

**SEE SHEET 3 FOR PLAN SHEET LAYOUT
AT TIME OF INVESTIGATION**

**STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT**

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5861	1	175

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THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

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PERSONNEL

J. MIZE

M. METRY

S&ME PERSONNEL

INVESTIGATED BY **RK&K, LLP**

DRAWN BY **A. BOZORGI**

CHECKED BY **G. GOINS**

SUBMITTED BY **RK&K, LLP**

DATE **MARCH 2020**

**ROADWAY
SUBSURFACE INVESTIGATION**

COUNTY CHEROKEE
PROJECT DESCRIPTION WIDENING US 19/29 FROM
THE GEORGIA STATE LINE TO US 64/74

INVENTORY

CROSS SECTIONS

LINE	STATION	SHEETS
-DR5-	12+00	150
-DR6-	12+50	151
-DR7-	11+00 - 13+00	152 - 153
-DR8-	13+00	154
-DR9-	11+50	155
-DR10-	12+00	156
-DR11-	10+50 - 11+50	157
-DR12-	10+50	158
-DR13-	10+50	159
-DR14-	11+00	160
-DR15-	11+00	161
-DR16-	11+00	162
-DR17-	11+00 - 11+25	163
-DR18-	10+50	164
-DR19-	10+50	165
-DR20-	10+55 - 10+95	166
-DR21-	10+00 - 10+50	167 - 168
-DR22-	10+00 - 13+00	169 - 170

* These cross sections are subsets of -L- cross sections.

APPENDICES

APPENDIX	TITLE	SHEETS
A	BORING LOGS	172
B	LAB RESULTS	173 - 175

CONTENTS

LINE	STATION	PLAN
-L_DET1-	10+00 - 40+11	4 - 5
-L_DET2-	10+00 - 39+12	6 - 7
-L_DET3-	10+00 - 23+06	8
-L_DET4-	10+00 - 42+99	9 - 11
-L_DET6-	10+00 - 31+46	12 - 13
-DET_DR18-	10+00 - 11+45	9
-DET_DR18B-	10+00 - 11+40	9
-DET_DR19-	10+06 - 11+76	9
-DET_DR22-	10+40 - 13+37	12
-DET_Y1-	10+00 - 13+24	5
-L-	10+25 - 209+47	14 - 31
-Y1-	09+97 - 16+77	15
-Y2-	10+00 - 15+55	15
-Y3-	10+00 - 13+55	17
-Y3A-	10+00 - 12+40	17
-Y4-	12+72 - 14+95	19
-Y5-	10+00 - 11+40	19
-Y6-	11+30 - 17+24	21
-Y7-	10+00 - 13+10	21
-Y8-	10+50 - 12+77	23
-Y9-	10+00 - 13+50	23
-Y10A-	11+00 - 14+04	24
-Y10B-	11+50 - 19+51	25 & 31
-Y11-	11+00 - 14+43	25
-Y11A-	10+00 - 14+29	25 - 26
-Y12-	18+67 - 35+00	21 & 31
-Y13-	10+00 - 13+70	31
-DRI-	10+00 - 11+23	14
-DR2-	10+00 - 12+64	14
-DR5-	11+20 - 12+57	16
-DR6-	12+22 - 12+98	17
-DR7-	10+00 - 13+57	16 - 17
-DR8-	12+58 - 13+80	18
-DR9-	10+00 - 11+90	19
-DR10-	11+10 - 12+40	20
-DR11-	10+00 - 11+50	20
-DR12-	10+00 - 11+35	21
-DR13-	10+00 - 11+35	21
-DR14-	10+00 - 13+00	21 - 22
-DR15-	10+00 - 13+30	22
-DR16-	10+45 - 11+99	24
-DR17-	10+00 - 11+31	24
-DR18-	10+00 - 11+45	24
-DR18B-	10+00 - 11+85	24
-DR19-	10+00 - 11+75	24
-DR20-	10+55 - 11+10	25
-DR21-	10+00 - 11+25	24
-DR22-	10+00 - 13+37	27
-DR23-	10+00 - 12+09	26
-DR24-	10+00 - 11+32	28

CROSS SECTIONS

LINE	STATION	SHEETS
-L-	10+50 - 208+00	32 - 121
-L_DET1-	10+00 - 40+00	33 - 46
-L_DET2-	10+00 - 39+12	58 - 75
-L_DET3-	10+00 - 23+06	80 - 87
-L_DET4-	10+00 - 42+99	91 - 107
-L_DET6-	10+00 - 31+46	110 - 120
-Y1-	11+00 - 16+00	122 - 123
-Y2-	11+00 - 13+00	124
-Y3-	11+00 - 13+00	125 - 126
-Y3A-	11+50	127
-Y4-	13+50 - 15+00	128 - 129
-Y5-	11+00	130
-Y6-	10+50 - 16+00	131 - 133
-Y7-	11+00 - 13+00	134
-Y8-	10+50	135
-Y9-	11+00 - 13+50	136 - 137
-Y10A-	11+00 - 13+50	138 - 140
-Y10B-	12+00 - 17+50	141 - 142
-Y11-	11+00 - 13+00	143
-Y11A-	11+00 - 13+00	144 - 145
-Y12-	21+50 - 35+00	146 - 147
-DRI-	10+50 - 11+00	148
-DR2-	12+00	149

REFERENCE: R-5861

PROJECT: 47427

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DocuSigned by:
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-DR11-	10+50 - 11+50	157
-DR12-	10+50	158
-DR13-	10+50	159
-DR14-	11+00	160
-DR15-	11+00	161
-DR16-	11+00	162
-DR17-	11+00 - 11+25	163
-DR18-	10+50	164
-DR19-	10+50	165
-DR20-	10+55 - 10+95	166
-DR21-	10+00 - 10+50	167 - 168
-DR22-	10+00 - 13+00	169 - 170

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-L-DET6-	10+00 - 31+46	12 - 13
-DET-DR18-	10+00 - 11+45	9
-DET-DR18B-	10+00 - 11+40	9
-DET-DR19-	10+06 - 11+76	9
-DET-DR22-	10+40 - 13+37	12
-DET-Y1-	10+00 - 13+24	5
-L-	10+25 - 209+47	14 - 31
-Y1-	09+97 - 16+77	15
-Y2-	10+00 - 15+55	15
-Y3-	10+00 - 13+55	17
-Y3A-	10+00 - 12+40	17
-Y4-	12+72 - 14+95	19
-Y5-	10+00 - 11+40	19
-Y6-	11+30 - 17+24	21
-Y7-	10+00 - 13+10	21
-Y8-	10+50 - 12+77	23
-Y9-	10+00 - 13+50	23
-Y10A-	11+00 - 14+04	24
-Y10B-	11+50 - 19+51	25 & 31
-Y11-	11+00 - 14+43	25
-Y11A-	10+00 - 14+29	25 - 26
-Y12-	18+67 - 35+00	21 & 31
-Y13-	10+00 - 13+70	31
-DR1-	10+00 - 11+23	14
-DR2-	10+00 - 12+64	14
-DR5-	11+20 - 12+57	16
-DR6-	12+22 - 12+98	17
-DR7-	10+00 - 13+57	16 - 17
-DR8-	12+58 - 13+80	18
-DR9-	10+00 - 11+90	19
-DR10-	11+10 - 12+40	20
-DR11-	10+00 - 11+50	20
-DR12-	10+00 - 11+35	21
-DR13-	10+00 - 11+35	21
-DR14-	10+00 - 13+00	21 - 22
-DR15-	10+00 - 13+30	22
-DR16-	10+45 - 11+99	24
-DR17-	10+00 - 11+31	24
-DR18-	10+00 - 11+45	24
-DR18B-	10+00 - 11+85	24
-DR19-	10+00 - 11+75	24
-DR20-	10+55 - 11+10	25
-DR21-	10+00 - 11+25	24
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-DR23-	10+00 - 12+09	26
-DR24-	10+00 - 11+32	28

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-L-DET3-	10+00 - 23+06	80 - 87
-L-DET4-	10+00 - 42+99	91 - 107
-L-DET6-	10+00 - 31+46	110 - 120
-Y1-	11+00 - 16+00	121 - 123
-Y2-	11+00 - 13+00	124
-Y3-	11+00 - 13+00	125 - 126
-Y3A-	11+50	127
-Y4-	13+50 - 15+00	128 - 129
-Y5-	11+00	130
-Y6-	10+50 - 16+00	131 - 133
-Y7-	11+00 - 13+00	134
-Y8-	10+50	135
-Y9-	11+00 - 13+50	136 - 137
-Y10A-	11+00 - 13+50	138 - 140
-Y10B-	12+00 - 17+50	141 - 142
-Y11-	11+00 - 13+00	143
-Y11A-	11+00 - 13+00	144 - 145
-Y12-	21+50 - 35+00	146 - 147
-DR1-	10+50 - 11+00	148
-DR2-	12+00	149

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March 2, 2020

WBS Number: 47427.1.1

TIP Number: R-5861

County: Cherokee

Description: Widening US 19/129 from the Georgia State Line to US 64/74

Subject: Roadway Subsurface Inventory Report

PROJECT DESCRIPTION

The project begins at the North Carolina-Georgia state line and extends approximately 4.2 miles north to US 64 in Cherokee County, North Carolina. The project consists of realigning/widening and improvements of existing US 19/129.

Two Diedrich D-50 drill rigs with automatic hammers were used for the geotechnical investigation from July to September of 2019. During this time, a total of 168 Standard Penetration Tests (SPT) borings and 8 Auger probe borings were drilled. Representative soil samples were collected for visual classification and laboratory testing. Bulk samples were collected from select proposed excavation areas for laboratory testing.

The following alignments were investigated. Selected cross sections of these alignments are included in this report.

<u>Line</u>	<u>Stations (±)</u>
-LDET1-	10+00 – 40+00
-LDET2-	10+00 – 39+12
-LDET3-	10+00 – 23+06
-LDET4-	10+00 – 42+99
-LDET6-	10+00 – 31+46
-DET_DR18-	10+00 – 11+45
-DET_DR18B-	10+00 – 11+40
-DET_DR19-	10+00 – 11+76
-DET_DR22-	10+00 – 13+37
-DET_Y1-	10+00 – 13+14
-L-	10+25 – 209+47
-Y1-	09+97 - 16+77
-Y2-	10+00 - 15+55
-Y3-	10+00 - 13+55
-Y3A-	10+00 - 12+40
-Y4-	12+72 - 14+95
-Y5-	10+00 - 11+40
-Y6-	11+30 - 17+24
-Y7-	10+00 - 13+10
-Y8-	10+50 - 12+77

R-5861: Widening US 19/129 from the Georgia State Line to US 64/74

-Y9-	10+00 - 13+50
-Y10A-	11+00 - 14+04
-Y10B-	11+50 - 19+51
-Y11-	11+00 - 14+43
-Y11A-	10+00 - 14+29
-Y12-	18+67 - 35+00
-Y13-	10+00 - 13+70
-DR1-	10+00 - 11+23
-DR2-	10+00 - 12+64
-DR5-	11+20 - 12+57
-DR6-	12+22 - 12+98
-DR7-	10+00 - 13+57
-DR8-	12+58 - 13+80
-DR9-	10+00 - 11+90
-DR10-	11+10 - 12+40
-DR11-	10+00 - 11+50
-DR12-	10+00 - 11+35
-DR13-	10+00 - 11+35
-DR14-	10+00 - 13+00
-DR15-	10+00 - 13+30
-DR16-	10+45 - 11+99
-DR17-	10+00 - 11+31
-DR18-	10+00 - 11+45
-DR18B-	10+00 - 11+85
-DR19-	10+00 - 11+75
-DR20-	10+55 - 11+10
-DR21-	10+00 - 11+25
-DR22-	10+00 - 13+37
-DR23-	10+00 - 12+09
-DR24-	10+00 - 11+32

PHYSIOGRAPHY AND GEOLOGY

The proposed project is located within the Blue Ridge Physiographic Province, along the existing US 19/129 corridor from the Georgia state line to the intersection with US-64/US-74, and passes through a populated rural area. Terrain within the proposed project corridor consists of large hills to mountains separated by mountain streams. The proposed project passes along and between steeply sloping hillsides.

The bedrock underlying the proposed project consists of members of the Ocoee Supergroup and Murphy Belt (Geologic Map of North Carolina, 1985). These rocks include schist, phyllite, slate, quartzite, and assorted slightly metamorphosed sedimentary rocks (metagraywacke, metasilstone, metasandstone, and metaconglomerate), several of which were encountered and identified during the investigation. Some existing cut slopes within the project have exposed underlying bedrock. The overlying residual soils are a result of physical and chemical weathering of the underlying bedrock.



SOIL PROPERTIES

Soils encountered during the geotechnical investigation are separated into four (4) categories based on soil origin. The origins consist of roadway embankment, artificial fill, alluvial soils, and residual soils.

Roadway Embankment: Materials interpreted as roadway embankment were encountered within the limits of the existing US 19/129 alignment. The roadway embankment generally consisted of loose to dense, sandy GRAVEL (A-1-b) and silty to clayey SAND (A-2-4, A-2-5, A-2-6, A-2-7) and medium stiff to very stiff, sandy to clayey SILT (A-4 and A-5) to sandy silty CLAY (A-6). The thickness of the encountered roadway embankment varied up to 11.5 feet.

Artificial Fill: Artificial fill was found in the proposed project area where land had been graded for construction of businesses and in the parking lots. The fill consists of stiff sandy CLAY (A-6). The thickness of the encountered artificial fill varied up to 2.0 feet.

Alluvial Soils: Alluvial soils were typically associated with drainage features or areas where creeks previously crossed or are adjacent to the proposed alignment. Alluvial soils generally consisted very soft to stiff sandy SILT (A-4) and sandy silty CLAY (A-6, A-7-5, and A-7-6), and very loose silty clayey SAND (A-2-5). The thickness of the encountered alluvial soils varied up to 12.0 feet.

Residual Soils: Soils classified as residual soils generally consisted of very loose to very dense, clayey and silty fine to coarse SAND (A-1-b, A-2-4, A-2-5, A-2-6, A-2-7.) and very soft to hard, sandy SILT (A-4, A-5) and slightly to highly plastic silty CLAY (A-6, A-7-5, A-7-6). Varying amounts of mica and rock fragments were noted within soils interpreted as residual soils.

ROCK PROPERTIES

Weathered Rock: Weathered rock was encountered in sixty-eight (68) borings. Weathered rock was encountered at the following locations above or within six (6) feet of proposed grade:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	19+50 – 21+25	LT
-L-	42+00 – 43+50	LT & RT
-L-	44+50 – 49+00	LT & RT
-L-	53+50 – 55+50	LT & RT
-L-	78+50 – 81+50	LT & RT
-L-	85+50 – 95+00	LT & RT
-L-	103+00 – 107+00	LT & RT
-L-	113+00 – 119+00	LT & RT
-L-	121+00 – 123+50	LT & RT
-L-	149+00 – 152+00	LT & RT
-L-	159+50 – 178+50	LT & RT
-L-	185+00 – 190+00	LT & RT
-L_DET2-	18+75 – 24+75	LT & RT
-L_DET3-	10+00 – 12+00	LT & RT
-L_DET4-	19+00 – 22+20	LT & RT
-L_DET4-	31+25 – 32+50	LT & RT

-L_DET4-	35+00 – 39+50	LT & RT
-L_DET6-	14+00 – 22+25	LT & RT
-L_DET6-	23+25 – 26+00	LT & RT
-Y6-	15+00 – 16+75	LT & RT
-Y10B-	13+00 – 15+00	LT & RT
-Y10B-	17+00 – 19+00	LT & RT
-DR9-	10+50 – 12+50	LT & RT
-DR14-	10+00 – 12+00	LT & RT
-DR15-	10+75 – 11+75	LT & RT
-DR22-	10+25 – 11+25	LT & RT
-DR23-	10+75 – 11+25	LT & RT

Crystalline Rock: Crystalline rock is defined as auger refusal or SPT refusal with penetration by split spoon of less than or equal to 0.1 feet per 60 blows. Crystalline rock was encountered in twenty-three (23) borings. Crystalline rock was encountered at the following locations above or within six (6) feet of proposed grade:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	18+25 – 19+50	LT
-L-	43+50 – 45+50	LT & RT
-L-	88+25 – 89+25	LT
-L-	90+25 – 92+75	LT
-L-	117+00 – 118+75	RT
-L-	165+50 – 167+50	LT & RT
-L_DET2-	18+40 – 19+40	LT & RT
-L_DET2-	20+50 – 23+00	LT & RT
-L_DET4-	19+20 – 20+75	LT & RT
-L_DET4-	35+00 – 36+90	LT & RT

GROUNDWATER

Groundwater was encountered during drilling operations (0-hr reading) within thirty-one (31) borings at elevations ranging from 1613.8 to 1759.6. Static (24-hr reading) measurements were recorded within forty-three (43) borings at elevations ranging from 1624.0 to 1766.2.

Ponds: Five (5) ponds are located within or in close proximity of right of way on this project. They are noted at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	82+24 – 86+61	RT
-L-	99+98 – 102+30	RT
-L-	102+81 – 105+11	RT
-Y9-	12+00 – 13+17	RT
-DR9-	10+04 – 10+79	LT

Water wells: Two water wells are located within right of way on this project. They are noted at the following locations:



-DR21- 10+00 – 10+95 LT & RT

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	107+43	LT
-L-	158+74	LT
-Y6-	12+64	LT
-Y10B-	17+32	LT

Groundwater: Groundwater was encountered at the following locations above or within six (6) feet of the proposed grade:

AREAS OF SPECIAL GEOTECHNICAL INTEREST

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	17+75 – 18+75	LT & RT
-L-	23+50 – 29+50	LT & RT
-L-	43+50 – 45+50	LT & RT
-L-	73+50 – 75+50	LT & RT
-L-	88+25 – 88+75	LT & RT
-L-	105+00 – 111+00	LT & RT
-L-	149+25 – 151+00	LT & RT
-L-	163+00 – 165+00	LT & RT
-L_DET2-	18+40 – 18+90	LT & RT
-L_DET4-	18+70 – 20+80	LT & RT
-Y1-	15+00 – 16+77	LT & RT
-Y2-	10+00 – 11+50	LT & RT
-Y6-	15+00 – 17+24	LT & RT
-Y9-	13+20 – 13+50	LT & RT
-Y10B-	16+30 – 19+51	LT & RT

Alluvial Soils: Alluvial soils were encountered along the proposed alignments at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	33+00 – 34+46	LT
-L-	35+96 – 37+19	LT
-L-	56+00 – 58+80	RT
-L-	71+21 – 73+64	LT & RT
-L-	83+90 – 86+26	LT & RT
-L-	126+57 – 128+25	LT & RT
-L_DET3-	14+40 – 16+55	LT & RT

Artificial Fill: Artificial fill was encountered along the proposed alignments at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-DR7-	10+64 – 11+55	LT & RT
-L-	108+19 – 110+30	LT

Soft, Loose and/or Wet Soils: Relatively soft or loose and/or wet soils were encountered along the proposed alignments at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L_DET3-	14+43 – 15+13	RT
-L_DET3-	15+75 – 16+55	RT
-L-	126+90 – 128+25	LT
-Y9-	12+60 – 13+20	RT

Highly Plastic Soils: Highly plastic soils with plasticity indices (PI) greater than 25 and within proposed cut sections or PI greater than 35 and/or high liquid limit within 3-ft of subgrade were encountered at the following locations:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	21+75 – 26+75	LT & RT
-L-	137+25 – 139+25	LT
-L-	158+75 – 160+75	LT & RT
-L-	170+75 – 172+75	LT & RT
-L-	190+75 – 192+25	LT & RT
-DR17-	10+20 – 11+40	LT & RT

The following areas contain groundwater above or within three (3) feet of the existing grade:

<u>Line</u>	<u>Stations (±)</u>	<u>Offset</u>
-L-	17+75 – 18+75	LT & RT
-L-	23+50 – 29+50	LT & RT
-L-	43+50 – 45+50	LT & RT
-L-	107+00 – 111+00	LT & RT
-L-	149+25 – 151+00	LT & RT
-L-	163+00 – 165+00	LT & RT
-L_DET4-	18+70 – 20+80	LT & RT
-Y1-	15+00 – 16+77	LT & RT
-Y2-	10+00 – 11+50	LT & RT
-Y6-	15+00 – 17+24	LT & RT
-Y10B-	16+30 – 19+51	LT & RT



Prepared by,



DocuSigned by:
Arash Bozorgi 3/3/2020
1D9ECF51F010436...

Arash Bozorgi, PhD, PE
Associate Engineer, Geotechnical
Registered, North Carolina 048490

DocuSigned by:
Greg Goins 3/3/2020
4725B2704A9E4D7...

Gregory Goins, PE
Project Manager, Geotechnical
Registered, North Carolina 041709

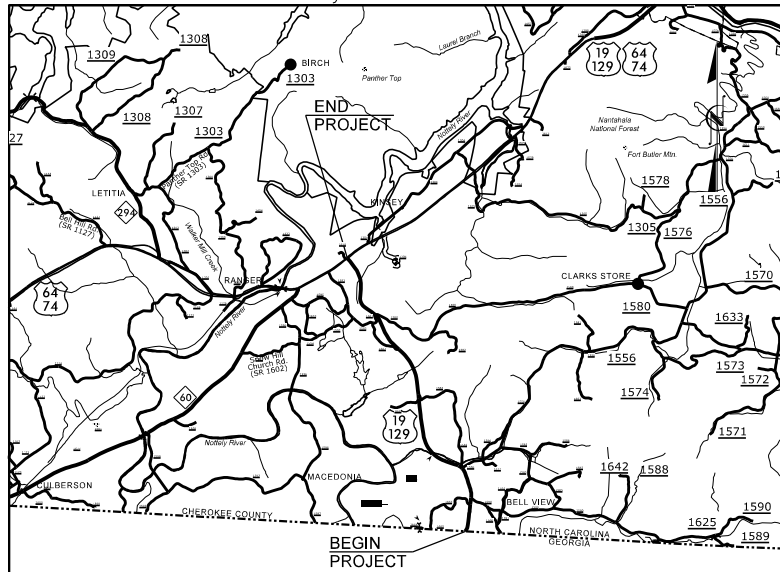
Appendix A

Bulk Samples

The following bulk samples were collected from cut sections for laboratory testing:

Sample No.	Line	Station	Offset	Depth (ft)	Test(s) Performed
S-225	-L-	90+00	90' LT	1.0 – 8.5	Standard Proctor, California Bearing Ratio
S-1159	-L-	172+00	0	2.0 – 8.0	Standard Proctor, California Bearing Ratio
S-1041	-L_DET6-	191+99	20' RT	0.0 – 8.5	Standard Proctor, California Bearing Ratio

See Sheet 1-A For Index of Sheets
See Sheet 1-B For Conventional Symbols



VICINITY MAP (NTS)

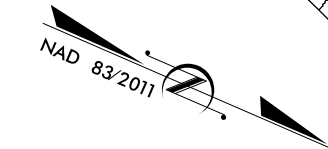
STATE OF NORTH CAROLINA
DIVISION OF HIGHWAYS

CHEROKEE COUNTY

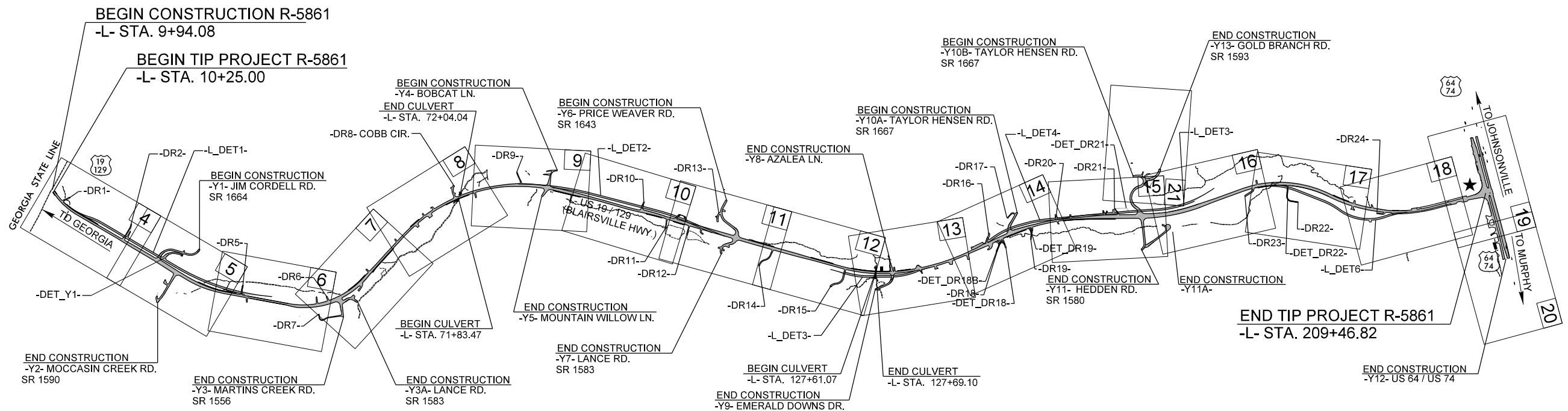
LOCATION: WIDENING US 19 /129 FROM THE GEORGIA STATE LINE TO US 64 /74.

TYPE OF WORK: GRADING, PAVING, WIDENING, DRAINAGE, CULVERTS, SIGNING, SIGNALS, & UTILITIES

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5861	3	
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
47427.1.1	NHP - 0019 (058)	PE	
47427.2.1	NHP - 0019 (058)	UTILITIES & RW	



TIP PROJECT: R-5861



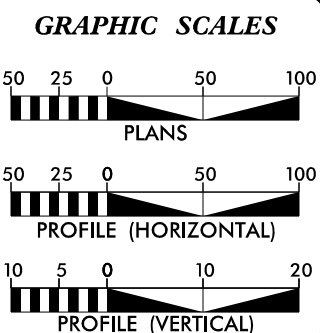
NOTES:

1. THIS PROJECT IS NOT WITHIN A MUNICIPAL BOUNDARY.
2. CLEARING ON THIS PROJECT SHALL BE PERFORMED TO THE LIMITS ESTABLISHED BY METHOD III (EXCEPT IN PARALLEL STREAM LOCATIONS CLEAR ONLY TO THE SLOPE STAKE LINE.)
3. DESIGN EXCEPTION FOR MINIMUM HORIZONTAL CURVE RADIUS, SAG VERTICAL CURVE, AND VERTICAL STOPPING SIGHT DISTANCE.

★ UPGRADE TRAFFIC SIGNAL

INCOMPLETE PLANS
DO NOT USE FOR R/W ACQUISITION
DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED

CONTRACT:



DESIGN DATA

ADT 2020 = 9,000
ADT 2050 = 11,122
V = 60 MPH
DHV = 8%
D = 55%
T = 4% *
(* TTST = 2% /* DUAL = 2%)
FUNC CLASS = RURAL ARTERIAL
STATEWIDE TIER
DESIGN EXCEPTIONS AS NOTED ON PLANS

PROJECT LENGTH

LENGTH ROADWAY TIP PROJECT R-5861.....	3.767 miles
LENGTH STRUCTURE TIP PROJECT R-5861.....	0.000 miles
TOTAL LENGTH OF PROJECT R-5861.....	3.767 miles

PLANS PREPARED BY:

RK&K
900 RIDGEFIELD DRIVE, SUITE 350
RALEIGH, NORTH CAROLINA 27609
NC LICENSE NO. F-0112
1-888-521-4455 OR 919-878-9560

FOR NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
2018 STANDARD SPECIFICATIONS

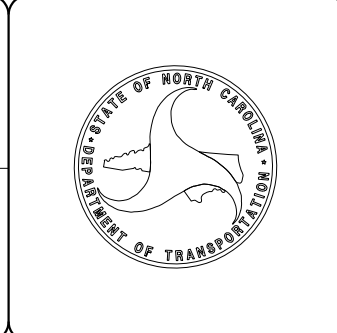
RIGHT OF WAY DATE:	Brandon McInnis, P.E. PROJECT ENGINEER
LETTING DATE:	Jillian Hinson, E.I. PROJECT DESIGN ENGINEER
NCDOT CONTACT:	Kenneth J. McDowell DIVISION 14

HYDRAULICS ENGINEER

SIGNATURE: _____ P.E.

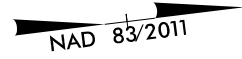
ROADWAY DESIGN ENGINEER

SIGNATURE: _____ P.E.



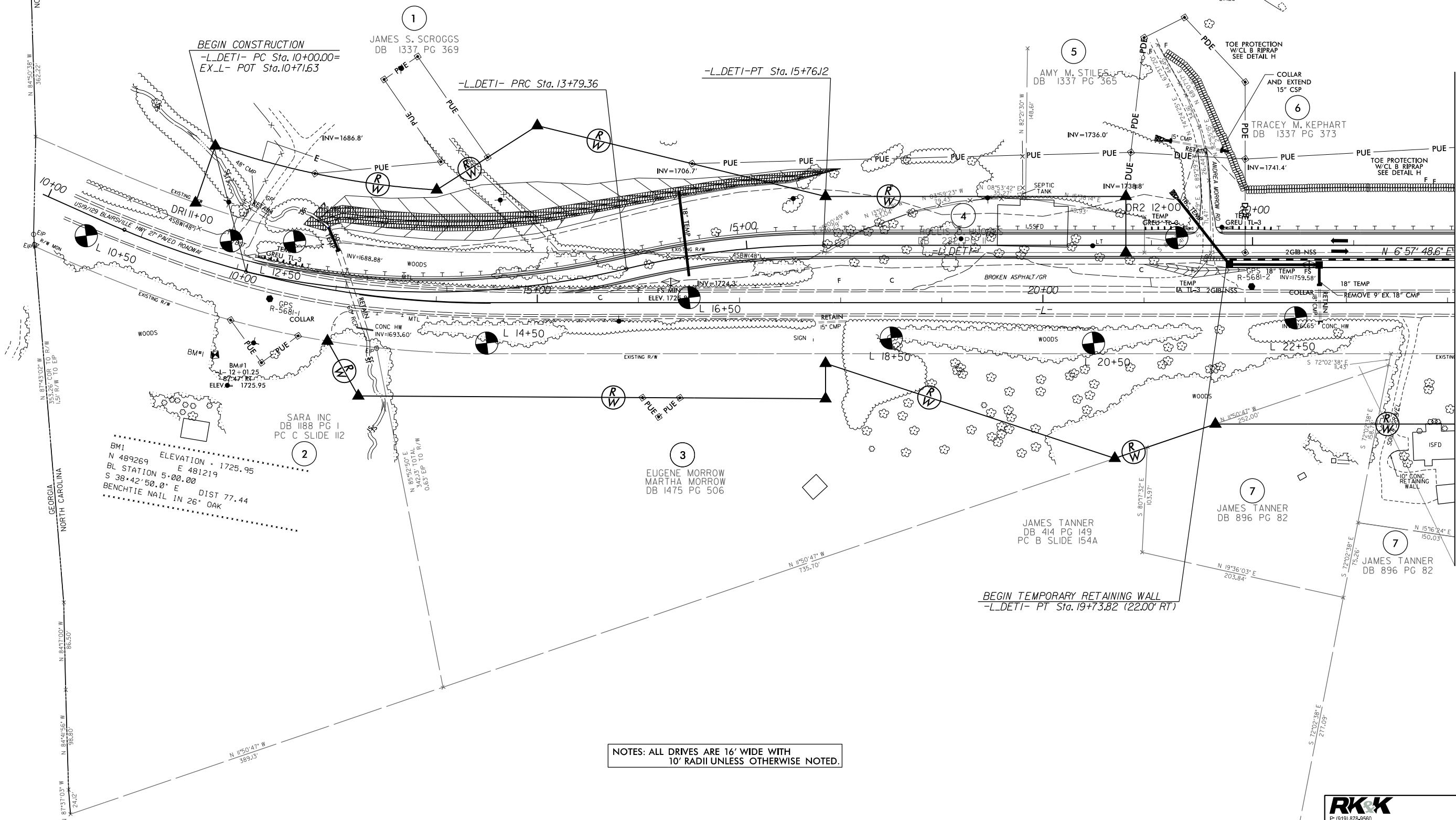
-L_DET1-

PROJECT REFERENCE NO. <i>R-586I</i>	SHEET NO. 4
R/W SHEET NO. 2B-1	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



-L_DET1-

PI Sta 11+93.13	PI Sta 14+78.25
$\Delta = 26^{\circ} 02' 45.8" (LT)$	$\Delta = 13^{\circ} 30' 33.5" (RT)$
$D = 6^{\circ} 51' 57.2"$	$D = 6^{\circ} 51' 57.2"$
$L = 379.36'$	$L = 196.76'$
$T = 193.13'$	$T = 98.90'$
$R = 835.00'$	$R = 835.00'$
$SE=0.06$	$SE=0.06$
$RO = 140$	$RO = 140$
$DS = 50 \text{ MPH}$	$DS = 50 \text{ MPH}$



BM1 ELEVATION = 1725.95
 N 489269 E 481219
 BL STATION 5+00.00
 S 38°42'50.0" E DIST 77.44
 BENCHTIE NAIL IN 26" OAK

NOTES: ALL DRIVES ARE 16' WIDE WITH
 10' RADII UNLESS OTHERWISE NOTED.

BEGIN TEMPORARY RETAINING WALL
 -L_DET1- PT Sta. 19+73.82 (22.00' RT)

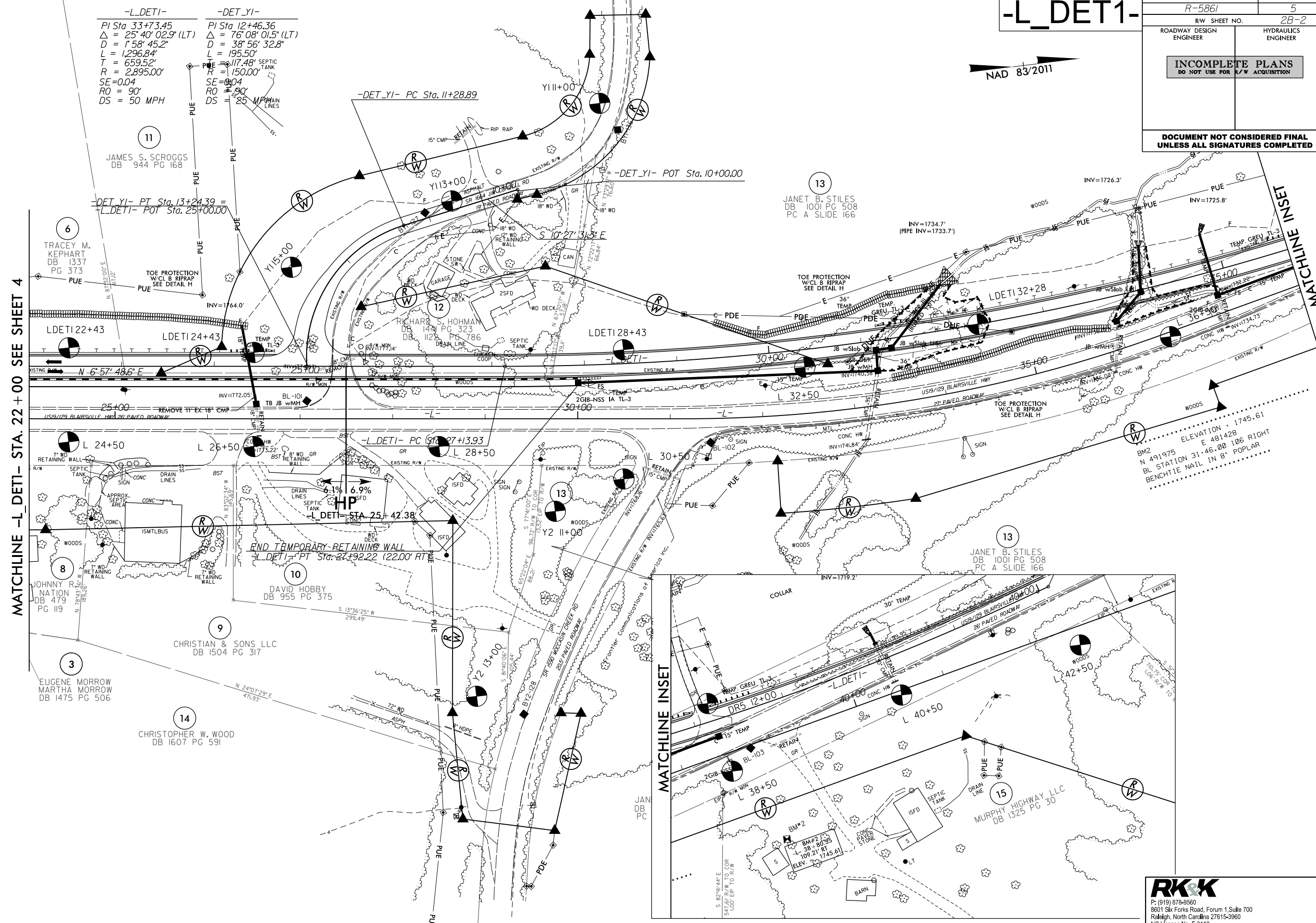
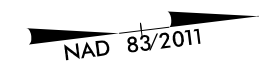
MATCHLINE -L_DET1- STA. 22+00 SEE SHEET 5

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-L_DET1-

PROJECT REFERENCE NO. R-5861	SHEET NO. 5
R/W SHEET NO. 2B-2	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



MATCHLINE -L_DET1- STA. 22+00 SEE SHEET 4

MATCHLINE INSET

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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-L_DET2-

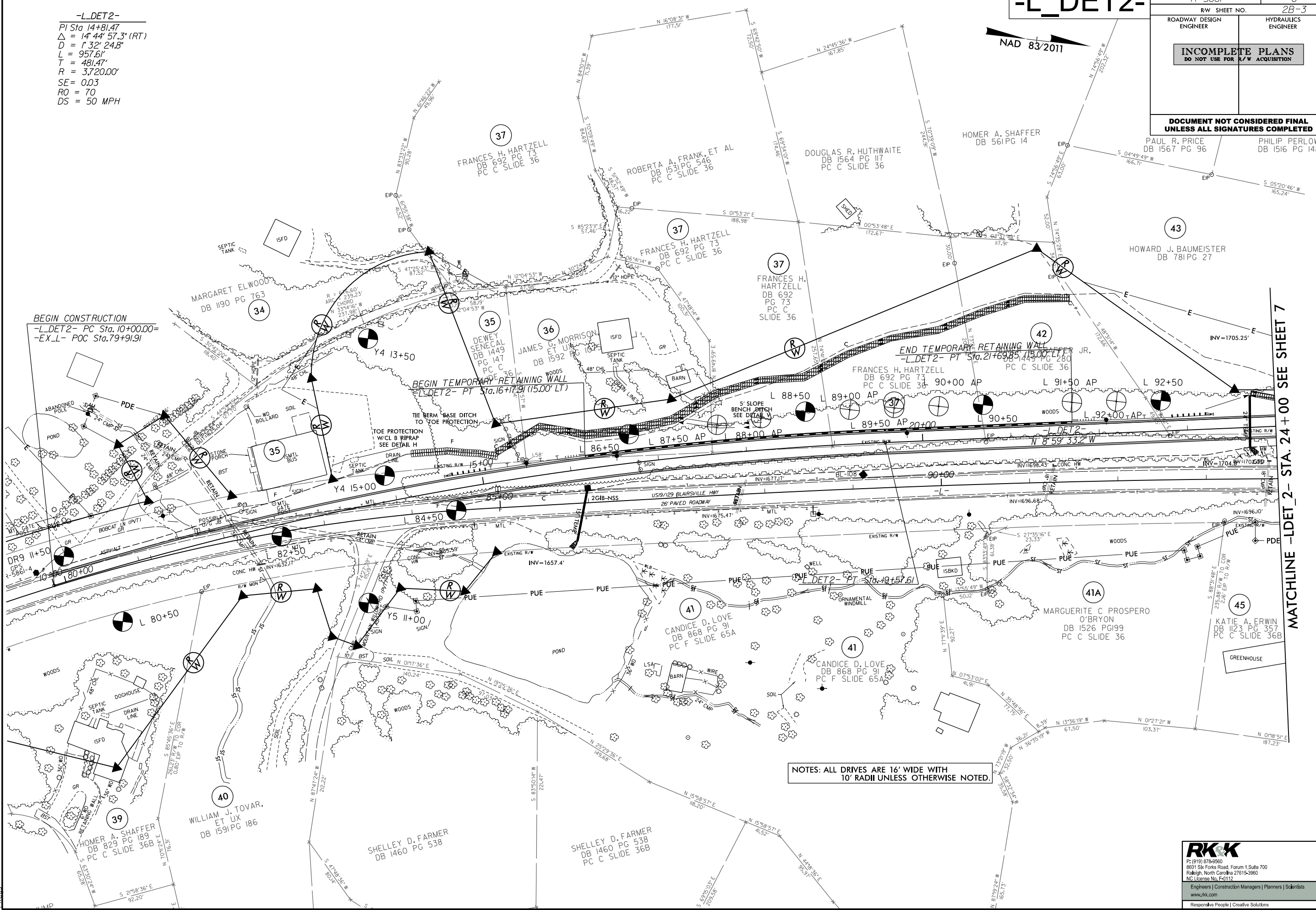
PI Sta 14+81.47
Δ = 14° 44' 57.3" (RT)
D = 1' 32' 24.8"
L = 957.61'
T = 481.47'
R = 3,720.00'
SE = 0.03
RO = 70
DS = 50 MPH

-L_DET2-

NAD 83/2011

PROJECT REFERENCE NO. R-5861	SHEET NO. 6
R/W SHEET NO. 2B-3	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	
PAUL R. PRICE DB 1567 PG 96	PHILIP PERLOW DB 1516 PG 148

BEGIN CONSTRUCTION
-L_DET2- PC Sta. 10+00.00=
-EX_L- POC Sta. 79+91.91



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

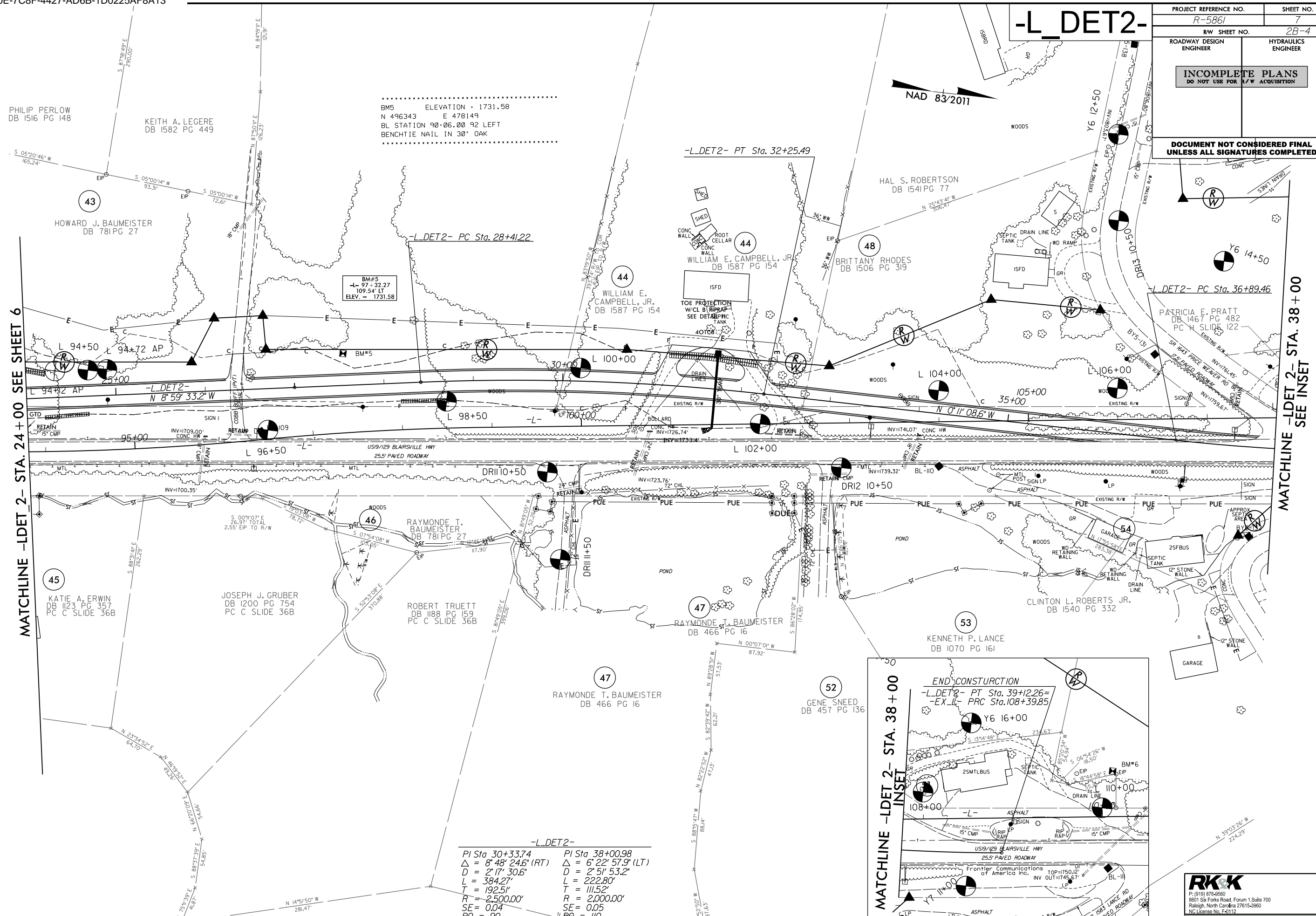
MATCHLINE -LDET2- STA. 24+00 SEE SHEET 7

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-L_DET2-

PROJECT REFERENCE NO. R-5861		SHEET NO. 7	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
RW SHEET NO. 2B-4			
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			



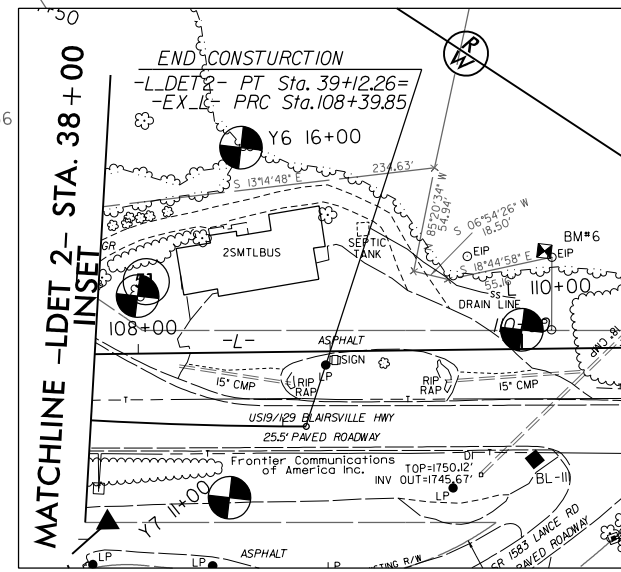
MATCHLINE -LDET 2- STA. 24+00 SEE SHEET 6

MATCHLINE -LDET 2- STA. 38+00 SEE INSET

BM5 ELEVATION = 1731.58
 N 496343 E 478149
 BL STATION 90+06.00 92 LEFT
 BENCHTIE NAIL IN 30' OAK

BM#5
 -L- 97+32.27
 109.54' LT
 ELEV. = 1731.58

-L_DET2-	
PI Sta 30+33.74	PI Sta 38+00.98
$\Delta = 8' 48' 24.6''$ (RT)	$\Delta = 6' 22' 57.9''$ (LT)
D = 2' 17' 30.6"	D = 2' 51' 53.2"
L = 384.27'	L = 222.80'
T = 192.51'	T = 111.52'
R = 2,500.00'	R = 2,000.00'
SE = 0.04	SE = 0.05
RO = 90	RO = 110
DS = 50 MPH	DS = 50 MPH



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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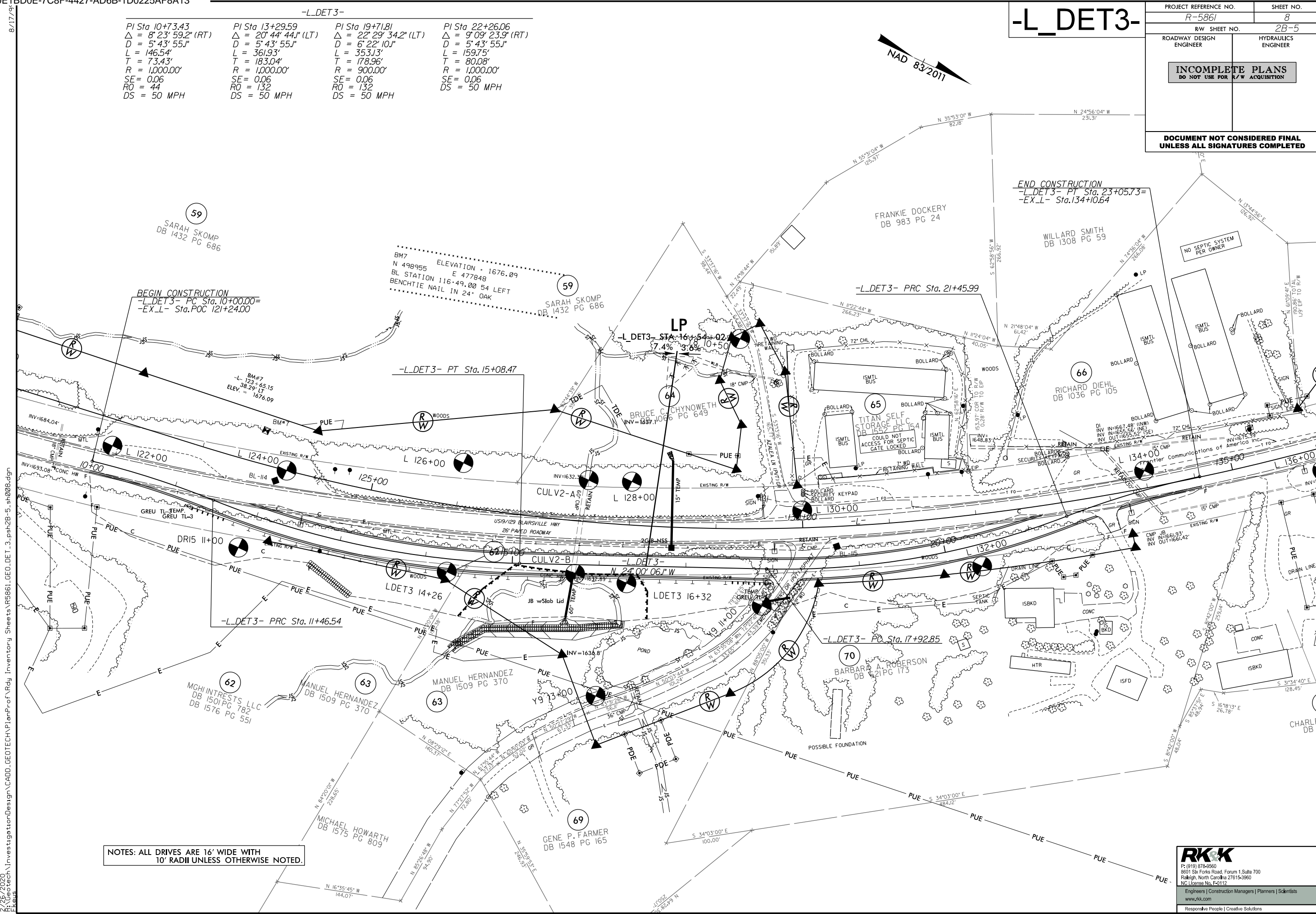
CADD_GEO...Rdy_Inventory_Sheets\RS5861_CEO_DET_2_psh2B-4_sh007.dgn

-L_DET3-

PI Sta 10+73.43 Δ = 8° 23' 59.2" (RT) D = 5' 43' 55.1" L = 146.54' T = 73.43' R = 1,000.00' SE = 0.06 RO = 44 DS = 50 MPH	PI Sta 13+29.59 Δ = 20° 44' 44.1" (LT) D = 5' 43' 55.1" L = 361.93' T = 183.04' R = 1,000.00' SE = 0.06 RO = 132 DS = 50 MPH	PI Sta 19+71.81 Δ = 22° 29' 34.2" (LT) D = 6' 22' 10.1" L = 353.13' T = 178.96' R = 900.00' SE = 0.06 RO = 132 DS = 50 MPH	PI Sta 22+26.06 Δ = 9° 09' 23.9" (RT) D = 5' 43' 55.1" L = 159.75' T = 80.08' R = 1,000.00' SE = 0.06 RO = 132 DS = 50 MPH
---	--	--	--

-L_DET3-

PROJECT REFERENCE NO. R-5861	SHEET NO. 8
R/W SHEET NO. 2B-5	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

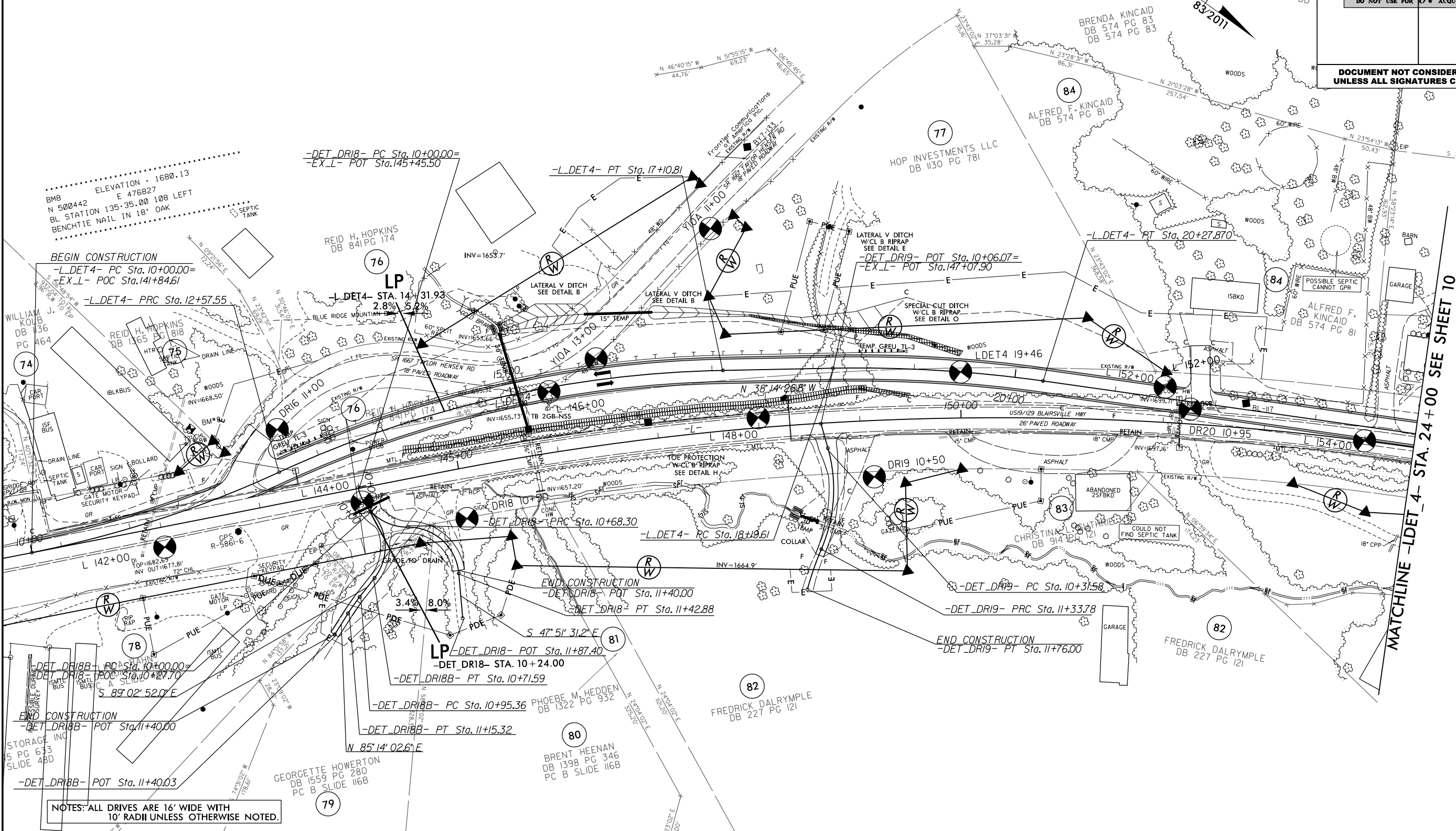
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-L_DET4-

PROJECT REFERENCE NO. R-5861	SHEET NO. 9
R/W SHEET NO. 2B-6	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

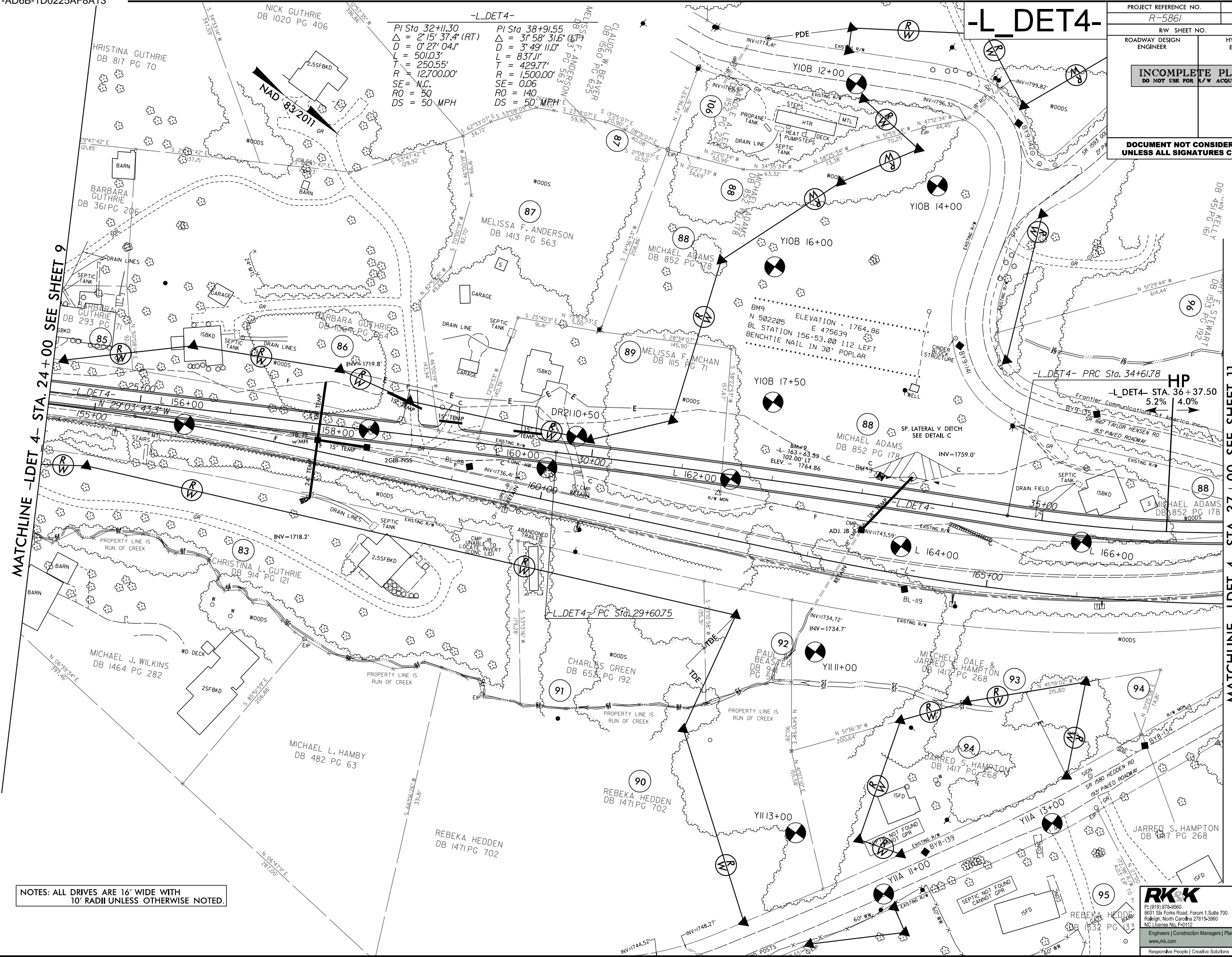
-L_DET4-		-DET_DR18-		-DET_DR18B-		-DET_DR19-	
PI Sta 11+29.41	PI Sta 14+87.52	PI Sta 10+23.97	PI Sta 10+40.68	PI Sta 11+4.49	PI Sta 10+43.49	PI Sta 10+84.76	PI Sta 11+54.93
$\Delta = 13^\circ 25' 10.6''$ (LT)	$\Delta = 23^\circ 37' 01.0''$ (RT)	$\Delta = 9^\circ 10' 43.4''$ (RT)	$\Delta = 78^\circ 15' 52.3''$ (LT)	$\Delta = 85^\circ 28' 02.8''$ (RT)	$\Delta = 82^\circ 02' 03.8''$ (RT)	$\Delta = 39^\circ 02' 18.7''$ (RT)	$\Delta = 8^\circ 03' 46.2''$ (LT)
D = 5' 12' 37.8"	D = 5' 12' 37.8"	D = 4' 24' 26.5"	D = 114' 35' 29.6"	D = 114' 35' 29.6"	D = 114' 35' 29.6"	D = 38' 11' 49.9"	D = 19' 05' 54.9"
L = 257.55'	L = 453.26'	L = 208.26'	L = 68.30'	L = 74.58'	L = 71.59'	L = 102.20'	L = 42.22'
T = 129.48'	T = 229.97'	T = 104.35'	T = 40.68'	T = 46.19'	T = 43.49'	T = 53.17'	T = 21.14'
R = 100.00'	R = 1,100.00'	R = 1,300.00'	R = 50.00'	R = 50.00'	R = 50.00'	R = 150.00'	R = 300.00'
	SE = 0.06	SE = 0.06					
	RO = 140	RO = 140					
	DS = 50 MPH	DS = 50 MPH					

MATCHLINE -LDET_4- STA. 24+00 SEE SHEET 10

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2/26/2020
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-L_DET4-

PROJECT REFERENCE NO. R-5861	SHEET NO. 10
R/W SHEET NO. 2B-7	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	

DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED

-L_DET4-

PI Sta 32+11.30	PI Sta 38+91.55
$\Delta = 2' 15' 37.4'' (RT)$	$\Delta = 3' 58' 31.6''$
$D = 0' 27' 04.1''$	$D = 3' 49' 11.0''$
$L = 501.03'$	$L = 837.11'$
$T = 250.55'$	$T = 429.77'$
$R = 12,700.00'$	$R = 1,500.00'$
SE = N.C.	SE = 0.06
RO = 50	RO = 140
DS = 50 MPH	DS = 50 MPH

MATCHLINE -LDET 4- STA. 24+00 SEE SHEET 9

MATCHLINE -LDET 4- STA. 37+00 SEE SHEET 11

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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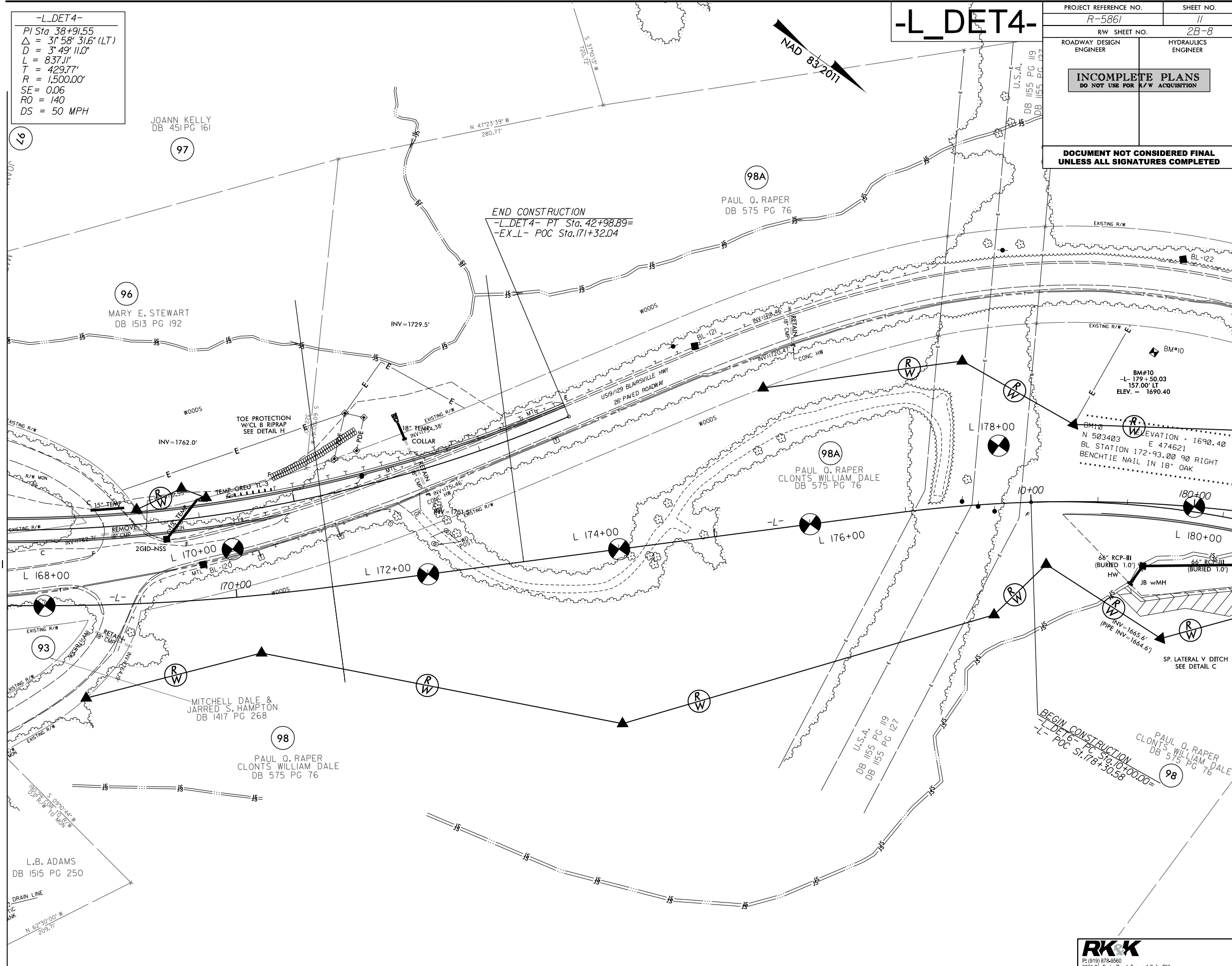
-L_DET4-
 PI Sta 38+91.55
 $\Delta = 31^{\circ} 58' 31.6" (LT)$
 $D = 3^{\circ} 49' 11.0"$
 $L = 837.11'$
 $T = 429.77'$
 $R = 1500.00'$
 $SE = 0.06$
 $RO = 140$
 $DS = 50 MPH$

-L_DET4-

PROJECT REFERENCE NO. R-5861	SHEET NO. 11
R/W SHEET NO. 2B-8	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	

DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED

MATCHLINE -LDET 4- STA. 37+00 SEE SHEET 10



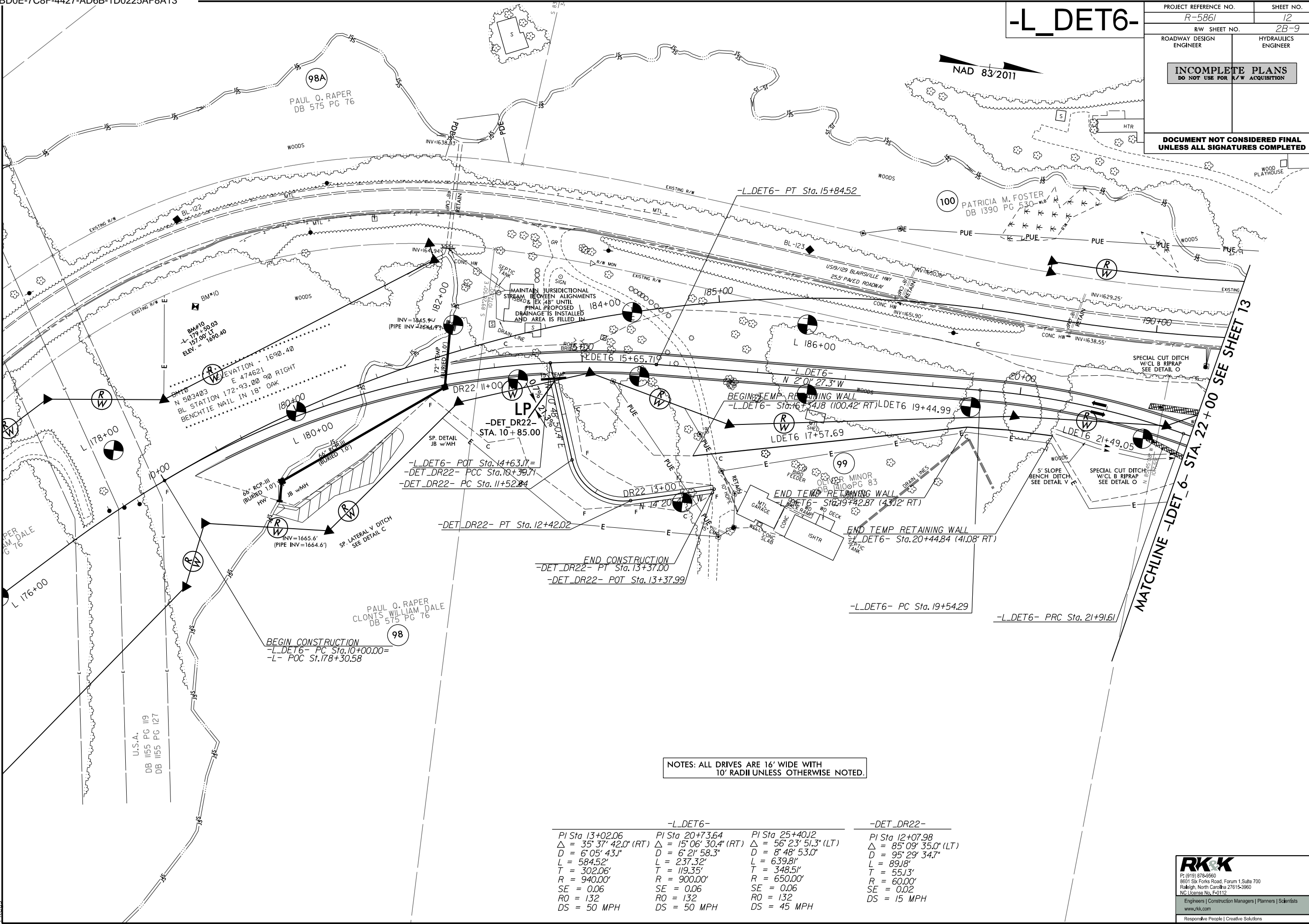
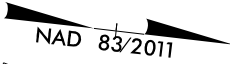
NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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-L_DET6-

PROJECT REFERENCE NO. <i>R-586I</i>	SHEET NO. <i>12</i>
R/W SHEET NO. <i>2B-9</i>	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

-L_DET6-			-DET_DR22-		
PI Sta 13+02.06	PI Sta 20+73.64	PI Sta 25+40.12	PI Sta 12+07.98		
$\Delta = 35^\circ 37' 42.0''$ (RT)	$\Delta = 15^\circ 06' 30.4''$ (RT)	$\Delta = 56^\circ 23' 51.3''$ (LT)	$\Delta = 85^\circ 09' 35.0''$ (LT)		
D = 6' 05' 43.1"	D = 6' 21' 58.3"	D = 8' 48' 53.0"	D = 95' 29' 34.7"		
L = 584.52'	L = 237.32'	L = 639.81'	L = 89.18'		
T = 302.06'	T = 119.35'	T = 348.51'	T = 55.13'		
R = 940.00'	R = 900.00'	R = 650.00'	R = 60.00'		
SE = 0.06	SE = 0.06	SE = 0.06	SE = 0.02		
RO = 132	RO = 132	RO = 132	DS = 15 MPH		
DS = 50 MPH	DS = 50 MPH	DS = 45 MPH			



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 PER M. DALE G 76
 U.S.A. DB 1155 PG 119 DB 1155 PG 127
 PAUL O. RAPER CLONTS WILLIAM DALE DB 575 PG 76
 MATCHLINE -LDET_6- STA. 22+00 SEE SHEET 13

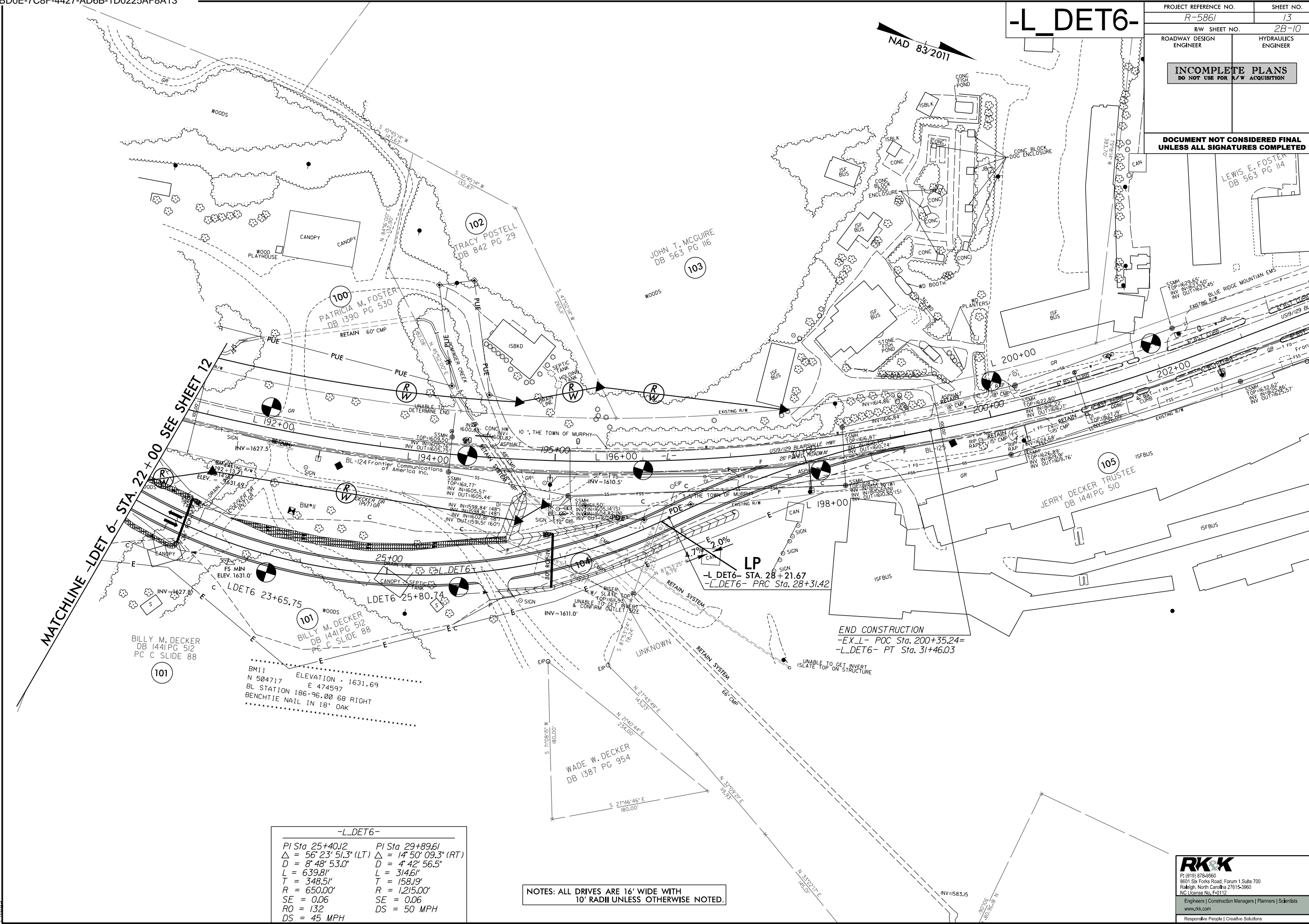
8/17/09

-L_DET6-

PROJECT REFERENCE NO. <i>R-5861</i>	SHEET NO. <i>13</i>
R/W SHEET NO. <i>2B-10</i>	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	

**DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED**

LEWIS E. FOSTER
DB 563 PG 14



MATCHLINE -LDET 6- STA. 22+00 SEE SHEET 12

-L_DET6-	
PI Sta 25+40.12	PI Sta 29+89.61
$\Delta = 56^{\circ} 23' 51.3" (LT)$	$\Delta = 14^{\circ} 50' 09.3" (RT)$
$D = 8^{\circ} 48' 53.0"$	$D = 4^{\circ} 42' 56.5"$
$L = 639.81'$	$L = 314.61'$
$T = 348.51'$	$T = 158.19'$
$R = 650.00'$	$R = 1,215.00'$
$SE = 0.06$	$SE = 0.06$
$RO = 132$	$DS = 50 MPH$
$DS = 45 MPH$	

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

END CONSTRUCTION
-EX_L- POC Sta. 200+35.24=
-L_DET6- PT Sta. 31+46.03

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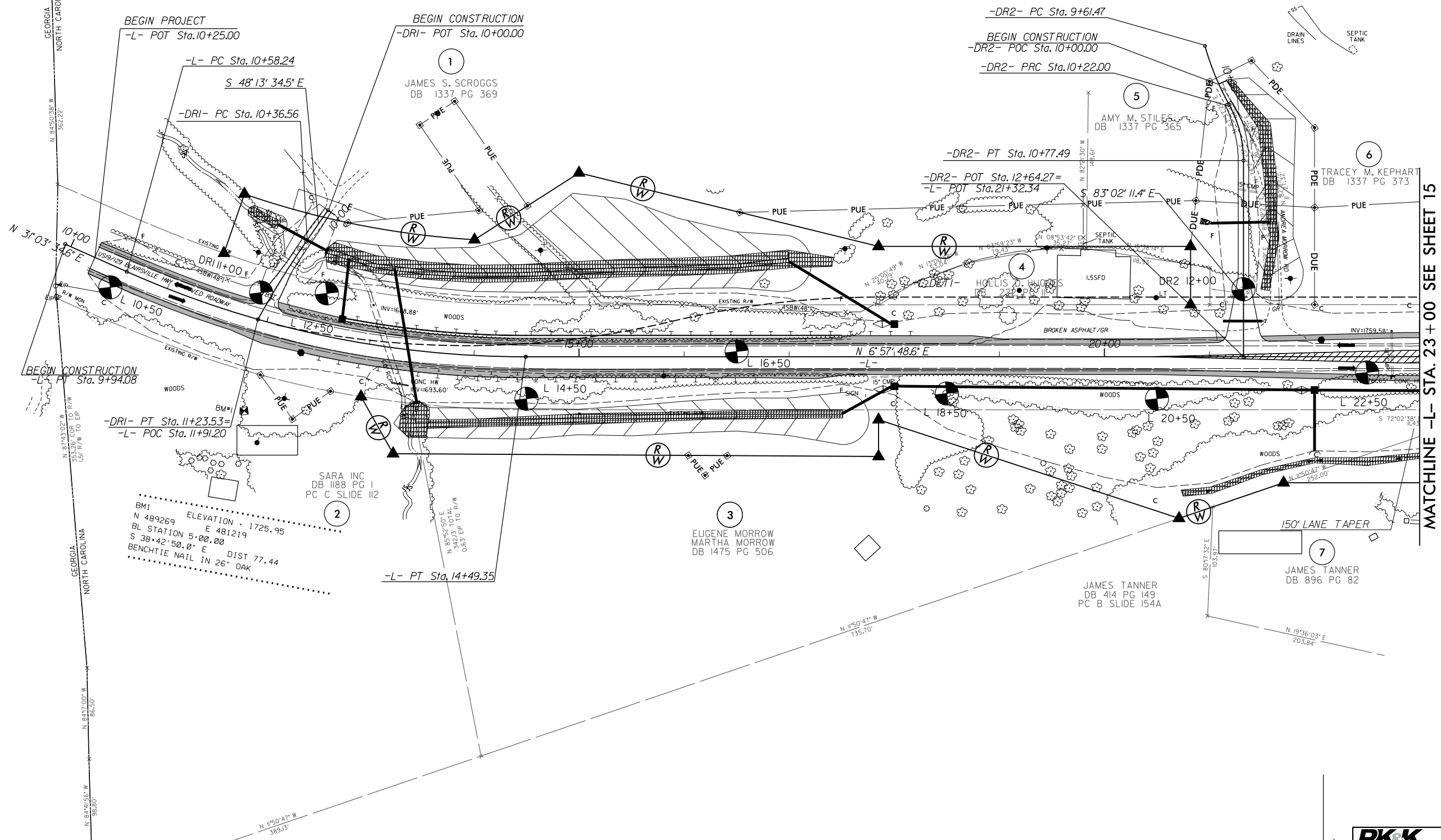
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8/17/09

-L-	-DRI-	-DR2-	
PI Sta 12+56.73	PI Sta 10+80.09	PI Sta 9+91.87	PI Sta 10+50.35
$\Delta = 24^{\circ} 05' 46.1" (LT)$	$\Delta = 6^{\circ} 06' 49.5" (LT)$	$\Delta = 13^{\circ} 05' 15.7" (LT)$	$\Delta = 28^{\circ} 53' 59.0" (RT)$
D = 6' 09' 39.0"	D = 7' 01' 48.6"	D = 21' 37' 15.8"	D = 52' 05' 13.5"
L = 391.12'	L = 86.96'	L = 60.53'	L = 55.48'
T = 198.49'	T = 43.52'	T = 30.40'	T = 28.35'
R = 930.00'	R = 815.00'	R = 265.00'	R = 110.00'
SE = 0.06	SE = 0.02	SE = 0.02	SE = 0.02
RO = 150'	DS = 15 MPH	DS = 15 MPH	DS = 15 MPH

NAD 83/2011

PROJECT REFERENCE NO. R-5861	SHEET NO. 14
RW SHEET NO. 4	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



BM1
N 489269 E 481219
BL STATION 5+00.00
S 38°42'50.0" E DIST 77.44
BENTHIE NAIL IN 26" OAK

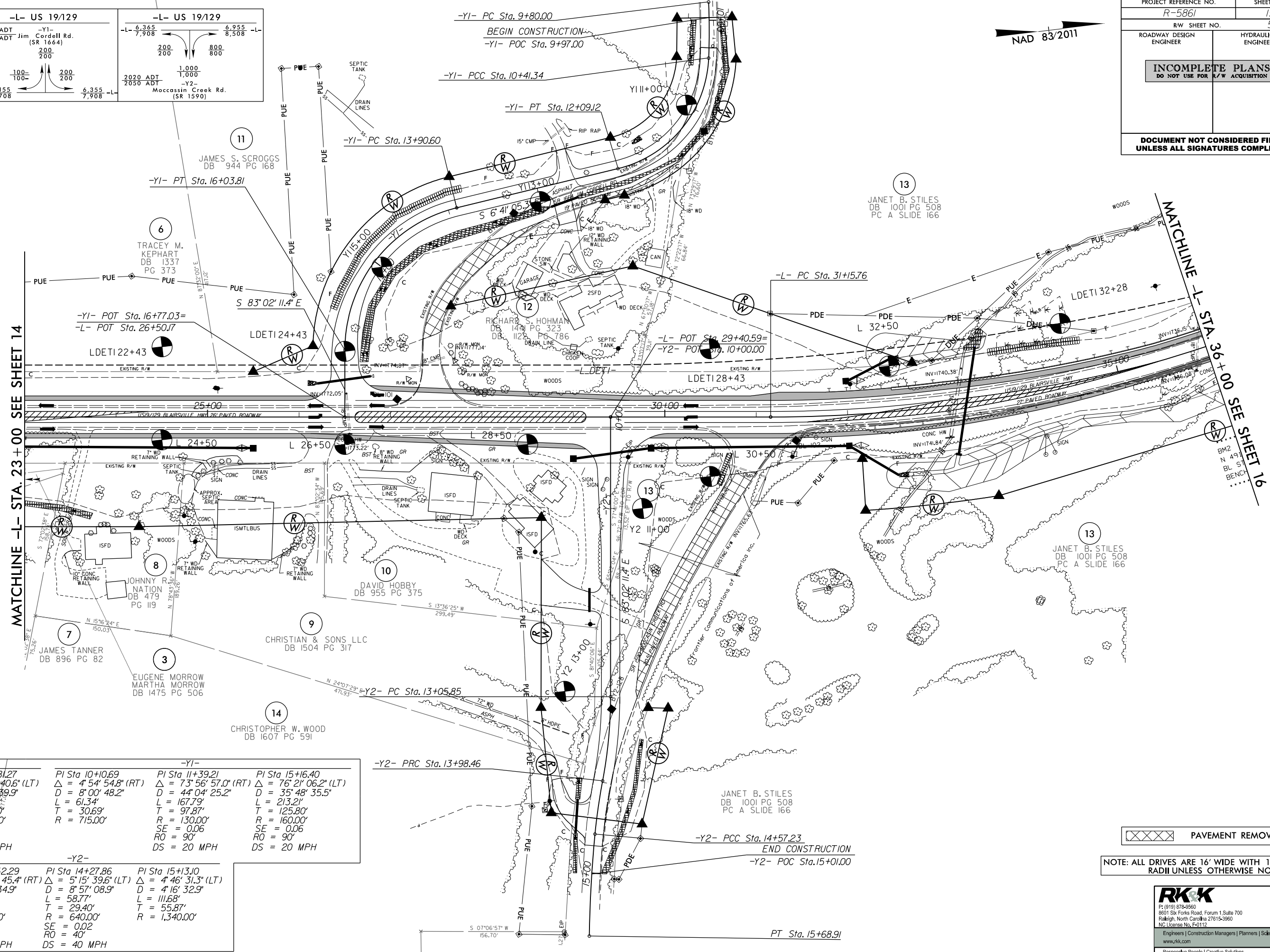
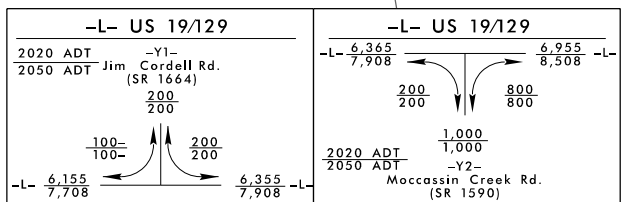
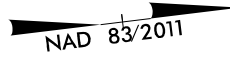
NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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R5861

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MATCHLINE -L- STA. 23+00 SEE SHEET 15

PROJECT REFERENCE NO. R-5861	SHEET NO. 15
R/W SHEET NO. 5	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



-L-		-Y1-		-Y2-	
PI Sta 33+81.27	PI Sta 10+10.69	PI Sta 11+39.21	PI Sta 15+16.40	PI Sta 13+52.29	PI Sta 14+27.86
$\Delta = 19^\circ 56' 40.6''$ (LT)	$\Delta = 4^\circ 54' 54.8''$ (RT)	$\Delta = 73^\circ 56' 57.0''$ (RT)	$\Delta = 76^\circ 21' 06.2''$ (LT)	$\Delta = 10^\circ 49' 45.4''$ (RT)	$\Delta = 5^\circ 15' 39.6''$ (LT)
D = 3' 47' 39.9"	D = 8' 00' 48.2"	D = 44' 04' 25.2"	D = 35' 48' 35.5"	D = 11' 41' 34.9"	D = 8' 57' 08.9"
L = 525.63'	L = 61.34'	L = 167.79'	L = 213.21'	L = 92.61'	L = 58.77'
T = 265.50'	T = 30.69'	T = 97.87'	T = 125.80'	T = 46.44'	T = 29.40'
R = 1,510.00'	R = 715.00'	R = 130.00'	R = 160.00'	R = 490.00'	R = 640.00'
SE = 0.06	SE = 0.06	SE = 0.06	SE = 0.06	SE = NC	SE = 0.02
RO = 210'	RO = 90'	RO = 90'	RO = 90'	RO = 40'	RO = 40'
DS = 60 MPH	DS = 20 MPH	DS = 20 MPH	DS = 20 MPH	DS = 40 MPH	DS = 40 MPH

PAVEMENT REMOVAL

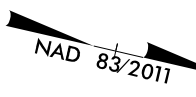
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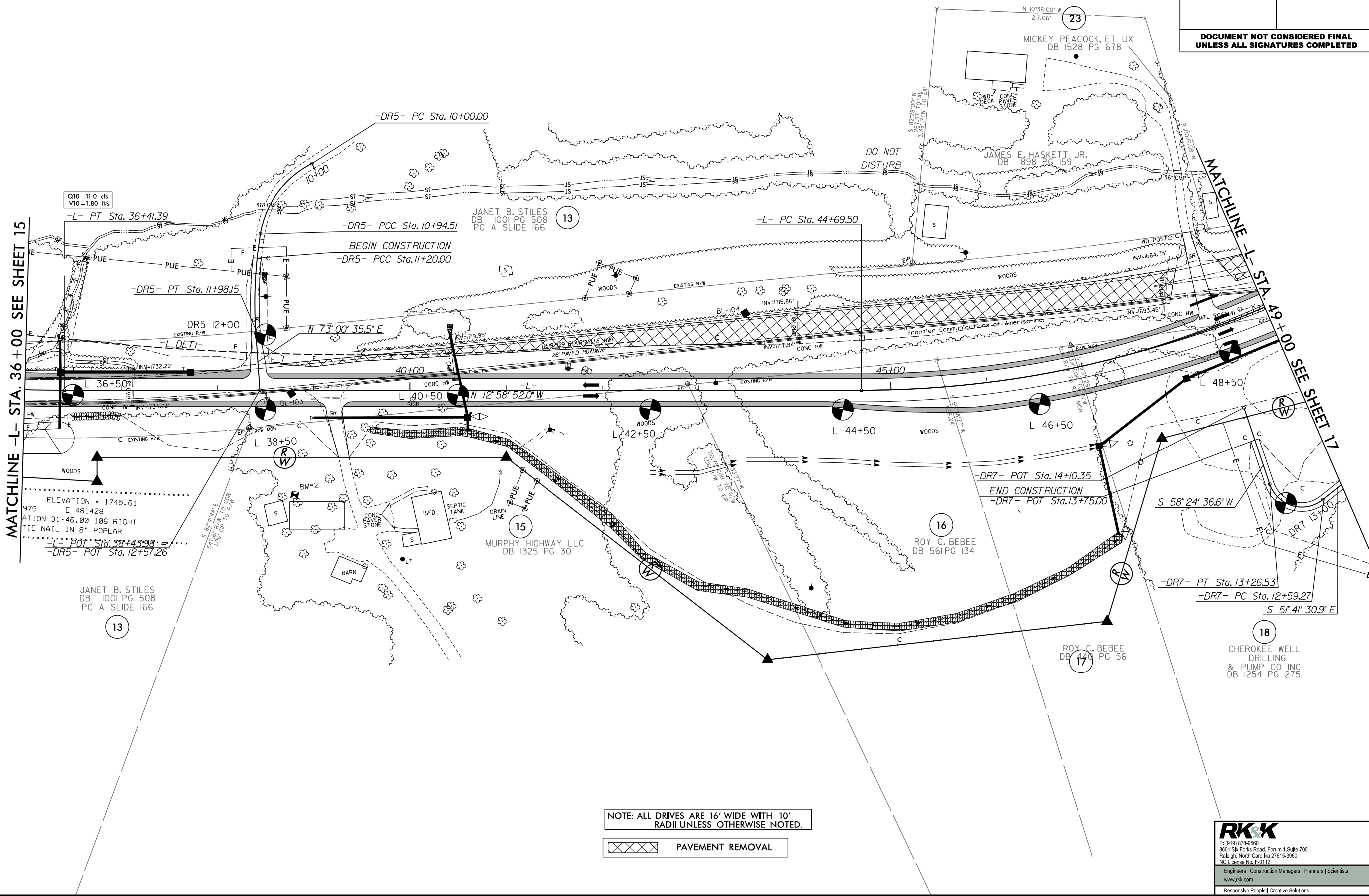
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8/17/09

-L-		-DR5-		-DR7-	
PI Sta 33+81.27	PI Sta 50+66.87	PI Sta 10+51.11	PI Sta 11+46.56	PI Sta 13+09.35	
$\Delta = 19^\circ 56' 40.6" (LT)$	$\Delta = 58^\circ 48' 26.3" (LT)$	$\Delta = 54^\circ 08' 51.5" (LT)$	$\Delta = 13^\circ 11' 45.2" (LT)$	$\Delta = 110^\circ 06' 07.5" (RT)$	
$D = 3^\circ 47' 39.9"$	$D = 5^\circ 24' 18.9"$	$D = 57^\circ 17' 44.8"$	$D = 12^\circ 43' 56.6"$	$D = 163^\circ 42' 08.0"$	
$L = 525.63'$	$L = 1,087.96'$	$L = 94.51'$	$L = 103.64'$	$L = 67.26'$	
$T = 265.50'$	$T = 597.37'$	$T = 51.11'$	$T = 52.05'$	$T = 50.08'$	
$R = 1,510.00'$	$R = 1,060.00'$	$R = 100.00'$	$R = 450.00'$	$R = 35.00'$	
$SE = 0.06$	$SE = 0.06$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$	
$RO = 210^\circ$	$RO = 195^\circ$	$DS = 15 \text{ MPH}$	$DS = 15 \text{ MPH}$	$DS = 15 \text{ MPH}$	



PROJECT REFERENCE NO. R-5861		SHEET NO. 16	
RW SHEET NO. 6		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			



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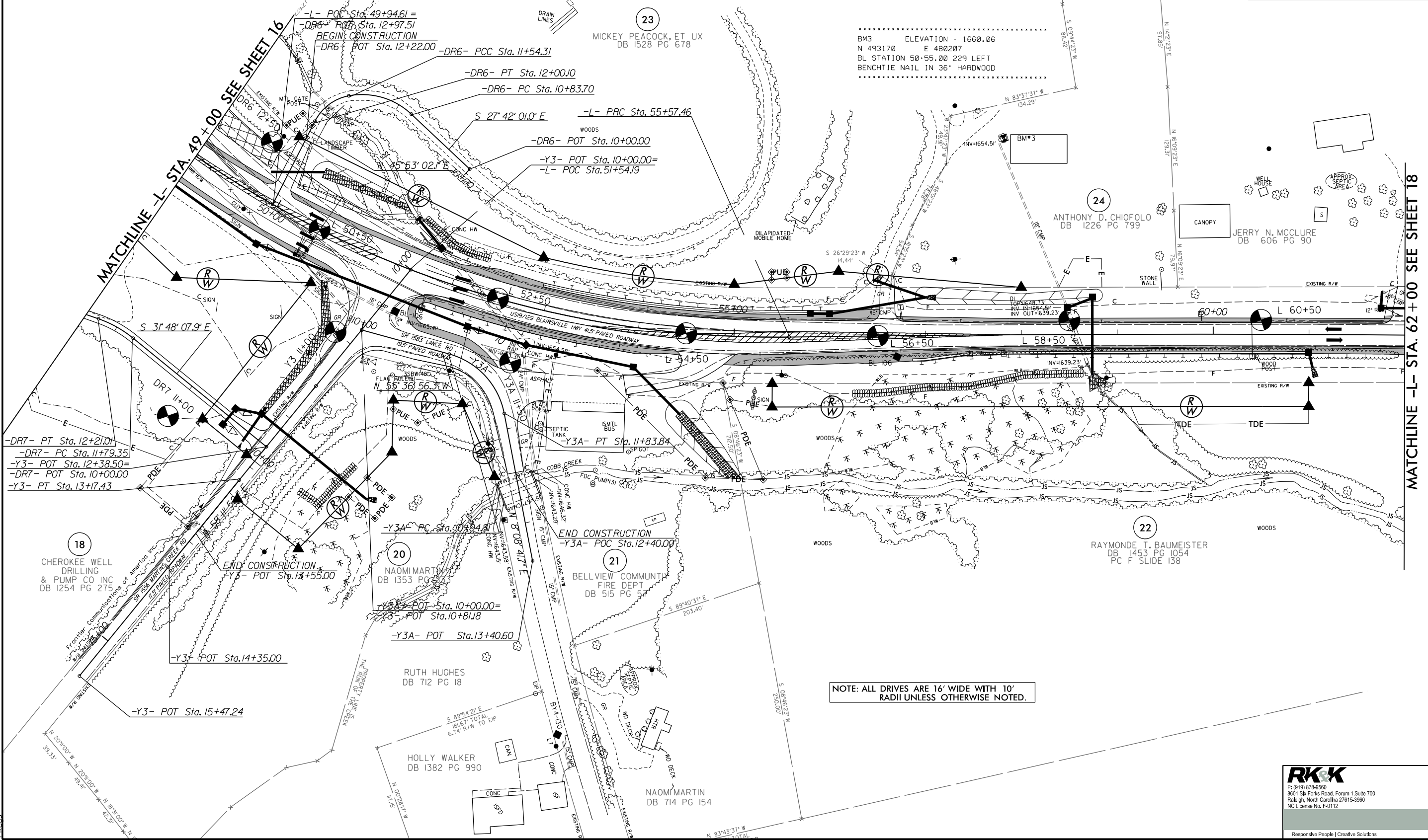
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2/26/2020
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-L-	-Y3A-	-DR6-	-DR7-
PI Sta 50+66.87	PI Sta 11+44.57	PI Sta 11+21.86	PI Sta 12+00.39
$\Delta = 58^\circ 48' 26.3" (LT)$	$\Delta = 63^\circ 45' 38.0" (RT)$	$\Delta = 53^\circ 56' 30.0" (LT)$	$\Delta = 19^\circ 53' 23.0" (LT)$
$D = 5^\circ 24' 18.9"$	$D = 71^\circ 37' 11.0"$	$D = 76^\circ 23' 39.7"$	$D = 47^\circ 44' 47.3"$
$L = 1,087.96'$	$L = 89.03'$	$L = 70.61'$	$L = 41.66'$
$T = 597.37'$	$T = 381.90'$	$T = 38.17'$	$T = 21.04'$
$R = 1,060.00'$	$R = 30,000.00'$	$R = 75.00'$	$R = 120.00'$
$SE = 0.06$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$
$RO = 195^\circ$	$RO = 70^\circ$	$RO = 90^\circ$	$RO = 90^\circ$
$DS = 55 \text{ MPH}$	$DS = 60 \text{ MPH}$	$DS = 15 \text{ MPH}$	$DS = 15 \text{ MPH}$

DESIGN EXCEPTION
REQUIRED FOR
MINIMUM HORIZONTAL
CURVE RADIUS.

PROJECT REFERENCE NO. R-5861	SHEET NO. 17
R/W SHEET NO. 7	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



MATCHLINE -L- STA. 49+00 SEE SHEET 16

MATCHLINE -L- STA. 62+00 SEE SHEET 18



BM3 ELEVATION = 1660.06
N 493170 E 480207
BL STATION 50+55.00 229 LEFT
BENCHTIE NAIL IN 36" HARDWOOD

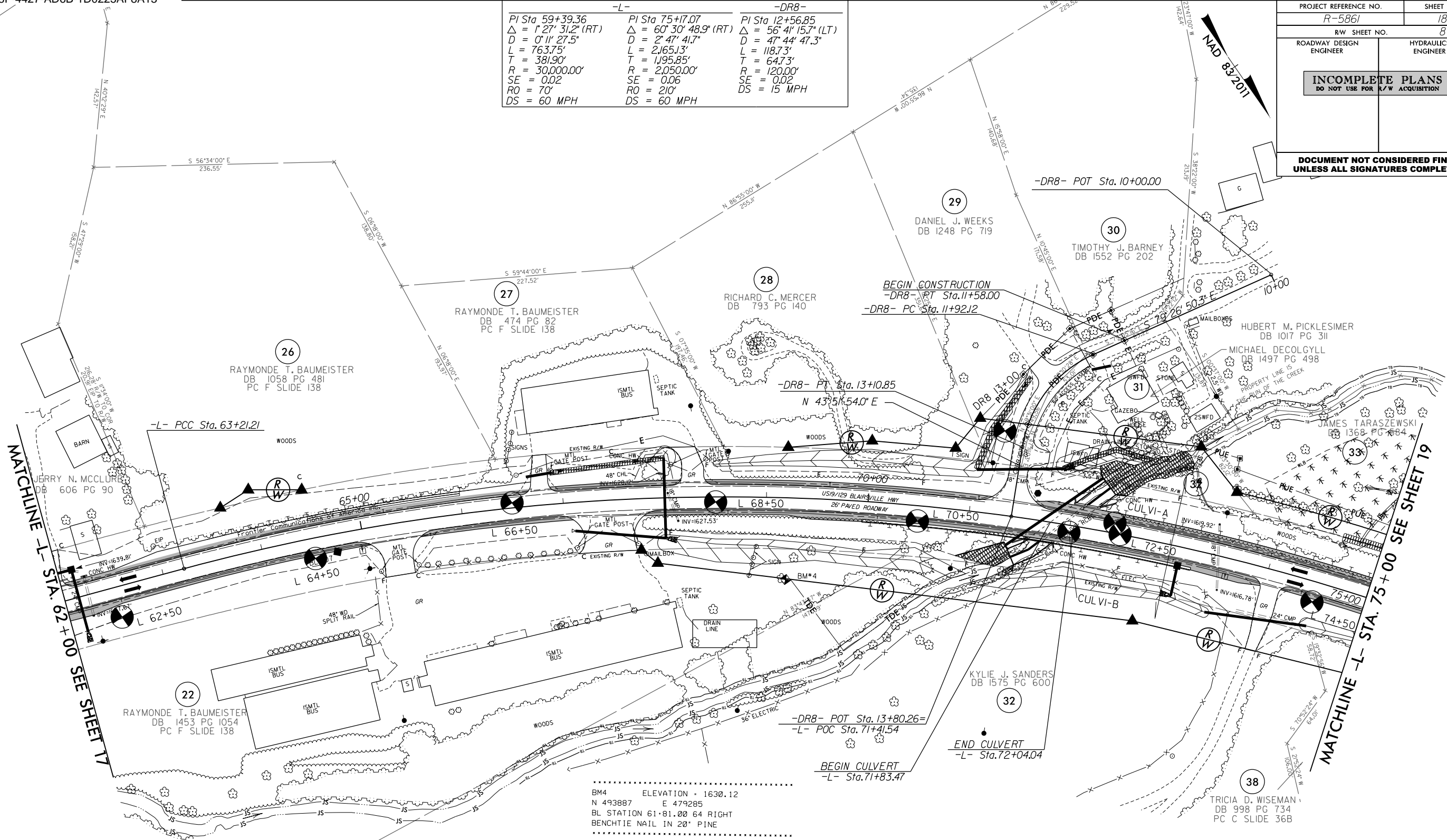
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-L-		-DR8-	
PI Sta 59+39.36	PI Sta 75+17.07	PI Sta 12+56.85	
$\Delta = 1^{\circ}27'31.2''$ (RT)	$\Delta = 60^{\circ}30'48.9''$ (RT)	$\Delta = 56^{\circ}41'15.7''$ (LT)	
D = 0'11'27.5"	D = 2'47'41.7"	D = 47'44'47.3"	
L = 763.75'	L = 2,165.13'	L = 118.73'	
T = 381.90'	T = 1,195.85'	T = 64.73'	
R = 30,000.00'	R = 2,050.00'	R = 120.00'	
SE = 0.02	SE = 0.06	SE = 0.02	
RO = 70'	RO = 210'	DS = 15 MPH	
DS = 60 MPH	DS = 60 MPH		

PROJECT REFERENCE NO. R-5861	SHEET NO. 18
R/W SHEET NO. 8	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



.....
 BM4 ELEVATION = 1630.12
 N 493887 E 479285
 BL STATION 61+81.00 64 RIGHT
 BENCHTIE NAIL IN 20' PINE

CULVERT #1
TWO BARRELS

	NORTH	EAST	ELEV.
CUL1	493988.22	479006.62	1618.40
CUL2	493995.76	478999.21	1618.39
CUL3	493996.70	478998.62	1618.33
CUL4	494003.99	478990.66	1618.43
CE1	493994.78	479000.15	1626.44
HW1	494000.61	478995.60	1628.15
CUL5	493990.38	479066.33	1618.45
CUL6	493998.30	479058.53	1618.40
CUL7	493999.27	479057.78	1618.37
CUL8	494005.81	479049.69	1618.54
CE2	493999.96	479055.77	1626.49
HW2	493997.29	479057.40	1628.27

NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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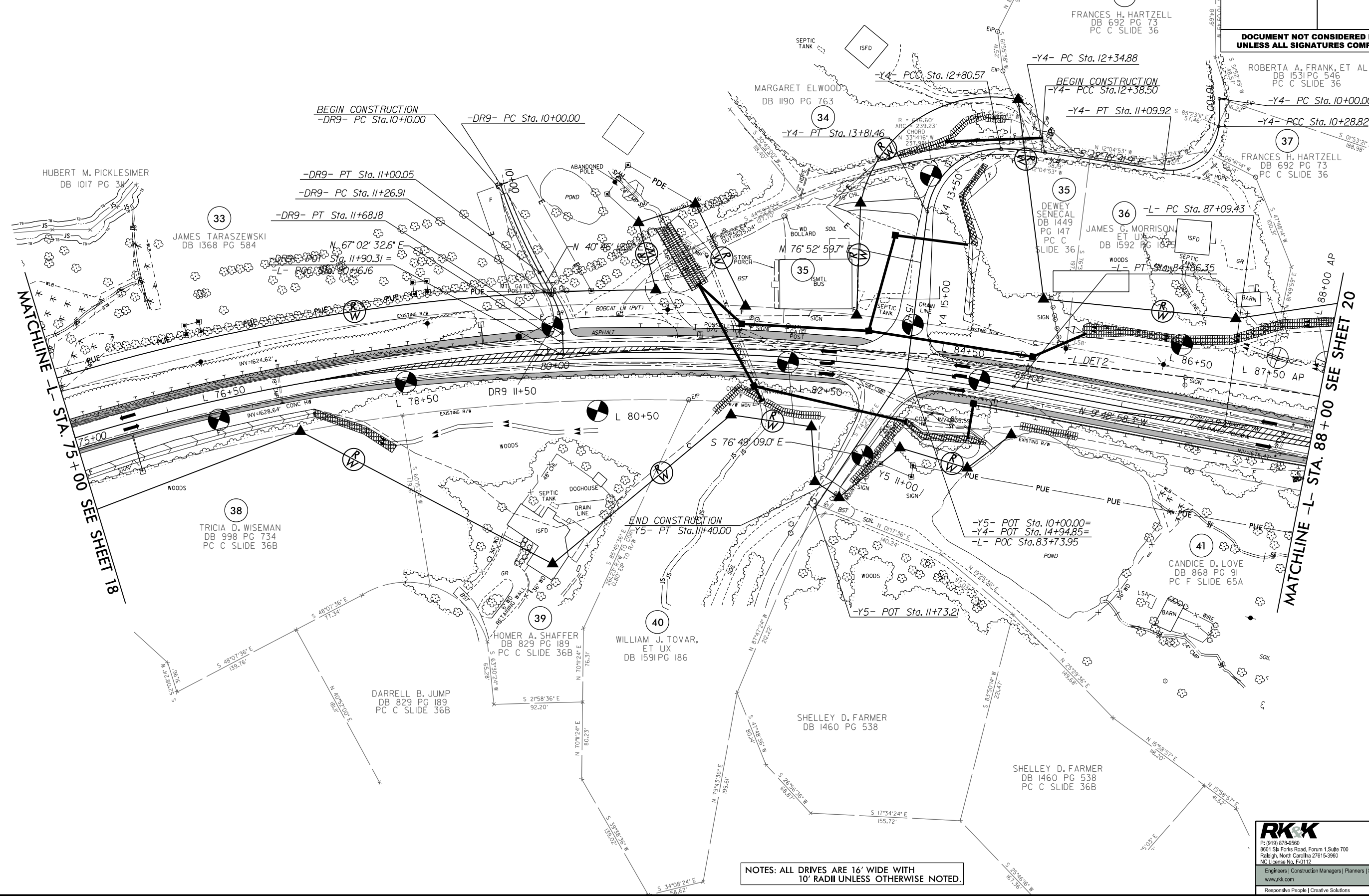
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8/17/09

-DR9-		-L-		-Y4-			
PI Sta 10+50.15	PI Sta 11+47.91	PI Sta 75+17.07	PI Sta 90+43.98	PI Sta 10+14.44	PI Sta 10+81.45	PI Sta 12+57.81	PI Sta 13+48.53
$\Delta = 9^{\circ} 53' 01.0" (LT)$	$\Delta = 26^{\circ} 16' 20.4" (RT)$	$\Delta = 60^{\circ} 30' 48.9" (RT)$	$\Delta = 2^{\circ} 47' 40.83" (RT)$	$\Delta = 7^{\circ} 51' 52.2" (RT)$	$\Delta = 92^{\circ} 55' 38.0" (RT)$	$\Delta = 6^{\circ} 28' 50.8" (LT)$	$\Delta = 84^{\circ} 21' 27.6" (LT)$
$D = 9^{\circ} 52' 42.9"$	$D = 63^{\circ} 39' 43.1"$	$D = 2^{\circ} 47' 41.7"$	$D = 0^{\circ} 25' 03.9"$	$D = 27^{\circ} 17' 01.3"$	$D = 114^{\circ} 35' 29.6"$	$D = 14^{\circ} 10' 59.9"$	$D = 83^{\circ} 37' 14.3"$
$L = 100.05'$	$L = 41.27'$	$L = 2,165.13'$	$L = 668.97'$	$L = 28.82'$	$L = 81.09'$	$L = 45.69'$	$L = 100.88'$
$T = 50.15'$	$T = 21.00'$	$T = 1,195.85'$	$T = 334.55'$	$T = 14.44'$	$T = 52.62'$	$T = 22.93'$	$T = 67.96'$
$R = 580.00'$	$R = 90.00'$	$R = 2,050.00'$	$R = 13,715.00'$	$R = 210.00'$	$R = 50.00'$	$R = 405.00'$	$R = 75.00'$
$SE = 0.02$	$SE = 0.02$	$SE = 0.06$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$	$SE = 0.02$
$DS = 15 MPH$	$DS = 15 MPH$	$RO = 210'$	$RO = 70'$	$DS = 15 MPH$	$DS = 15 MPH$	$RO = 30'$	$RO = 30'$



PROJECT REFERENCE NO. R-5861	SHEET NO. 19
R/W SHEET NO. 9	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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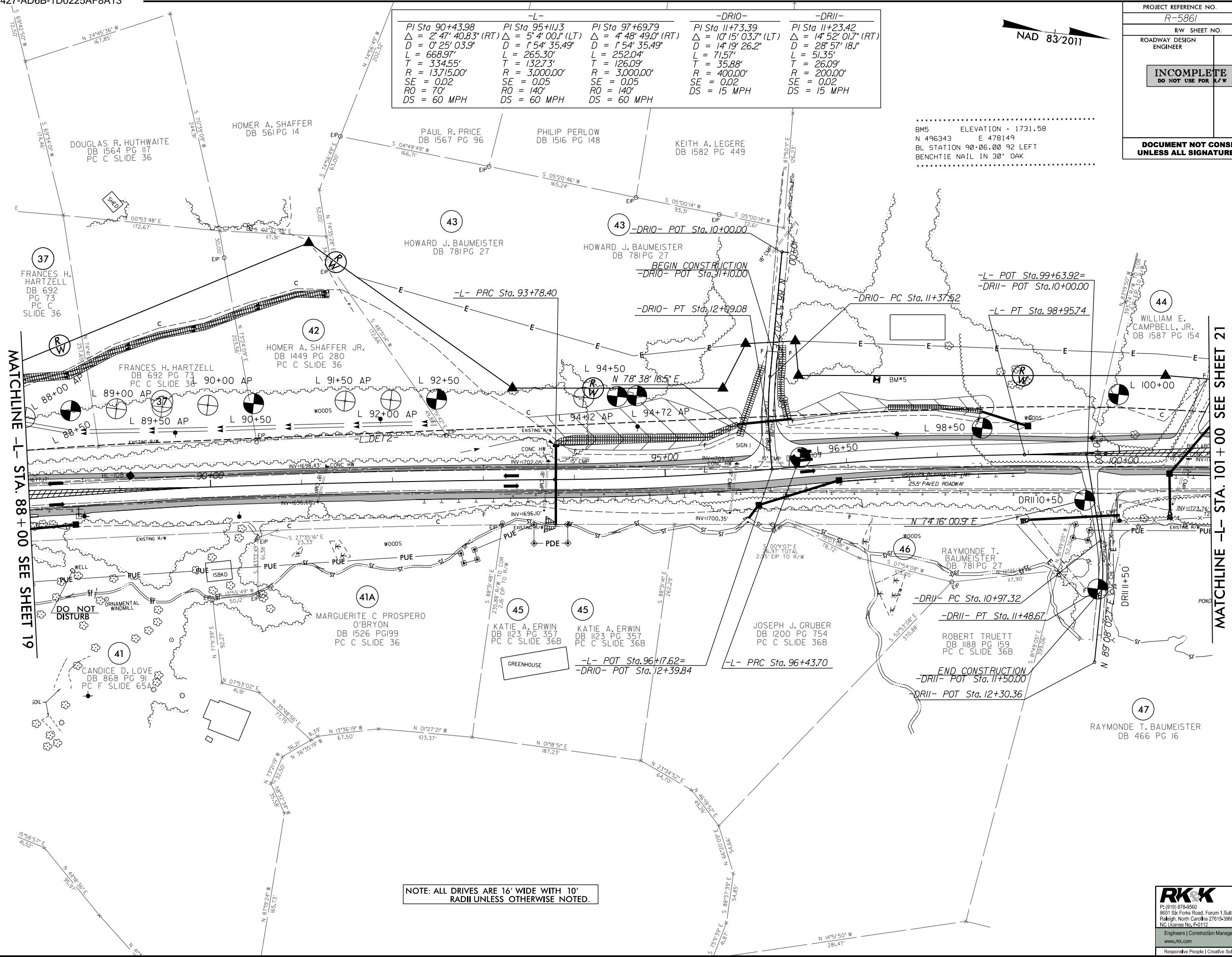
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 R5861

PROJECT REFERENCE NO. <i>R-5861</i>		SHEET NO. <i>20</i>	
RW SHEET NO. <i>10</i>		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			

-L-			-DRIO-		-DRII-	
PI Sta 90+43.98	PI Sta 95+111.3	PI Sta 97+69.79	PI Sta 11+73.39	PI Sta 11+23.42	PI Sta 11+23.42	PI Sta 11+23.42
$\Delta = 2' 47" 40.83" (RT)$	$\Delta = 5' 4" 00.1" (LT)$	$\Delta = 4' 48" 49.0" (RT)$	$\Delta = 10' 15" 03.7" (LT)$	$\Delta = 14' 52" 01.7" (RT)$	$\Delta = 14' 52" 01.7" (RT)$	$\Delta = 14' 52" 01.7" (RT)$
D = 0' 25' 03.9"	D = 1' 54' 35.49"	D = 1' 54' 35.49"	D = 14' 19' 26.2"	D = 28' 57' 18.1"	D = 28' 57' 18.1"	D = 28' 57' 18.1"
L = 668.97'	L = 265.30'	L = 252.04'	L = 71.57'	L = 51.35'	L = 51.35'	L = 51.35'
T = 334.55'	T = 132.73'	T = 126.09'	T = 35.88'	T = 26.09'	T = 26.09'	T = 26.09'
R = 13,715.00'	R = 3,000.00'	R = 3,000.00'	R = 400.00'	R = 200.00'	R = 200.00'	R = 200.00'
SE = 0.02	SE = 0.05	SE = 0.05	SE = 0.02	SE = 0.02	SE = 0.02	SE = 0.02
RO = 70'	RO = 140'	RO = 140'	DS = 15 MPH	DS = 15 MPH	DS = 15 MPH	DS = 15 MPH
DS = 60 MPH	DS = 60 MPH	DS = 60 MPH				

NAD 83/2011

.....
 BMS ELEVATION + 1731.58
 N 496343 E 478149
 BL STATION 90+06.00 92 LEFT
 BENCHMARK NAIL IN 30" OAK



MATCHLINE -L- STA. 88 + 00 SEE SHEET 19

MATCHLINE -L- STA. 101 + 00 SEE SHEET 21

NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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PI Sta 11+20.71 Δ = 0° 38' 52.86" (LT) D = 0' 15' 37.57" L = 248.82' T = 124.41' R = 22,000.00' SE = NC RO = 70' DS = 60 MPH	PI Sta 13+60.37 Δ = 81° 00' 06.6" (LT) D = 39° 30' 51.6" L = 204.99' T = 123.85' R = 145.00' SE = 0.06 RO = 100' DS = 25 MPH	PI Sta 16+47.26 Δ = 66° 29' 36.7" (RT) D = 67° 24' 24.5" L = 98.65' T = 55.72' R = 85.00' SE = 0.05 RO = 75' DS = 20 MPH
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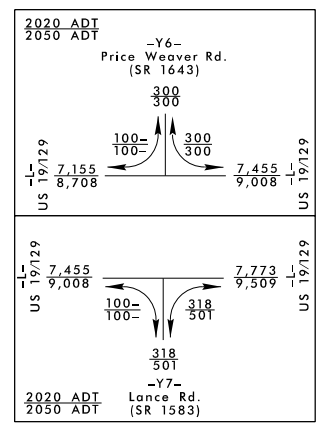
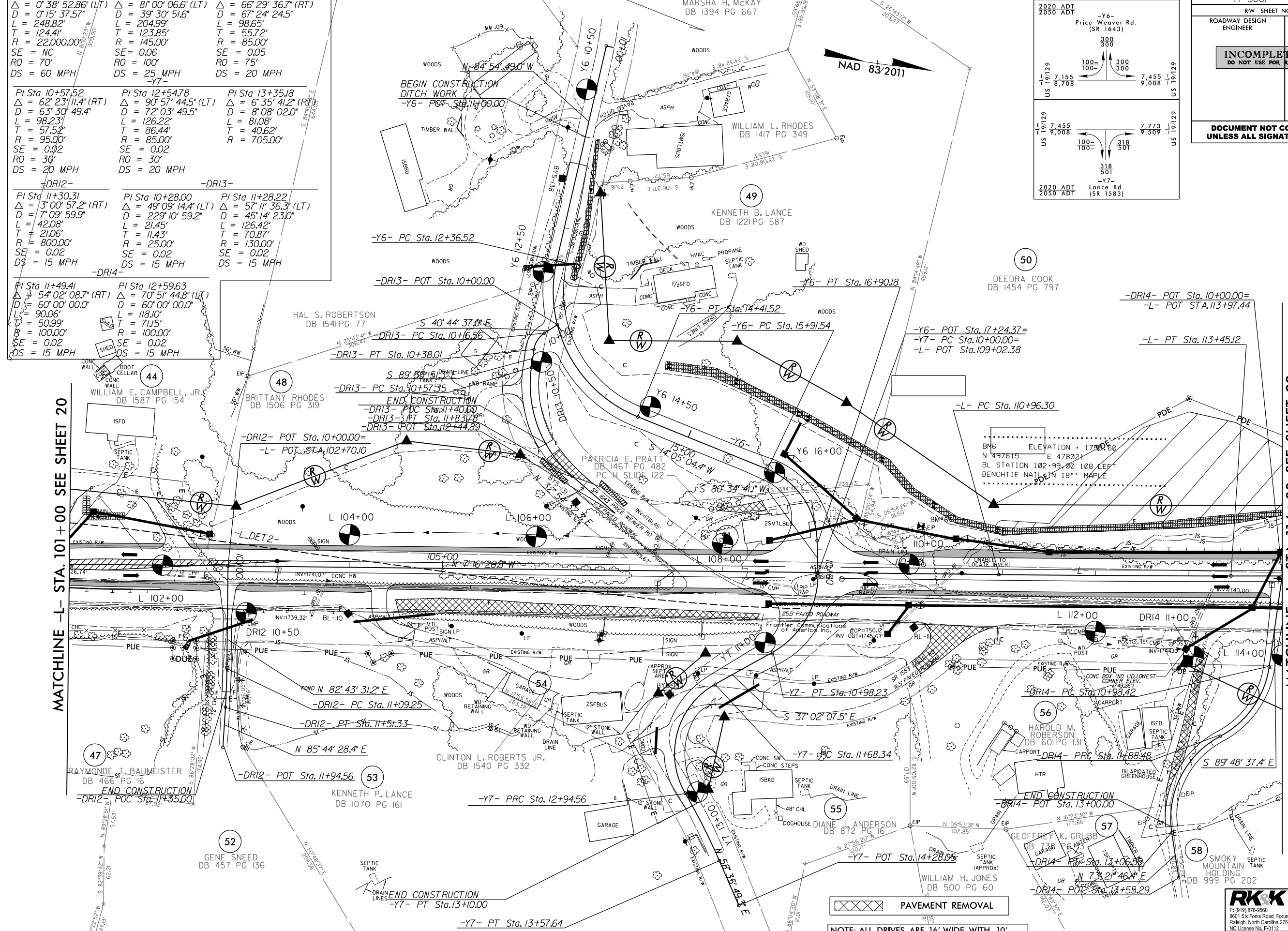
PI Sta 10+57.52 Δ = 62° 23' 11.4" (RT) D = 63° 30' 49.4" L = 98.23' T = 57.52' R = 95.00' SE = 0.02 RO = 30' DS = 20 MPH	PI Sta 12+54.78 Δ = 90° 57' 44.5" (LT) D = 72° 03' 49.5" L = 126.22' T = 86.44' R = 85.00' SE = 0.02 RO = 30' DS = 20 MPH	PI Sta 13+35.18 Δ = 6° 35' 41.2" (RT) D = 8° 08' 02.0" L = 81.08' T = 40.62' R = 705.00' SE = 0.02 RO = 75' DS = 20 MPH
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PI Sta 11+30.31 Δ = 3° 00' 57.2" (RT) D = 7° 09' 59.9" L = 42.08' T = 21.06' R = 800.00' SE = 0.02 DS = 15 MPH	PI Sta 10+28.00 Δ = 49° 09' 14.4" (LT) D = 229° 10' 59.2" L = 21.45' T = 11.43' R = 25.00' SE = 0.02 DS = 15 MPH	PI Sta 11+28.22 Δ = 57° 11' 36.3" (LT) D = 45° 14' 23.0" L = 126.42' T = 70.87' R = 130.00' SE = 0.02 DS = 15 MPH
---	---	--

PI Sta 11+49.41 Δ = 54° 02' 08.7" (RT) D = 60° 00' 00.0" L = 90.06' T = 50.99' R = 100.00' SE = 0.02 DS = 15 MPH	PI Sta 12+59.63 Δ = 70° 51' 44.8" (LT) D = 60° 00' 00.0" L = 118.10' T = 71.15' R = 100.00' SE = 0.02 DS = 15 MPH
---	--

MATCHLINE -L- STA. 101+00 SEE SHEET 20

MATCHLINE -L- STA. 114+00 SEE SHEET 22



PROJECT REFERENCE NO. R-5861	SHEET NO. 21
R/W SHEET NO. II	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	

INCOMPLETE PLANS
DO NOT USE FOR R/W ACQUISITION

DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED

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NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

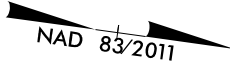
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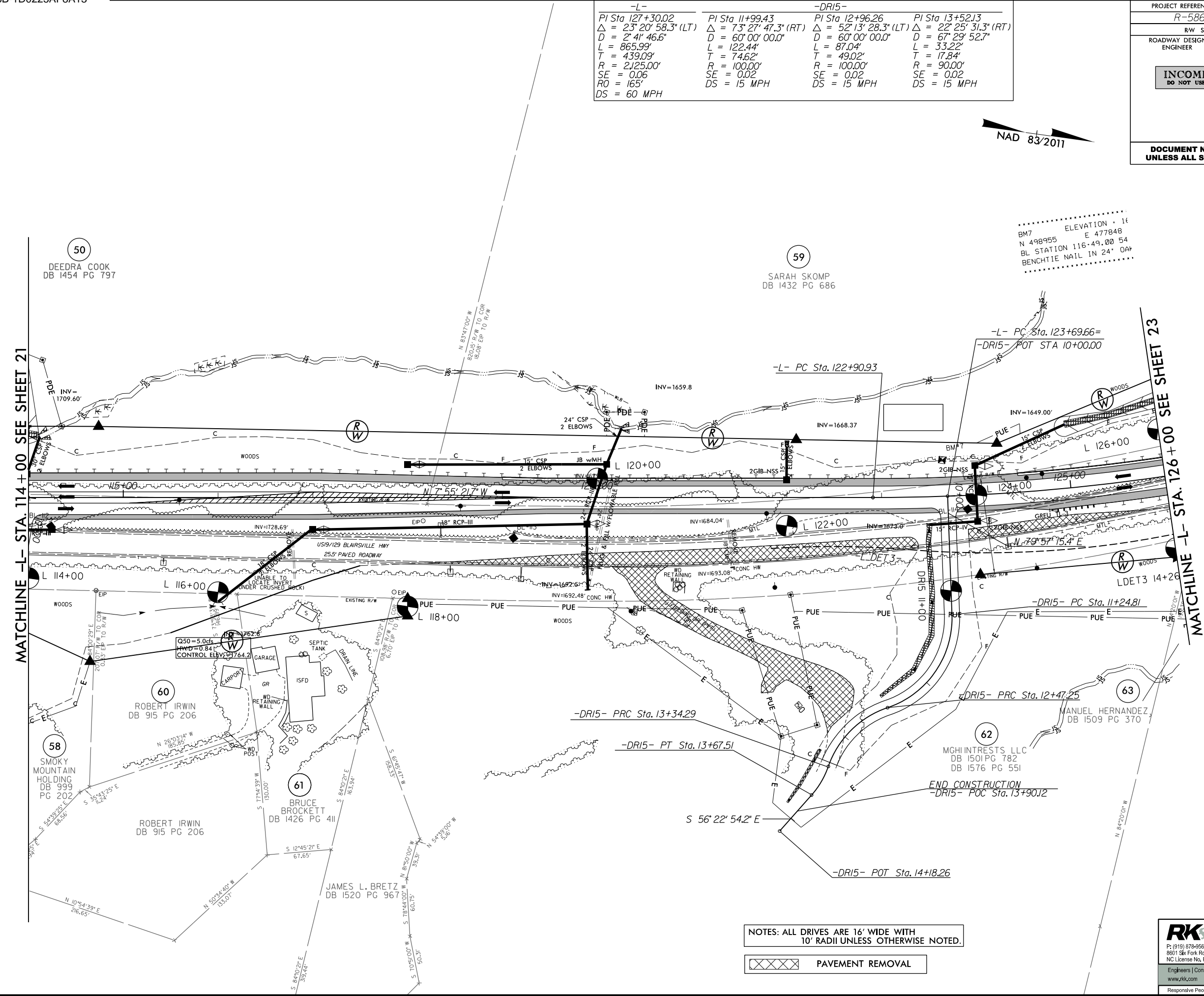
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-L-		-DRI5-	
PI Sta 127+30.02	PI Sta 11+99.43	PI Sta 12+96.26	PI Sta 13+52.13
$\Delta = 23^\circ 20' 58.3" (LT)$	$\Delta = 73^\circ 27' 47.3" (RT)$	$\Delta = 52^\circ 13' 28.3" (LT)$	$\Delta = 22^\circ 25' 31.3" (RT)$
D = 2' 41' 46.6"	D = 60' 00' 00.0"	D = 60' 00' 00.0"	D = 67' 29' 52.7"
L = 865.99'	L = 122.44'	L = 87.04'	L = 33.22'
T = 439.09'	T = 74.62'	T = 49.02'	T = 17.84'
R = 2125.00'	R = 100.00'	R = 100.00'	R = 90.00'
SE = 0.06	SE = 0.02	SE = 0.02	SE = 0.02
RO = 165'	DS = 15 MPH	DS = 15 MPH	DS = 15 MPH
DS = 60 MPH			

PROJECT REFERENCE NO. R-5861	SHEET NO. 22
RW SHEET NO. 12	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



ELEVATION = 11'
 BM7 N 498955 E 477848
 BL STATION 116+49.00 54
 BENCHTIE NAIL IN 24" OAH



MATCHLINE -L- STA. 114+00 SEE SHEET 21

MATCHLINE -L- STA. 126+00 SEE SHEET 23

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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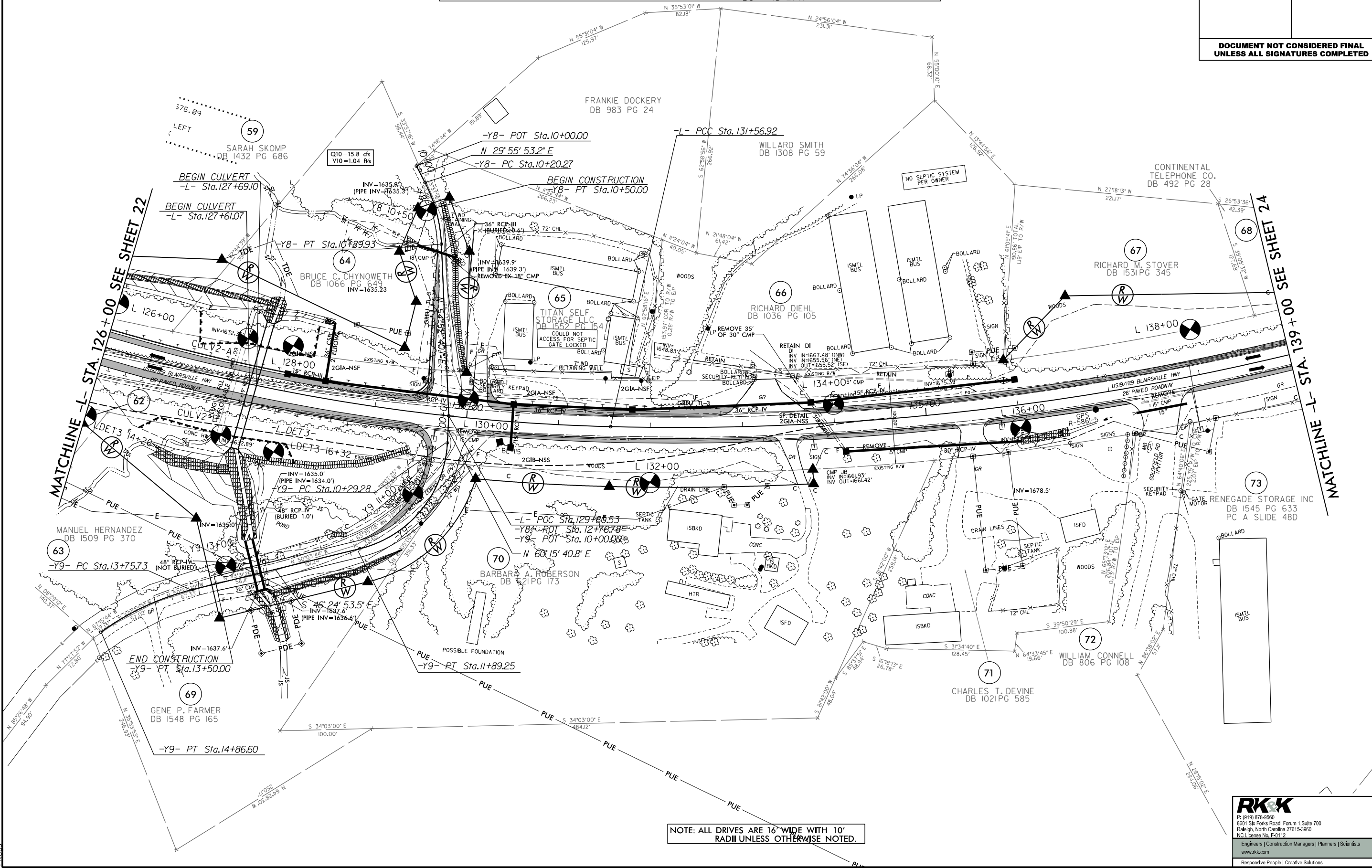
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-L-	-Y8-	-Y9-
PI Sta 127+30.02	PI Sta 135+82.23	PI Sta 10+55.66
$\Delta = 23^\circ 20' 58.3" (LT)$	$\Delta = 16^\circ 58' 31.5" (LT)$	$\Delta = 24^\circ 56' 46.9" (RT)$
$D = 2' 41' 46.6"$	$D = 2' 00' 37.4"$	$D = 35' 48' 35.5"$
$L = 865.99'$	$L = 844.39'$	$L = 69.66'$
$R = 439.09'$	$R = 425.31'$	$R = 35.39'$
$T = 2,125.00'$	$T = 2,850.00'$	$T = 160.00'$
$SE = 0.06$	$SE = 0.05$	$SE = 0.03$
$DS = 60 \text{ MPH}$	$DS = 60 \text{ MPH}$	$DS = 15 \text{ MPH}$
		$DS = 15 \text{ MPH}$



PROJECT REFERENCE NO. R-5861	SHEET NO. 23
R/W SHEET NO. 13	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	



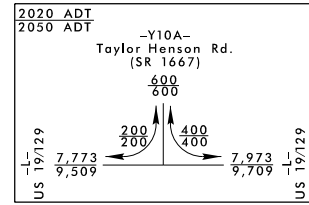
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PROJECT REFERENCE NO. R-5861		SHEET NO. 24	
RW SHEET NO. 14		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			

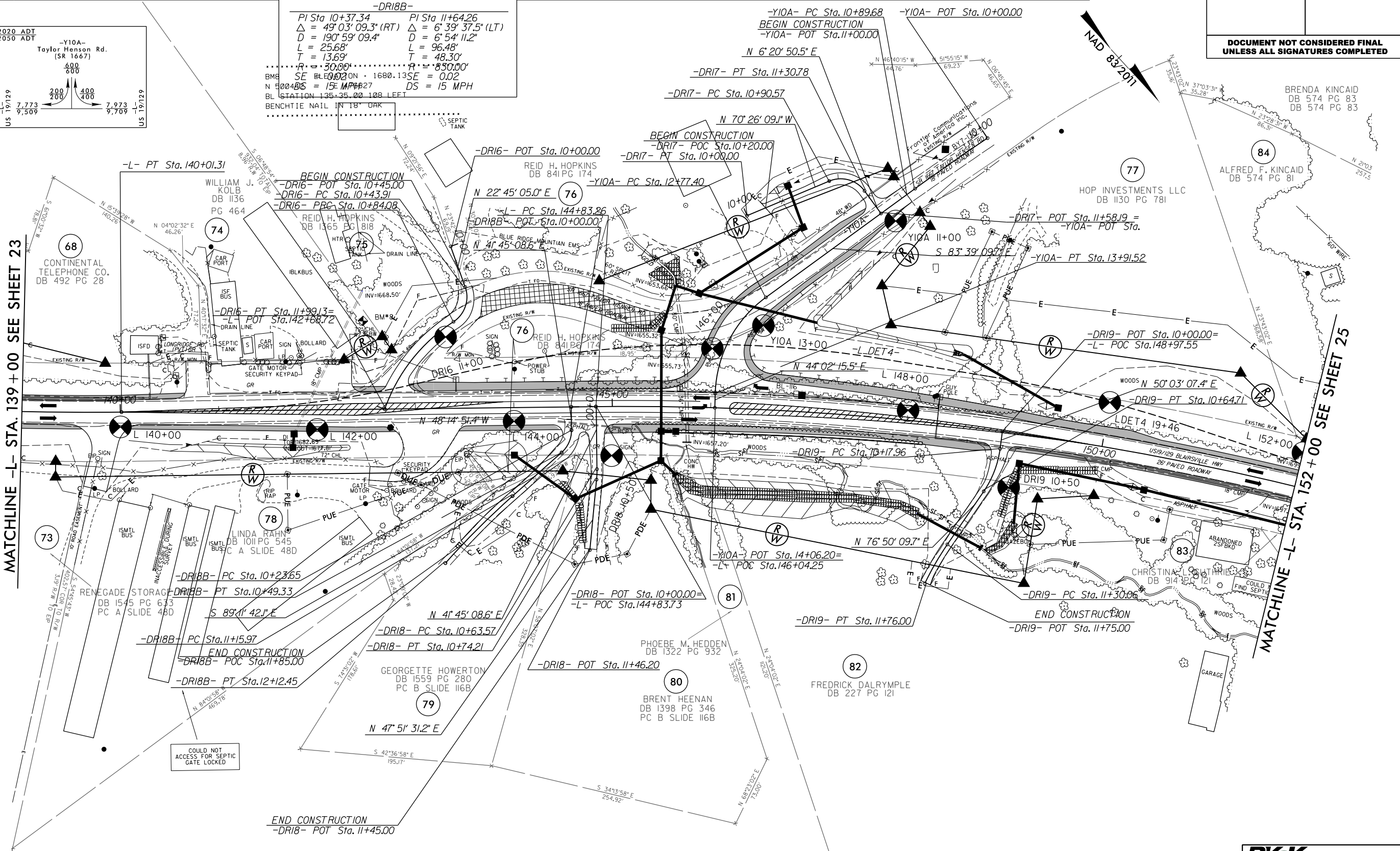
-L- PI Sta 135+82.23 Δ = 16° 58' 31.5" (LT) D = 2' 00' 37.4" L = 844.39' T = 425.31' R = 2,850.00' SE = 0.05 DS = 60 MPH	-L- PI Sta 151+02.43 Δ = 24° 25' 52.3" (RT) D = 2' 00' 12.1" L = 1,219.52' T = 619.17' R = 2,869.00' SE = 0.05 DS = 60 MPH	-Y10A- PI Sta 10+44.85 Δ = 2° 20' 08.2" (LT) D = 2' 36' 15.7" L = 89.68' T = 44.85' R = 2,200.00'	-Y10A- PI Sta 13+38.78 Δ = 52° 18' 34.8" (LT) D = 45' 50' 11.8" L = 114.12' T = 61.39' R = 125.00' SE = 0.03 DS = 20 MPH	-DR16- PI Sta 10+67.65 Δ = 76° 43' 07.2" (RT) D = 190' 59' 09.4" L = 114.12' T = 23.74' R = 30.00' SE = 0.02 DS = 15 MPH	-DR16- PI Sta 11+43.77 Δ = 37° 40' 05.5" (LT) D = 32' 44' 25.6" L = 115.05' T = 59.69' R = 175.00' SE = 0.02 DS = 15 MPH	-DR17- PI Sta 11+43.77 Δ = 76° 46' 59.6" (RT) D = 190' 59' 09.4" L = 40.20' T = 23.77' R = 30.00' SE = 0.02 DS = 15 MPH	-DR18- PI Sta 10+68.89 Δ = 6° 05' 49.0" (RT) D = 57' 17' 44.8" L = 10.64' T = 5.33' R = 100.00' SE = 0.02 DS = 15 MPH	-DR19- PI Sta 10+41.77 Δ = 26° 47' 02.3" (RT) D = 57' 17' 44.8" L = 46.75' T = 23.81' R = 100.00' SE = 0.02 DS = 15 MPH	-DR19- PI Sta 11+53.07 Δ = 8° 46' 24.5" (LT) D = 19' 05' 54.9" L = 45.94' T = 23.01' R = 300.00' SE = 0.02 DS = 15 MPH
---	---	--	---	---	---	--	--	--	---



-DR18B- PI Sta 10+37.34 Δ = 49° 03' 09.3" (RT) D = 190' 59' 09.4" L = 25.68' T = 13.69' R = 30.00' SE = 0.02 DS = 15 MPH	-DR18B- PI Sta 11+64.26 Δ = 6° 39' 37.5" (LT) D = 6' 54' 11.2" L = 96.48' T = 48.30' R = 830.00' SE = 0.02 DS = 15 MPH
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MATCHLINE -L- STA. 139+00 SEE SHEET 23

MATCHLINE -L- STA. 152+00 SEE SHEET 25

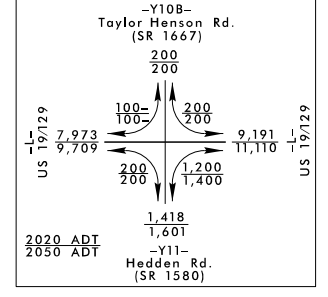
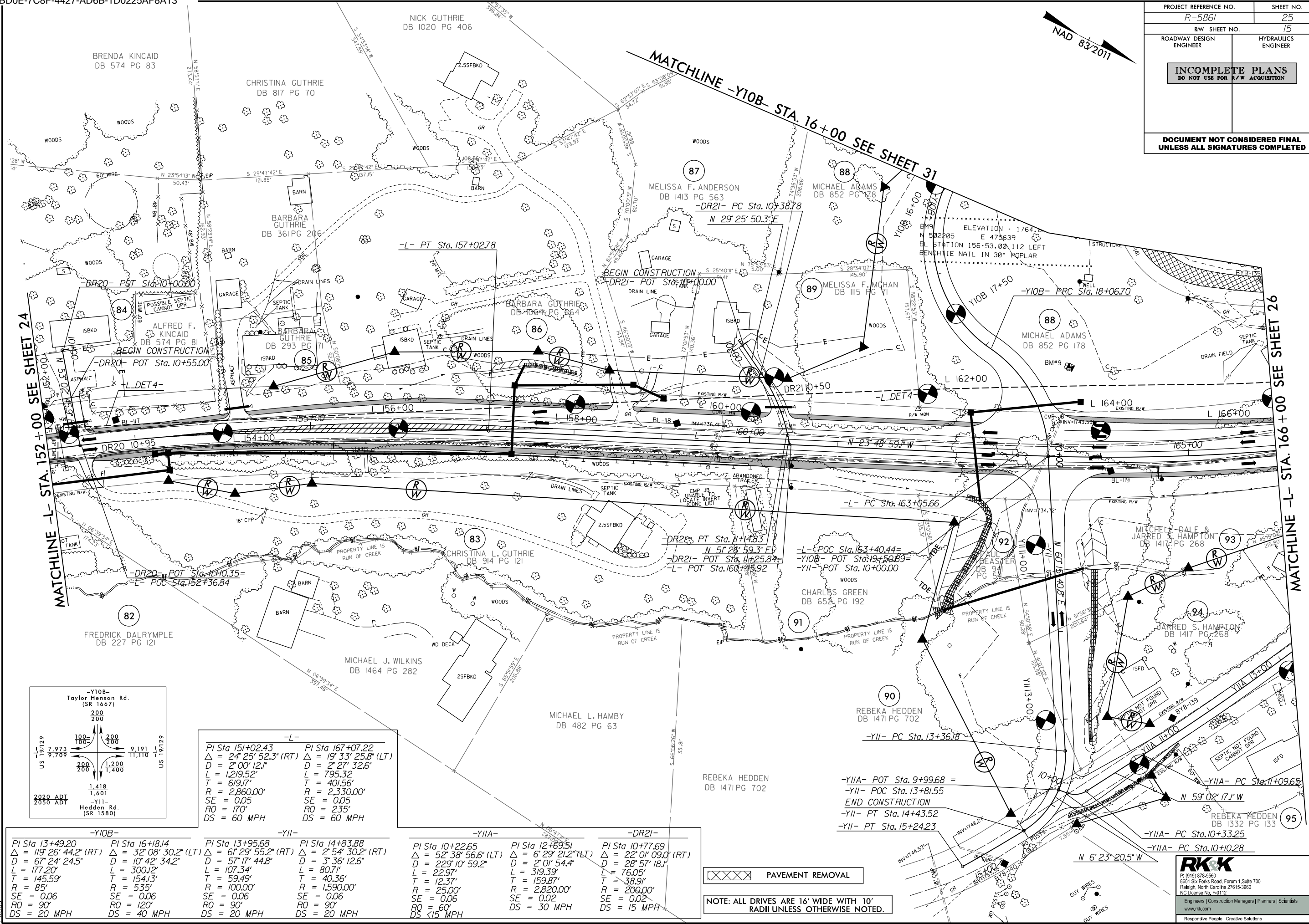


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PROJECT REFERENCE NO. R-5861		SHEET NO. 25	
RW SHEET NO. 15		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			



-L-	
PI Sta 151+02.43	PI Sta 167+07.22
$\Delta = 24^\circ 25' 52.3"$ (RT)	$\Delta = 19^\circ 33' 25.8"$ (LT)
D = 2' 00" 12.1"	D = 2' 27" 32.6"
L = 1,219.52'	L = 795.32'
T = 619.17'	T = 401.56'
R = 2,860.00'	R = 2,330.00'
SE = 0.05	SE = 0.05
RO = 170'	RO = 235'
DS = 60 MPH	DS = 60 MPH

-Y10B-		-Y11-	
PI Sta 13+49.20	PI Sta 16+18.14	PI Sta 13+95.68	PI Sta 14+83.88
$\Delta = 119^\circ 26' 44.2"$ (RT)	$\Delta = 32^\circ 08' 30.2"$ (LT)	$\Delta = 61^\circ 29' 55.2"$ (RT)	$\Delta = 2^\circ 54' 30.2"$ (RT)
D = 67' 24" 24.5"	D = 10' 42" 34.2"	D = 57' 17" 44.8"	D = 3' 36" 12.6"
L = 177.20'	L = 300.12'	L = 107.34'	L = 80.71'
T = 145.59'	T = 154.13'	T = 59.49'	T = 40.36'
R = 85'	R = 535'	R = 100.00'	R = 1,590.00'
SE = 0.06	SE = 0.06	SE = 0.06	SE = 0.06
RO = 90'	RO = 120'	RO = 90'	RO = 90'
DS = 20 MPH	DS = 40 MPH	DS = 20 MPH	DS = 20 MPH

-Y12-		-Y13-	
PI Sta 13+95.68	PI Sta 14+83.88	PI Sta 13+95.68	PI Sta 14+83.88
$\Delta = 61^\circ 29' 55.2"$ (RT)	$\Delta = 2^\circ 54' 30.2"$ (RT)	$\Delta = 61^\circ 29' 55.2"$ (RT)	$\Delta = 2^\circ 54' 30.2"$ (RT)
D = 57' 17" 44.8"	D = 3' 36" 12.6"	D = 57' 17" 44.8"	D = 3' 36" 12.6"
L = 107.34'	L = 80.71'	L = 107.34'	L = 80.71'
T = 59.49'	T = 40.36'	T = 59.49'	T = 40.36'
R = 100.00'	R = 1,590.00'	R = 100.00'	R = 1,590.00'
SE = 0.06	SE = 0.06	SE = 0.06	SE = 0.06
RO = 90'	RO = 90'	RO = 90'	RO = 90'
DS = 20 MPH	DS = 20 MPH	DS = 20 MPH	DS = 20 MPH

-Y14-		-Y15-	
PI Sta 10+22.65	PI Sta 12+69.51	PI Sta 10+22.65	PI Sta 12+69.51
$\Delta = 52^\circ 38' 56.6"$ (LT)	$\Delta = 6^\circ 29' 21.2"$ (LT)	$\Delta = 52^\circ 38' 56.6"$ (LT)	$\Delta = 6^\circ 29' 21.2"$ (LT)
D = 229' 10' 59.2"	D = 2' 01' 54.4"	D = 229' 10' 59.2"	D = 2' 01' 54.4"
L = 22.97'	L = 319.39'	L = 22.97'	L = 319.39'
T = 12.37'	T = 159.87'	T = 12.37'	T = 159.87'
R = 25.00'	R = 2,820.00'	R = 25.00'	R = 2,820.00'
SE = 0.06	SE = 0.02	SE = 0.06	SE = 0.02
RO = 60'	DS = 30 MPH	RO = 60'	DS = 15 MPH

-DR21-		-DR22-	
PI Sta 10+77.69	PI Sta 10+77.69	PI Sta 10+77.69	PI Sta 10+77.69
$\Delta = 22^\circ 01' 09.0"$ (RT)	$\Delta = 22^\circ 01' 09.0"$ (RT)	$\Delta = 22^\circ 01' 09.0"$ (RT)	$\Delta = 22^\circ 01' 09.0"$ (RT)
D = 28' 57' 18.1"	D = 28' 57' 18.1"	D = 28' 57' 18.1"	D = 28' 57' 18.1"
L = 76.05'	L = 76.05'	L = 76.05'	L = 76.05'
T = 38.91'	T = 38.91'	T = 38.91'	T = 38.91'
R = 200.00'	R = 200.00'	R = 200.00'	R = 200.00'
SE = 0.02	SE = 0.02	SE = 0.02	SE = 0.02
RO = 60'	DS = 15 MPH	RO = 60'	DS = 15 MPH



NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

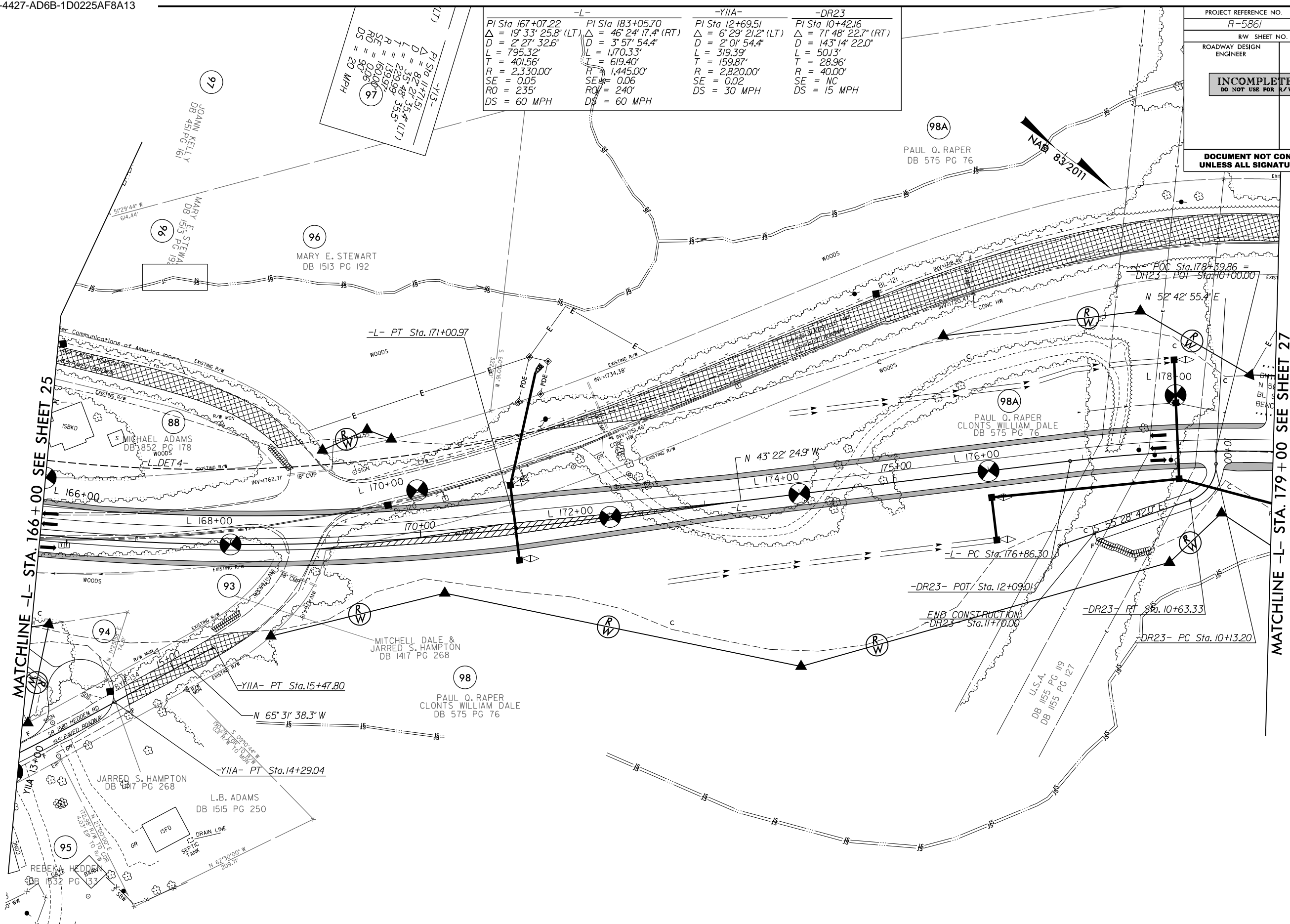
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 9,709
 200
 200
 1,418
 1,601
 2050 ADT
 2050 ADT
 1,418
 1,601
 2050 ADT
 2050 ADT

8/17/09

PROJECT REFERENCE NO. R-5861	SHEET NO. 26
R/W SHEET NO. 16	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

-L-	-YIIA-	-DR23-
PI Sta 167+07.22	PI Sta 183+05.70	PI Sta 12+69.51
$\Delta = 19^\circ 33' 25.8" (LT)$	$\Delta = 46^\circ 24' 17.4" (RT)$	$\Delta = 6^\circ 29' 21.2" (LT)$
$D = 2^\circ 27' 32.6"$	$D = 3^\circ 57' 54.4"$	$D = 2^\circ 01' 54.4"$
$L = 795.32'$	$L = 1,170.33'$	$L = 319.39'$
$T = 401.56'$	$T = 619.40'$	$T = 159.87'$
$R = 2,330.00'$	$R = 1,445.00'$	$R = 2,820.00'$
$SE = 0.05$	$SE = 0.06$	$SE = 0.02$
$RO = 235'$	$RO = 240'$	$SE = NC$
$DS = 60 \text{ MPH}$	$DS = 60 \text{ MPH}$	$DS = 15 \text{ MPH}$



MATCHLINE -L- STA. 166+00 SEE SHEET 25

MATCHLINE -L- STA. 179+00 SEE SHEET 27

NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

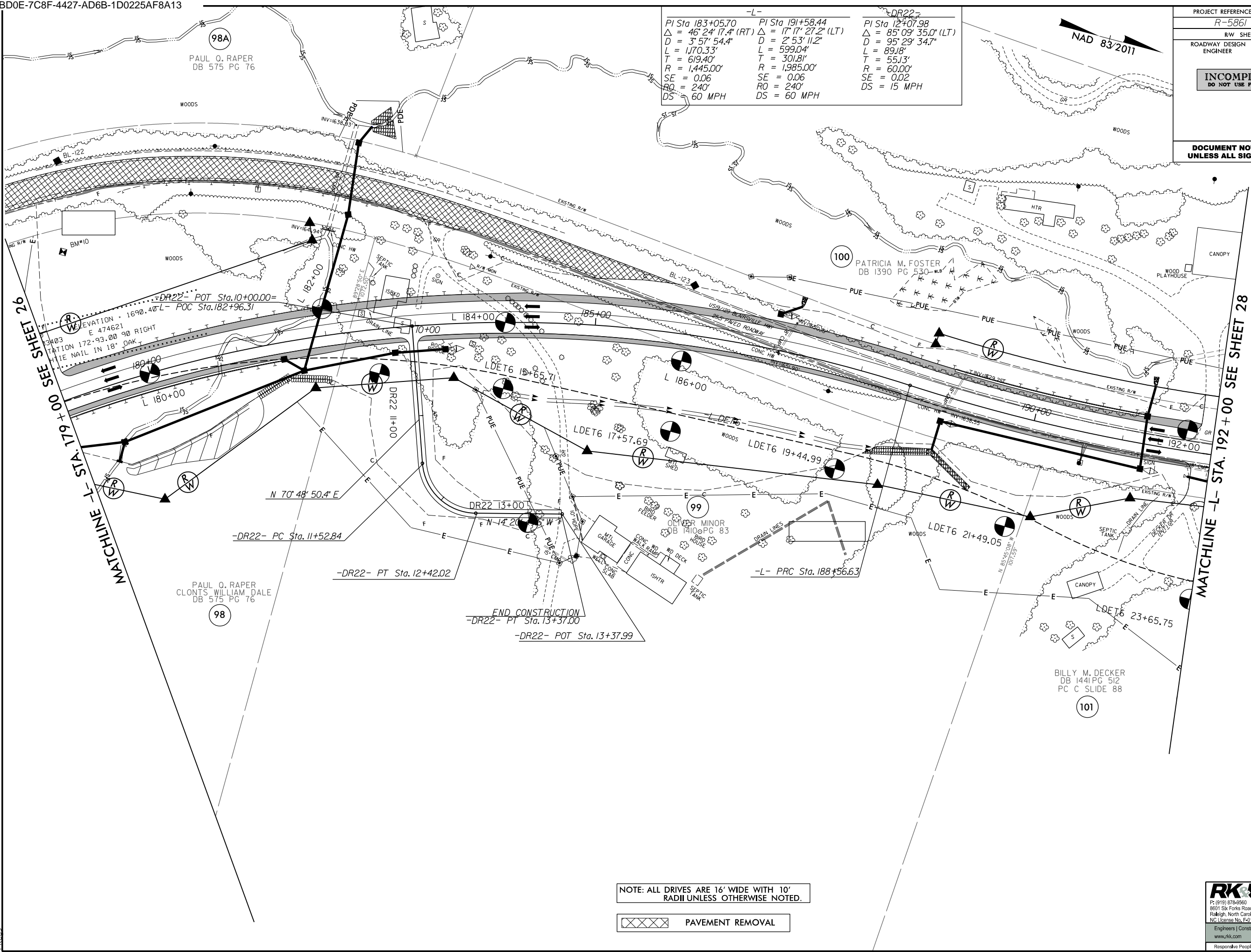
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PROJECT REFERENCE NO. R-586I		SHEET NO. 27	
RW SHEET NO. 17		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			

-L-		DR22
PI Sta 183+05.70	PI Sta 191+58.44	PI Sta 12+07.98
$\Delta = 46^{\circ} 24' 17.4" (RT)$	$\Delta = 17^{\circ} 17' 27.2" (LT)$	$\Delta = 85^{\circ} 09' 35.0" (LT)$
D = 3' 57' 54.4"	D = 2' 53' 11.2"	D = 95' 29' 34.7"
L = 1,170.33'	L = 599.04'	L = 89.18'
T = 619.40'	T = 301.81'	T = 55.13'
R = 1,445.00'	R = 1,985.00'	R = 60.00'
SE = 0.06	SE = 0.06	SE = 0.02
RO = 240'	RO = 240'	DS = 15 MPH
DS = 60 MPH	DS = 60 MPH	



NOTE: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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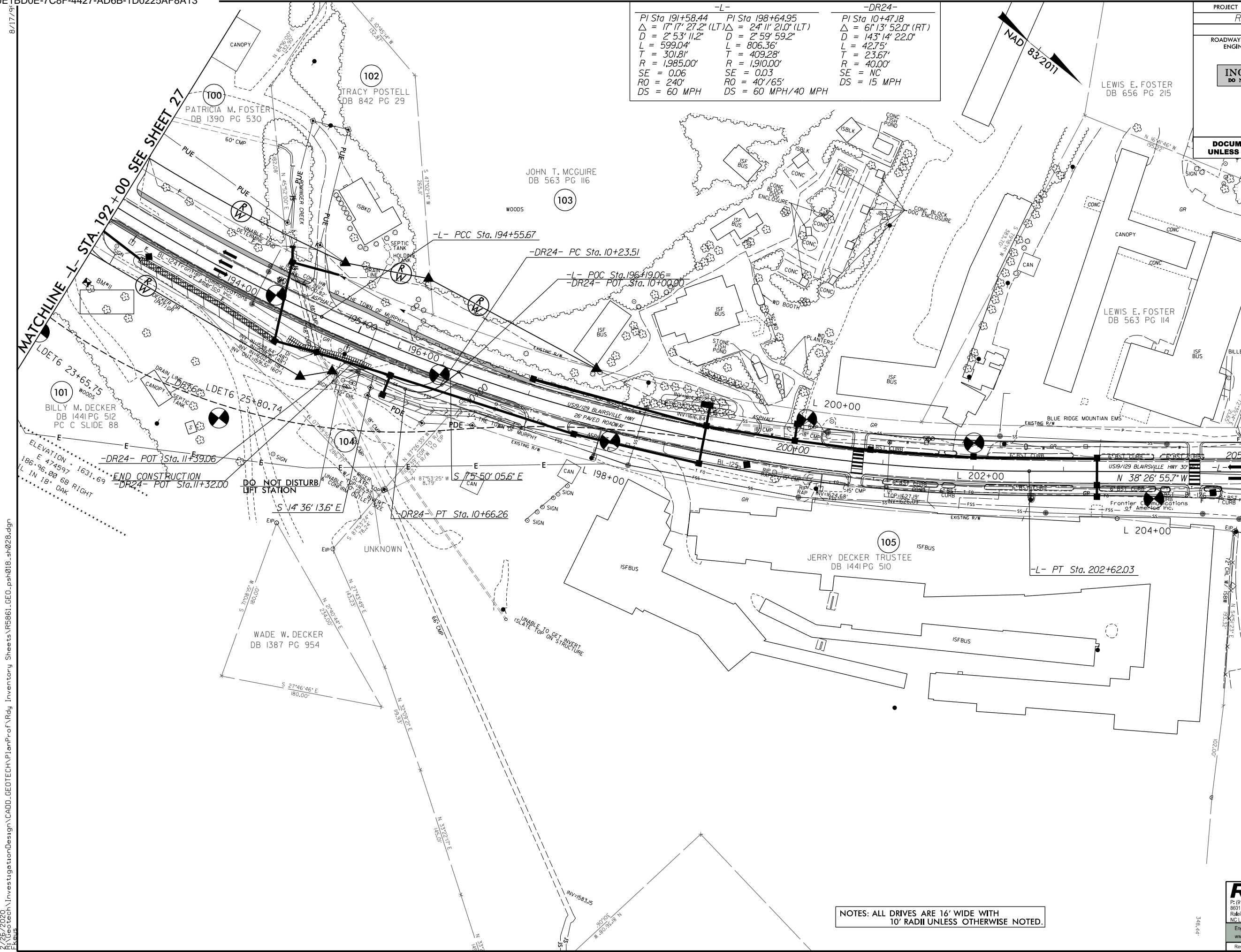
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-L-		-DR24-	
PI Sta 191+58.44	PI Sta 198+64.95	PI Sta 10+47.18	
$\Delta = 17' 17" 27.2"$ (LT)	$\Delta = 24' 11" 21.0"$ (LT)	$\Delta = 6' 13' 52.0"$ (RT)	
D = 2' 53' 11.2"	D = 2' 59' 59.2"	D = 143' 14' 22.0"	
L = 599.04'	L = 806.36'	L = 42.75'	
T = 301.81'	T = 409.28'	T = 23.67'	
R = 1,985.00'	R = 1,910.00'	R = 40.00'	
SE = 0.06	SE = 0.03	SE = NC	
RO = 240'	RO = 40' / 65'	DS = 15 MPH	
DS = 60 MPH	DS = 60 MPH / 40 MPH		

PROJECT REFERENCE NO. R-5861	SHEET NO. 28
R/W SHEET NO. 18	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	

DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED

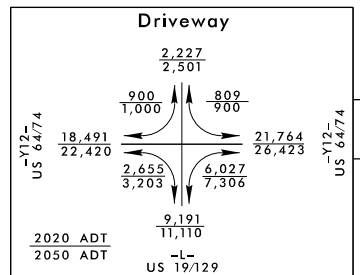


NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

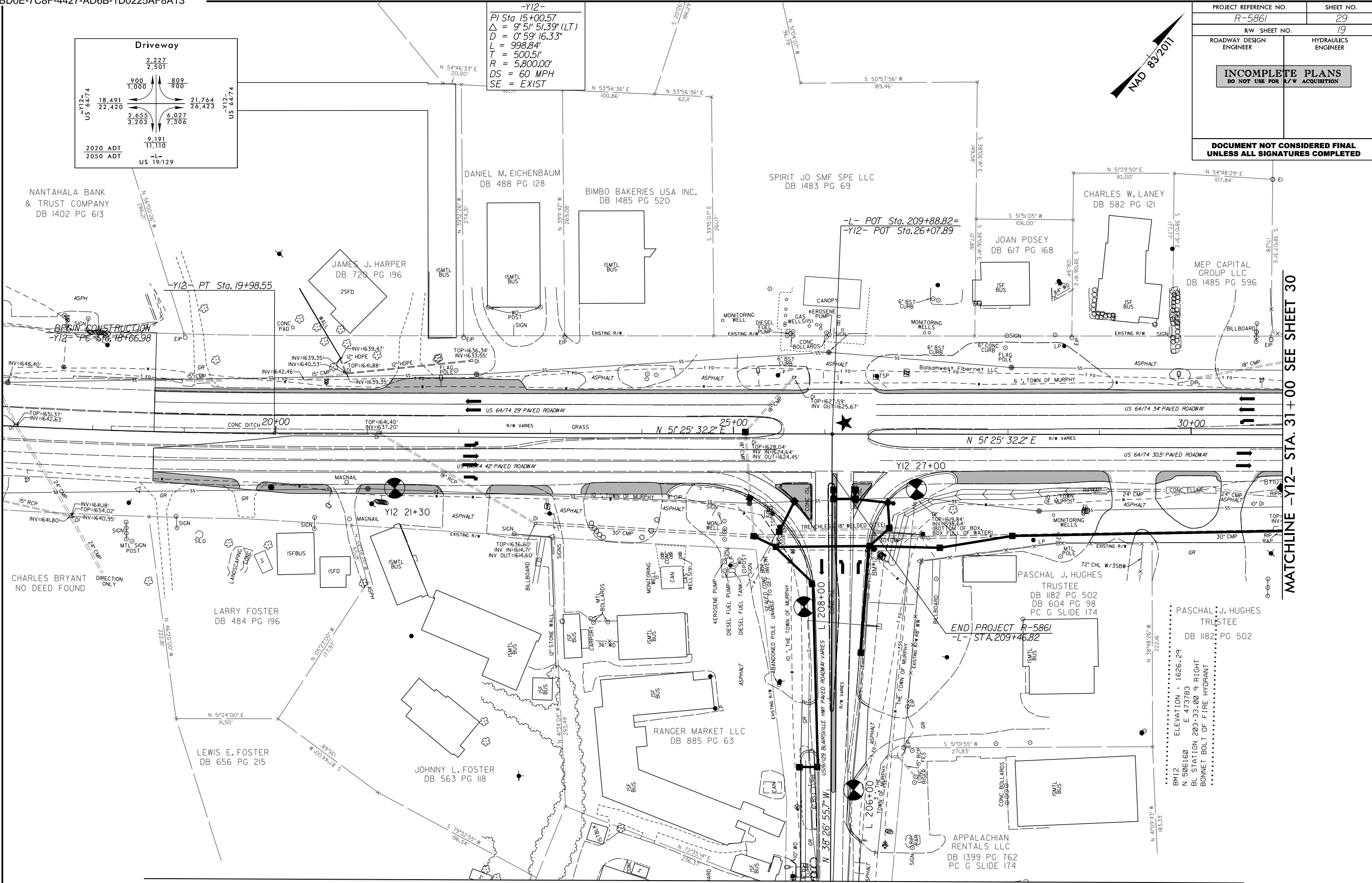
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PROJECT REFERENCE NO. <i>R-5861</i>		SHEET NO. <i>29</i>	
RW SHEET NO. <i>19</i>		HYDRAULICS ENGINEER	
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION			
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED			



-Y12-
 PI Sta 15+00.57
 $\Delta = 9^{\circ} 51' 51.39''$ (LT)
 $D = 0^{\circ} 59' 16.33''$
 $L = 998.84'$
 $T = 500.51'$
 $R = 5,800.00'$
 $DS = 60$ MPH
 $SE = EXIST$



MATCHLINE -Y12- STA. 31+00 SEE SHEET 30

MATCHLINE -L- STA. 205+00 SEE SHEET 28

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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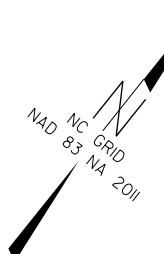
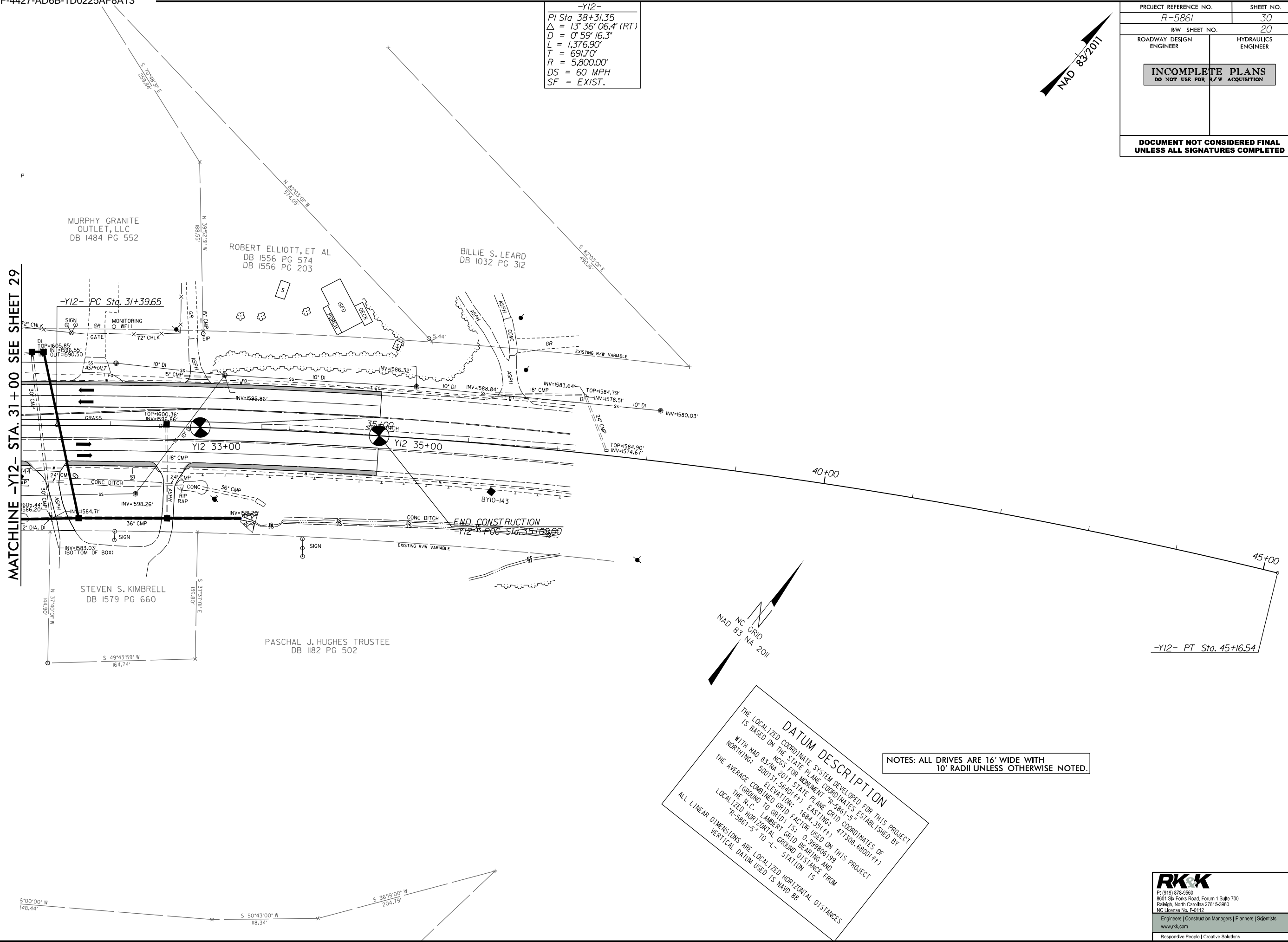
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-Y12-
 PI Sta 38+31.35
 $\Delta = 13^{\circ} 36' 06.4" (RT)$
 $D = 0^{\circ} 59' 16.3"$
 $L = 1,376.90'$
 $T = 691.70'$
 $R = 5,800.00'$
 $DS = 60 \text{ MPH}$
 $SF = \text{EXIST.}$



PROJECT REFERENCE NO. R-5861	SHEET NO. 30
R/W SHEET NO. 20	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

MATCHLINE -Y12- STA. 31+00 SEE SHEET 29



DATUM DESCRIPTION
 THE LOCALIZED COORDINATE SYSTEM DEVELOPED FOR THIS PROJECT IS BASED ON THE STATE PLANE COORDINATES ESTABLISHED BY NCGS FOR MONUMENT "R-5861-S"
 WITH NAD 83/NA 2011 STATE PLANE GRID COORDINATES OF
 NORTHING: 500131.5640(F+)
 ELEVATION: 1684.35(F+)
 THE AVERAGE COMBINED GRID FACTOR USED ON THIS PROJECT (GROUND TO GRID) IS: 0.999806199
 THE N.C. LAMBERT GRID BEARING AND LOCALIZED HORIZONTAL GROUND DISTANCE FROM "R-5861-S" TO "L" STATION IS
 ALL LINEAR DIMENSIONS ARE LOCALIZED HORIZONTAL DISTANCES
 VERTICAL DATUM USED IS NAVD 88

NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

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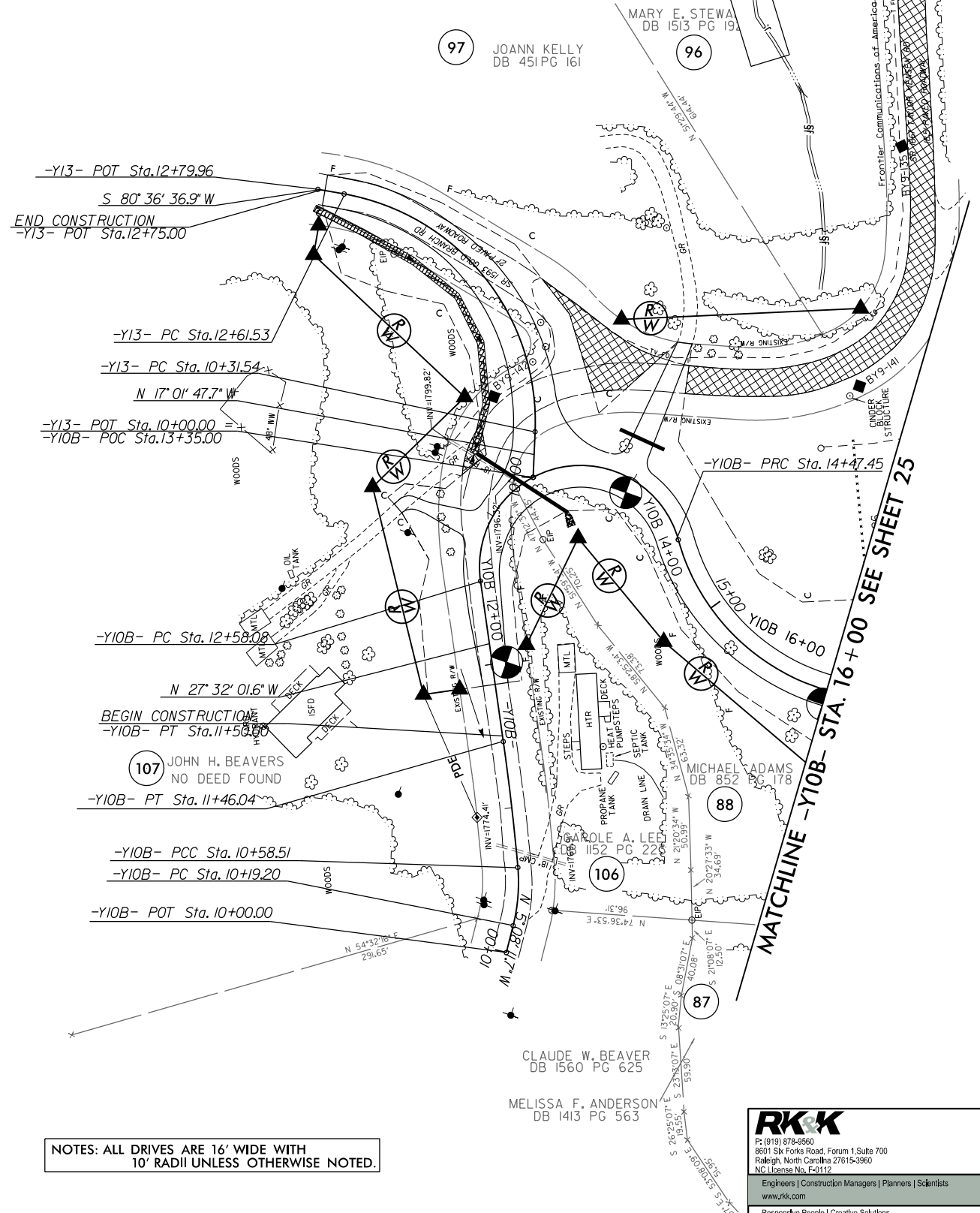
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REVISIONS

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-Y10B-		-Y13-		
PI Sta 10+39.67	PI Sta 11+02.29	PI Sta 13+52.77	PI Sta 18+30.42	PI Sta 11+71.51
$\Delta = 19^\circ 21' 25.9" (LT)$	$\Delta = 3^\circ 02' 24.0" (LT)$	$\Delta = 172^\circ 38' 45.0" (RT)$	$\Delta = 137^\circ 13' 19.0" (LT)$	$\Delta = 82^\circ 21' 35.4" (LT)$
$D = 49' 14' 55.1"$	$D = 3' 28' 22.8"$	$D = 91' 10' 09.8"$	$D = 38' 11' 49.9"$	$D = 35' 48' 35.5"$
$L = 39.31'$	$L = 87.53'$	$L = 189.37'$	$L = 359.25'$	$L = 229.99'$
$T = 20.47'$	$T = 43.78'$	$T = 1089.23'$	$T = 382.97'$	$T = 139.97'$
$R = 120.00'$	$R = 1650.00'$	$R = 70.00'$	$R = 150.00'$	$R = 160.00'$
		$SE = 0.06$	$SE = 0.06$	$SE = 0.06$
		$RO = 120'$	$RO = 100'$	$RO = 90'$
		$DS = 15 MPH$	$DS = 25 MPH$	$DS = 20 MPH$

PROJECT REFERENCE NO. R-5861	SHEET NO. 31
R/W SHEET NO. 21	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR R/W ACQUISITION	
DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED	

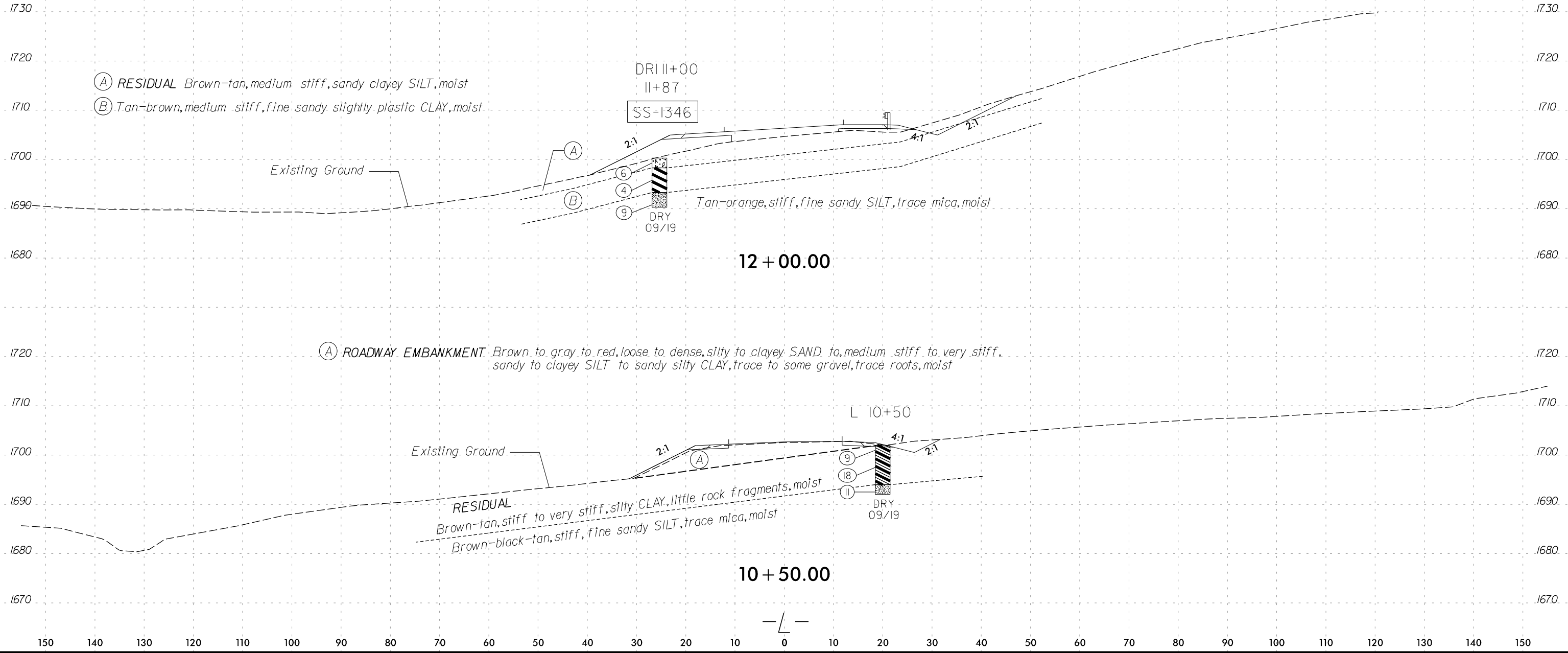


NOTES: ALL DRIVES ARE 16' WIDE WITH 10' RADII UNLESS OTHERWISE NOTED.

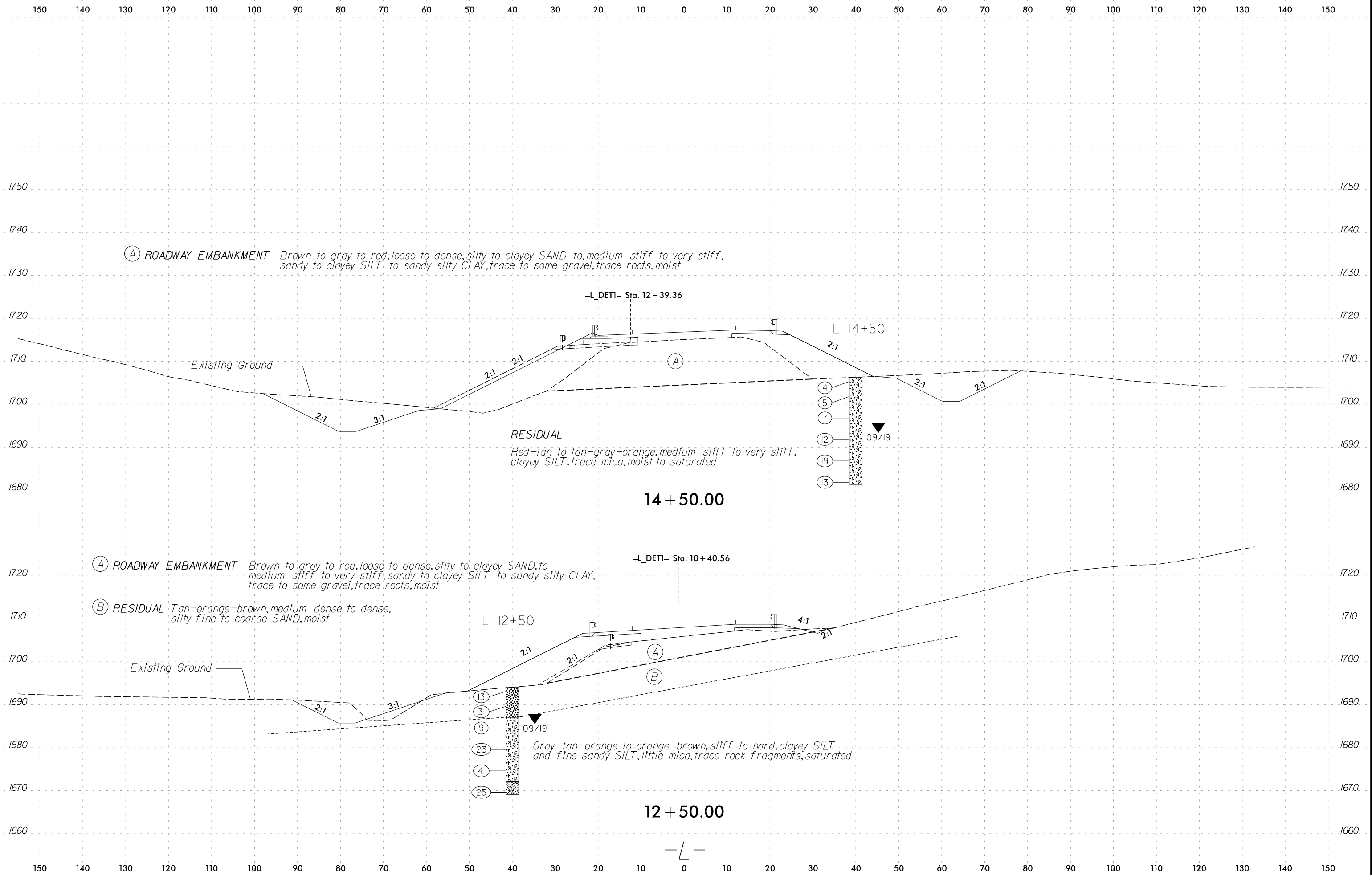
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 Raleigh, North Carolina 27615-3960
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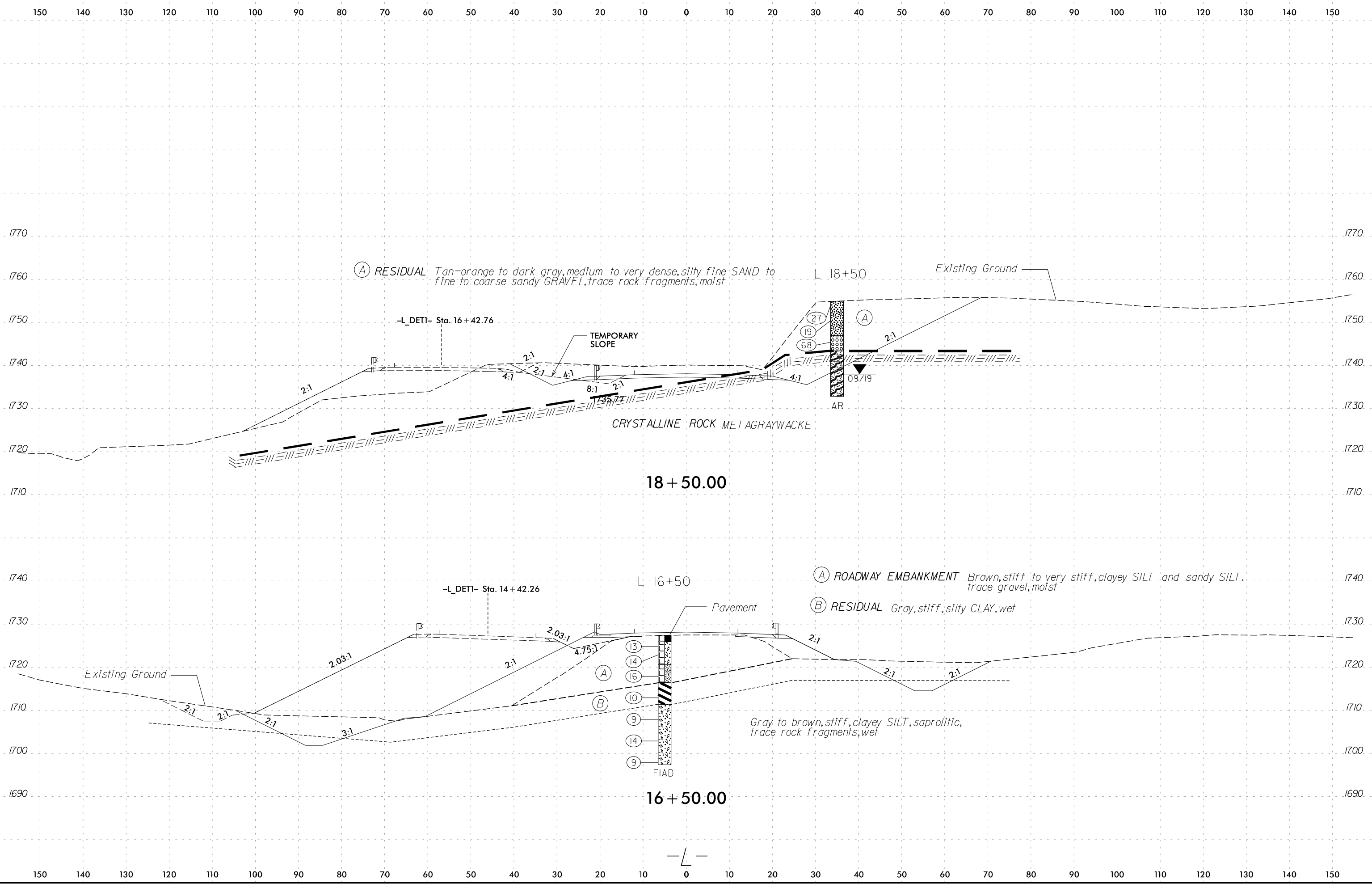
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1346	11+87	25' LT	3.5-5.0	A-7-6 (7)	41	12	8	37	19	36	98	94	62.3	24.3	-



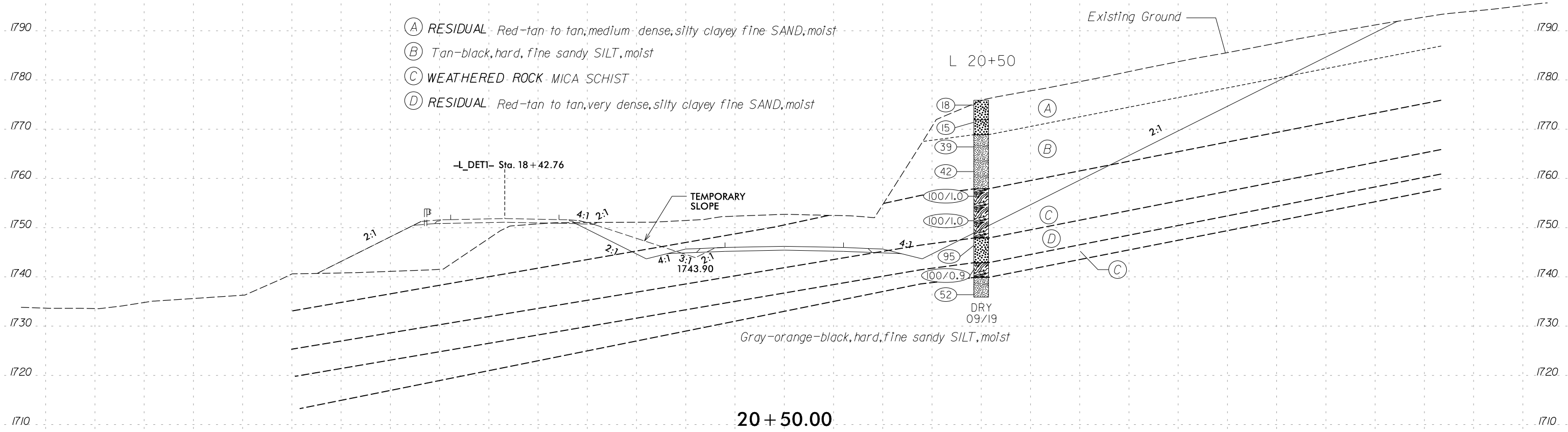
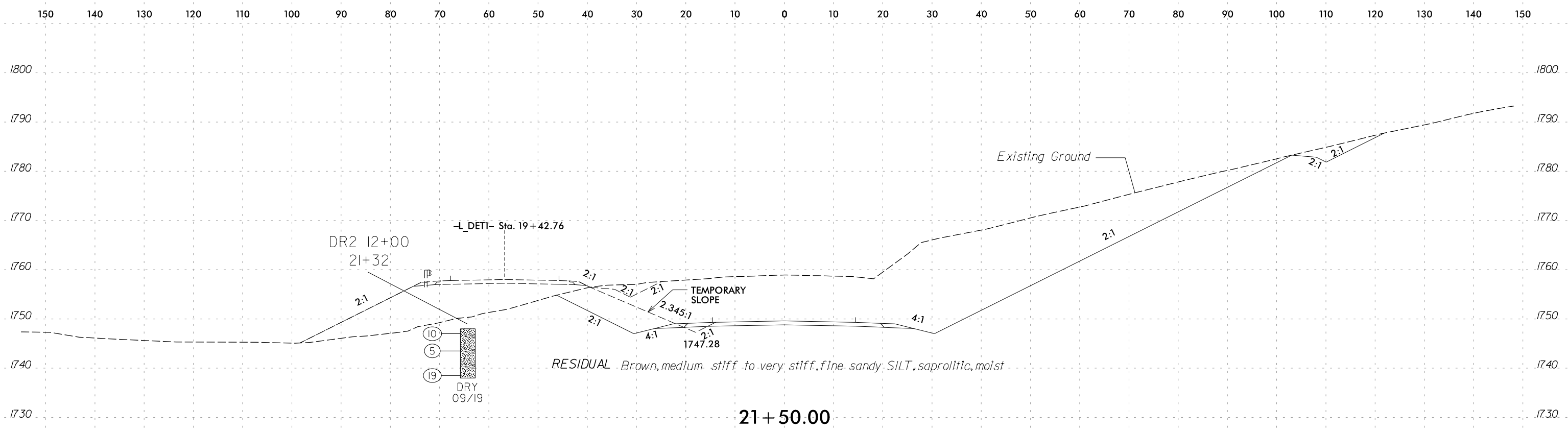
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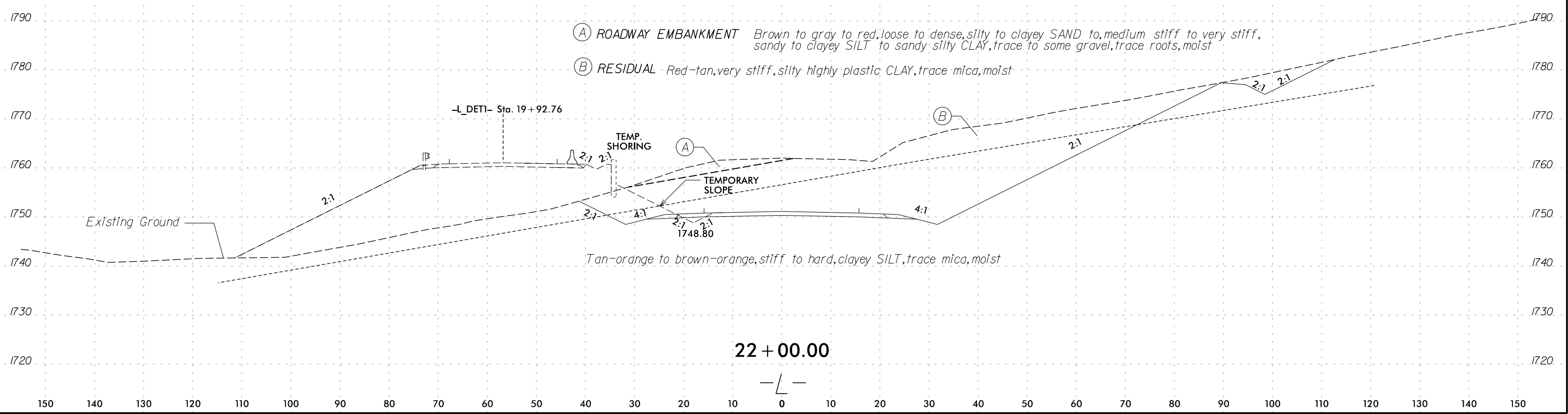
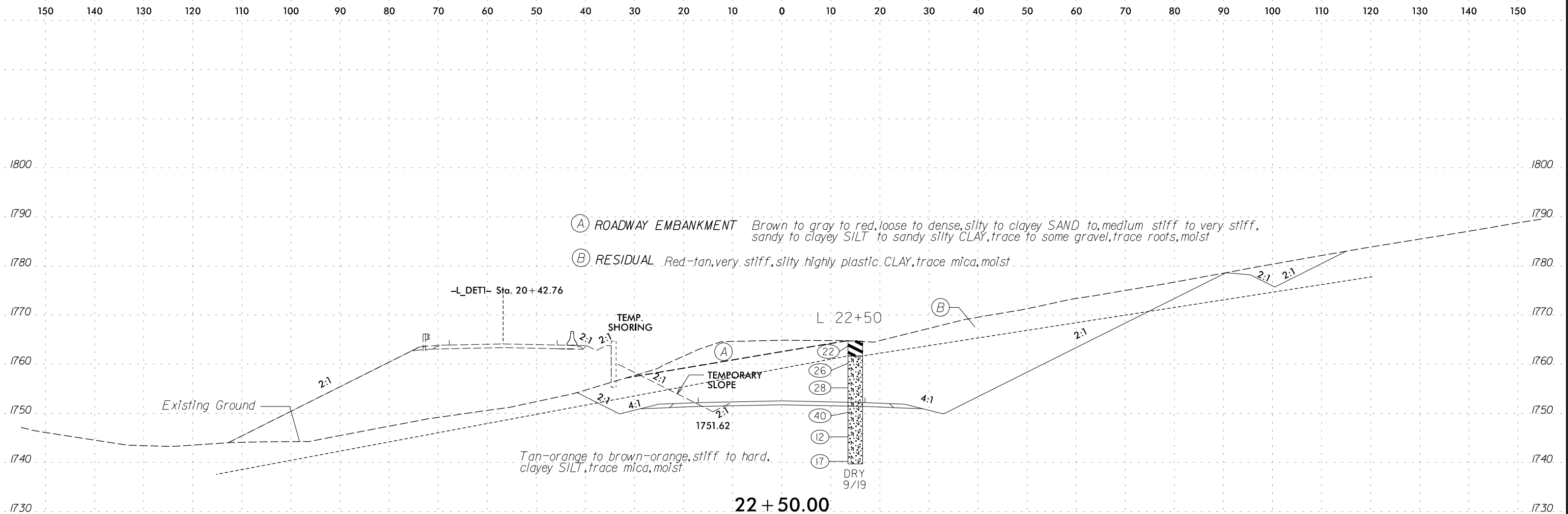
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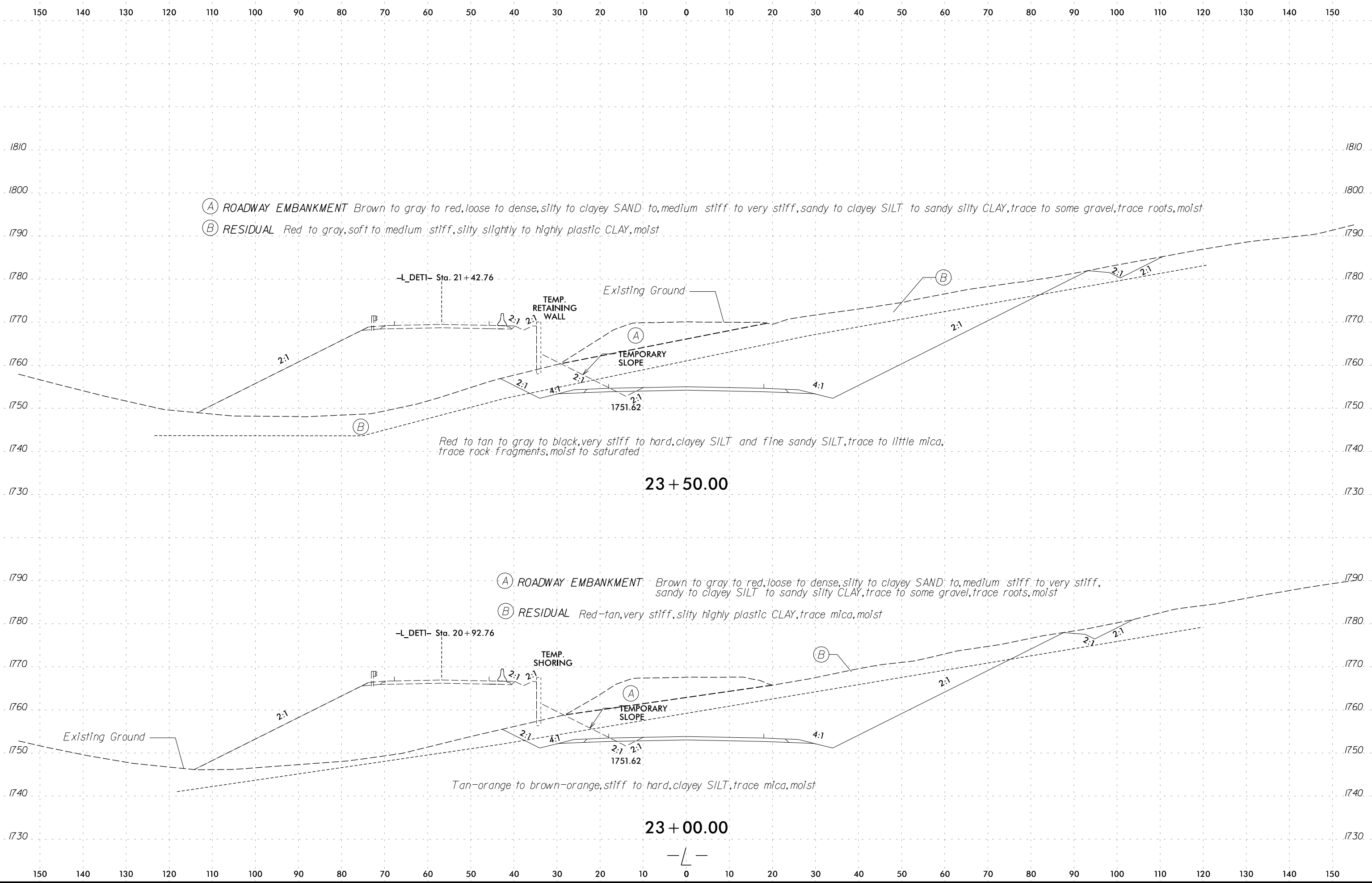
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(A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*

(B) RESIDUAL *Red to gray, soft to medium stiff, silty slightly to highly plastic CLAY, moist*

Red to tan to gray to black, very stiff to hard, clayey SILT and fine sandy SILT, trace to little mica, trace rock fragments, moist to saturated

23 + 50.00

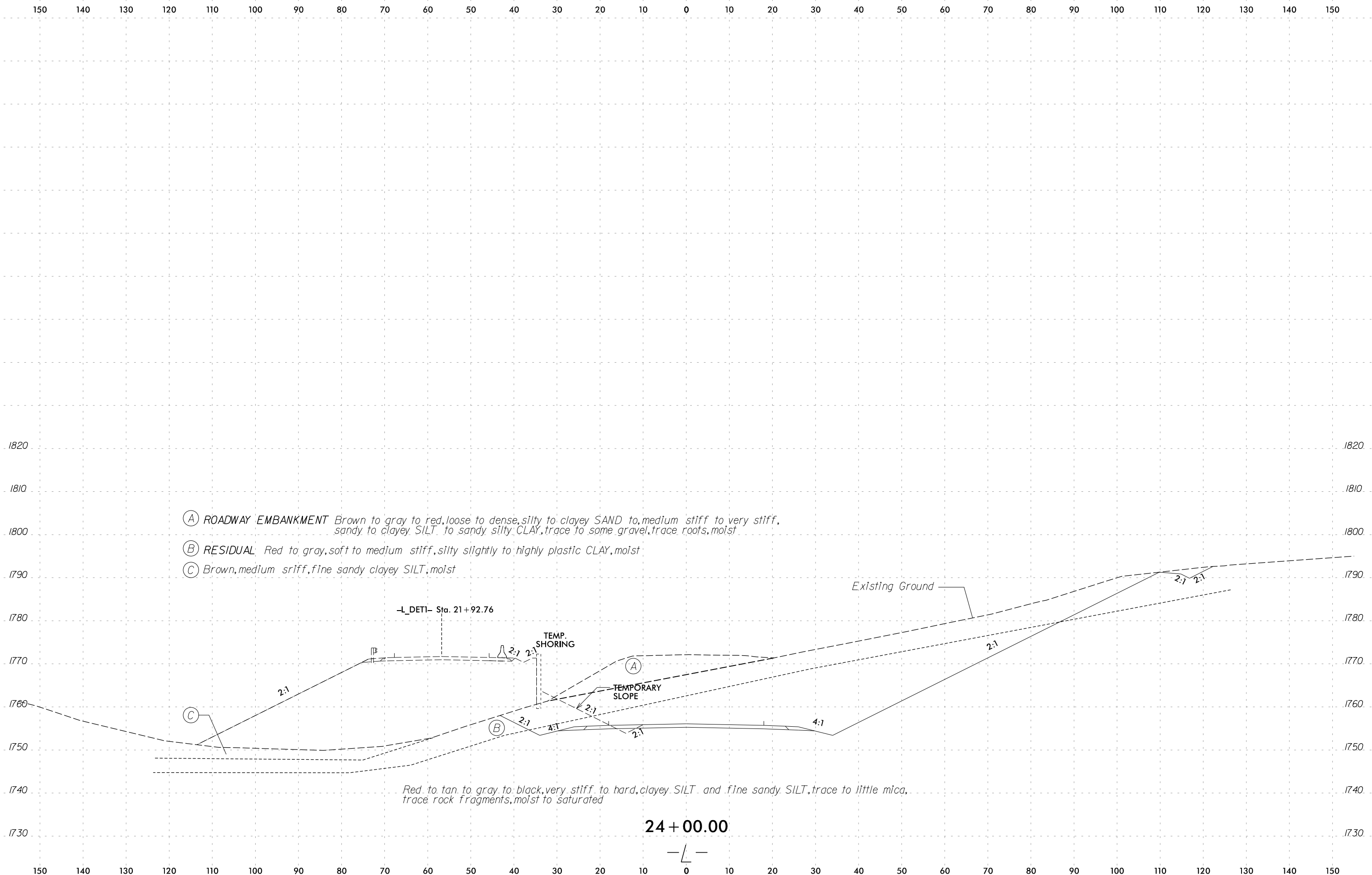
(A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*

(B) RESIDUAL *Red-tan, very stiff, silty highly plastic CLAY, trace mica, moist*

Tan-orange to brown-orange, stiff to hard, clayey SILT, trace mica, moist

23 + 00.00

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- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Red to gray, soft to medium stiff, silty slightly to highly plastic CLAY, moist*
- (C) *Brown, medium stiff, fine sandy clayey SILT, moist*

-L DETI- Sta. 21+92.76

TEMP. SHORING

TEMPORARY SLOPE

Existing Ground

Red to tan to gray to black, very stiff to hard, clayey SILT and fine sandy SILT, trace to little mica, trace rock fragments, moist to saturated

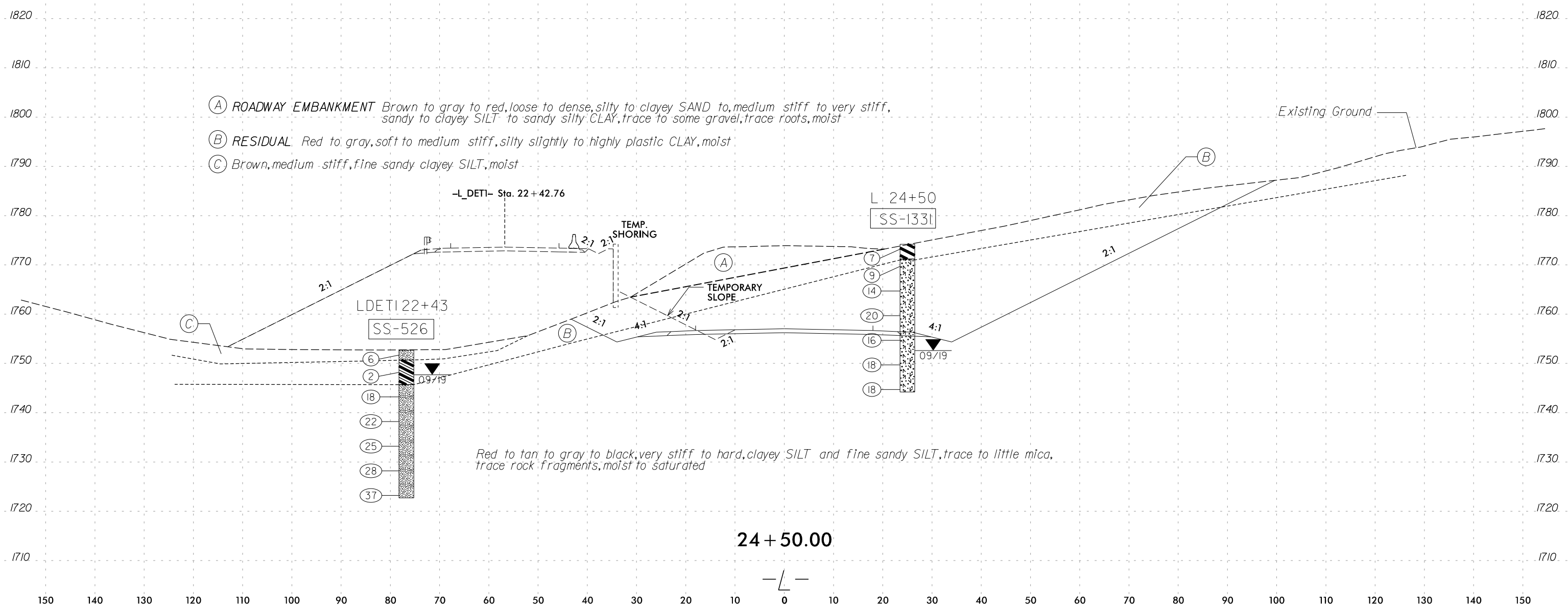
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P. Keijs

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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1331	24+50	25' RT	0.0-1.5	A-7-5 (26)	64	30	3	26	16	55	100	99	77.9	33	-
SS-526	24+50	77' LT	3.5-5.0	A-6 (5)	35	11	7	42	17	34	100	98	61.2	29.2	-

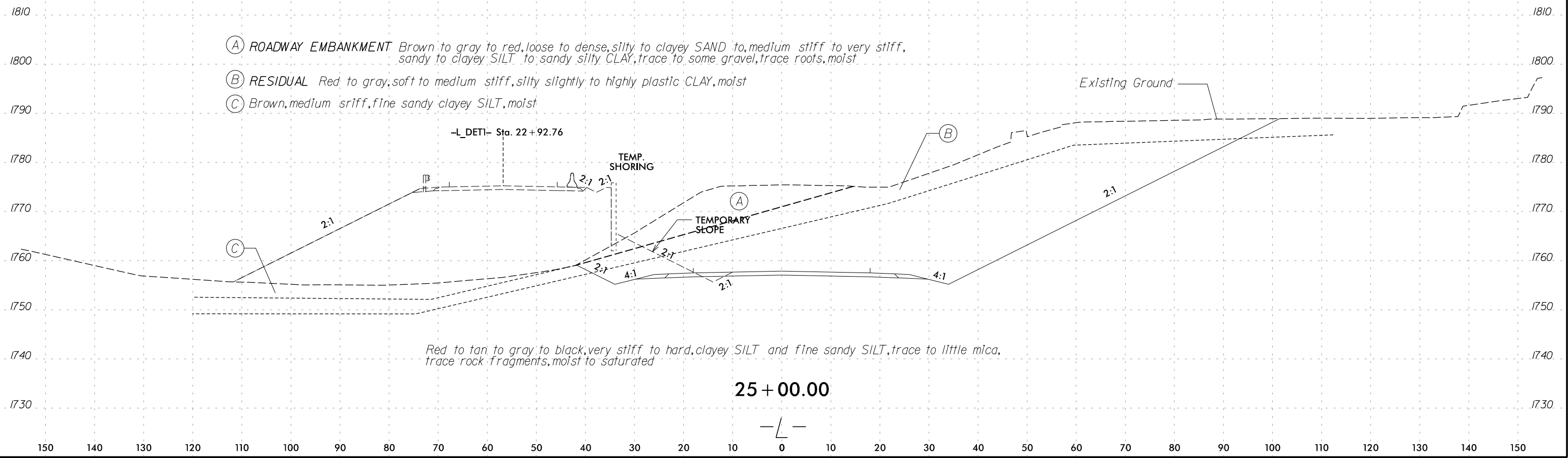
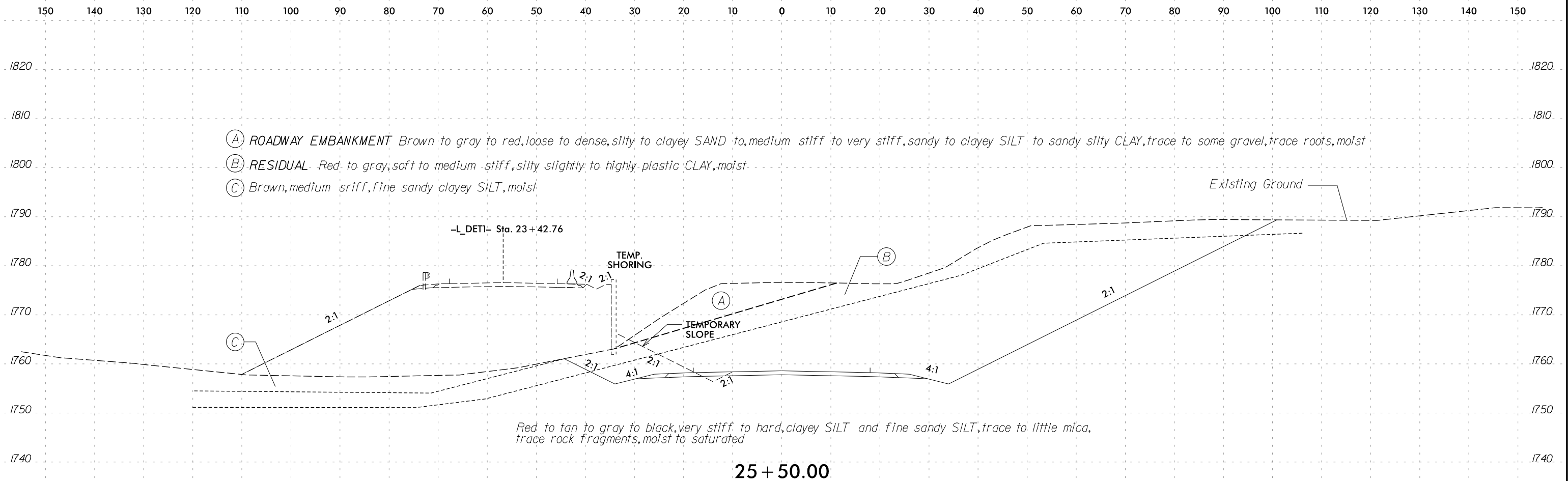


- (A) ROADWAY EMBANKMENT Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist
- (B) RESIDUAL Red to gray, soft to medium stiff, silty slightly to highly plastic CLAY, moist
- (C) Brown, medium stiff, fine sandy clayey SILT, moist

Red to tan to gray to black, very stiff to hard, clayey SILT and fine sandy SILT, trace to little mica, trace rock fragments, moist to saturated

24 + 50.00

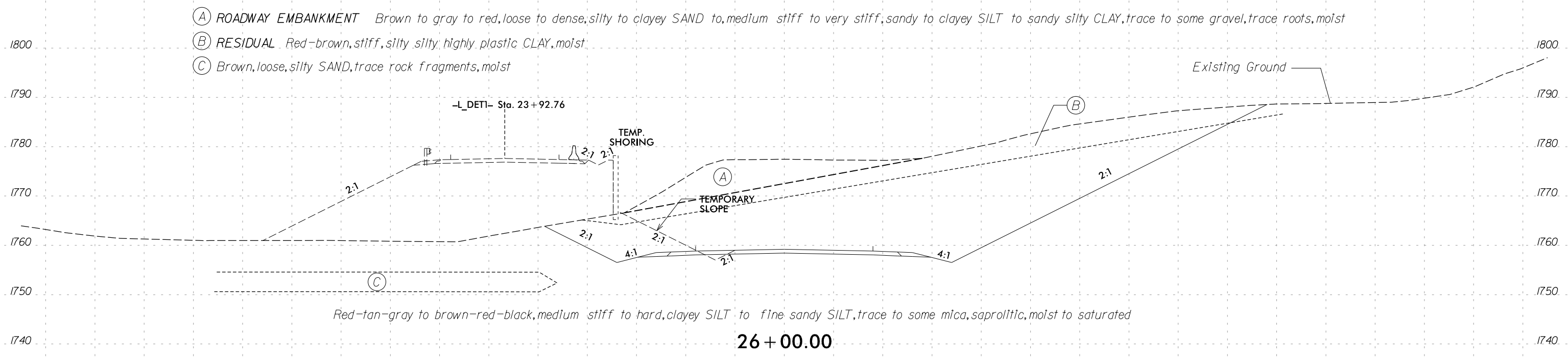
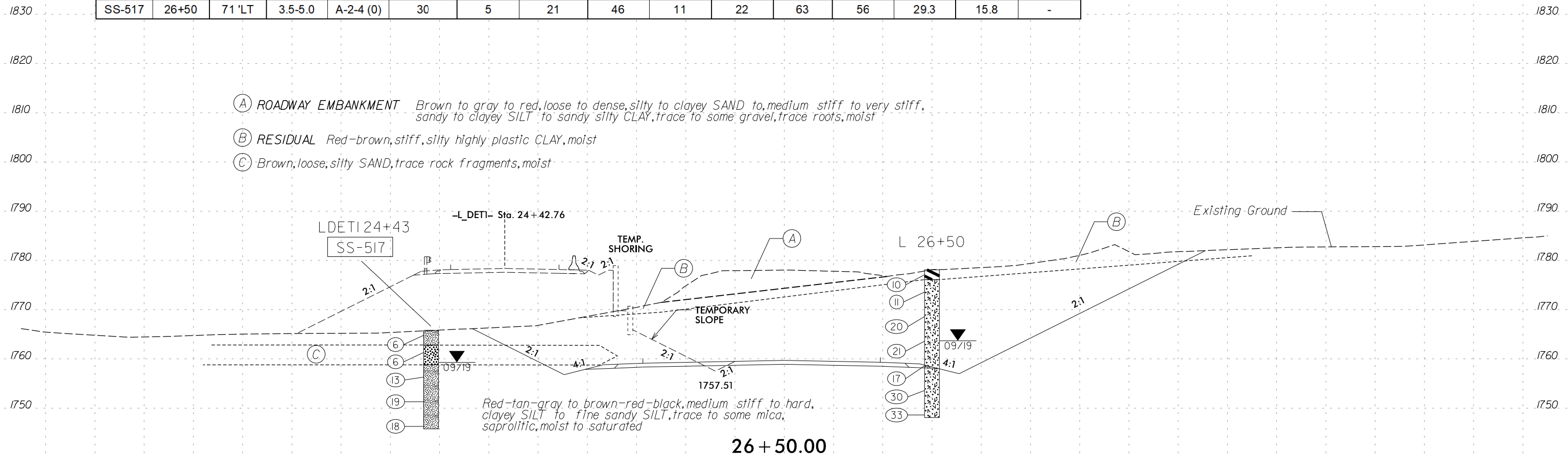
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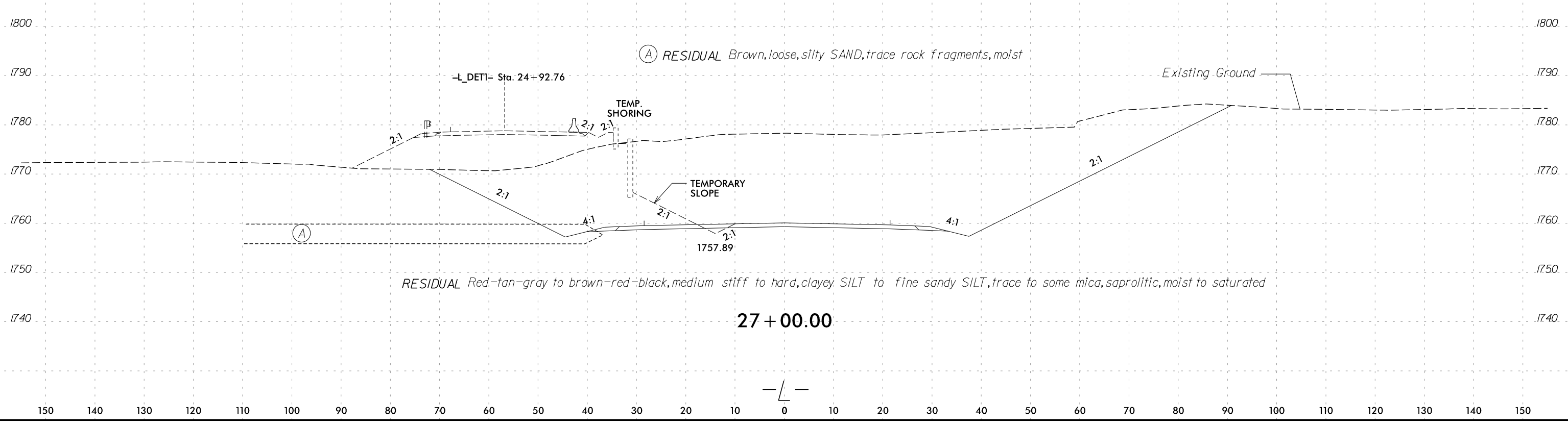
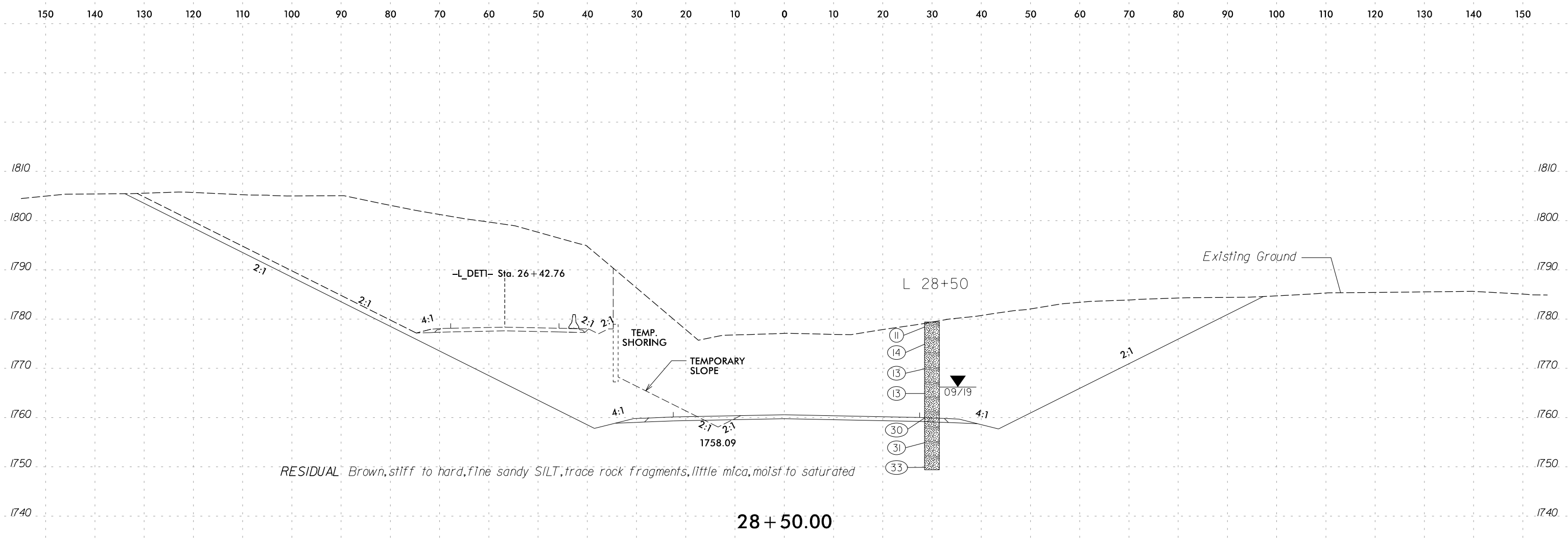
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-517	26+50	71 'LT	3.5-5.0	A-2-4 (0)	30	5	21	46	11	22	63	56	29.3	15.8	-



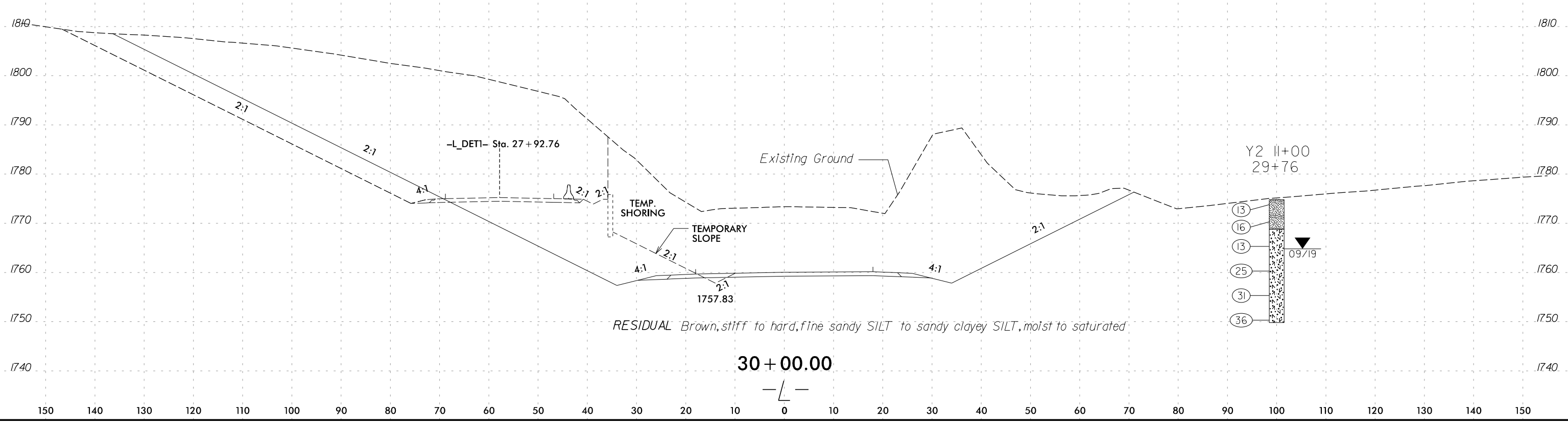
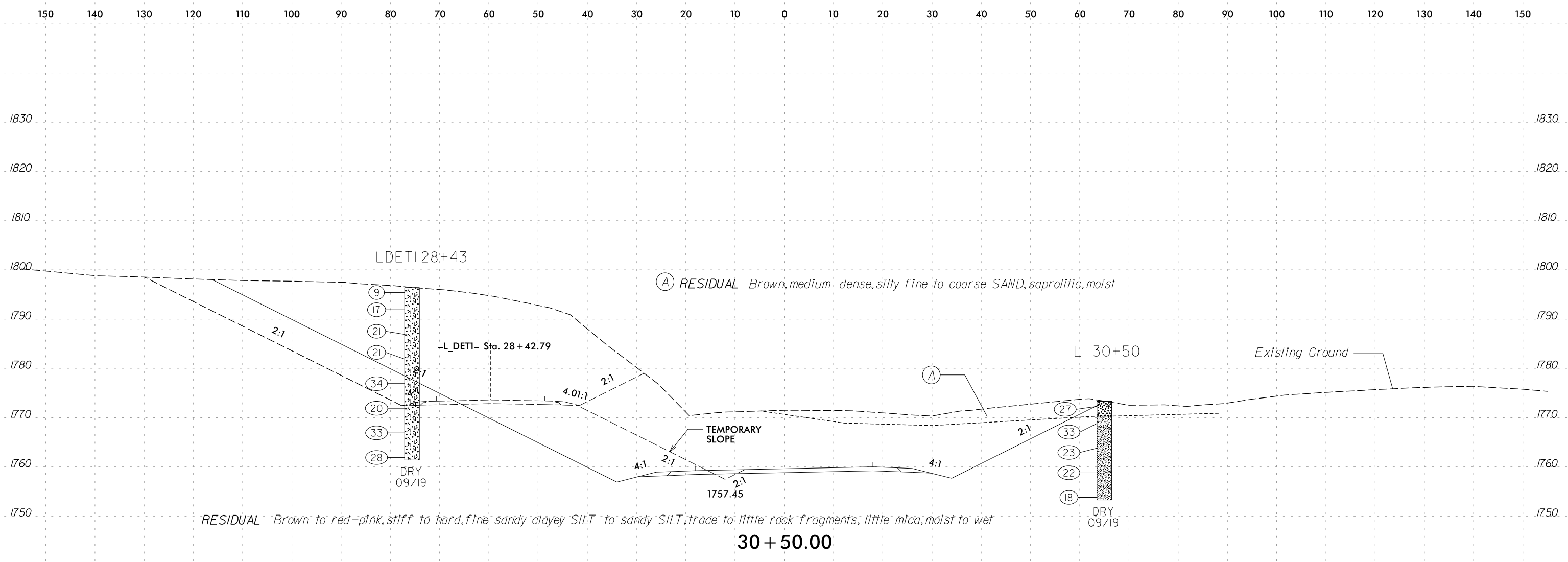
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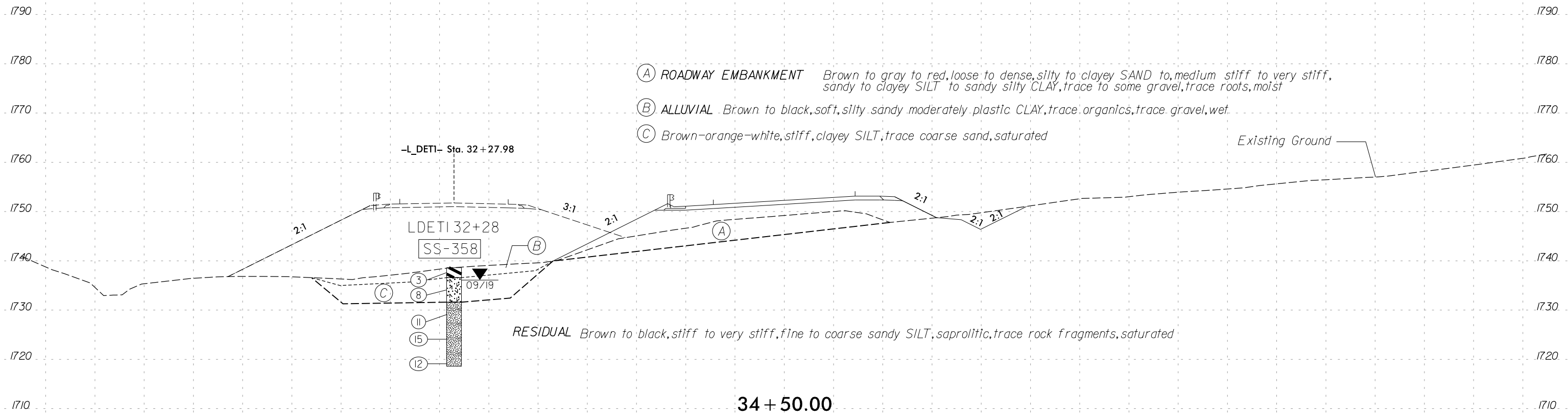
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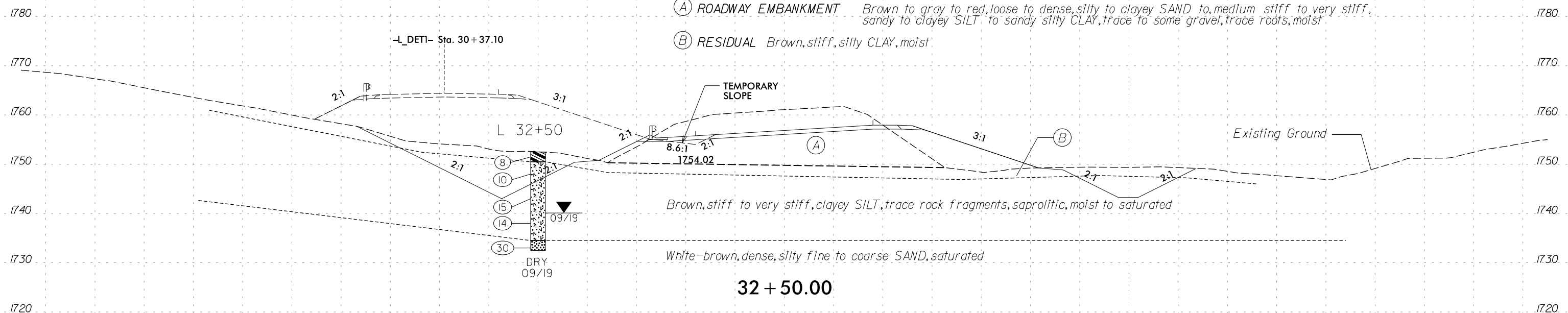
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-358	34+50	67' LT	0.0-1.5	A-7-5 (6)	58	17	19	37	23	21	90	80	47.1	44.2	-

- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) ALLUVIAL *Brown to black, soft, silty sandy moderately plastic CLAY, trace organics, trace gravel, wet*
- (C) *Brown-orange-white, stiff, clayey SILT, trace coarse sand, saturated*



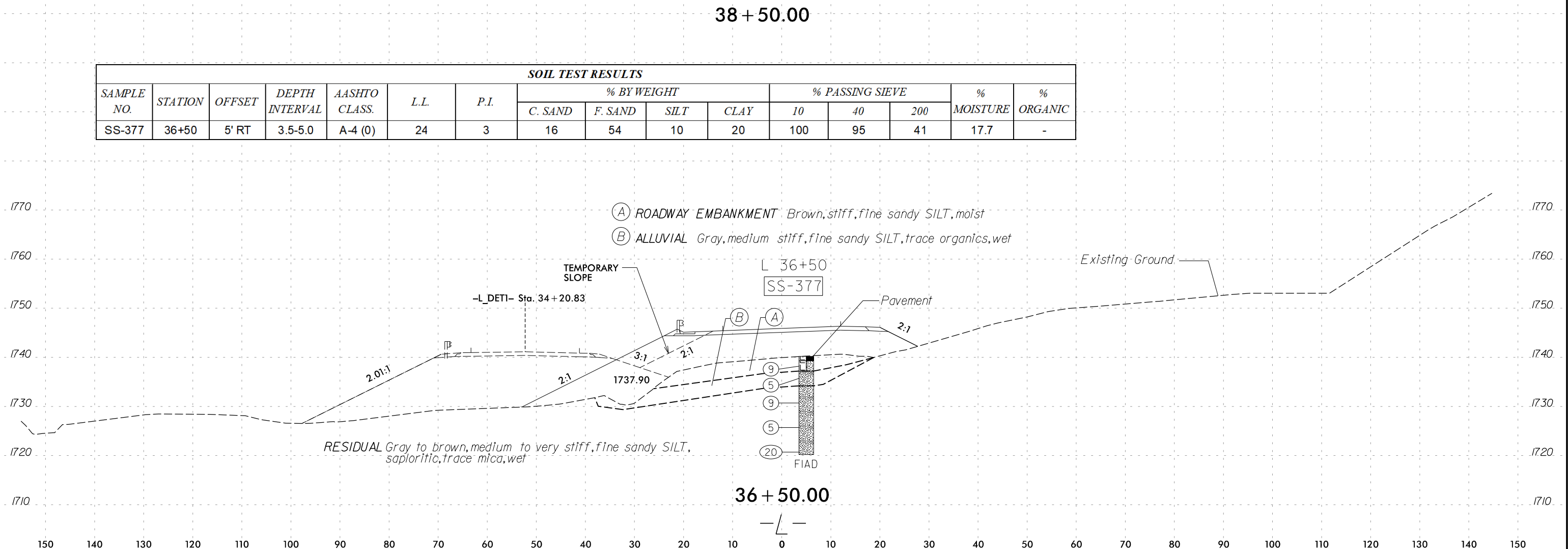
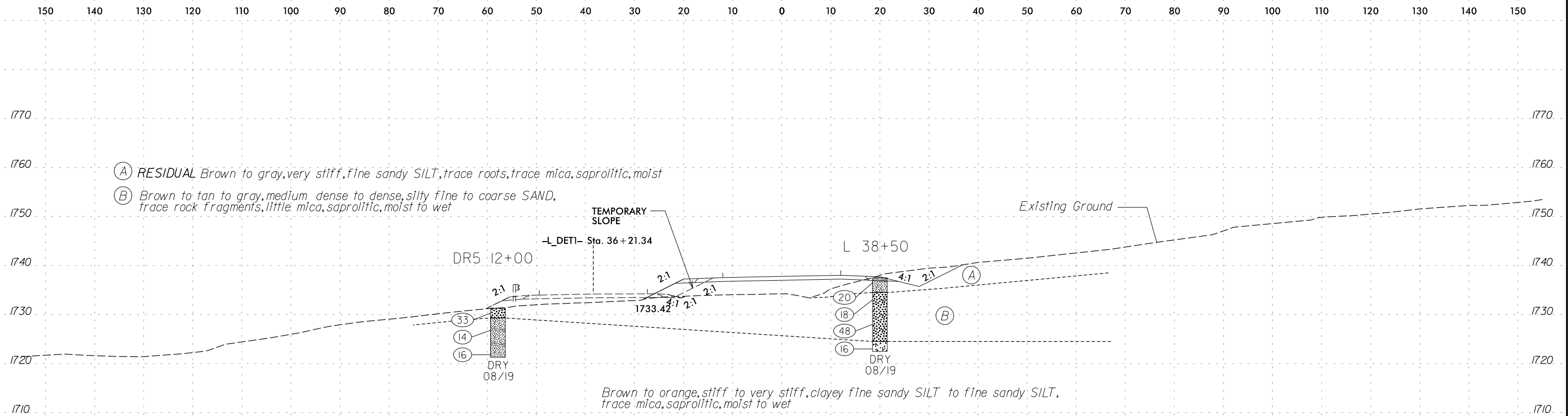
34 + 50.00

- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown, stiff, silty CLAY, moist*

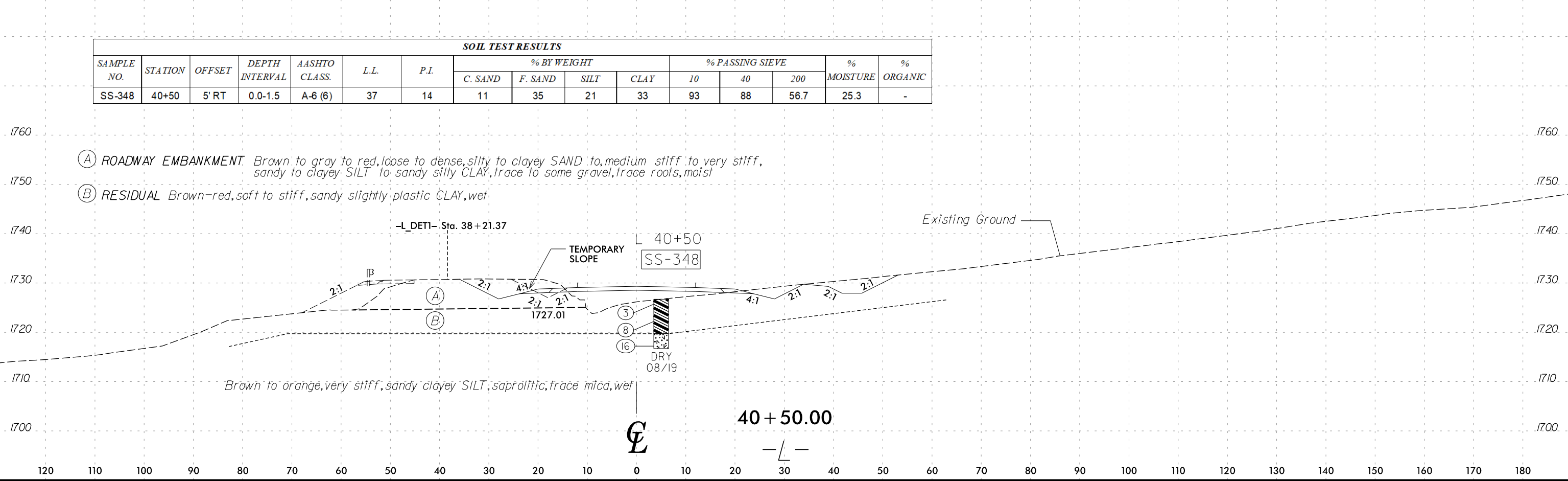
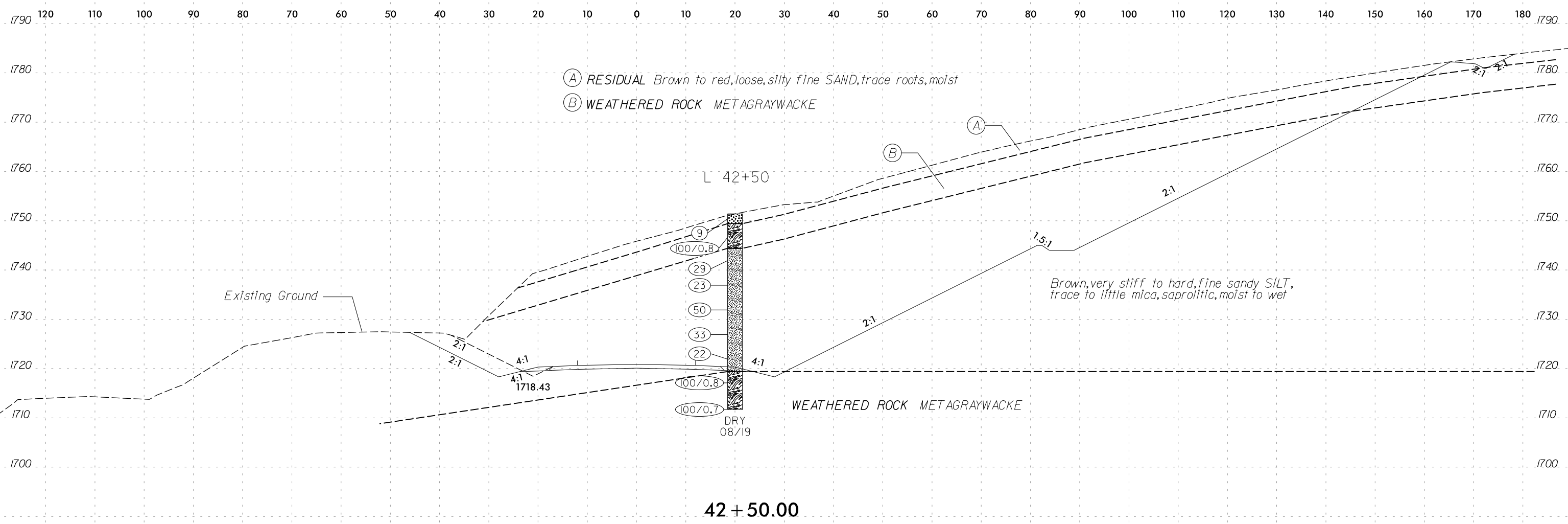


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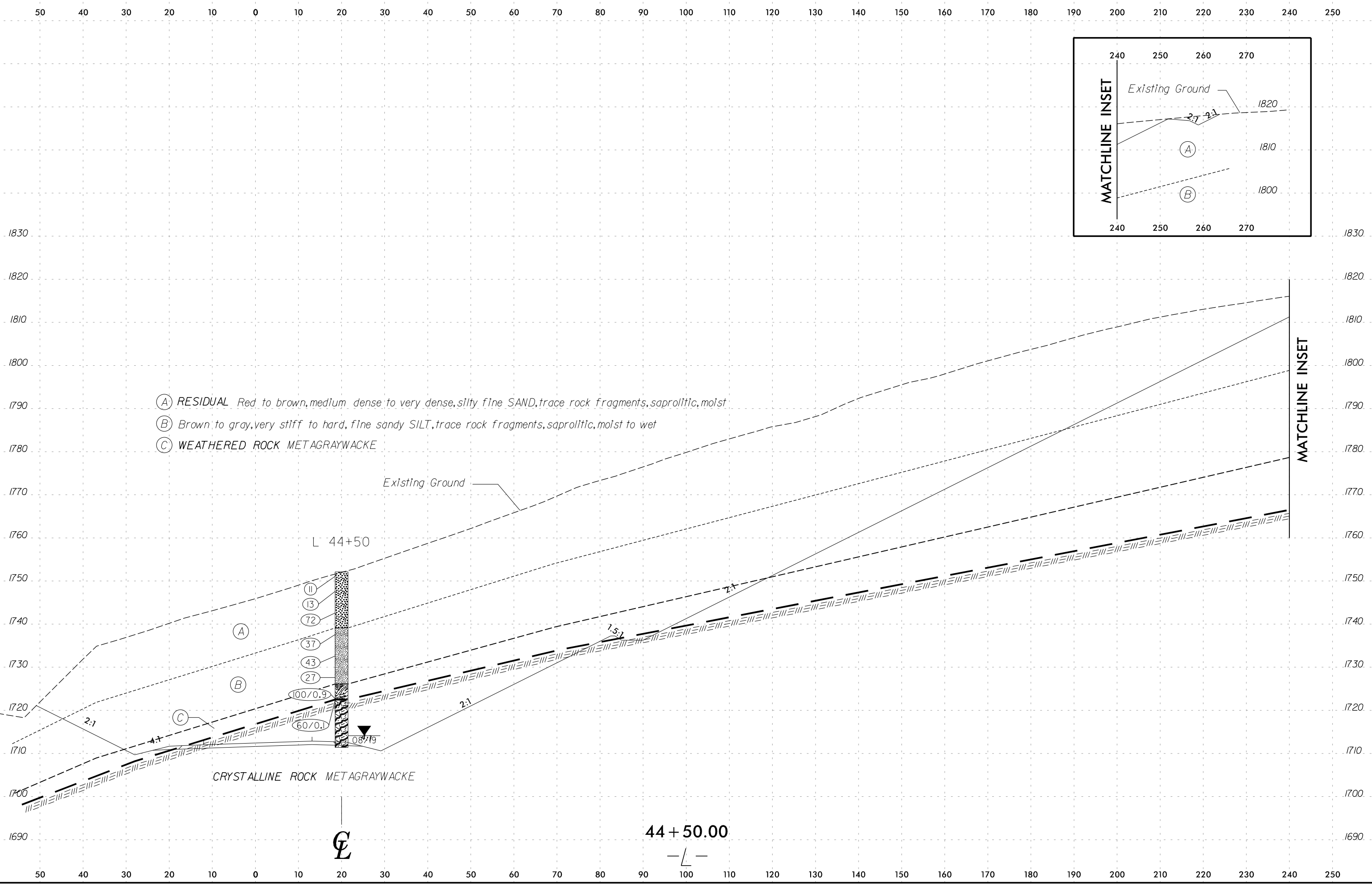
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- (A) RESIDUAL Red to brown, medium dense to very dense, silty fine SAND, trace rock fragments, saprolitic, moist
- (B) Brown to gray, very stiff to hard, fine sandy SILT, trace rock fragments, saprolitic, moist to wet
- (C) WEATHERED ROCK METAGRAYWACKE

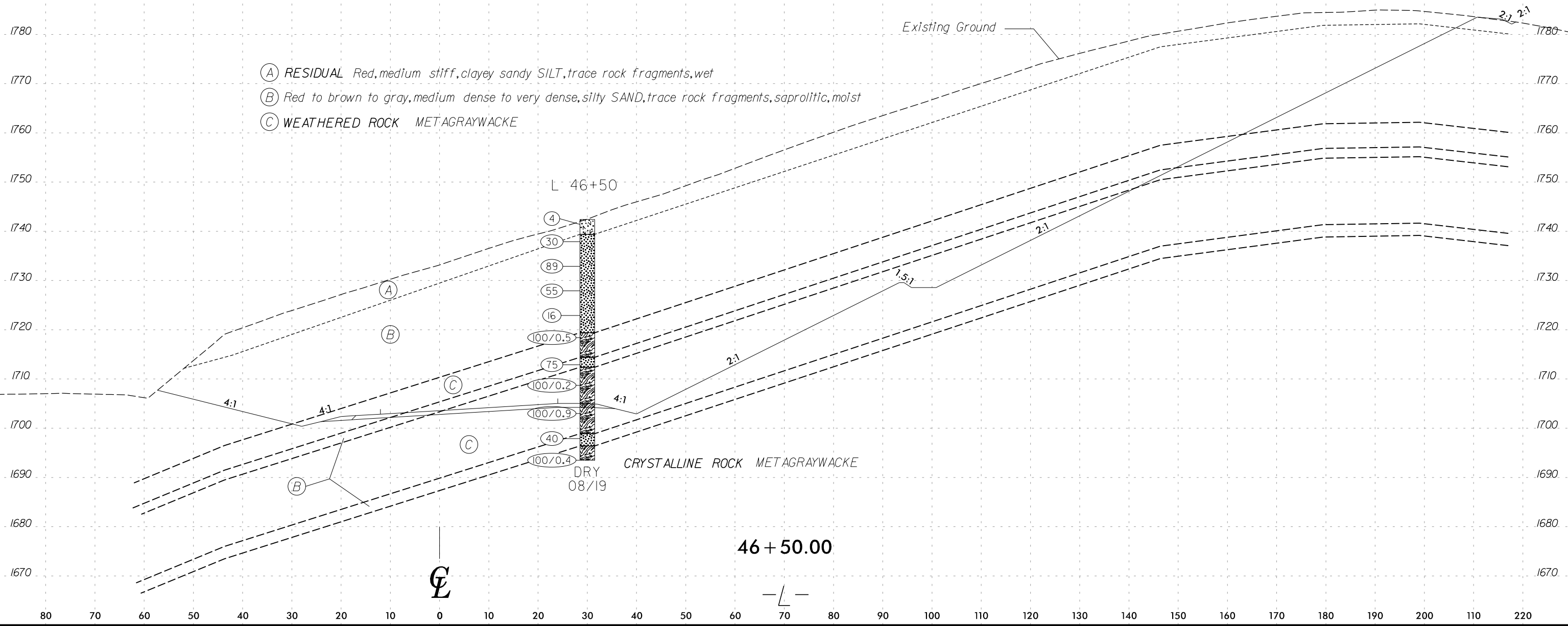
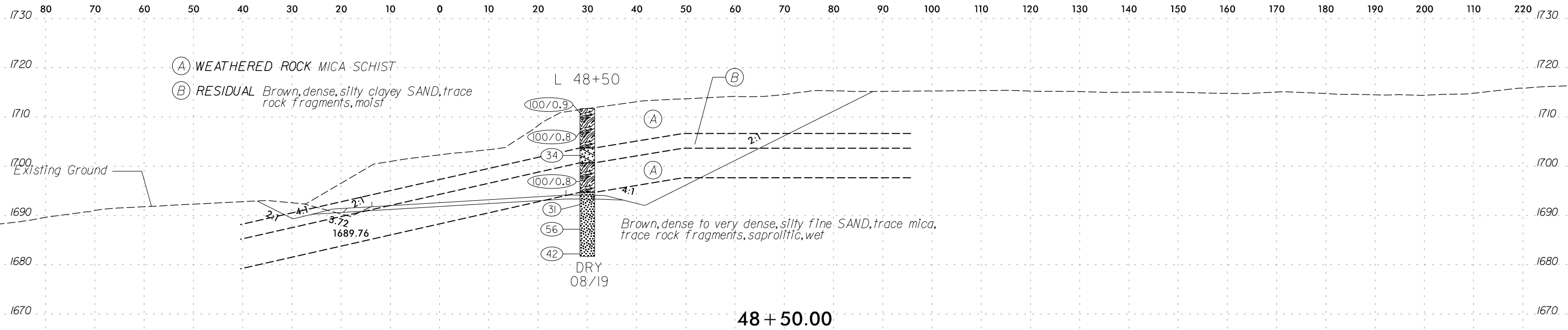
CRYSTALLINE ROCK METAGRAYWACKE

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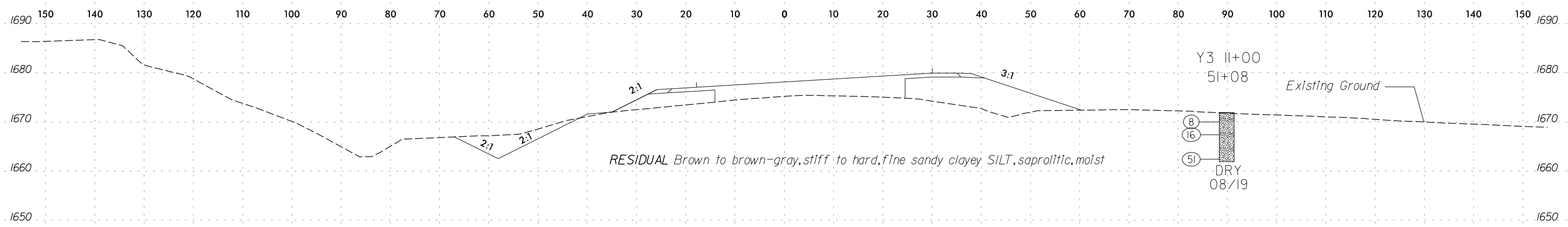
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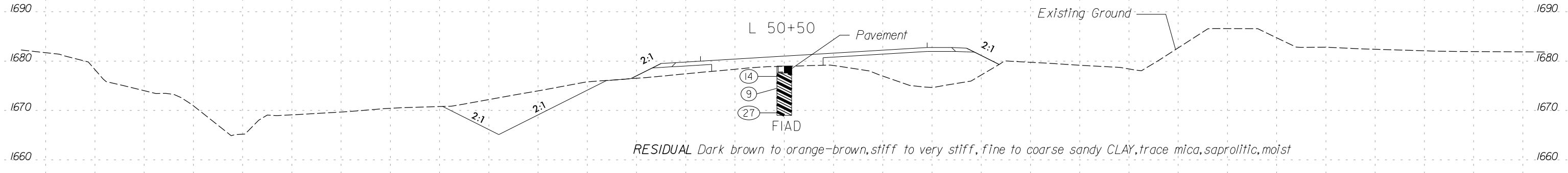
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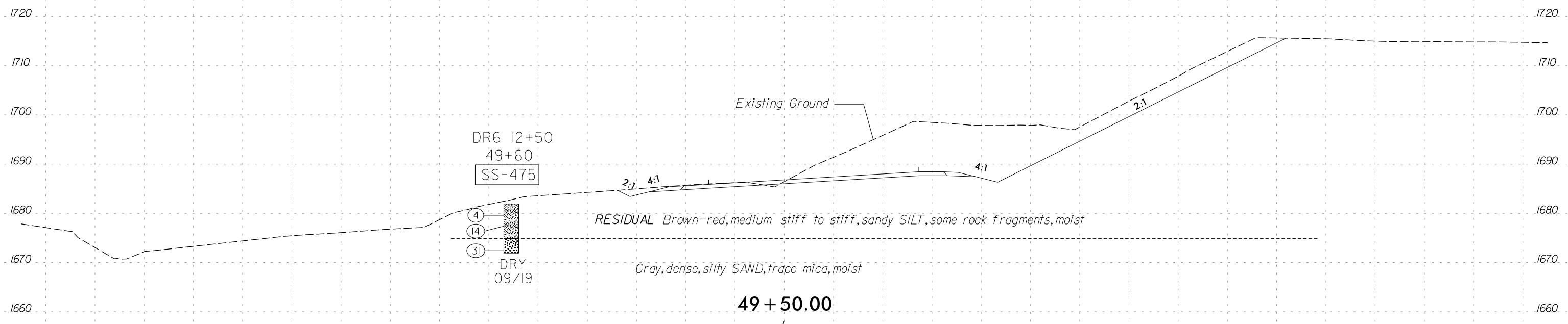


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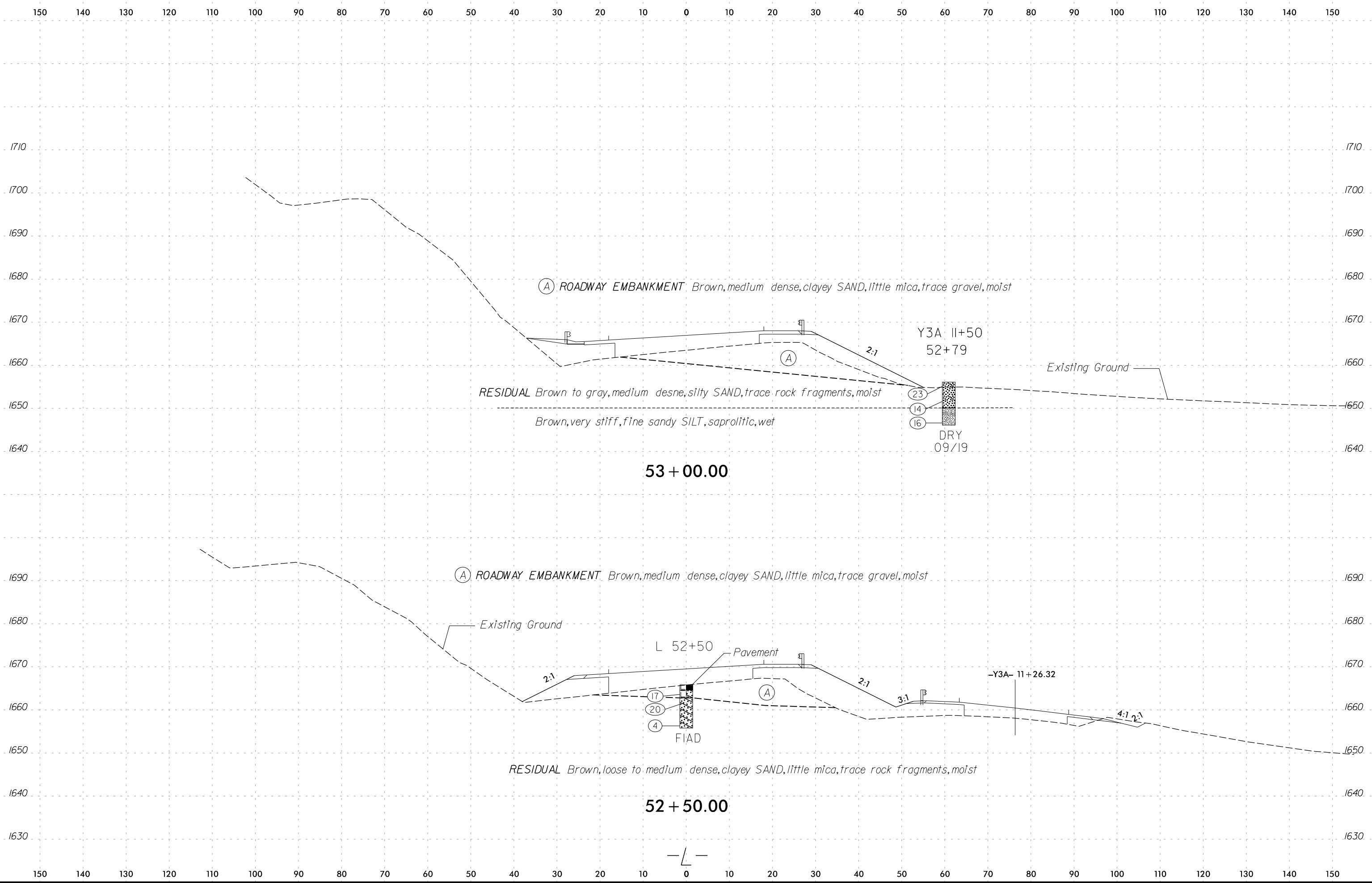
50 + 50.00

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-475	49+60	55' LT	1.3-2.8	A-4 (4)	32	10	13	32	21	34	97	91	58.5	18	-



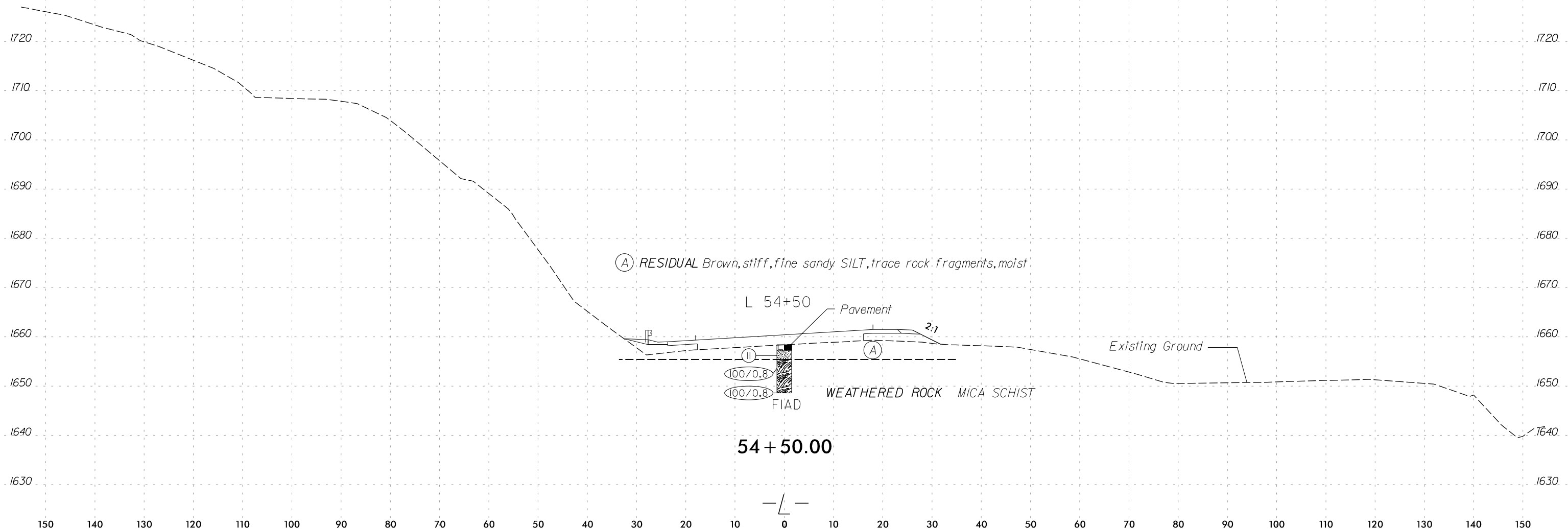
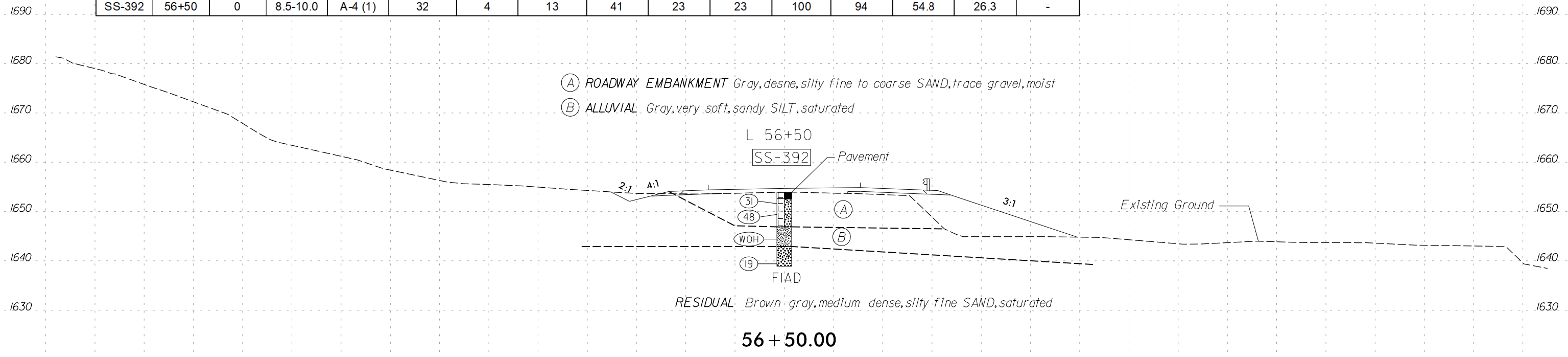
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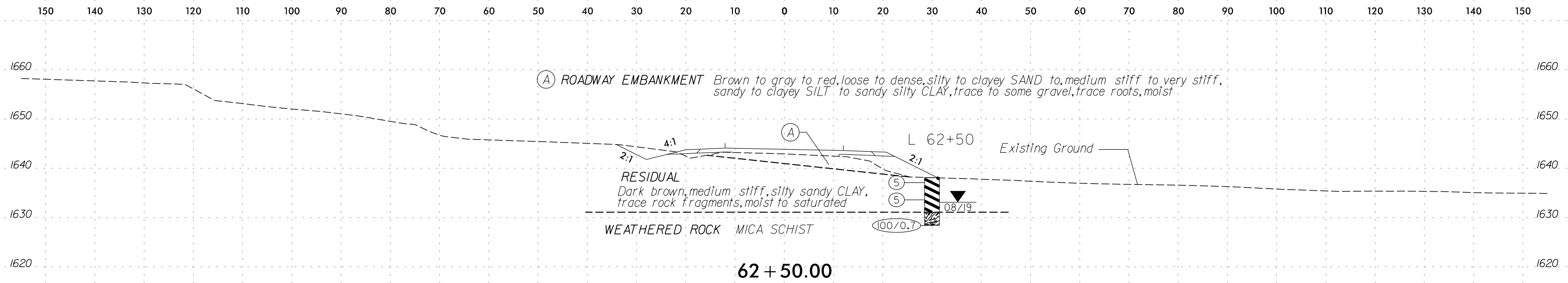


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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-392	56+50	0	8.5-10.0	A-4 (1)	32	4	13	41	23	23	100	94	54.8	26.3	-



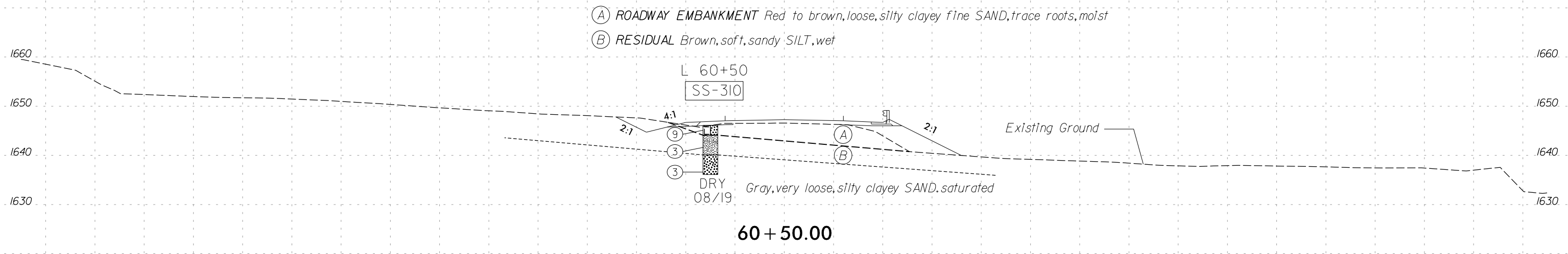
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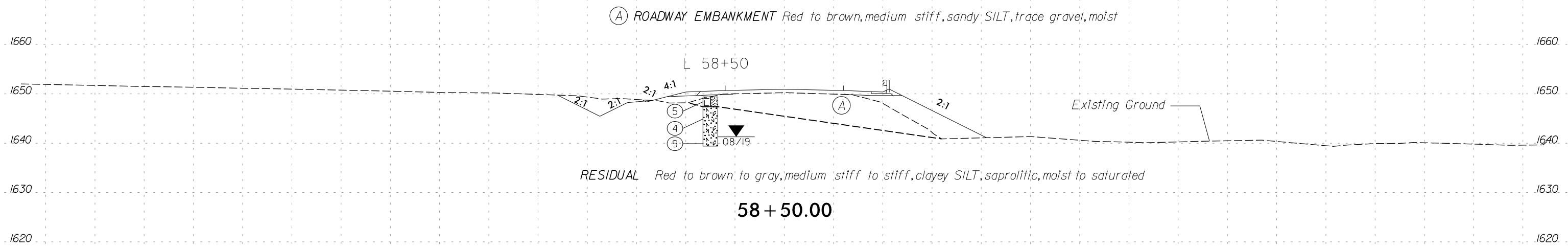
62 + 50.00

SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-310	60+50	15' LT	3.5-5.0	A-4 (0)	25	6	16	48	11	25	98	92	43.4	19.5	-

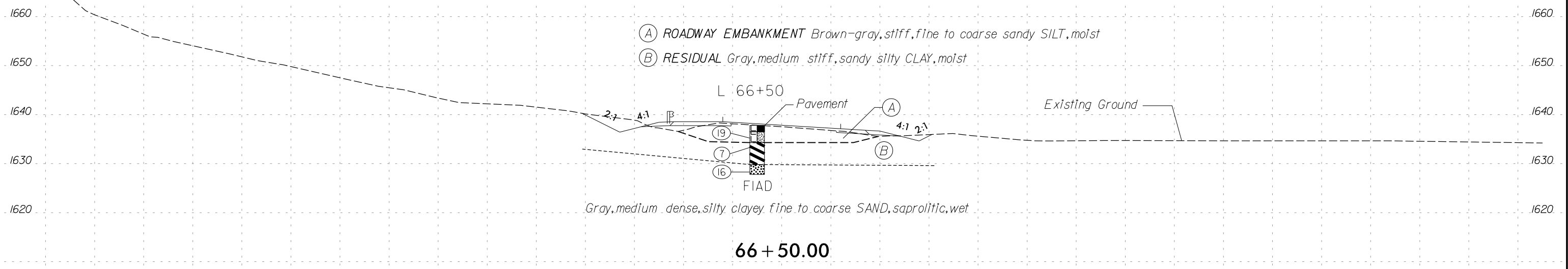
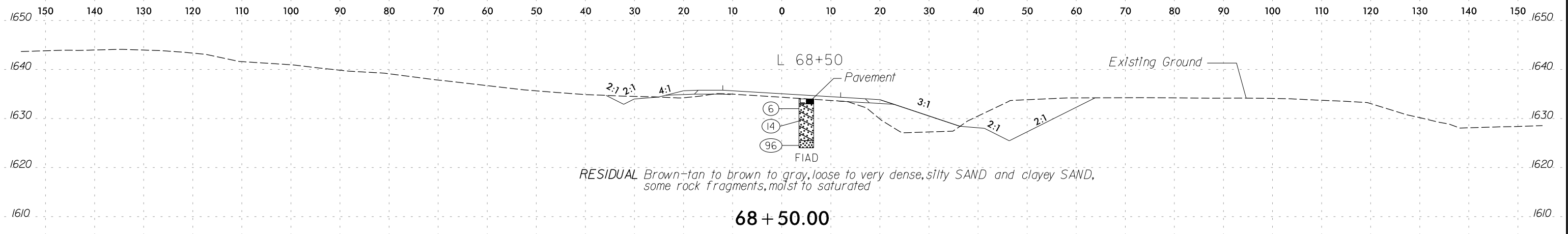


60 + 50.00



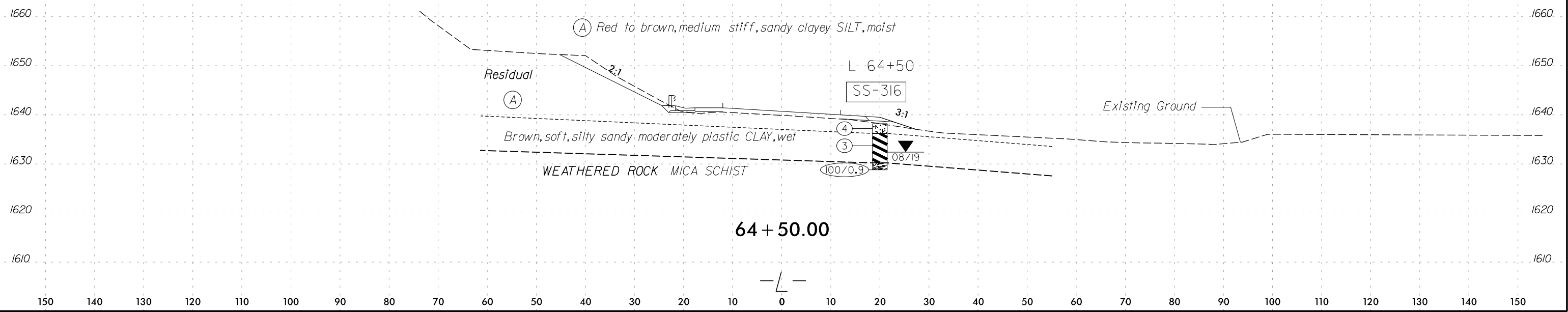
58 + 50.00

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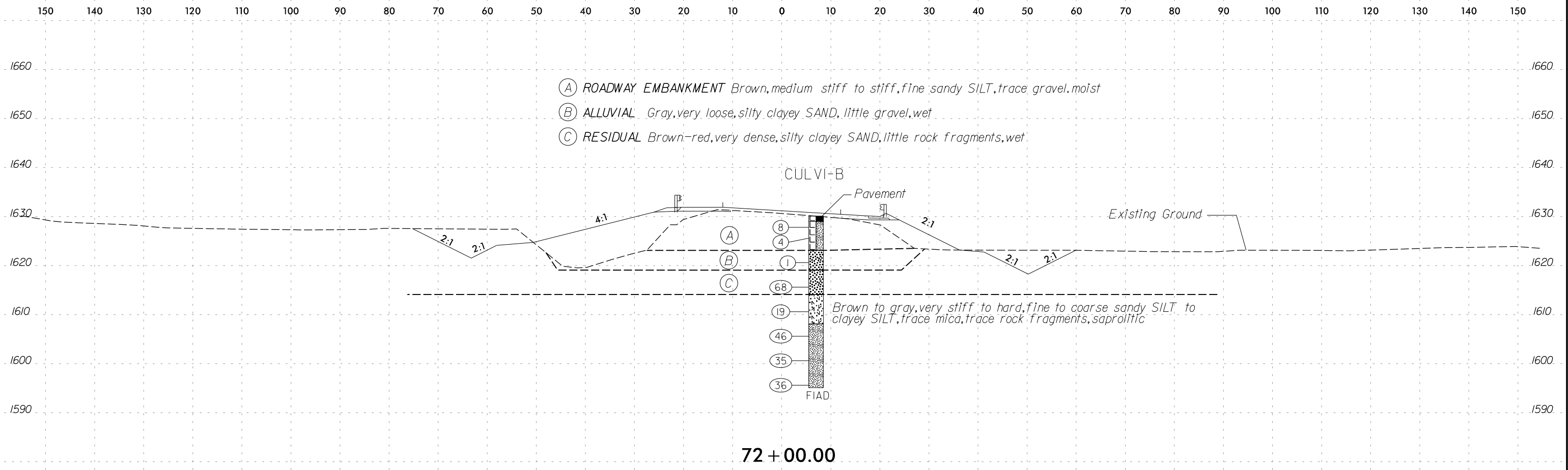


SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-316	64+50	20' RT	3.5-5.0	A-7-6 (13)	46	19	6	31	24	39	100	98	70.2	30.7	-

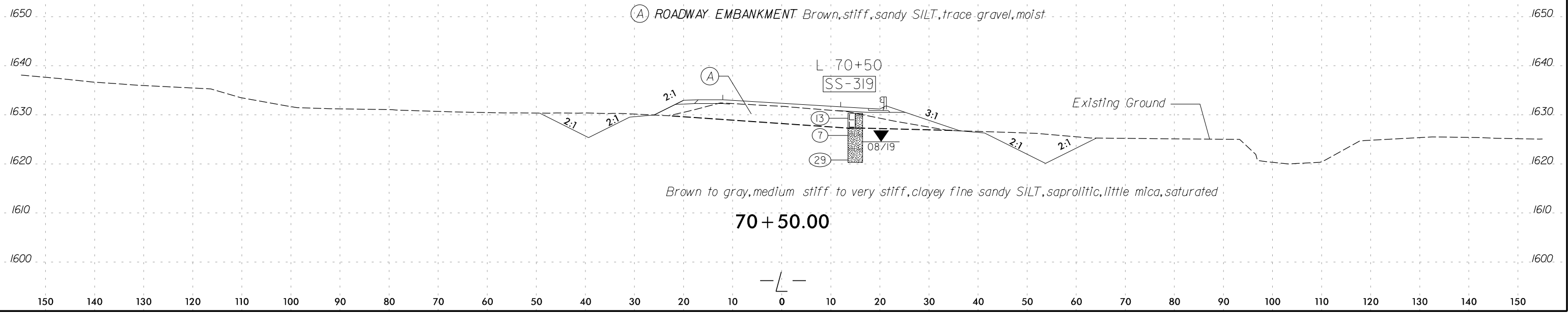


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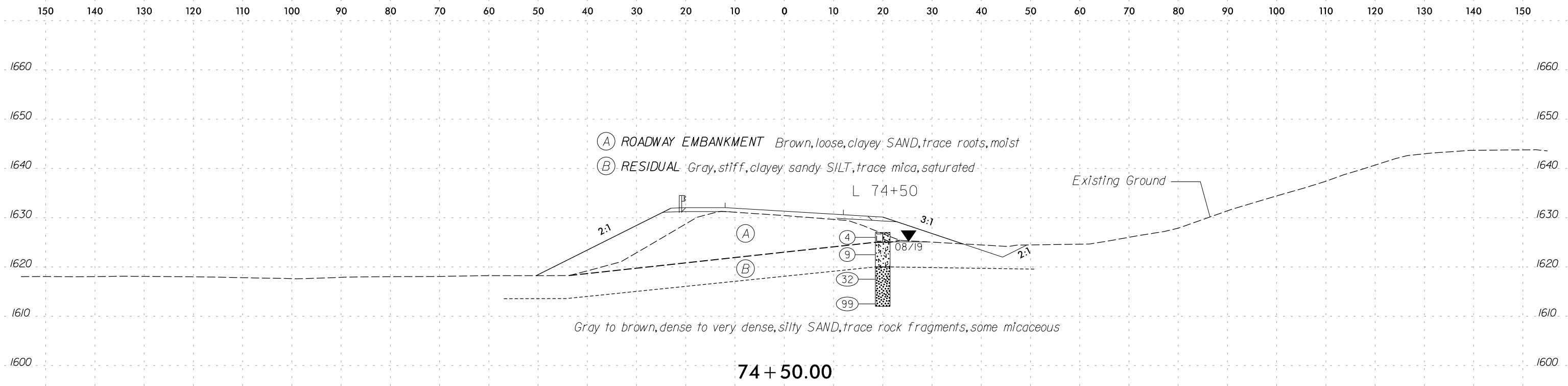


SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-319	70+50	50' RT	3.5-5.0	A-4 (0)	27	5	8	51	17	24	100	98	51.5	18.3	-

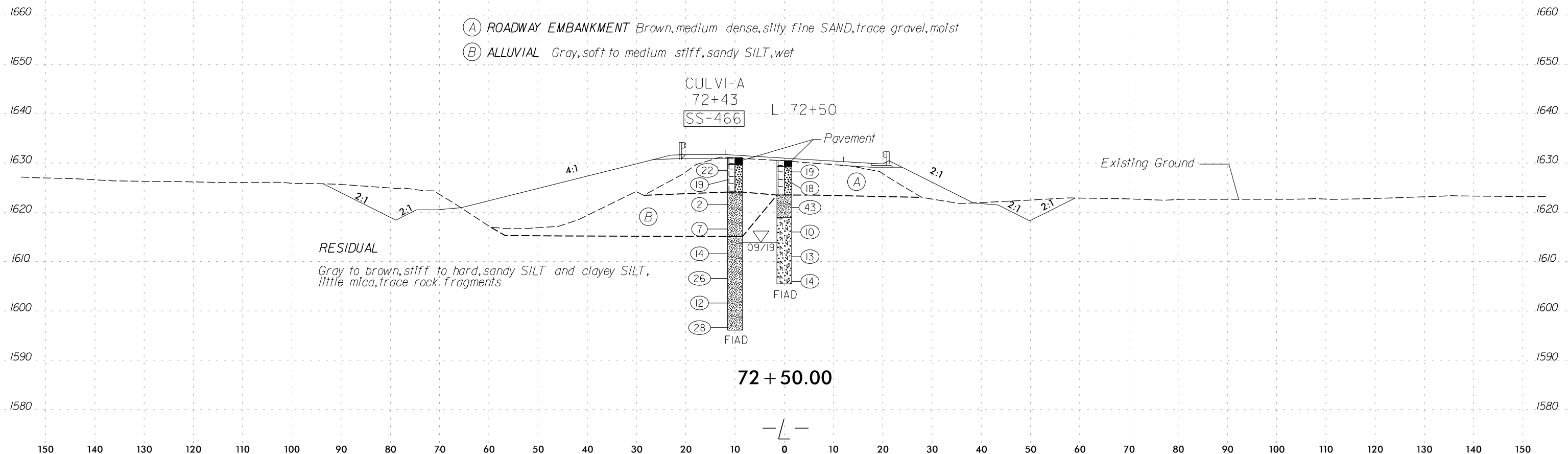


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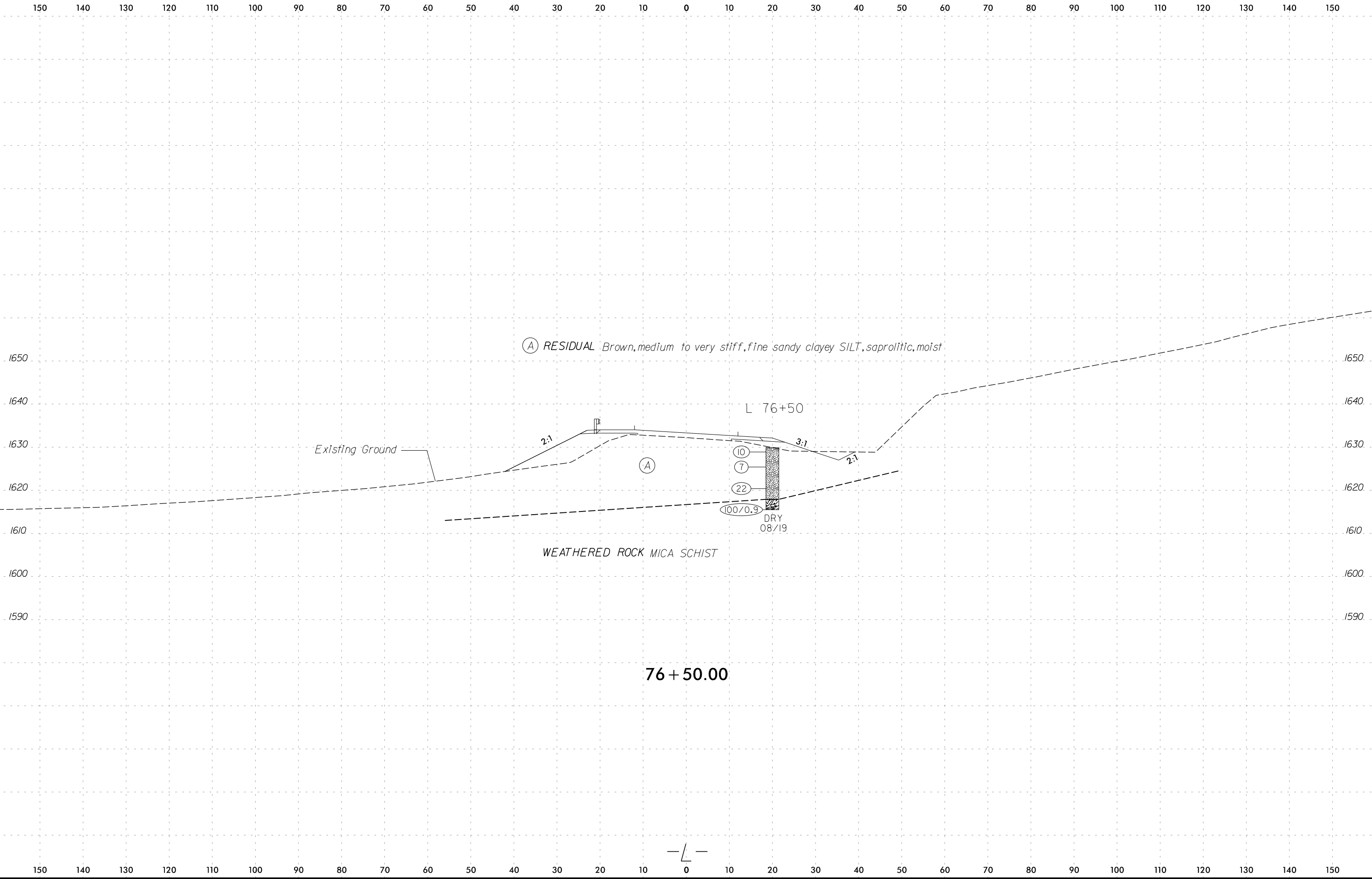
SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-466	72+43	10' LT	8.5-10.0	A-4 (3)	31	8	8	36	22	34	99	97	63.5	29.2	-

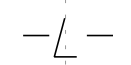


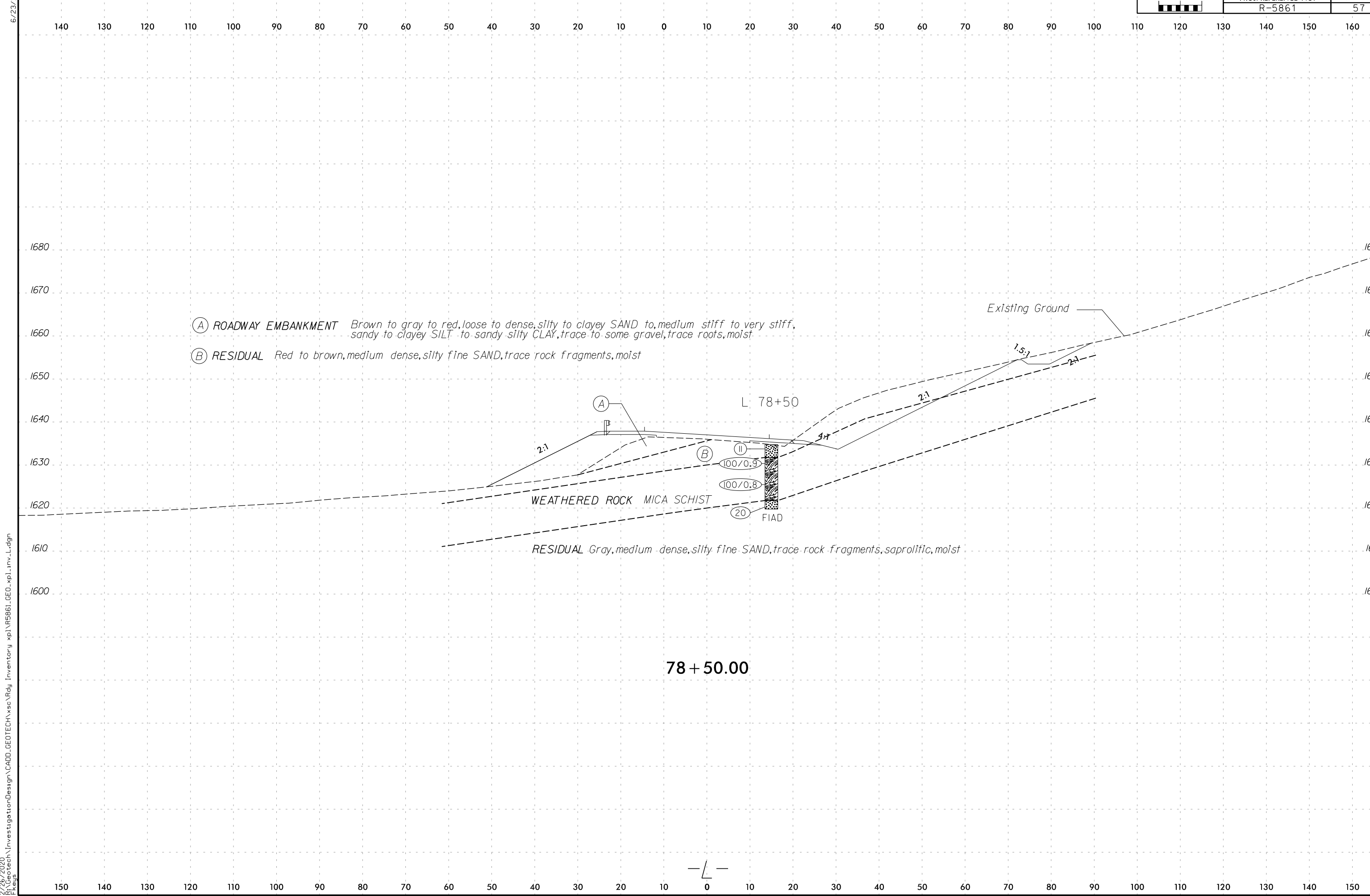
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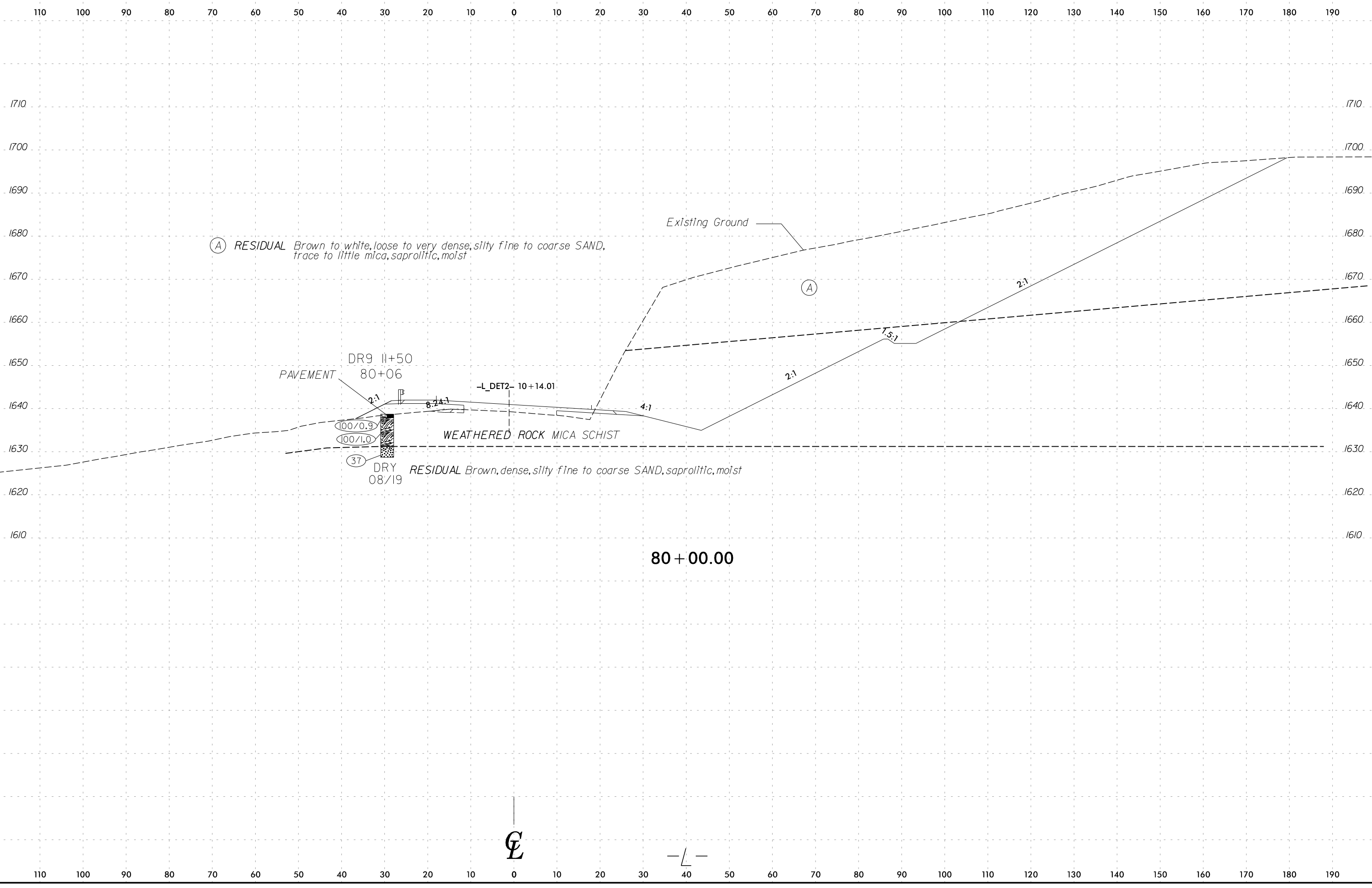
- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Red to brown, medium dense, silty fine SAND, trace rock fragments, moist*

WEATHERED ROCK MICA SCHIST

RESIDUAL *Gray, medium dense, silty fine SAND, trace rock fragments, saprolitic, moist*

78 + 50.00

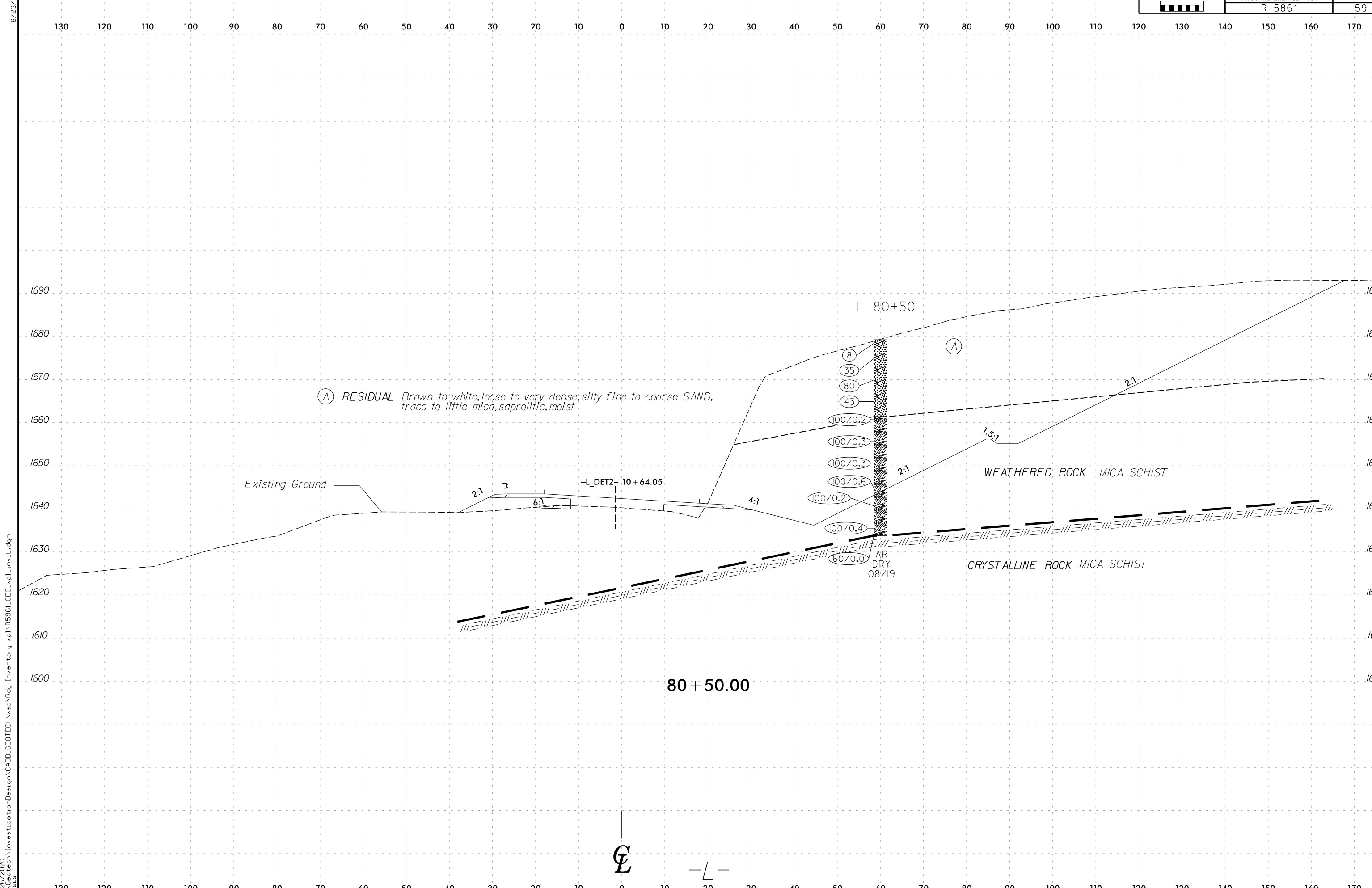
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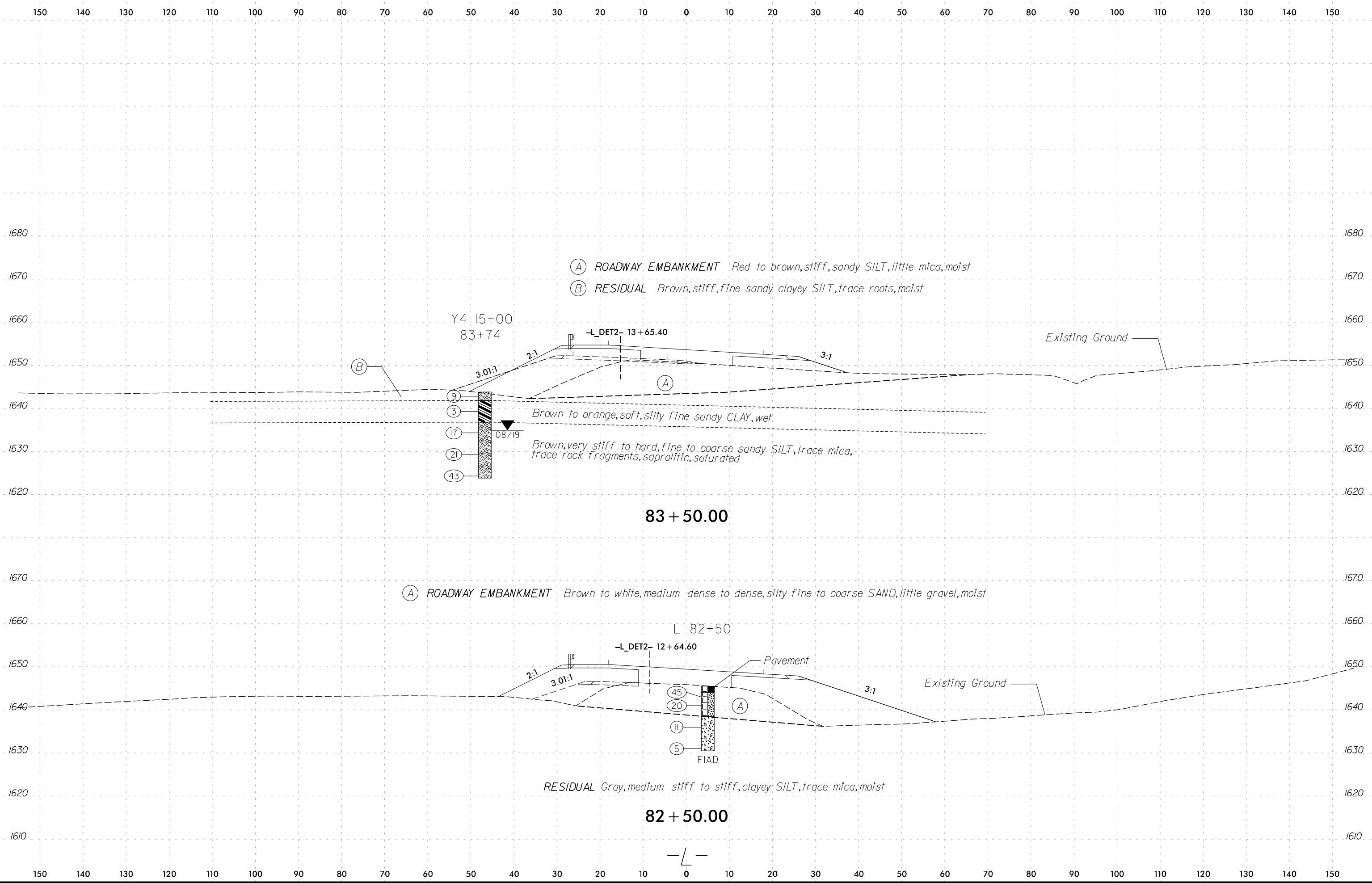
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(A) ROADWAY EMBANKMENT Red to brown, stiff, sandy SILT, little mica, moist
 (B) RESIDUAL Brown, stiff, fine sandy clayey SILT, trace roots, moist

Y4 15+00
 83+74
 -L_DET2- 13+65.40

9
 3
 17
 21
 43
 08/19
 Brown to orange, soft, silty fine sandy CLAY, wet
 Brown, very stiff to hard, fine to coarse sandy SILT, trace mica, trace rock fragments, saprofitic, saturated

83 + 50.00

(A) ROADWAY EMBANKMENT Brown to white, medium dense to dense, silty fine to coarse SAND, little gravel, moist

L 82+50
 -L_DET2- 12+64.60

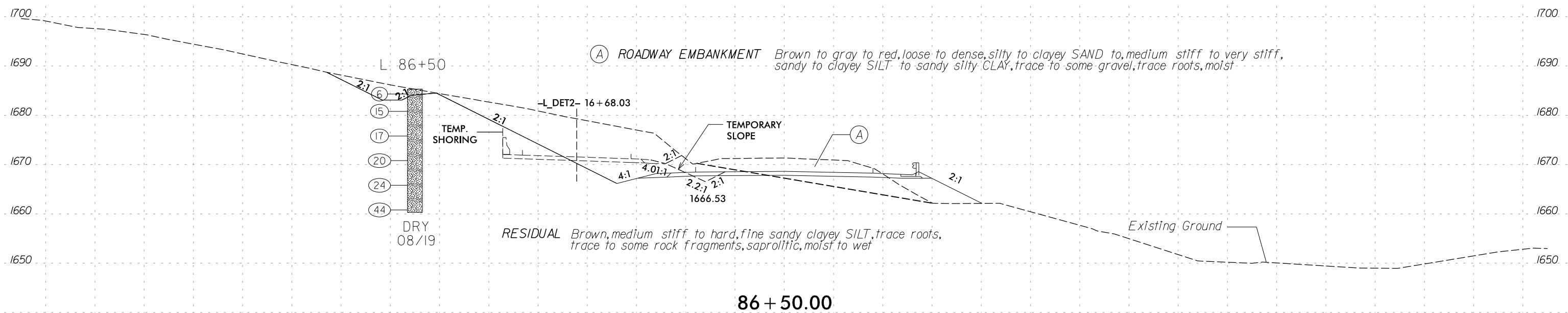
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RESIDUAL Gray, medium stiff to stiff, clayey SILT, trace mica, moist

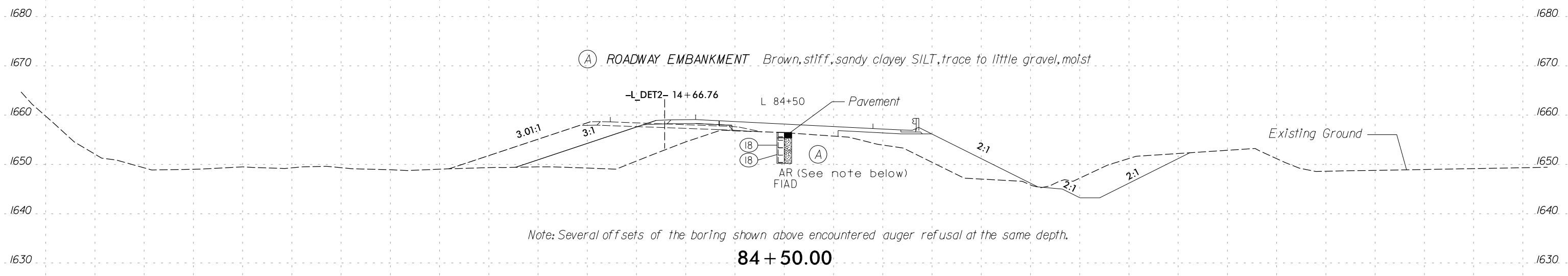
82 + 50.00

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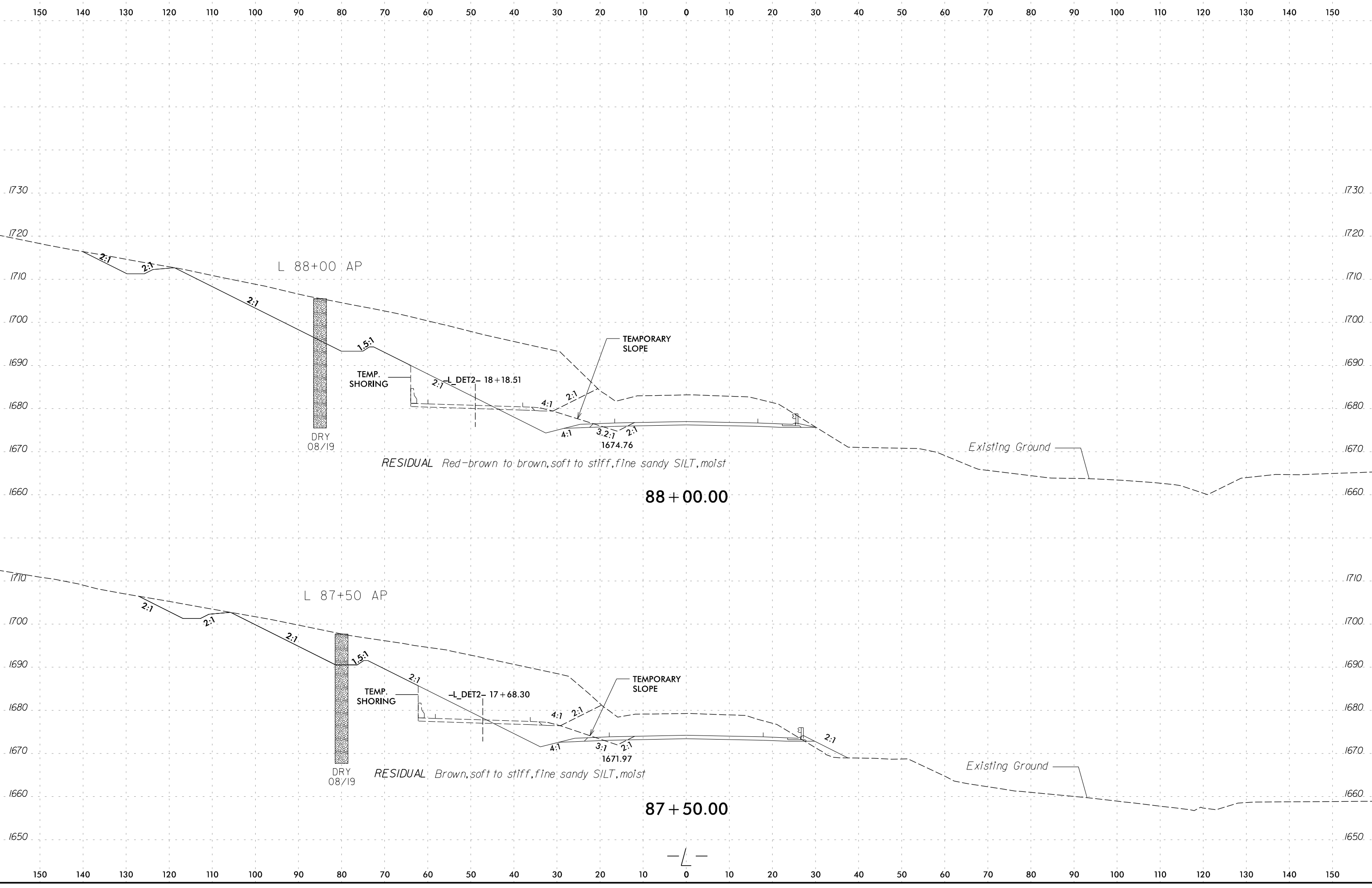
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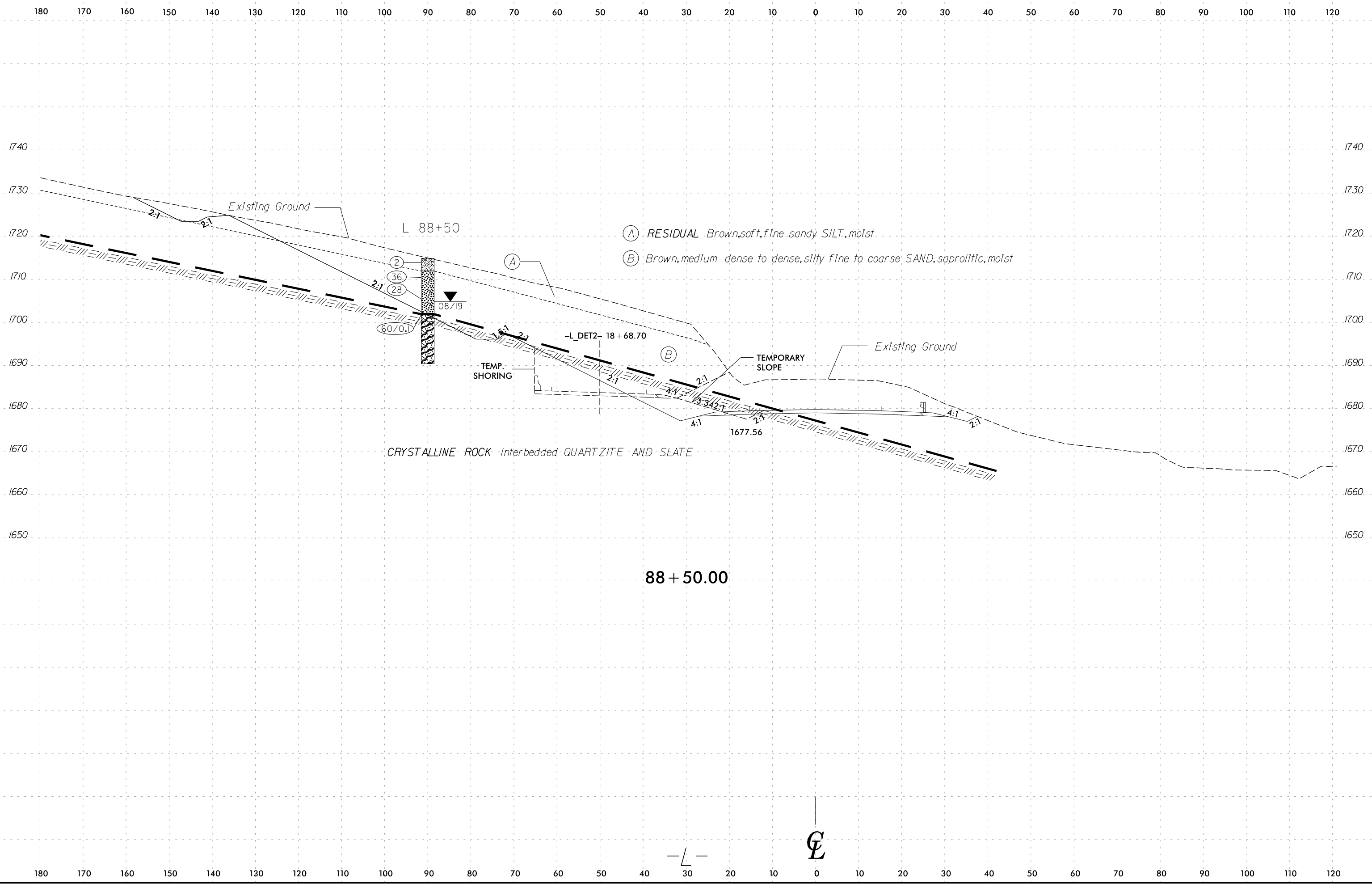
84 + 50.00

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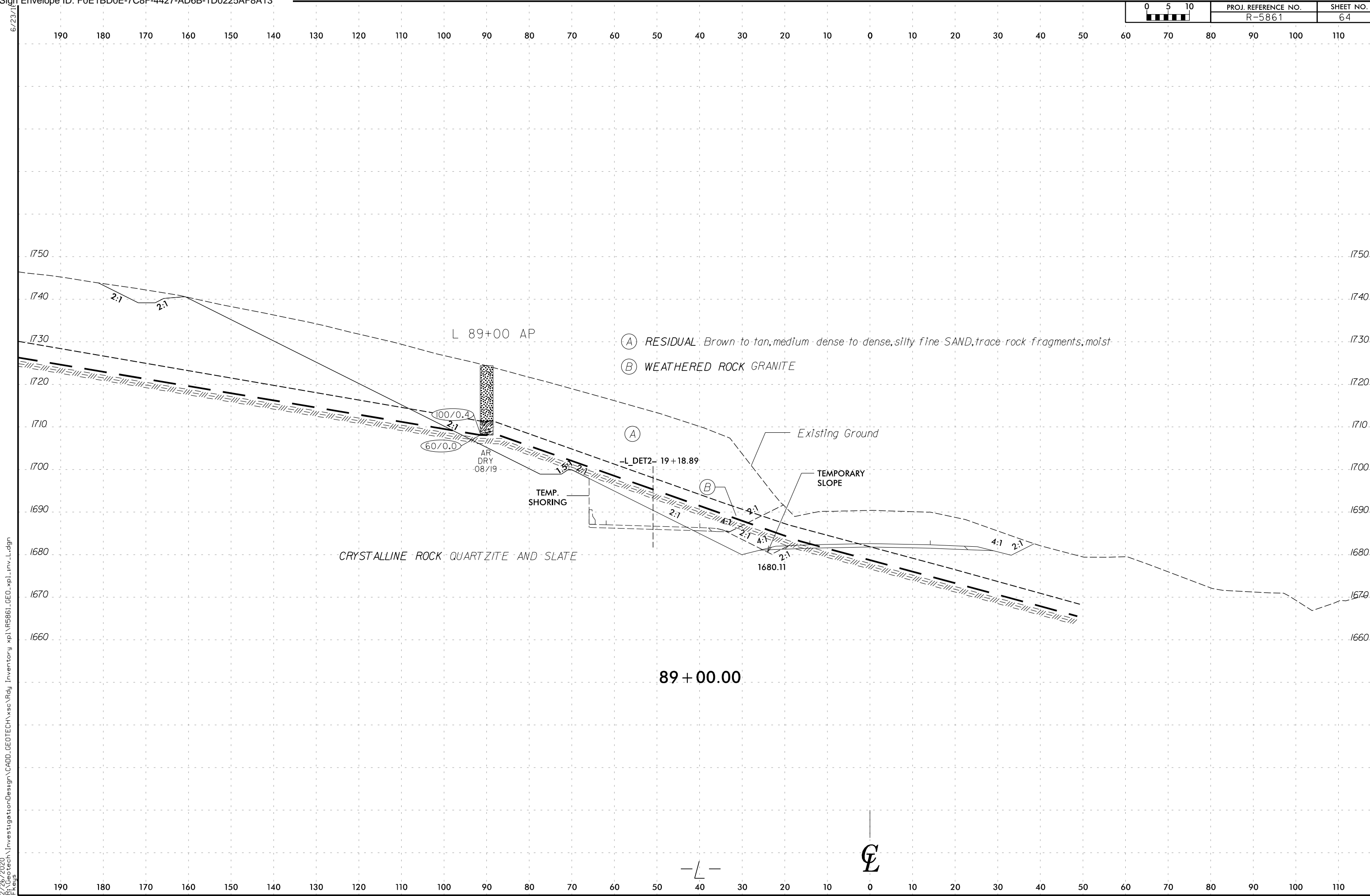
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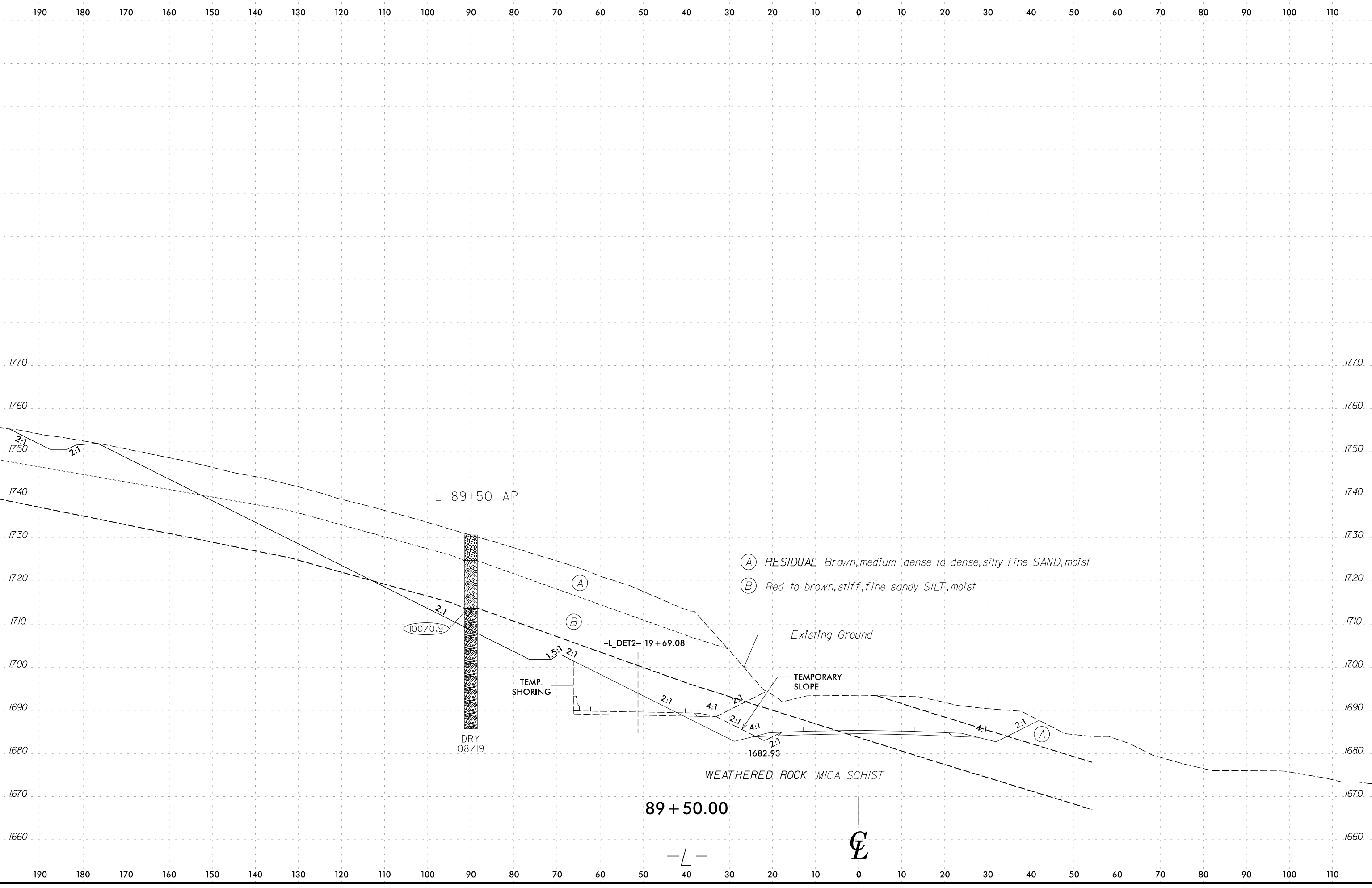
- (A) RESIDUAL: Brown to tan, medium dense to dense, silty fine SAND, trace rock fragments, moist
- (B) WEATHERED ROCK GRANITE

CRYSTALLINE ROCK QUARTZITE AND SLATE

89 + 00.00



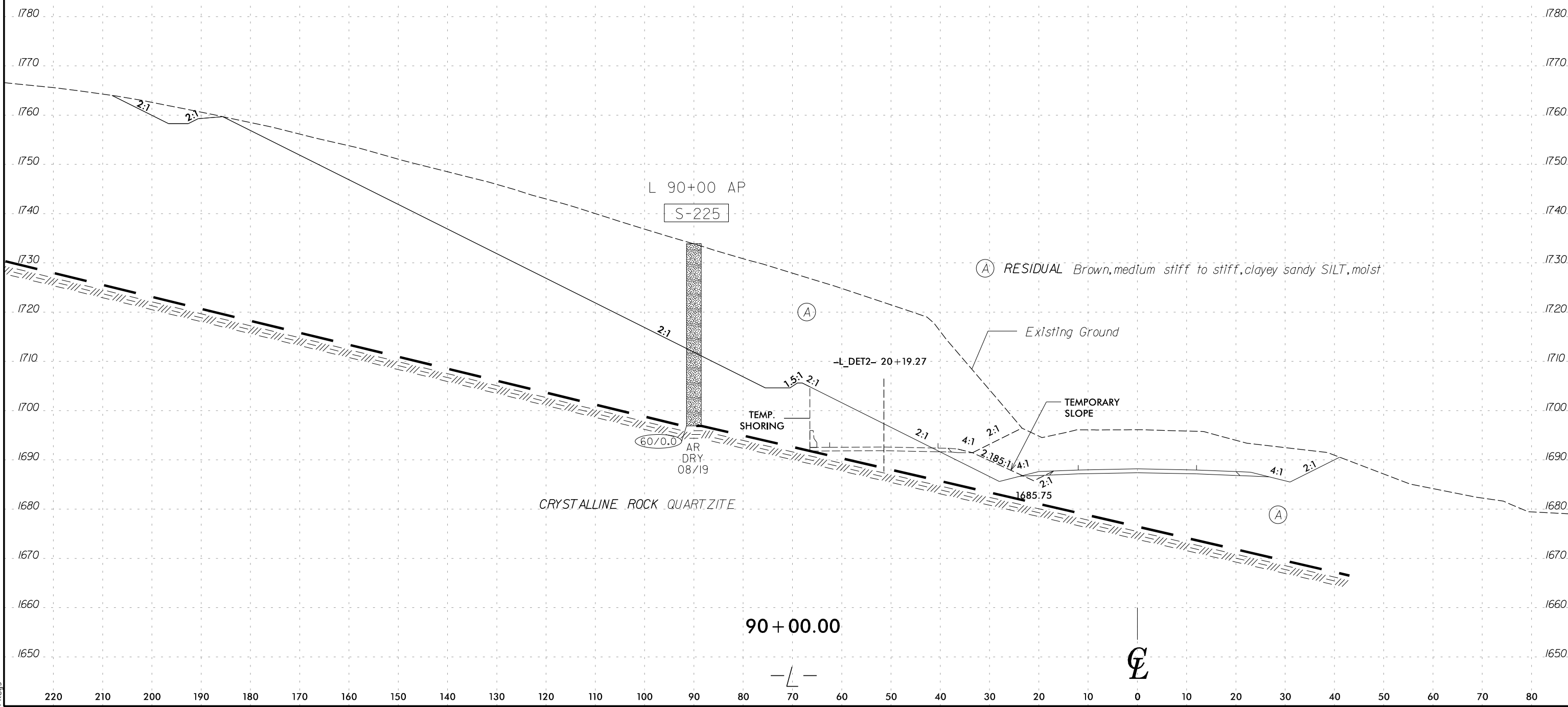
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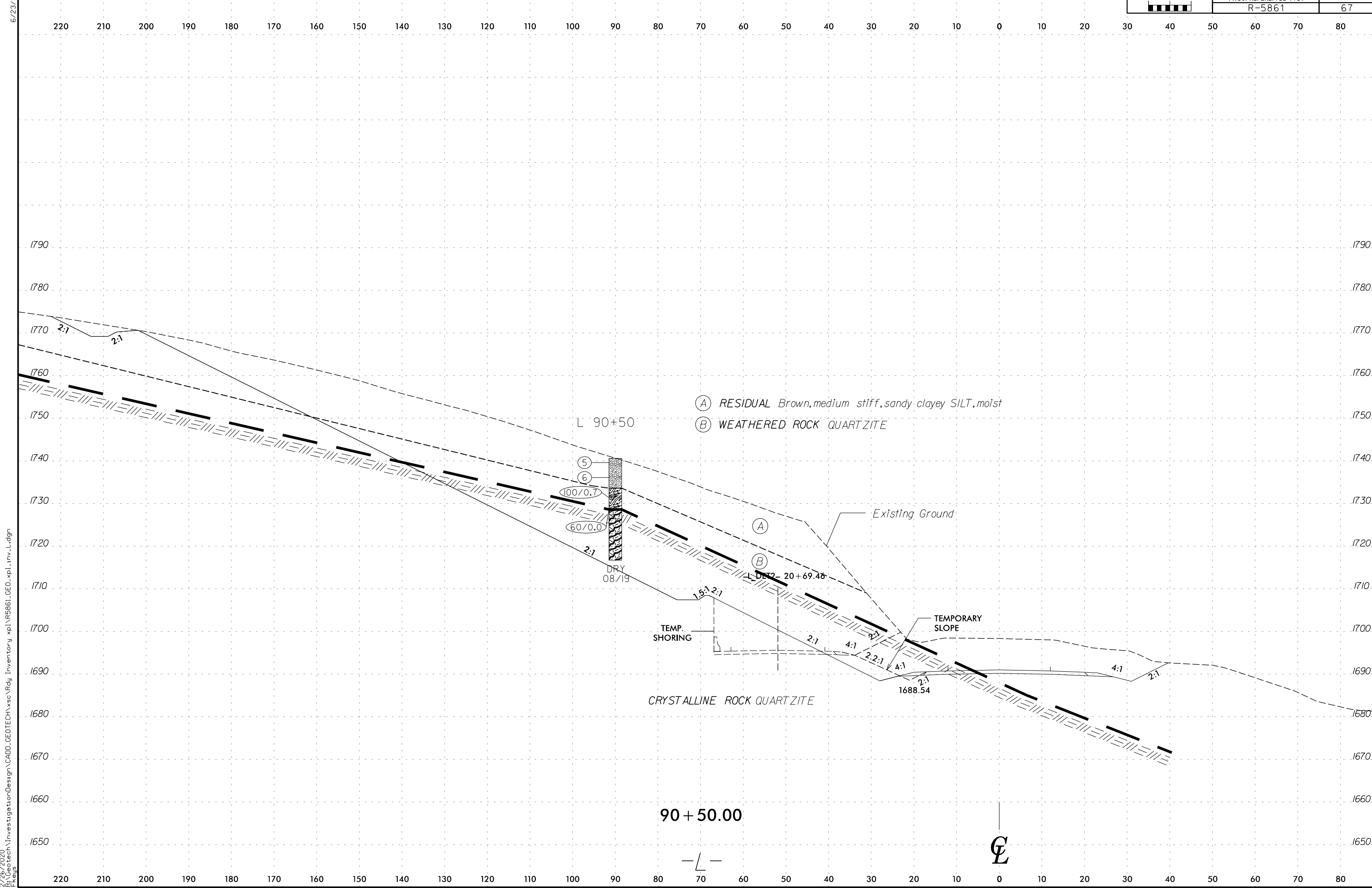
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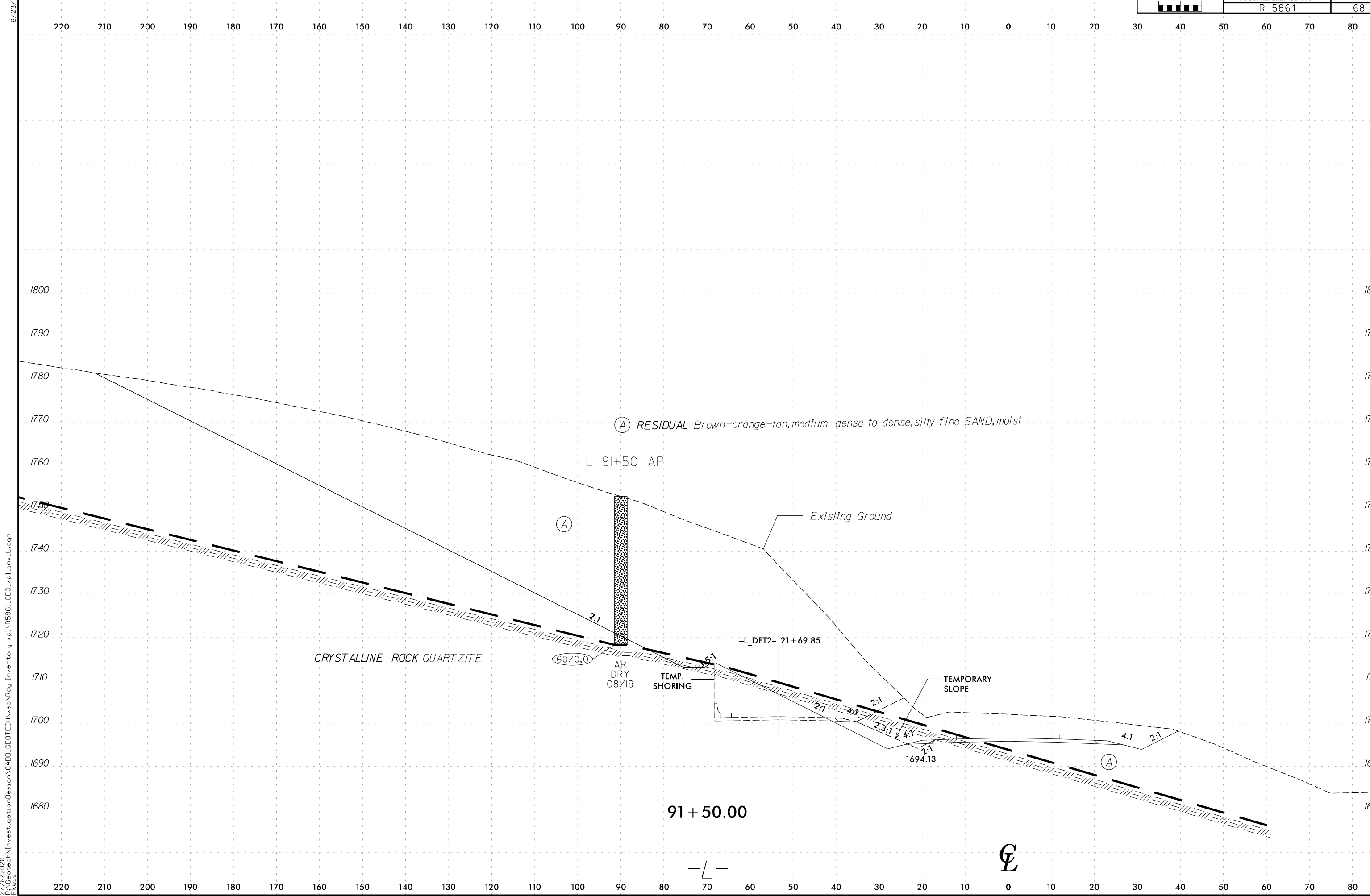
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
S-225	90+00	90' LT	1.0-8.5	A-4 (0)	29	5	10	51	17	22	96	92	46.2	ND	-



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(A) RESIDUAL Brown-orange-tan, medium dense to dense, silty fine SAND, moist

L 91+50 AP

Existing Ground

CRYSTALLINE ROCK QUARTZITE

(60/0.0)

AR DRY 08/19

TEMP. SHORING

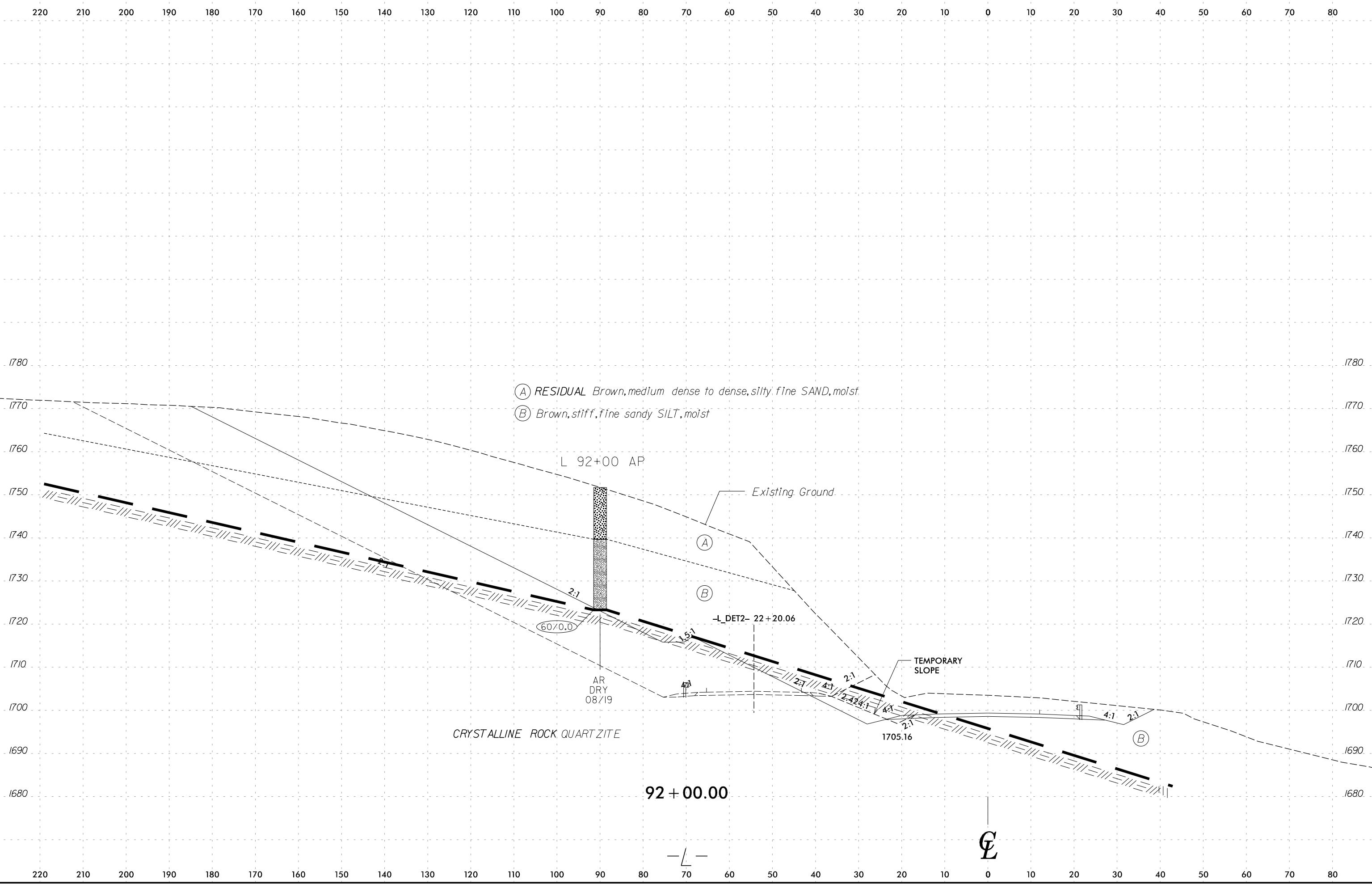
-L_DET2- 21+69.85

TEMPORARY SLOPE

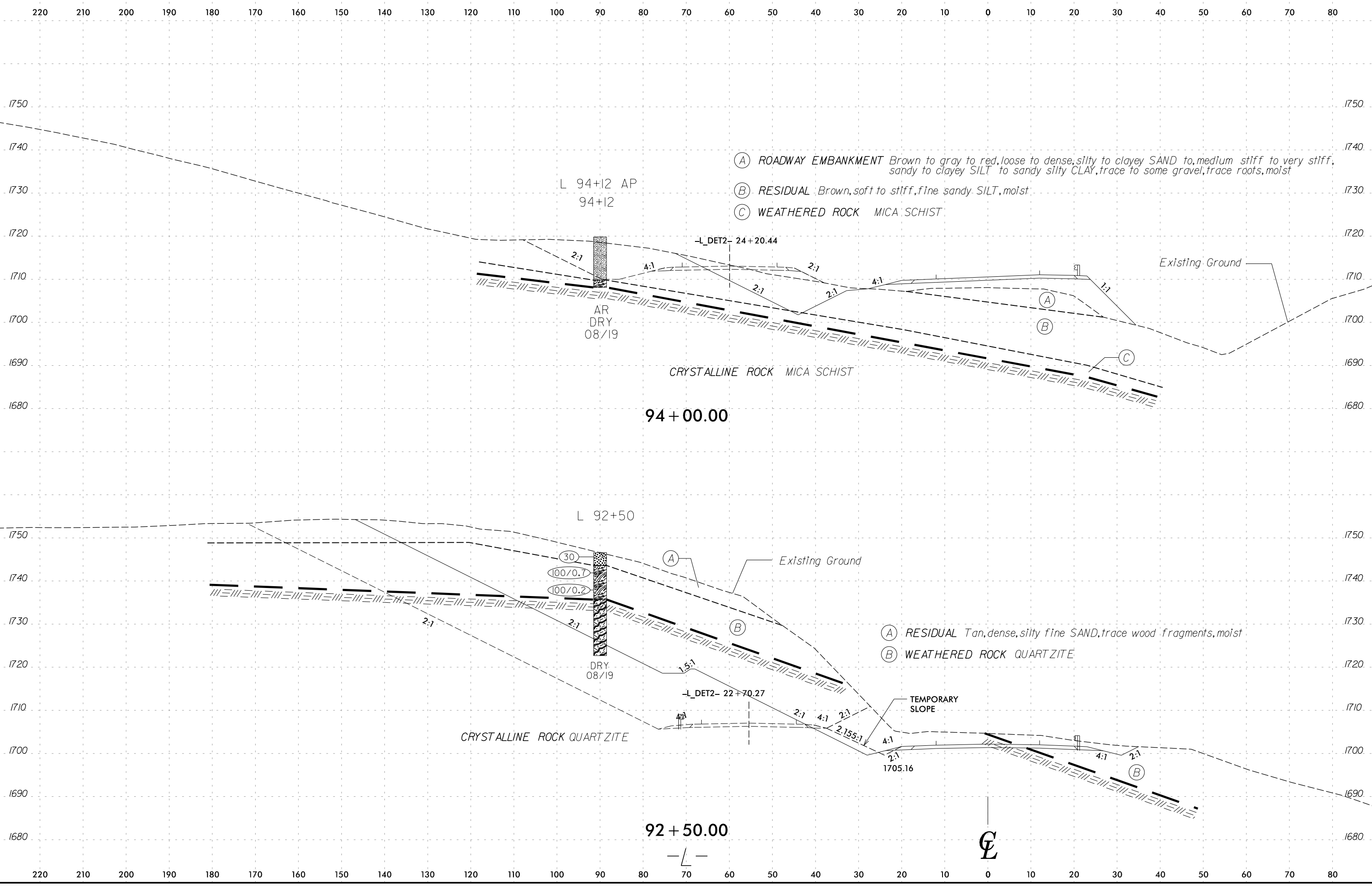
1694.13

91 + 50.00

CL



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- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown, soft to stiff, fine sandy SILT, moist*
- (C) WEATHERED ROCK *MICA SCHIST*

L 94+12 AP
94+12

-L_DET2- 24+20.44

AR
DRY
08/19

Existing Ground

CRYSTALLINE ROCK MICA SCHIST

94 + 00.00

L 92+50

30
100/0.7
100/0.2
DRY
08/19

Existing Ground

- (A) RESIDUAL *Tan, dense, silty fine SAND, trace wood fragments, moist*
- (B) WEATHERED ROCK *QUARTZITE*

CRYSTALLINE ROCK QUARTZITE

-L_DET2- 22+70.27

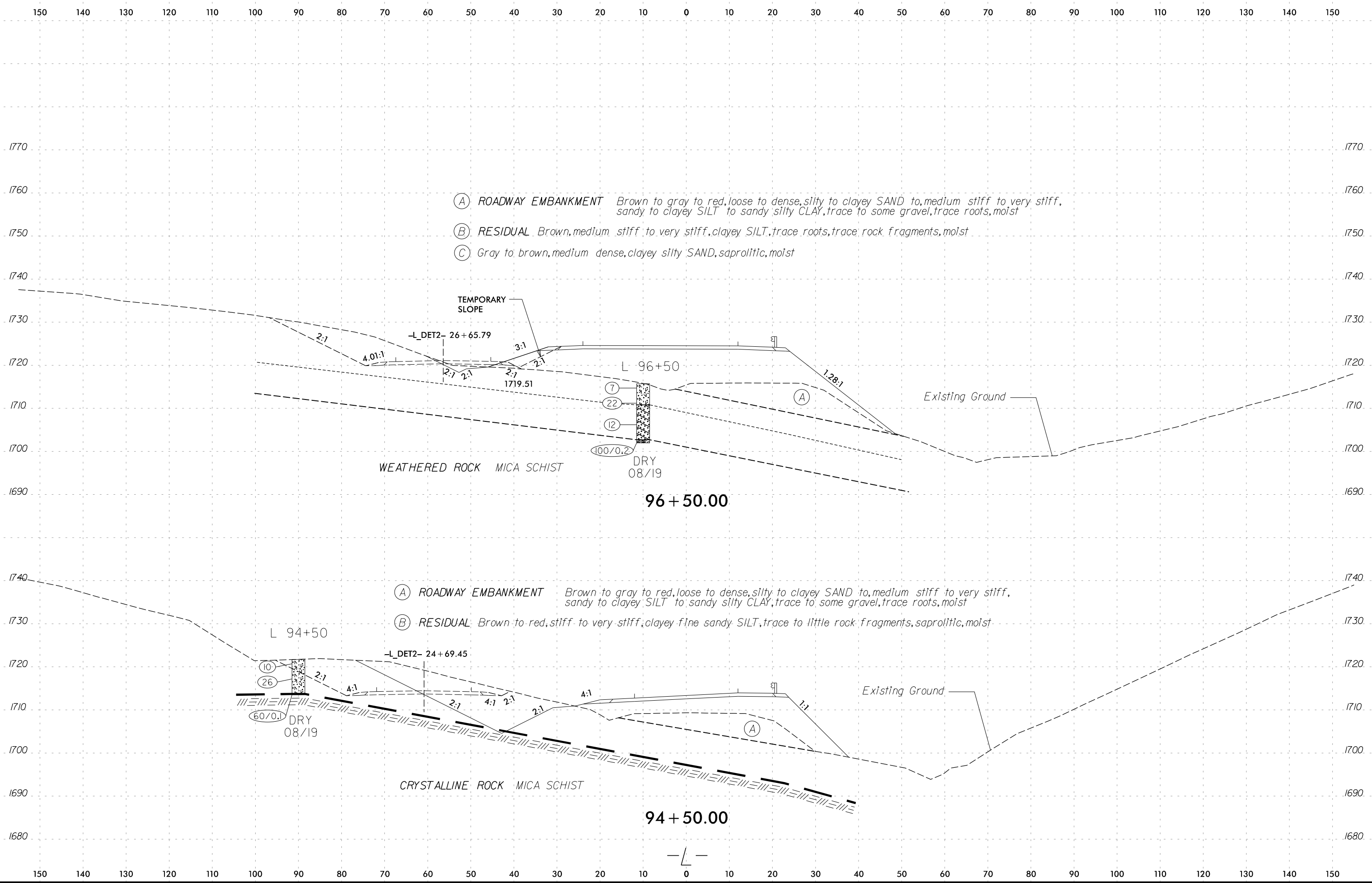
TEMPORARY SLOPE

1705.16

92 + 50.00

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- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown, medium stiff to very stiff, clayey SILT, trace roots, trace rock fragments, moist*
- (C) *Gray to brown, medium dense, clayey silty SAND, saprolitic, moist*

WEATHERED ROCK MICA SCHIST

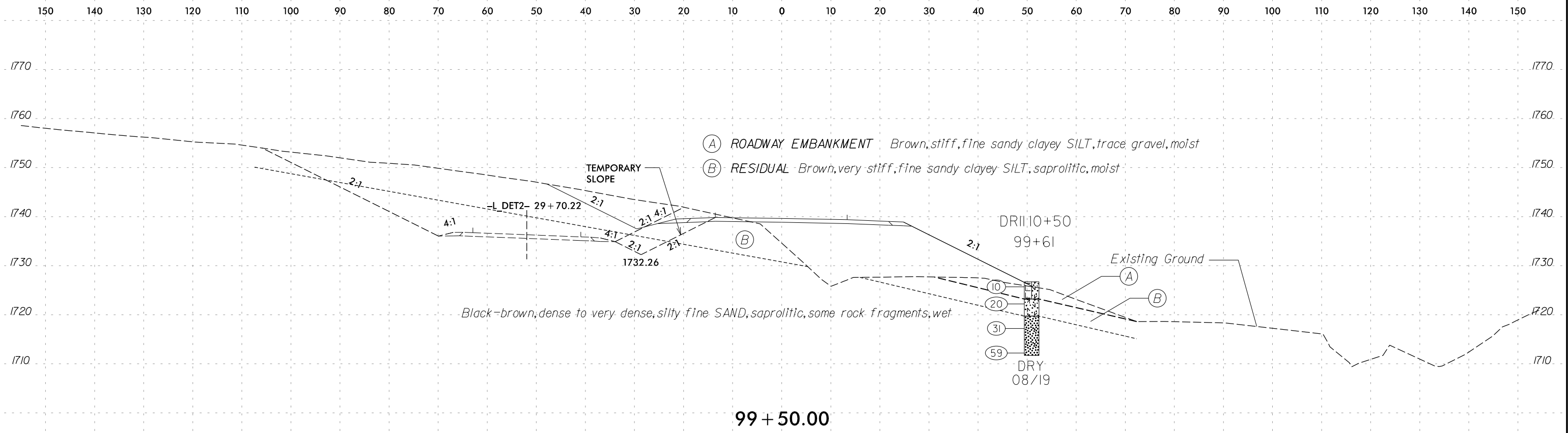
96 + 50.00

- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Brown to red, stiff to very stiff, clayey fine sandy SILT, trace to little rock fragments, saprolitic, moist*

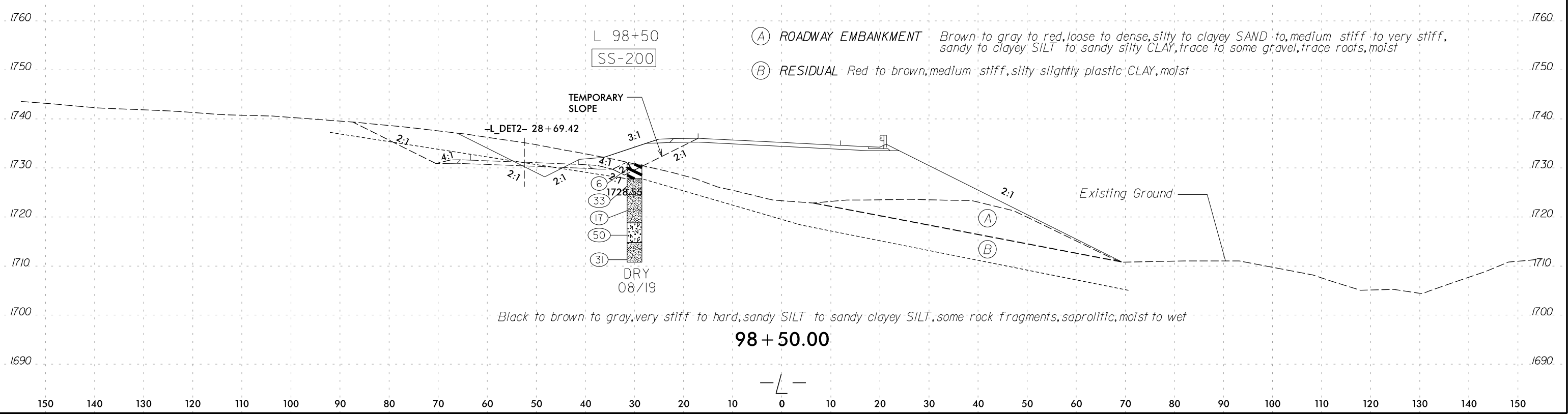
CRYSTALLINE ROCK MICA SCHIST

94 + 50.00

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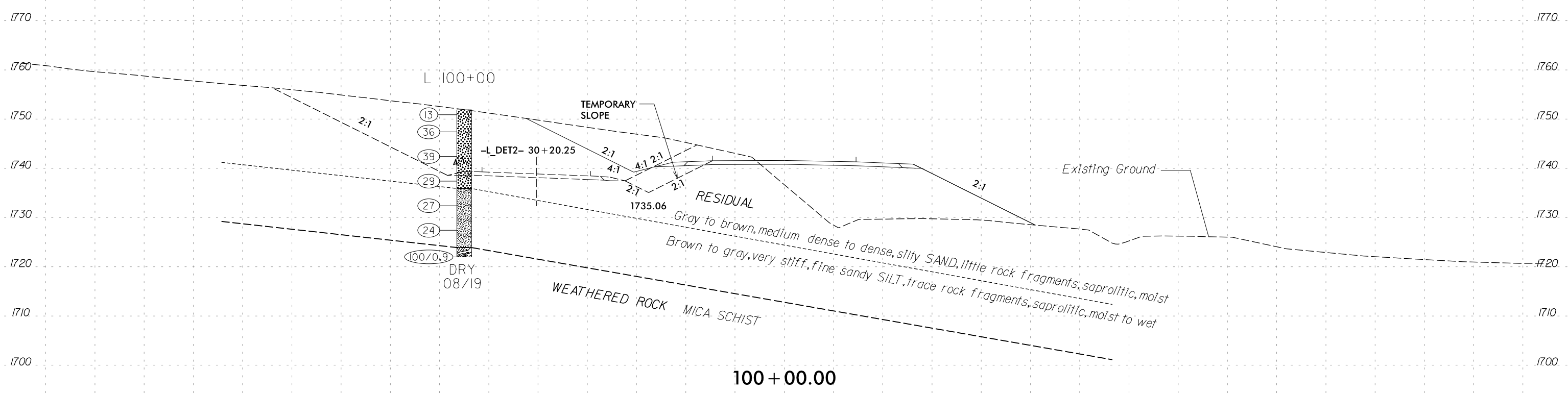
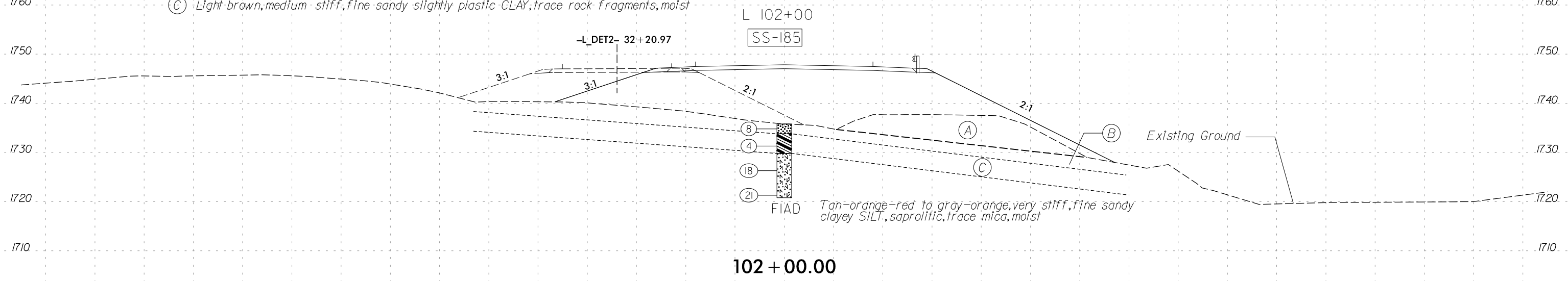
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-200	98+50	30' LT	0.0-1.5	A-7-6 (10)	41	15	17	22	23	38	100	87	68.5	23.2	-



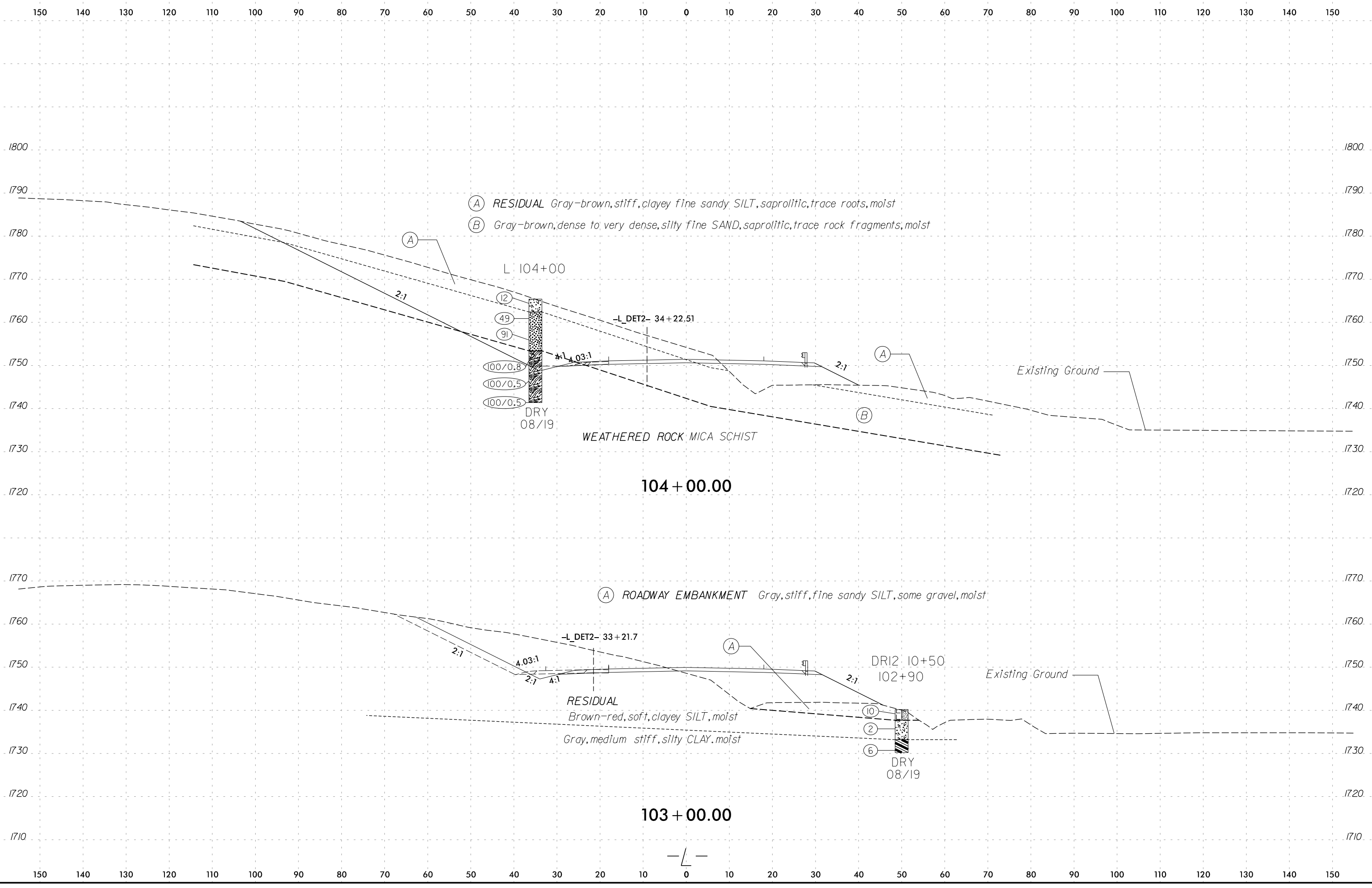
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-185	102+00	0	3.5-5.0	A-6 (9)	37	14	8	20	31	41	93	88	71.8	19.8	-

- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Tan to brown, loose, silty fine SAND, dry*
- (C) *Light brown, medium stiff, fine sandy slightly plastic CLAY, trace rock fragments, moist*

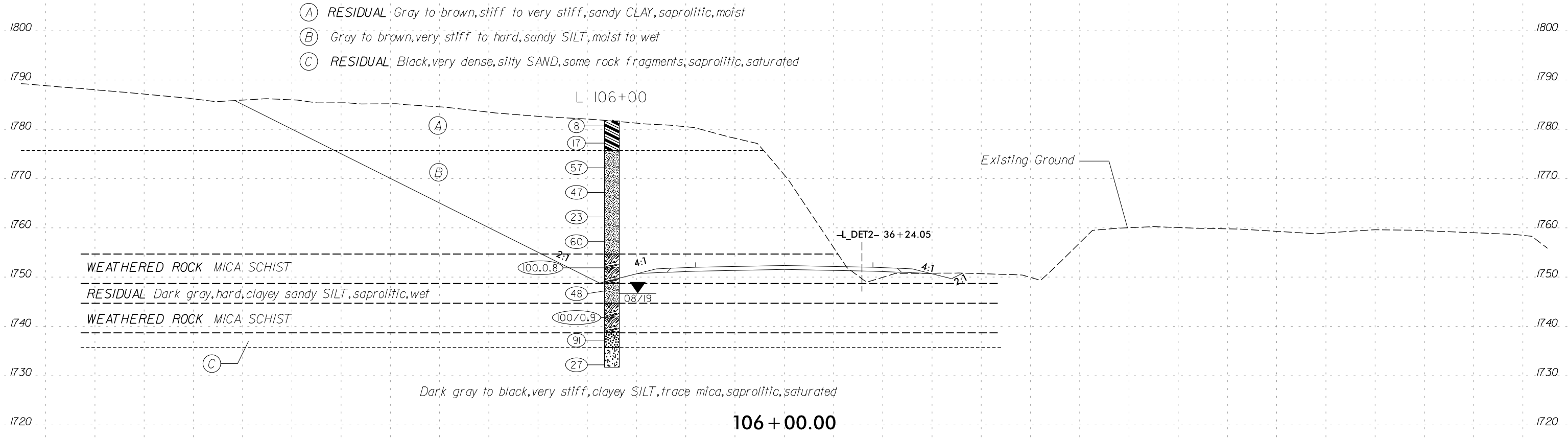
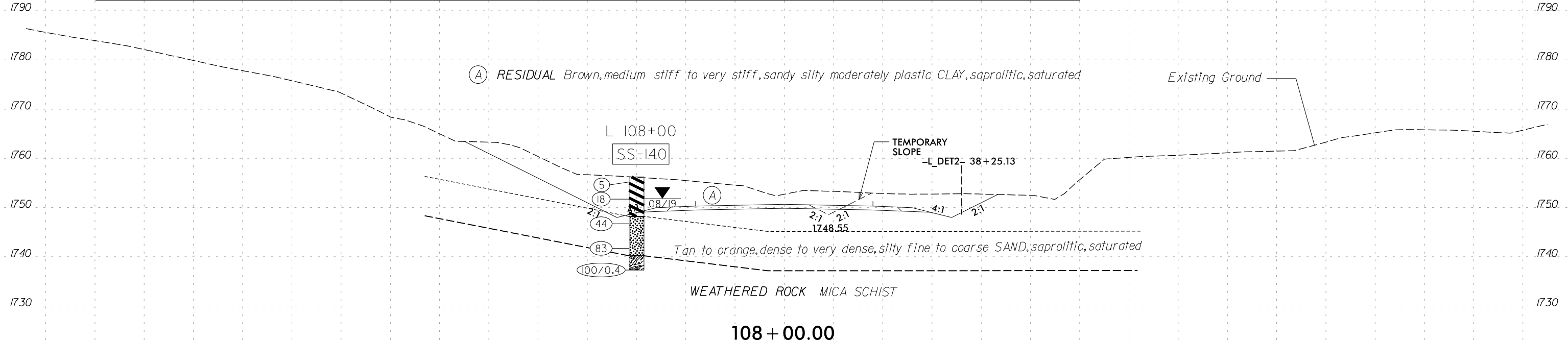


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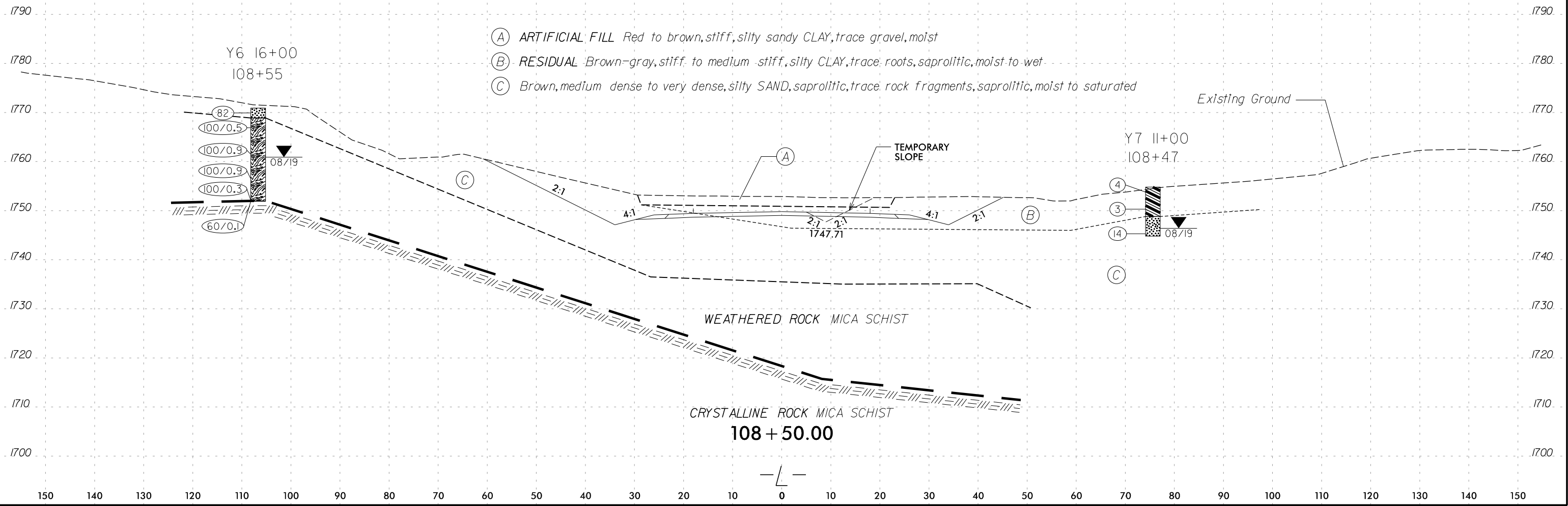
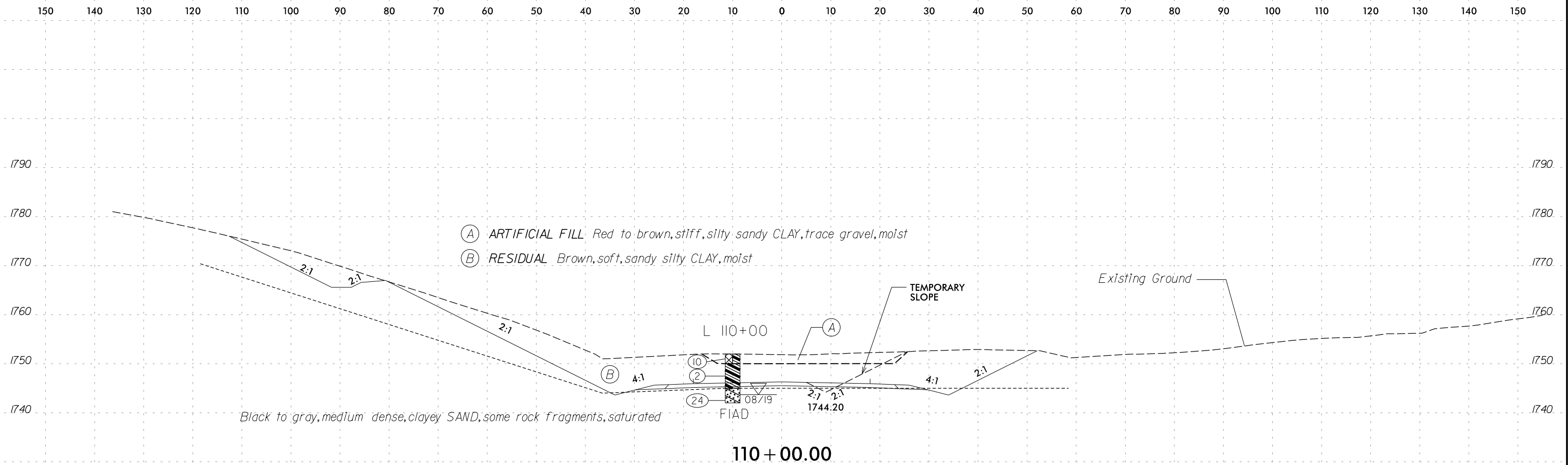


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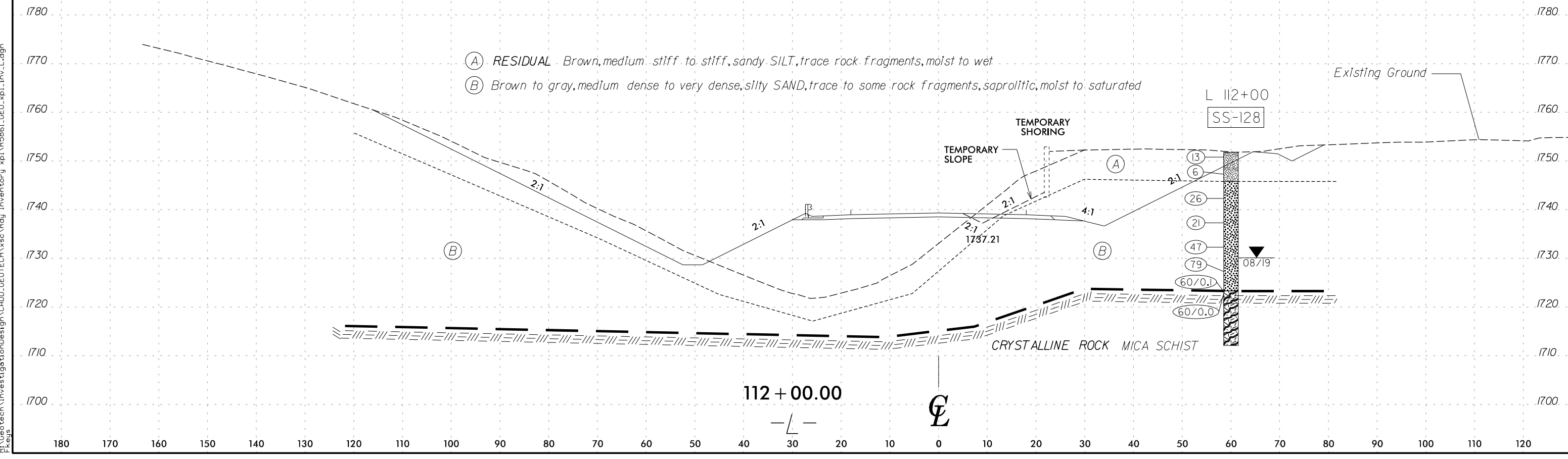
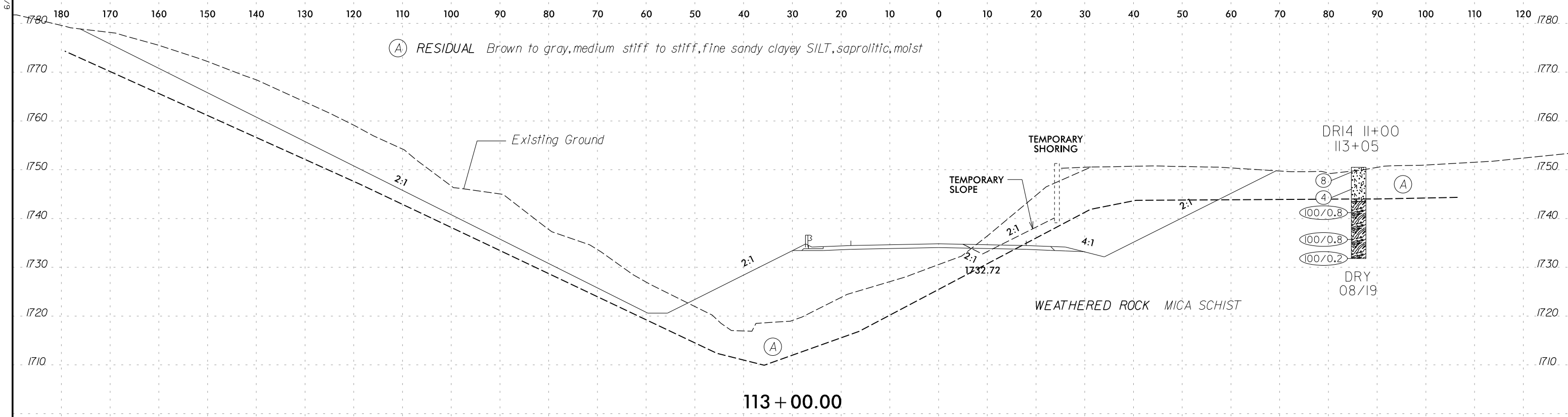
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-140	108+00	30' LT	0.0-1.5	A-7-6 (18)	44	19	2	16	31	51	100	99	86.9	27.4	-



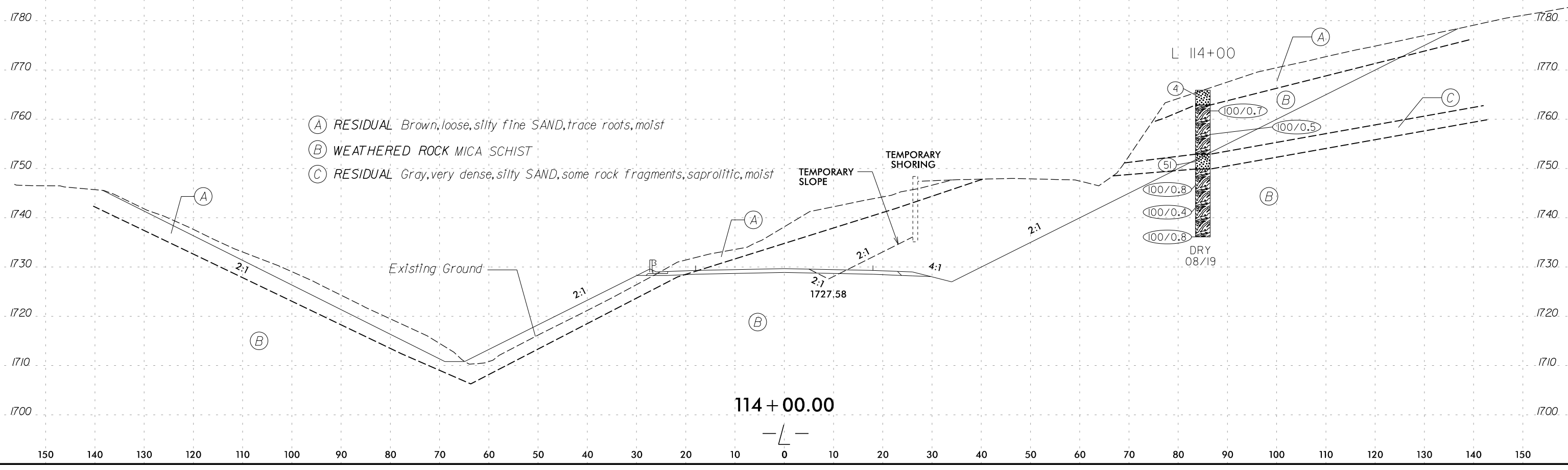
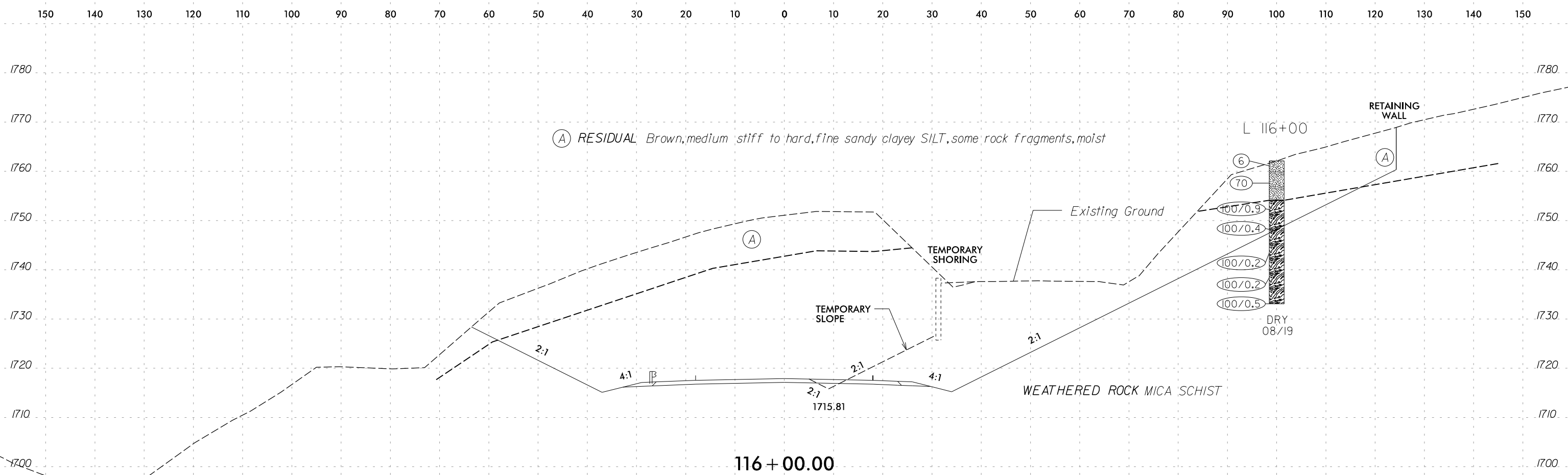
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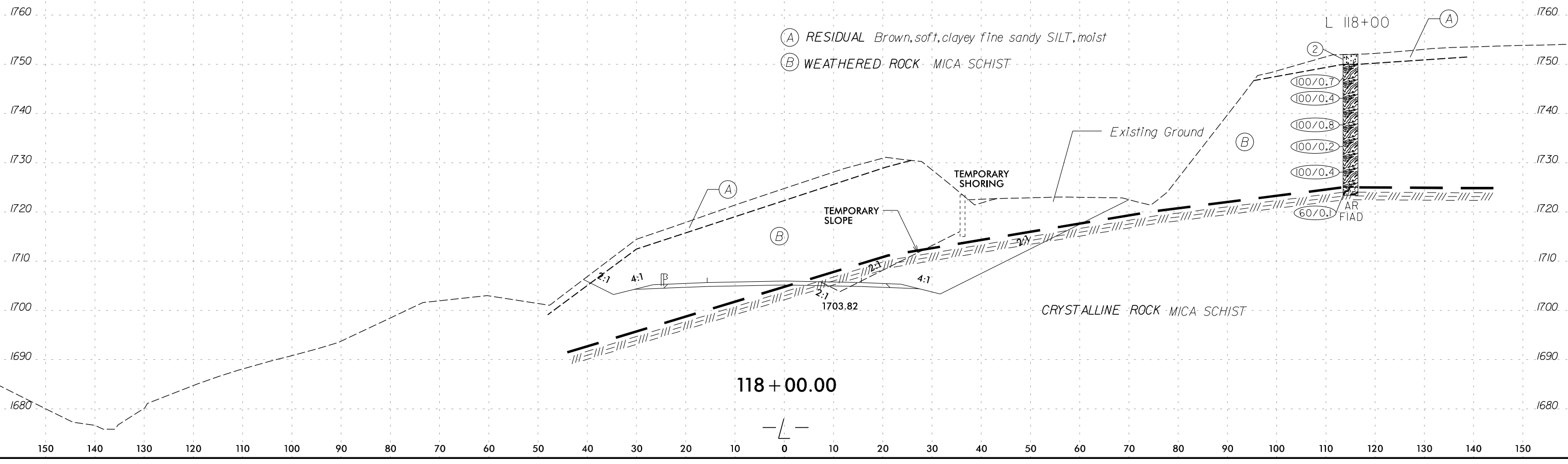
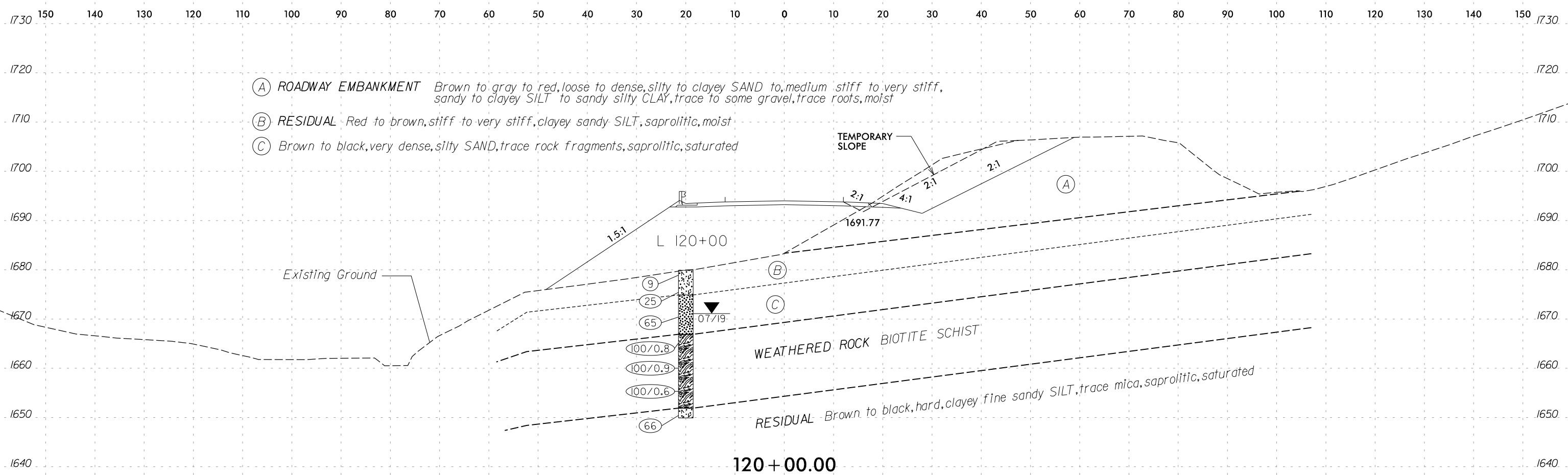
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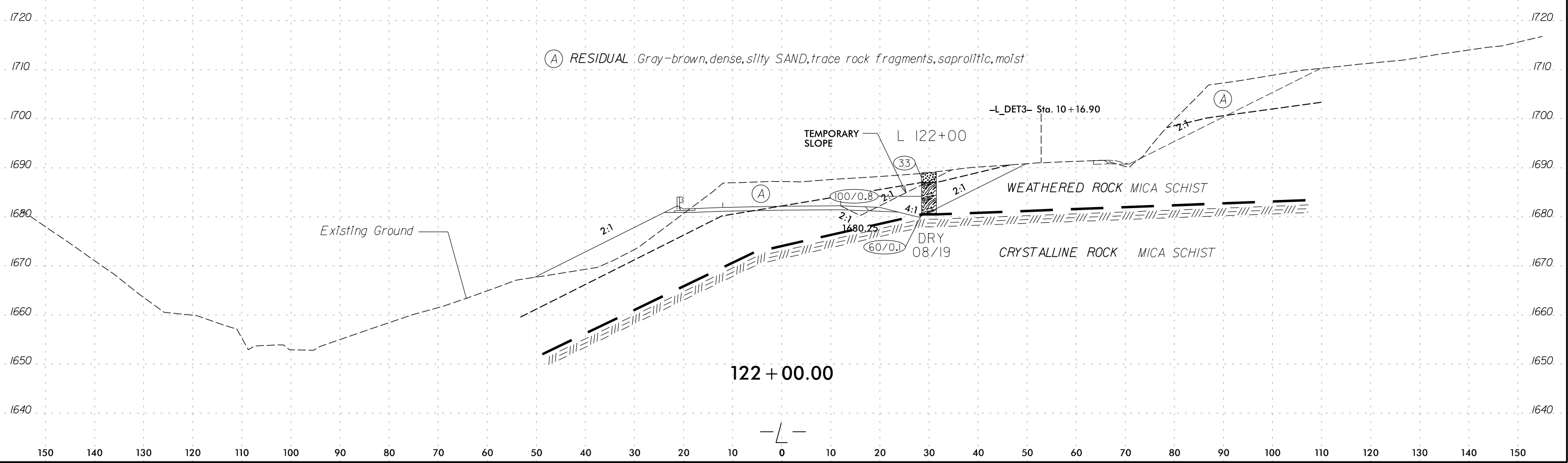
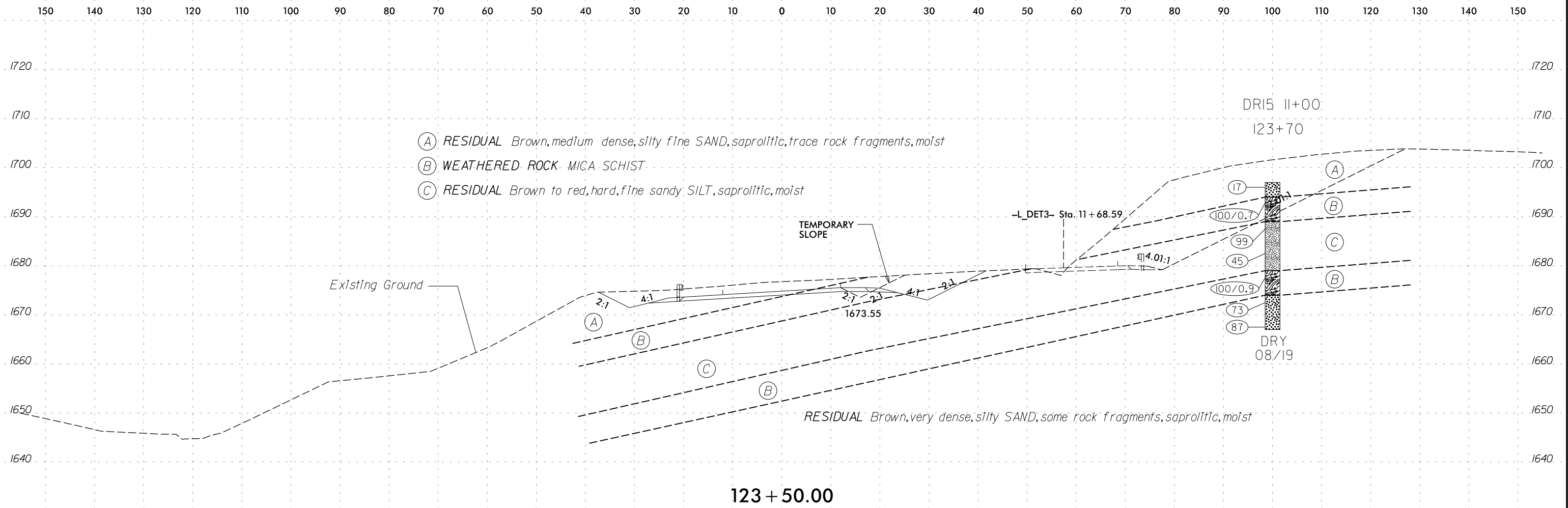
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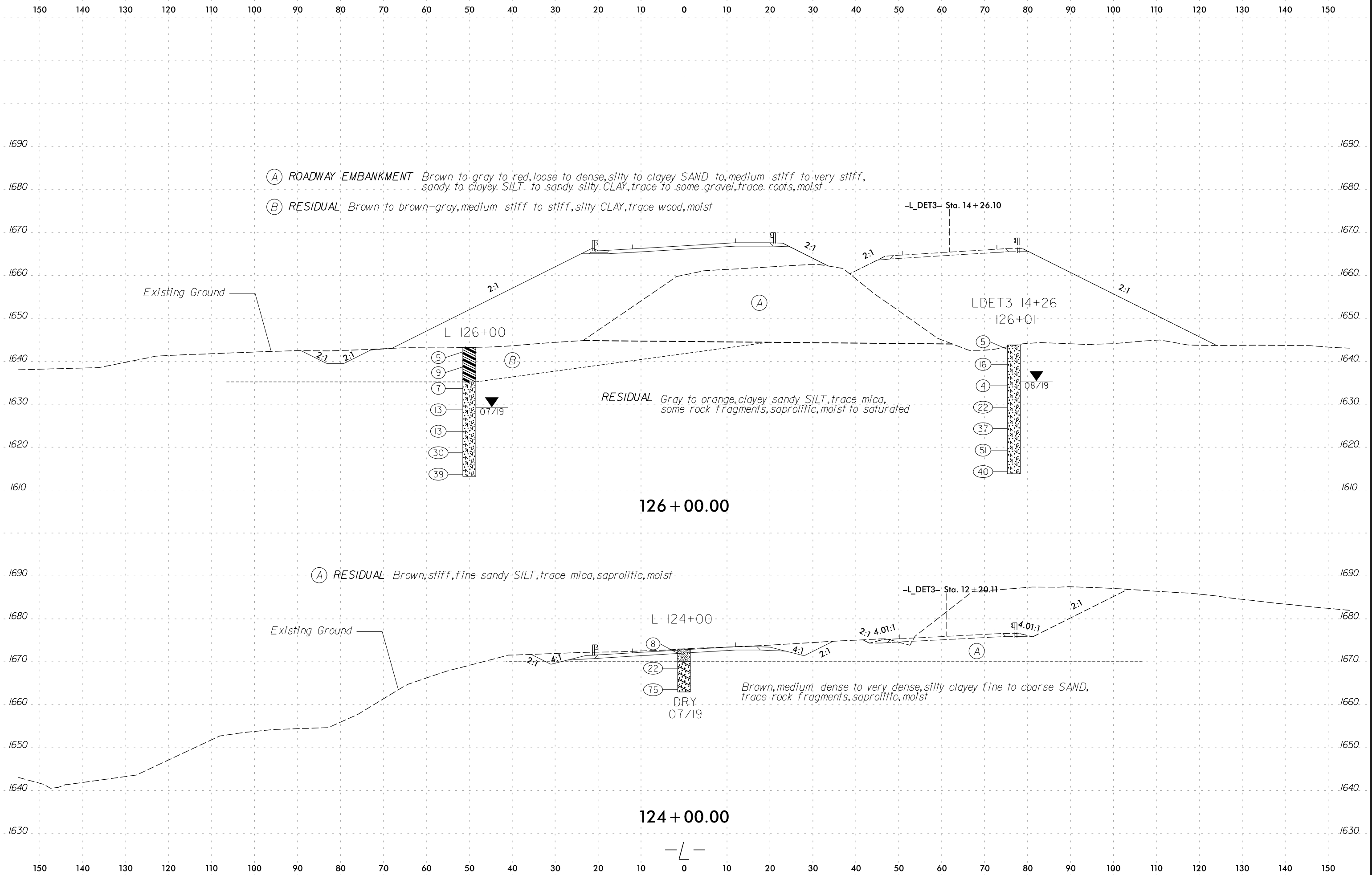
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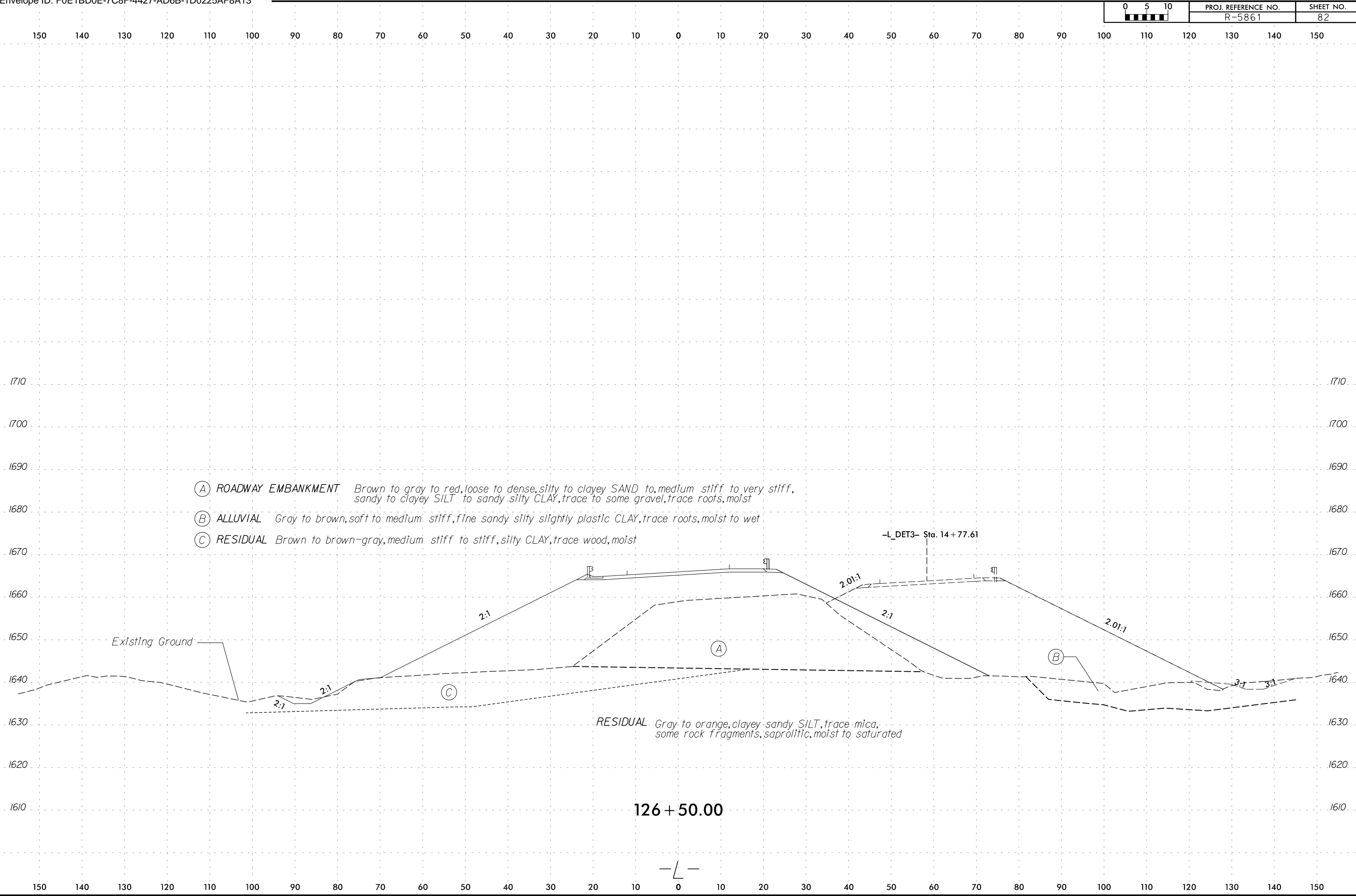


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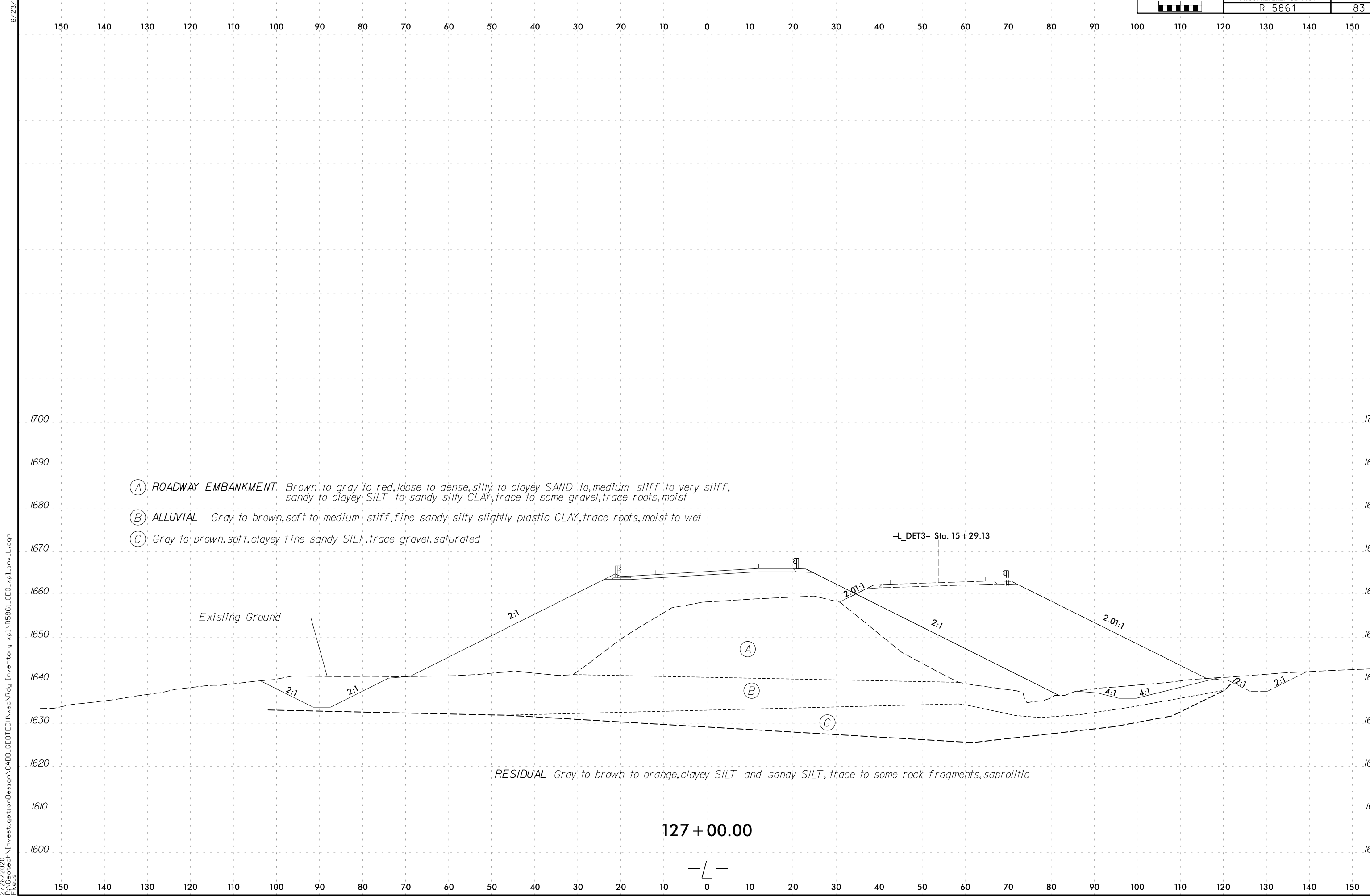


- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) ALLUVIAL *Gray to brown, soft to medium stiff, fine sandy silty slightly plastic CLAY, trace roots, moist to wet*
- (C) RESIDUAL *Brown to brown-gray, medium stiff to stiff, silty CLAY, trace wood, moist*

RESIDUAL *Gray to orange, clayey sandy SILT, trace mica, some rock fragments, saprolitic, moist to saturated*

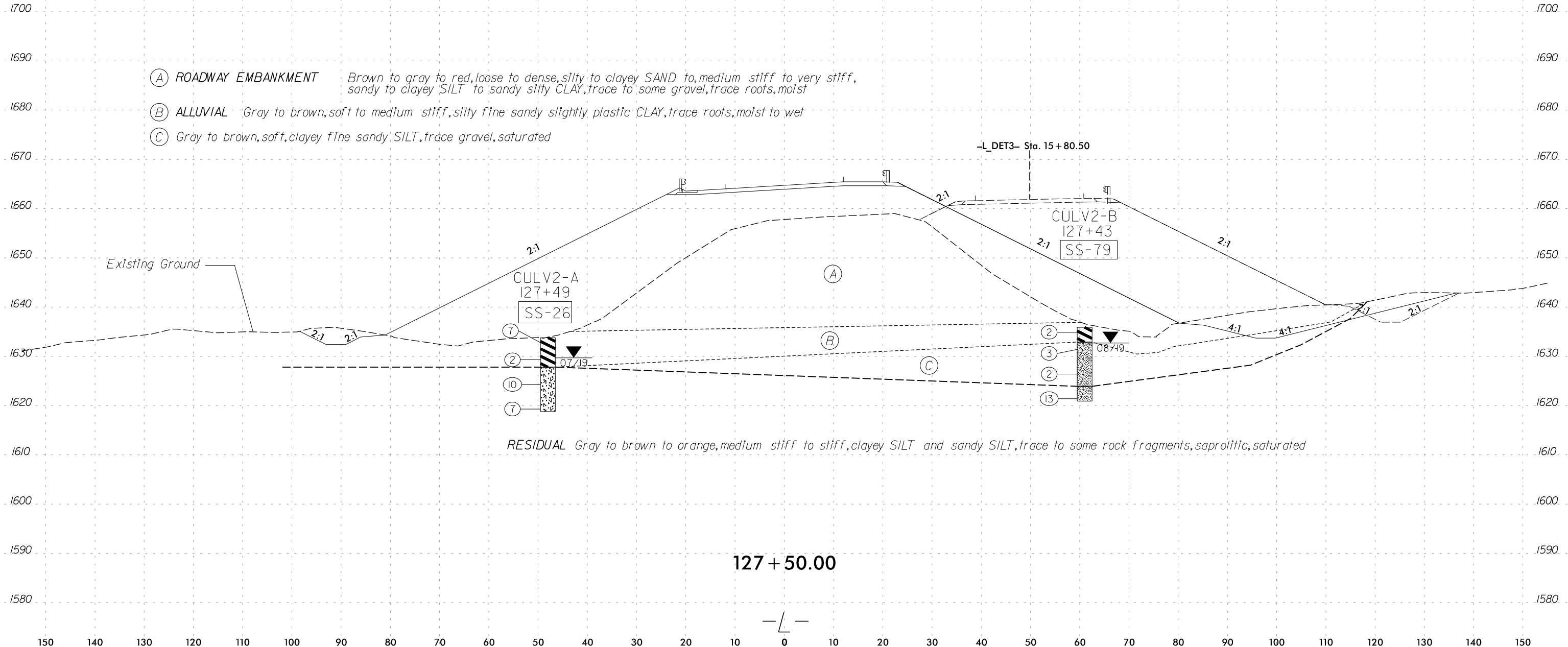
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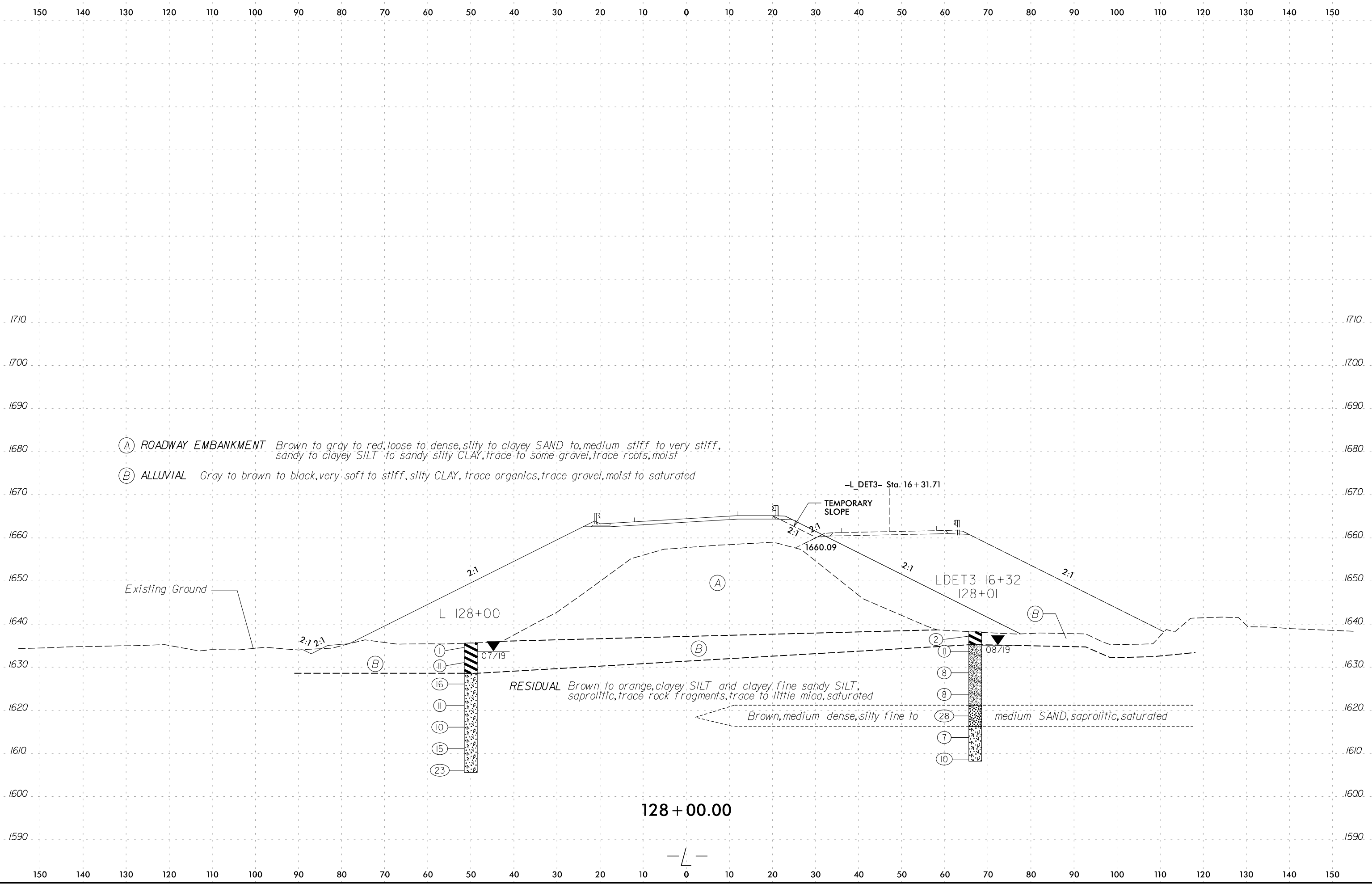


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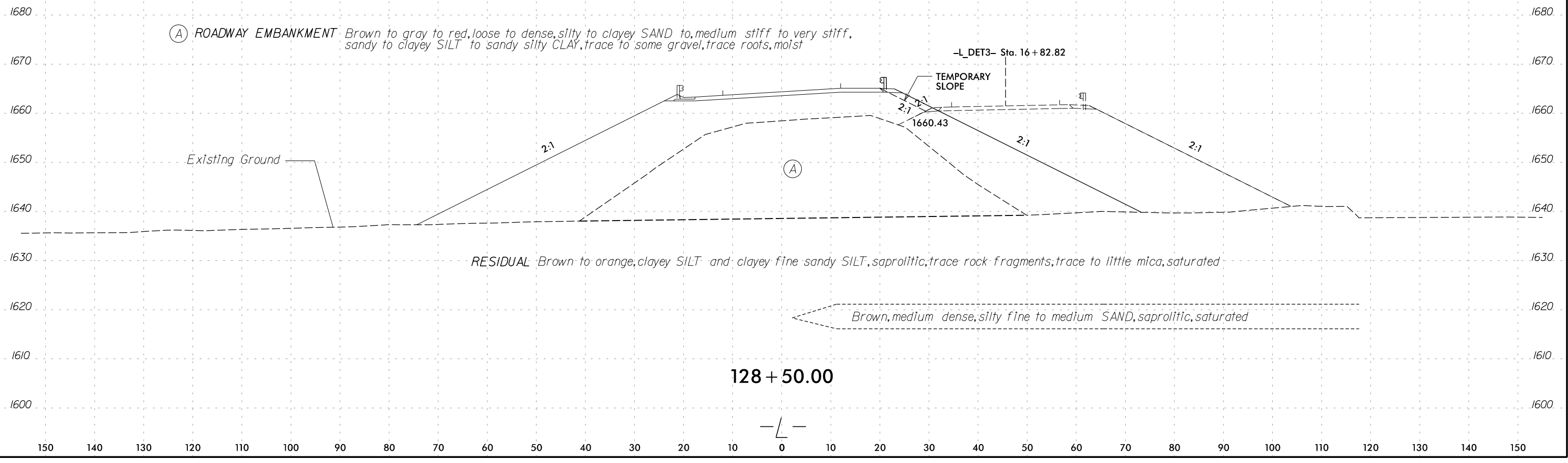
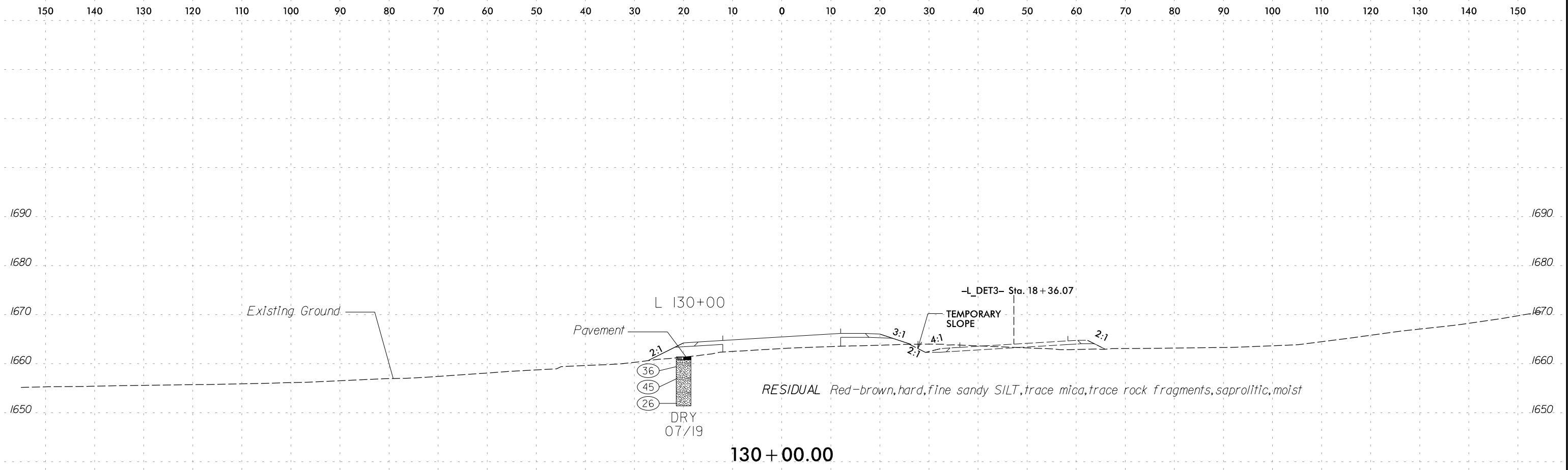
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-26	127+49	48' LT	3.5-5.0	A-7-5 (10)	55	14	9	37	34	20	98	93	63.9	45.8	-
SS-79	127+43	61' RT	3.5-5.0	A-4 (1)	34	7	19	39	18	24	91	82	48	27.5	-



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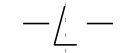
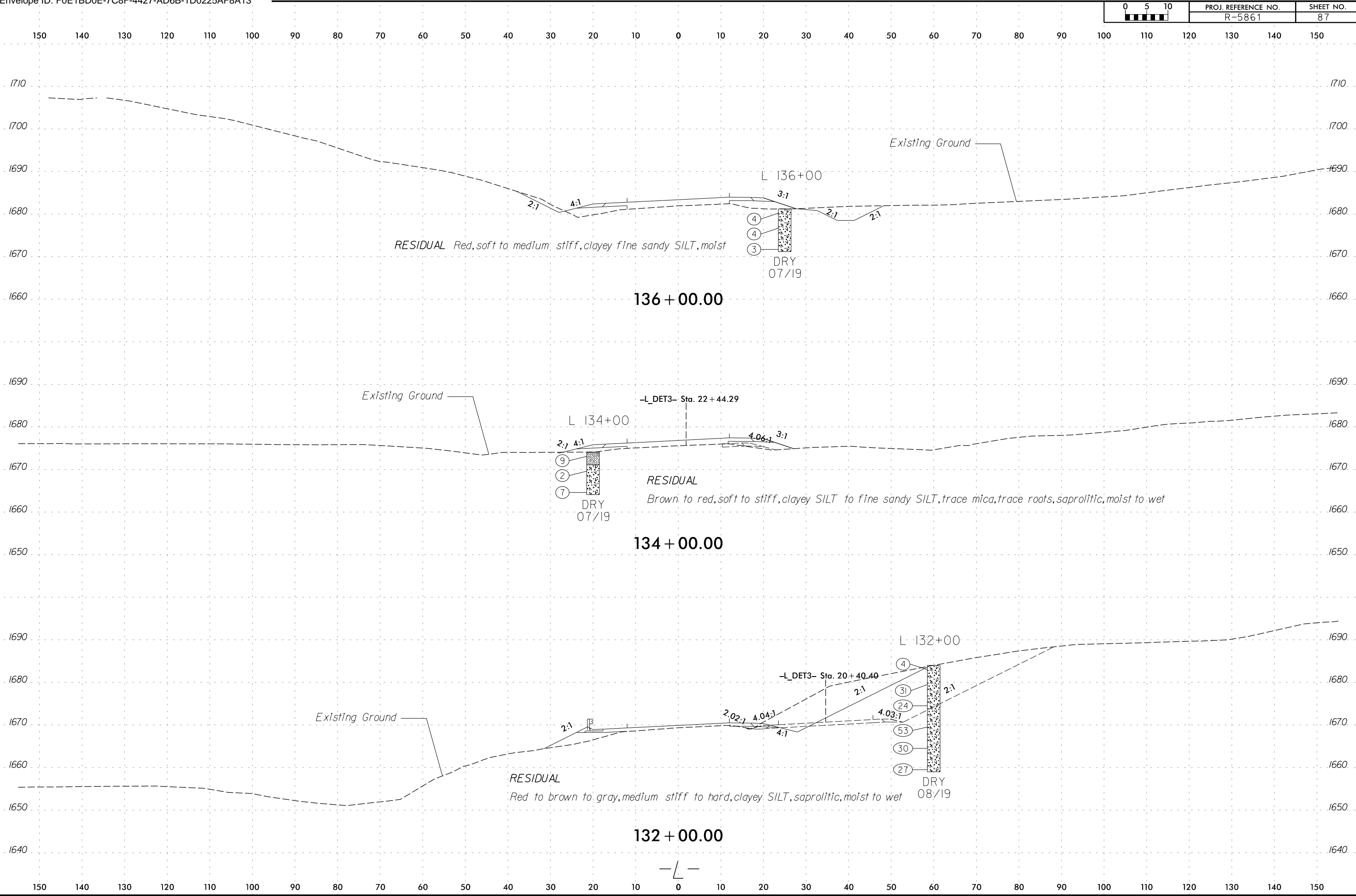


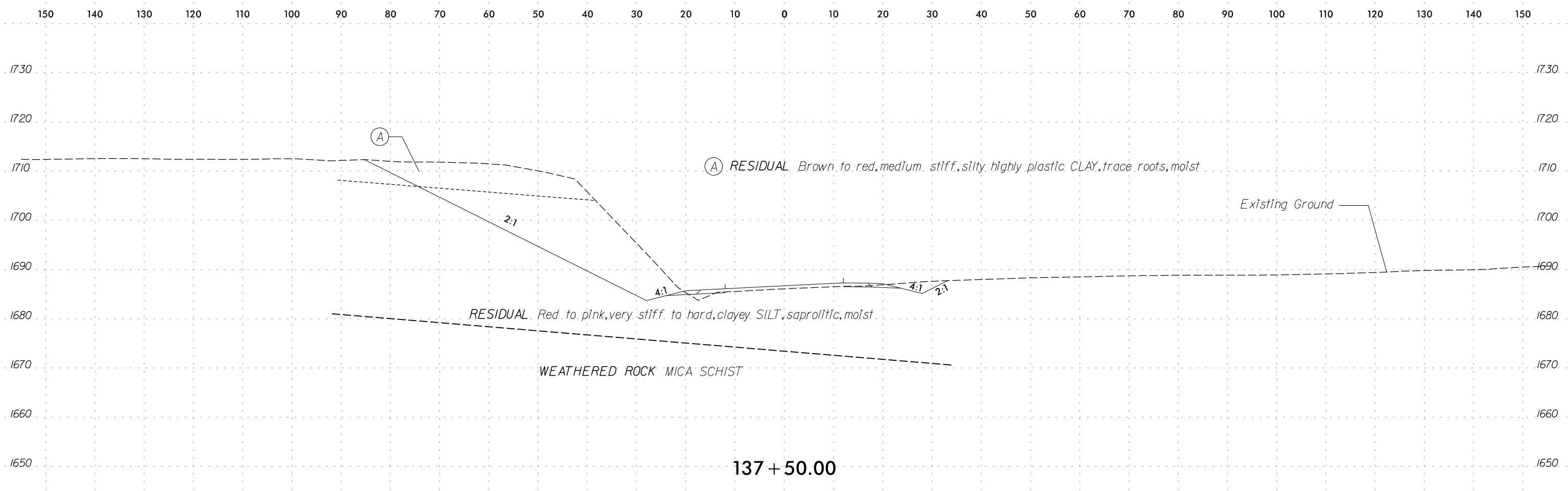
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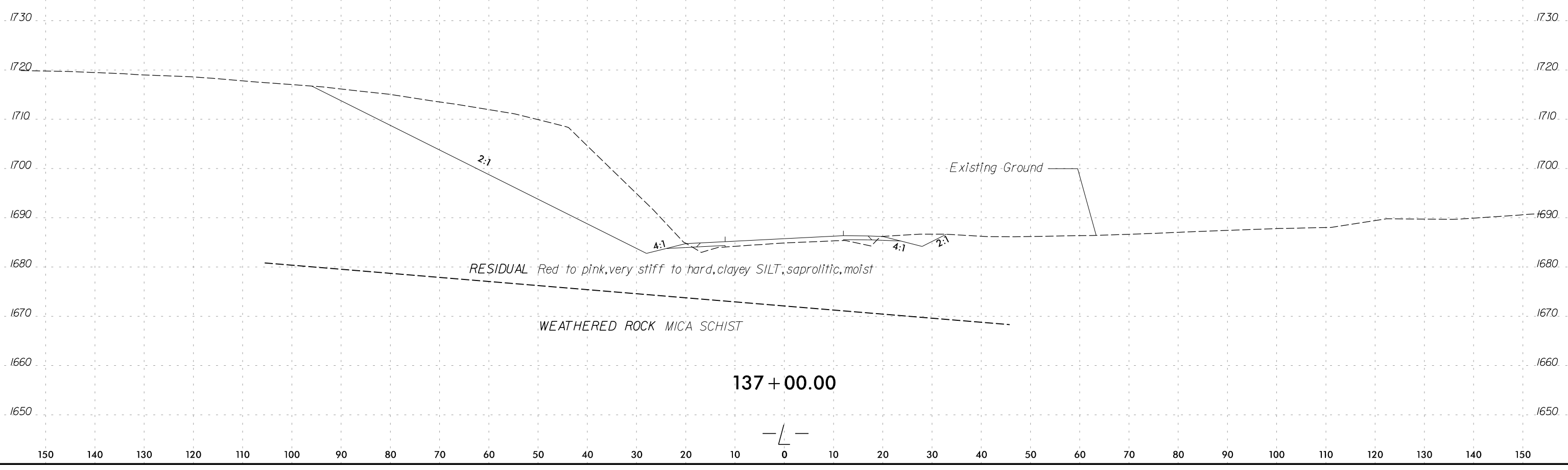
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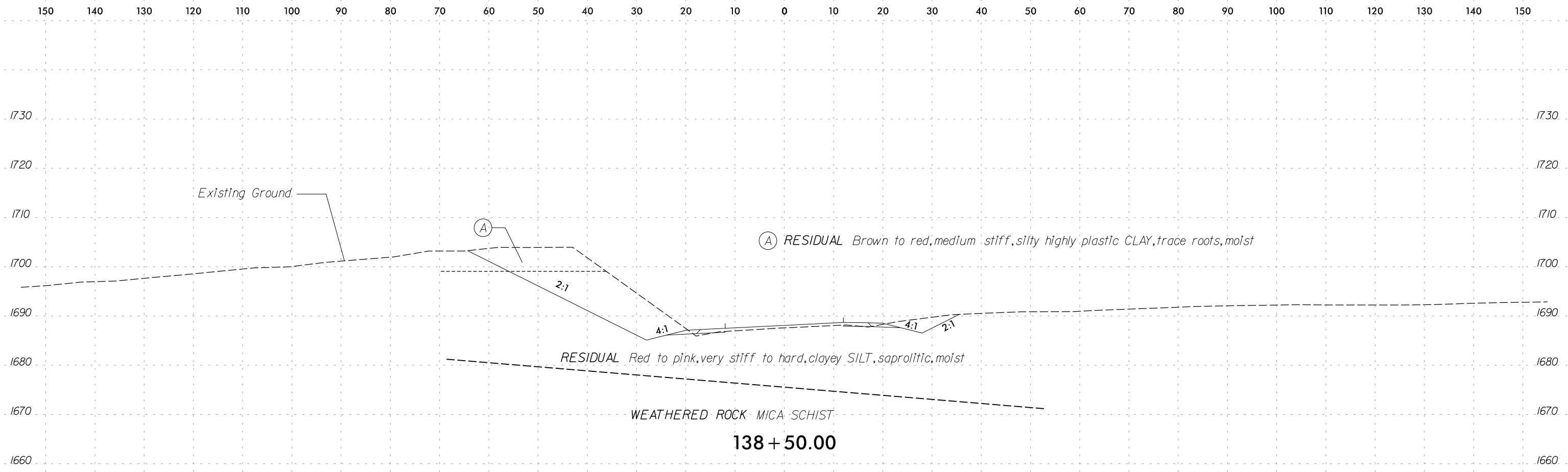


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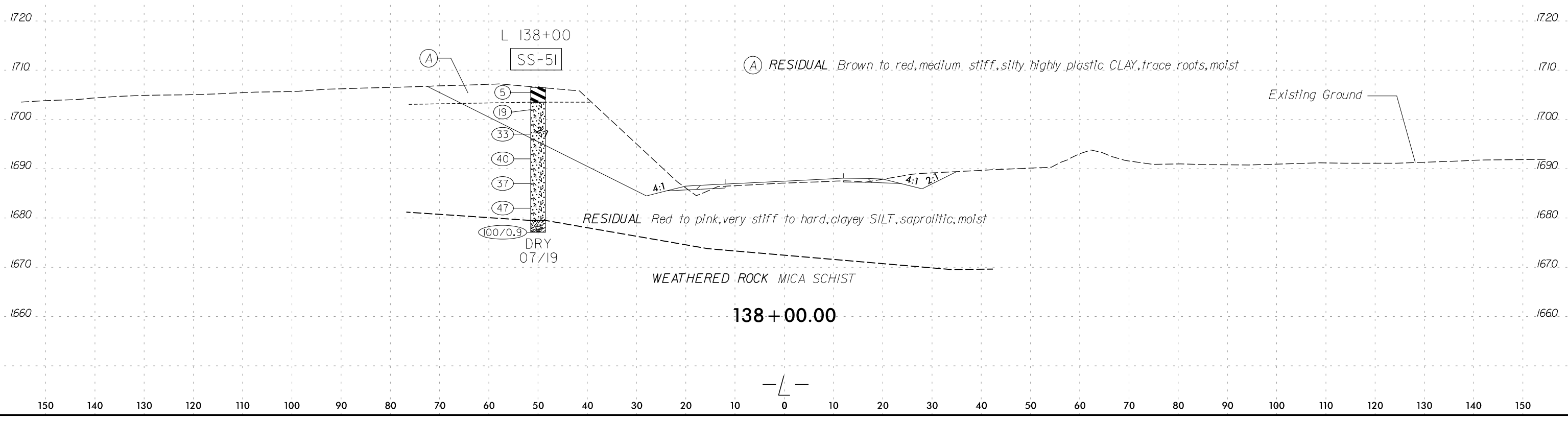


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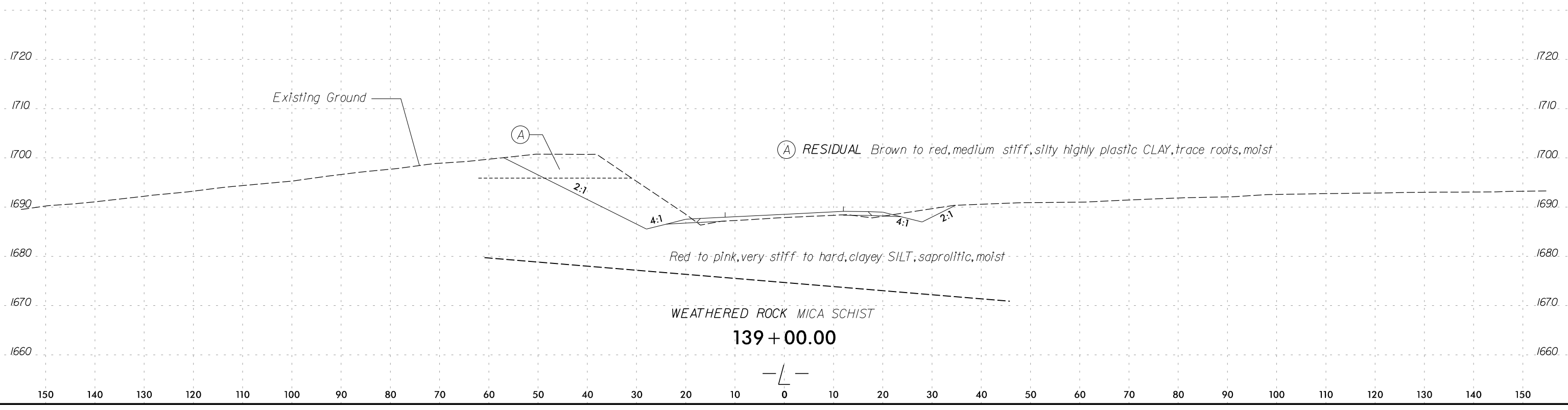
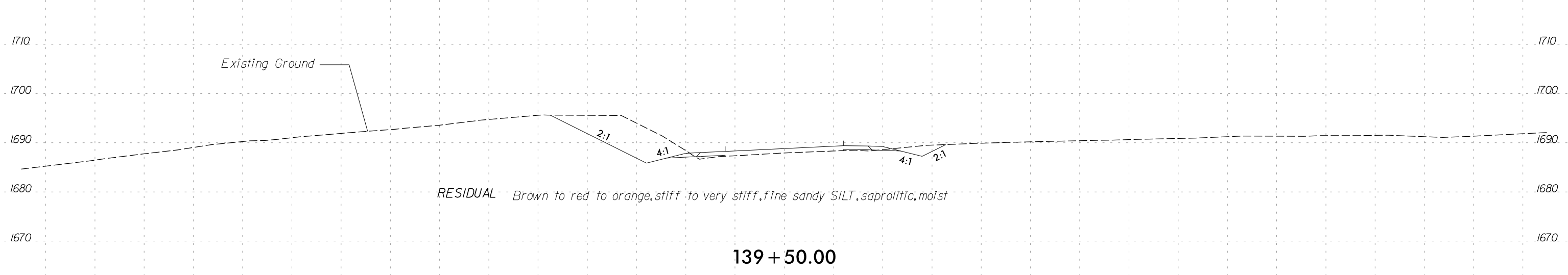
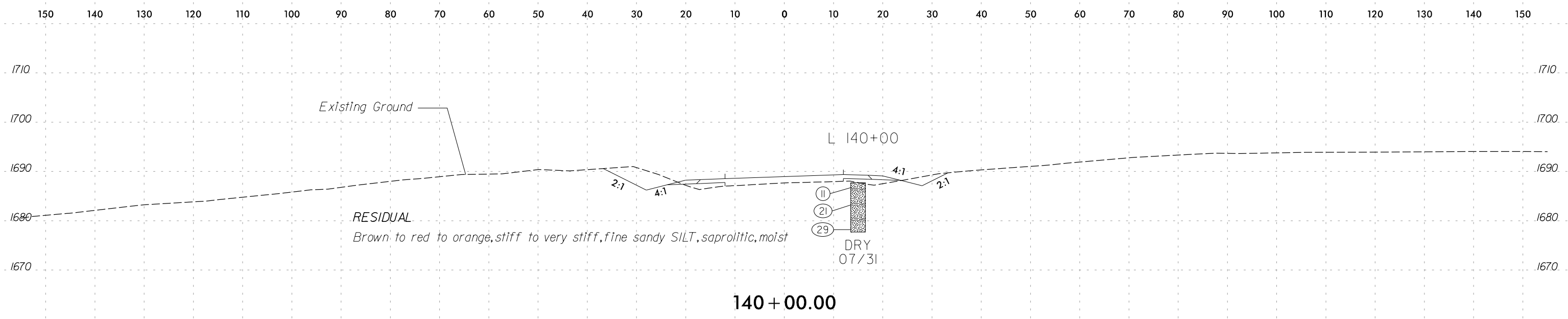
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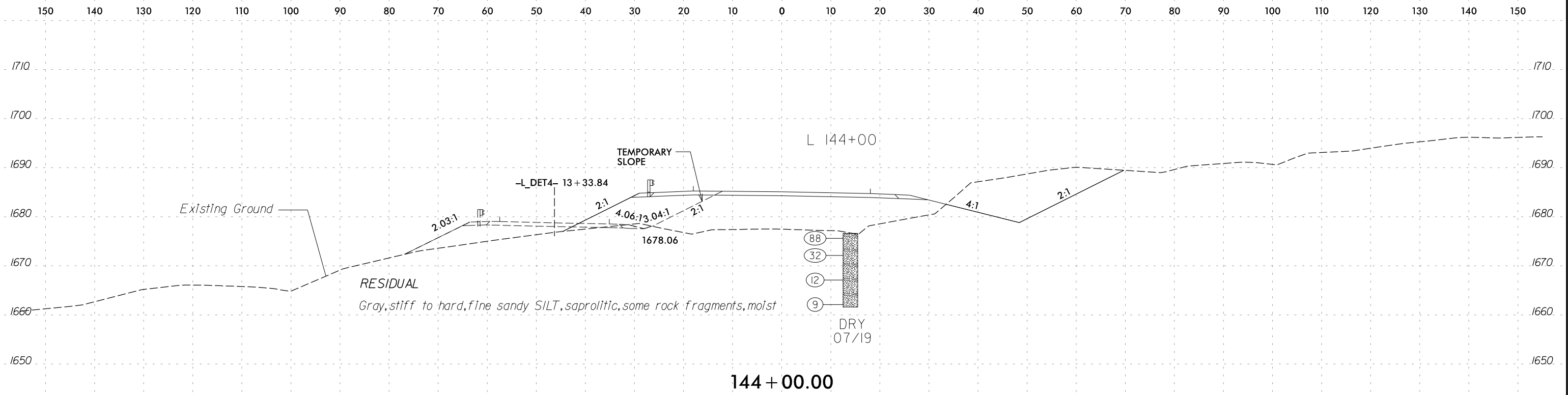
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-51	138+00	50' LT	0.0-1.5	A-7-5 (29)	57	26	1	12	33	54	99	99	93.8	30	-



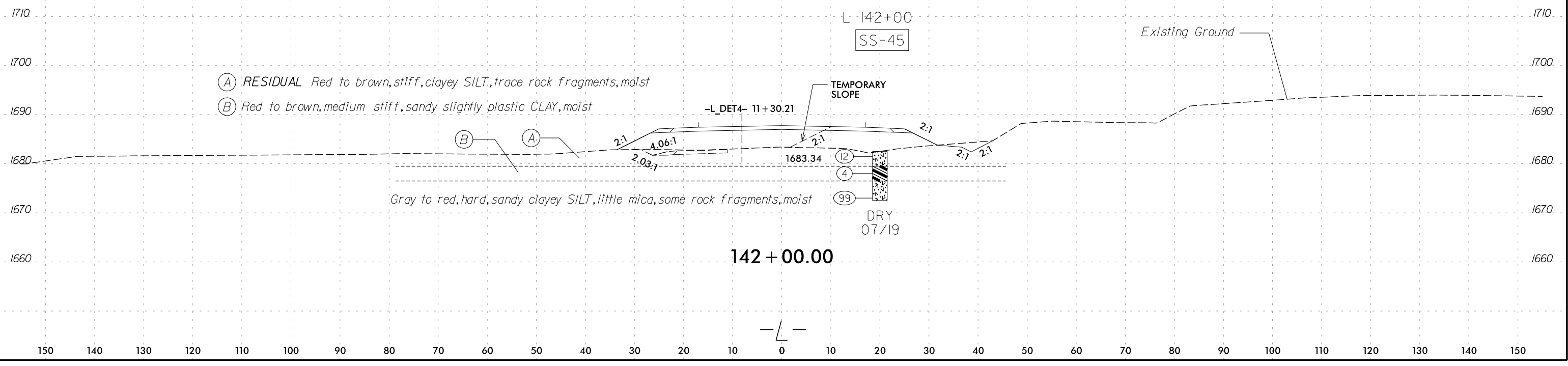
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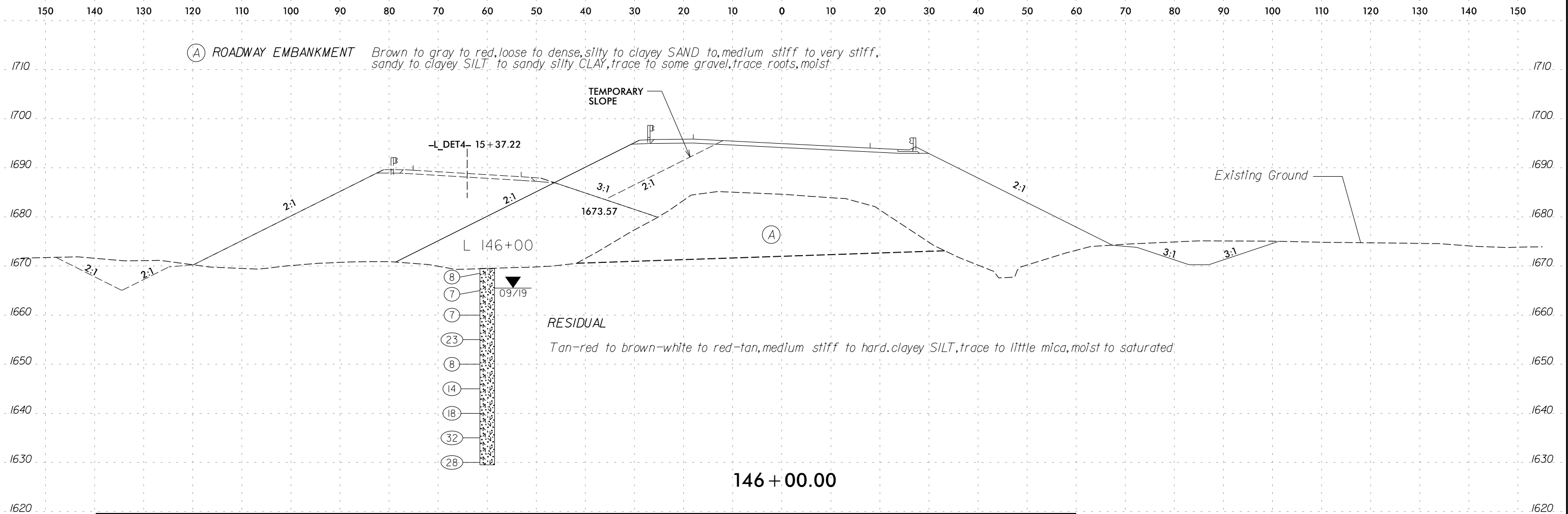
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-45	142+00	20' RT	3.5-5.0	A-6 (4)	38	11	26	17	30	27	85	67	53	20.5	-

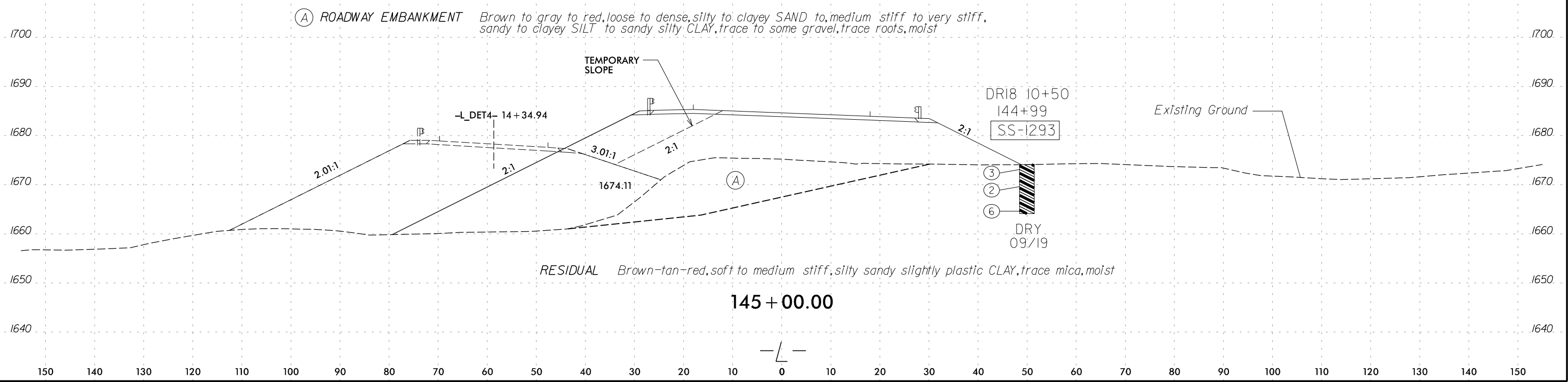


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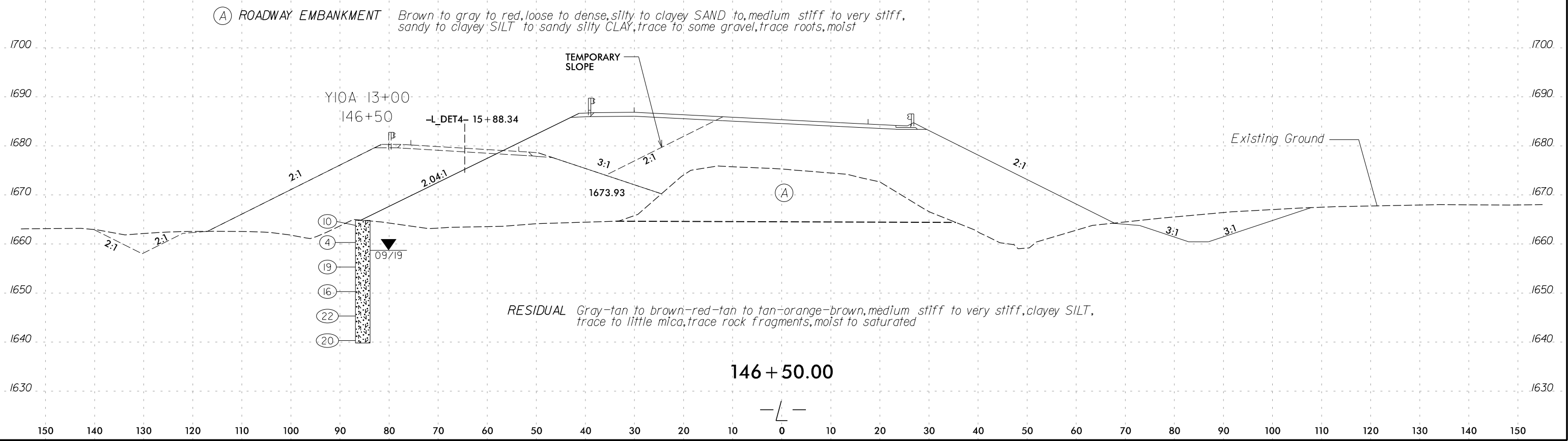
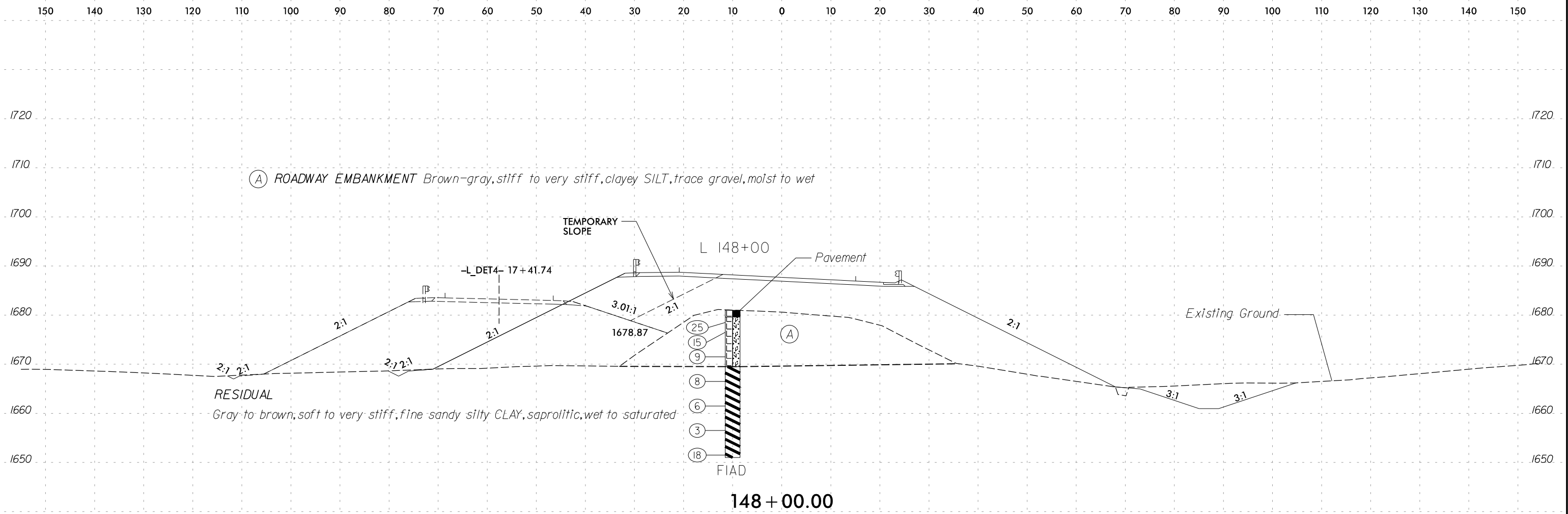
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1293	144+99	50' RT	3.5-5.0	A-6 (3)	40	11	22	12	32	34	69	57	47.4	24.6	-

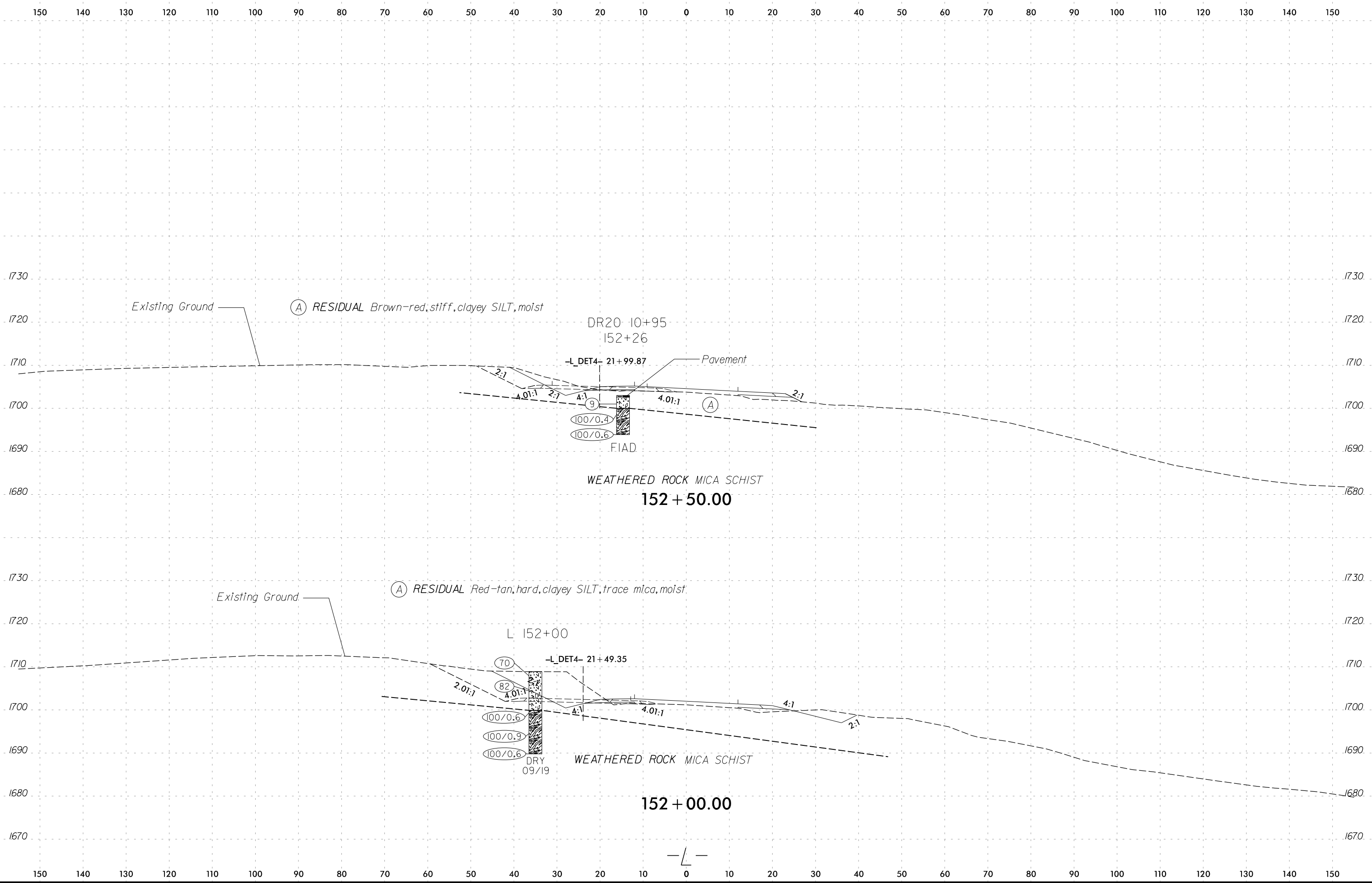


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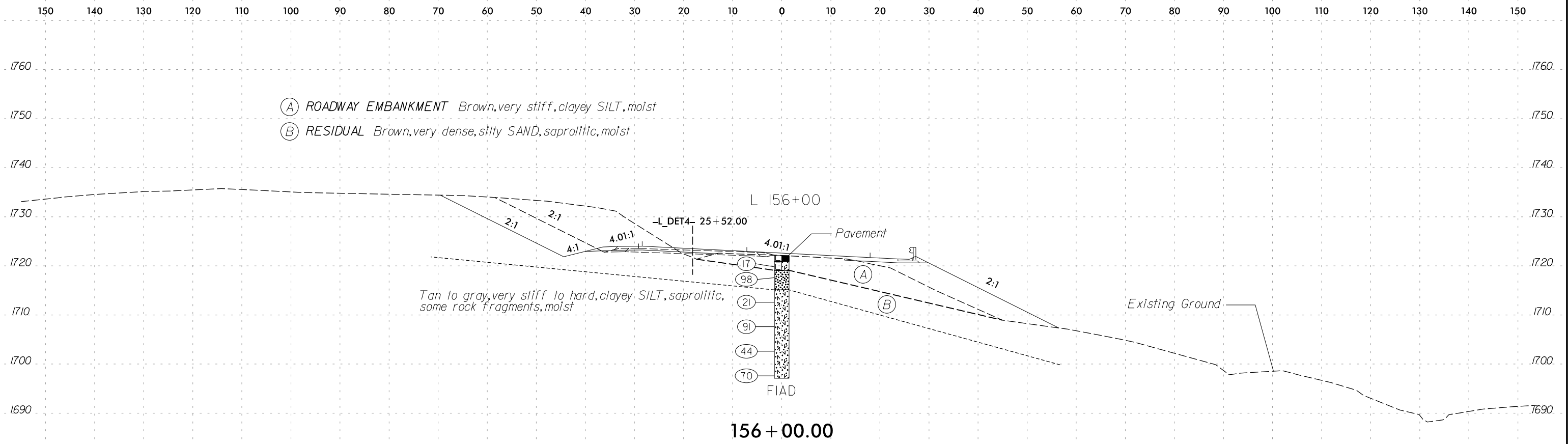
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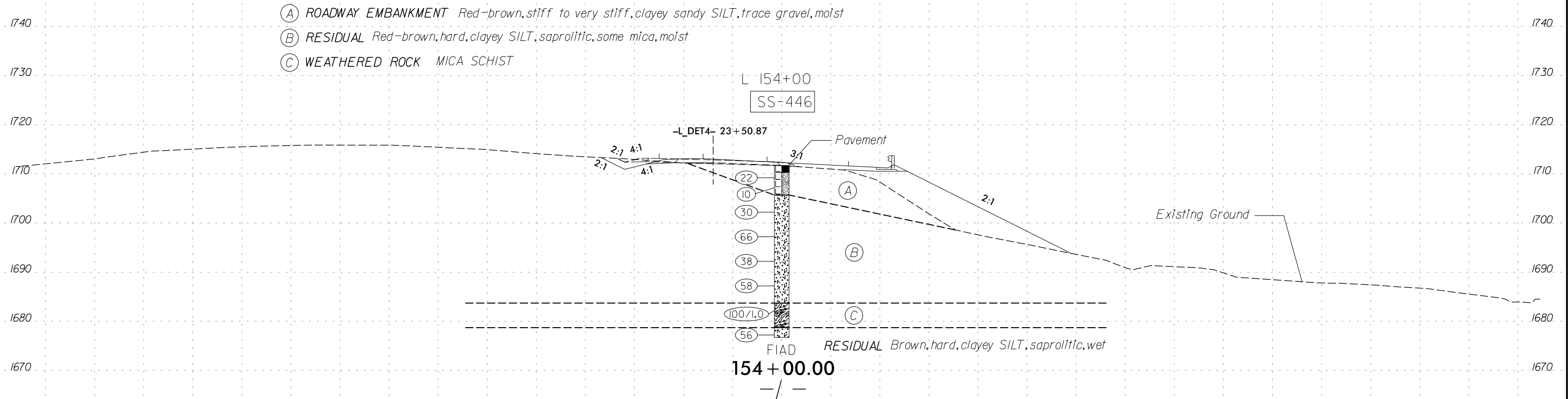
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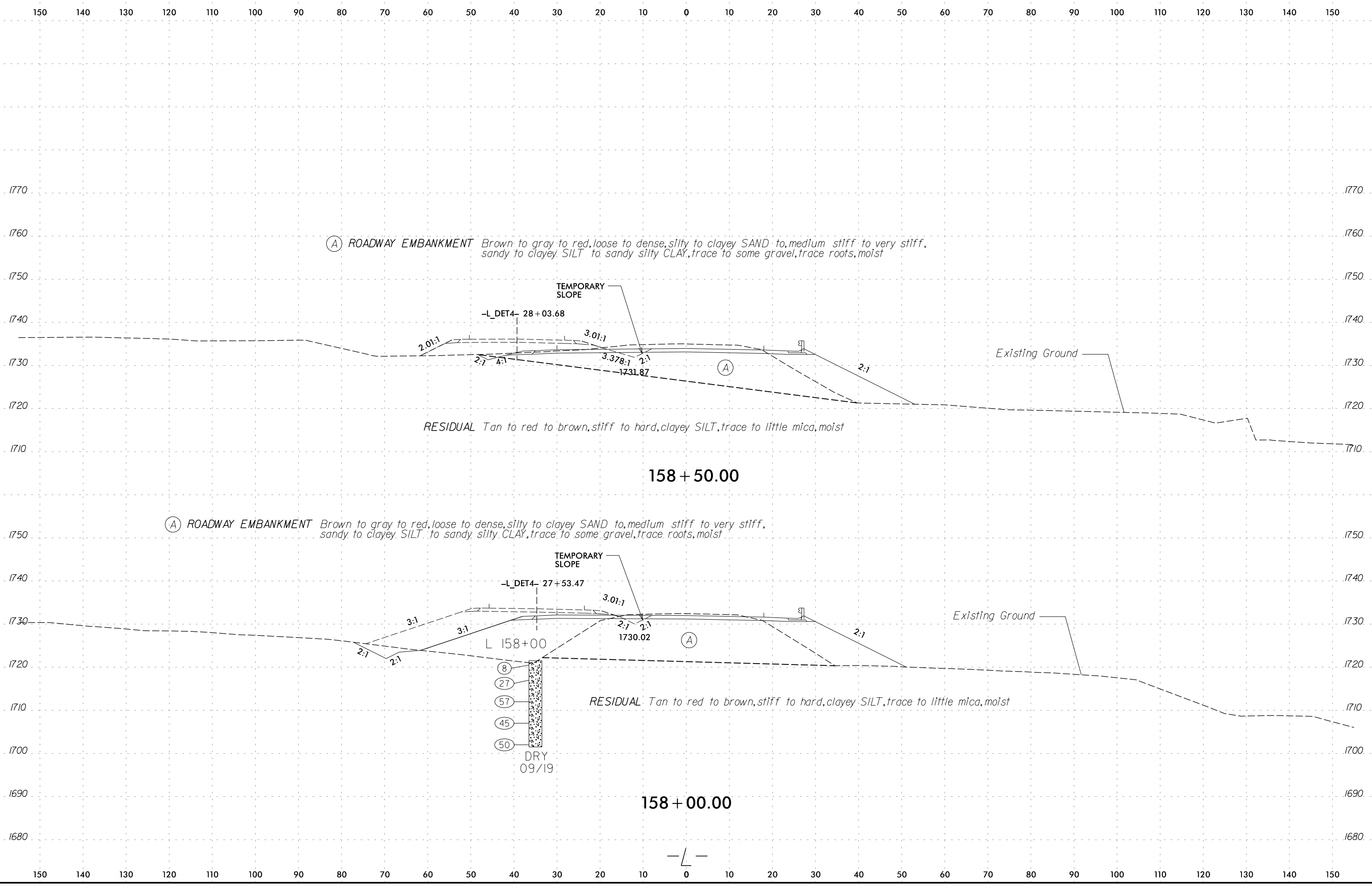
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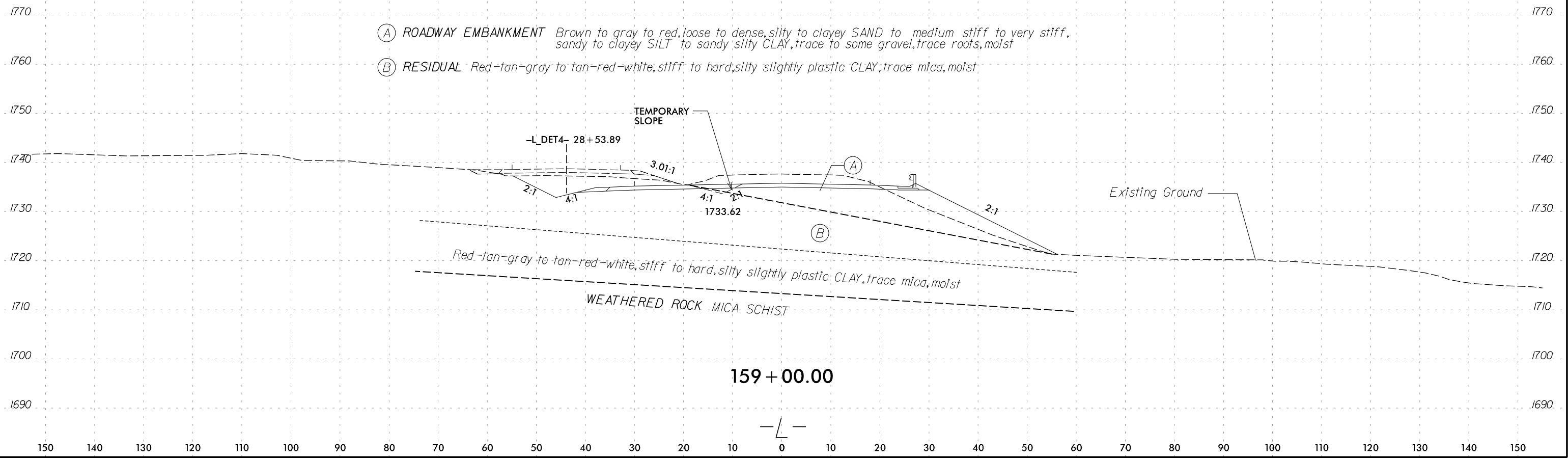
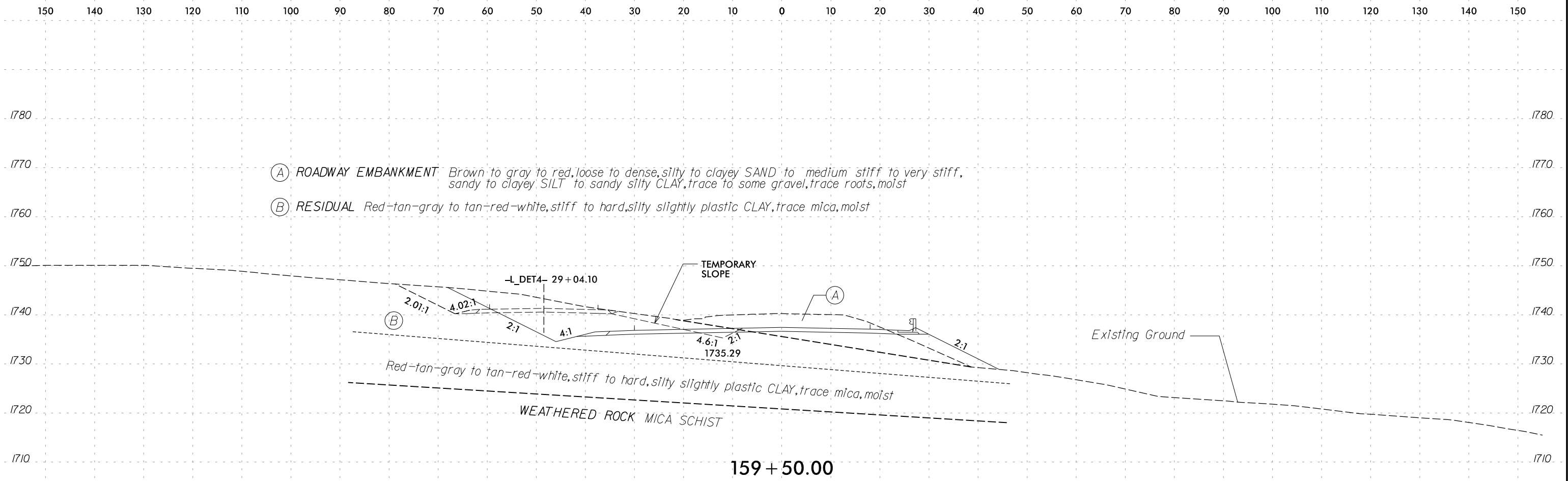
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SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-446	154+00	0	1.5-3.0	A-4 (0)	33	3	34	21	27	18	92	68	46.5	13.1	-



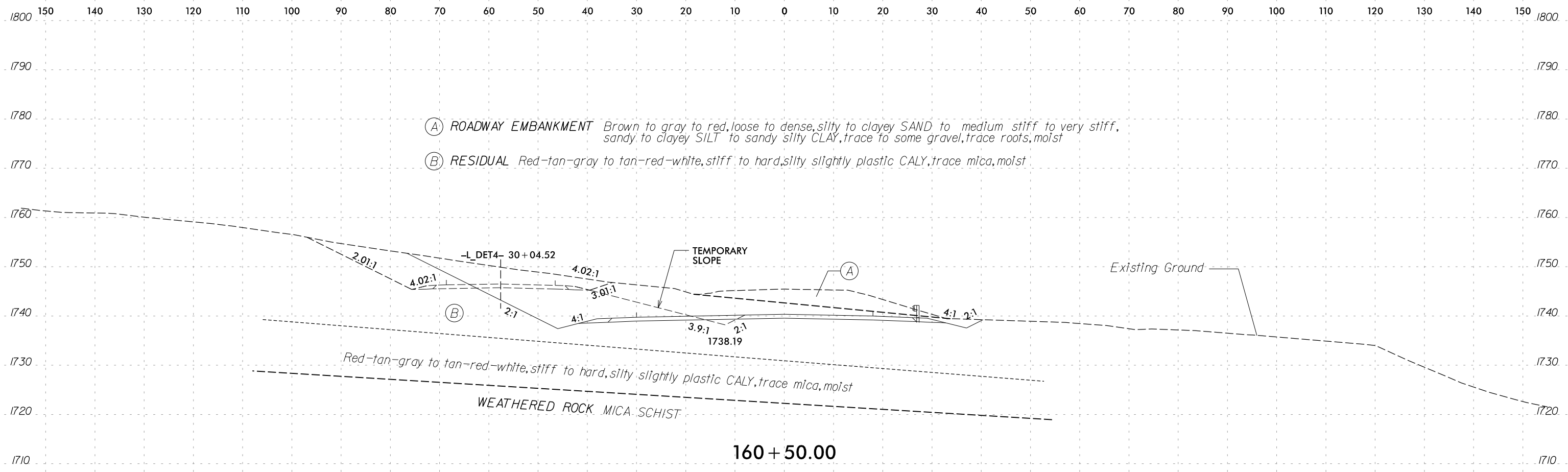
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- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Red-tan-gray to tan-red-white, stiff to hard, silty slightly plastic CALY, trace mica, moist*

Red-tan-gray to tan-red-white, stiff to hard, silty slightly plastic CALY, trace mica, moist
 WEATHERED ROCK MICA SCHIST

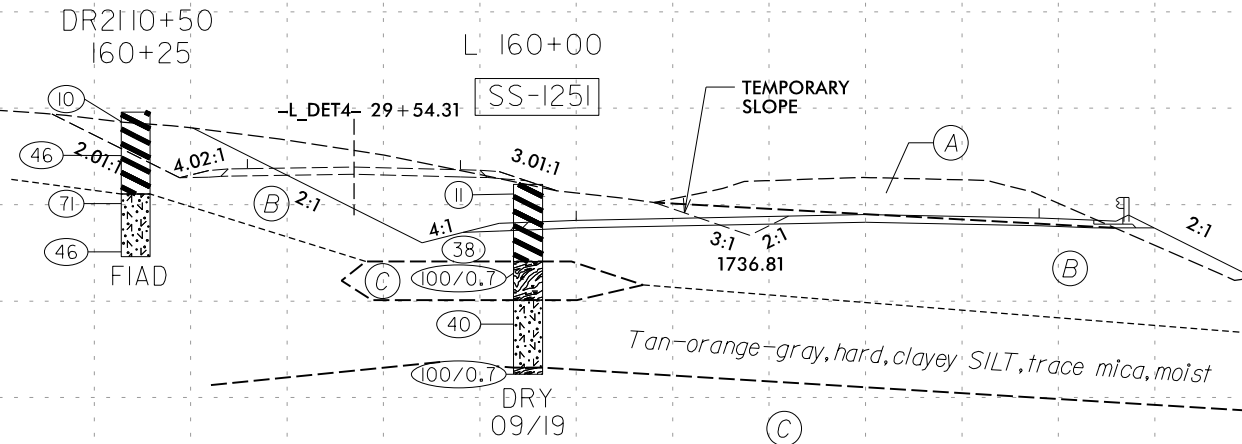
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SOIL TEST RESULTS															
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1251	160+00	35' LT	0.0-1.5	A-7-5 (14)	44	11	1	15	52	32	100	100	94.3	12.3	-

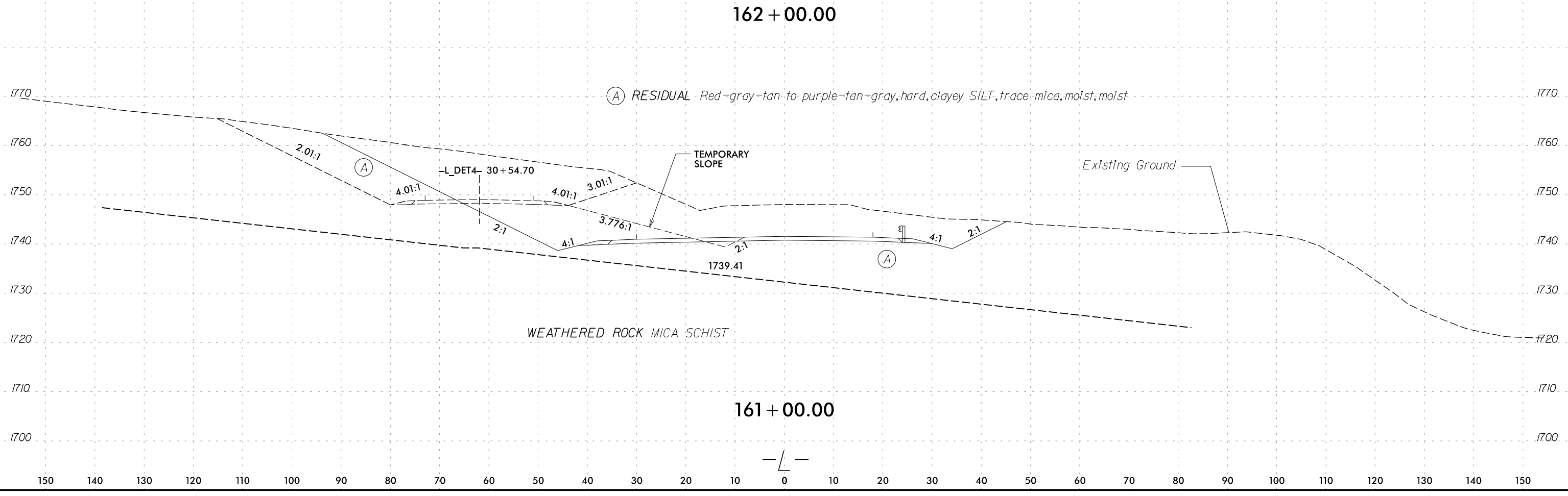
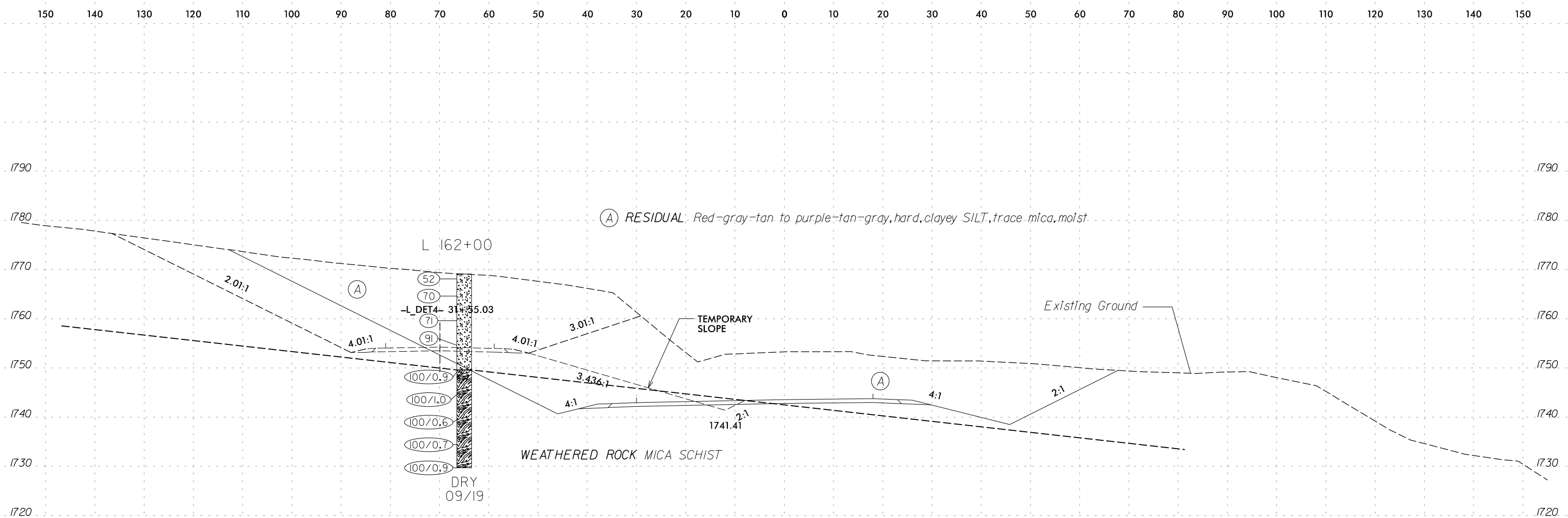
- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Red-tan-gray to tan-red-white, stiff to hard, silty slightly plastic CLAY, trace mica, moist*
- (C) WEATHERED ROCK MICA SCHIST

Tan-orange-gray, hard, clayey SILT, trace mica, moist

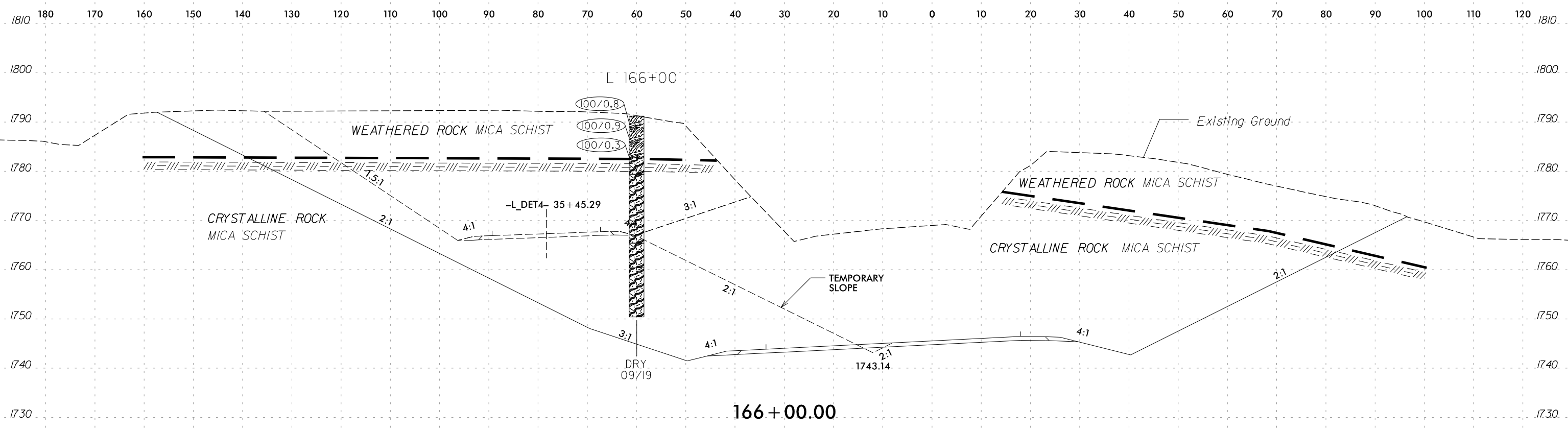
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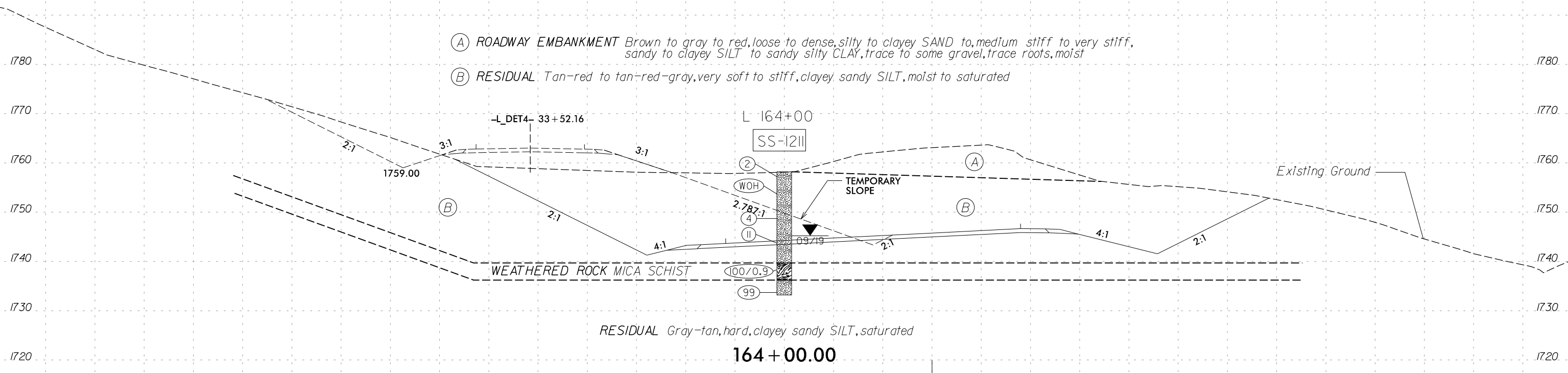


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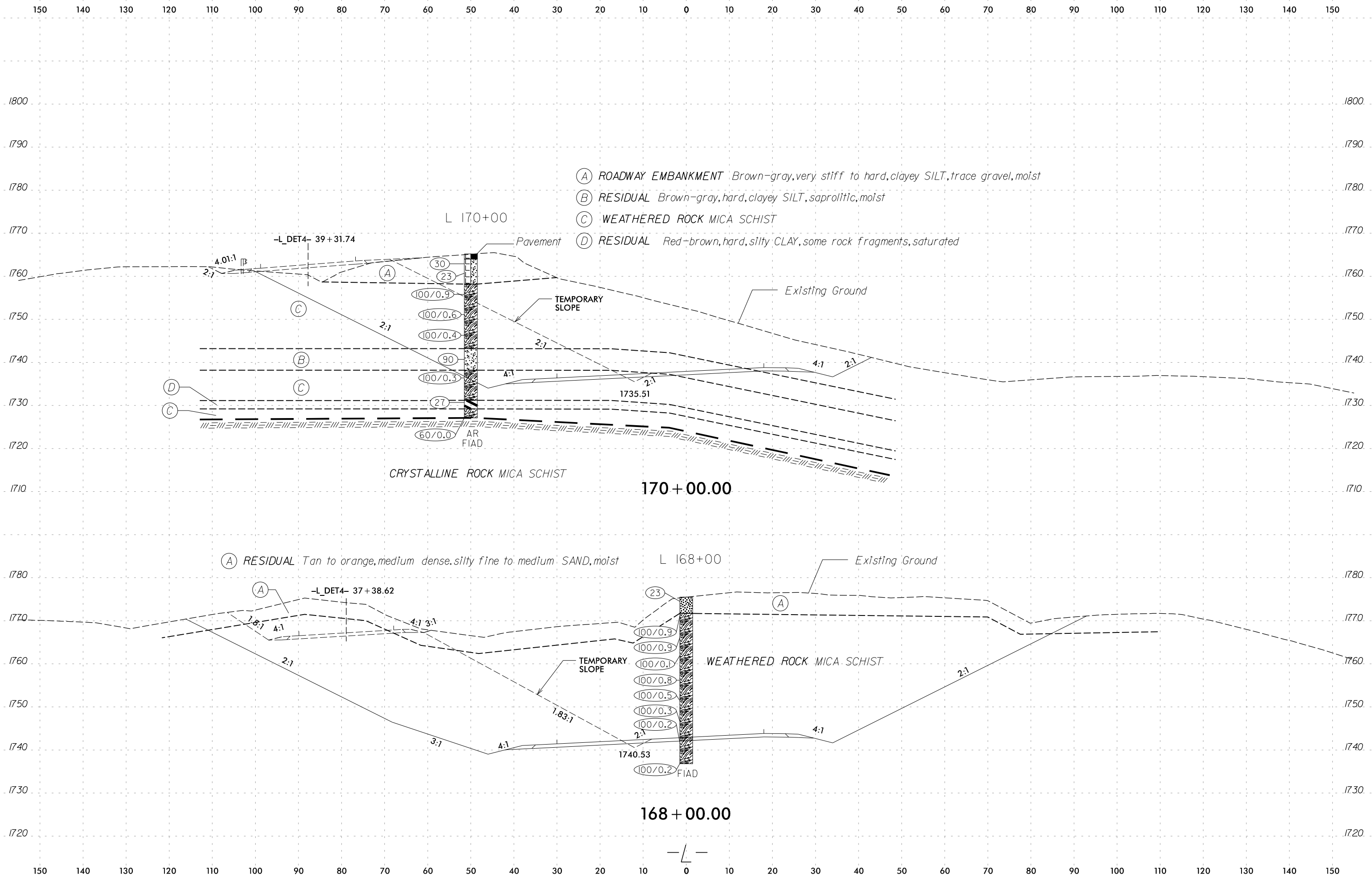
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1211	164+00	30' LT	3.5-5.0	A-4 (2)	40	6	13	28	39	20	78	71	54.5	21.9	-

- (A) ROADWAY EMBANKMENT Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist
- (B) RESIDUAL Tan-red to tan-red-gray, very soft to stiff, clayey sandy SILT, moist to saturated



RESIDUAL Gray-tan, hard, clayey sandy SILT, saturated

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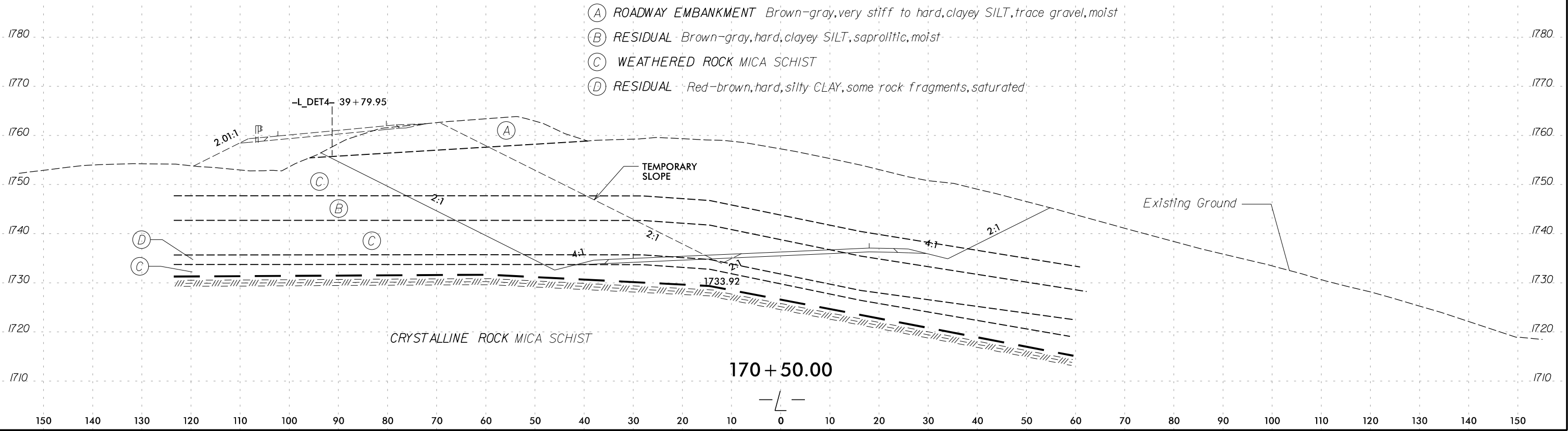
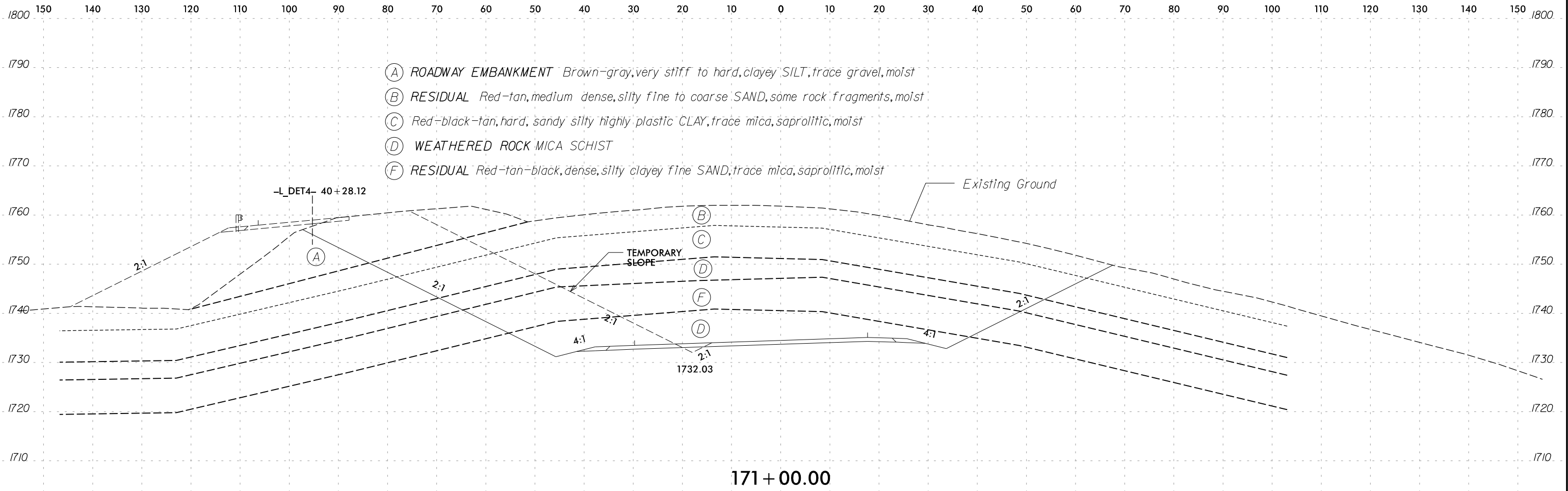


- (A) ROADWAY EMBANKMENT *Brown-gray, very stiff to hard, clayey SILT, trace gravel, moist*
- (B) RESIDUAL *Brown-gray, hard, clayey SILT, saprolitic, moist*
- (C) WEATHERED ROCK MICA SCHIST
- (D) RESIDUAL *Red-brown, hard, silty CLAY, some rock fragments, saturated*

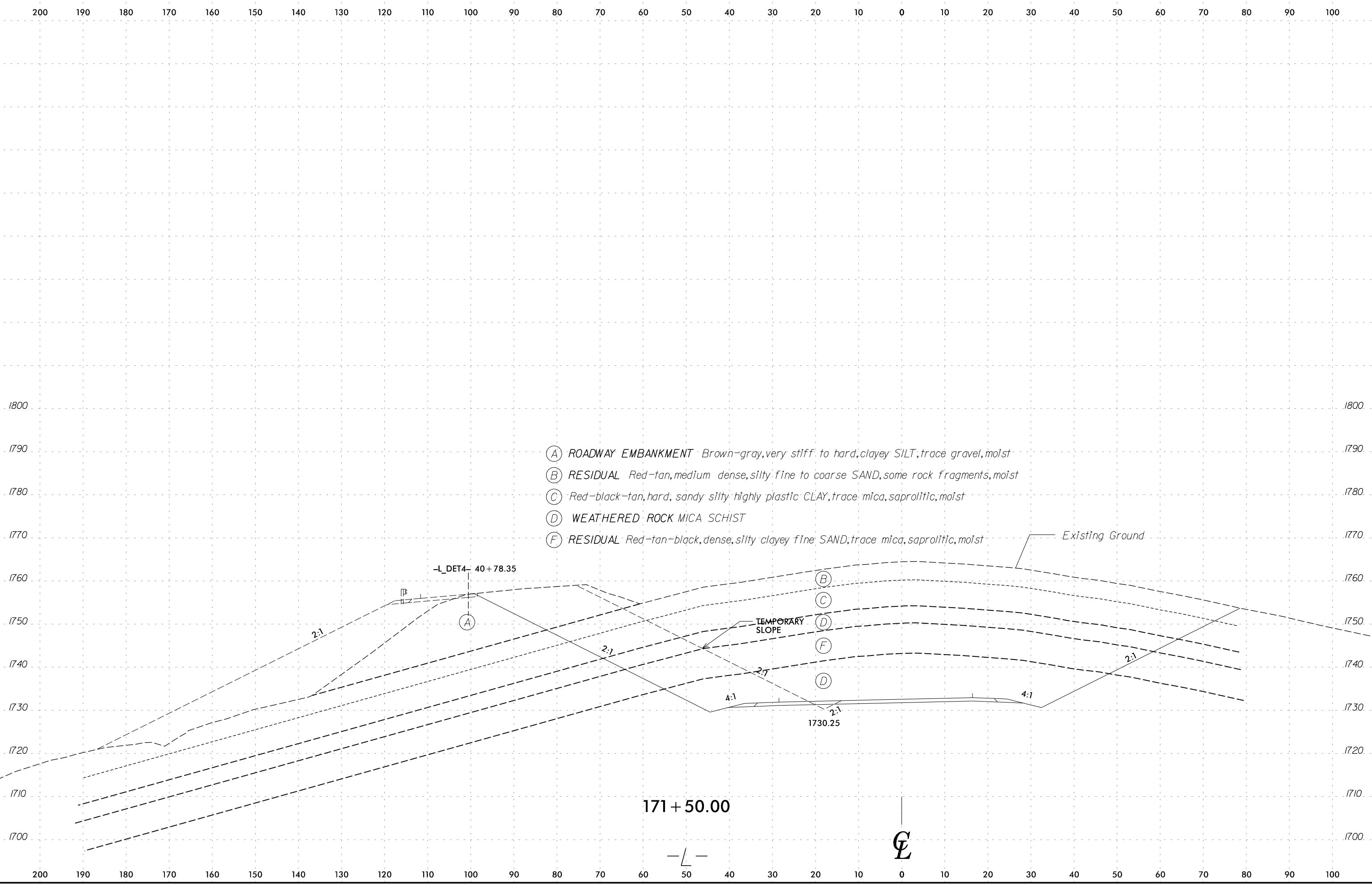
(A) RESIDUAL *Tan to orange, medium dense, silty fine to medium SAND, moist*

WEATHERED ROCK MICA SCHIST

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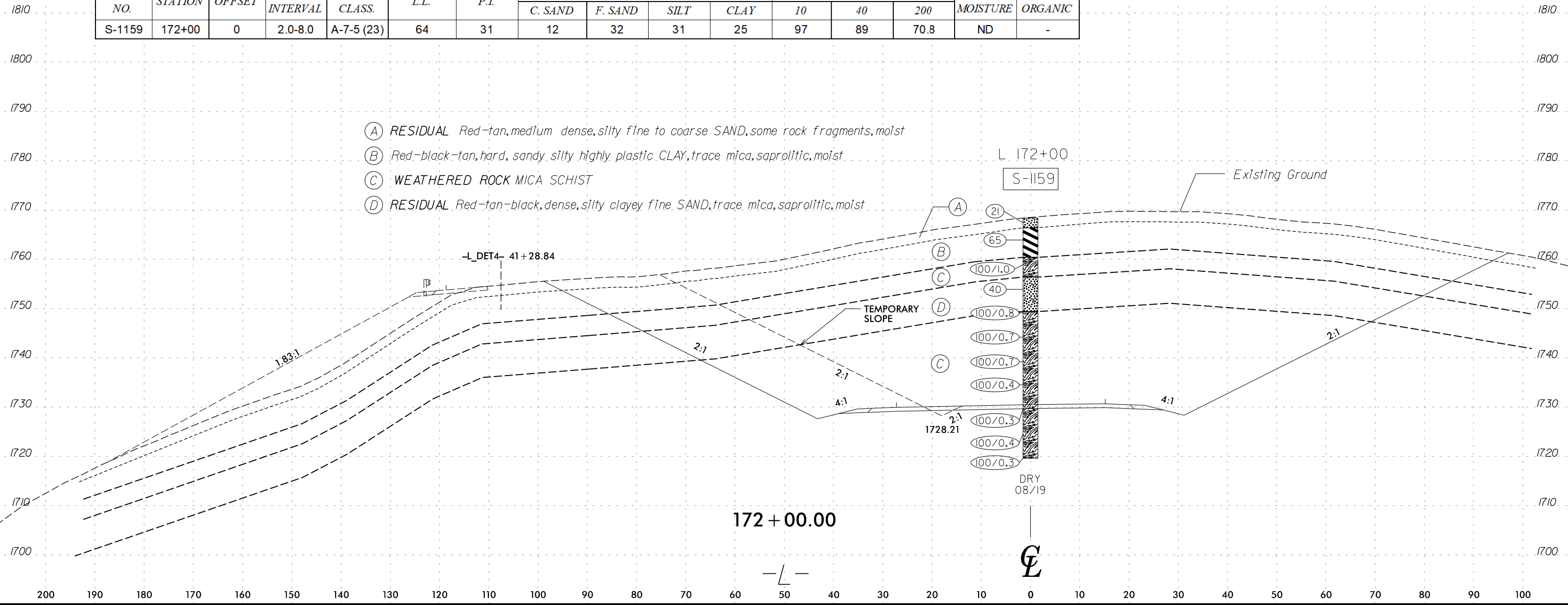


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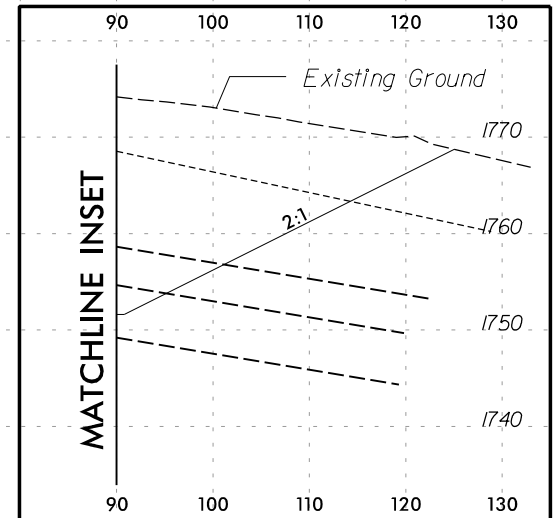
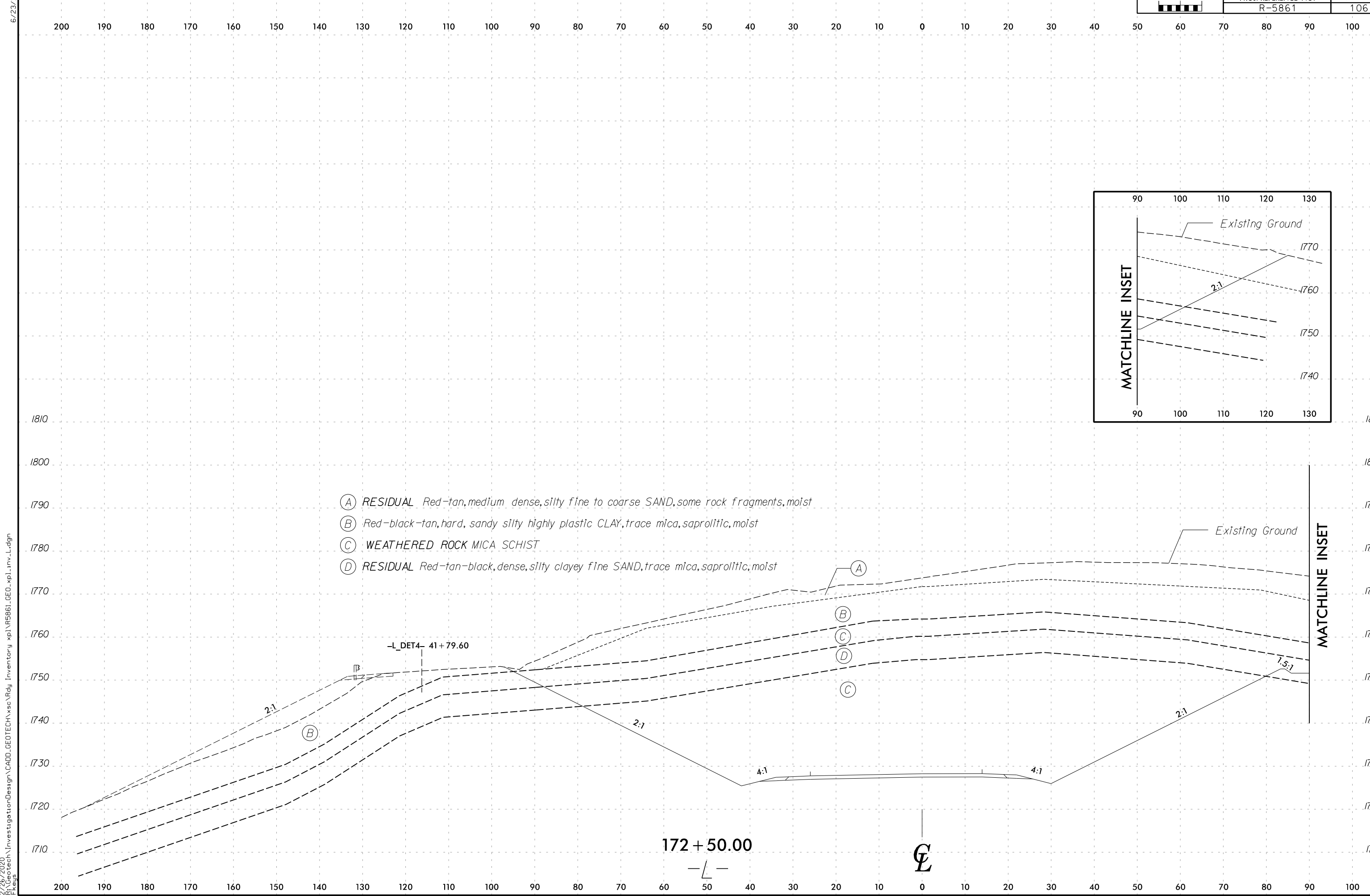
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
S-1159	172+00	0	2.0-8.0	A-7-5 (23)	64	31	12	32	31	25	97	89	70.8	ND	-

- (A) RESIDUAL Red-tan, medium dense, silty fine to coarse SAND, some rock fragments, moist
- (B) Red-black-tan, hard, sandy silty highly plastic CLAY, trace mica, saprolitic, moist
- (C) WEATHERED ROCK MICA SCHIST
- (D) RESIDUAL Red-tan-black, dense, silty clayey fine SAND, trace mica, saprolitic, moist

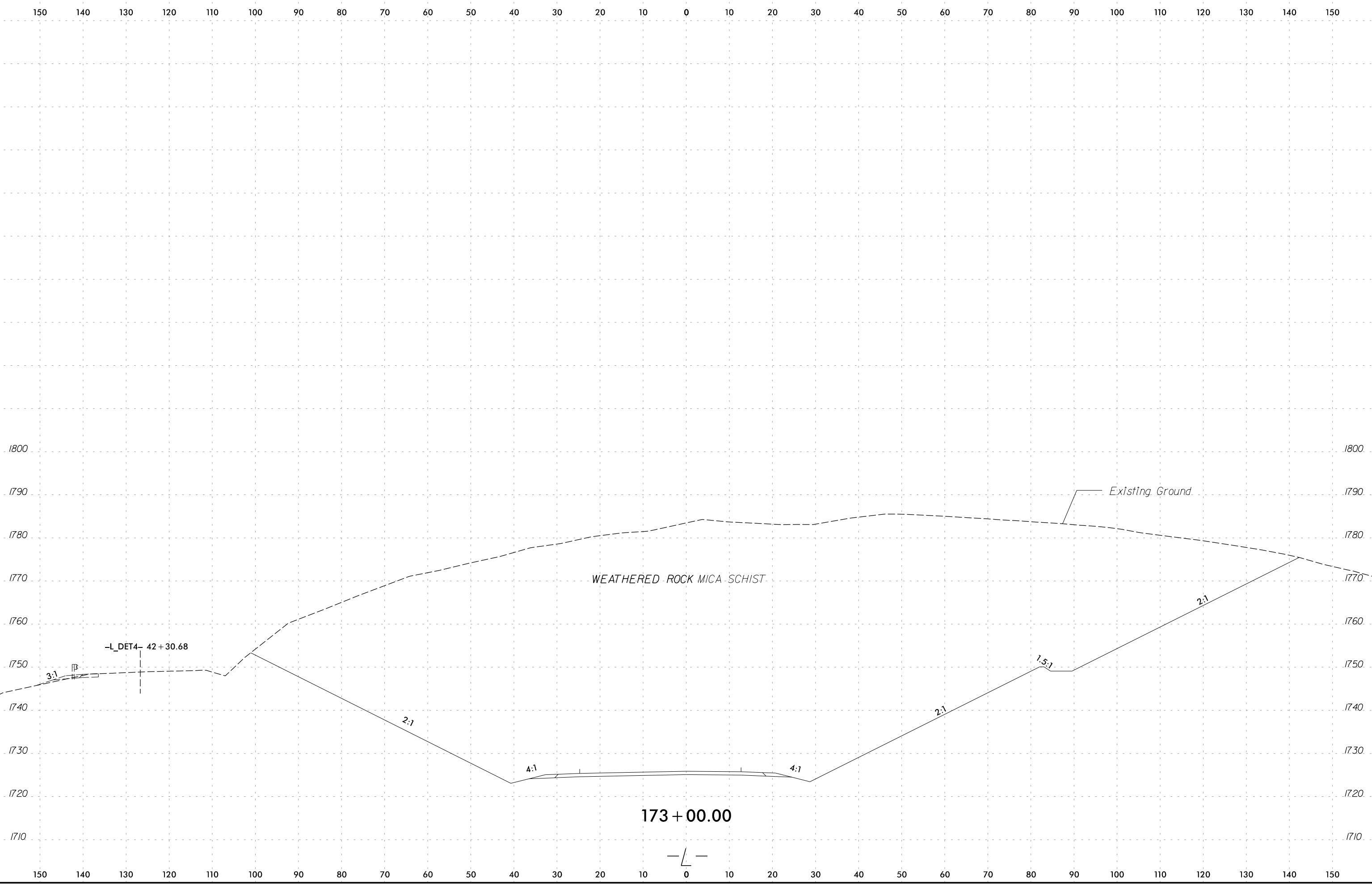


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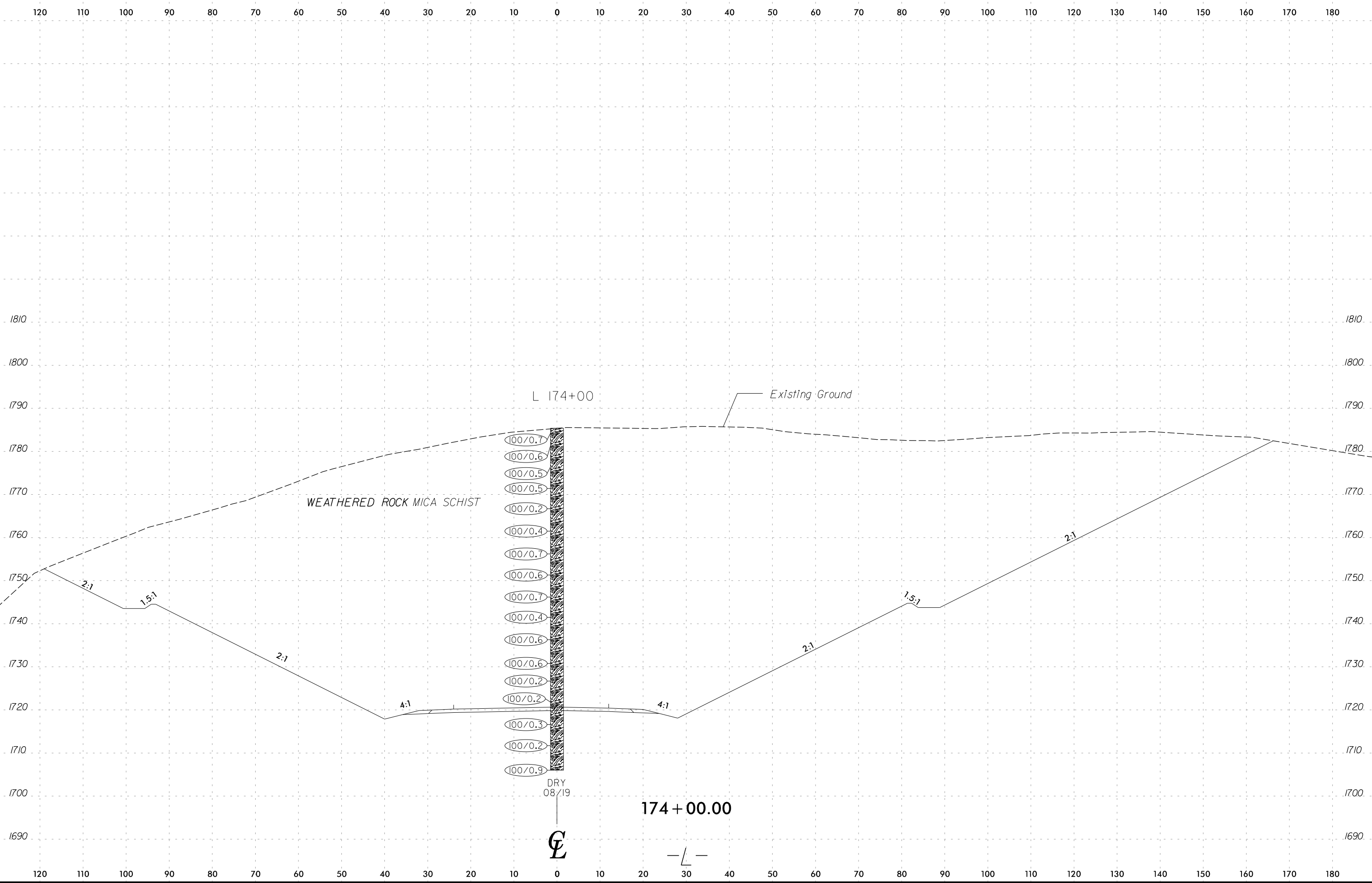


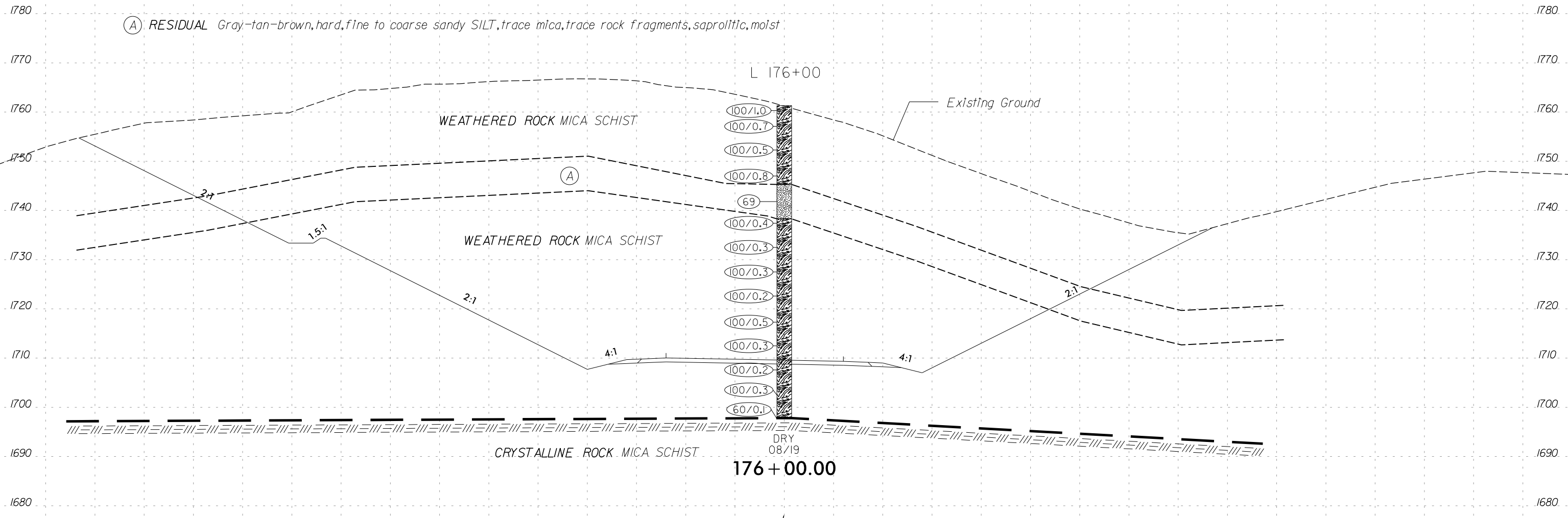
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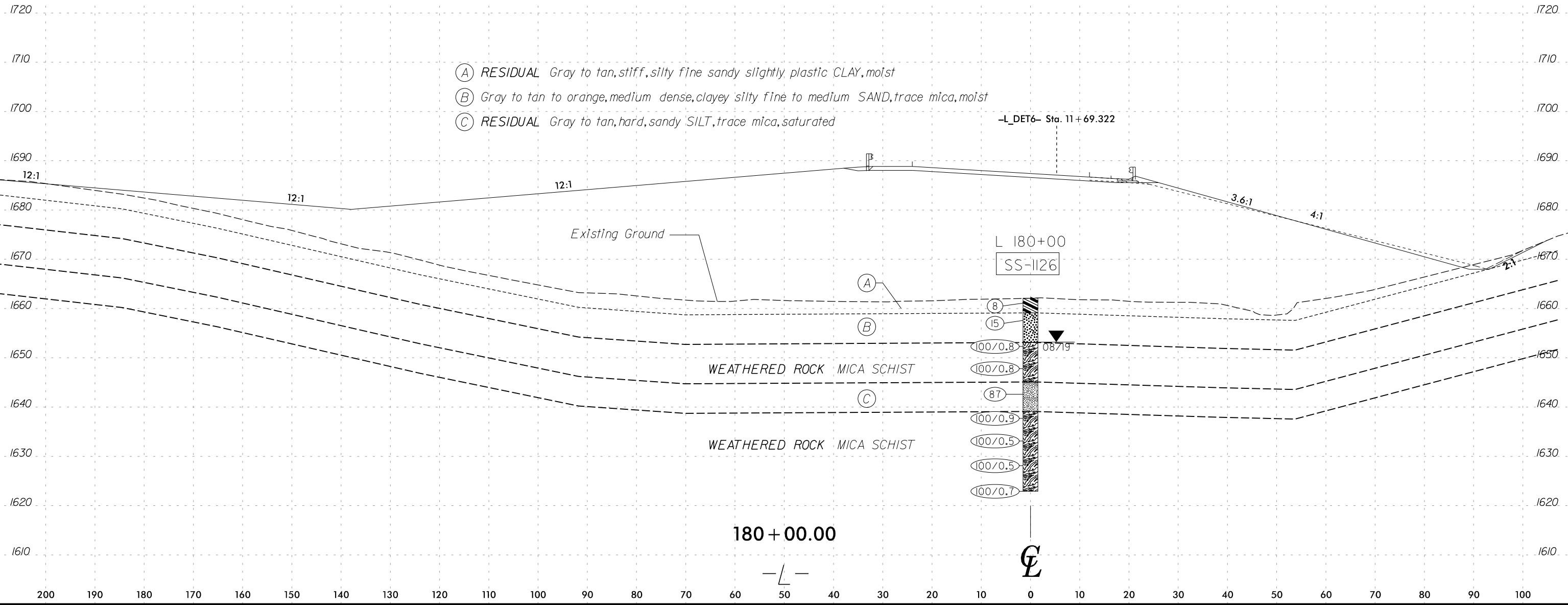


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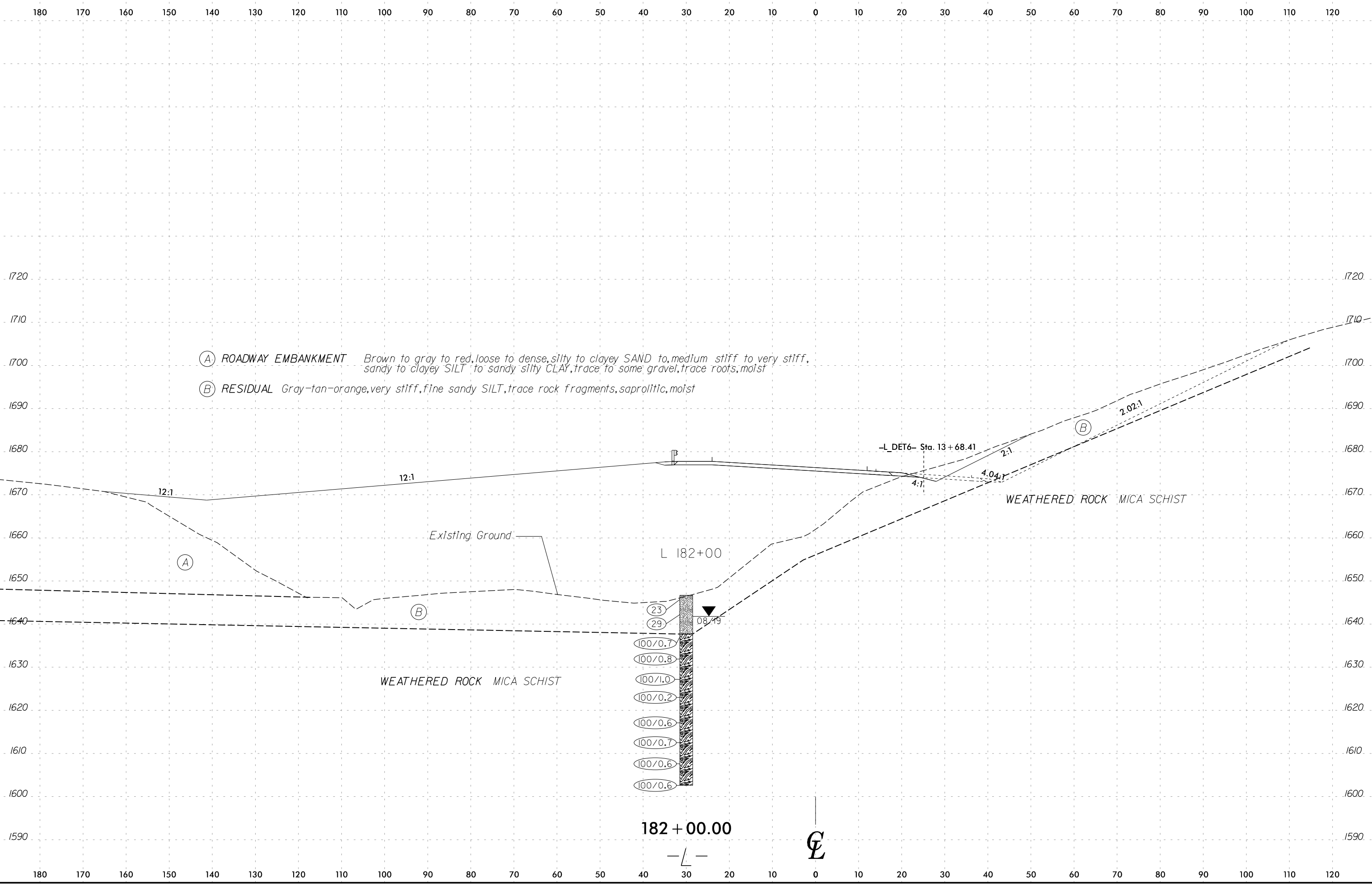
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1126	180+00	0	0.0-1.5	A-6 (8)	38	11	6	27	33	34	96	92	73.9	23	-

- (A) RESIDUAL Gray to tan, stiff, silty fine sandy slightly plastic CLAY, moist
- (B) Gray to tan to orange, medium dense, clayey silty fine to medium SAND, trace mica, moist
- (C) RESIDUAL Gray to tan, hard, sandy SILT, trace mica, saturated



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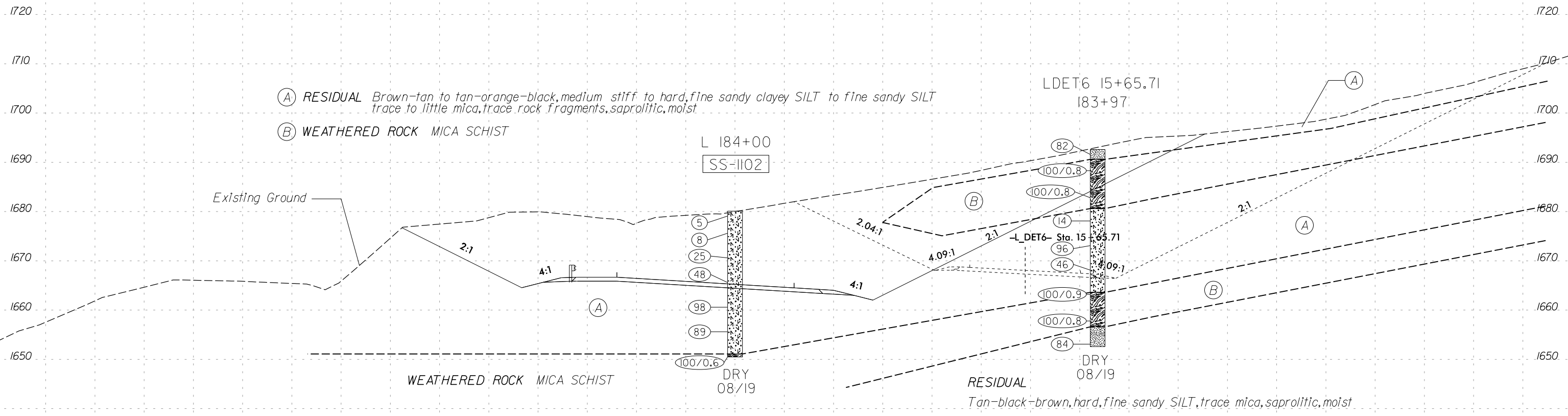


- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Gray-tan-orange, very stiff, fine sandy SILT, trace rock fragments, saprolitic, moist*

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140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160

SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1102	184+00	0	0.0-1.5	A-5 (5)	41	7	15	26	31	28	93	82	64.8	21.4	-



(A) RESIDUAL Brown-tan to tan-orange-black, medium stiff to hard, fine sandy clayey SILT to fine sandy SILT trace to little mica, trace rock fragments, saprolitic, moist
 (B) WEATHERED ROCK MICA SCHIST

LDET6 15+65.71
183+97

L 184+00
SS-1102

Existing Ground

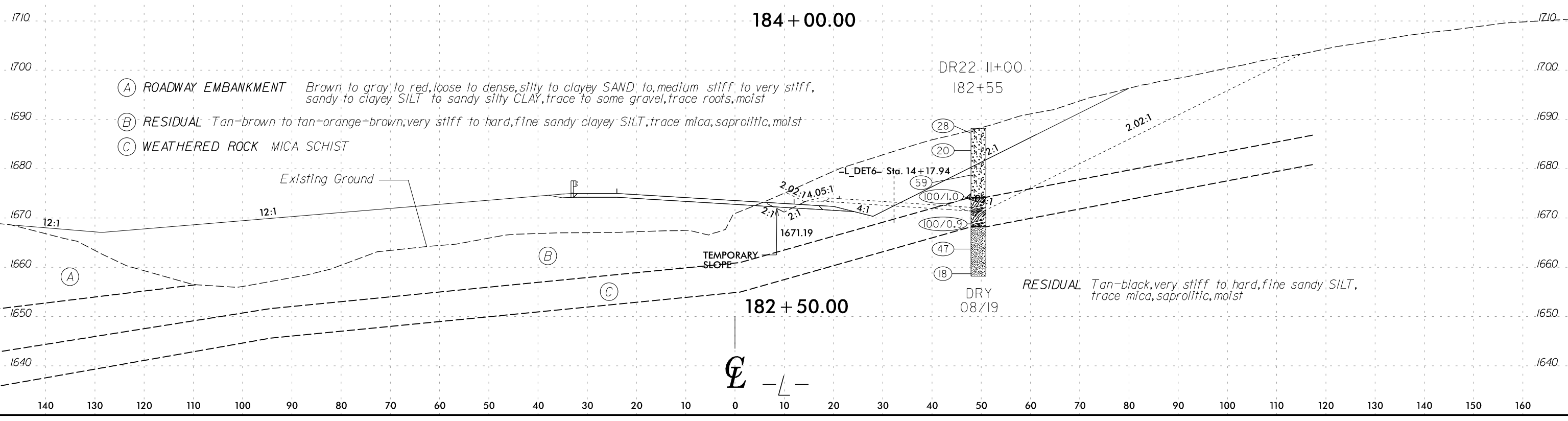
WEATHERED ROCK MICA SCHIST

DRY 08/19

RESIDUAL

Tan-black-brown, hard, fine sandy SILT, trace mica, saprolitic, moist

DRY 08/19



(A) ROADWAY EMBANKMENT Brown to gray to red, loose to dense, silty to clayey SAND to medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist
 (B) RESIDUAL Tan-brown to tan-orange-brown, very stiff to hard, fine sandy clayey SILT, trace mica, saprolitic, moist
 (C) WEATHERED ROCK MICA SCHIST

DR22 11+00
182+55

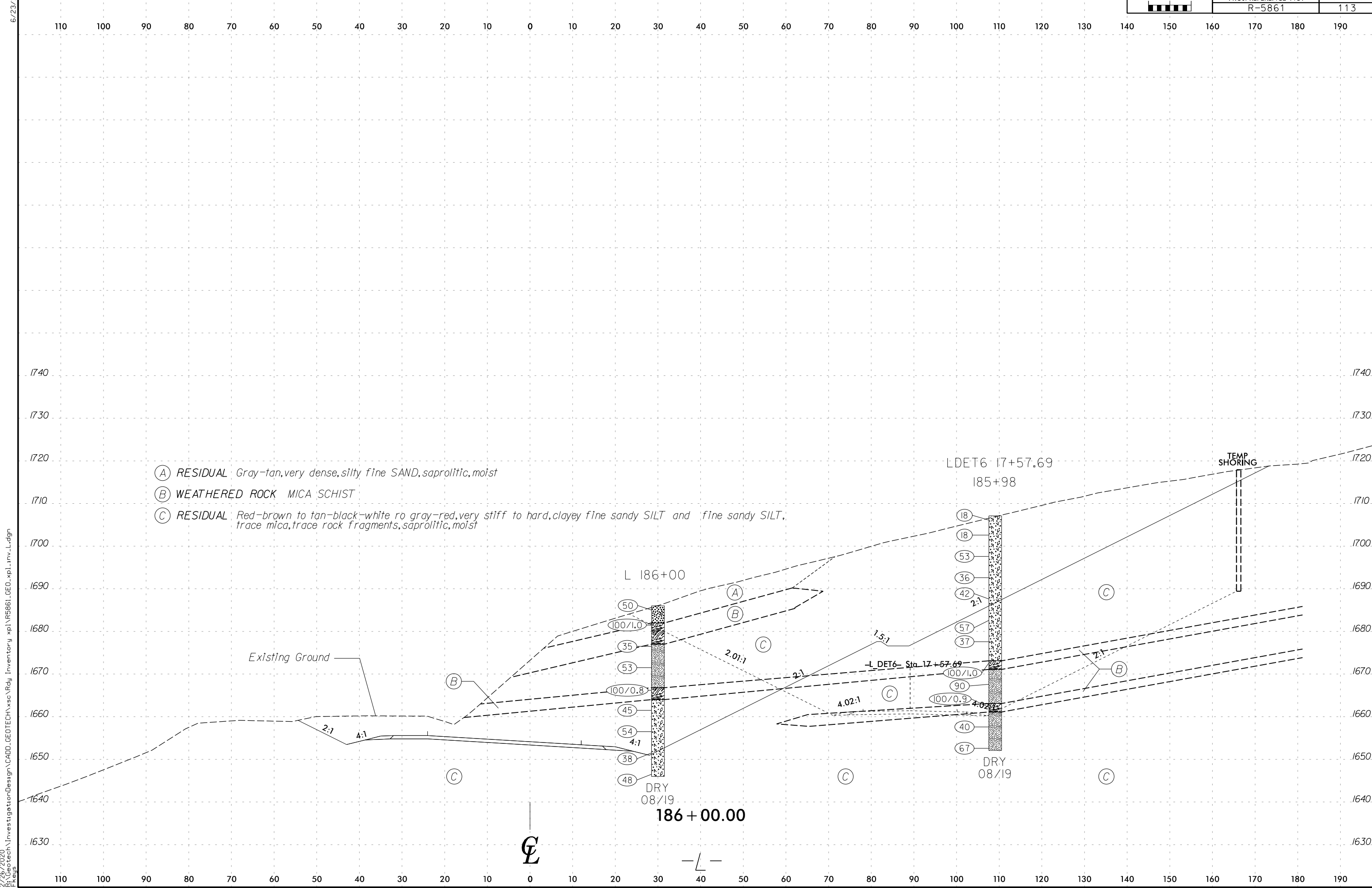
Existing Ground

TEMPORARY SLOPE

DRY 08/19

RESIDUAL Tan-black, very stiff to hard, fine sandy SILT, trace mica, saprolitic, moist

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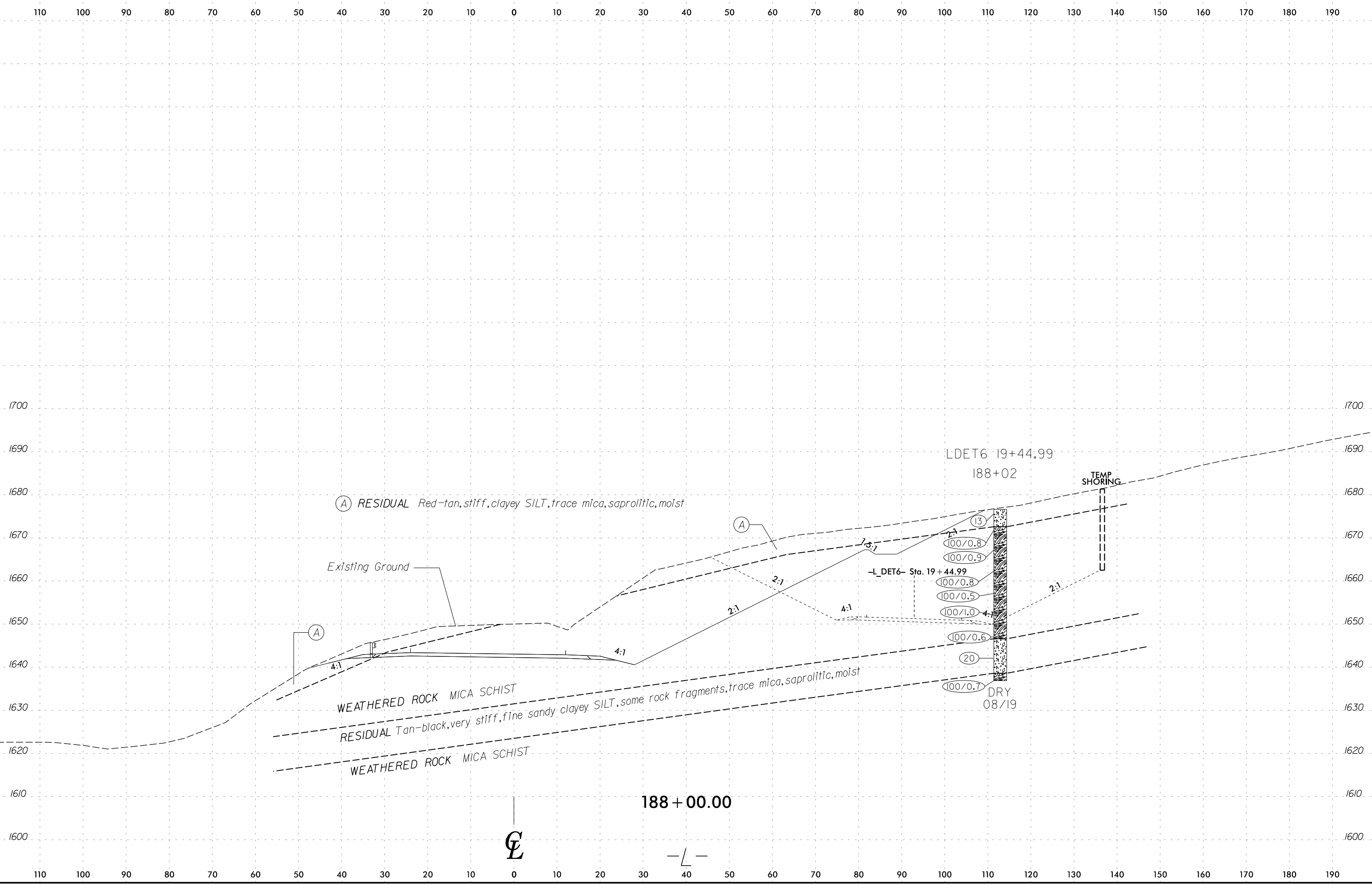


- (A) RESIDUAL Gray-tan, very dense, silty fine SAND, saprolitic, moist
- (B) WEATHERED ROCK MICA SCHIST
- (C) RESIDUAL Red-brown to tan-black-white to gray-red, very stiff to hard, clayey fine sandy SILT and fine sandy SILT, trace mica, trace rock fragments, saprolitic, moist

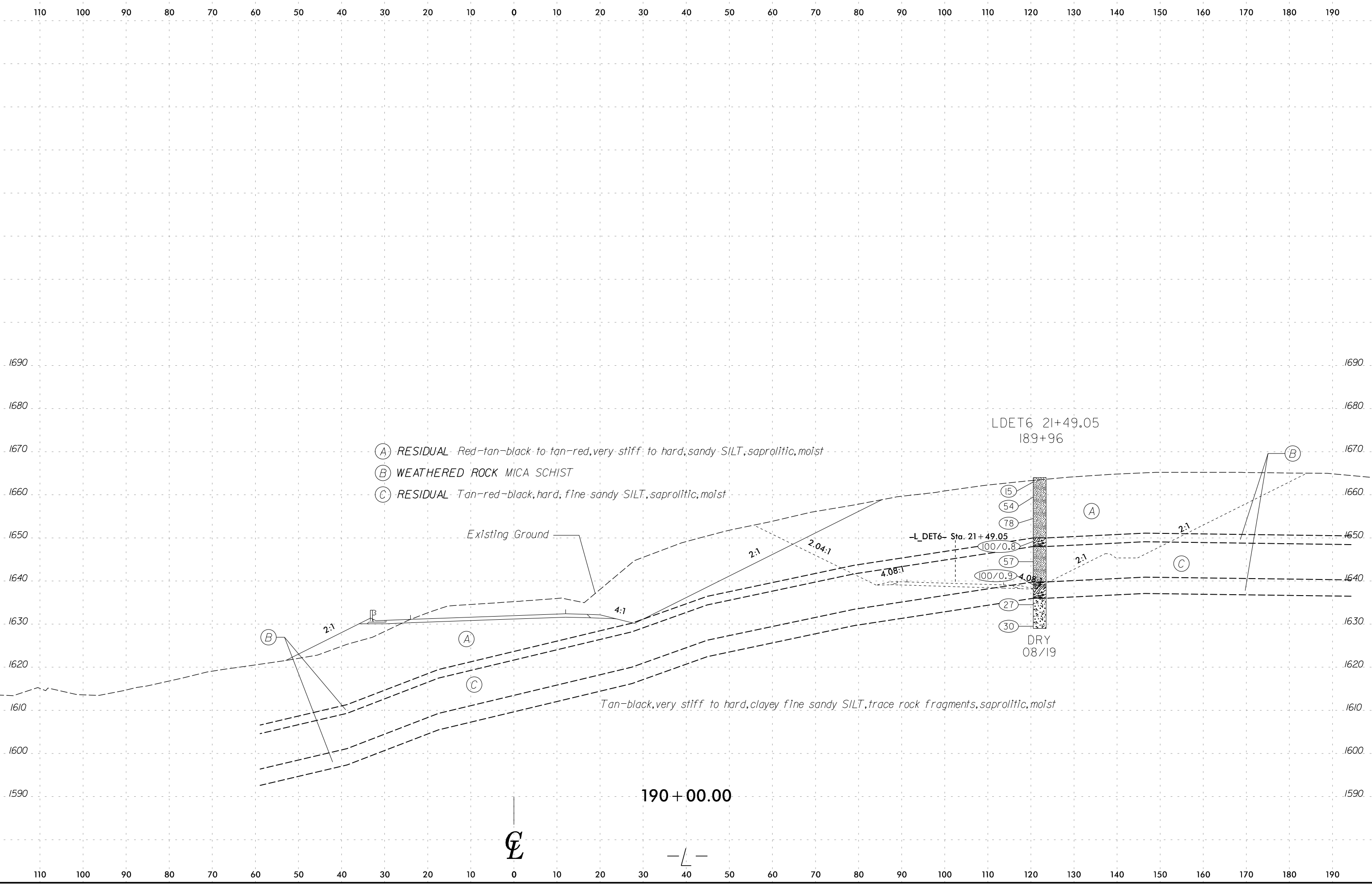
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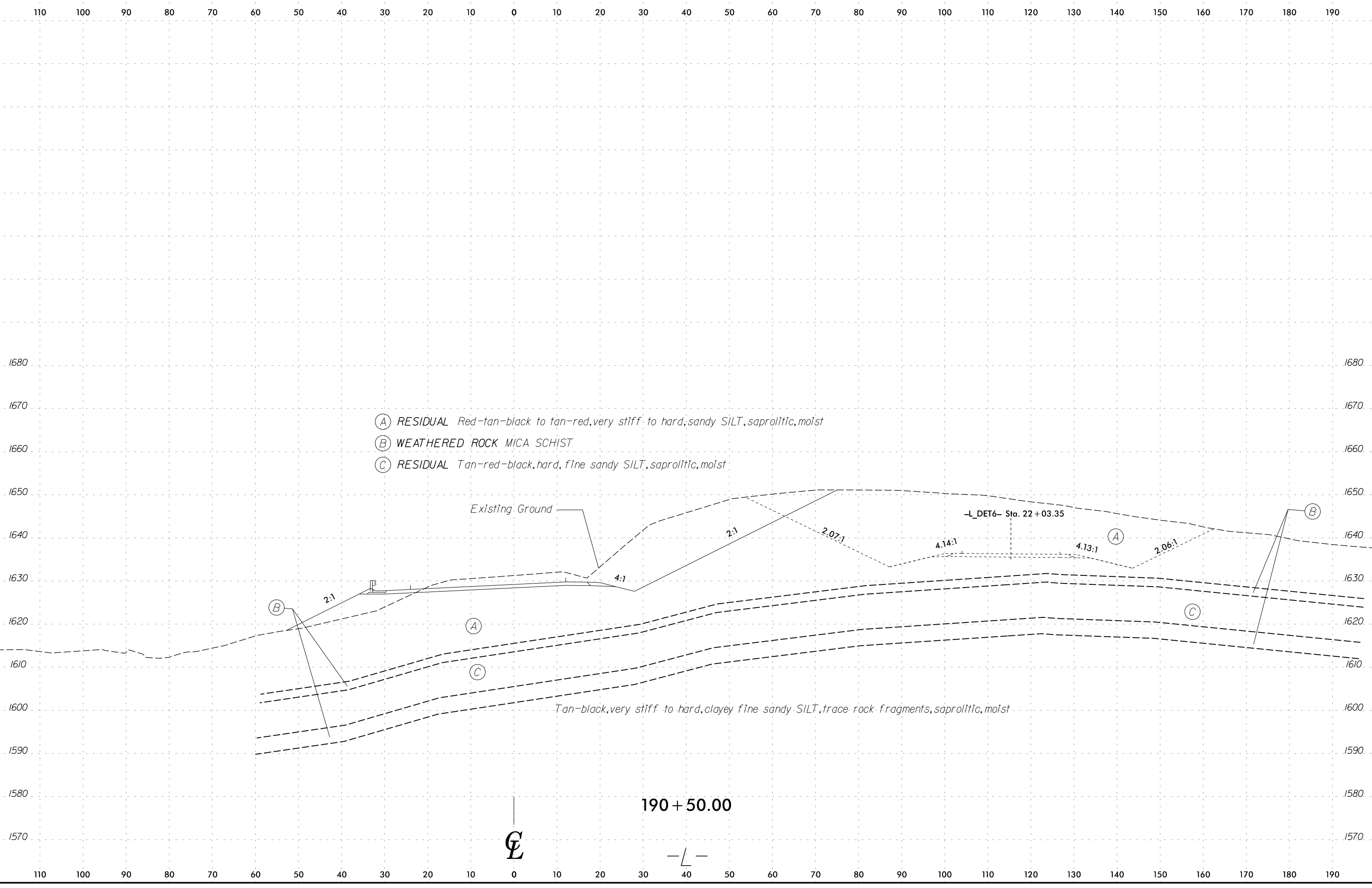
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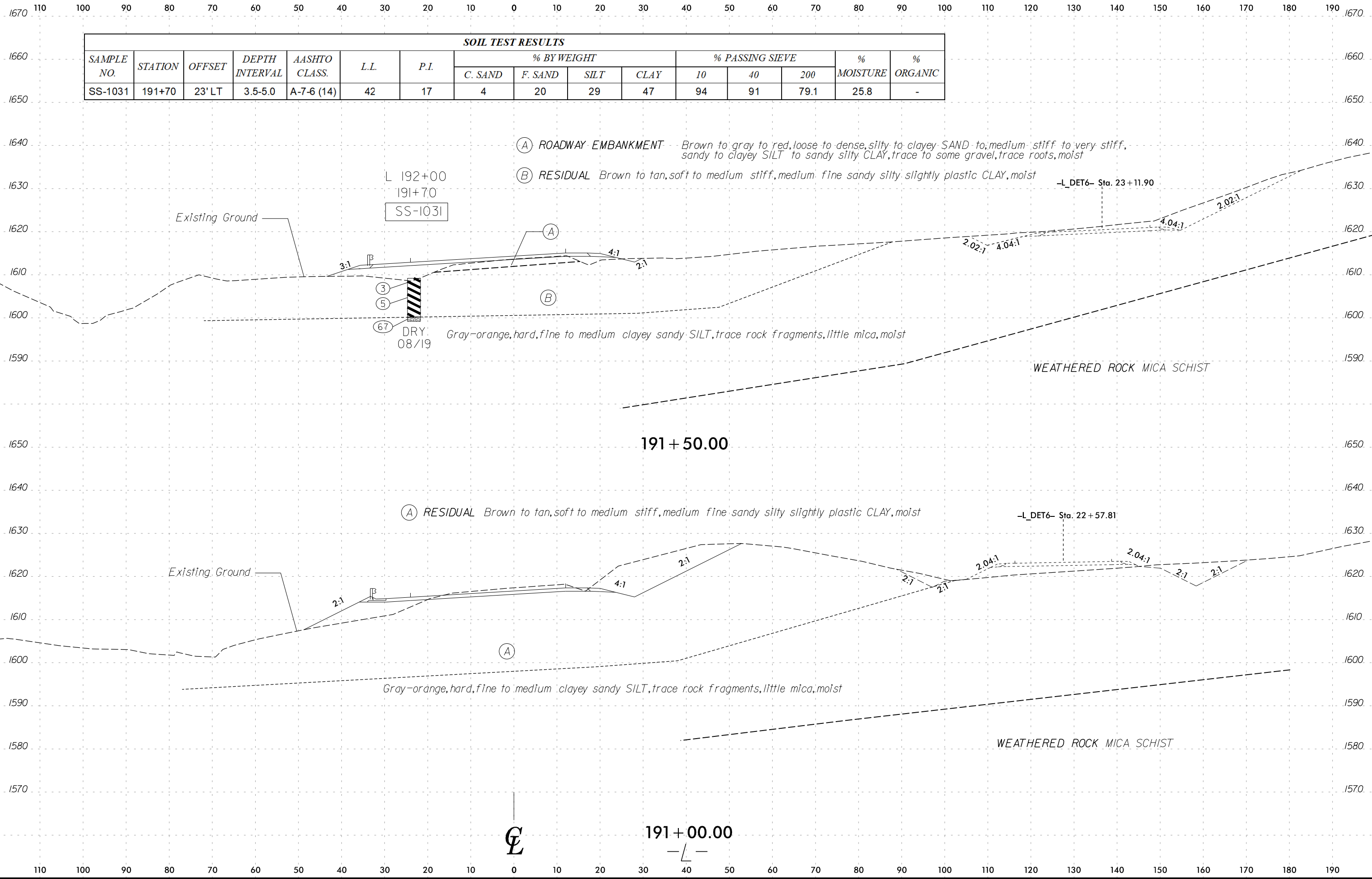


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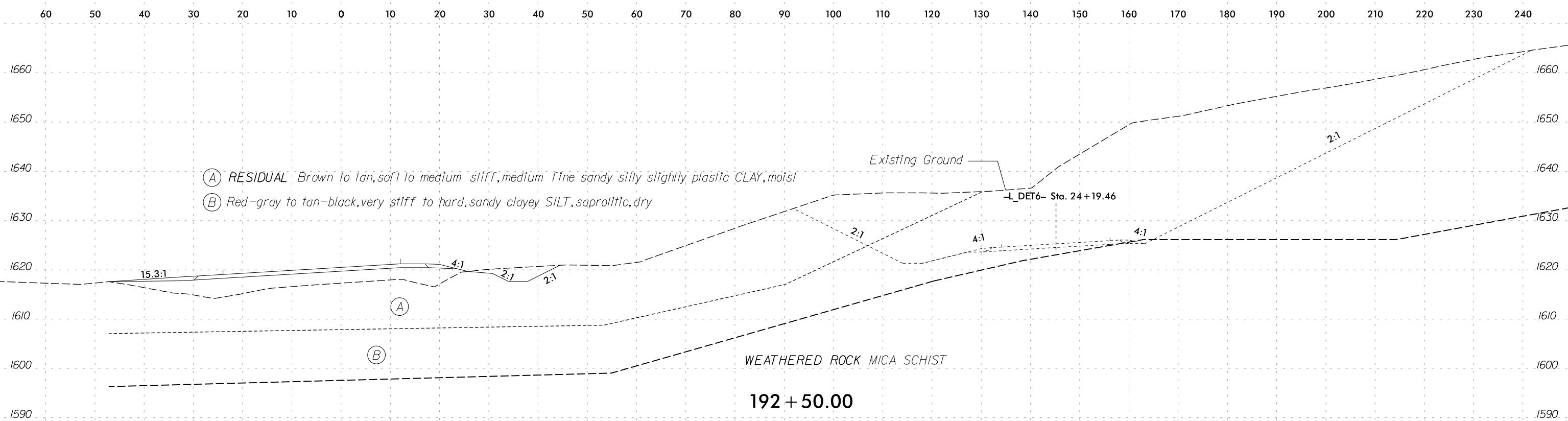


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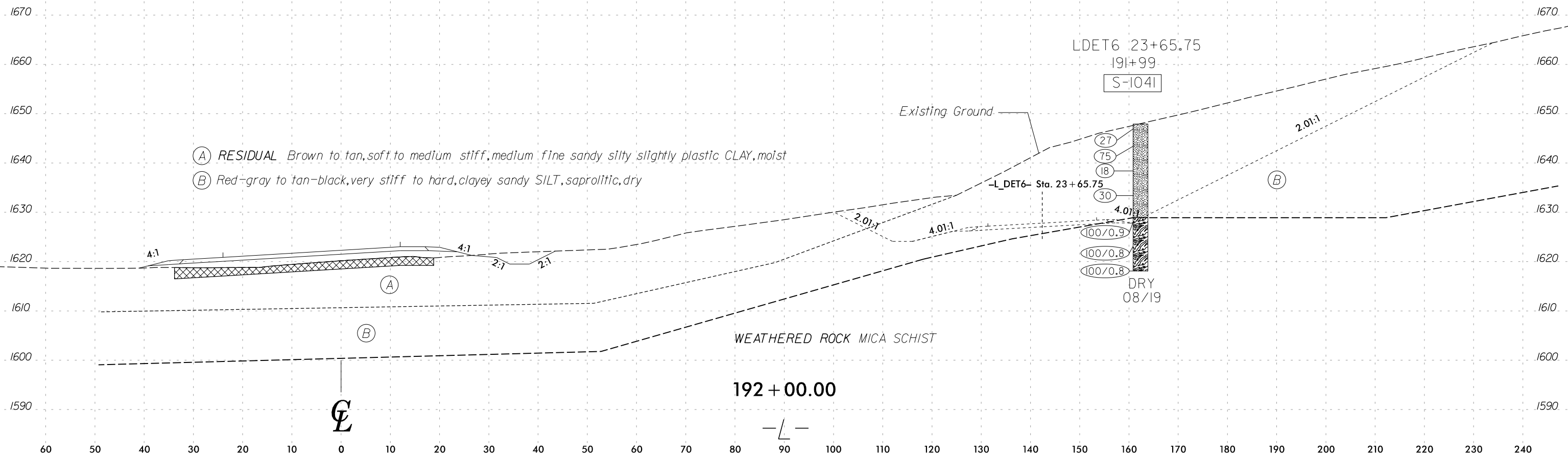
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1031	191+70	23' LT	3.5-5.0	A-7-6 (14)	42	17	4	20	29	47	94	91	79.1	25.8	-



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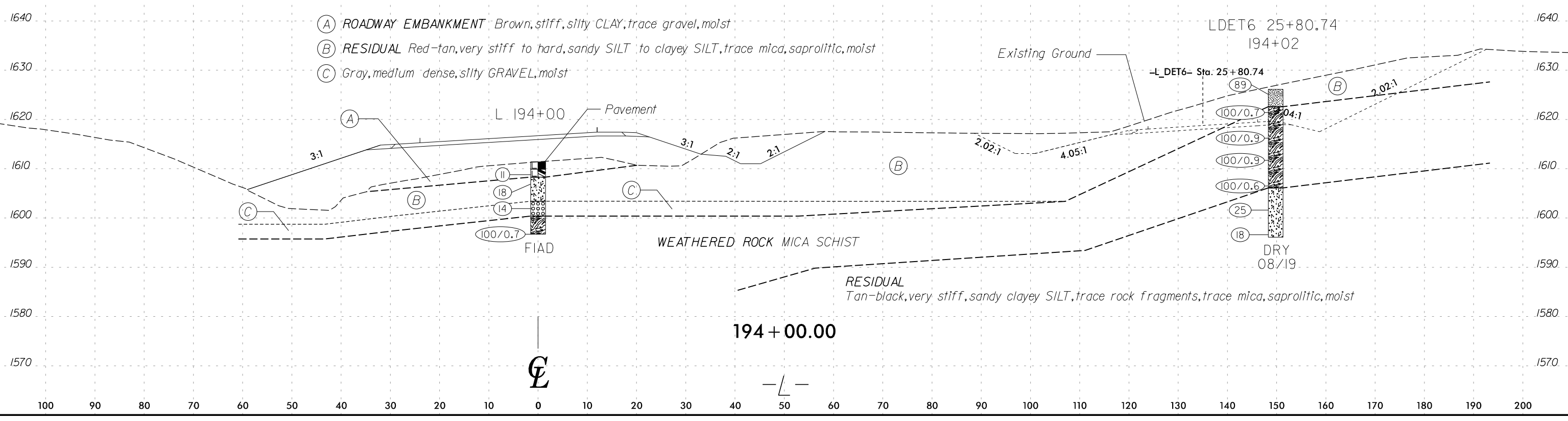
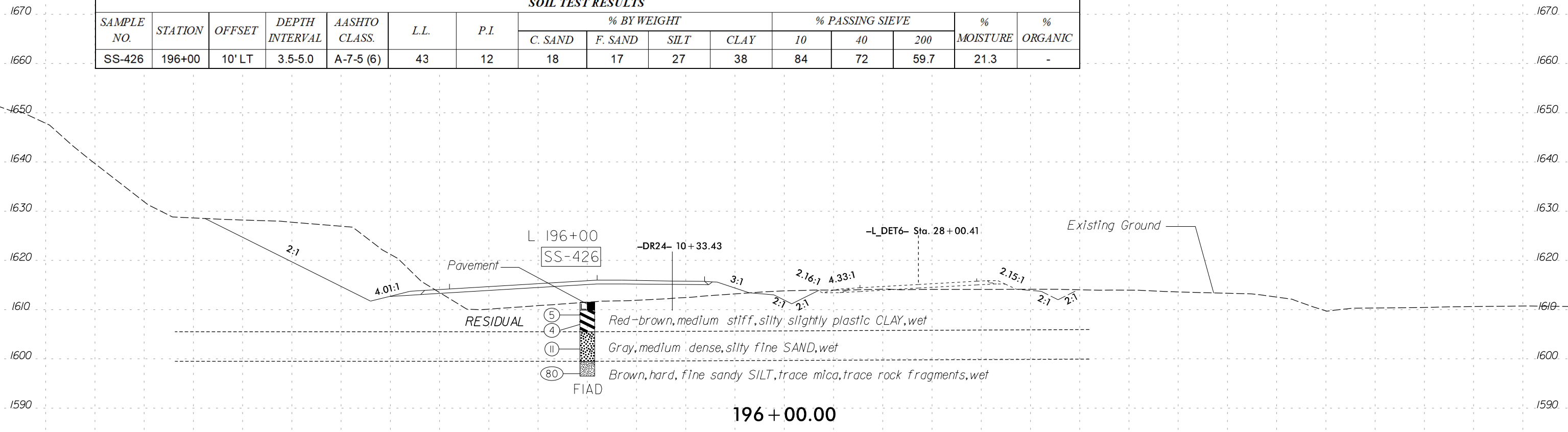
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
S-1041	191+99	162' RT	0.0-8.5	A-4 (8)	39	10	3	31	36	30	99	97	78.3	ND	-



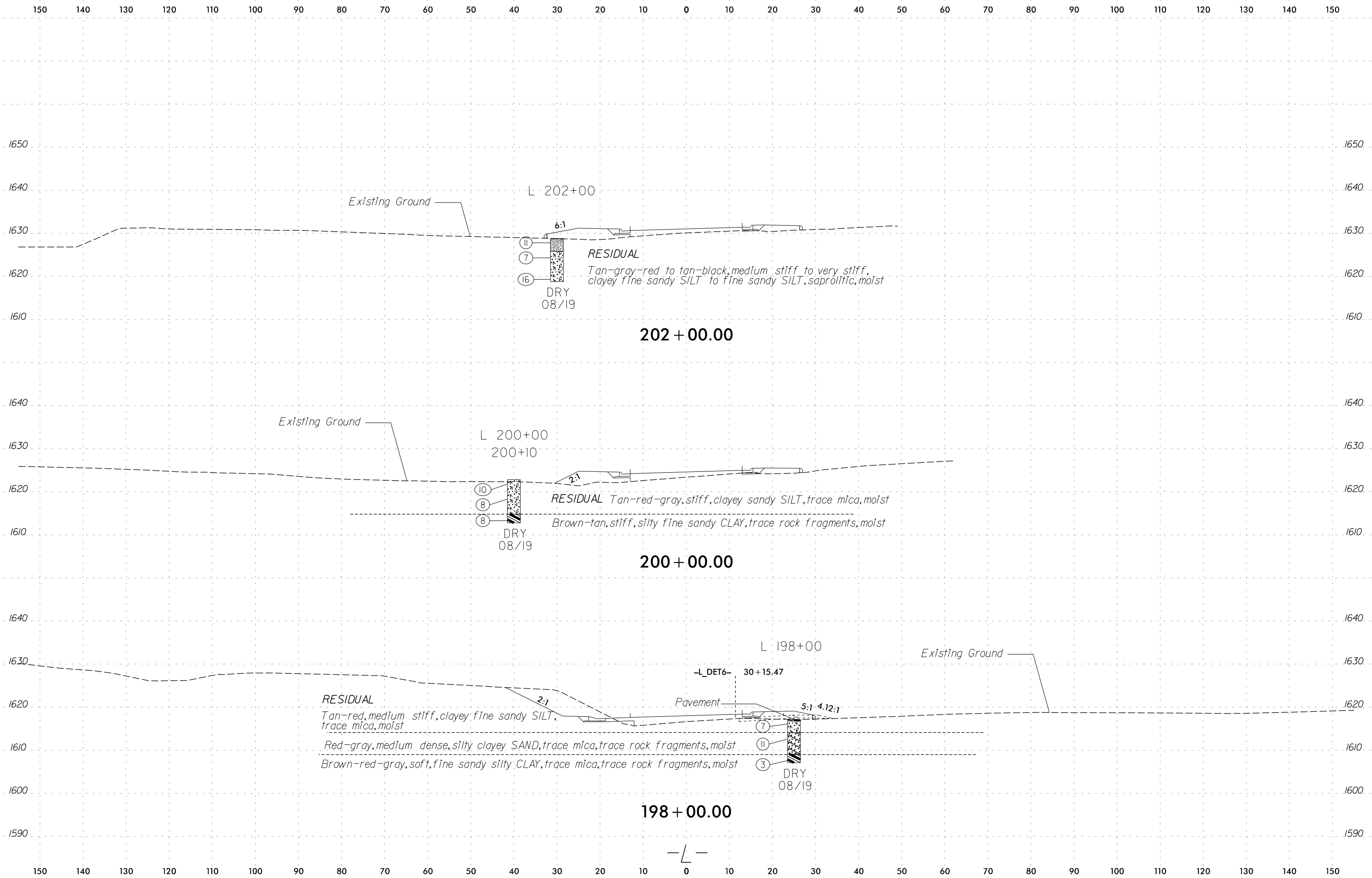
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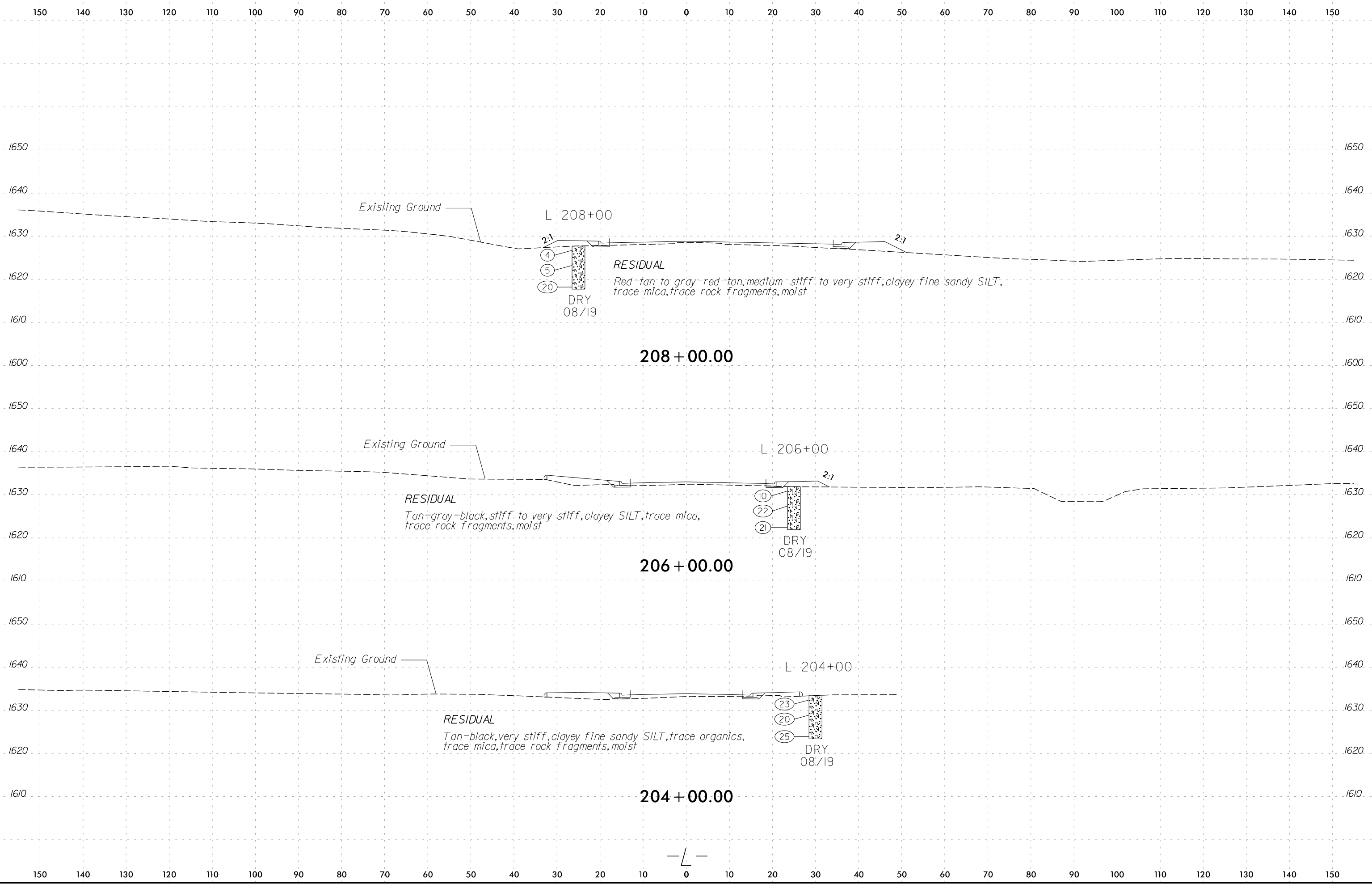
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SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-426	196+00	10' LT	3.5-5.0	A-7-5 (6)	43	12	18	17	27	38	84	72	59.7	21.3	-



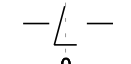
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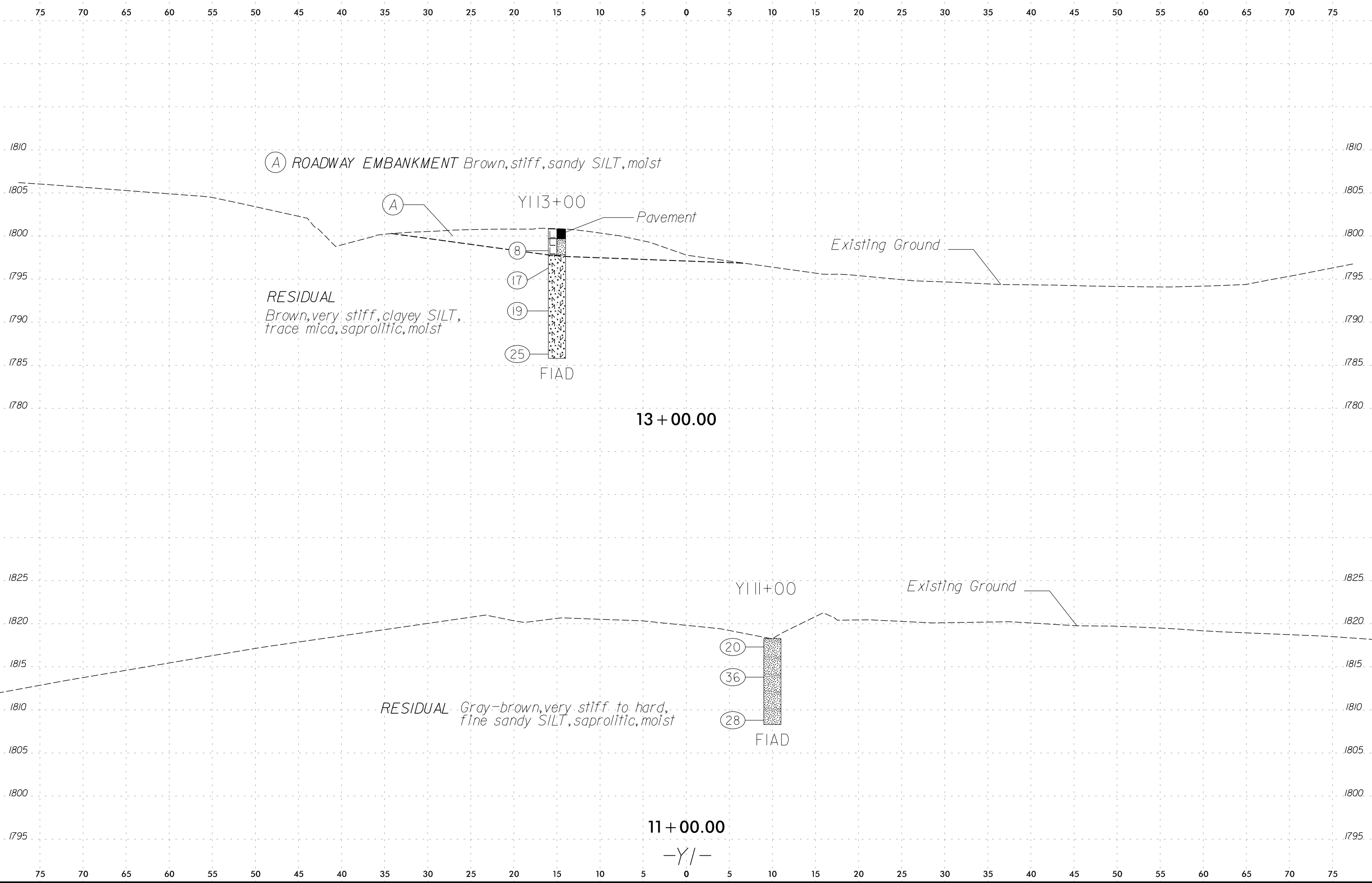


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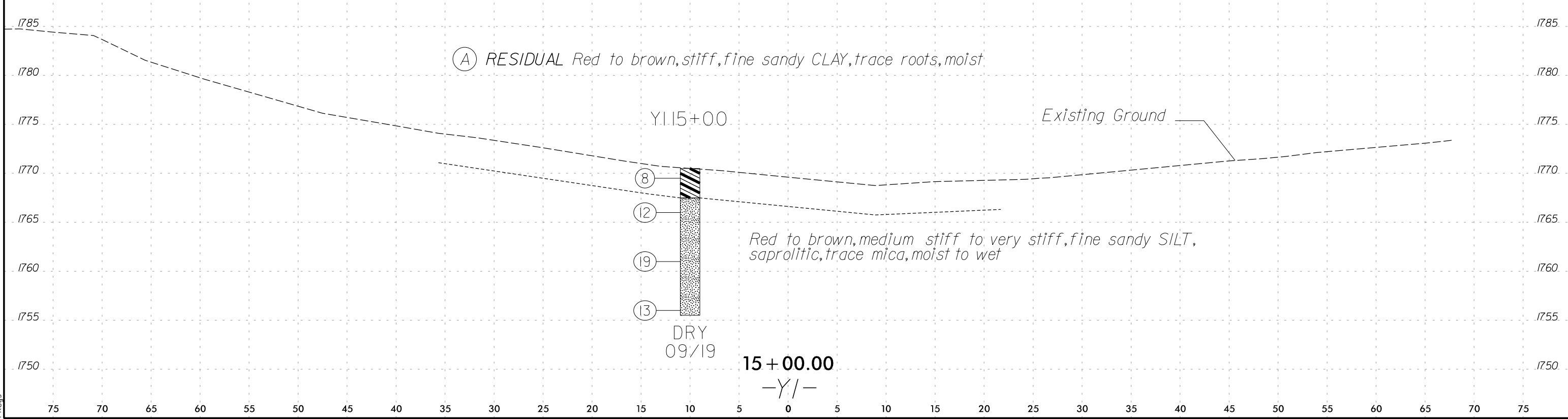
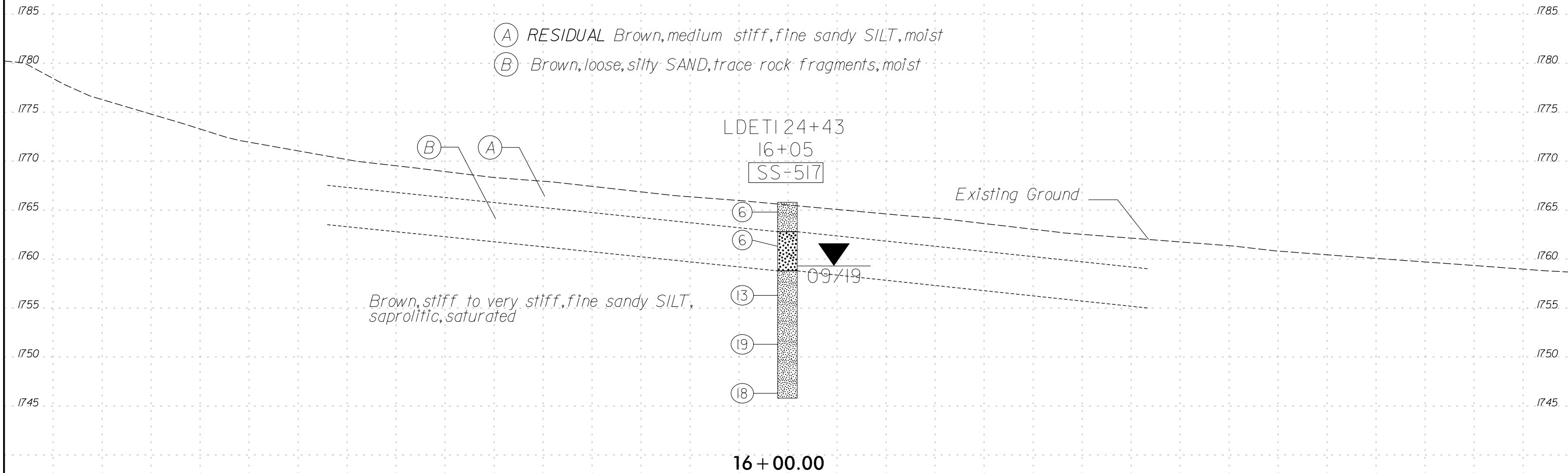
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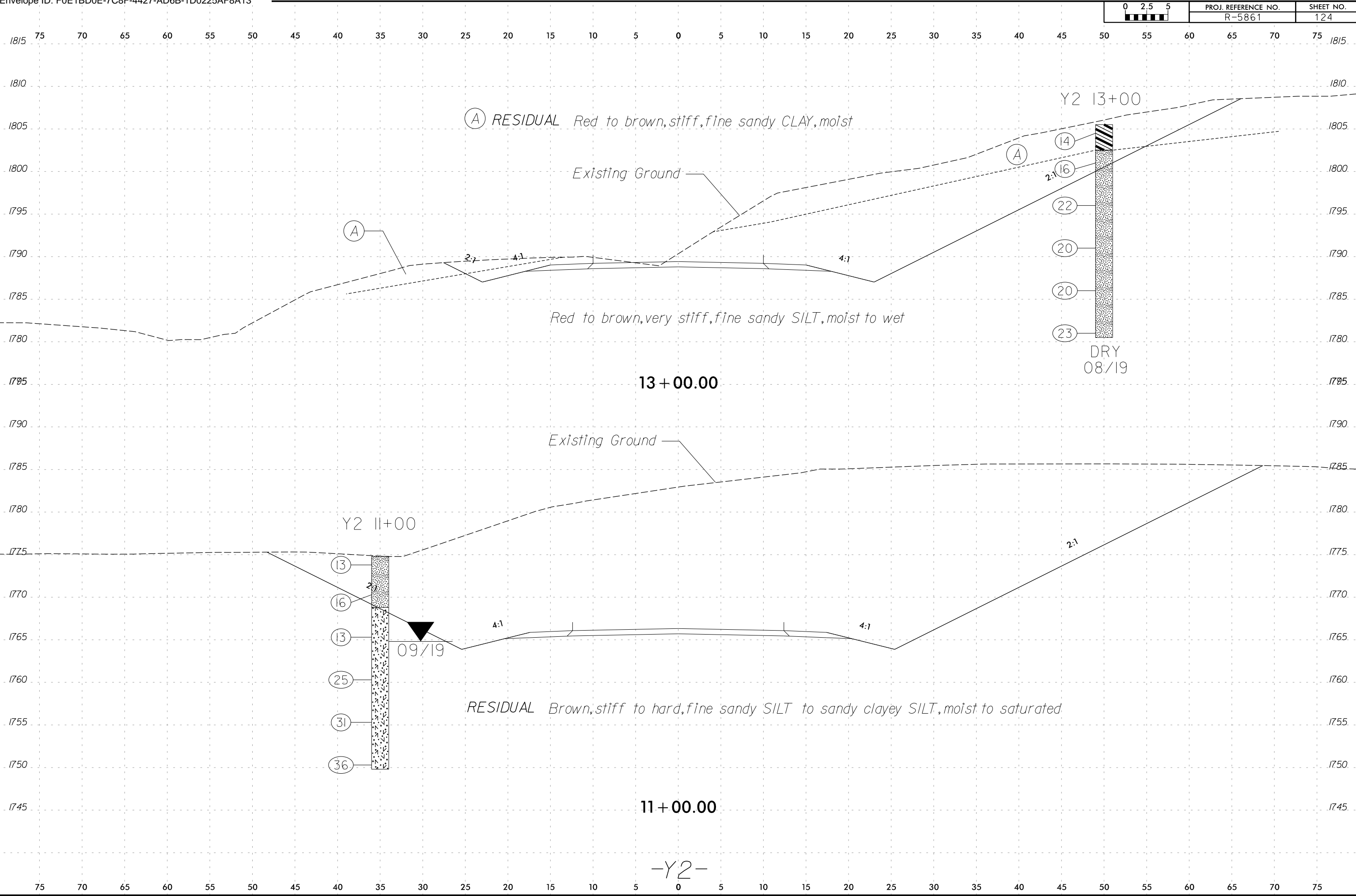
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-517	16+05	0	3.5-5.0	A-2-4 (0)	30	5	21	46	11	22	63	56	29.3	15.8	-



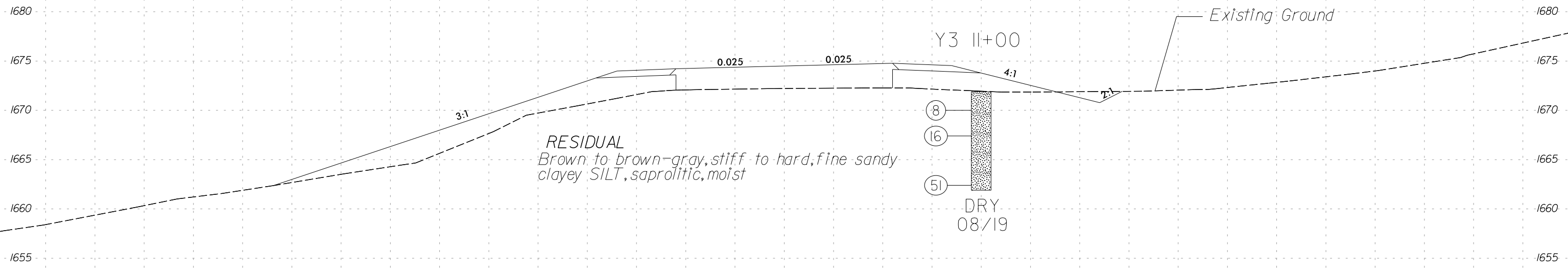
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Pkups



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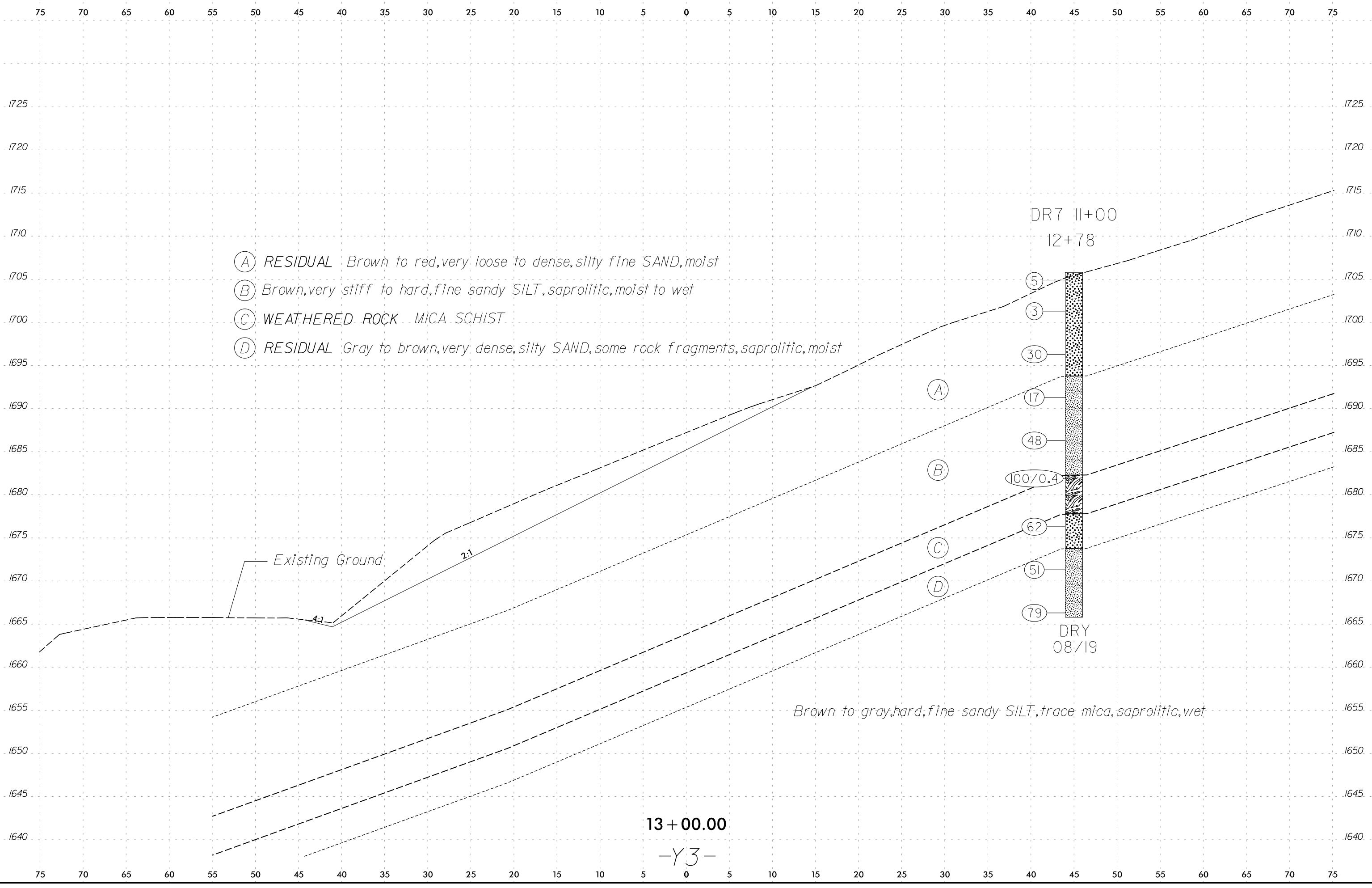


11 + 00.00

-Y3-

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- (A) RESIDUAL Brown to red, very loose to dense, silty fine SAND, moist
- (B) Brown, very stiff to hard, fine sandy SILT, saprolitic, moist to wet
- (C) WEATHERED ROCK MICA SCHIST
- (D) RESIDUAL Gray to brown, very dense, silty SAND, some rock fragments, saprolitic, moist

DR7 II+00
12+78

- (5)
- (3)
- (30)
- (17)
- (48)
- (100/0.4)
- (62)
- (51)
- (79)

DRY
08/19

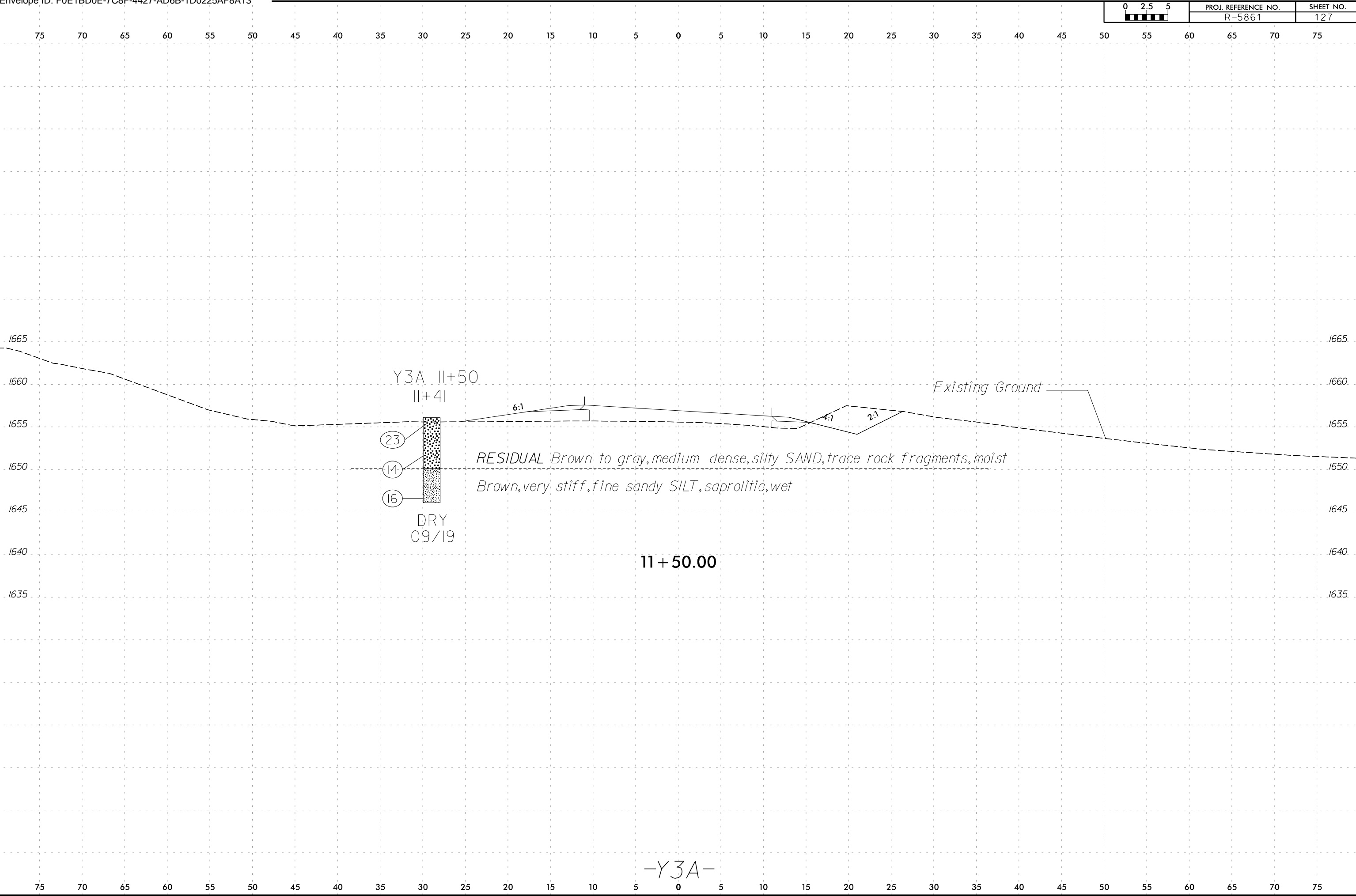
Brown to gray, hard, fine sandy SILT, trace mica, saprolitic, wet

13 + 00.00

-Y3-

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P.keja



Y3A 11+50
11+41

23
14
16

DRY
09/19

RESIDUAL Brown to gray, medium dense, silty SAND, trace rock fragments, moist
Brown, very stiff, fine sandy SILT, saprolitic, wet

Existing Ground

6:1

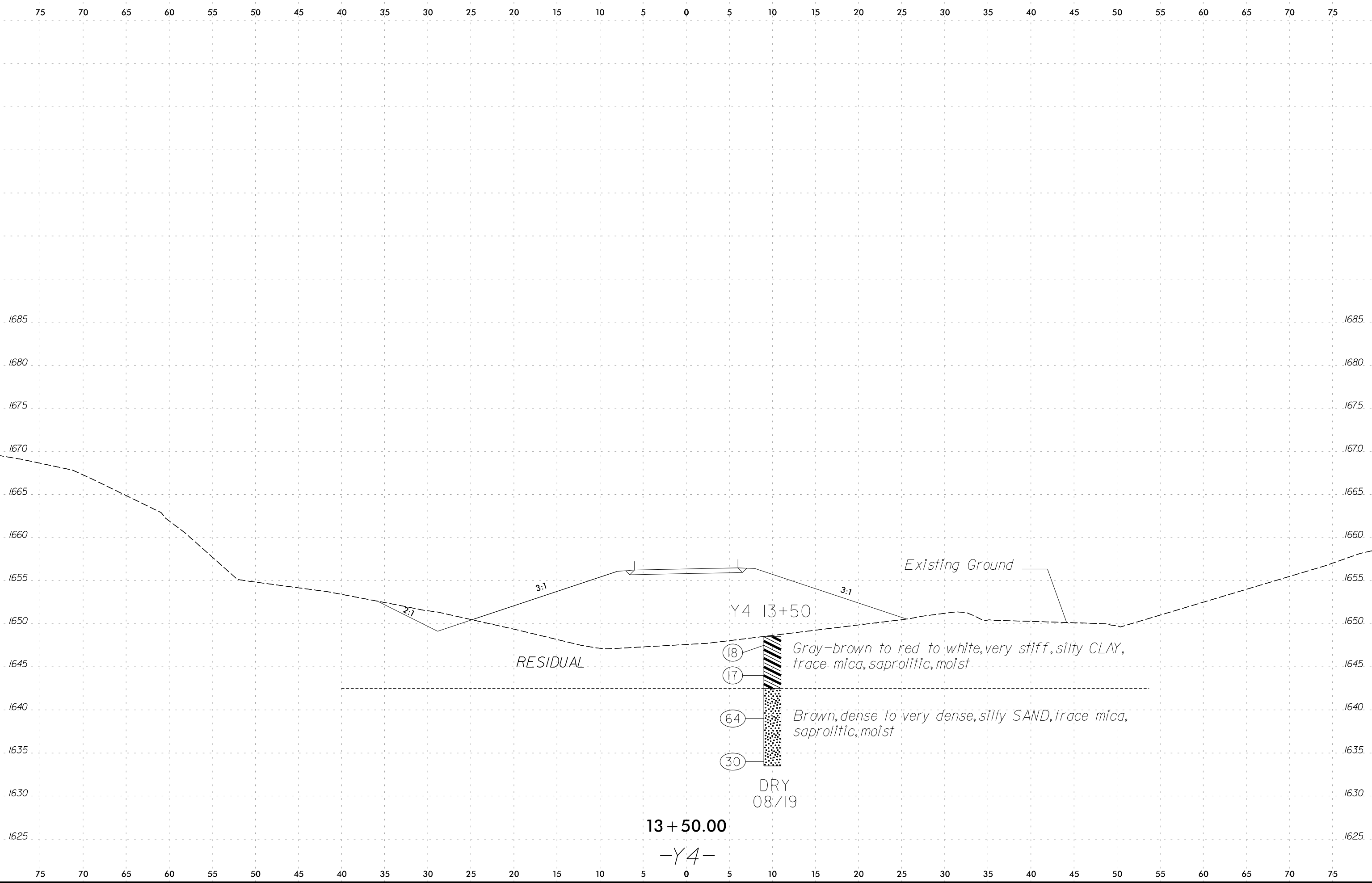
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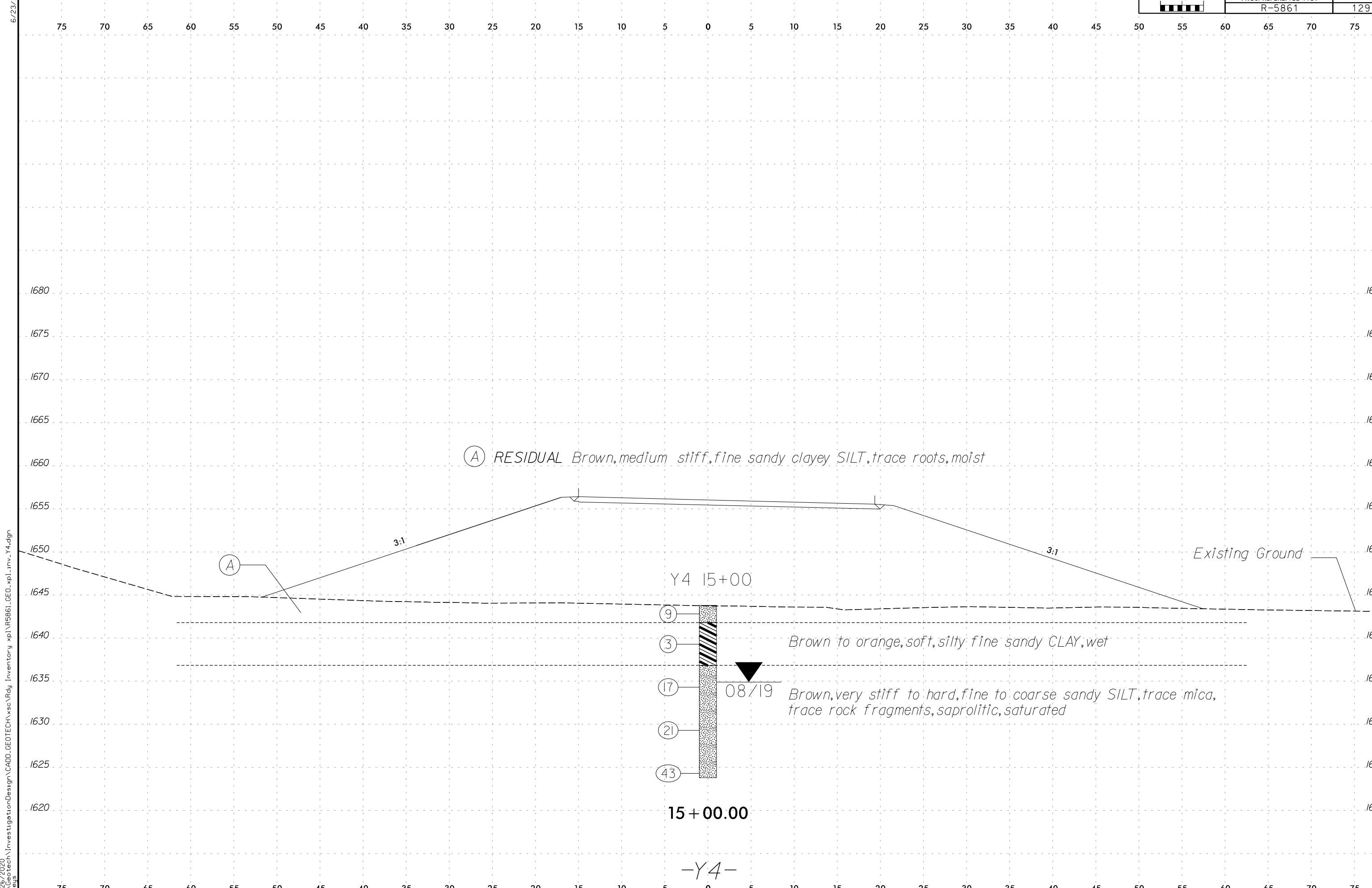
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11 + 50.00

-Y3A-

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(A) RESIDUAL Brown, medium stiff, fine sandy clayey SILT, trace roots, moist

Existing Ground

Y4 15+00

- (9)
- (3)
- (17)
- (21)
- (43)

Brown to orange, soft, silty fine sandy CLAY, wet

08/19 Brown, very stiff to hard, fine to coarse sandy SILT, trace mica, trace rock fragments, saprolitic, saturated

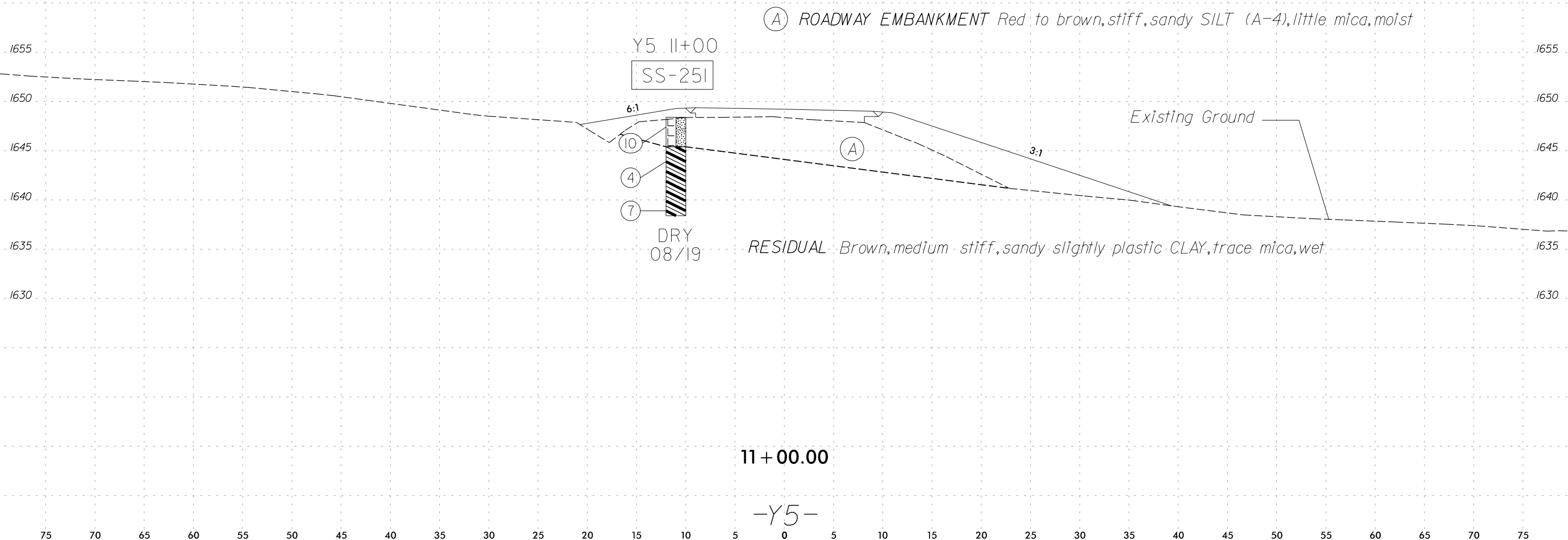
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-Y4-

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Pkups

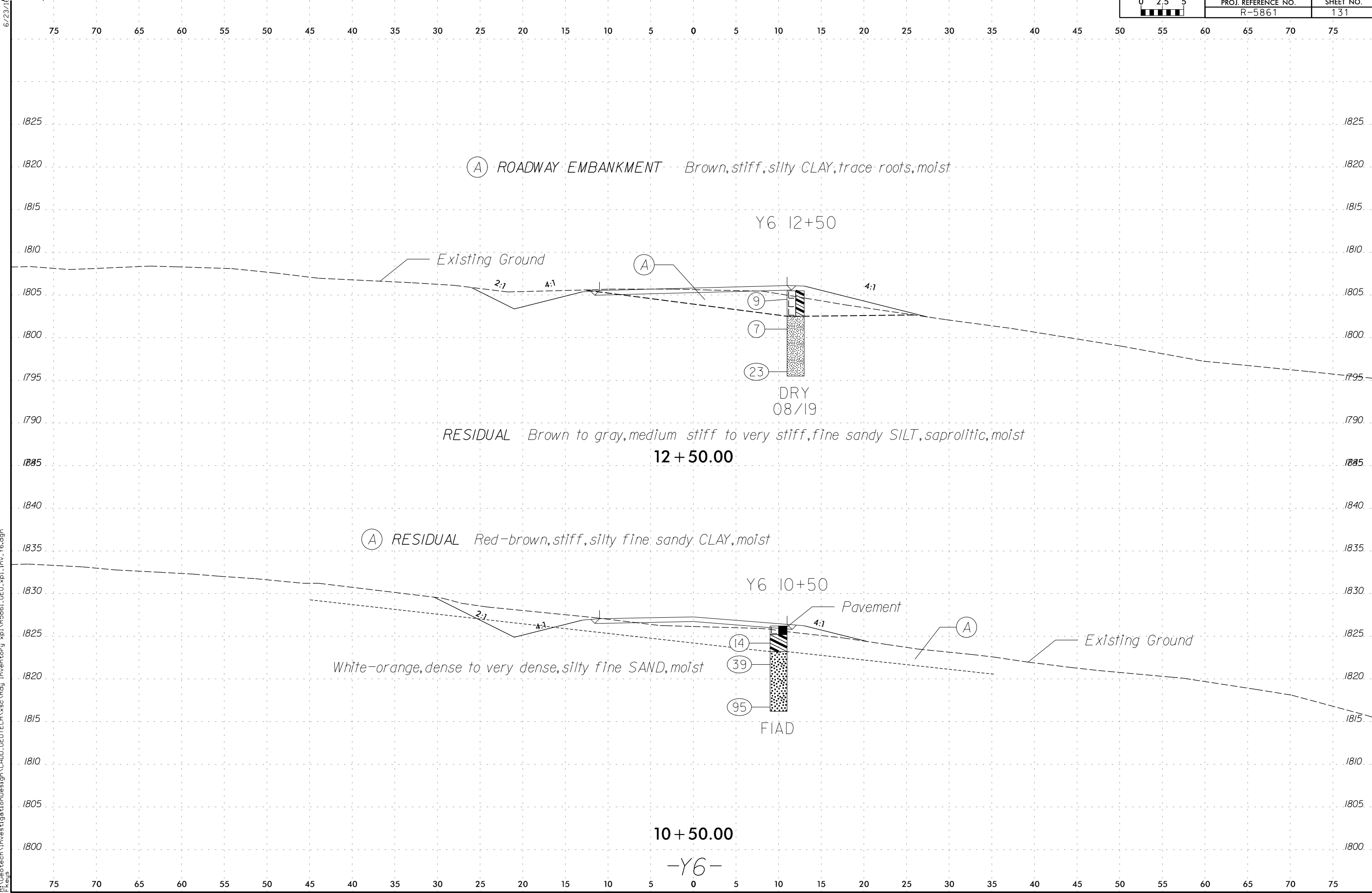
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-251	11+00	11' LT	3.5-5.0	A-6 (4)	37	12	18	33	16	33	96	85	52.6	23.3	-

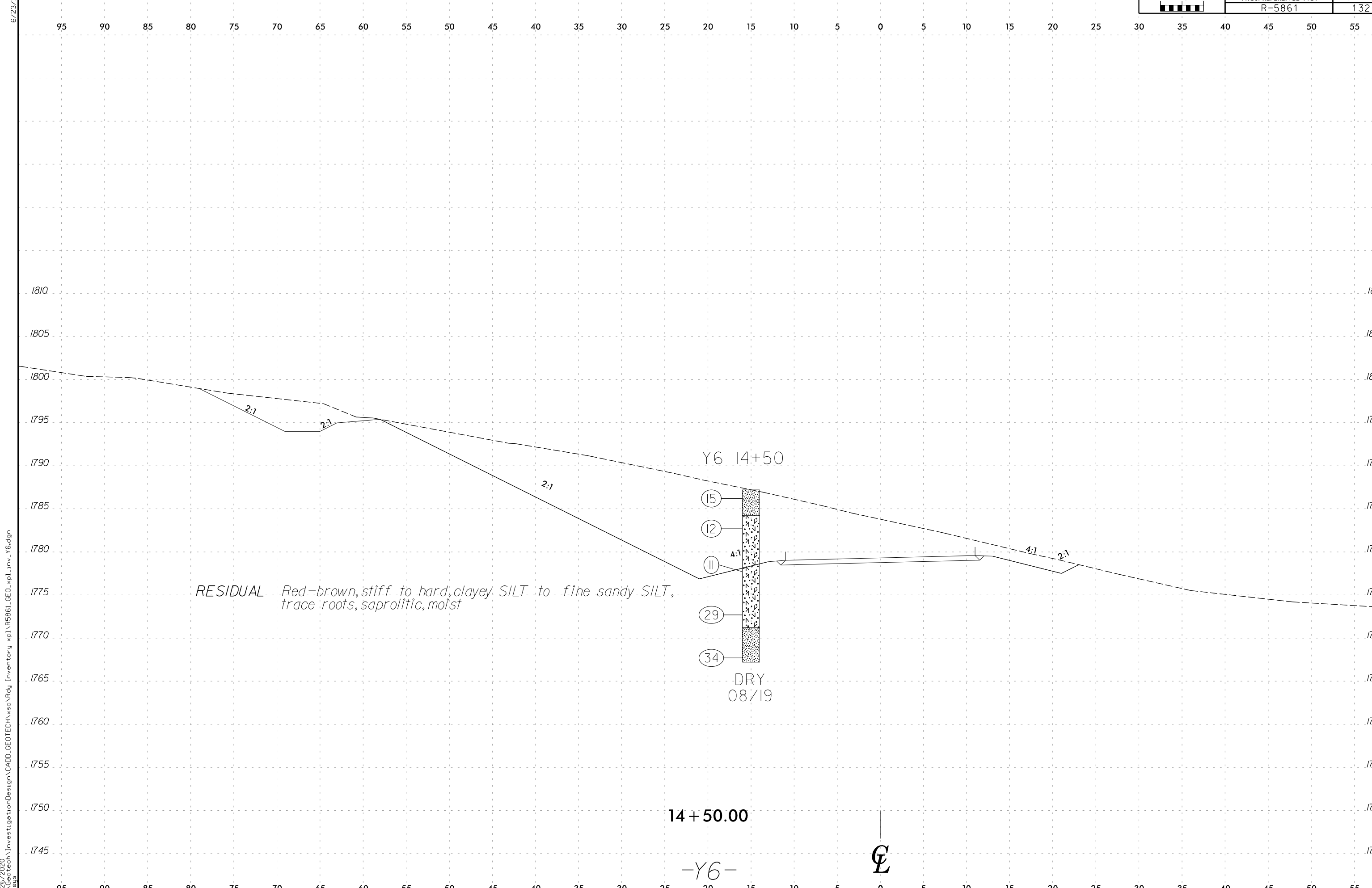


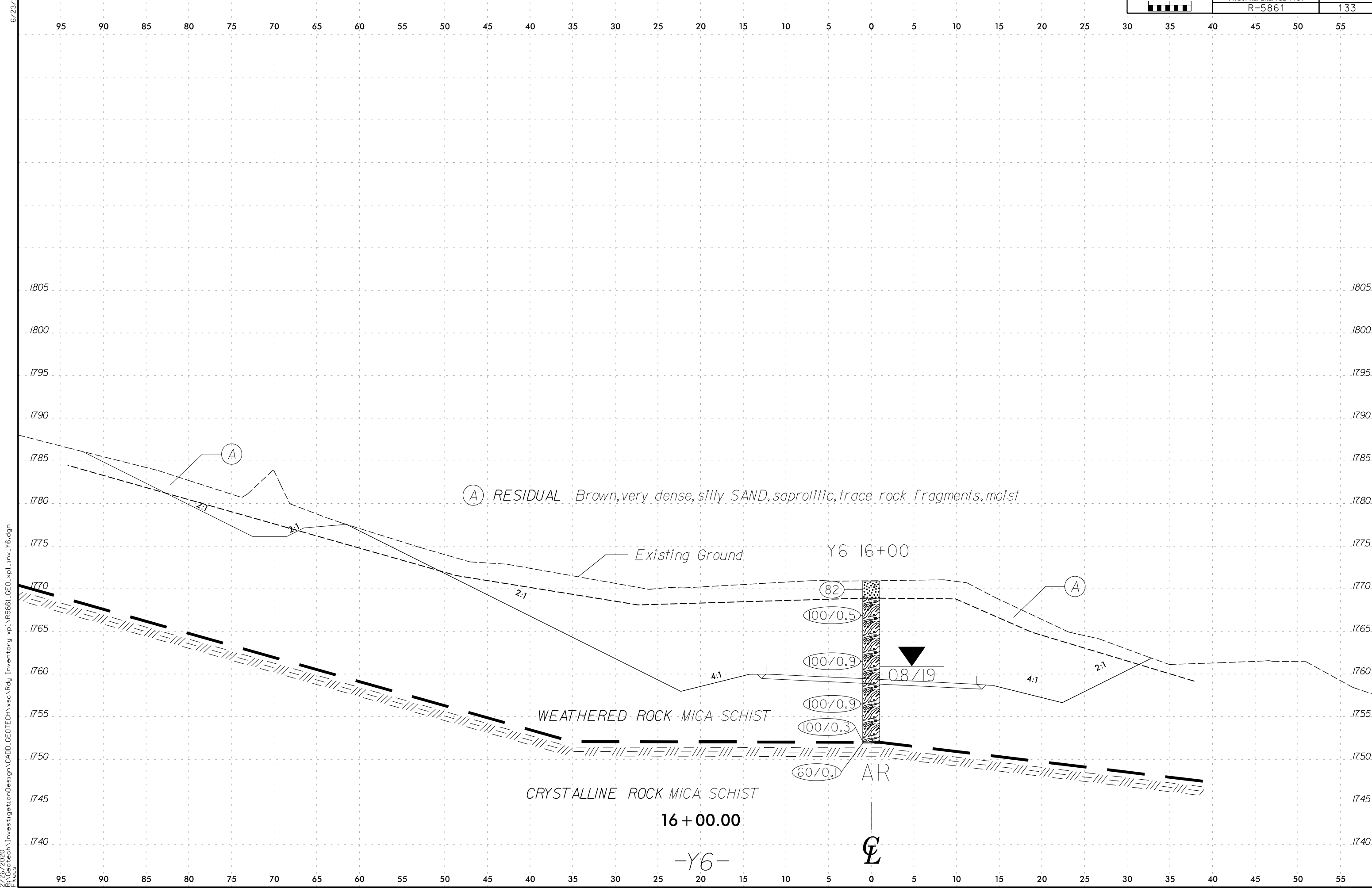
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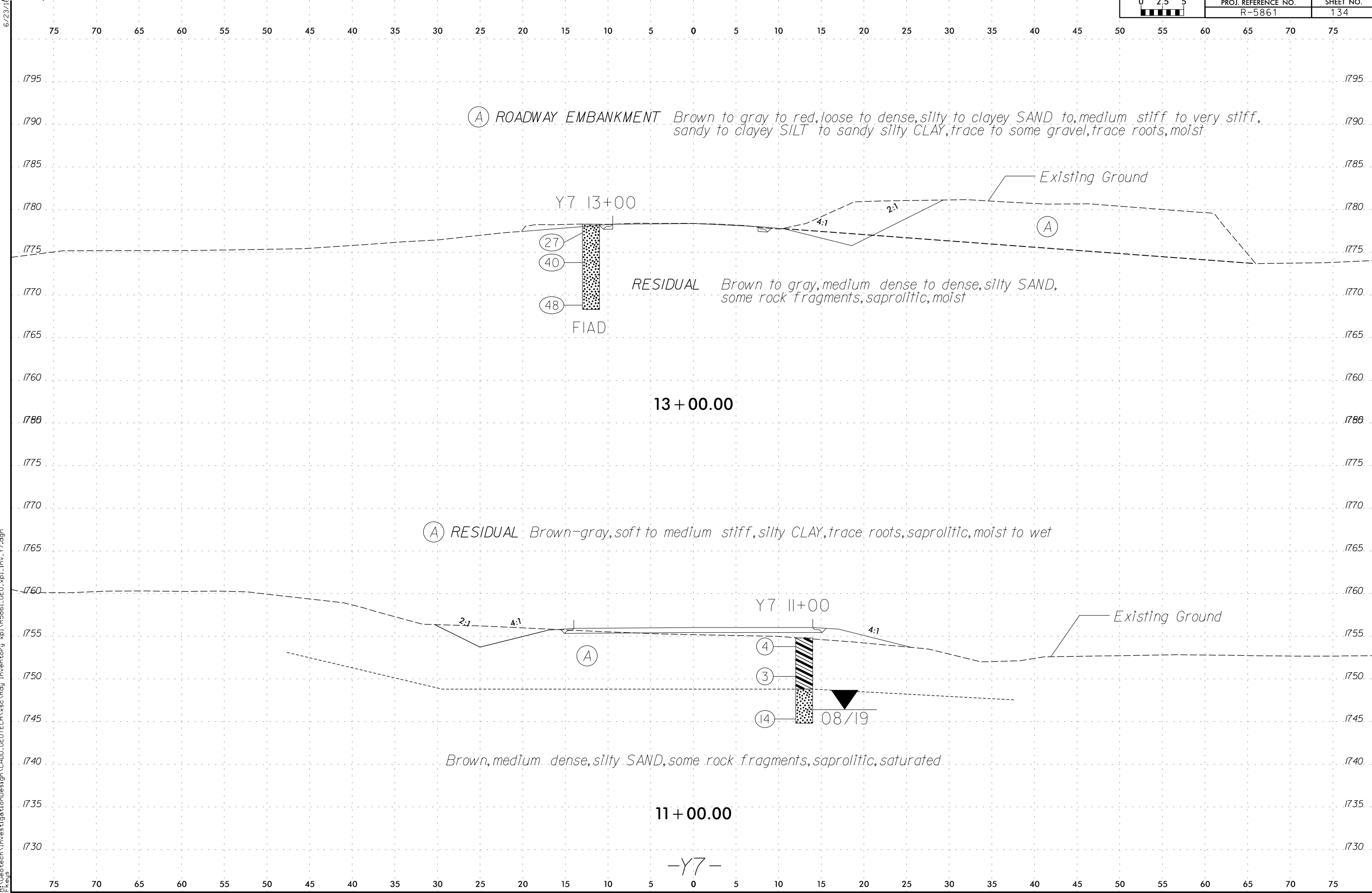


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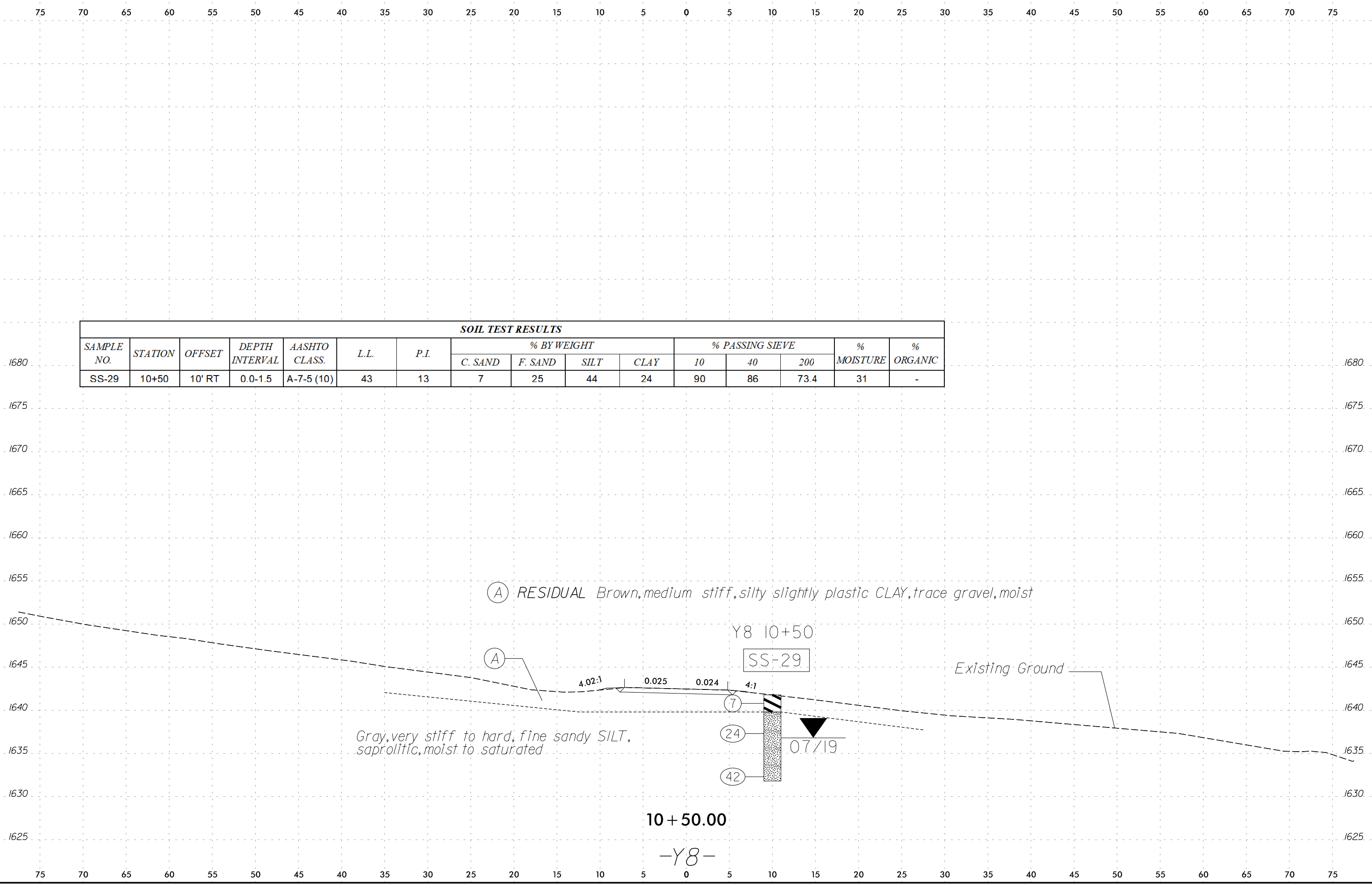


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-Y7-



SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-29	10+50	10' RT	0.0-1.5	A-7-5 (10)	43	13	7	25	44	24	90	86	73.4	31	-

(A) RESIDUAL Brown, medium stiff, silty slightly plastic CLAY, trace gravel, moist

Gray, very stiff to hard, fine sandy SILT, saprolitic, moist to saturated

Y8 10+50

SS-29

Existing Ground

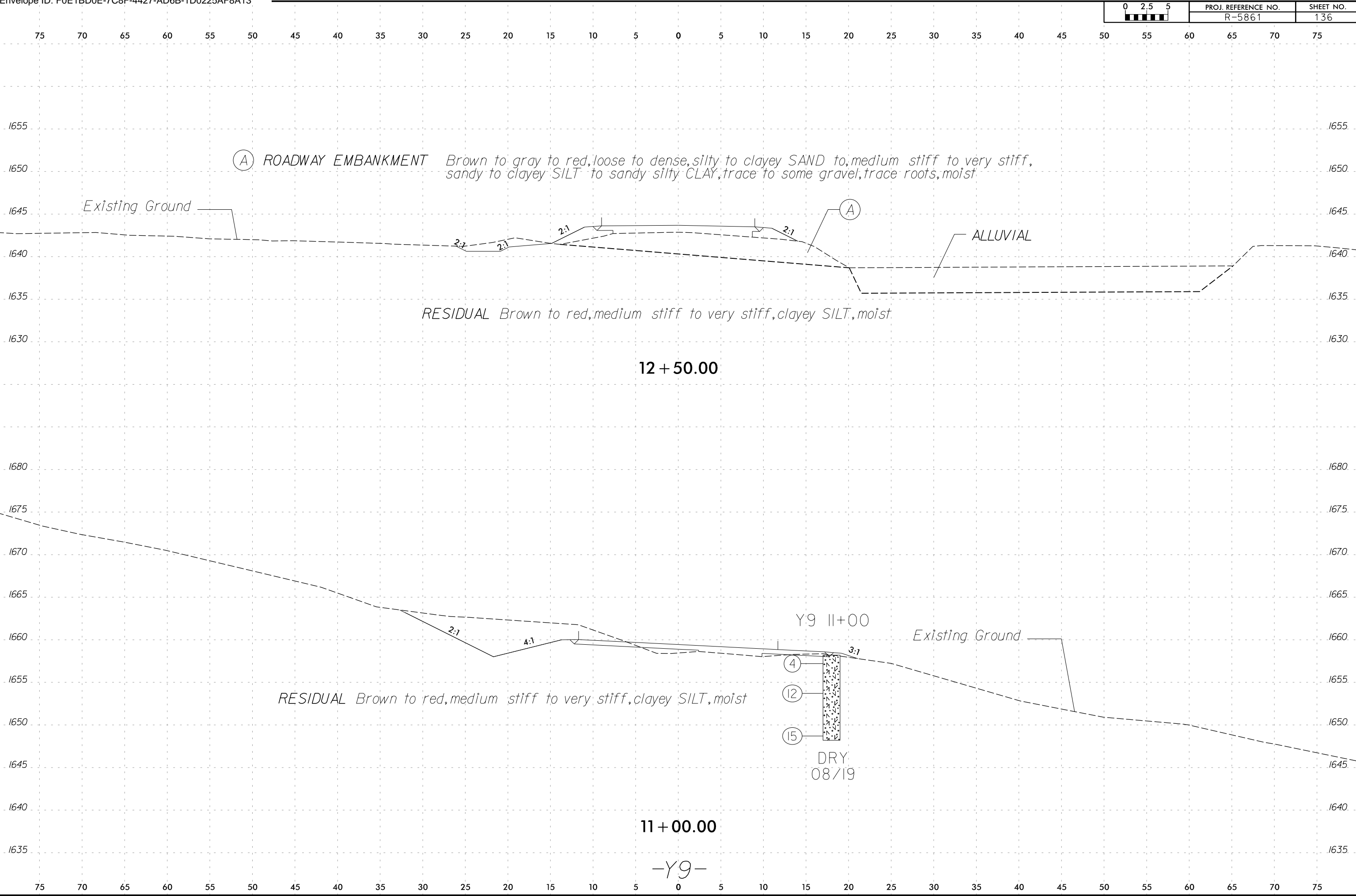
07/19

10 + 50.00

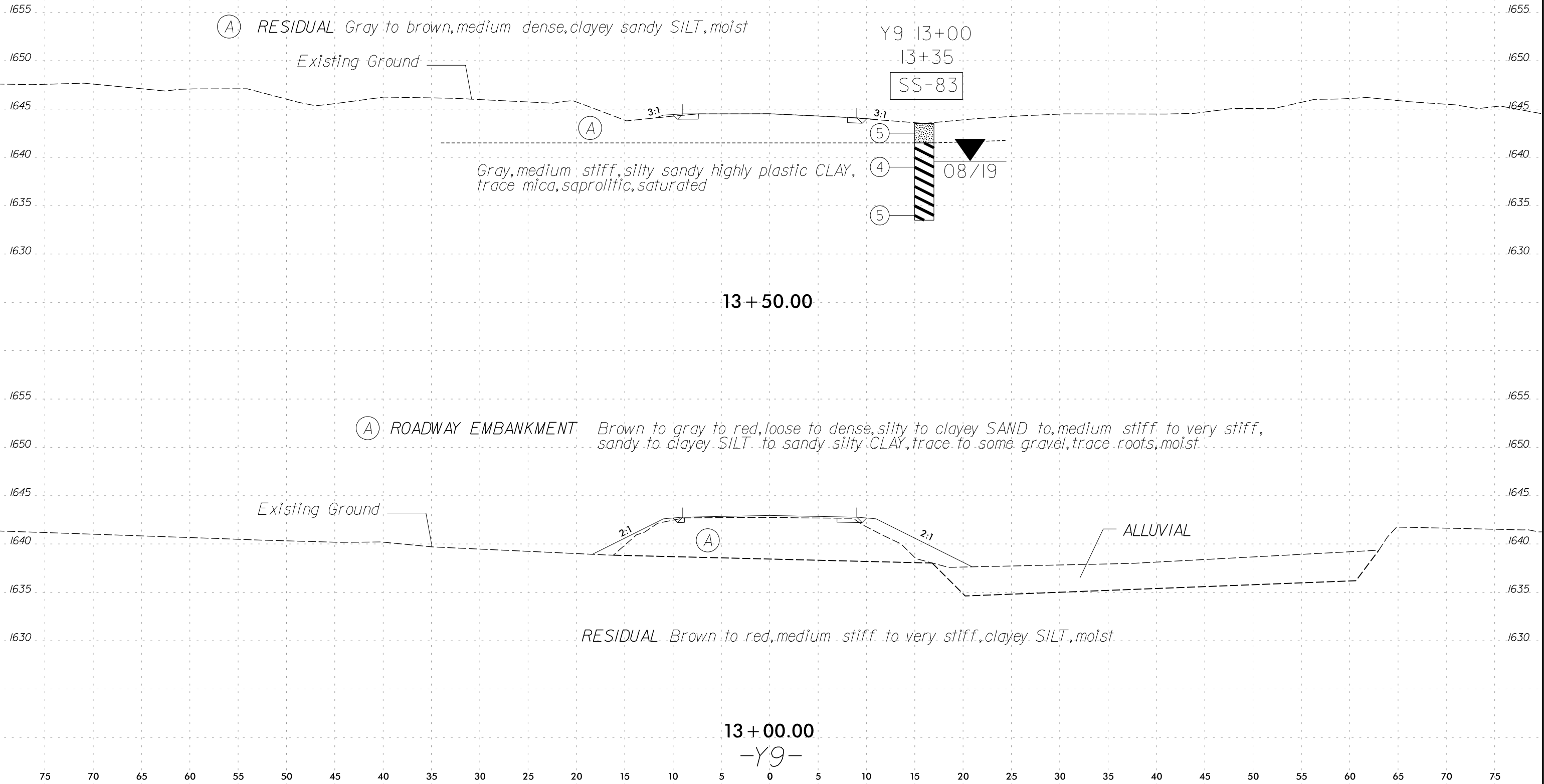
-Y8-

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P.kuj

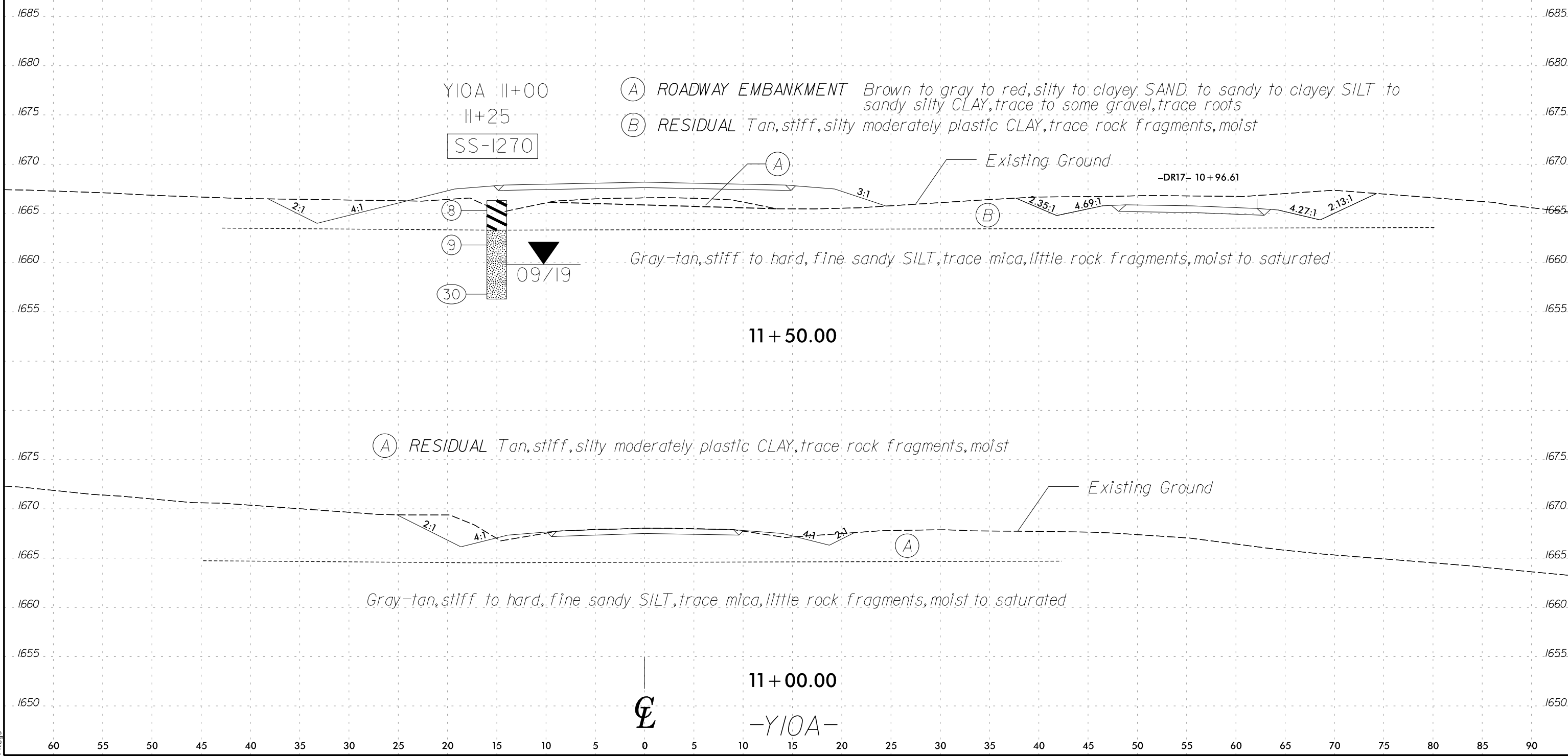


SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-83	13+00	16' RT	3.5-5.0	A-7-5 (25)	64	33	5	37	24	34	100	97	71.3	43.3	-

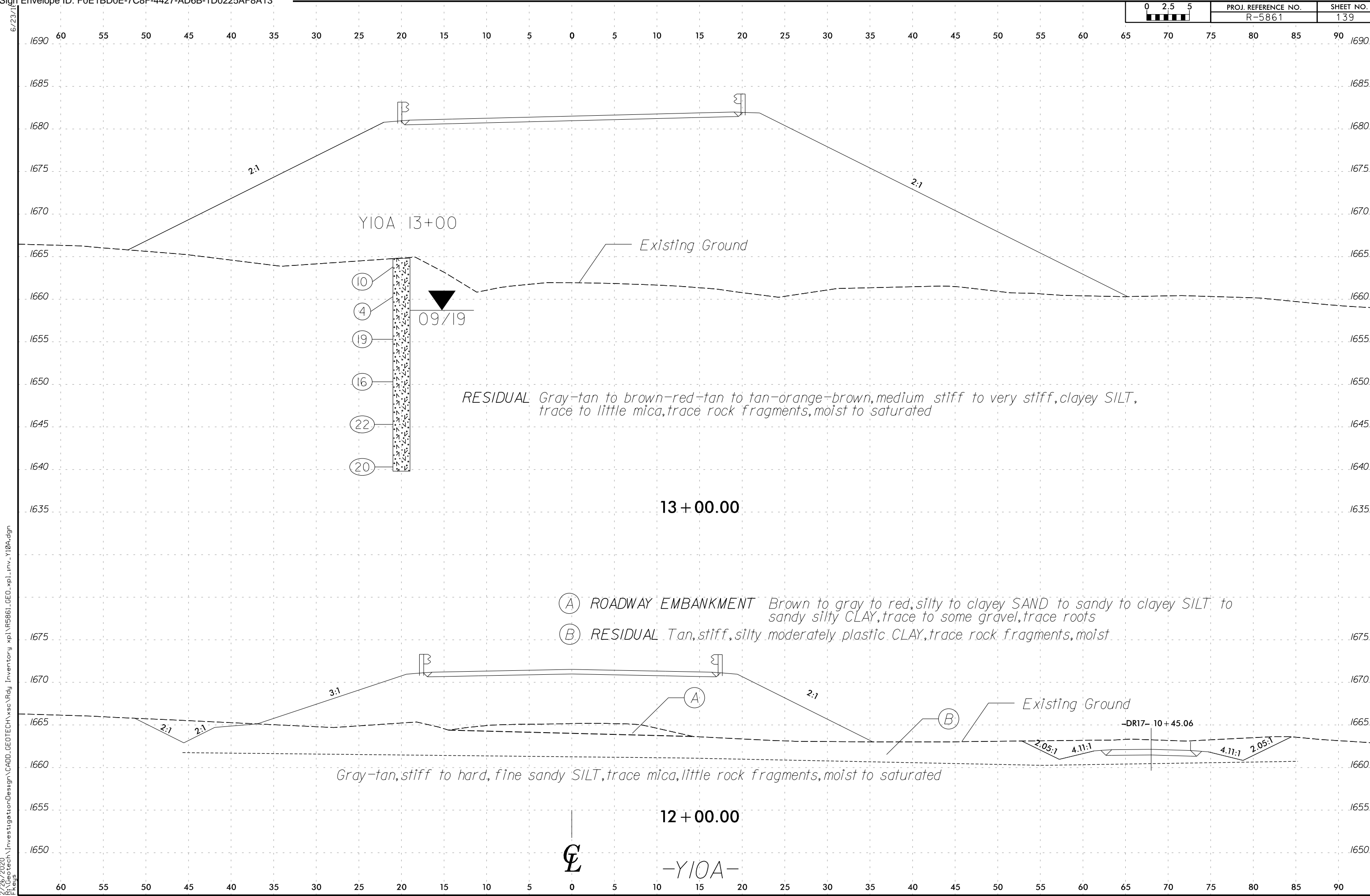


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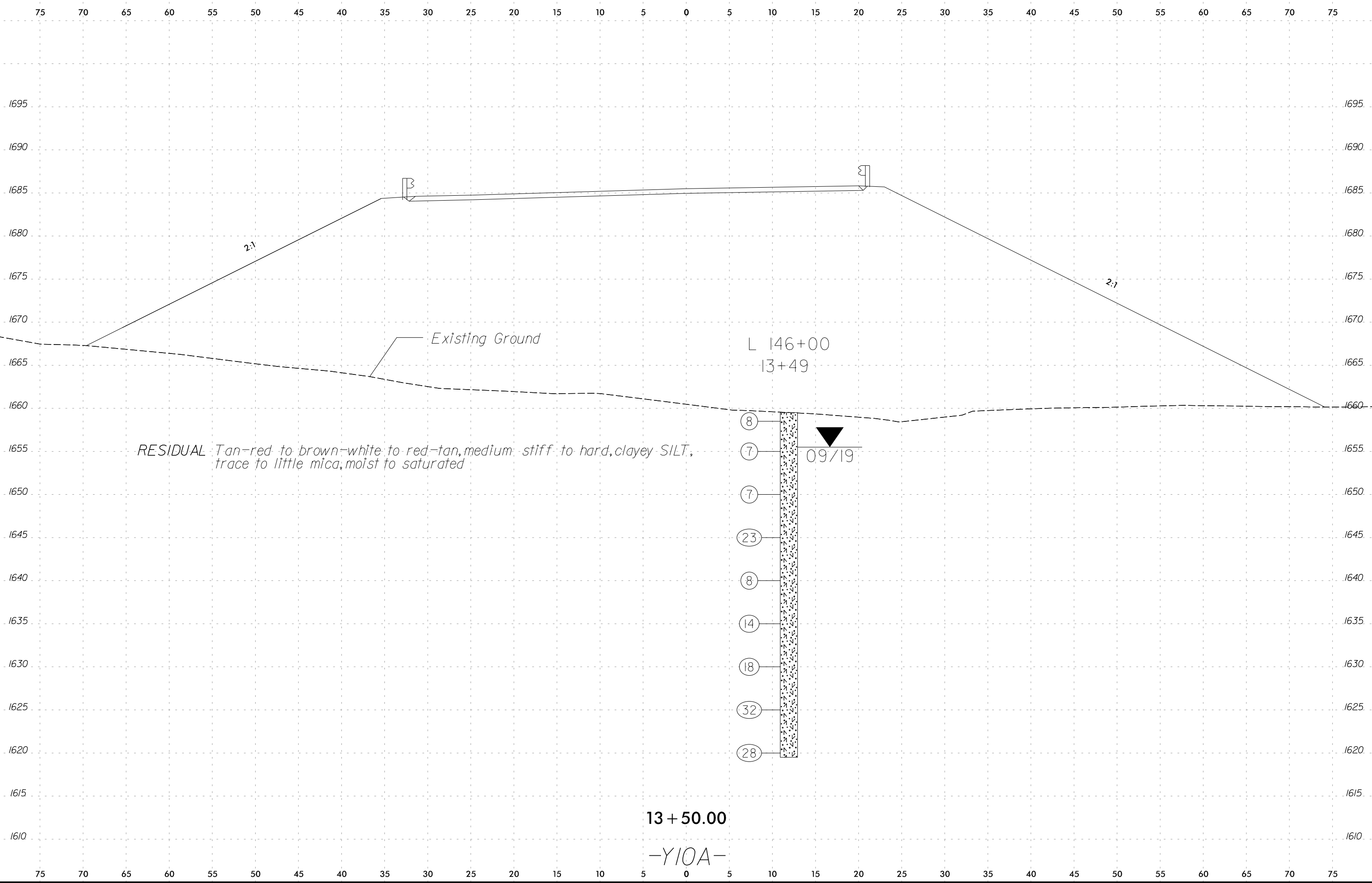
SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1270	11+25	15' LT	0.0-1.5	A-7-6 (23)	51	23	4	9	37	50	98	95	88.9	22.5	-



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RESIDUAL Tan-red to brown-white to red-tan, medium stiff to hard, clayey SILT, trace to little mica, moist to saturated

Existing Ground

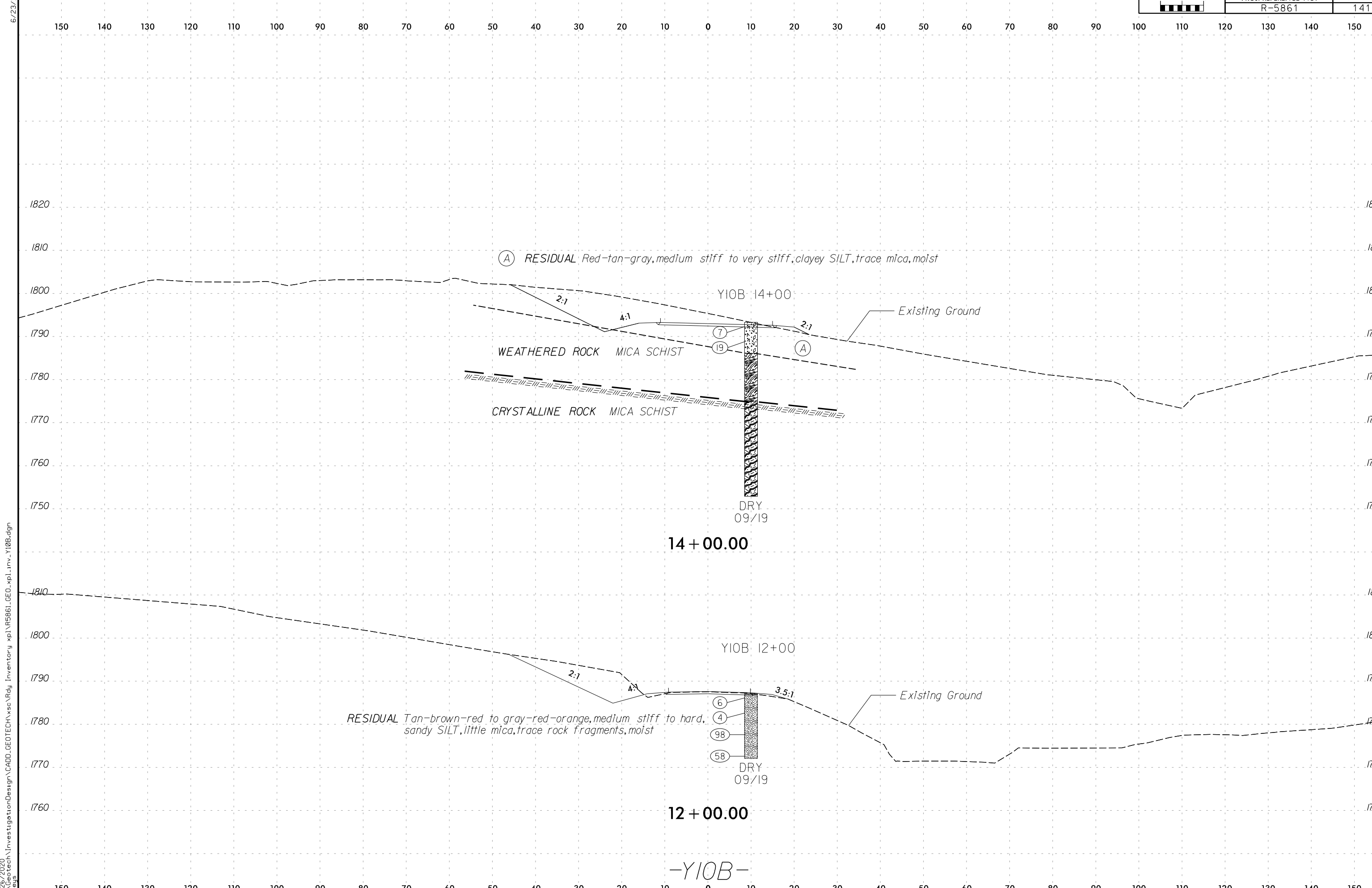
L 146+00
13+49

09/19

13 + 50.00

-Y10A-

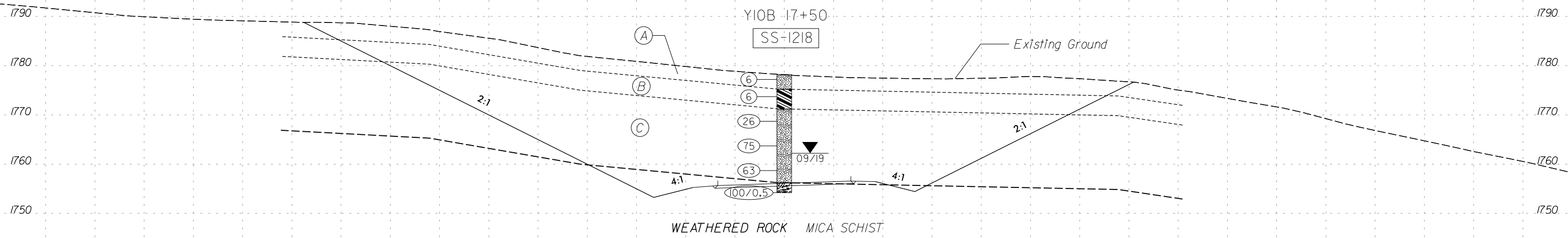
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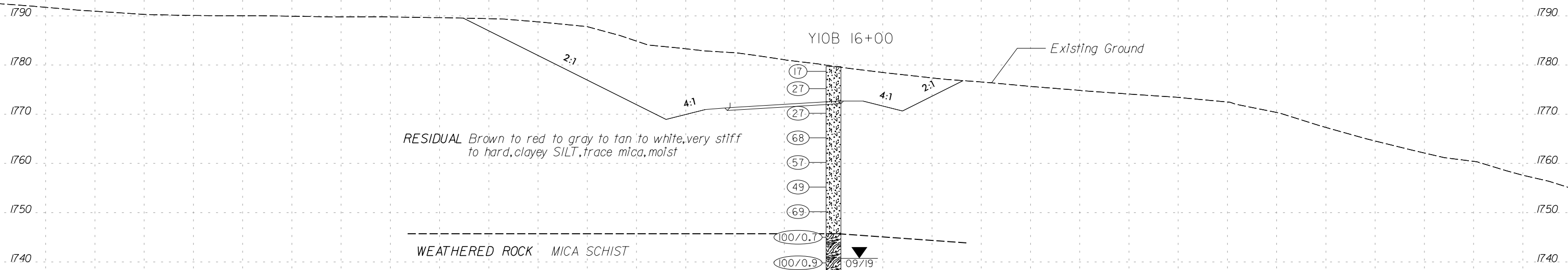
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1218	17+50	0	8.5-10.0	A-4 (5)	38	6	8	28	50	14	100	95	75.2	20.9	-

- (A) RESIDUAL Tan-gray-red, medium stiff, sandy SILT, moist
- (B) Brown-gray-tan, medium stiff, fine sandy silty CLAY, moist
- (C) Red-tan to orange-black-red, hard, fine sandy SILT, trace to little mica, moist to saturated



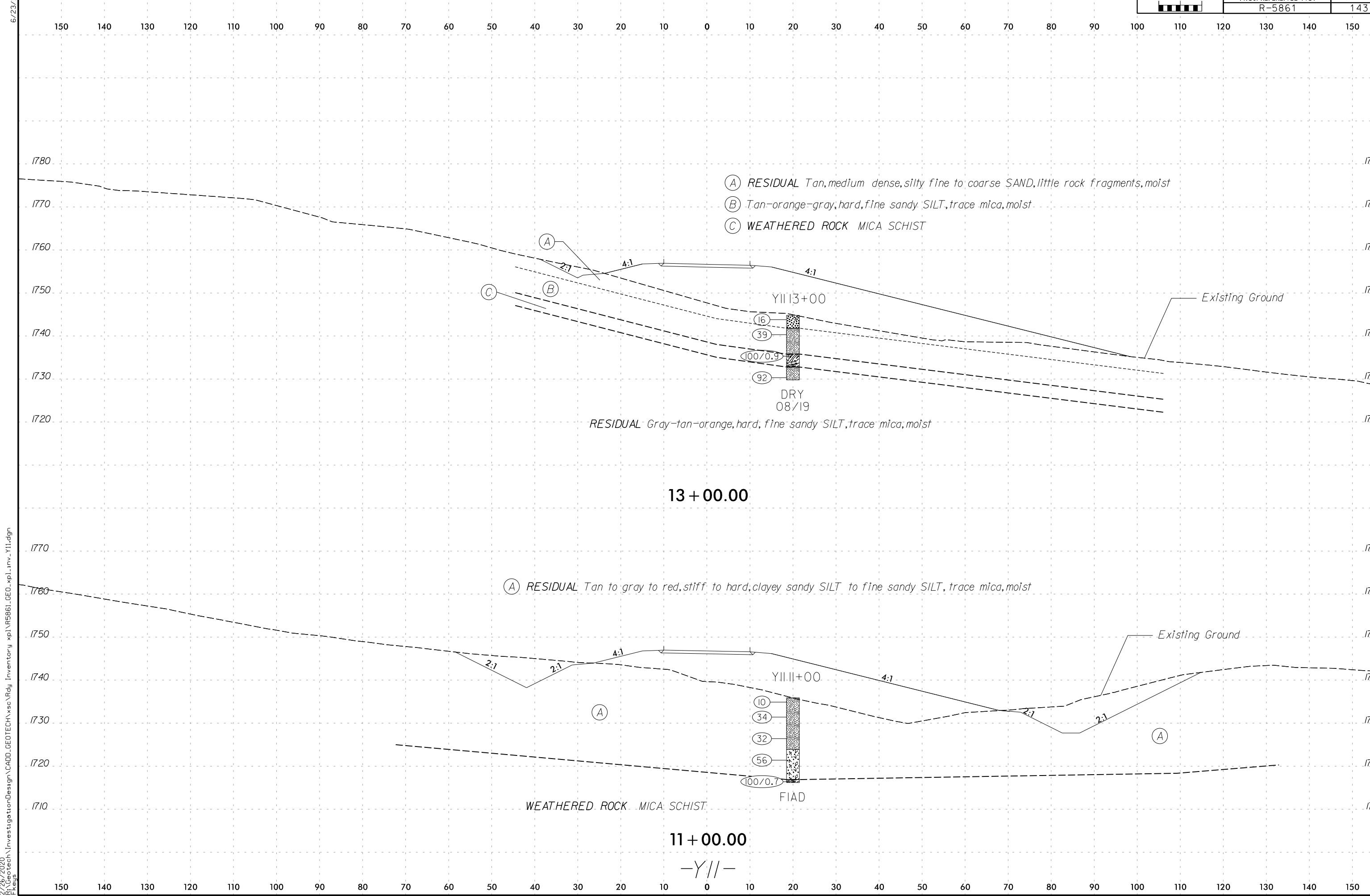
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16 + 00.00

-Y10B-

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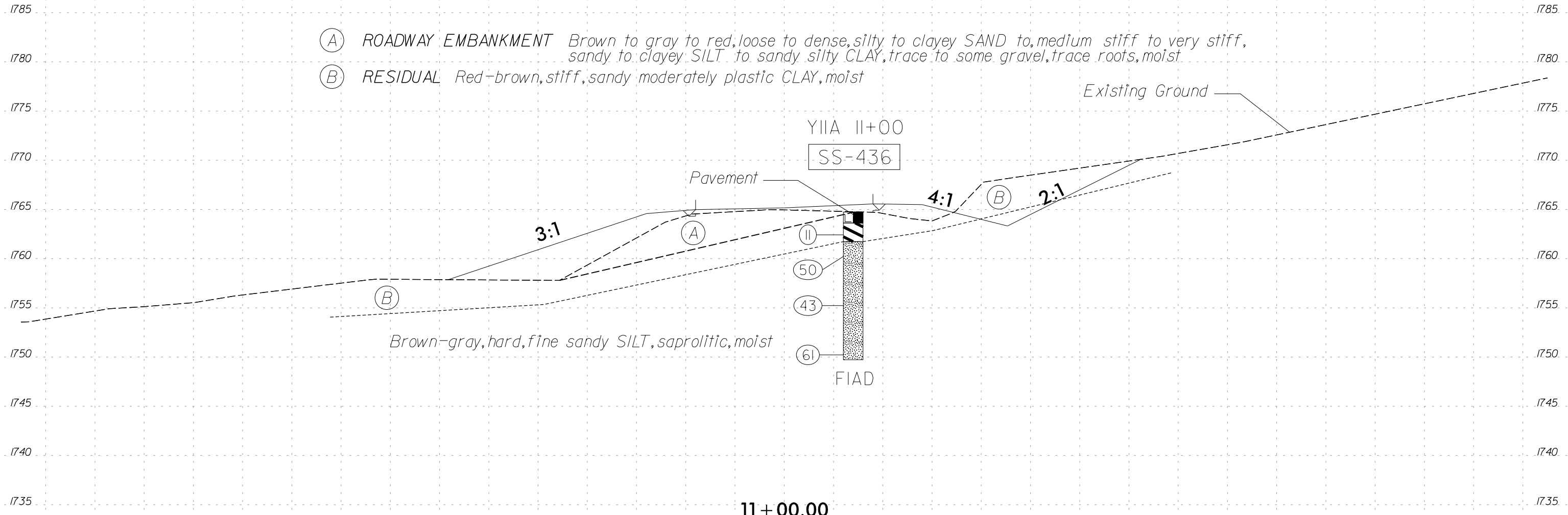


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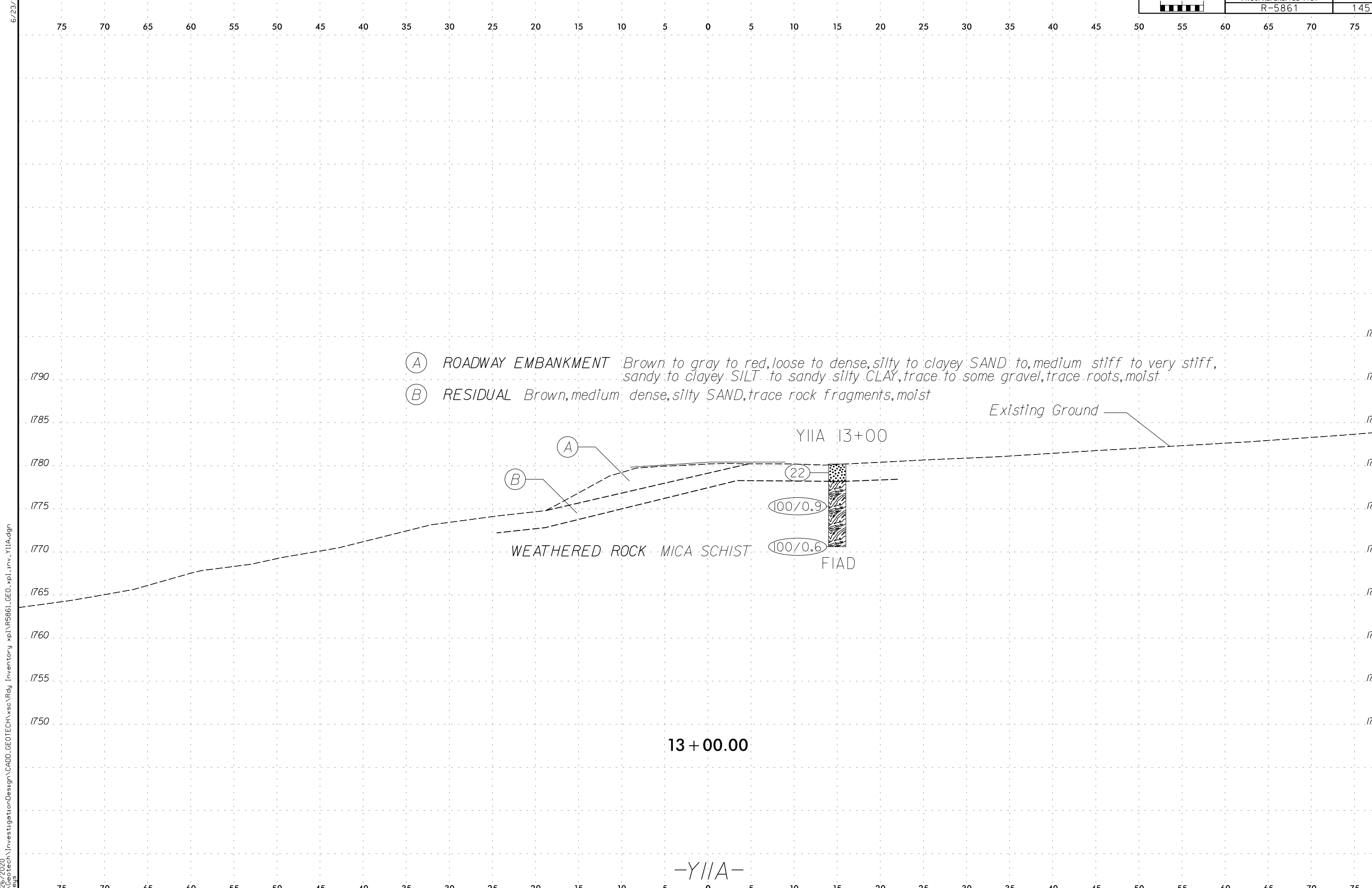
SOIL TEST RESULTS															
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-436	11+00	7' RT	1.3-2.8	A-7-6 (9)	44	17	16	25	23	36	87	77	59.5	19.5	-

- (A) ROADWAY EMBANKMENT *Brown to gray to red, loose to dense, silty to clayey SAND to, medium stiff to very stiff, sandy to clayey SILT to sandy silty CLAY, trace to some gravel, trace roots, moist*
- (B) RESIDUAL *Red-brown, stiff, sandy moderately plastic CLAY, moist*

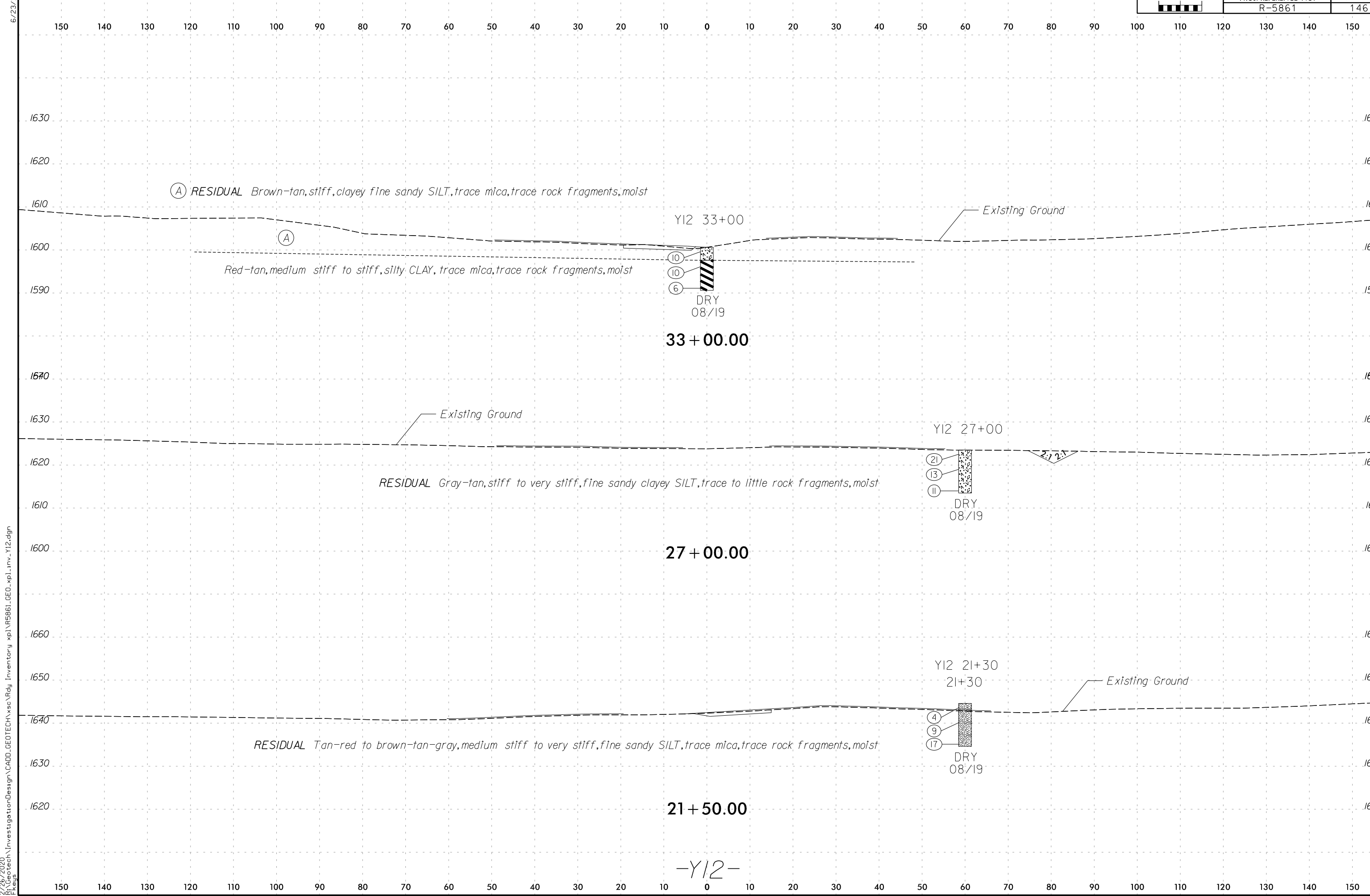


11 + 00.00

-Y//A-



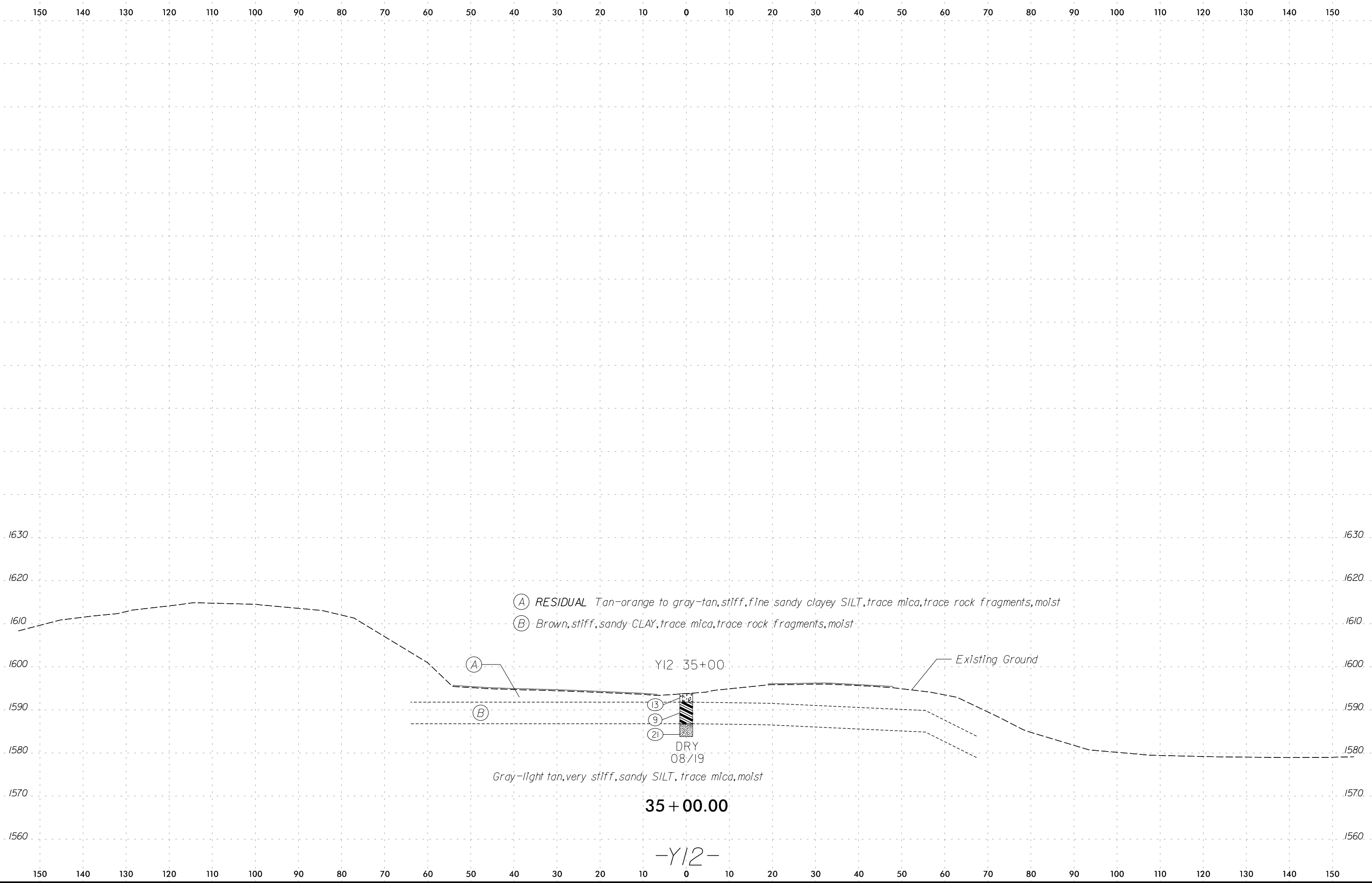
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-Y12-

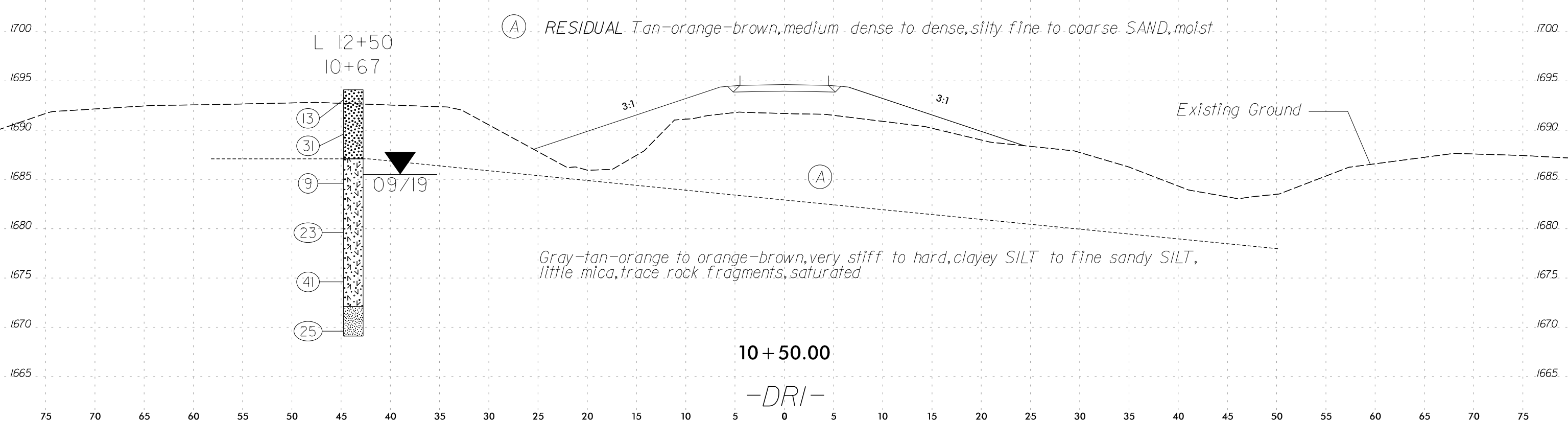
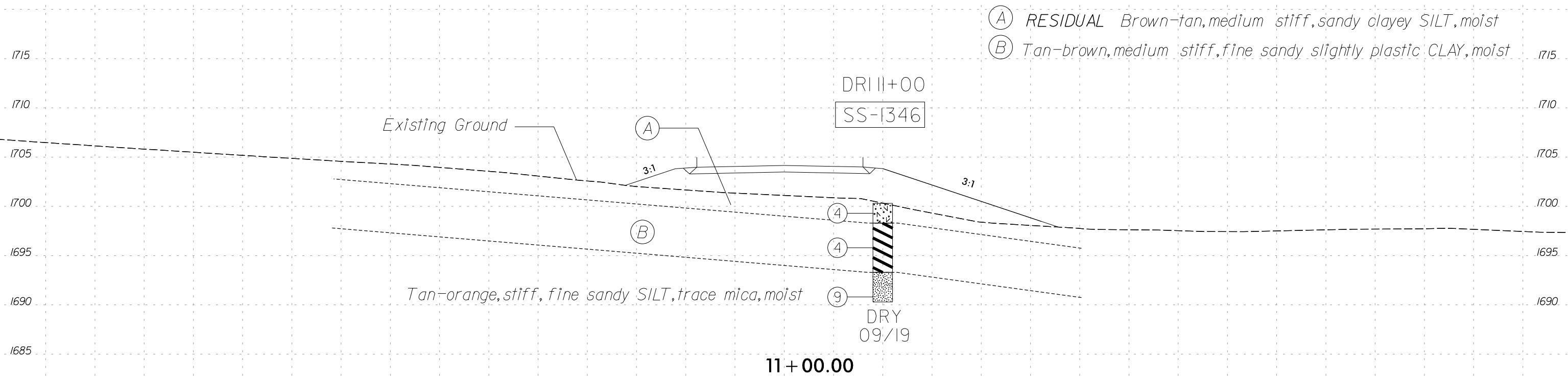
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P. Keijs

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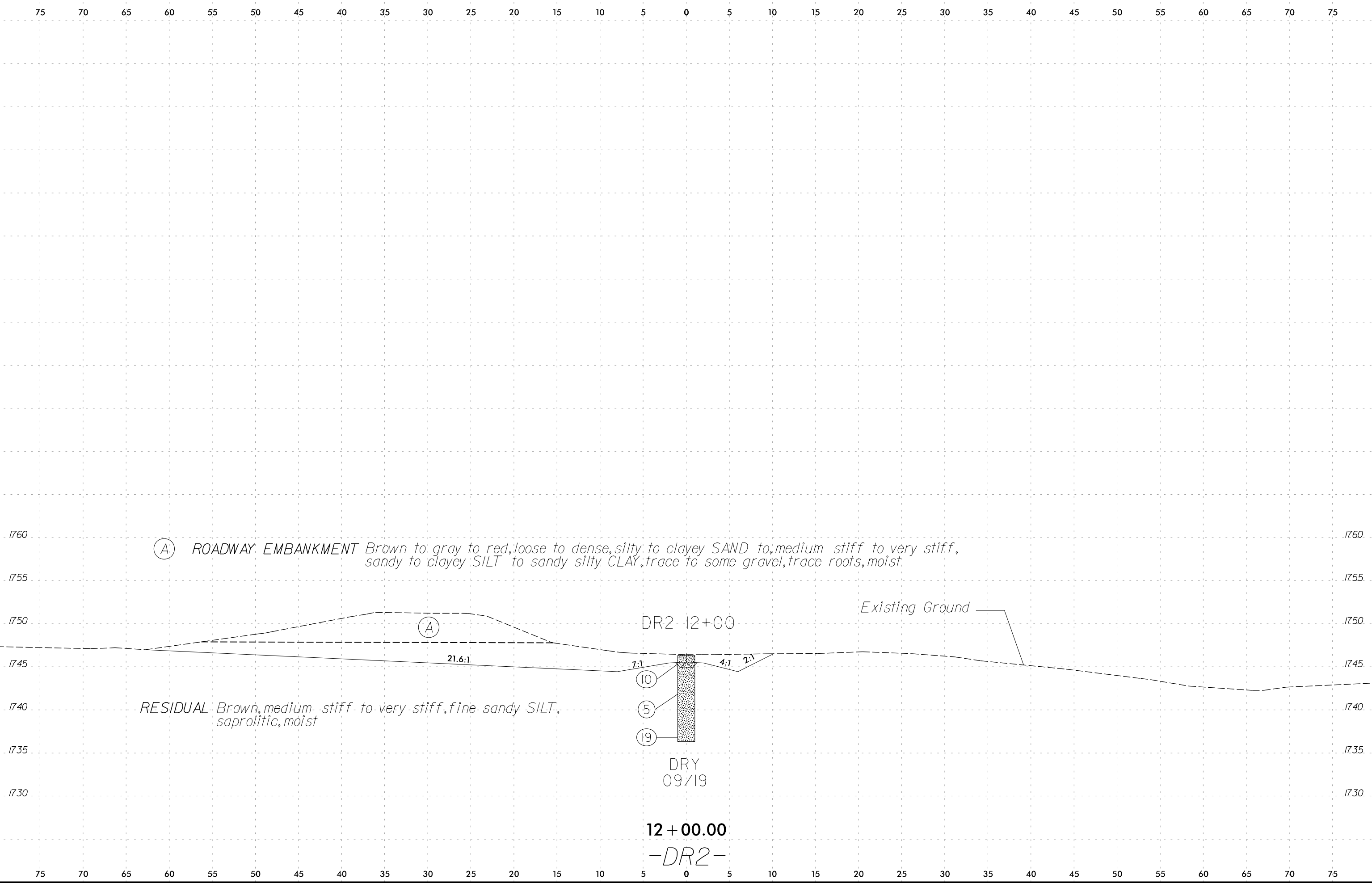
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SOIL TEST RESULTS															
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1346	11+00	20' RT	3.5-5.0	A-7-6 (7)	41	12	8	37	19	36	98	94	62.3	24.3	-

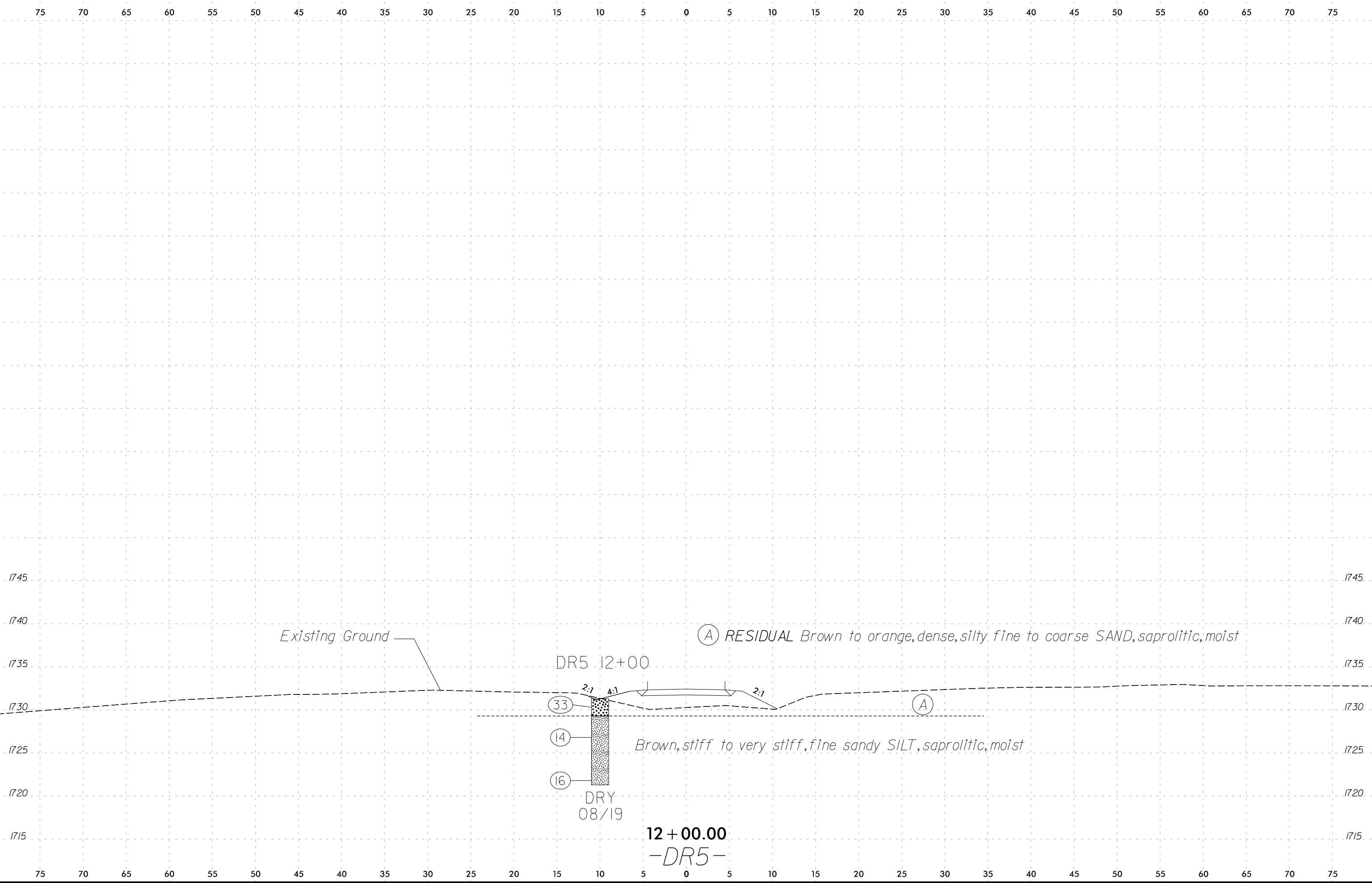


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P. Keijs

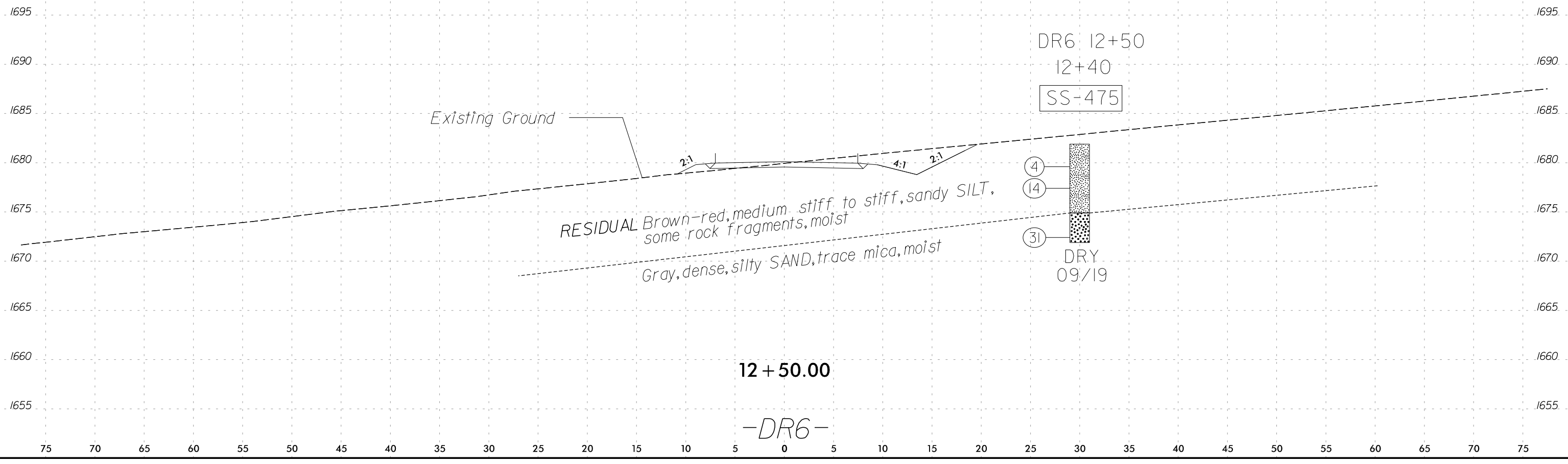


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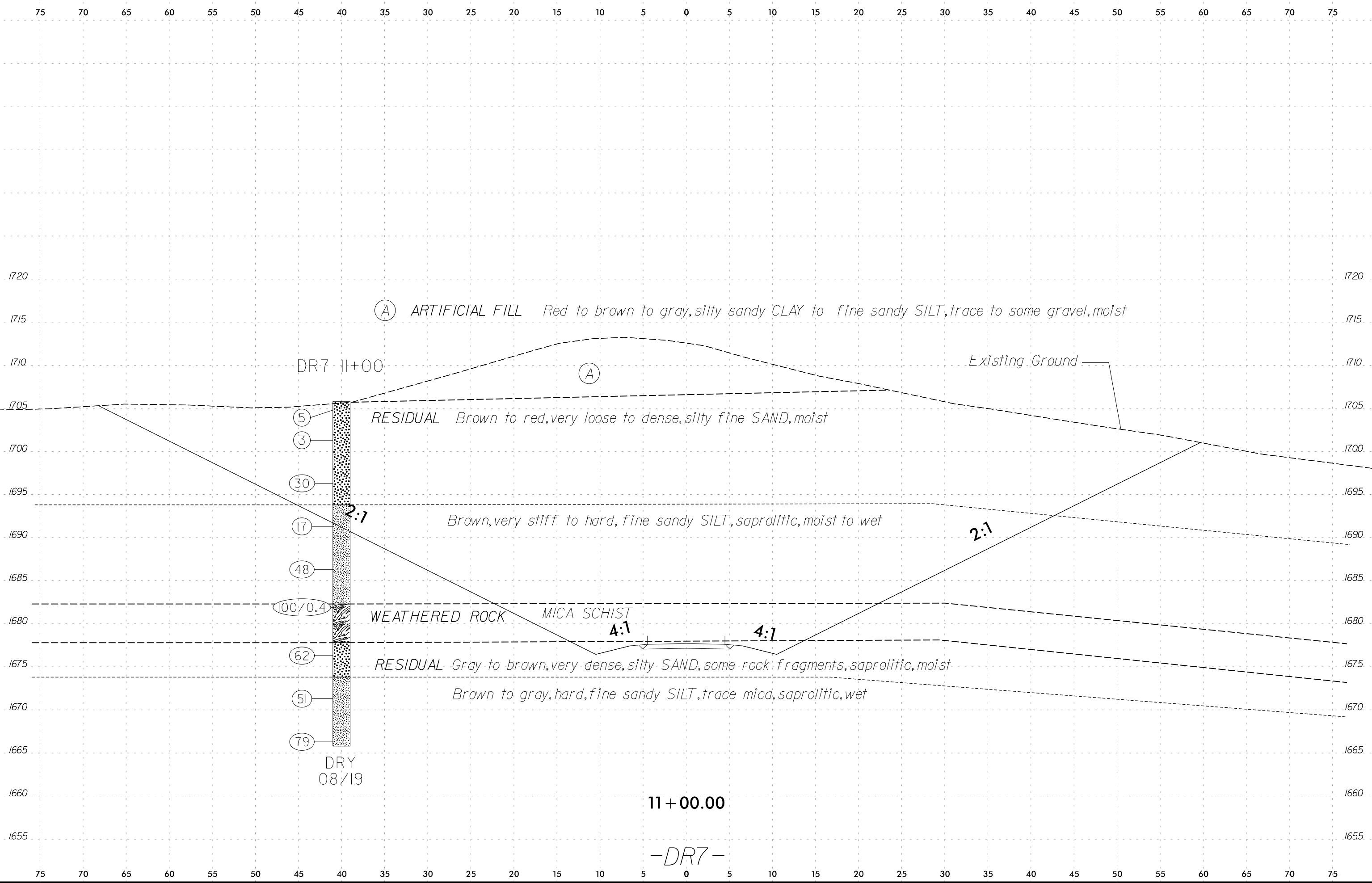


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SOIL TEST RESULTS															
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-475	12+40	30' RT	1.3-2.8	A-4 (4)	32	10	13	32	21	34	97	91	58.5	18	-



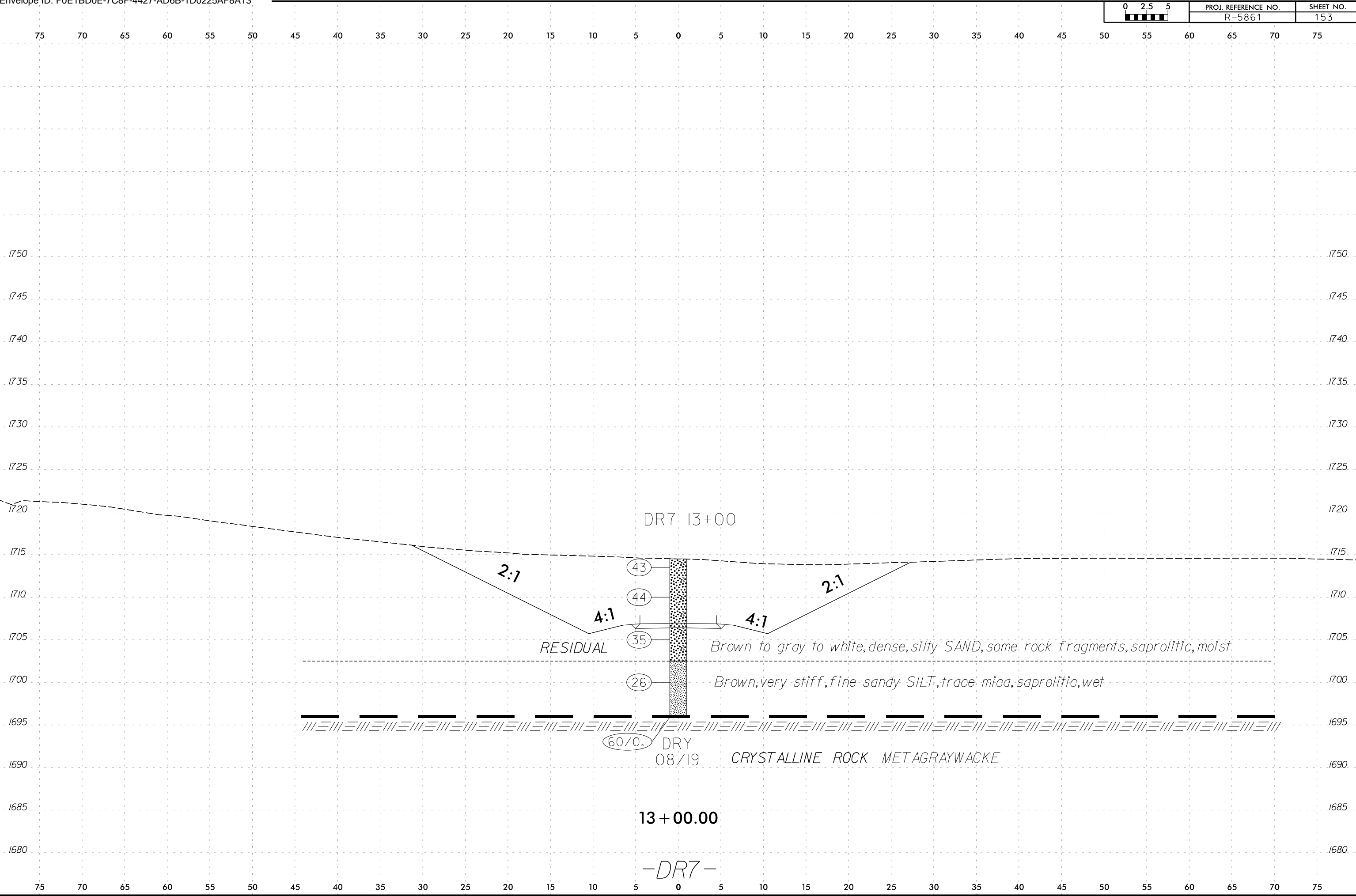
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11 + 00.00
-DR7-

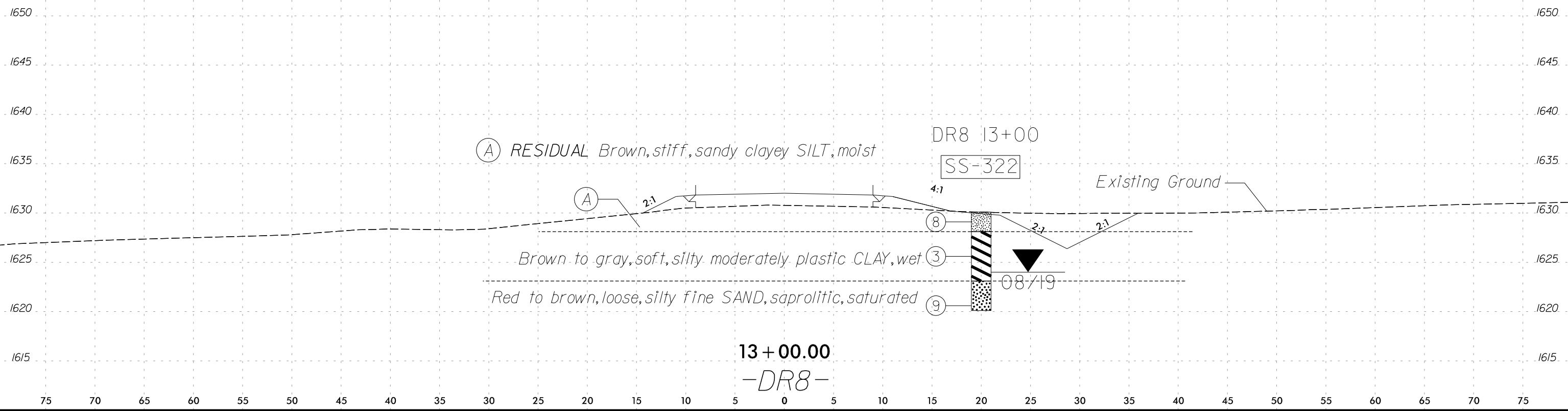
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SOIL TEST RESULTS															
SAMPLE NO.	STATION	OFFSET	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING SIEVE			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-322	13+00	20' RT	3.5-5.0	A-7-6 (19)	47	23	3	24	23	50	100	99	79.9	32.4	-

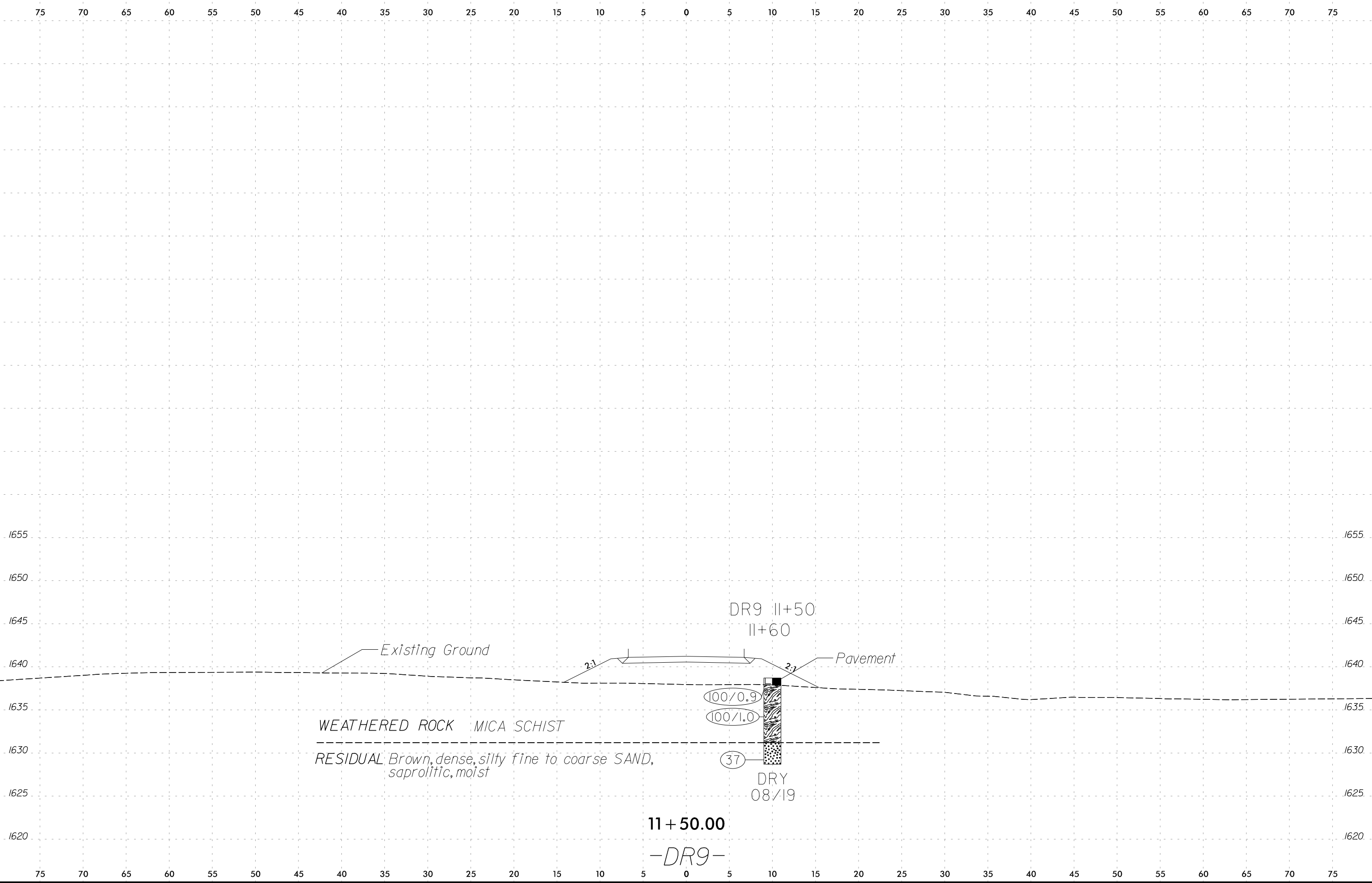
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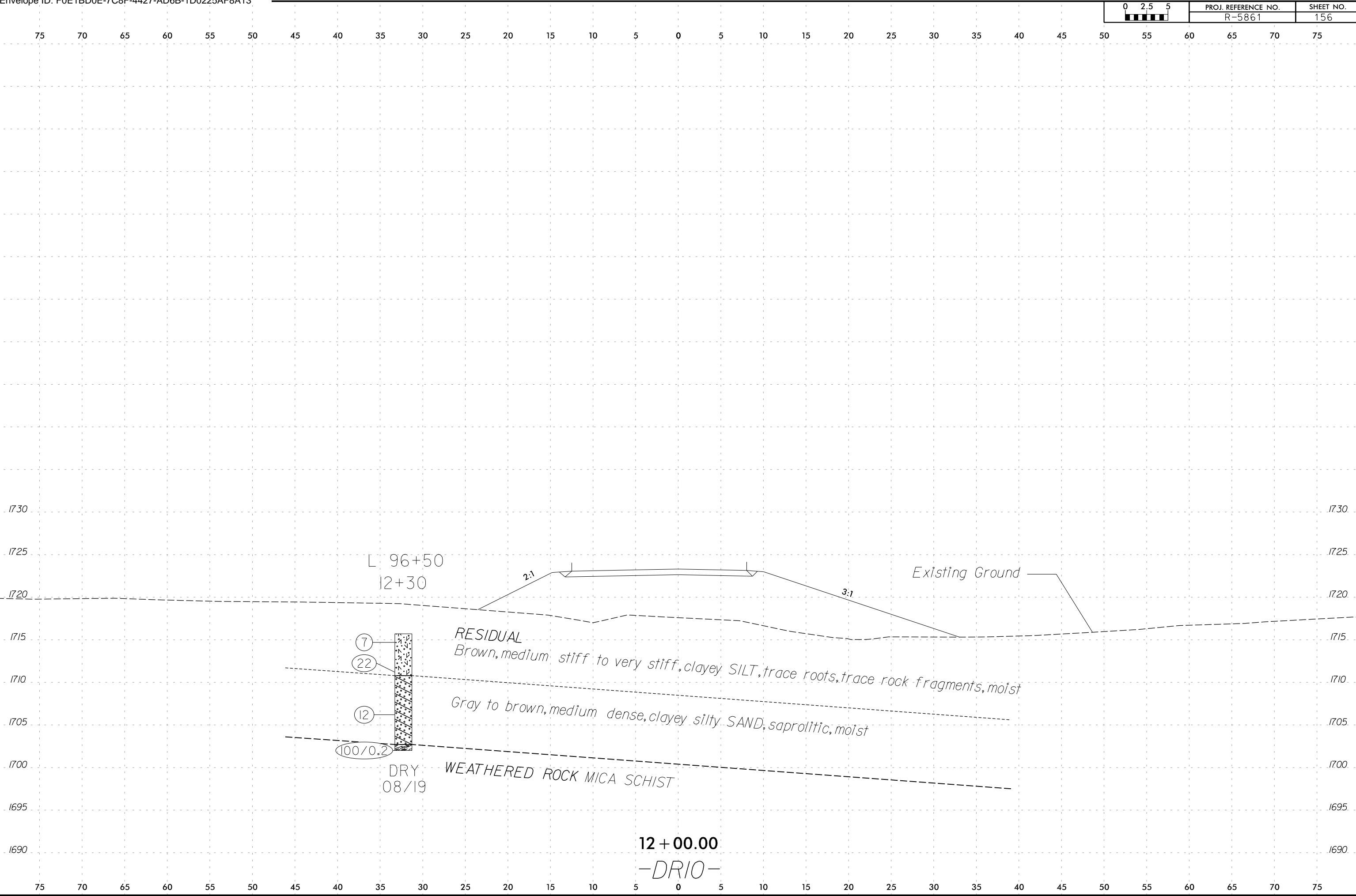
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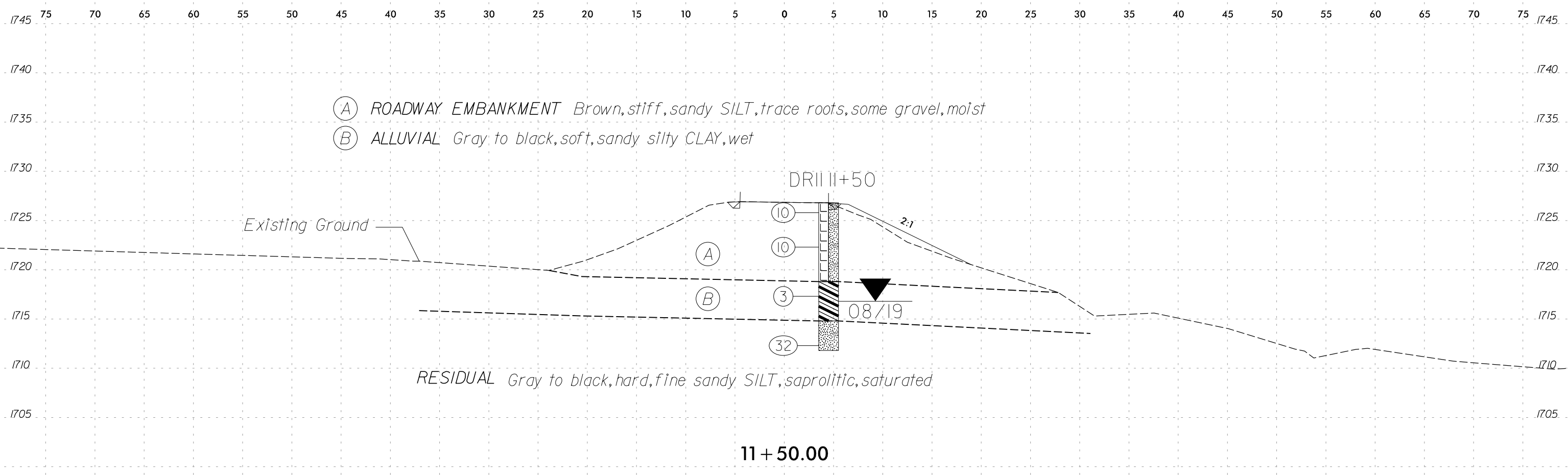
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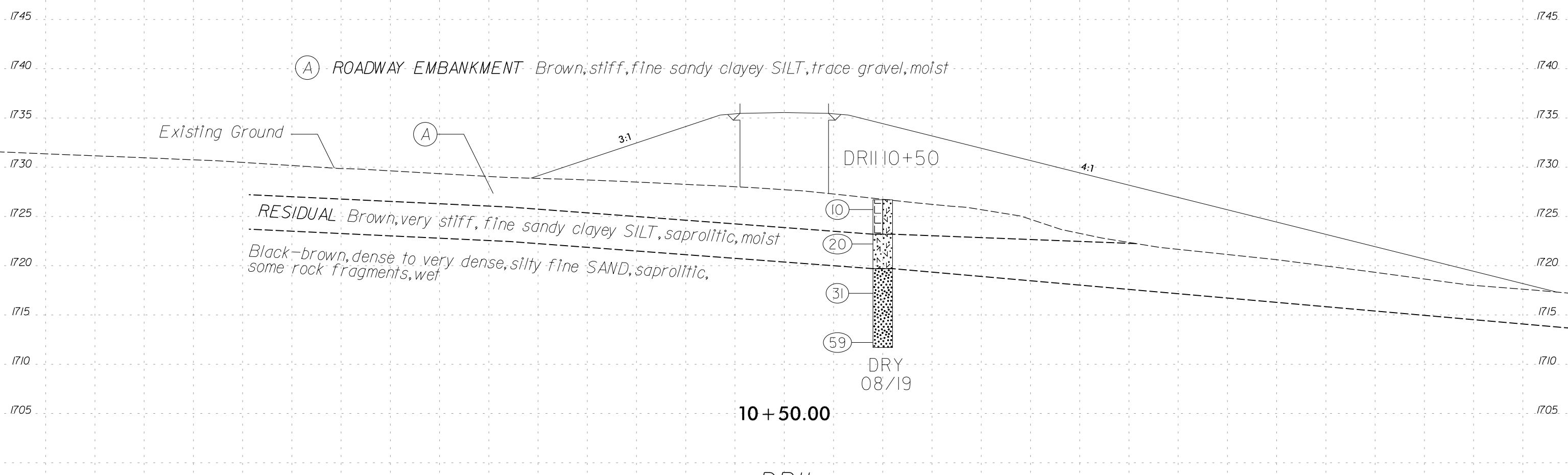
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-DR10-



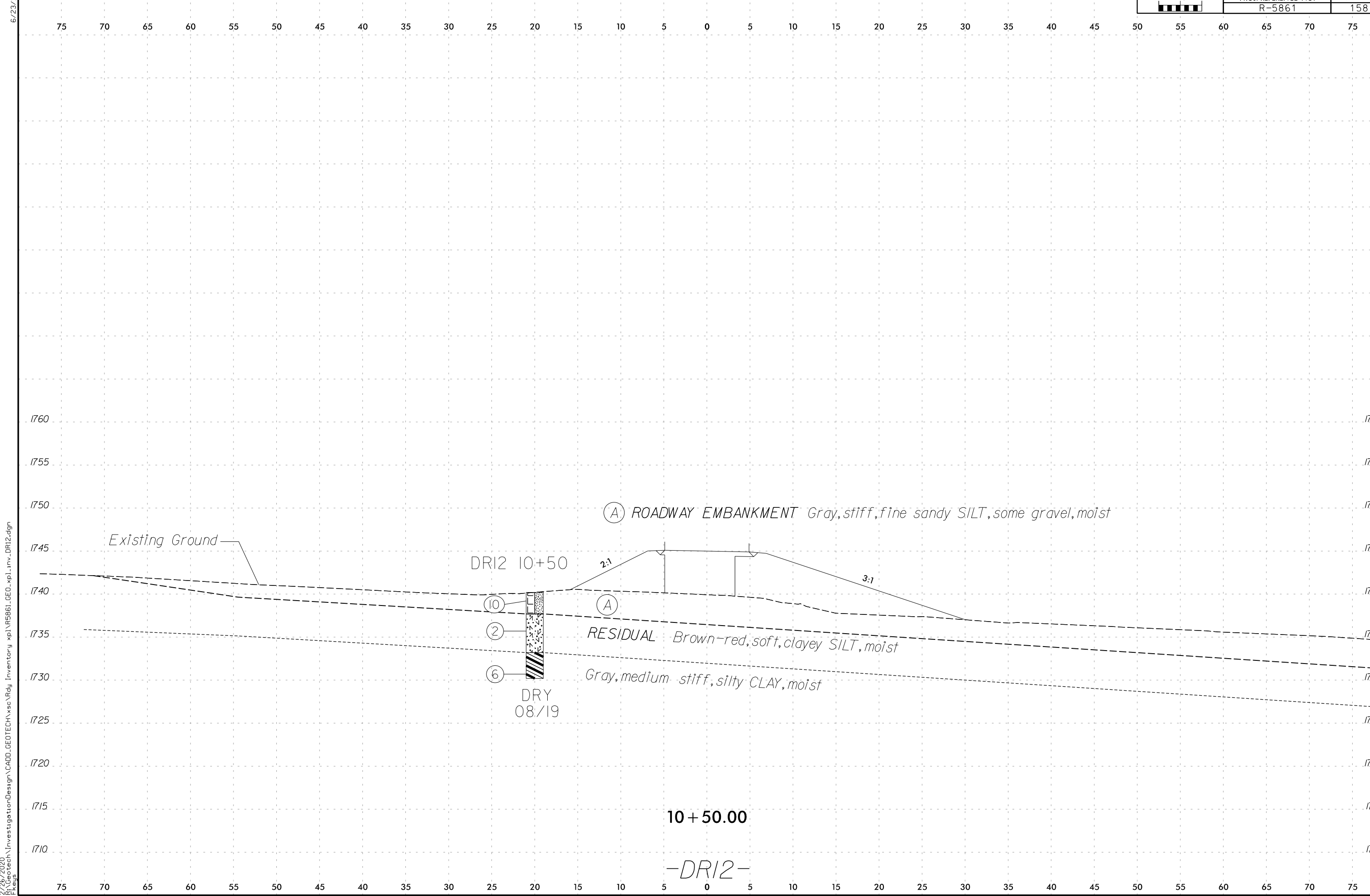
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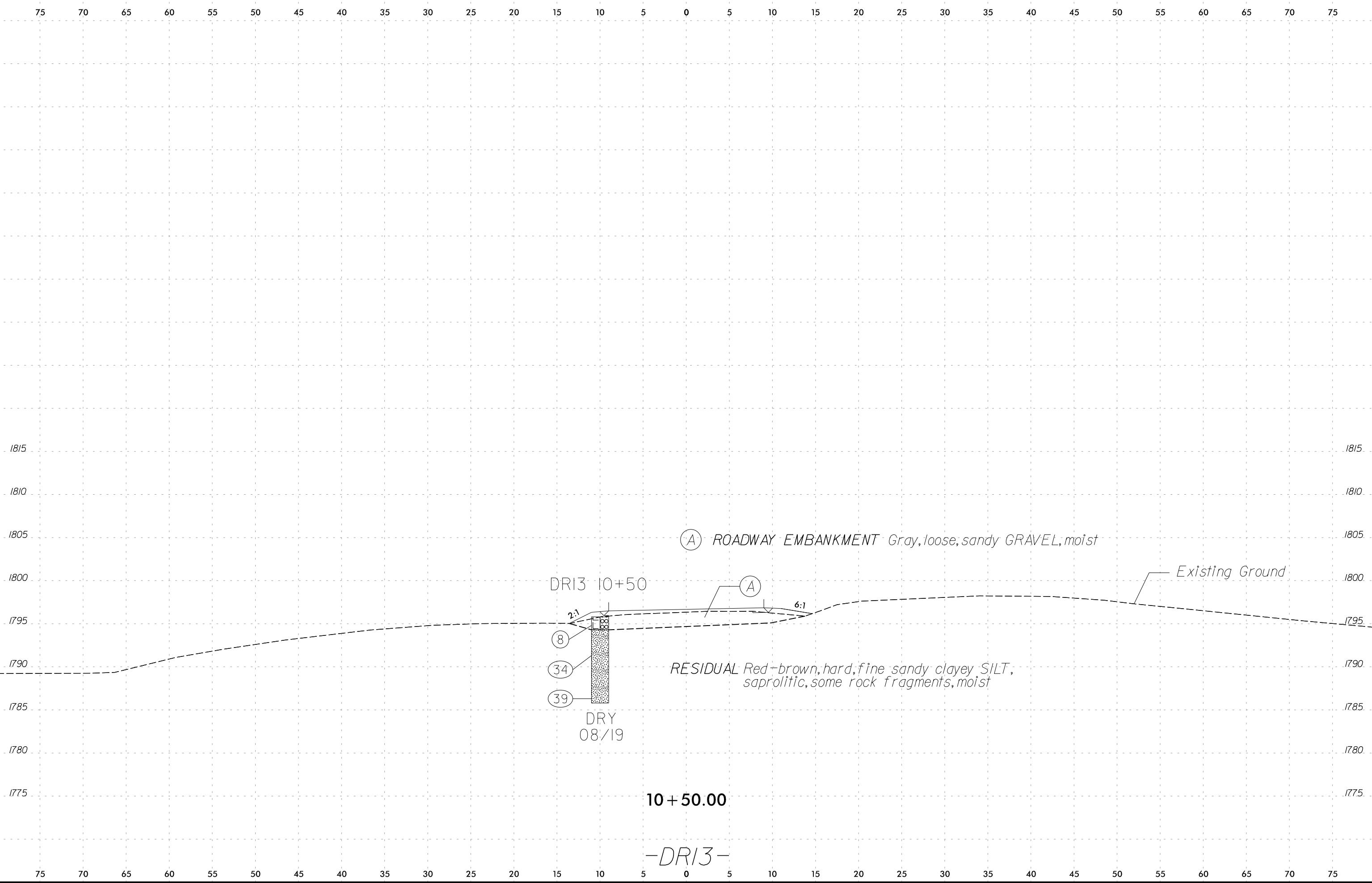
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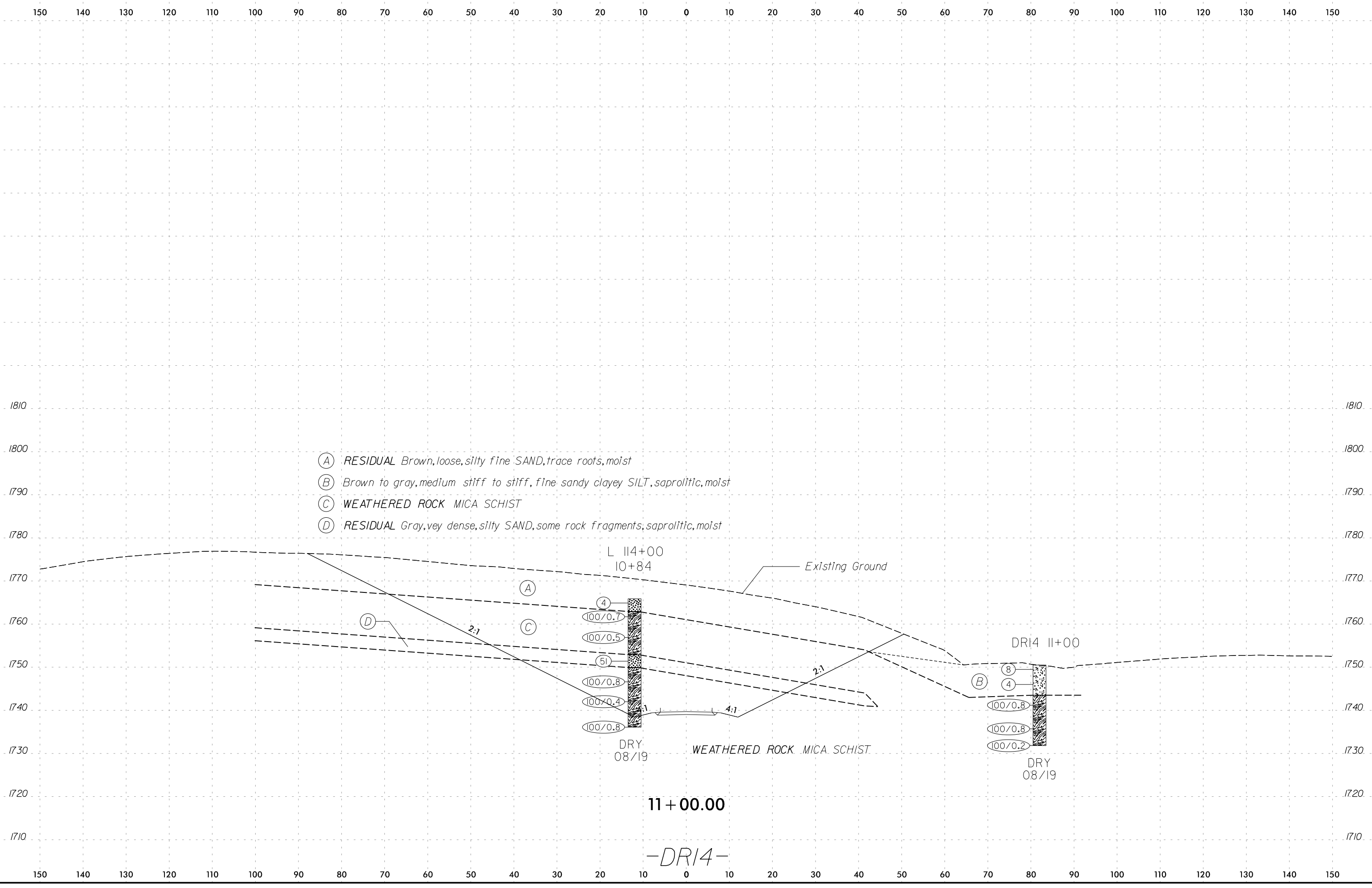
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- (A) RESIDUAL Brown, loose, silty fine SAND, trace roots, moist
- (B) Brown to gray, medium stiff to stiff, fine sandy clayey SILT, saprolitic, moist
- (C) WEATHERED ROCK MICA SCHIST
- (D) RESIDUAL Gray, very dense, silty SAND, some rock fragments, saprolitic, moist

L 11+00
10+84

Existing Ground

DRI4 11+00

DRY
08/19

WEATHERED ROCK MICA SCHIST

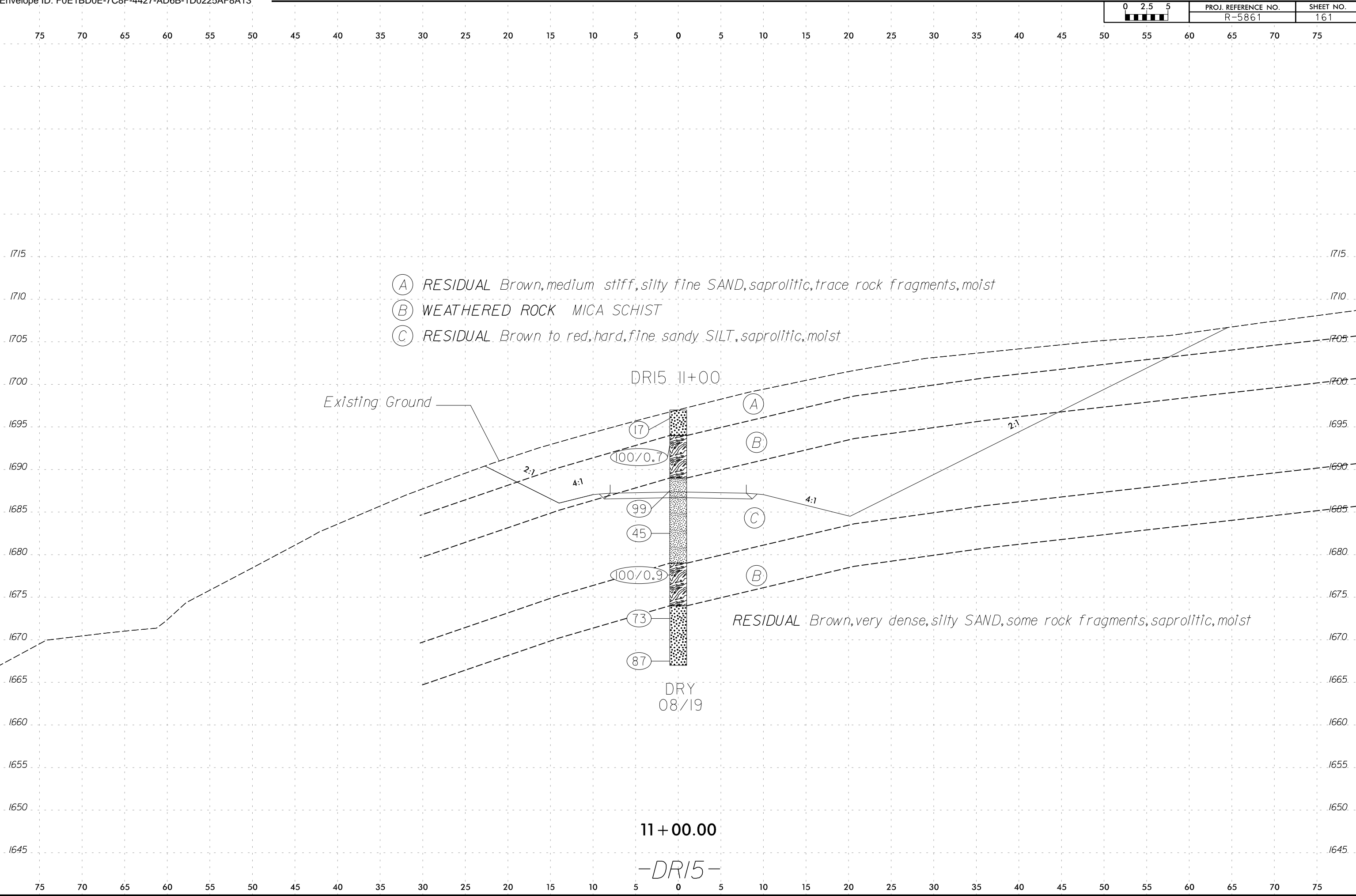
DRY
08/19

11 + 00.00

-DRI4-

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- (A) RESIDUAL Brown, medium stiff, silty fine SAND, saprolitic, trace rock fragments, moist
- (B) WEATHERED ROCK MICA SCHIST
- (C) RESIDUAL Brown to red, hard, fine sandy SILT, saprolitic, moist

RESIDUAL Brown, very dense, silty SAND, some rock fragments, saprolitic, moist

DR15 11+00

DRY
08/19

11 + 00.00

—DR15—

Existing Ground

2:1

4:1

4:1

2:1

(17)

(100/0.7)

(99)

(45)

(100/0.9)

(73)

(87)

(A)

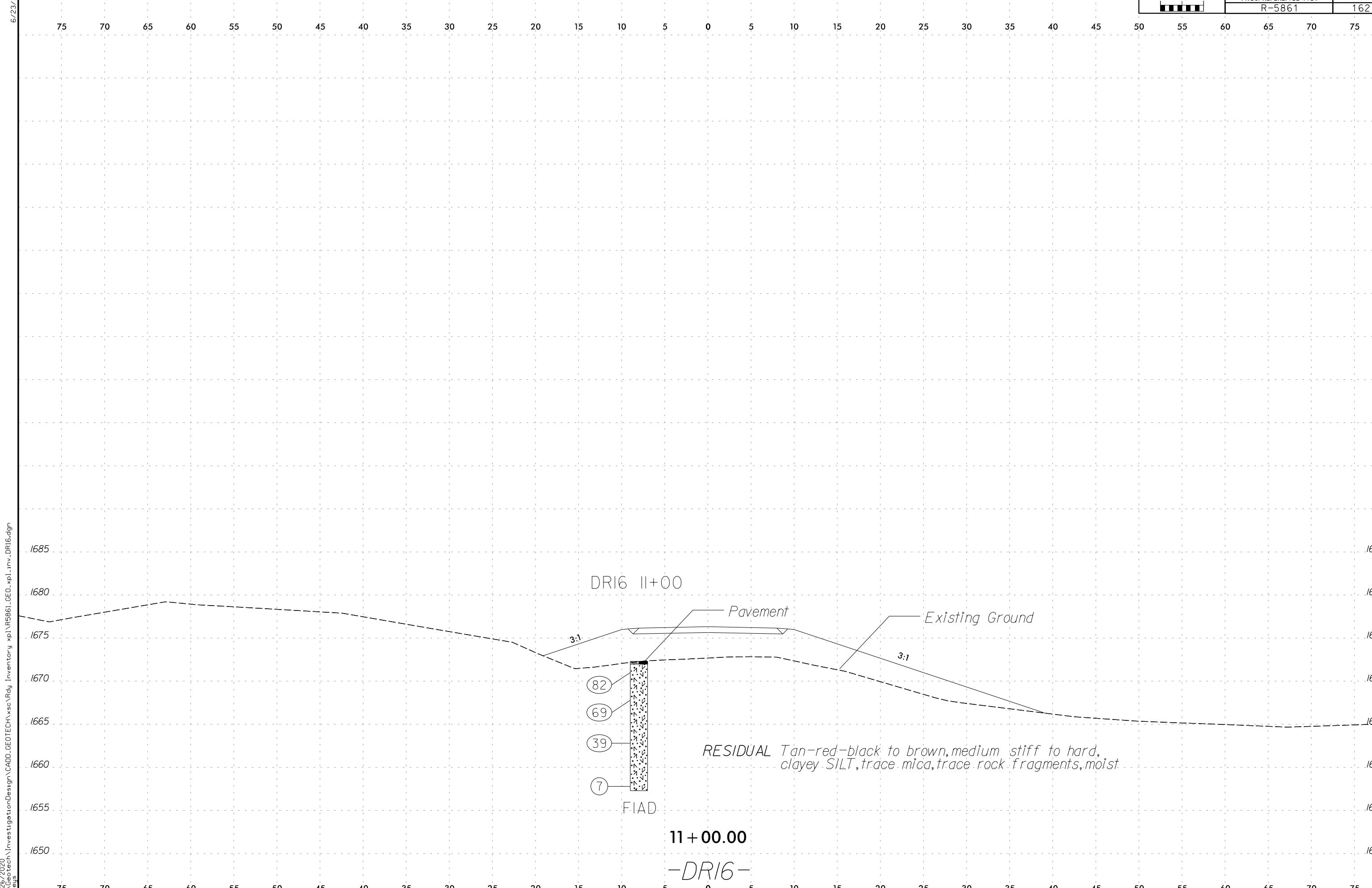
(B)

(C)

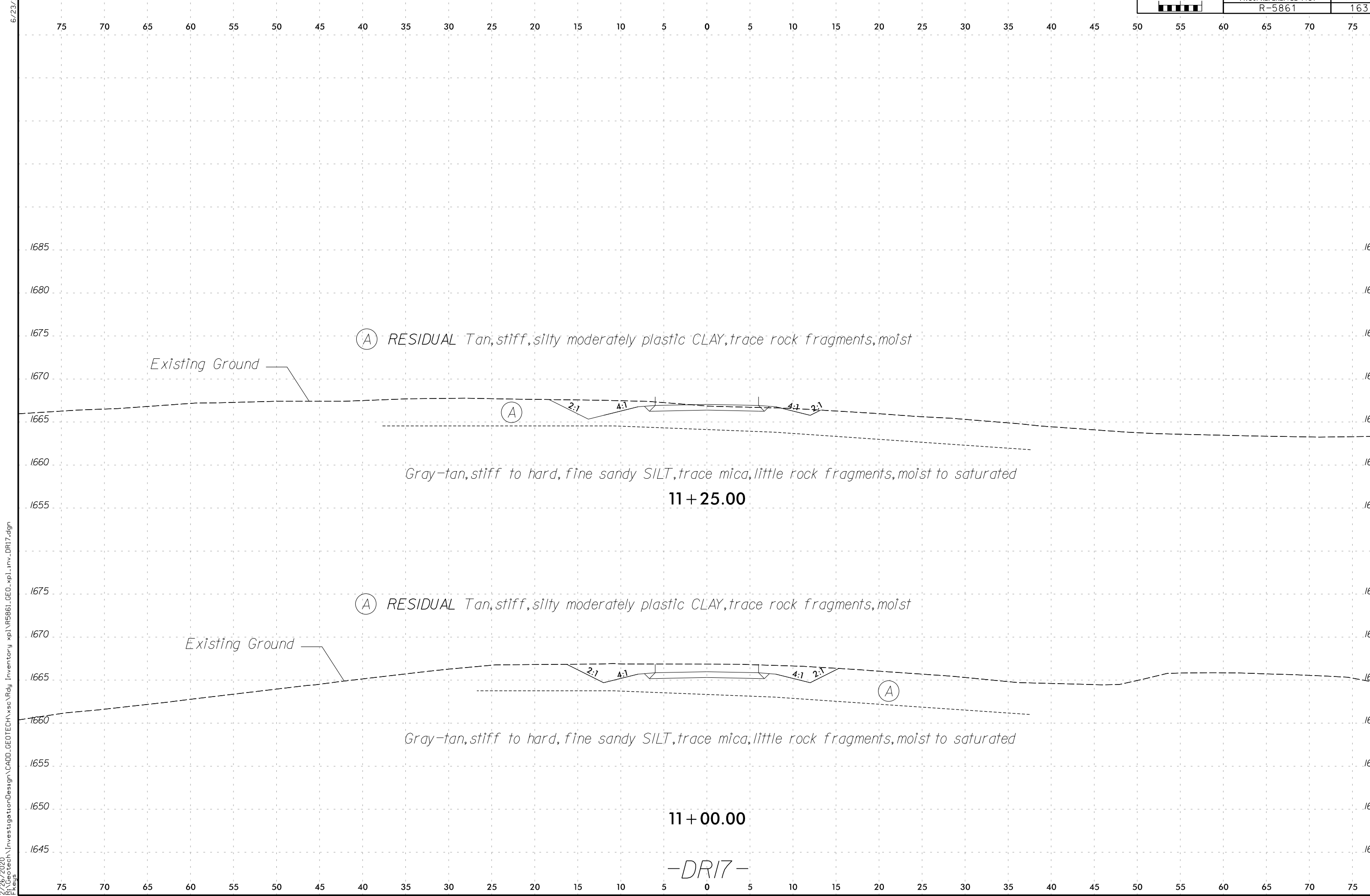
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1715 1710 1705 1700 1695 1690 1685 1680 1675 1670 1665 1660 1655 1650 1645



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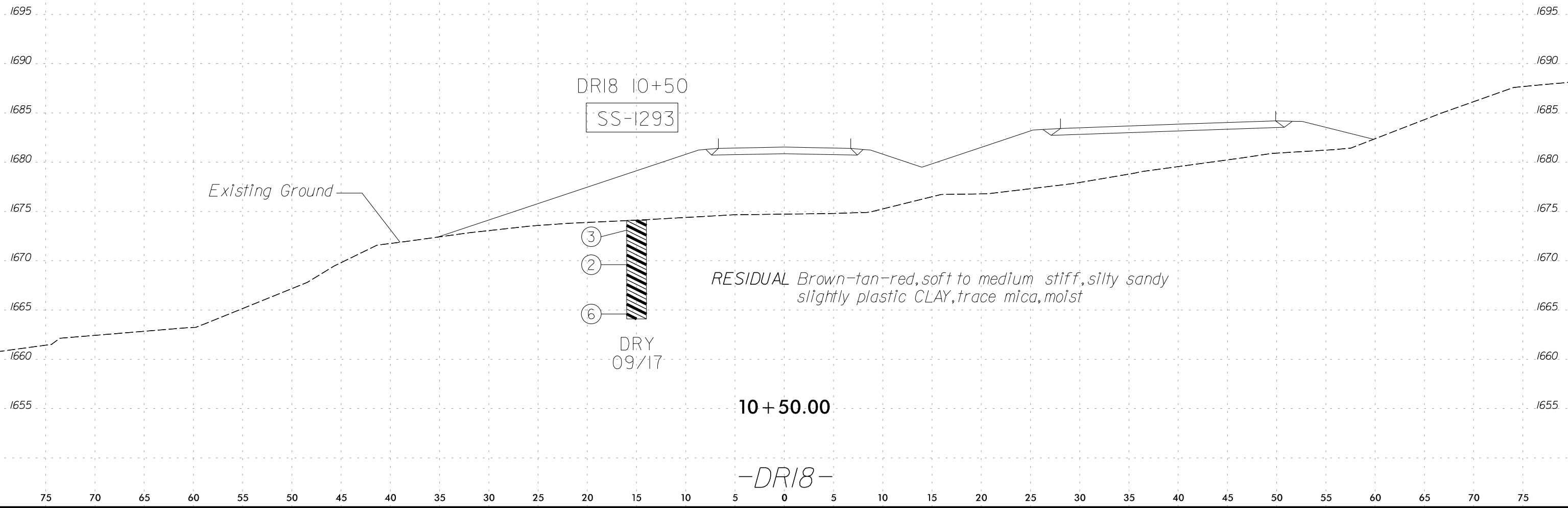


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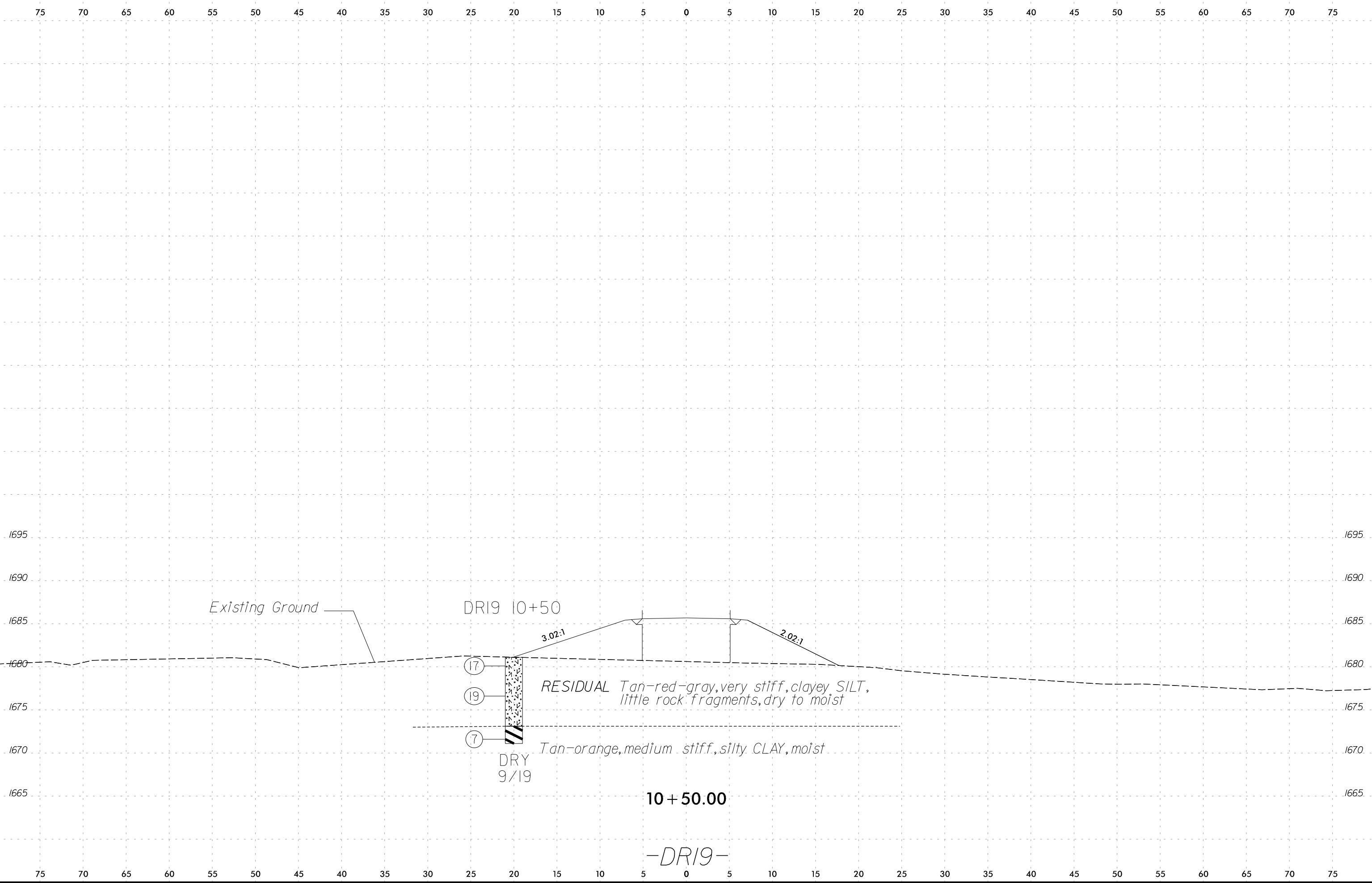
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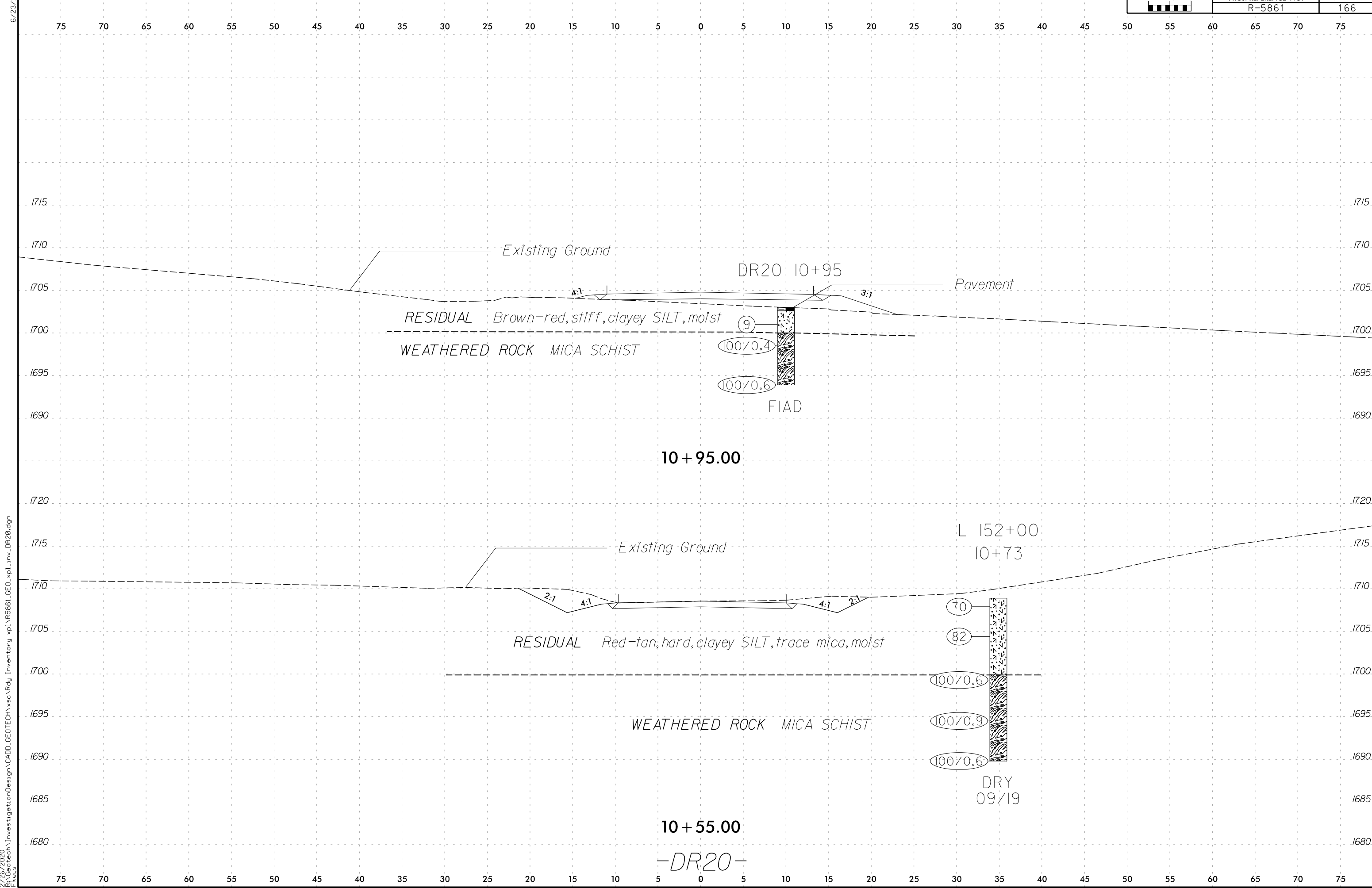
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1293	10+50	15' LT	3.5-5.0	A-6 (3)	40	11	22	12	32	34	69	57	47.4	24.6	-



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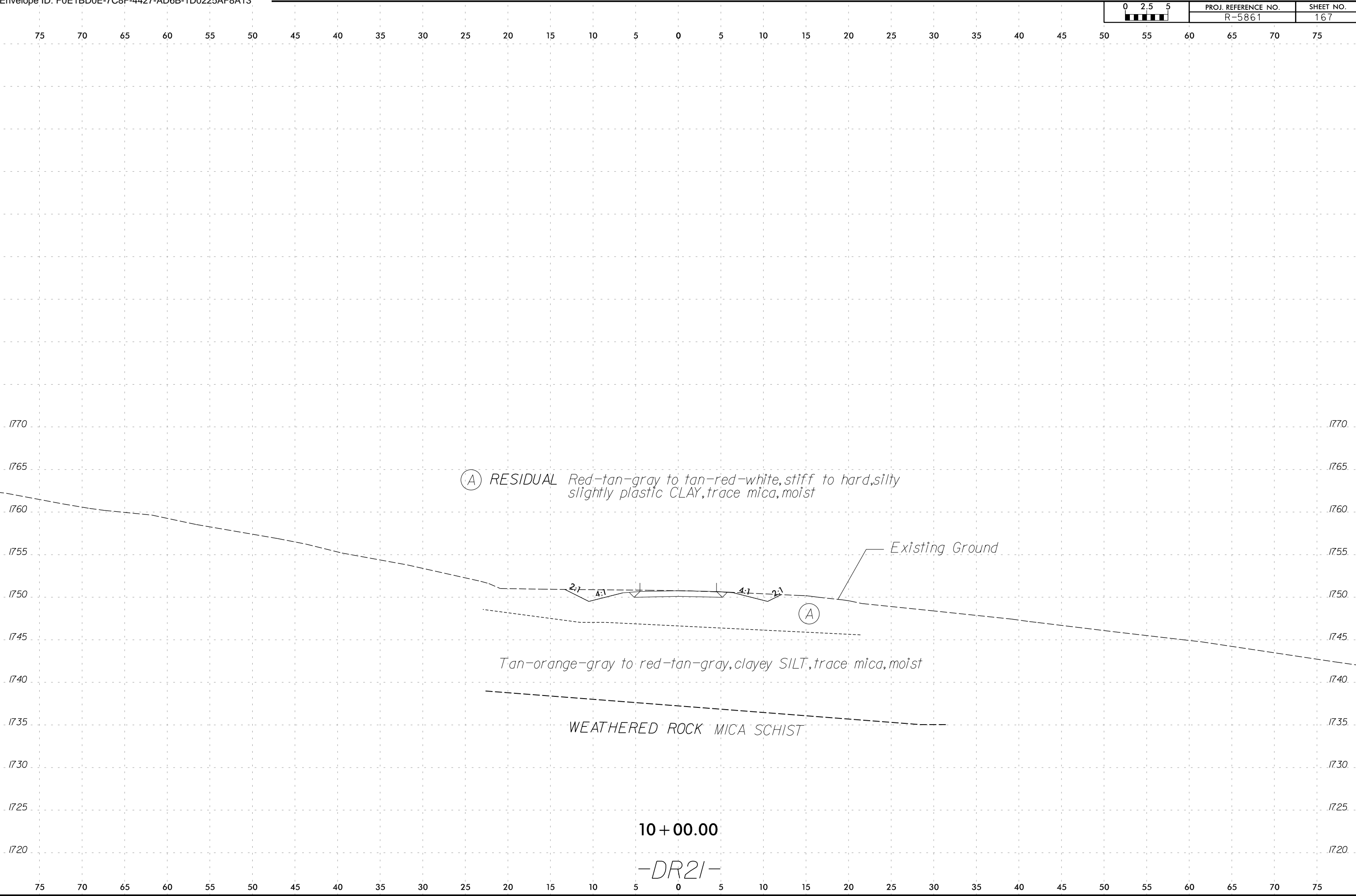
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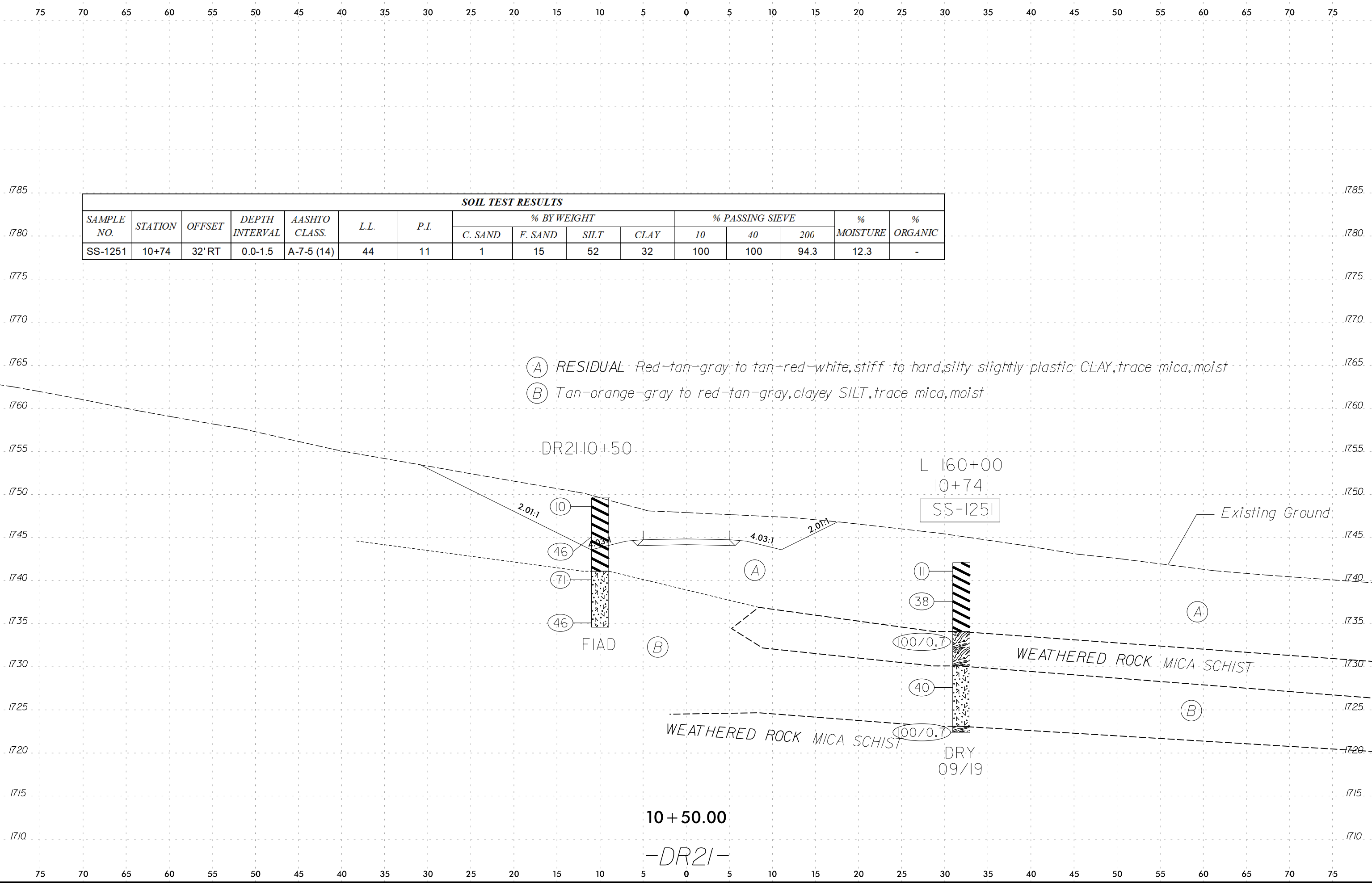




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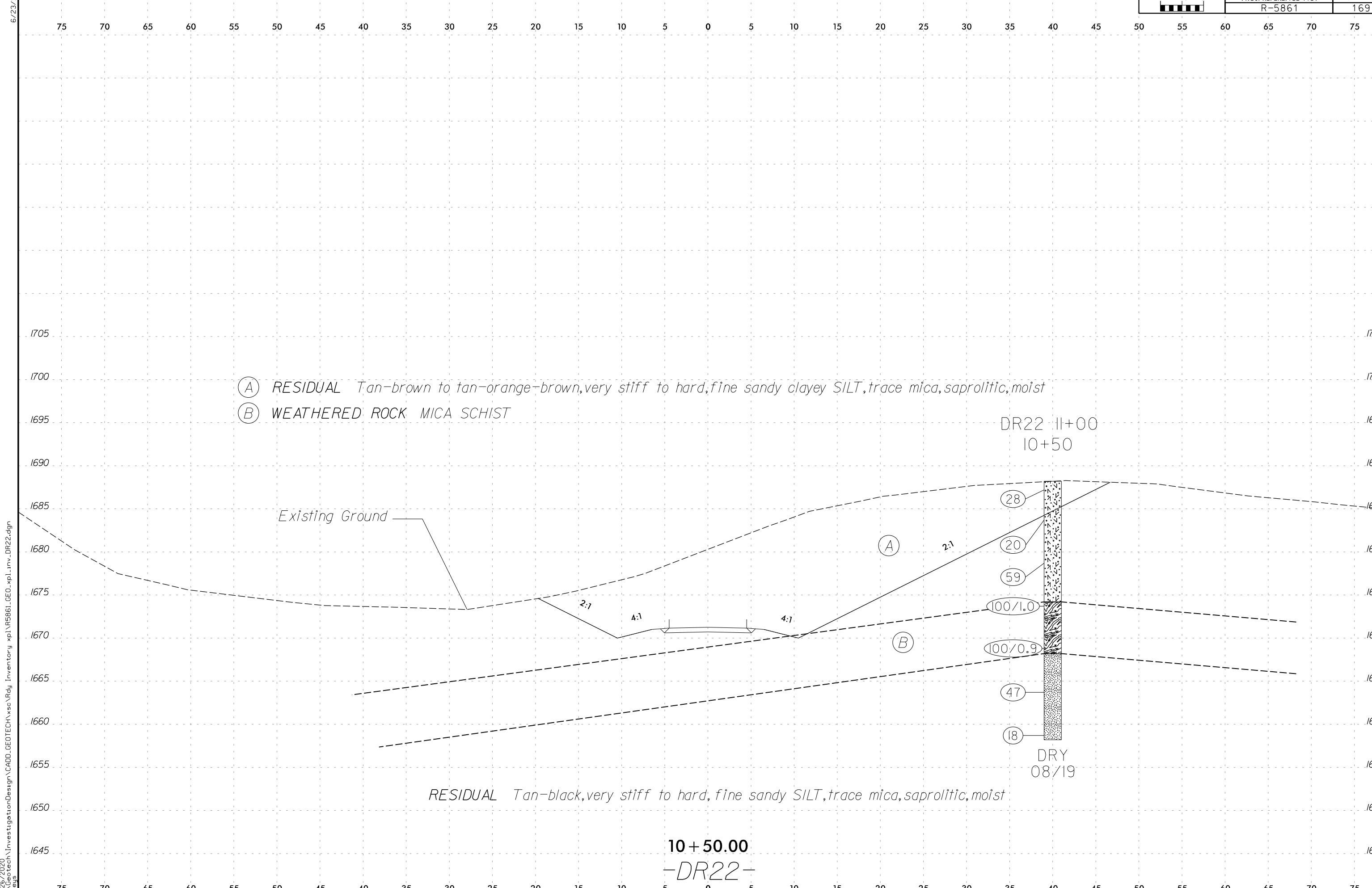




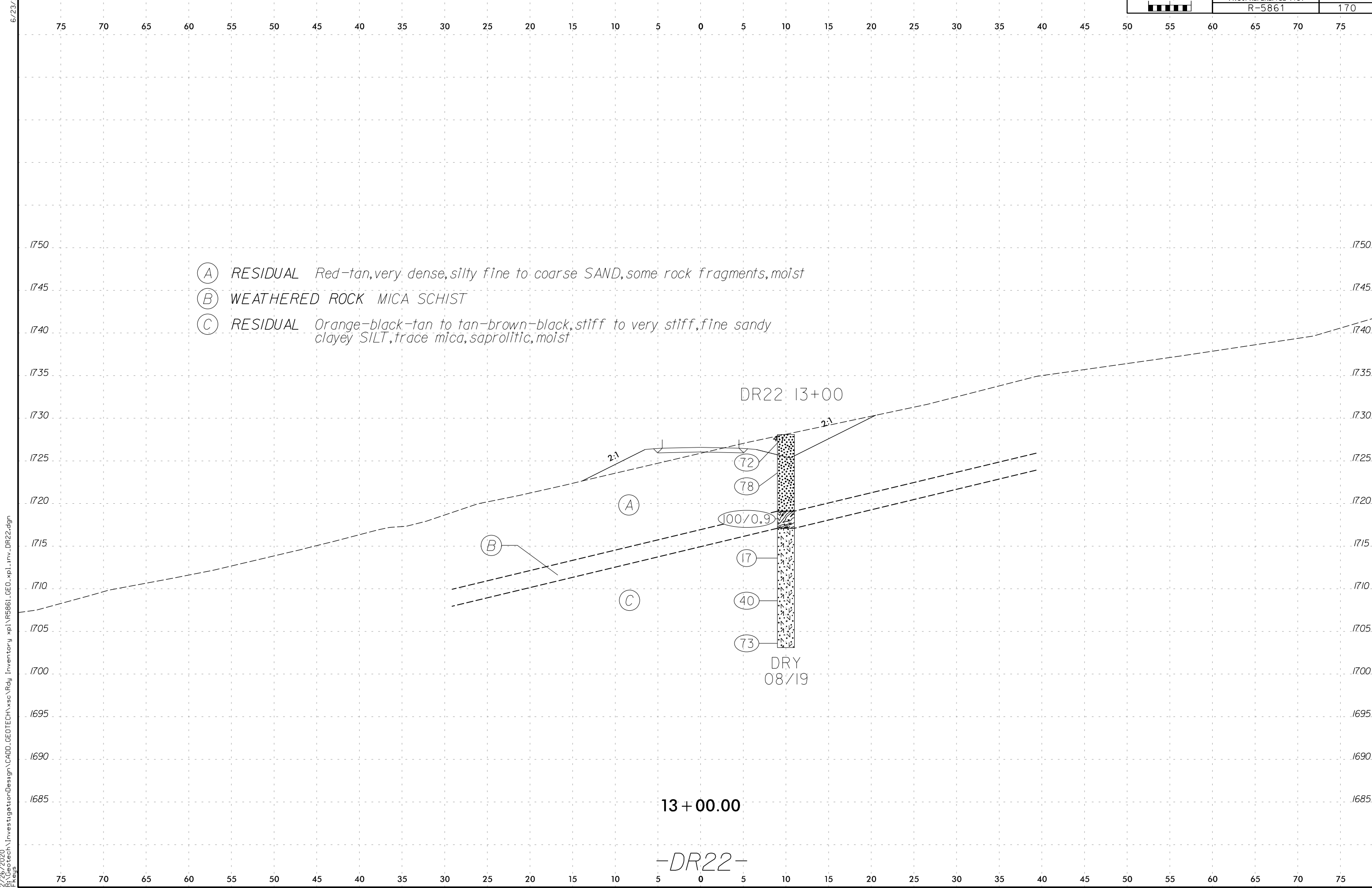
SOIL TEST RESULTS															
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							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1251	10+74	32' RT	0.0-1.5	A-7-5 (14)	44	11	1	15	52	32	100	100	94.3	12.3	-

- (A) RESIDUAL Red-tan-gray to tan-red-white, stiff to hard, silty slightly plastic CLAY, trace mica, moist
- (B) Tan-orange-gray to red-tan-gray, clayey SILT, trace mica, moist

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Pk



- (A) RESIDUAL Red-tan, very dense, silty fine to coarse SAND, some rock fragments, moist
- (B) WEATHERED ROCK MICA SCHIST
- (C) RESIDUAL Orange-black-tan to tan-brown-black, stiff to very stiff, fine sandy clayey SILT, trace mica, saprolitic, moist

DR22 13+00

2:1

2:1

72

78

100/0.9

17

40

73

DRY
08/19

(A)

(B)

(C)

13 + 00.00

-DR22-

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STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	R-5861	1	171

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

ROADWAY
SUBSURFACE INVESTIGATION
APPENDICES

REFERENCE: R-5861

PROJECT: 47427



P: (919) 878-9560
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GEOTECHNICAL BORING REPORT

BORE LOG

WBS 47427.1.1		TIP R-5861		COUNTY CHEROKEE		GEOLOGIST Mize, J.										
SITE DESCRIPTION Widening US 19/129 from the Georgia State Line to US 64/74							GROUND WTR (ft)									
BORING NO. L 94+72 AP		STATION 94+72		OFFSET 90 ft LT		ALIGNMENT L	0 HR. Dry									
COLLAR ELEV. 1,722.2 ft		TOTAL DEPTH 17.7 ft		NORTHING 496,083		EASTING 478,197	24 HR. Dry									
DRILL RIG/HAMMER EFF./DATE SME267 DIEDRICH D-50 74% 10/20/2017				DRILL METHOD H.S. Augers		HAMMER TYPE Automatic										
DRILLER Blizzard, B.		START DATE 08/13/19		COMP. DATE 08/13/19		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft)	DEPTH (ft)		
1725														1,722.2	0.0	GROUND SURFACE
1720																RESIDUAL Brown, sandy SILT (A-4)
1715																
1710	1,711.0	11.2												1,713.2	9.0	WEATHERED ROCK MICA SCHIST
	1,708.7	13.5	100/0.4													
1705	1,704.5	17.7	44	40	60/0.2									1,704.5	17.7	Boring Terminated BY AUGER REFUSAL at Elevation 1,704.5 ft on Crystalline Rock: MICA SCHIST

NCDOT BORE DOUBLE R-5861.GPJ NC_DOT.GDT 2/23/20

**CBR (CALIFORNIA BEARING RATIO)
OF LABORATORY COMPACTED SOIL**



AASHTO T 193

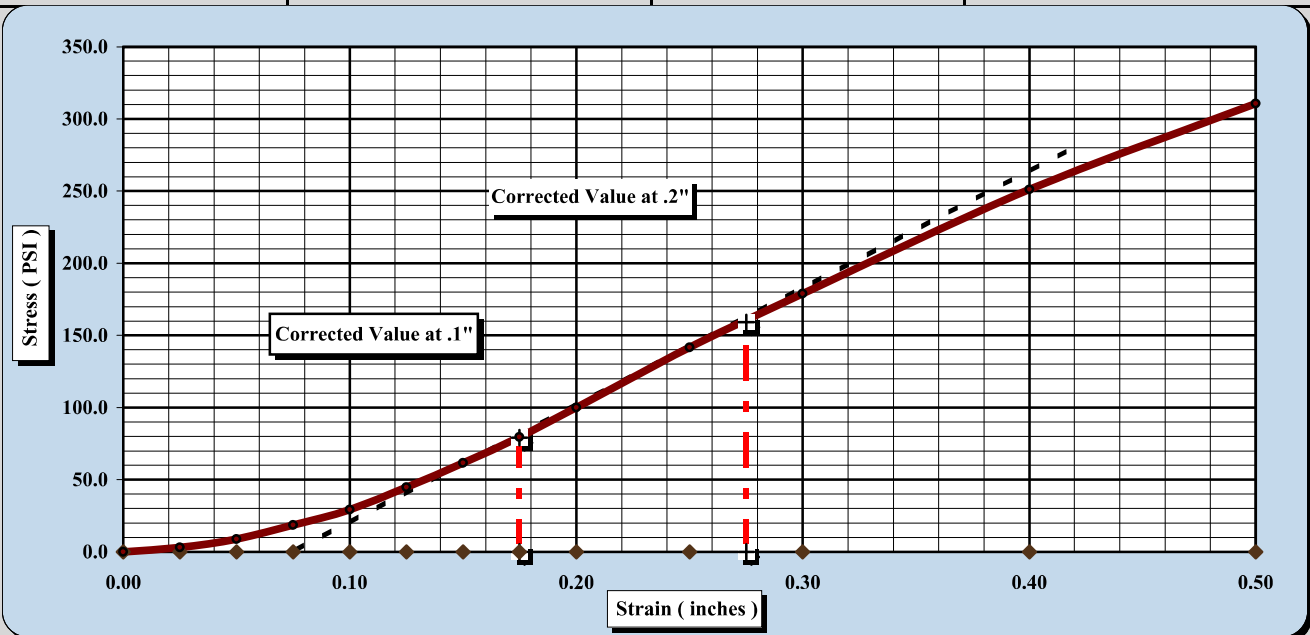
S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

Project #:	1934-19-002	Report Date:	10/16/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s)	10/10 - 10/16/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	L 90+00 AP	Sample #:	S-225
Station #:	90+00	Sample Date:	N/A
	Offset: N/A	Depth (ft):	1.0-8.5

Sample Description: Tan Coarse to Fine Sandy Silty CLAY (A-4) (0)

AASHTO T99 Method A	Maximum Dry Density:	115.0 PCF	Optimum Moisture Content:	14.5%
	Compaction Test performed on grading complying with CBR spec.		% Retained on the 3/4" sieve:	0.0%

Uncorrected CBR Values		Corrected CBR Values	
CBR at 0.1 in.	2.9	CBR at 0.1 in.	7.9
CBR at 0.2 in.	6.7	CBR at 0.2 in.	10.6



CBR Sample Preparation:

The entire gradation was used and compacted in a 6" CBR mold in accordance with AASHTO T 193, Section 5.1.1

Before Soaking		After Soaking	
Compactive Effort (Blows per Layer)	56	Final Dry Density (PCF)	114.4
Initial Dry Density (PCF)	115.0	Average Final Moisture Content	16.0%
Moisture Content of the Compacted Specimen	14.5%	Moisture Content (top 1" after soaking)	17.8%
Percent Compaction	100.0%	Percent Swell	0.7%

Soak Time:	96 hrs.	Surcharge Weight	10.0	Surcharge Wt. per sq. Ft.	50.9
Liquid Limit	29	Plastic Index	5		

Notes/Deviations/References:

Test specimen compacted to 100% at optimum moisture.

Mal Krajan, ET
Technical Responsibility

Signature

Laboratory Manager
Position

10/16/2019
Date

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MOISTURE - DENSITY REPORT



SHEET 172

Quality Assurance

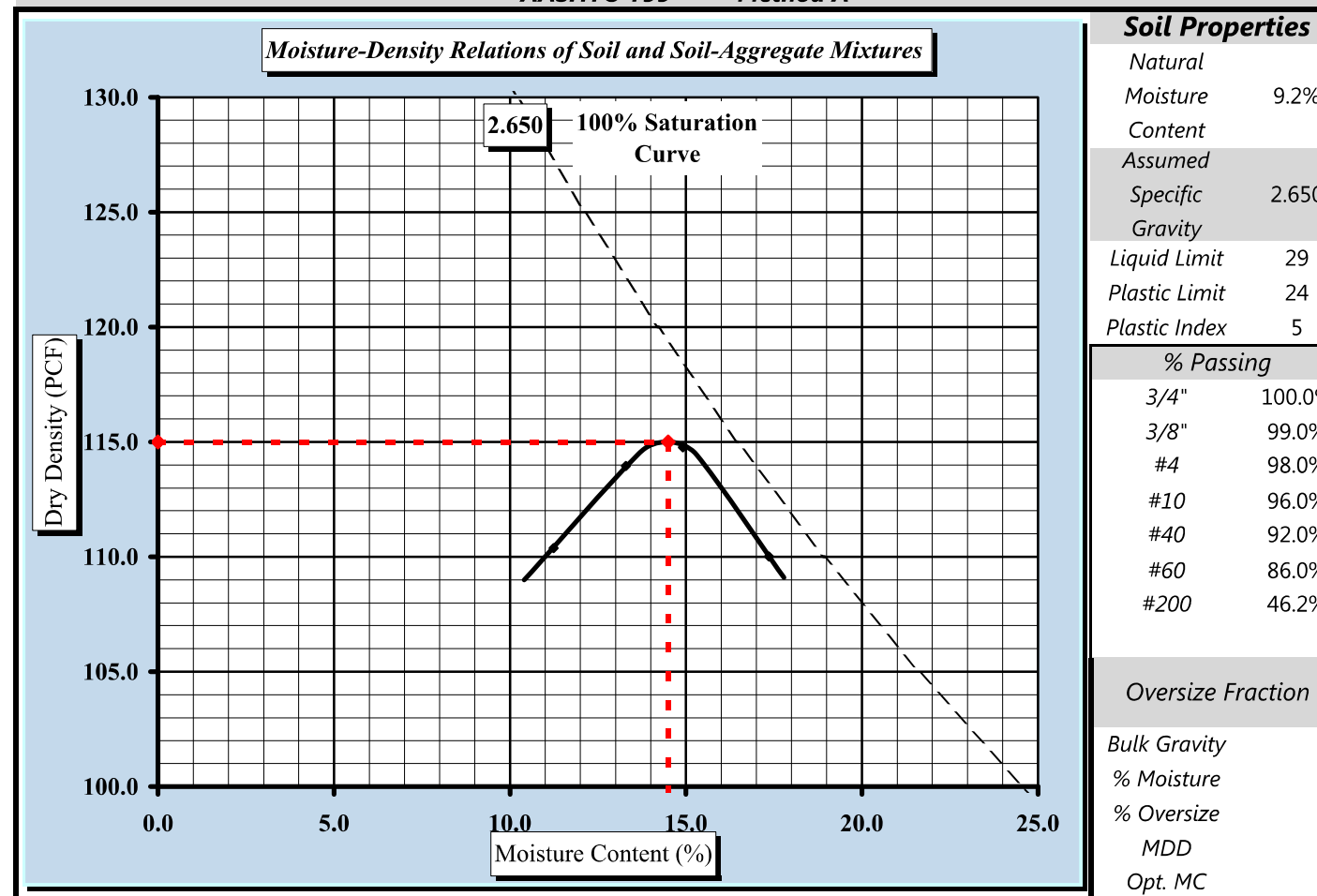
S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

S&ME Project #:	1943-19-002	Report Date:	10/11/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s):	10/4 - 10/11/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	L 900+00 AP	Sample #:	S-225
Satation:	90+00	Sample Date:	N/A
	Offset: N/A	Depth (ft):	1.0 - 8.5 ft.

Sample Description: Tan Coarse to Fine Sandy Silty CLAY (A-4) (0)

Maximum Dry Density	115.0 PCF.	Optimum Moisture Content	14.5%
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AASHTO T99 - - Method A



Moisture-Density Curve Displayed:	Fine Fraction <input checked="" type="checkbox"/>	Corrected for Oversize Fraction (ASTM D 4718)	<input type="checkbox"/>
Sieve Size used to separate the Oversize Fraction:	#4 Sieve <input checked="" type="checkbox"/>	3/8 inch Sieve	<input type="checkbox"/>
Mechanical Rammer	<input type="checkbox"/>	Manual Rammer	<input checked="" type="checkbox"/>
		Moist Preparation	<input type="checkbox"/>
		Dry Preparation	<input checked="" type="checkbox"/>

References / Comments / Deviations:

AASHTO T265: Laboratory Determination of Moisture Content of Soils

AASHTO T 99: Moisture-Density Relations of Soil Using a 5.5 Lb. Rammer and a 12" Drop

Mal Krajan, ET
Technical Responsibility

Signature

Laboratory Manager
Position

10/11/2019
Date

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CBR (CALIFORNIA BEARING RATIO) OF LABORATORY COMPACTED SOIL



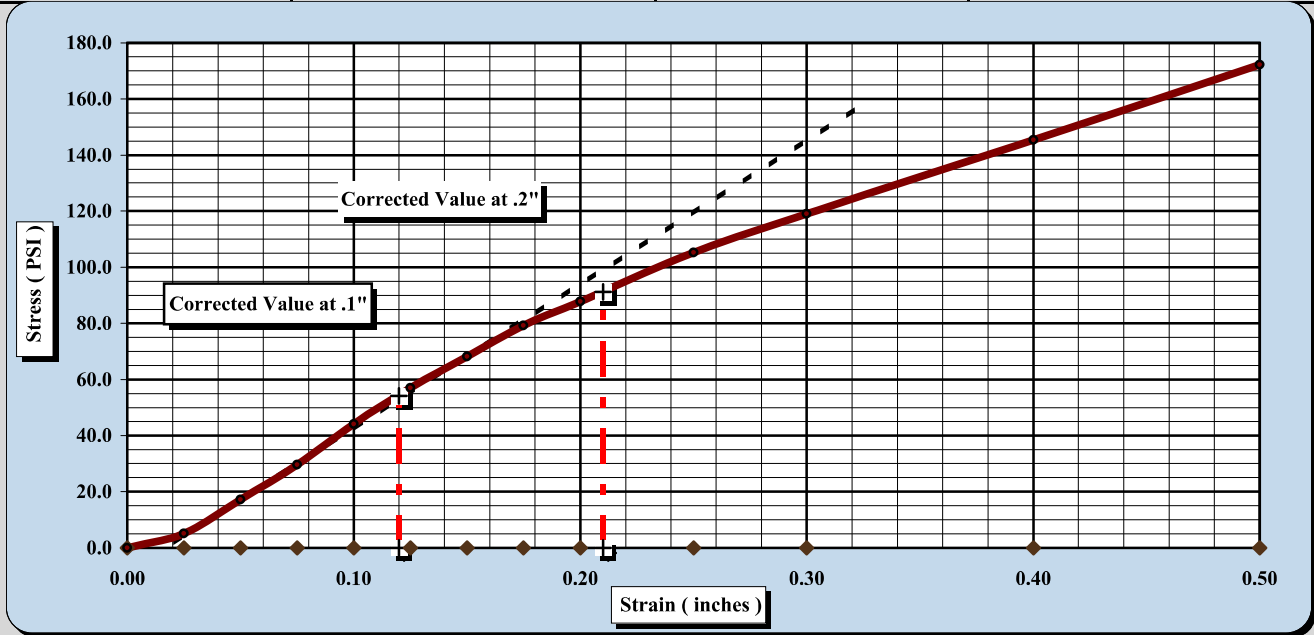
AASHTO T 193

S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

Project #:	1934-19-002	Report Date:	10/16/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s)	10/10 - 10/16/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	LDET6 23+65.75	Sample #:	S-1041
Station #:	23+65.75	Offset:	N/A
		Depth (ft):	0.0 - 8.5 ft.

Sample Description: Tan Coarse to Fine Sandy Clayey SILT (A-4) (8)
 AASHTO T99 Method A Maximum Dry Density: 107.1 PCF Optimum Moisture Content: 17.9%
 Compaction Test performed on grading complying with CBR spec. % Retained on the 3/4" sieve: 0.0%

Uncorrected CBR Values		Corrected CBR Values	
CBR at 0.1 in.	4.4	CBR at 0.1 in.	5.4
CBR at 0.2 in.	5.9	CBR at 0.2 in.	6.1



CBR Sample Preparation: The entire gradation was used and compacted in a 6" CBR mold in accordance with AASHTO T 193, Section 5.1.1

Before Soaking		After Soaking	
Compactive Effort (Blows per Layer)	56	Final Dry Density (PCF)	105.4
Initial Dry Density (PCF)	106.8	Average Final Moisture Content	19.9%
Moisture Content of the Compacted Specimen	17.8%	Moisture Content (top 1" after soaking)	22.3%
Percent Compaction	99.7%	Percent Swell	1.5%

Soak Time: 96 hrs. Surcharge Weight 10.0 Surcharge Wt. per sq. Ft. 50.9
 Liquid Limit 39 Plastic Index 10

Notes/Deviations/References:
 Test specimen compacted to 100% at optimum moisture.

Mal Krajan, ET Technical Responsibility Signature Position Laboratory Manager Date 10/16/2019

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MOISTURE - DENSITY REPORT



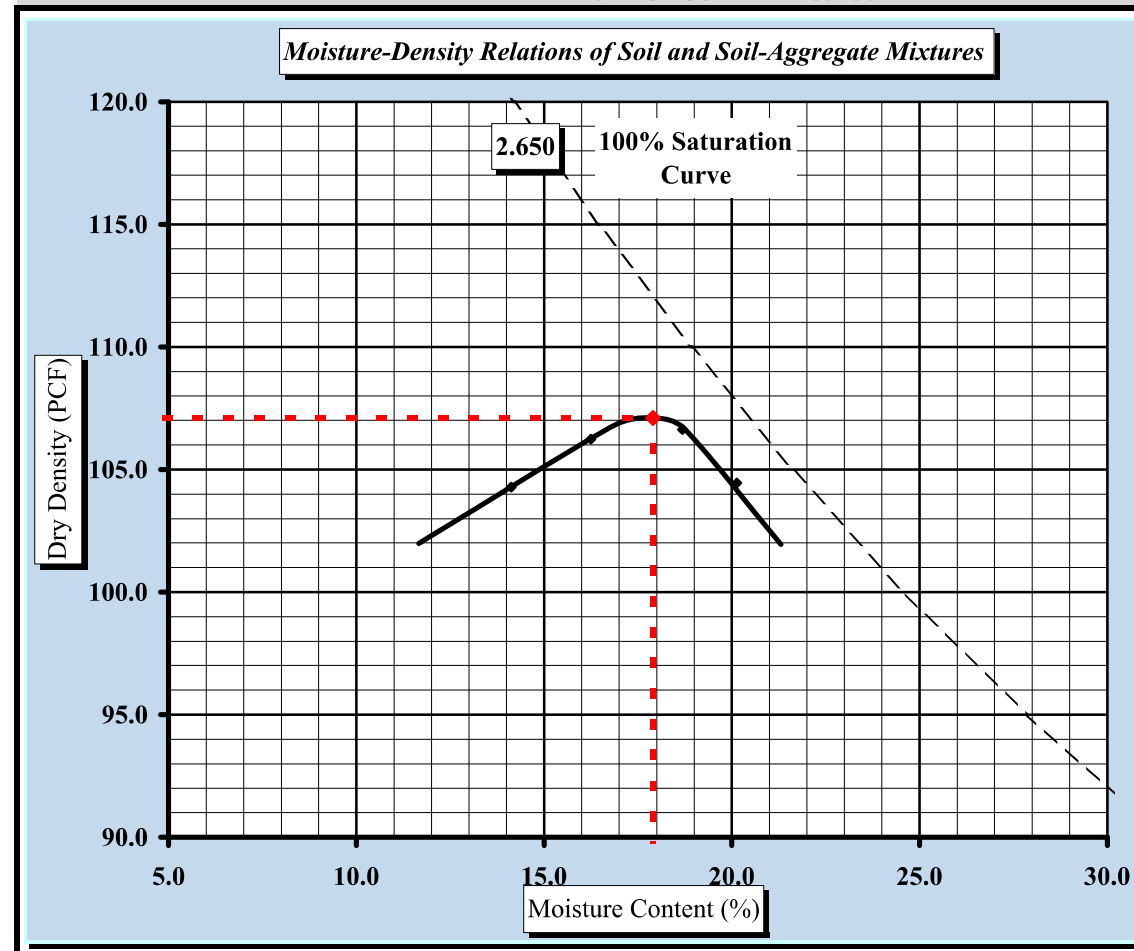
SHEET 174

Quality Assurance S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

S&ME Project #:	1943-19-022	Report Date:	10/11/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s):	10/4 - 10/11/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	LDET6 23+65.75	Sample #:	S-1041
Station:	23+65.75	Offset:	N/A
		Depth (ft):	0.0 - 8.5 ft.

Sample Description: Tan Coarse to Fine Sandy Clayey SILT (A-4) (8)
 Maximum Dry Density 107.1 PCF. Optimum Moisture Content 17.9%

AASHTO T99 - - Method A



Soil Properties	
Natural Moisture Content	1.3%
Assumed Specific Gravity	2.650
Liquid Limit	39
Plastic Limit	29
Plastic Index	10
% Passing	
3/4"	100.0%
3/8"	100.0%
#4	100.0%
#10	99.0%
#40	97.0%
#60	96.0%
#200	78.3%
Oversize Fraction	
Bulk Gravity	
% Moisture	
% Oversize	
MDD	
Opt. MC	

Moisture-Density Curve Displayed: Fine Fraction Corrected for Oversize Fraction (ASTM D 4718)
 Sieve Size used to separate the Oversize Fraction: #4 Sieve 3/8 inch Sieve 3/4 inch Sieve
 Mechanical Rammer Manual Rammer Moist Preparation Dry Preparation

References / Comments / Deviations:
 AASHTO T265: Laboratory Determination of Moisture Content of Soils
 AASHTO T 99: Moisture-Density Relations of Soil Using a 5.5 Lb. Rammer and a 12" Drop

Mal Krajan, ET Technical Responsibility Signature Position Laboratory Manager Date 10/11/2019

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**CBR (CALIFORNIA BEARING RATIO)
OF LABORATORY COMPACTED SOIL**



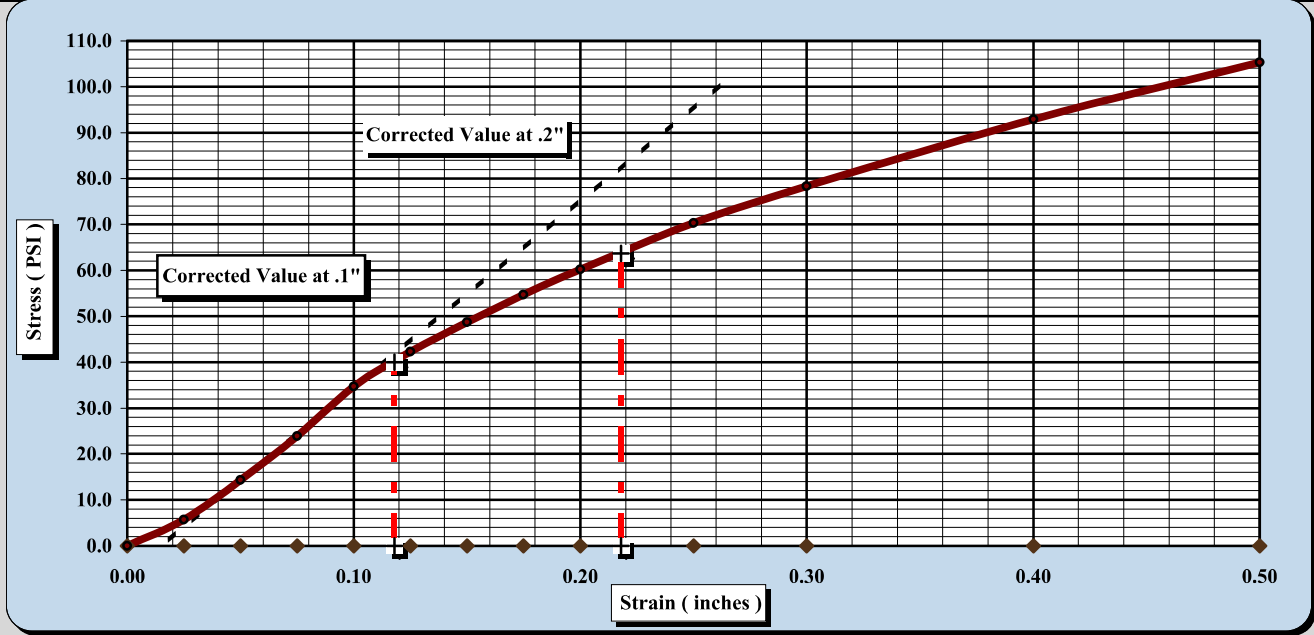
AASHTO T 193

S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

Project #:	1934-19-002	Report Date:	10/16/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s)	10/10 - 10/16/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	L 172+00	Sample #:	S-1159
Station #:	172+00	Offset:	N/A
		Sample Date:	N/A
		Depth (ft):	0.0 - 8.5 ft.

Sample Description: Red Coarse to Fine Sandy Silty CLAY (A-7-5) (23)
 AASHTO T99 Method A Maximum Dry Density: 101.0 PCF Optimum Moisture Content: 20.8%
 Compaction Test performed on grading complying with CBR spec. % Retained on the 3/4" sieve: 0.0%

Uncorrected CBR Values		Corrected CBR Values	
CBR at 0.1 in.	3.5	CBR at 0.1 in.	4.0
CBR at 0.2 in.	4.0	CBR at 0.2 in.	4.2



CBR Sample Preparation: The entire gradation was used and compacted in a 6" CBR mold in accordance with AASHTO T 193, Section 5.1.1

Before Soaking		After Soaking	
Compactive Effort (Blows per Layer)	56	Final Dry Density (PCF)	99.4
Initial Dry Density (PCF)	100.8	Average Final Moisture Content	22.5%
Moisture Content of the Compacted Specimen	20.9%	Moisture Content (top 1" after soaking)	24.8%
Percent Compaction	99.8%	Percent Swell	1.6%

Soak Time: 96 hrs. Surcharge Weight 10.0 Surcharge Wt. per sq. Ft. 50.9
 Liquid Limit 64 Plastic Index 31

Notes/Deviations/References:
 Test specimen compacted to 100% at optimum moisture.

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MOISTURE - DENSITY REPORT



SHEET 175

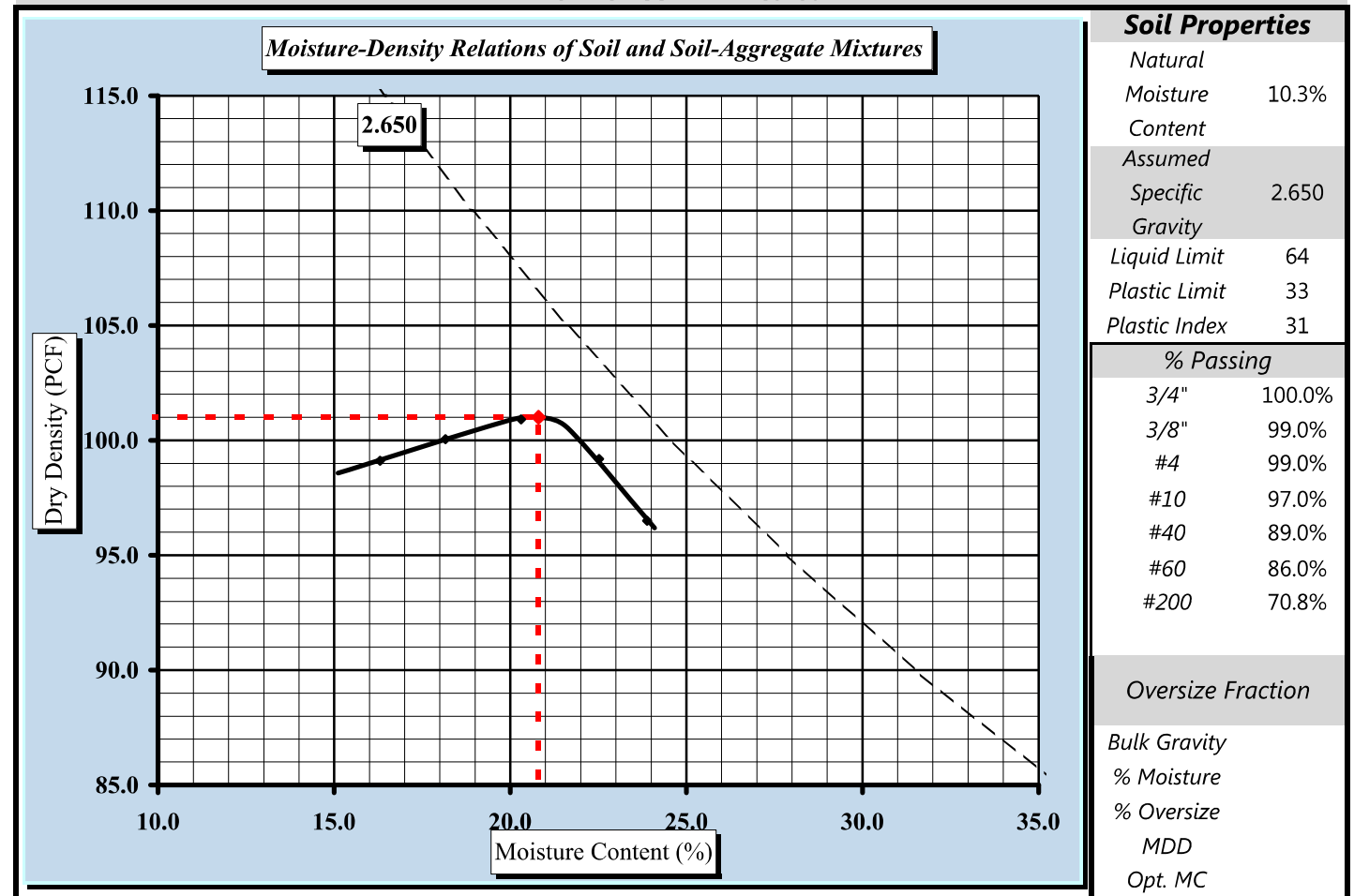
Quality Assurance

S&ME, Inc. Raleigh: 3201 Spring Forest Road, Raleigh, NC 27616

S&ME Project #:	1943-19-002	Report Date:	10/11/2019
Project Name:	R-5861 US19/129 from Georgia State Line to US64/74	Test Date(s):	10/4 - 10/11/19
Client Name:	RK&K		
Client Address:	Raleigh, NC		
Boring #:	L 172+00	Sample #:	S-1159
Station:	172+00	Offset:	N/A
		Sample Date:	N/A
		Depth (ft):	0.0 - 8.5 ft.

Sample Description: Red Coarse to Fine Sandy Silty CLAY (A-7-5) (23)
 Maximum Dry Density 101.0 PCF. Optimum Moisture Content 20.8%

AASHTO T99 - - Method A



Moisture-Density Curve Displayed: Fine Fraction Corrected for Oversize Fraction (ASTM D 4718)
 Sieve Size used to separate the Oversize Fraction: #4 Sieve 3/8 inch Sieve 3/4 inch Sieve
 Mechanical Rammer Manual Rammer Moist Preparation Dry Preparation

References / Comments / Deviations:
 AASHTO T265: Laboratory Determination of Moisture Content of Soils
 AASHTO T 99: Moisture-Density Relations of Soil Using a 5.5 Lb. Rammer and a 12" Drop

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