

REFERENCE: BR-0048

PROJECT: 35026

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STRUCTURE
SUBSURFACE INVESTIGATION

COUNTY SURRY
PROJECT DESCRIPTION REPLACEMENT OF BRIDGE
NO. 103 ON NC 268 OVER MITCHELL RIVER
US 311 I-40
SITE DESCRIPTION STA. 18+75 -L-

CONTENTS

SHEET NO.	DESCRIPTION
1	TITLE SHEET
2	LEGEND (SOIL & ROCK)
2A	SUPPLEMENTAL LEGEND (GSI)
3	SITE PLAN
4	PROFILE
5	CROSS SECTIONS
6-15	BORE LOGS, CORE REPORTS & CORE PHOTOGRAPHS
16	ROCK LABORATORY RESULTS
17	SITE PHOTOGRAPHS

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	BR-0048	1	17

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

NOTES:

- THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
- BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

PERSONNEL

J. STICKNEY

C. DRISCOLL

C. SMITH

TRIGON EXPLORATION

INVESTIGATED BY J. STICKNEY

DRAWN BY S. PAPKE

CHECKED BY E. BEVERLY

SUBMITTED BY K. MILLER

DATE JULY 2019



Signature of Kevin B. Miller

957A789AE6/2019

SIGNATURE

DATE

DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION												GRADATION					ROCK DESCRIPTION					TERMS AND DEFINITIONS																																																																																																																																																																																																																																																							
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 208, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6												WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.					HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS: 					ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (IN OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.																																																																																																																																																																																																																																																							
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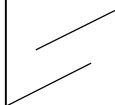
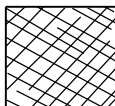


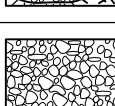
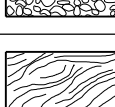
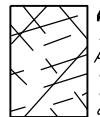


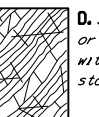




NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

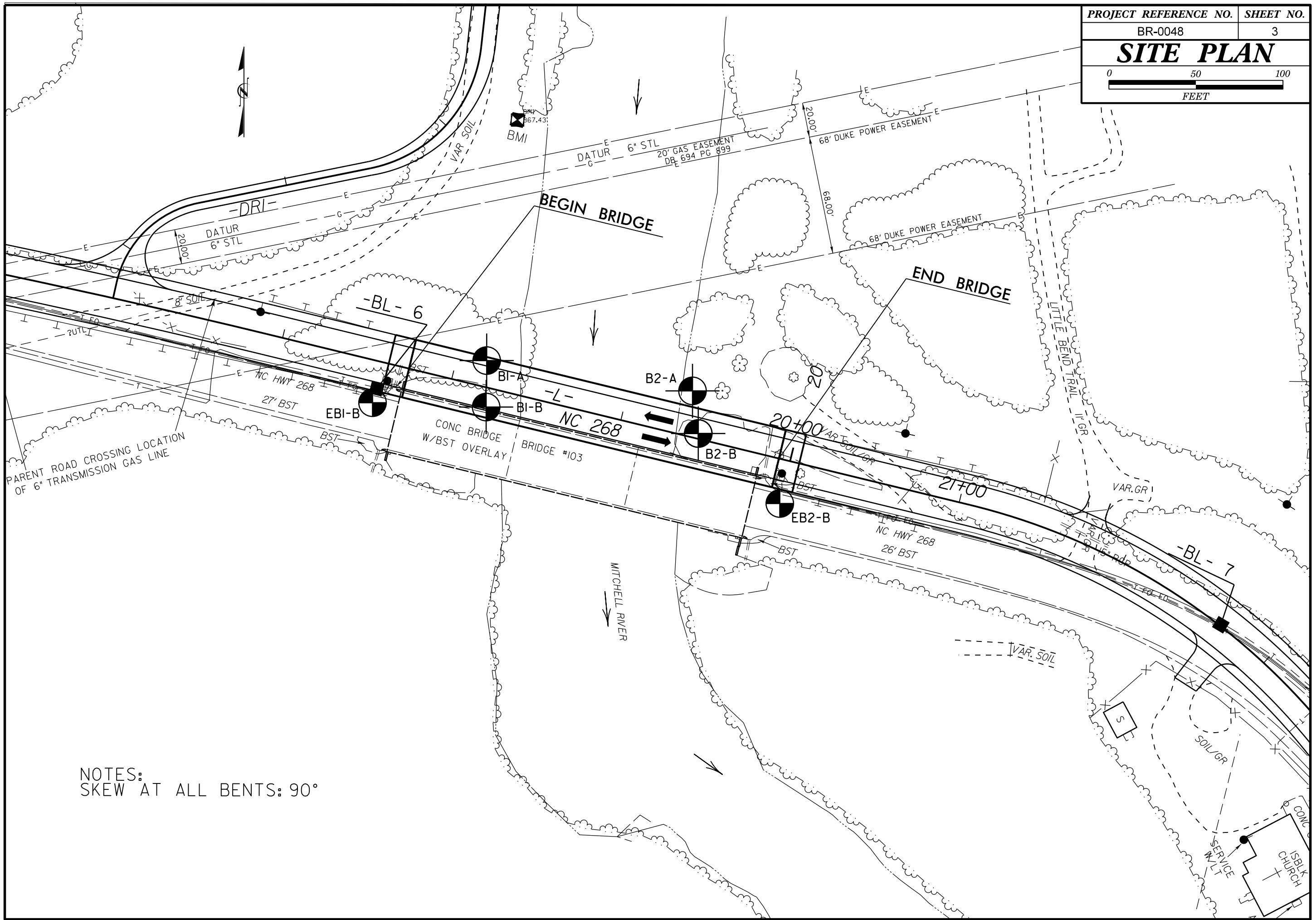
SUBSURFACE INVESTIGATION

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES
FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

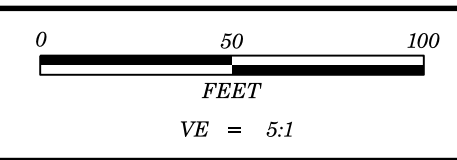
AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

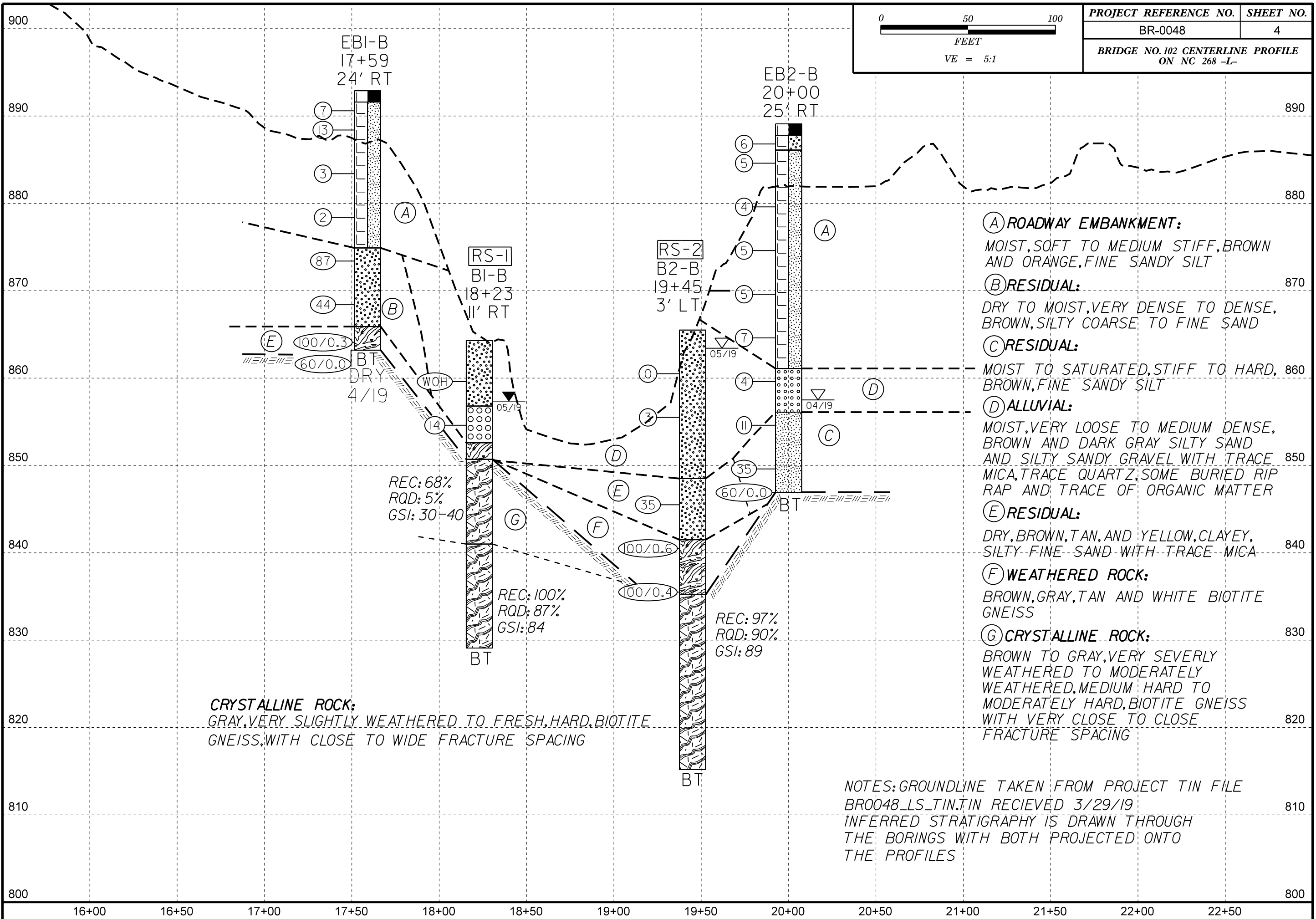
<p>GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000)</p> <p>From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.</p> <p>STRUCTURE</p>	<p>SURFACE CONDITIONS</p> <p>VERY GOOD Very rough, fresh unweathered surfaces</p> <p>GOOD Rough, slightly weathered, iron stained surfaces</p> <p>FAIR Smooth, moderately weathered and altered surfaces</p> <p>POOR Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments</p> <p>VERY POOR Slickensided, highly weathered surfaces with soft clay coatings or fillings</p> <p>DECREASING SURFACE QUALITY →</p>					<p>GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000)</p> <p>From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.</p> <p>COMPOSITION AND STRUCTURE</p>	<p>SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes)</p> <p>VERY GOOD - Very Rough, fresh unweathered surfaces</p> <p>GOOD - Rough, slightly weathered surfaces</p> <p>FAIR - Smooth, moderately weathered and altered surfaces</p> <p>POOR - Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments</p> <p>VERY POOR - Very smooth, slickensided or highly weathered surfaces with soft clay coatings or fillings</p>				
<p>INTERLOCKING OF ROCK PIECES</p> <p>DECREASING INTERLOCKING OF ROCK PIECES ↓</p> <p> INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities</p> <p> BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets</p> <p> VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets</p> <p> BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity</p> <p> DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces</p> <p> LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes</p>	<p>90</p> <p>80</p> <p>70</p> <p>60</p> <p>50</p> <p>40</p> <p>30</p> <p>20</p> <p>10</p>	<p>N/A</p> <p>N/A</p>	<p>N/A</p> <p>N/A</p>	<p>N/A</p> <p>N/A</p>	<p>N/A</p> <p>N/A</p>	<p> A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.</p> <p> B. Sandstone with thin inter-layers of siltstone</p> <p> C. Sandstone and siltstone in similar amounts</p> <p> D. Siltstone or silty shale with sandstone layers</p> <p> E. Weak siltstone or clayey shale with sandstone layers</p> <p>C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H.</p> <p> F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure</p> <p> G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers</p> <p> H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces.</p> <p>→ Means deformation after tectonic disturbance</p>	<p>70</p> <p>60</p> <p>50</p> <p>40</p> <p>30</p> <p>20</p> <p>10</p>	<p>A</p> <p>B</p> <p>C</p> <p>D</p> <p>E</p> <p>F</p> <p>G</p> <p>H</p>	<p>A</p> <p>B</p> <p>C</p> <p>D</p> <p>E</p> <p>F</p> <p>G</p> <p>H</p>	<p>A</p> <p>B</p> <p>C</p> <p>D</p> <p>E</p> <p>F</p> <p>G</p> <p>H</p>	<p>A</p> <p>B</p> <p>C</p> <p>D</p> <p>E</p> <p>F</p> <p>G</p> <p>H</p>



NOTES:
SKEW AT ALL BENTS: 90°



PROJECT REFERENCE NO.	SHEET NO.
BR-0048	4
BRIDGE NO. 102 CENTERLINE PROFILE ON NC 268 -L-	



- (A) ROADWAY EMBANKMENT:**
MOIST, SOFT TO MEDIUM STIFF, BROWN AND ORANGE, FINE SANDY SILT
- (B) RESIDUAL:**
DRY TO MOIST, VERY DENSE TO DENSE, BROWN, SILTY COARSE TO FINE SAND
- (C) RESIDUAL:**
MOIST TO SATURATED, STIFF TO HARD, BROWN, FINE SANDY SILT
- (D) ALLUVIAL:**
MOIST, VERY LOOSE TO MEDIUM DENSE, BROWN AND DARK GRAY SILTY SAND AND SILTY SANDY GRAVEL WITH TRACE MICA, TRACE QUARTZ, SOME BURIED RIP RAP AND TRACE OF ORGANIC MATTER
- (E) RESIDUAL:**
DRY, BROWN, TAN, AND YELLOW, CLAYEY, SILTY FINE SAND WITH TRACE MICA
- (F) WEATHERED ROCK:**
BROWN, GRAY, TAN AND WHITE BIOTITE GNEISS
- (G) CRYSTALLINE ROCK:**
BROWN TO GRAY, VERY SEVERLY WEATHERED TO MODERATELY WEATHERED, MEDIUM HARD TO MODERATELY HARD, BIOTITE GNEISS WITH VERY CLOSE TO CLOSE FRACTURE SPACING

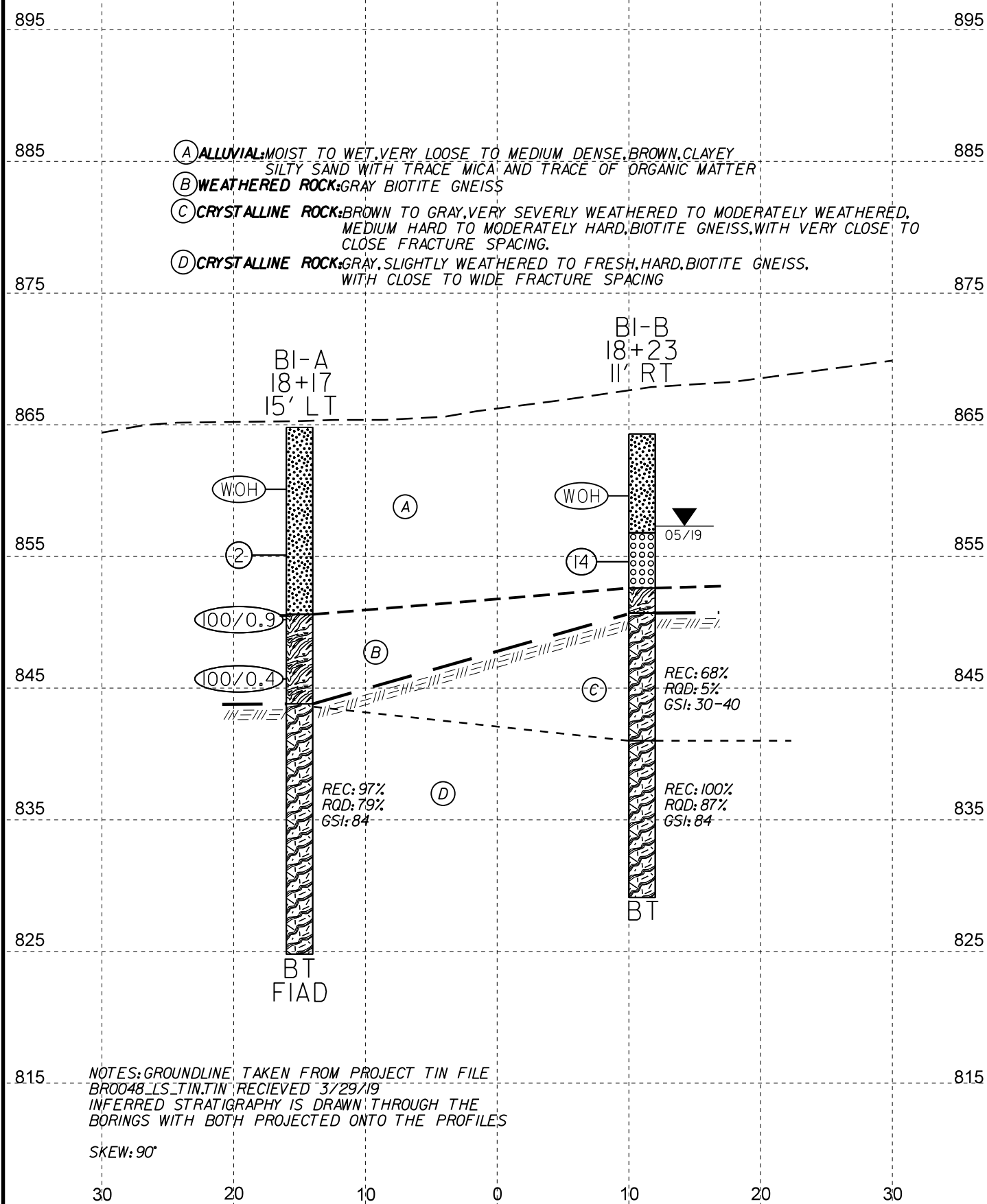
CRYSTALLINE ROCK:
GRAY, VERY SLIGHTLY WEATHERED TO FRESH, HARD, BIOTITE GNEISS, WITH CLOSE TO WIDE FRACTURE SPACING

REC: 68%
RQD: 5%
GSI: 30-40

REC: 100%
RQD: 87%
GSI: 84

REC: 97%
RQD: 90%
GSI: 89

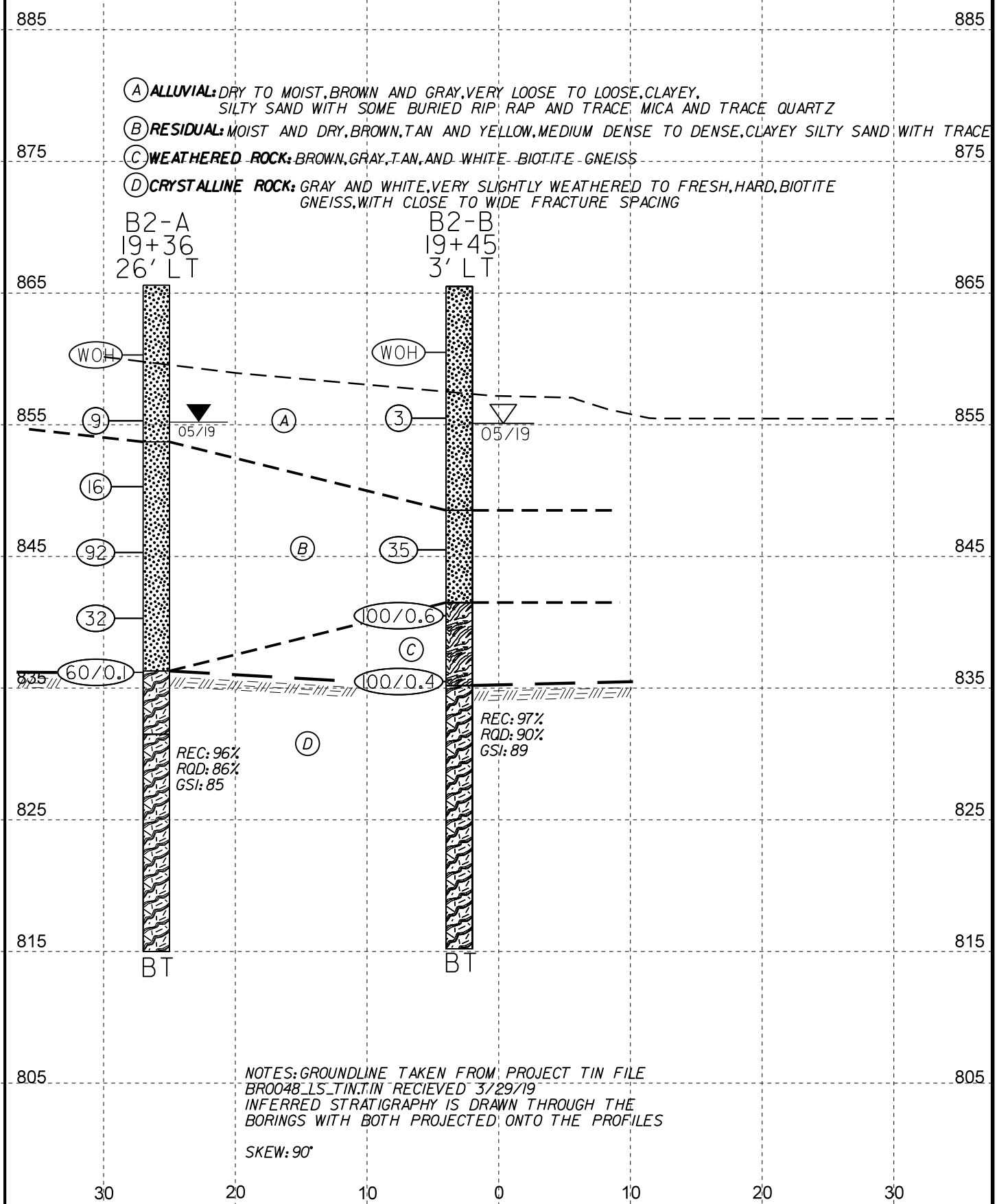
NOTES: GROUNDLINE TAKEN FROM PROJECT TIN FILE BR0048_LS_TIN.TIN RECEIVED 3/29/19
INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE PROFILES



NOTES: GROUNDLINE TAKEN FROM PROJECT TIN FILE BR0048_LS_TIN.TIN RECEIVED 3/29/19
 INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE PROFILES
 SKEW: 90°

HORIZ. SCALE 0 10 20 (FEET) VE = 1:1

CROSS SECTION ALONG BENT 1 AT 18+17.50



NOTES: GROUNDLINE TAKEN FROM PROJECT TIN FILE BR0048_LS_TIN.TIN RECEIVED 3/29/19
 INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE PROFILES
 SKEW: 90°

HORIZ. SCALE 0 10 20 (FEET) VE = 1:1

CROSS SECTION ALONG BENT 2 AT STA. 19+32.50

GEOTECHNICAL BORING REPORT

BORE LOG

WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST C. Driscoll										
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)									
BORING NO. EB1-B		STATION 17+59		OFFSET 24 ft RT		ALIGNMENT -L-	0 HR. Dry									
COLLAR ELEV. 892.9 ft		TOTAL DEPTH 29.7 ft		NORTHING 924,558		EASTING 1,477,944	24 HR. FIAD									
DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 87% 03/21/2019				DRILL METHOD H.S. Augers		HAMMER TYPE Automatic										
DRILLER R. Toothman		START DATE 04/15/19		COMP. DATE 04/15/19		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft)	DEPTH (ft)		
895																
	891.6	1.3												892.9	0.0	GROUND SURFACE
890	889.4	3.5	7	4	3									891.6	1.3	ROADWAY EMBANKMENT Asphalt (0.0 - 0.5 Foot) ABC Stone (0.5 - 1.3 Feet)
			5	6	7											Brown and Orange, Fine Sandy SILT
885	884.4	8.5														
			2	1	2											
880	879.4	13.5	1	1	1											
875	874.4	18.5	20	17	70									874.9	18.0	RESIDUAL Brown, Silty Coarse to Fine SAND
870	869.4	23.5	3	17	27											
865	864.4	28.5												865.9	27.0	WEATHERED ROCK Gray and White GNEISS
	863.2	29.7	100/0.3											863.2	29.7	Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 863.2 ft on CRYSTALLINE ROCK: GNEISS
			60/0.0													

NCDOT BORE DOUBLE BR0048_GEO_BRDG_GINT.GPJ NC_DOT.GDT 6/19/19

GEOTECHNICAL BORING REPORT BORE LOG

GEOTECHNICAL BORING REPORT CORE LOG

WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST Stickney, J. K.										
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)									
BORING NO. B1-A		STATION 18+17		OFFSET 15 ft LT		ALIGNMENT -L-										
COLLAR ELEV. 864.8 ft		TOTAL DEPTH 40.0 ft		NORTHING 924,714		EASTING 1,478,042										
DRILL RIG/HAMMER EFF./DATE HFO0072 CME-550X 92% 08/15/2018			DRILL METHOD NW Casing W/SPT & Core		HAMMER TYPE Automatic											
DRILLER Smith, C. L.		START DATE 05/22/19		COMP. DATE 05/22/19		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft)	DEPTH (ft)		
865														864.8	0.0	GROUND SURFACE
860	861.1	3.7	WOH	WOH	WOH							M				ALLUVIAL Brown, Clayey Silty SAND with Trace Mica and Trace of Organic Matter (Leaves and Wood)
855	856.1	8.7	2	1	1							W				
850	851.1	13.7	2	98/0.4										850.6	14.2	WEATHERED ROCK Gray BIOTITE GNEISS
845	846.1	18.7	100/0.4													
840																
835																
830																
825														824.8	40.0	Boring Terminated at Elevation 824.8 ft in CRYSTALLINE ROCK: BIOTITE GNEISS

WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST Stickney, J. K.					
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)				
BORING NO. B1-A		STATION 18+17		OFFSET 15 ft LT		ALIGNMENT -L-					
COLLAR ELEV. 864.8 ft		TOTAL DEPTH 40.0 ft		NORTHING 924,714		EASTING 1,478,042					
DRILL RIG/HAMMER EFF./DATE HFO0072 CME-550X 92% 08/15/2018			DRILL METHOD NW Casing W/SPT & Core		HAMMER TYPE Automatic						
DRILLER Smith, C. L.		START DATE 05/22/19		COMP. DATE 05/22/19		SURFACE WATER DEPTH N/A					
CORE SIZE NX		TOTAL RUN 19.0 ft									
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN		SAMP. NO.	STRATA		LOG	DESCRIPTION AND REMARKS
					REC. (%)	RQD (%)		REC. (%)	RQD (%)		
843.8	843.8	21.0	4.0	NM/1.0 NM/1.0 1:44/1.0 1:50/1.0	(3.6) 90%	(3.2) 80%		(18.4) 97%	(15.1) 79%		Begin Coring @ 21.0 ft CRYSTALLINE ROCK Gray, Slightly Weathered to Fresh, Hard, Biotite Gneiss with Close to Wide Fracture Spacing GSI: 84
840	839.8	25.0	5.0	1:38/1.0 1:41/1.0 1:40/1.0 1:45/1.0 1:41/1.0	(4.9) 98%	(4.3) 86%					
835	834.8	30.0	5.0	1:50/1.0 1:40/1.0 1:42/1.0 1:44/1.0 1:41/1.0	(4.9) 98%	(3.9) 78%					
830	829.8	35.0	5.0	1:38/1.0 1:35/1.0 1:41/1.0 1:39/1.0 1:44/1.0	(5.0) 100%	(3.7) 74%					
825	824.8	40.0									Boring Terminated at Elevation 824.8 ft in CRYSTALLINE ROCK: BIOTITE GNEISS

CORE PHOTOGRAPHS

B1-A BOX 1 & 2: 21.0 to 40.0 FEET



GEOTECHNICAL BORING REPORT

BORE LOG

GEOTECHNICAL BORING REPORT

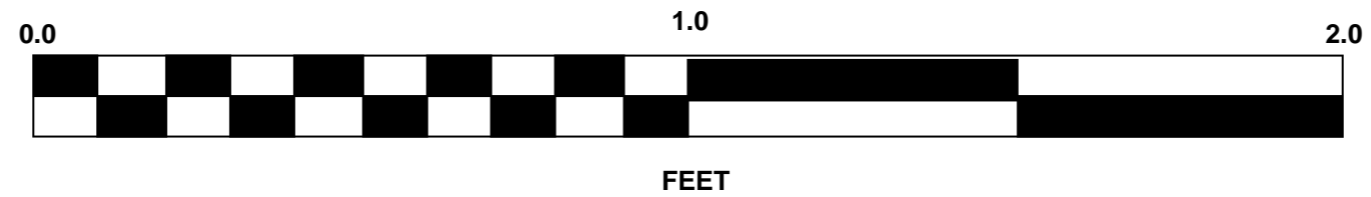
CORE LOG

WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST Stickney, J. K.												
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)											
BORING NO. B1-B		STATION 18+23		OFFSET 11 ft RT		ALIGNMENT -L-												
COLLAR ELEV. 864.3 ft		TOTAL DEPTH 35.2 ft		NORTHING 924,556		EASTING 1,478,009												
DRILL RIG/HAMMER EFF./DATE HFO0072 CME-550X 92% 08/15/2018			DRILL METHOD NW Casing W/SPT & Core		HAMMER TYPE Automatic													
DRILLER Smith, C. L.		START DATE 05/22/19		COMP. DATE 05/22/19		SURFACE WATER DEPTH N/A												
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG MOI	L O G	SOIL AND ROCK DESCRIPTION				
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)			
865															864.3	GROUND SURFACE	0.0	
860	860.6	3.7	WOH	WOH	WOH								M			ALLUVIAL Brown, Clayey, Silty fine SAND with Trace Mica		
855	855.6	8.7													856.8	Dark Gray, Silty Sandy GRAVEL with Trace of Organic Matter (Wood) and Trace Quartz	7.9	
850															852.6	WEATHERED ROCK BIOTITE GNEISS	11.7	
845															850.7	CRYSTALLINE ROCK Brown to Gray BIOTITE GNEISS	13.6	
840															841.0	Gray BIOTITE GNEISS	23.3	
835																		
830															829.1	Boring Terminated at Elevation 829.1 ft in CRYSTALLINE ROCK: BIOTITE GNEISS	35.2	

WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST Stickney, J. K.						
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)					
BORING NO. B1-B		STATION 18+23		OFFSET 11 ft RT		ALIGNMENT -L-						
COLLAR ELEV. 864.3 ft		TOTAL DEPTH 35.2 ft		NORTHING 924,556		EASTING 1,478,009						
DRILL RIG/HAMMER EFF./DATE HFO0072 CME-550X 92% 08/15/2018			DRILL METHOD NW Casing W/SPT & Core		HAMMER TYPE Automatic							
DRILLER Smith, C. L.		START DATE 05/22/19		COMP. DATE 05/22/19		SURFACE WATER DEPTH N/A						
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN		SAMP. NO.	STRATA		L O G	DESCRIPTION AND REMARKS	
					REC. (ft) %	RQD (ft) %		REC. (ft) %	RQD (ft) %		ELEV. (ft)	DEPTH (ft)
850.7												Begin Coring @ 13.6 ft
850.7	849.1	13.6	1.6	NM/1.0	(0.8)	(0.5)		(6.6)	(0.5)		850.7	CRYSTALLINE ROCK Brown to Gray, Very Severly Weathered to Moderately Weathered, Medium Hard to Moderately Hard, BIOTITE GNEISS, with Very Close to Close Fracture Spacing. (13.6-14.2' is Fresh White Plagioclase Feldspar) GSI: 30-40
845												
845	844.1	20.2	5.0	NM/1.0	(3.1)	(0.0)						
840												
840	839.1	25.2	5.0	1:45/1.0	(4.7)	(1.8)					841.0	Gray, Very Slightly Weathered to Fresh, Hard, BIOTITE GNEISS, with Close to Wide Fracture Spacing GSI: 84
835												
835	834.1	30.2	5.0	1:42/1.0	(5.0)	(5.0)						
830												
830	829.1	35.2	5.0	1:47/1.0	(5.0)	(3.6)					829.1	Boring Terminated at Elevation 829.1 ft in CRYSTALLINE ROCK: BIOTITE GNEISS

CORE PHOTOGRAPHS

B1-B BOX 1: 13.6 to 35.2 FEET



GEOTECHNICAL BORING REPORT

BORE LOG

GEOTECHNICAL BORING REPORT

CORE LOG

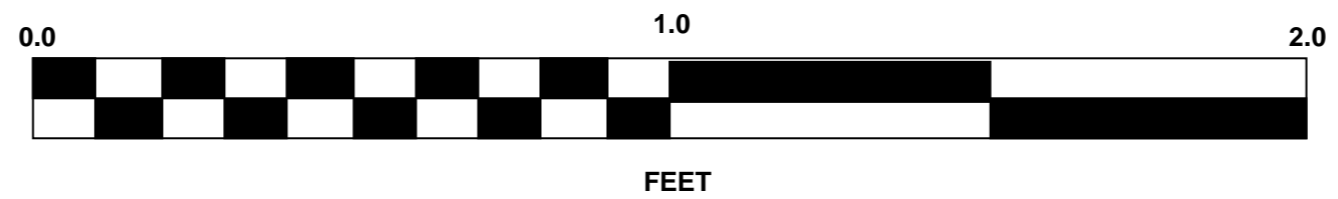
WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST Stickney, J. K.									
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)								
BORING NO. B2-A		STATION 19+36		OFFSET 26 ft LT		ALIGNMENT -L-									
COLLAR ELEV. 865.6 ft		TOTAL DEPTH 50.6 ft		NORTHING 924,565		EASTING 1,478,128									
DRILL RIG/HAMMER EFF./DATE HFO0072 CME-550X 92% 08/15/2018			DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic									
DRILLER Smith, C. L.		START DATE 05/28/19		COMP. DATE 05/28/19		SURFACE WATER DEPTH N/A									
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100					
870															
865														865.6	0.0
860	861.3	4.3	WOH	WOH	WOH								M		
855	856.3	9.3	1	8	1										
850	851.3	14.3	4	7	9								M	853.7	11.9
845	846.3	19.3	28	34	58								D		
840	841.3	24.3	15	12	20								M		
835	836.3	29.3	60/0.1											836.3	29.3
830														831.5	34.1
825															
820															
815														815.0	50.6
Boring Terminated at Elevation 815.0 ft in CRYSTALLINE ROCK: BIOTITE GNEISS															

WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST Stickney, J. K.				
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)			
BORING NO. B2-A		STATION 19+36		OFFSET 26 ft LT		ALIGNMENT -L-				
COLLAR ELEV. 865.6 ft		TOTAL DEPTH 50.6 ft		NORTHING 924,565		EASTING 1,478,128				
DRILL RIG/HAMMER EFF./DATE HFO0072 CME-550X 92% 08/15/2018			DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic				
DRILLER Smith, C. L.		START DATE 05/28/19		COMP. DATE 05/28/19		SURFACE WATER DEPTH N/A				
CORE SIZE NX				TOTAL RUN 16.5 ft				LOG	DESCRIPTION AND REMARKS	DEPTH (ft)
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	REC. (ft) %	RQD (ft) %	SAMP. NO.			
831.5	831.5	34.1	1.5	NM/1.0	(1.3)	(1.3)		(15.3)	(14.2)	831.5
830	830.0	35.6	5.0	NM/0.5	87%	87%		93%	86%	34.1
				1:33/1.0	(4.0)	(3.1)				
				1:29/1.0	80%	62%				
				1:30/1.0						
				1:35/1.0						
				1:28/1.0						
825	825.0	40.6	5.0	1:33/1.0	(5.0)	(4.9)				
				1:40/1.0	100%	98%				
				1:39/1.0						
				1:42/1.0						
820	820.0	45.6	5.0	1:45/1.0	(5.0)	(4.9)				
				1:48/1.0	100%	98%				
				1:56/1.0						
				1:49/1.0						
815	815.0	50.6		1:53/1.0						50.6
Boring Terminated at Elevation 815.0 ft in CRYSTALLINE ROCK: BIOTITE GNEISS										

NCDOT BORE DOUBLE BR0048_GEO_BRDG_GINT.GPJ NC_DOT.GDT 7/10/19

CORE PHOTOGRAPHS

B2-A
BOX 1 & 2: 34.1 to 50.6 FEET



GEOTECHNICAL BORING REPORT BORE LOG

GEOTECHNICAL BORING REPORT CORE LOG

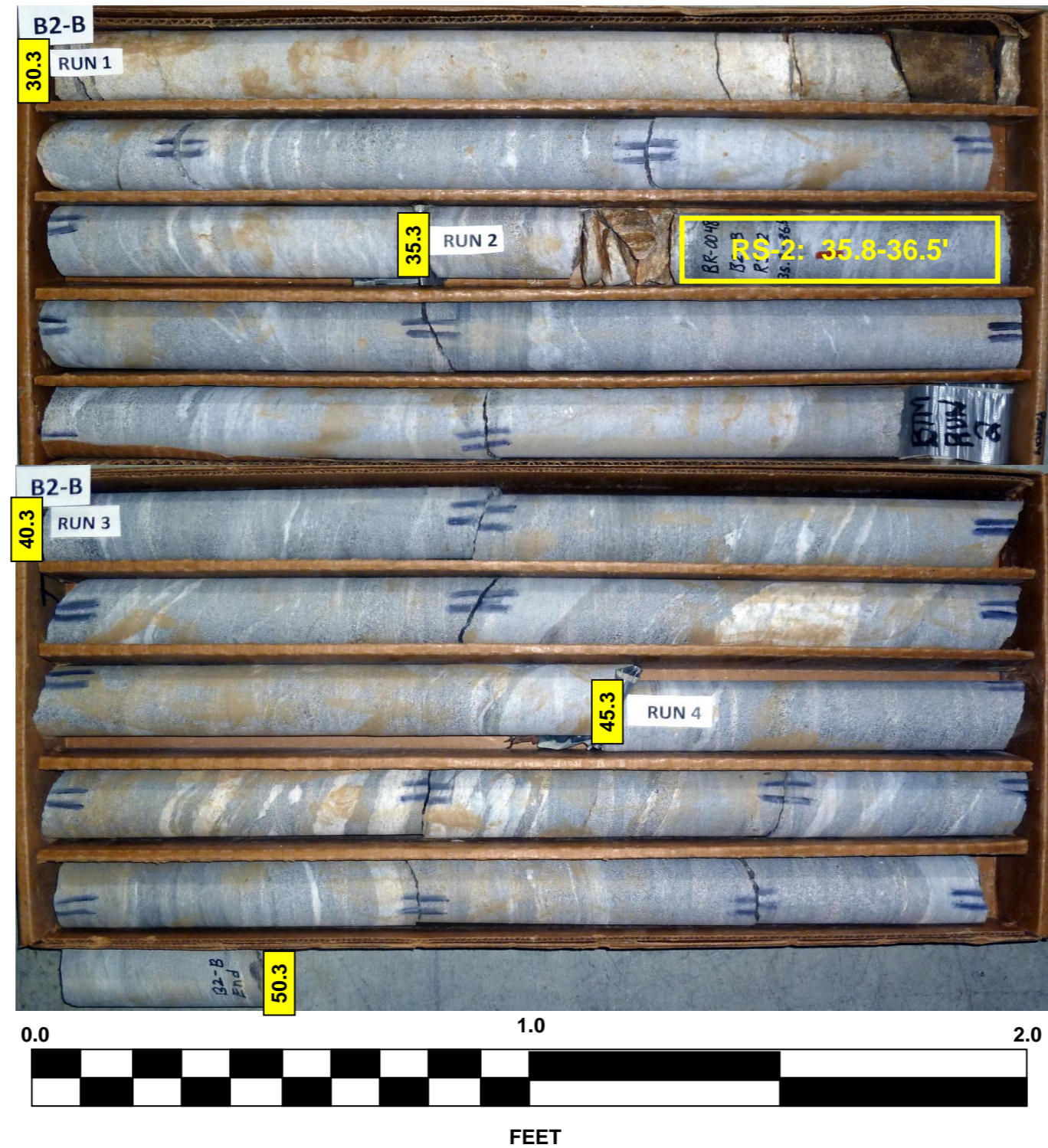
WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST Stickney, J. K.										
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)									
BORING NO. B2-B		STATION 19+45		OFFSET 3 ft LT		ALIGNMENT -L-										
COLLAR ELEV. 865.5 ft		TOTAL DEPTH 50.3 ft		NORTHING 924,541		EASTING 1,478,131										
DRILL RIG/HAMMER EFF./DATE HFO0072 CME-550X 92% 08/15/2018			DRILL METHOD NW Casing w/ Core			HAMMER TYPE Automatic										
DRILLER Smith, C. L.		START DATE 05/28/19		COMP. DATE 05/28/19		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)		
			0.5ft	0.5ft	0.5ft	0	25	50	75	100						
870																
865																
860	861.5	4.0		WOH	WOH	WOH										
855	856.5	9.0		1	1	2										
850																
845	846.5	19.0		5	10	25										
840	841.5	24.0		74	26/0.1											
835	836.5	29.0		100/0.4												
830																
825																
820																
Boring Terminated at Elevation 815.2 ft in CRYSTALLINE ROCK: BIOTITE GNEISS																

WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST Stickney, J. K.						
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)					
BORING NO. B2-B		STATION 19+45		OFFSET 3 ft LT		ALIGNMENT -L-						
COLLAR ELEV. 865.5 ft		TOTAL DEPTH 50.3 ft		NORTHING 924,541		EASTING 1,478,131						
DRILL RIG/HAMMER EFF./DATE HFO0072 CME-550X 92% 08/15/2018			DRILL METHOD NW Casing w/ Core			HAMMER TYPE Automatic						
DRILLER Smith, C. L.		START DATE 05/28/19		COMP. DATE 05/28/19		SURFACE WATER DEPTH N/A						
CORE SIZE NX				TOTAL RUN 20.0 ft								
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN		SAMP. NO.	STRATA		LOG	DESCRIPTION AND REMARKS	DEPTH (ft)
					REC. (%)	RQD (%)		REC. (%)	RQD (%)			
835.2		30.3	5.0	1:40/1.0 1:32/1.0 1:38/1.0 1:30/1.0 1:41/1.0	(4.5) 90%	(3.6) 72%		(19.3) 97%	(17.9) 90%			
830	830.2	35.3	5.0	1:45/1.0 1:47/1.0 1:40/1.0 1:43/1.0 1:51/1.0	(4.8) 96%	(4.3) 86%	RS-2					
825	825.2	40.3	5.0	1:39/1.0 1:42/1.0 1:48/1.0 1:40/1.0 1:43/1.0	(5.0) 100%	(5.0) 100%						
820	820.2	45.3	5.0	1:48/1.0 1:40/1.0 1:42/1.0 1:50/1.0 1:41/1.0	(5.0) 100%	(5.0) 100%						
Boring Terminated at Elevation 815.2 ft in CRYSTALLINE ROCK: BIOTITE GNEISS												

NCDOT BORE DOUBLE BR0048_GEO_BRDG_GINT.GPJ_NC_DOT.GDT 7/10/19

CORE PHOTOGRAPHS

B2-B BOX 1 & 2: 30.3to 50.3 FEET



GEOTECHNICAL BORING REPORT

BORE LOG

WBS 67048.1.1		TIP BR-0048		COUNTY SURRY		GEOLOGIST C. Driscoll										
SITE DESCRIPTION Replacement of Bridge 103 on NC 268 over Mitchell River							GROUND WTR (ft)									
BORING NO. EB2-B		STATION 20+00		OFFSET 25 ft RT		ALIGNMENT -L-										
COLLAR ELEV. 889.1 ft		TOTAL DEPTH 42.2 ft		NORTHING 924,501		EASTING 1,478,178										
DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 87% 03/21/2019				DRILL METHOD H.S. Augers		HAMMER TYPE Automatic										
DRILLER R. Toothman		START DATE 04/15/19		COMP. DATE 04/15/19		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft)	DEPTH (ft)		
890														889.1	0.0	GROUND SURFACE
	887.8	1.3	5	3	3								M	887.8	1.3	ROADWAY EMBANKMENT
885	885.6	3.5	2	2	3								M	886.1	3.0	Asphalt (0.0 - 0.5 Foot) ABC Stone (0.5 - 1.3 Feet)
																Gray and Brown, Silty Coarse to Fine SAND with Trace Gravel Orange and Brown, Fine Sandy SILT
880	880.6	8.5	2	2	2								M			
875	875.6	13.5	2	2	3								M			
870	870.6	18.5	WOH	2	3								M			
865	865.6	23.5	2	3	4								M			
860	860.6	28.5	2	2	2								M	861.1	28.0	ALLUVIAL Brown, Fine SAND
855	855.6	33.5	2	2	9								M	856.1	33.0	RESIDUAL Brown, Fine Sandy SILT
850	850.6	38.5	12	22	13								Sat.			
	846.9	42.2	60/0.0											846.9	42.2	Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 846.9 ft on CRYSTALLINE ROCK: GNEISS

NCDOT BORE DOUBLE BR0048_GEO_BRDG_GINT.GPJ NC_DOT.GDT 7/10/19

LABORATORY SUMMARY SHEET FOR ROCK CORE SAMPLES

SHEET 16

PROJECT NO.: 67048.1.1 (BR-0048)

COUNTY: SURRY

REPLACEMENT OF BRIDGE NO. 103 ON NC 268 OVER MITCHELL RIVER

Sample No.	Boring No.	Depth (ft)	Rock Type	Geologic Map Unit	Run RQD (%)	Length (in)	Diameter (in)	Wet Unit Weight (lb/ft ³)	Unconfined Compressive Strength (ksi)	Young's Modulus (psi)	Splitting Tensile Strength (psi)	Remarks
RS-1	B1-B	27.3-27.8	Biotite Gneiss	CZmg	100	3.70	1.86	174.7	11.68	N/A	N/A	GSI 84
RS-2	B2-B	35.8-36.5	Biotite Gneiss	CZmg	90	3.69	1.86	169.9	16.05	N/A	N/A	GSI 89

WBS NO.: 67048.1.1 - TIP NO.: BR-0048
REPLACEMENT OF BRIDGE NO. 103 ON NC 268 OVER MITCHELL RIVER
SITE PHOTOGRAPHS



View from End Bent 1 Looking East



View from Downstream Side of Bridge