COMPUTED BY:	CJP	DATE:	5/25/2022
CHECKED BY:	RBH	DATE:	12/5/2022

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS

PROJECT REFERENCE NO.SHEET NO.W-570/B3D-2

Note: Invert Elevations indicated are for Bid Purposes only and shall not be used for project construction stakeout. See "Standard Specifications for Roads and Structures, Section 300-5."

	, ENDWALLS,	ETC. (FOR	PIPES	1 (Q) 99 (Q)	UNDER
(()) 🍽					
V					

	_													`	<u> </u>	1 1.1.		9 11/11/1	1 1 1 1	V V A 2		109 111	<u> </u>	<u> </u>		11 1	<u> </u>			<u> </u>	1 10 1		,				
LINE & STATION	OFFSET	STRUCTURE NO.			ELEV	ERT ELEVATION	JM REQUIRED SLO	SI RCP, CSP	DE DRAIN , CAAP, H PVC)		C.S. or PIPE		R.C. P CLASS		R.C. PIPE CLASS IV	STD. (STD. (UN NC	NALLS 838.01 OR 838.11 LESS OTED RWISE)	QUANTITIES FOR DRAINAGE	STRUCTURI	*TOTAL L.F. FOR PAY QUANTITY SHALL BE COL. 'A' + (1.3 X COL.'B')	,	FRAME, GRATES, AND HOOD STANDARD 840.03	SEE DETAIL SHEET NO. 2C-3 FOR PLACING A TBDI IN CONCRETE ISLANDS	0.15	D. 840.16 OR 840.26		S STD. 840.22	WO GRATES STD. 840.24 FLAT GRATES. STD. 840.29		TD. 840.54		AIL SHEET NO. 2C-4	SIZE	, C.Y. STD. 840.71	.Y. STD. 840.72		ABBREVIATIONS C.B. CATCH BASIN N.D.I. NARROW DROP INLET D.I. DROP INLET G.D.I. GRATED DROP INLET G.D.I.(N.S.) (NARROW SLOT) J.B. JUNCTION BOX
SIZE				3	≧	2	WINIW 1	15" 18"		۳,	15" 18	8" 15"	18" 24'	" 30" 3	6" 15" 18'	CU.	YARDS		ļ	FT.	D. 84			. 840	STI 0.17	0.18	0FL 0GR	WO F	AME	R S		DET	ა ა	LUG,	3" C.		M.H. MANHOLE
THICKNESS OR GAUGE		FROM	10				V %			DO NOT USE CAAP OO NOT USE HDPE, P						R.C.P.	C.S.P.	PER EACH (0' THRU 5.0	.0' THRU 10.0'	.0' AND ABOVE Φ	B. STD. 840.01 OR ST	TYPE OF GRATE	SOP INLET	D.I. STD. 840.14 OR STD	FRAME AND I TYPE "A"	. TYPE "B" STD. 84 . TYPE "D" STD. 84	G.D.I. FRAME WITH TW G.D.I. FRAME WITH TW	G.D.I. (N.S.) FRAME WITH G.D.I. (N.S.) FR. WITH TWC J.B. STD. 840.31 OR 840.32	3JB STD. 840.34 B.D.I. STD. 840.36 TEEL GRATE AND FR.		51 CB 51 DI	CONV DI TO JBMH SEE FLOWABLE FILL (CY)	.S. PIPE ELBOWS NO	ONC. & BRICK PIPE P	ONC. COLLARS CL. "I	PE REMOVAL LIN. FT	T.B.D.I. TRAFFIC BEARING DROP INLET T.B.J.B. TRAFFIC BEARING JUNCTION BOX
	+ -			_	_	_	_		-	-					+		+	==	2.0	10	ပ	E F G	DR S		<u> </u>	G.D.	<u> ග්</u>	<u>ල් ල් දු</u>		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	<u> </u>	<u> </u>	-)	03	■	REMARKS
SHEET 8	04 1-	4504		7				+			++	_	++		+	1		1					1 1	\dashv		+		+ + +		1	+	\dashv				1	
- L- 162+45.02 - L- 162+45.02	-21 LT	1501 1501	1502		3.6	73.1 0	0.1%	+				52	2			 	-	1			\vdash		1 1	+		+	+	+ + +	1 1	1	++	\dashv				+	
- L- 163+00.00	15 RT		76		J.U	70.1	J. 1 /0	+				1 3,		+++		†	+	1						+		1		1 1			+	\dashv				1	
- L- 163+00.00	RT		1502		3.2	72.9 0	0.5%					88	8					İ											<u> </u>			_				1_	
- L- 162+10.90	18 RT	1502	77	.3														1					1						1	1							
- L- 162+10.90	RT	1502	1506	7:	2.9	69.5 0	0.5%					270	6																								
- L- 165+80.97	0 CL	1	73															1	5.0							1		1									
- L- 165+77.42	7 RT	—	78			60.4	2 00/	+			+		+	1		-		1	5.0	4.8				+	1	+		1 1			\dashv	\dashv			-		SPECIAL DETAIL, SEE DETAIL SHEET 2C-2
- L- 165+77.42	RT	1504 1505	 	_	3.8	63.4 3	3.9%						++	8	+ +						\vdash		1			++				1 1	-						+
- L- 165+80.97	U CL	1505	73	.4									++				_									$\dashv \dashv$											
																																					1
	1 1														\bot								1			\perp				\bot \bot							
	+ +												++										+			++											
011557.0	+			_									+		+		-	-					+			+	_			+							
SHEET 9 - L- 173+19.14	-23 LT	1604	84	6	-	-+	\dashv						++		+	1	+	1			\vdash		1	+		++	_			1	\dashv	\dashv			+	+	+
- L- 173+19.14 - L- 173+19.14	-23 L1		1605		0.4	80.1 0	0.5%					1/	1					+ '								++											
- L- 173+19.14 - L- 172+86.51	11 RT		84	_	0.4	00.1	0.570					- 4	4					1					1			++			1	1							
- L- 172+86.51	RT	—	1601	81	0.1	79.1 0	0.4%					96	6					 					1 1			+++				1 1							†
- L- 171+91.00	28 RT		83															1					1						1	1							
- L- 171+91.00	RT	1601	1602	79	9.1	79.1 0	0.4%					10	6																								
- L- 171+90.00	10 RT	1602	82															1					1						1	1							
- L- 171+90.00	RT	1002	1603	79	9.1	79.0 0	0.5%	$\perp \downarrow \perp \downarrow$				28	8			<u> </u>					$\sqcup \!\!\! \perp$					\perp				\bot	$\perp \downarrow \perp$	$\perp \downarrow \downarrow$				1	<u> </u>
- L- 171+60.18	7 RT	1003	82					\dashv								 	-	1 .	5.0	4.3	$\vdash \vdash$			\parallel		+		1		1 1	+	\dashv			_		SPECIAL DETAIL, SEE DETAIL SHEET 2C-5
- L- 173+32.00	28 RT	 	1607		0.7	80.5 0	7 40/	+	\dashv		+	0.0		++	+-	+	+	1	 		$\vdash \vdash$	++-	1	$\dashv \dashv$		++	$\overline{}$	+ + +	1 1	1	++	\dashv			-	+	+
- L- 173+32.00 - L- 174+30.00	13 RT	1000	1007		U.1	00.5	J.4%	+	+			60	<u> </u>		++-	 	-	1			$\vdash \vdash$					1	+			+ + +	++	\dashv				1	
- L- 174+30.00	IS RT			_	1.4	81.3 0	0.4%	+			+	40				†	 	† '			$\vdash \vdash$					-	+			+ + +	++	\dashv					
- L- 173+89.75	6 RT		86	_		1.5		<u> </u>			1		† †		1	1		1	3.0											1 1	+	$\dashv \uparrow$				1	
- L- 173+91.09	102 RT	1609	81															1	3.4									1		1							
- L- 173+91.09	RT			7:	2.7	72.2 0	0.5%					144	4						[]																		
- L- 180+71.00	8 RT	+	90	_				$\perp \downarrow \perp \downarrow$								1		1					1						1 1	1	$\perp \downarrow \perp \downarrow$	$\perp \downarrow \downarrow$				1	
- L- 180+71.00	RT		1612	_	6.1	86.1 0	0.5%	+	-		+	10	6	+ +							$\vdash \vdash$			+		\dashv				1	\dashv	\dashv				1	
- L- 180+73.00 - L- 180+73.00	28 RT	1612 1612			6.1	85.8 0	7 50/	+			+	92	2	+		+	+	1	 		$\vdash \vdash$		1	+		++	+	+ + +	1 1	1	++	++				+	
- L- 180+73.00 - L- 181+67.26	12 RT				U. I	00.0	0.070	+	\dashv	-	++	9,	<u> </u>	++		+	+	1	0.2		$\vdash \vdash$		1	$\dashv \dashv$		++	+	+ + +	1	1	++	$\dashv \dashv$				+	
- L- 181+67.26		1613			5.8	85.7 0	0.5%	+	+		++	36	6	+++	+	1		+ '-	0.2		\vdash		+	+		++		 	 	+ + +	++	$\dashv \dashv$				1	
- L- 181+97.51	28 RT				-			 			++	<u> </u>	+	++	1	1		1	0.7				1			\dashv			1 1	1	+	$\dashv \uparrow$				1	
- L- 181+97.51		1614			5.7	85.2 0	0.5%					136	6																								
- L- 183+34.50	15 RT	1615	89															1								1		1									
- L- 183+34.50	RT	 			5.2	85.2 0	0.8%						8			<u> </u>		<u> </u>	 													$\bot \!\!\! \bot \!\!\! \bot$					
- L- 183+34.50	5 RT	1616	90	.9				$\perp \perp \perp \downarrow$					+					1	1.4		$\vdash \vdash$			\bot		\dashv		1		1 1	$\perp \downarrow \perp$	$\perp \downarrow \downarrow$				1	
	+			+				+								1	-	1			$\vdash \vdash$			+		++				+	+	\dashv			-	+	
	+-+	\vdash		+			-+	+	+		++		++		+	 		 			\vdash			+		++	+	+ + +		+ + +	++	+				+	<u> </u>
3D-1 SHEET TOTALS	+ +	 		-		+	-+					0 113	2 0	0 8	0 0		0 0	20	23.7	9.0		0 0 4	0 11	0 0	0 4	4 0	0 0	5 0 4	0 11 1	1 5 0	0 0	1 0	2 @ 15	n		0 '	
T 3D-1 SHEEL IOLALS								v v			Į U	UJ 1137	۷ U	اه ام	ν Ι υ	<u>′I </u>	<u> </u>	20 إر	23.1	9.0	V	υ υ (<u> </u>	υJU	ן טן זן	4 0	υj U	, J U 4	η υμίτη 1	1 0 0	V U	1 0	∠ (<u>w</u> 15	l U		<u> </u>	

6/2022 Roadway\Proj\W57Ø1B_Rdy_psh_Ø3D.dgn efler

P: (919) 878-9560 8601 Six Forks Road, Forum 1,Suite 700 Raleigh, North Carolina 27615-3960 NC License No. F-0112

NC License No. F-0112

Engineers | Construction Managers | Planners | Scientists

www.rkk.com

Responsive People | Creative Solutions