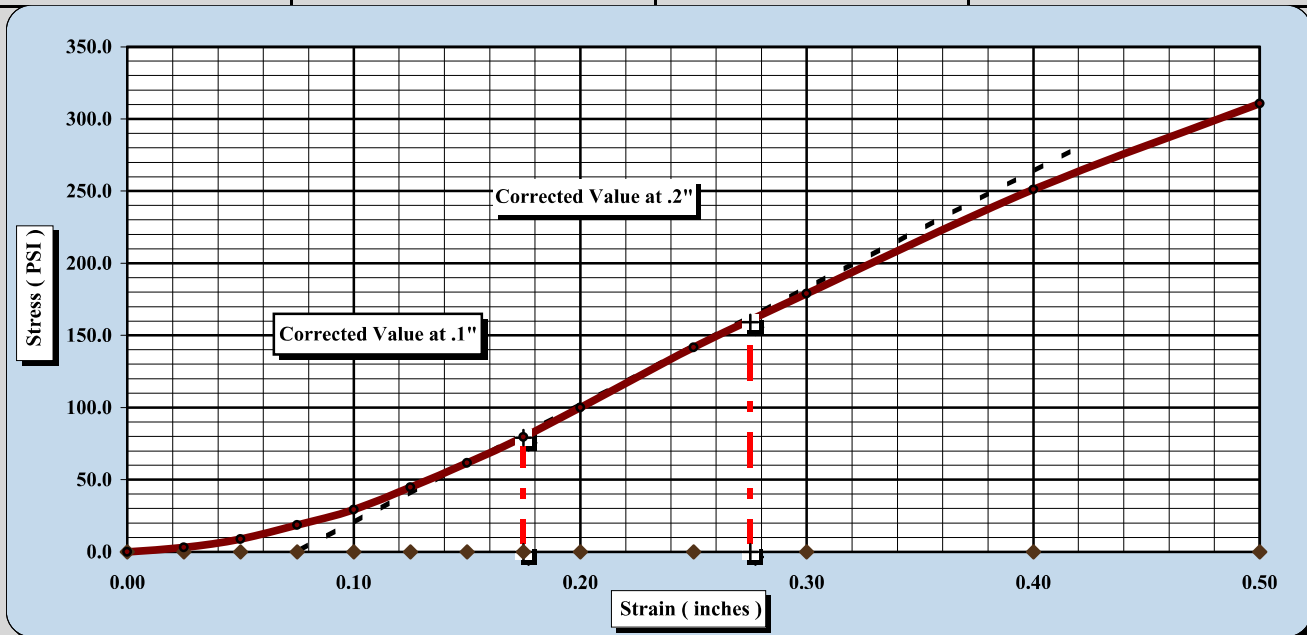
S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

Project #:	1934-19-002	Report Date:	10/16/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s)	10/10 - 10/16/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	L 90+00 AP	Sample #:	S-225
Station #:	90+00	Sample Date:	N/A
	Offset: N/A	Depth (ft):	1.0-8.5

Sample Description: Tan Coarse to Fine Sandy Silty CLAY (A-4) (0)

AASHTO T99 Method A	Maximum Dry Density: 115.0 PCF	Optimum Moisture Content: 14.5%
Compaction Test performed on grading complying with CBR spec.	% Retained on the 3/4" sieve: 0.0%	

Uncorrected CBR Values		Corrected CBR Values	
CBR at 0.1 in.	2.9	CBR at 0.1 in.	7.9
CBR at 0.2 in.	6.7	CBR at 0.2 in.	10.6



CBR Sample Preparation:

The entire gradation was used and compacted in a 6" CBR mold in accordance with AASHTO T 193, Section 5.1.1

Before Soaking		After Soaking	
Compactive Effort (Blows per Layer)	56	Final Dry Density (PCF)	114.4
Initial Dry Density (PCF)	115.0	Average Final Moisture Content	16.0%
Moisture Content of the Compacted Specimen	14.5%	Moisture Content (top 1" after soaking)	17.8%
Percent Compaction	100.0%	Percent Swell	0.7%

Soak Time:	96 hrs.	Surcharge Weight	10.0	Surcharge Wt. per sq. Ft.	50.9
Liquid Limit	29	Plastic Index	5		

Notes/Deviations/References:

Test specimen compacted to 100% at optimum moisture.

Mal Krajan, ET  
Technical Responsibility

*[Signature]*  
Signature

Laboratory Manager  
Position

10/16/2019  
Date

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**MOISTURE - DENSITY REPORT**



SHEET 172

Quality Assurance

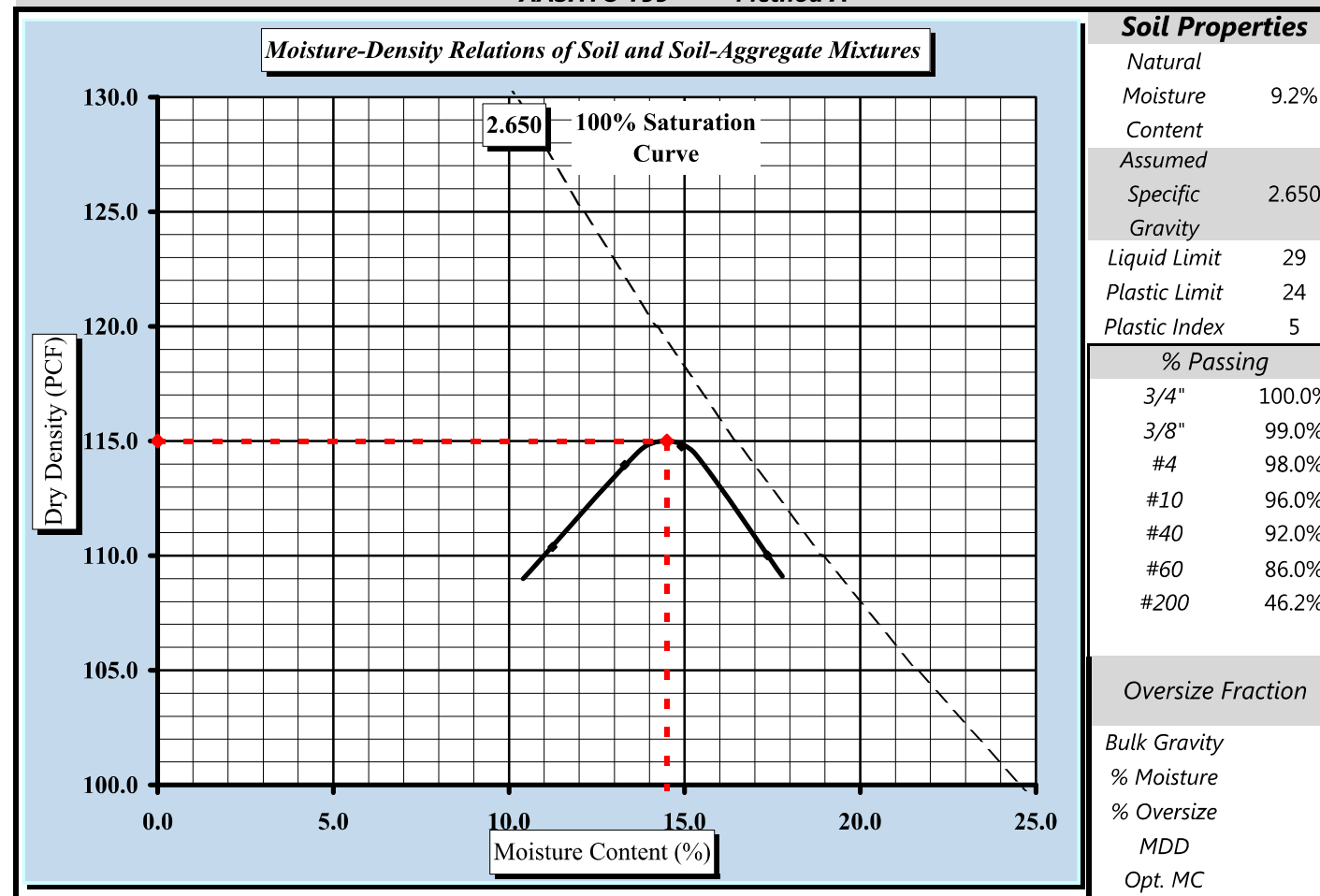
S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

S&ME Project #:	1943-19-002	Report Date:	10/11/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s):	10/4 - 10/11/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	L 900+00 AP	Sample #:	S-225
Satation:	90+00	Sample Date:	N/A
	Offset: N/A	Depth (ft):	1.0 - 8.5 ft.

Sample Description: Tan Coarse to Fine Sandy Silty CLAY (A-4) (0)

Maximum Dry Density	115.0	PCF.	Optimum Moisture Content	14.5%
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AASHTO T99 - - Method A



Moisture-Density Curve Displayed: Fine Fraction  Corrected for Oversize Fraction (ASTM D 4718)   
 Sieve Size used to separate the Oversize Fraction: #4 Sieve  3/8 inch Sieve  3/4 inch Sieve   
 Mechanical Rammer  Manual Rammer  Moist Preparation  Dry Preparation

References / Comments / Deviations:

AASHTO T265: Laboratory Determination of Moisture Content of Soils  
 AASHTO T 99: Moisture-Density Relations of Soil Using a 5.5 Lb. Rammer and a 12" Drop

Mal Krajan, ET  
Technical Responsibility

*[Signature]*  
Signature

Laboratory Manager  
Position

10/11/2019  
Date

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**CBR (CALIFORNIA BEARING RATIO)  
OF LABORATORY COMPACTED SOIL**



AASHTO T 193

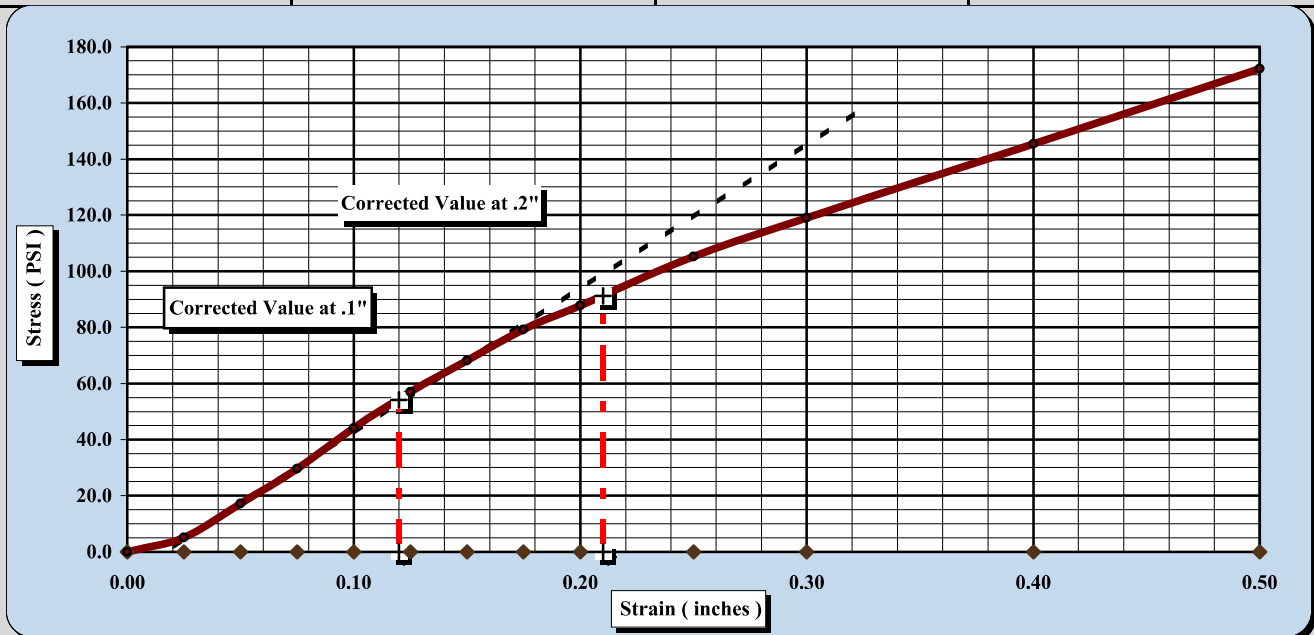
S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

Project #:	1934-19-002	Report Date:	10/16/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s)	10/10 - 10/16/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	LDET6 23+65.75	Sample #:	S-1041
Station #:	23+65.75	Offset:	N/A
		Depth (ft):	0.0 - 8.5 ft.

Sample Description: Tan Coarse to Fine Sandy Clayey SILT (A-4) (8)

AASHTO T99 Method A	Maximum Dry Density:	107.1 PCF	Optimum Moisture Content:	17.9%
	Compaction Test performed on grading complying with CBR spec.		% Retained on the 3/4" sieve:	0.0%

Uncorrected CBR Values		Corrected CBR Values	
CBR at 0.1 in.	4.4	CBR at 0.1 in.	5.4
CBR at 0.2 in.	5.9	CBR at 0.2 in.	6.1



CBR Sample Preparation:

The entire gradation was used and compacted in a 6" CBR mold in accordance with AASHTO T 193, Section 5.1.1

Before Soaking		After Soaking	
Compactive Effort (Blows per Layer)	56	Final Dry Density (PCF)	105.4
Initial Dry Density (PCF)	106.8	Average Final Moisture Content	19.9%
Moisture Content of the Compacted Specimen	17.8%	Moisture Content (top 1" after soaking)	22.3%
Percent Compaction	99.7%	Percent Swell	1.5%

Soak Time:	96 hrs.	Surcharge Weight	10.0	Surcharge Wt. per sq. Ft.	50.9
Liquid Limit	39	Plastic Index	10		

Notes/Deviations/References:

Test specimen compacted to 100% at optimum moisture.

Mal Krajan, ET  
Technical Responsibility

Signature

Laboratory Manager  
Position

10/16/2019  
Date

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**MOISTURE - DENSITY REPORT**



SHEET 174

Quality Assurance

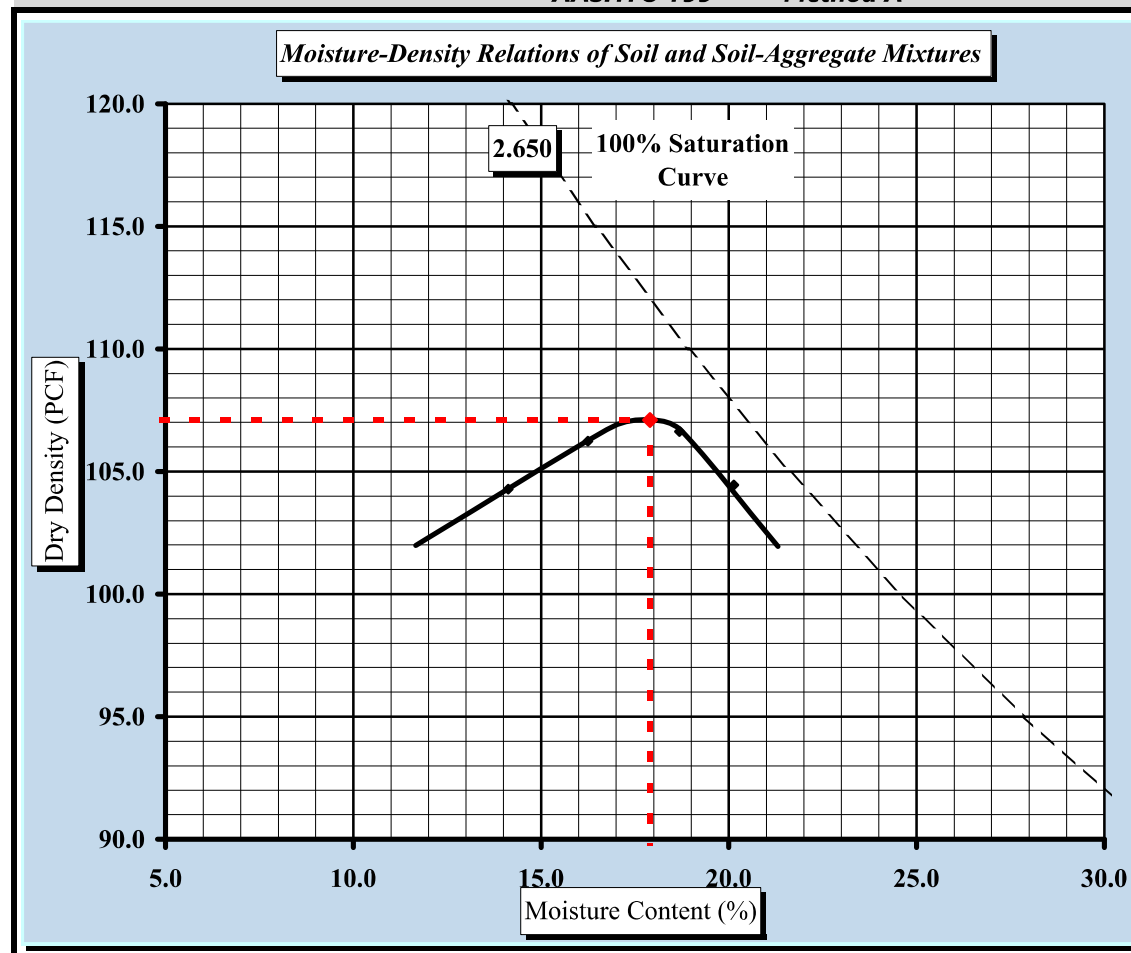
S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

S&ME Project #:	1943-19-022	Report Date:	10/11/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s):	10/4 - 10/11/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	LDET6 23+65.75	Sample #:	S-1041
Station:	23+65.75	Offset:	N/A
		Depth (ft):	0.0 - 8.5 ft.

Sample Description: Tan Coarse to Fine Sandy Clayey SILT (A-4) (8)

Maximum Dry Density	107.1 PCF.	Optimum Moisture Content	17.9%
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AASHTO T99 - - Method A



**Soil Properties**

Natural Moisture Content	1.3%
Assumed Specific Gravity	2.650
Liquid Limit	39
Plastic Limit	29
Plastic Index	10

% Passing	
3/4"	100.0%
3/8"	100.0%
#4	100.0%
#10	99.0%
#40	97.0%
#60	96.0%
#200	78.3%

**Overflow Fraction**

Bulk Gravity	
% Moisture	
% Overflow MDD	
Opt. MC	

Moisture-Density Curve Displayed:	Fine Fraction <input checked="" type="checkbox"/>	Corrected for Oversize Fraction (ASTM D 4718)	<input type="checkbox"/>
Sieve Size used to separate the Oversize Fraction:	#4 Sieve <input checked="" type="checkbox"/>	3/8 inch Sieve	<input type="checkbox"/>
Mechanical Rammer	<input type="checkbox"/>	Manual Rammer	<input checked="" type="checkbox"/>
		Moist Preparation	<input type="checkbox"/>
		Dry Preparation	<input checked="" type="checkbox"/>

References / Comments / Deviations:

AASHTO T265: Laboratory Determination of Moisture Content of Soils

AASHTO T 99: Moisture-Density Relations of Soil Using a 5.5 Lb. Rammer and a 12" Drop

Mal Krajan, ET  
Technical Responsibility

Signature

Laboratory Manager  
Position

10/11/2019  
Date

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### CBR (CALIFORNIA BEARING RATIO) OF LABORATORY COMPACTED SOIL



AASHTO T 193

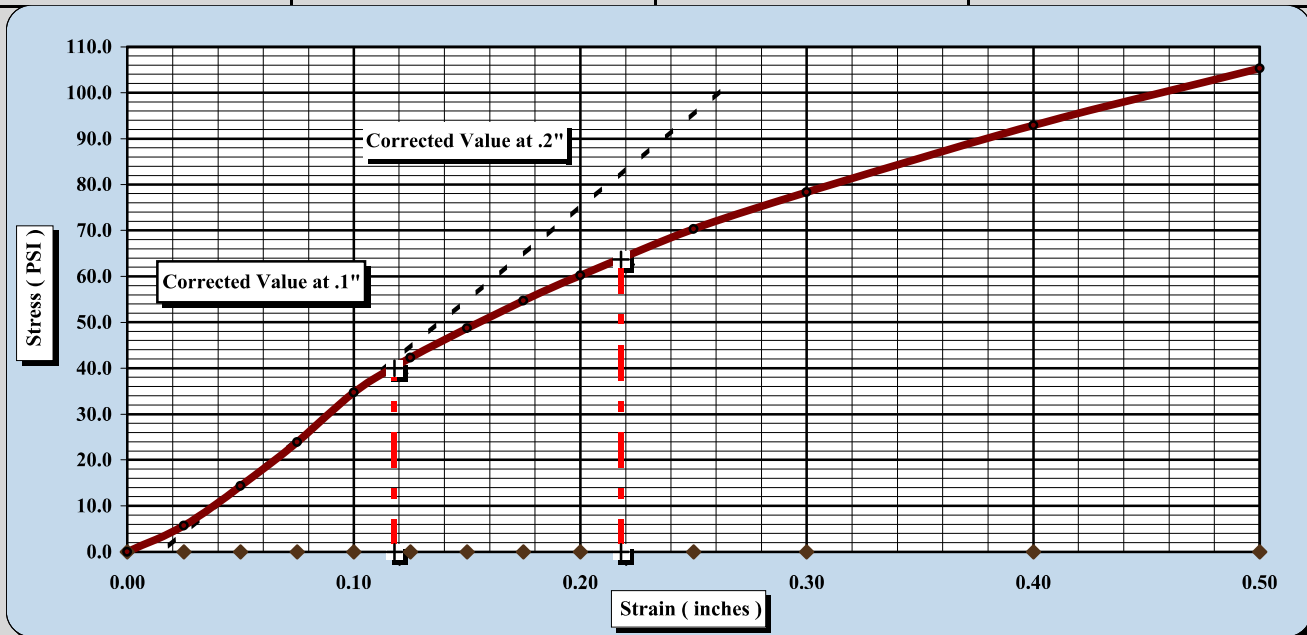
S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

Project #:	1934-19-002	Report Date:	10/16/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s)	10/10 - 10/16/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	L 172+00	Sample #:	S-1159
Station #:	172+00	Offset:	N/A
		Sample Date:	N/A
		Depth (ft):	0.0 - 8.5 ft.

Sample Description: Red Coarse to Fine Sandy Silty CLAY (A-7-5) (23)

AASHTO T99 Method A	Maximum Dry Density:	101.0 PCF	Optimum Moisture Content:	20.8%
	Compaction Test performed on grading complying with CBR spec.		% Retained on the 3/4" sieve:	0.0%

Uncorrected CBR Values		Corrected CBR Values	
CBR at 0.1 in.	3.5	CBR at 0.1 in.	4.0
CBR at 0.2 in.	4.0	CBR at 0.2 in.	4.2



CBR Sample Preparation: The entire gradation was used and compacted in a 6" CBR mold in accordance with AASHTO T 193, Section 5.1.1

Before Soaking		After Soaking	
Compactive Effort (Blows per Layer)	56	Final Dry Density (PCF)	99.4
Initial Dry Density (PCF)	100.8	Average Final Moisture Content	22.5%
Moisture Content of the Compacted Specimen	20.9%	Moisture Content (top 1" after soaking)	24.8%
Percent Compaction	99.8%	Percent Swell	1.6%

Soak Time:	96 hrs.	Surcharge Weight	10.0	Surcharge Wt. per sq. Ft.	50.9
Liquid Limit	64	Plastic Index	31		

Notes/Deviations/References:

Test specimen compacted to 100% at optimum moisture.

Mal Krajan, ET  
Technical Responsibility

*[Signature]*  
Signature

Laboratory Manager  
Position

10/16/2019  
Date

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### MOISTURE - DENSITY REPORT



SHEET 175

Quality Assurance

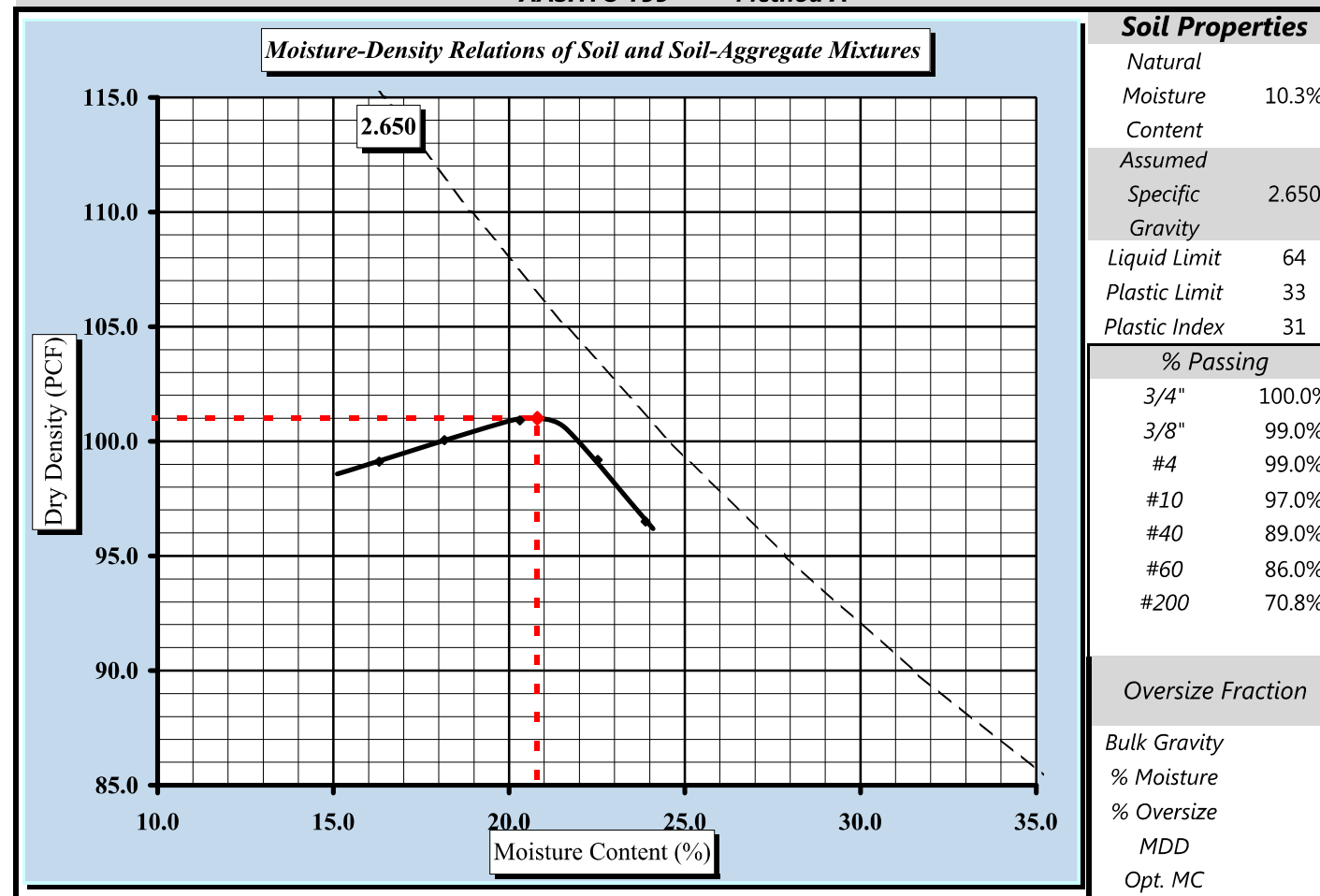
S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

S&ME Project #:	1943-19-002	Report Date:	10/11/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s):	10/4 - 10/11/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	L 172+00	Sample #:	S-1159
Station #:	172+00	Offset:	N/A
		Sample Date:	N/A
		Depth (ft):	0.0 - 8.5 ft.

Sample Description: Red Coarse to Fine Sandy Silty CLAY (A-7-5) (23)

Maximum Dry Density	101.0 PCF.	Optimum Moisture Content	20.8%
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AASHTO T99 - - Method A



Moisture-Density Curve Displayed: Fine Fraction  Corrected for Oversize Fraction (ASTM D 4718)   
 Sieve Size used to separate the Oversize Fraction: #4 Sieve  3/8 inch Sieve  3/4 inch Sieve   
 Mechanical Rammer  Manual Rammer  Moist Preparation  Dry Preparation

References / Comments / Deviations:

AASHTO T265: Laboratory Determination of Moisture Content of Soils

AASHTO T 99: Moisture-Density Relations of Soil Using a 5.5 Lb. Rammer and a 12" Drop

Mal Krajan, ET  
Technical Responsibility

*[Signature]*  
Signature

Laboratory Manager  
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