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4516

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# STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS** GEOTECHNICAL ENGINEERING UNIT

# **STRUCTURE** SUBSURFACE INVESTIGATION

COUNTY FRANKLIN

PROJECT DESCRIPTION BRIDGE NO. 52 ON SR 1433 (PERSON RD.) OVER SANDY CREEK

SITE DESCRIPTION 15+17 -L-

# 38400 PROJECT

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	B-4516	1	13

#### CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOLI TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT 1999 107-6860. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORNICS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU UN-FLACED TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE ONSERVED WATER LEVELS OR SOL MOISTURE CONDITIONS MOLATED IN THE SUBSURFACE RELIVESTIGATIONS AND REAS RECORDED AT THE TIME OF THE INVESTIGATION. THES WATER LEVELS OR SOL MOISTURE CONDITIONS MAY LARY CONSIDERABLY WITH THE ACCORDING TO CLIMATIC CONDITIONS NICLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OF CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPHION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATION AS HE DEEMS NECESSARY TO SATISY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OF FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDENTIONS OF CONTANT THE SIDE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

- NOTES: I. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N.C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT. 2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE. 2.

PERSONNEL

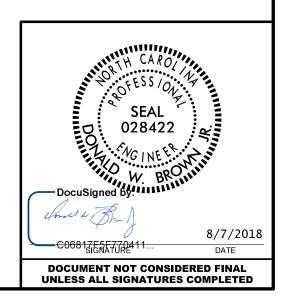
CAROLINA DRILLING

J. ANDERSON

S. ANDERSON

C.T. TANG, EI

- INVESTIGATED BY <u>C.T. TANG, EI</u> DRAWN BY \_\_C.T. TANG, EI CHECKED BY \_\_\_\_\_\_ D. BROWN, PE SUBMITTED BY \_\_\_\_\_. BROWN, PE
- DATE AUGUST 2018



# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

			SOIL D	ESCRIP	TION					(	GRADATION						ESCRIPTION
							RTH MATERIALS ' HAN 100 BLOWS		WELL GRADED - INDICAT					HARD ROCK IS ROCK LINE IN	NON-COASTAL	. PLAIN MATERIAL THAT LEVEL AT WHICH NON-CO	WOULD YIELD SPT REFUSAL IF TESTE DASTAL PLAIN MATERIAL WOULD YIELD
ACCORD	ING TO THE	STANDARD PE	NETRATION TES	ST (AASHTO	) T 206,	ASTM D158	6). SOIL CLASSIF	ICATION	UNIFORMLY GRADED - IN GAP-GRADED - INDICATE					SPT REFUSAL	IS PENETRATI	ON BY A SPLIT SPOON	SAMPLER EQUAL TO OR LESS THAN 0.1 RANSITION BETWEEN SOIL AND ROCK
CONSIST	ENCY, COLOR,	, TEXTURE, MOIS	STURE, AASHTO	CLASSIFIC	CATION, A	ND OTHER	PERTINENT FACT	ORS SUCH		ANGULA	RITY OF GRAI	NS		REPRESENTED	BY A ZONE OF	F WEATHERED ROCK.	
							TC. FOR EXAMPL SHLY PLASTIC.A-7-				OF SOIL GRAINS IS D	DESIGNATED BY	THE TERMS:		LS ARE TYPIC	CALLY DIVIDED AS FOLL	
	-		ND AND					-	ANGULAR, SUBAN		<u>d, or rounded</u> . GICAL COMPOS			WEATHERED ROCK (WR)		100 BLOWS PER	AIN MATERIAL THAT WOULD YIELD SPT FOOT IF TESTED.
GENERAL CLASS.		GRANULAR MATER ≤ 35% PASSING			Lay Mater Passing		ORGANIC MATE	RIALS	MINERAL NAM		TZ, FELDSPAR, MICA,		тс.	CRYSTALLINE		FINE TO COARSE	GRAIN IGNEOUS AND METAMORPHIC RO T REFUSAL IF TESTED. ROCK TYPE INC
GROUP	A-1	A-3	A-2		A-5 A-6	-	-1, A-2 A-4, A-5				EN THEY ARE CONSI			ROCK (CR)		GNEISS, GABBRO,	SCHIST, ETC.
CLASS.	A-1-a A-1-b	A-2-4 A-	2-5 A-2-6 A-2-	7	-		A-3 A-6, A-7				PRESSIBILITY			NON-CRYSTALL ROCK (NCR)		SEDIMENTARY RO	GRAIN METAMORPHIC AND NON-COASTA CK THAT WOULD YEILD SPT REFUSAL I
SYMBOL										HTLY COMPRESSIBLE RATELY COMPRESSI		LL < 31 LL = 31 - 1	50	COASTAL PLAI			UDES PHYLLITE, SLATE, SANDSTONE, ETC SEDIMENTS CEMENTED INTO ROCK, BUT
% PASSING	55555655555						· · · · · · · · · · · · · · · · · · ·			LY COMPRESSIBLE		LL > 50		SEDIMENTARY			DCK TYPE INCLUDES LIMESTONE, SANDS
=10 =40	50 MX	E1 MA					ANULAR SILT- CLAY	MUCK, PEAT		PERCENT	AGE OF MATER	RIAL		(CP)			
	30 MX 50 MX 15 MX 25 MX	10 MX 35 MX 35	MX 35 MX 35 M	X 36 MN 36	MN 36 MP		SOILS	FEHI	ORGANIC MATERIAL	GRANULAR SOILS	SILT - CLAY	OTHER	MATERIAL	FRESH	ROCK FRESH.CF		INTS MAY SHOW SLIGHT STAINING. ROCK I
MATERIAL							·		TRACE OF ORGANIC M	ATTER 2 - 3%	3 - 5%	TRACE	1 - 10%		HAMMER IF CRY		
PASSING 40	_	- 40 MY 4	MN 40 MX 41 M		MN 40 M		SOILS WITH		LITTLE ORGANIC MAT MODERATELY ORGANIC		5 - 12% 12 - 20%	LITTLE SOME	10 - 20% 20 - 35%				D, SOME JOINTS MAY SHOW THIN CLAY CO SHINE BRIGHTLY. ROCK RINGS UNDER HA
PI	6 MX		MX 11 MN 11 M				LITTLE OR MODERATE	HIGHL Y	HIGHLY ORGANIC	> 10%	> 20%	HIGHLY	35% AND ABOVE		OF A CRYSTALL		SHINE BRIGHTLT. RUCK RINGS UNDER HE
GROUP INDEX	0	0 0	4 MX	8 MX 12	MX 16 MX	K NO MX	AMOUNTS OF	ORGANIC SOILS		GRO	OUND WATER						D AND DISCOLORATION EXTENDS INTO RO
USUAL TYPES	STONE FRAGS.	FINE SILT	Y OR CLAYEY	SILTY	CL	AYEY	ORGANIC		$\nabla$	WATER LEVEL IN	N BORE HOLE IMMEDI	ATELY AFTER (	DRILLING				Y. IN GRANITOID ROCKS SOME OCCASIONAL CRYSTALLINE ROCKS RING UNDER HAMMER
OF MAJOR MATERIALS	GRAVEL, AND SAND	SAND GRAV	'el and sand	SOILS	sr	OILS			▼	STATIC WATER L	EVEL AFTER 168	HOURS					DISCOLORATION AND WEATHERING EFFECTS
GEN. RATING		EXCELLENT TO G	000		IR TO POOR	F	AIR TO POOR	UNSUITABLE	<u> </u>	PERCHED WATER,	SATURATED ZONE, OF	R WATER BEARI	ING STRATA				DULL AND DISCOLORED, SOME SHOW CLAY SHOWS SIGNIFICANT LOSS OF STRENGTH
AS SUBGRADE							POOR	UNSULTABLE	O-M-	SPRING OR SEEP	•				VITH FRESH RO		SHOWS STONIFICHINI LUSS OF STRENGTH
		PI OF A-7-5 SUB					.L - 30		000			0.0					OR STAINED. IN GRANITOID ROCKS, ALL F
			<u>ISISTENC</u>					00151150		MISCELL	ANEOUS SYMB	ULS					KAOLINIZATION. ROCK SHOWS SEVERE LO SIST'S PICK. ROCK GIVES "CLUNK" SOUND W
PRIMARY S	SOIL TYPE	COMPACT CONSIS		PENETRAT	OF STAN TION RESI		RANGE OF UN COMPRESSIVE	STRENGTH	ROADWAY EMB	HINKMENT (NE)	025 DIP & DIP DIF	RECTION				ULD YIELD SPT REFUSAL	
				1)	N-VALUE)		(TONS/	FT~)		1	→ OF ROCK STRU						OR STAINED. ROCK FABRIC CLEAR AND EX . IN GRANITOID ROCKS ALL FELDSPARS A
GENERA		VERY LOC			< 4 4 TO 10				SOIL SYMBOL		DPT DMT TEST BO	IRING	SLOPE INDICATOR		TO SOME EXTEN	NT. SOME FRAGMENTS OF	STRONG ROCK USUALLY REMAIN.
GRANUL		MEDIUM			Ø TO 3Ø		N/A			ILL (AF) OTHER		; <b>(</b>	CONE PENETROMETER			ULD YIELD SPT N VALUES	
(NON-CO	HESIVE)	DEI VERY			0 TO 50 > 50				THAN ROADWA	Y EMBANKMENT			TEST				OR STAINED. ROCK FABRIC ELEMENTS AR
		VERY	SOFT		< 2		< 0.2	5	- INFERRED SOI	L BOUNDARY -(	- CORE BORING	•	SOUNDING ROD	(V SEV.)	REMAINING, SAP	PROLITE IS AN EXAMPLE	OF ROCK WEATHERED TO A DEGREE THAT
GENERAL SILT-CL		SO MEDIUM			2 TO 4 4 TO 8		0.25 TC 0.5 TO		INFERRED ROO		⊤ ◯ MONITORING W		TEST BORING				MAIN. <u>IF TESTED, WOULD YIELD SPT N VI</u> NOT DISCERNIBLE, OR DISCERNIBLE ONLY 1
MATERIA	AL	ST	IFF	ε	B TO 15		1 TO	2				Y	WITH CORE		SCATTERED COM	NCENTRATIONS. QUARTZ M	AY BE PRESENT AS DIKES OR STRINGERS.
(COHESI	VE)	VERY HA			5 TO 30 > 30		2 TO > 4		ALLUVIAL SOI	L BOUNDARY		-	SPT N-VALUE		ALSO AN EXAMP		
		T	EXTURE	JR GRA	IN SI	ZE				RECOMME	NDATION SYME	BOLS					HARDNESS
U.S. STD. SI	EVE SIZE		4 10	40	60	200	270						IFIED EXCAVATION -			RATCHED BY KNIFE OR SH BLOWS OF THE GEOLOGIS	HARP PICK. BREAKING OF HAND SPECIMENS
OPENING (M			4.76 2.00	0.42	0.25		0.053			UNSUITABLE W			BLE, BUT NOT TO BE THE TOP 3 FEET OF				ONLY WITH DIFFICULTY. HARD HAMMER BL
BOULDE	R CO	BBLE G	RAVEL	COARSE SAND		F INE SAND	SILT	CLAY	UNDERCUT	ACCEPTABLE D	EGRADABLE ROCK		ENT OR BACKFILL		TO DETACH HAN		
(BLDR.)	) (0	COB.)	(GR.)	(CSE, SD.)	,	(F SD.)	(SL.)	(CL.)			BREVIATIONS						GOUGES OR GROOVES TO 0.25 INCHES DE GIST'S PICK, HAND SPECIMENS CAN BE DE
GRAIN MM		75	2.0		0.25		0.05 0.00	95	AR - AUGER REFUSAL		- MEDIUM		VANE SHEAR TEST		BY MODERATE E		
SIZE IN.	. 12	3							BT - BORING TERMINATED CL CLAY		- MICACEOUS - MODERATELY		WEATHERED NIT WEIGHT				ES DEEP BY FIRM PRESSURE OF KNIFE OF PEICES 1 INCH MAXIMUM SIZE BY HARD
		SOIL MOIS			ATION	I OF TI	ERMS		CPT - CONE PENETRATION	N TEST NP -	NON PLASTIC	γ <sub>a</sub> - DF	RY UNIT WEIGHT			EOLOGIST'S PICK.	
	MOISTURE		FIELD MC DESCRI		GUID	E FOR FIE	LD MOISTURE D	ESCRIPTION	CSE COARSE DMT - DILATOMETER TES		<ul> <li>ORGANIC</li> <li>PRESSUREMETER T</li> </ul>	FST SAM	PLE ABBREVIATIONS				KNIFE OR PICK. CAN BE EXCAVATED IN
									DPT - DYNAMIC PENETRA	TION TEST SAP.	- SAPROLITIC	S - BU	LK			BROKEN BY FINGER PRE	ZE BY MODERATE BLOWS OF A PICK POINT SSURE.
			- SATURA (SAT.)				D:VERY WET.US HE GROUND WAT		e – VOID RATIO F – FINE		SAND, SANDY SILT, SILTY		PLIT SPOON HELBY TUBE				CAVATED READILY WITH POINT OF PICK.
		LIMIT							FOSS FOSSILIFEROUS	SLI.	- SLIGHTLY	RS - R	OCK		OR MORE IN TH FINGERNAIL.	HICKNESS CAN BE BROKEN	BY FINGER PRESSURE. CAN BE SCRATCH
PLASTIC RANGE <			- WET -	(W)			UIRES DRYING 1	0	FRAC FRACTURED, FRAC FRAGS FRAGMENTS		- TRICONE REFUSAL MOISTURE CONTENT		ECOMPACTED TRIAXIAL CALIFORNIA BEARING		RACTURE	SPACING	BEDDING
(PI) PL	PLASTI	IC LIMIT					M MOISTURE		HI HIGHLY	v - v			RATIO	TERM		SPACING	TERM
			- MOIST	- (M)	SOLT	D- 4T OR N	EAR OPTIMUM N	INTSTURE	EO	UIPMENT USE	D ON SUBJEC	T_PROJEC	Т	VERY WIDE WIDE	I	MORE THAN 10 FEET 3 TO 10 FEET	VERY THICKLY BEDDED THICKLY BEDDED 1.
	L OPTIMU	M MOISTURE	10101		SOLI	<b>D</b> , HI OK I		IO10 FORE	DRILL UNITS:	ADVANCING TOOLS	5:	HAMMER TY		MODERATEL	Y CLOSE	1 TO 3 FEET	THINLY BEDDED 0.1
	T				REQU	IRES ADDI	TIONAL WATER	то	Х СМЕ-45С	X CLAY BITS		X AUTO	MATIC MANUAL	CLOSE VERY CLOS		0.16 TO 1 FOOT ESS THAN 0.16 FEET	VERY THINLY BEDDED 0.03 THICKLY LAMINATED 0.00
			- DRY -	0)			M MOISTURE		CME-55		OUS FLIGHT AUGER	CORE SIZE					THINLY LAMINATED <
			PLA	STICIT	Y				1	8" HOLLOW	AUGERS	в	нн				JRATION
			PLASTI	CITY INDE	X (PI)		DRY STREM	IGTH	CME-550		D FINGER BITS	X -N Q		FOR SEDIMENT	ARY ROCKS, IN		ENING OF MATERIAL BY CEMENTING, HE
	I PLASTIC	CT1C		Ø-5			VERY LO	W	VANE SHEAR TEST	TUNGCARB	IDE INSERTS			FRIABLE			H FINGER FREES NUMEROUS GRAINS: W BY HAMMER DISINTEGRATES SAMPLE.
	GHTLY PLAS DERATELY P			6-15 16-25			SLIGH1 MEDIUN			X CASING X	₩/ ADVANCER	HAND TOOL	HOLE DIGGER			CRAINE CAN	BE SEPARATED FROM SAMPLE WITH STI
HIG	HLY PLASTI		2	6 OR MORE	1		HIGH		PORTABLE HOIST		STEEL TEETH		AUGER	MODERA	TELY INDURAT		LY WHEN HIT WITH HAMMER.
			(	COLOR					4 🗂		TUNGCARB.		DING ROD	INDURA	ED		DIFFICULT TO SEPARATE WITH STEEL I
DESCRIPT	TIONS MAY	INCLUDE COLO	R OR COLOR	COMBINAT	IONS (TF	AN, RED, YE	LLOW-BROWN, BL	UE-GRAY).		CORE BIT			SHEAR TEST				D BREAK WITH HAMMER.
							RIBE APPEARAN							EXTREM	ELY INDURATE		ER BLOWS REQUIRED TO BREAK SAMPLE AKS ACROSS GRAINS.

### PROJECT REFERENCE NO.





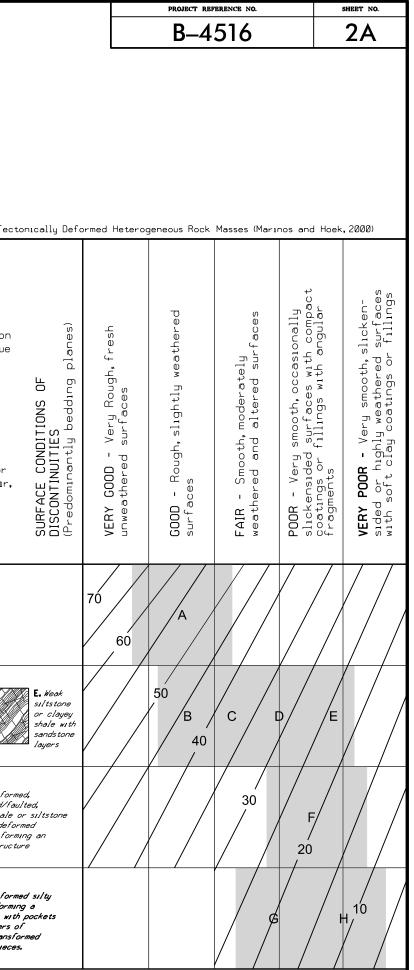
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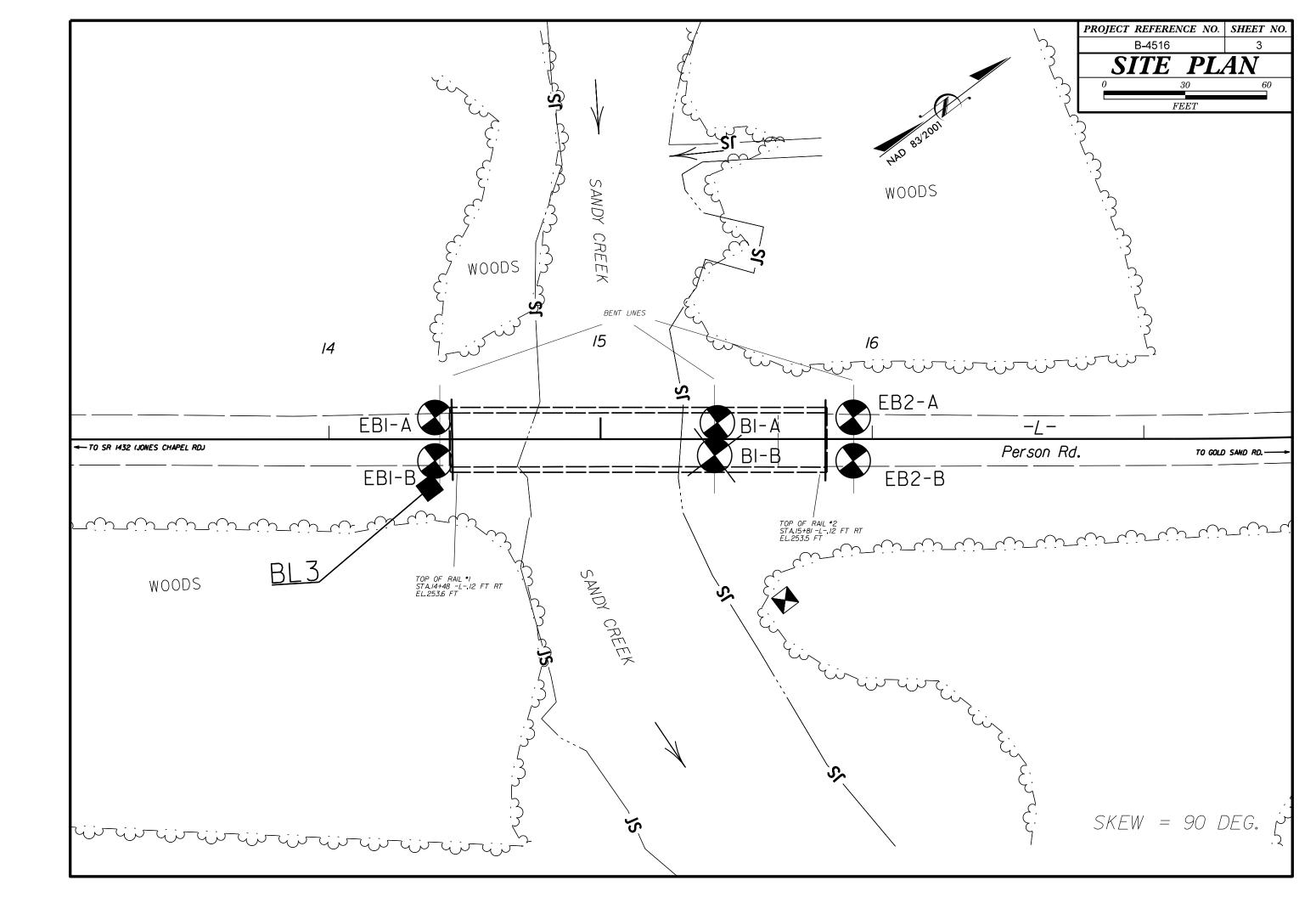
	TERMS AND DEFINITIONS
D. AN INFERRED	ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
SPT REFUSAL. FOOT PER 60	AQUIFER - A WATER BEARING FORMATION OR STRATA.
IS OFTEN	ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
	ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING
N VALUES >	A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.
	ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT
CK THAT CLUDES GRANITE.	WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
CLODES ONHINITE,	CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
	COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM
IF TESTED. C.	OF SLOPE.
MAY NOT YIELD TONE, CEMENTED	CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED
TONE, CEMENTED	BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
	DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
RINGS UNDER	DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE
	HORIZONTAL.
DATINGS IF OPEN, AMMER BLOWS IF	DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE
HINEN DEGNS IN	LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
СК ИР ТО	FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE
L FELDSPAR BLOWS.	SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.
5. IN	FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELT SPACED PARALLEL PLANES.
Y. ROCK HAS	FLUAT - RUCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL PUSITION AND DISCUDDED FROM PARENT MATERIAL.
AS COMPARED	FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
	FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE
ELDSPARS DULL OSS OF STRENGTH	FIELD.
WHEN STRUCK.	JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
	LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO
VIDENT BUT RE KAOLINIZED	ITS LATERAL EXTENT.
INE KHOLINIZED	LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
	MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
E DISCERNIBLE	
F STRONG ROCK ONLY MINOR	PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.
ALUES < 100 BPF	RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
IN SMALL AND	ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF
. SAPROLITE IS	ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE
	RUN AND EXPRESSED AS A PERCENTAGE.
	SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
5 REQUIRES	SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND
LOWS REQUIRED	RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO
	THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
EP CAN BE	<u>SLICKENSIDE</u> - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
ETACHED	STANDARD PENETRATION TEST (PENETRATION RESISTANCE)(SPT) - NUMBER OF BLOWS (N OR BPF) OF
R PICK POINT.	A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL
BLOWS OF THE	WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
504045450	STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY
FRAGMENTS T. SMALL.THIN	TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
	STRATA ROCK QUALITY DESIGNATION (SRQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL
PIECES 1 INCH	LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
ED READILY BY	TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
THICKNESS	BENCH MARK: BL#3 AT II+17.92 -BL-, N:888510.855 E:2235073.439.
4 FEET	ELEVATION: 251.02 FEET
.5 - 4 FEET .6 - 1.5 FEET	
3 - 0.16 FEET	NOTES:
0.003 FEET 0.008 FEET	
0.000 FEEI	
AT, PRESSURE, ETC.	
EEL PROBE;	
PROBE:	
	DATE: 8-15-14

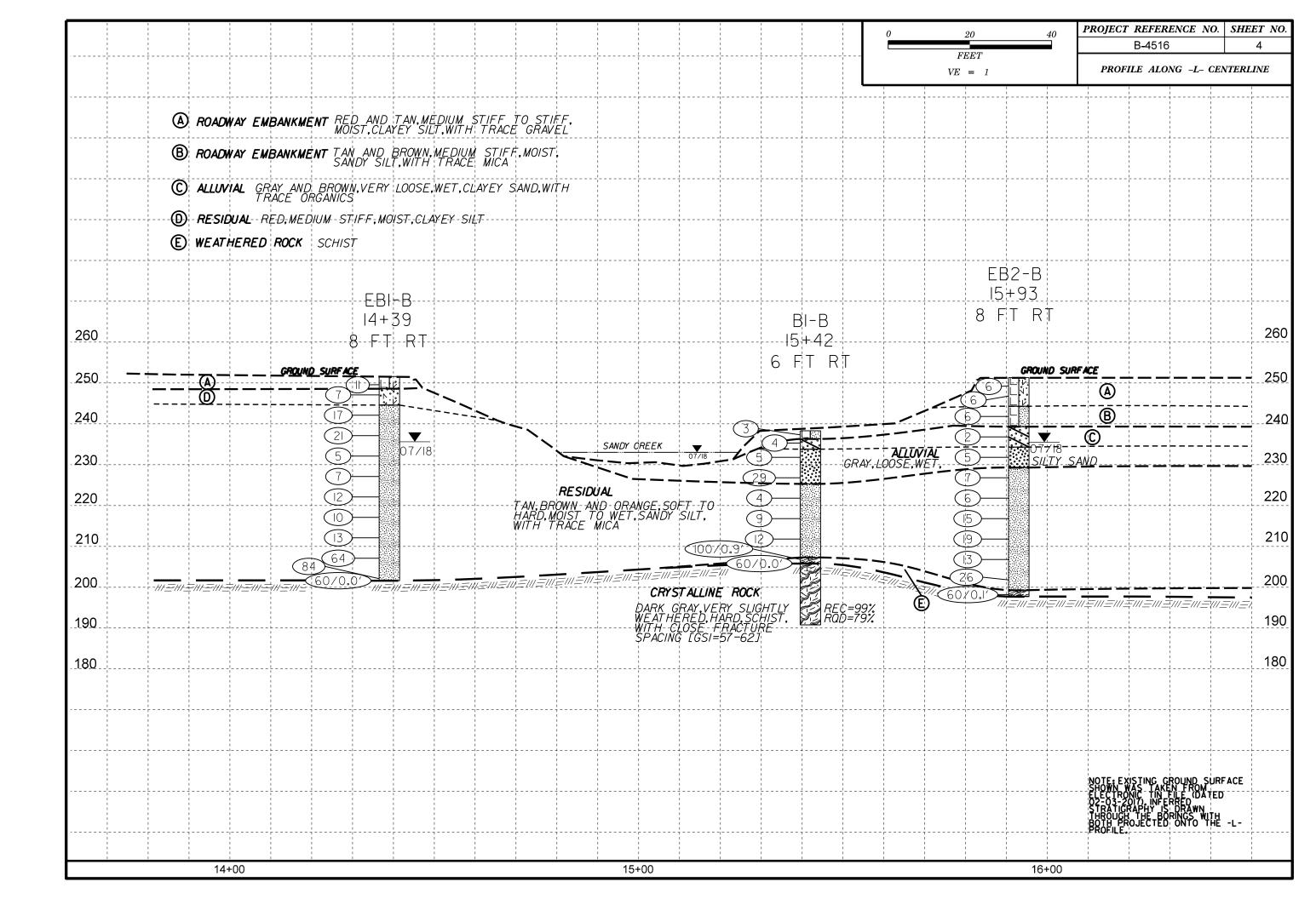
# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION

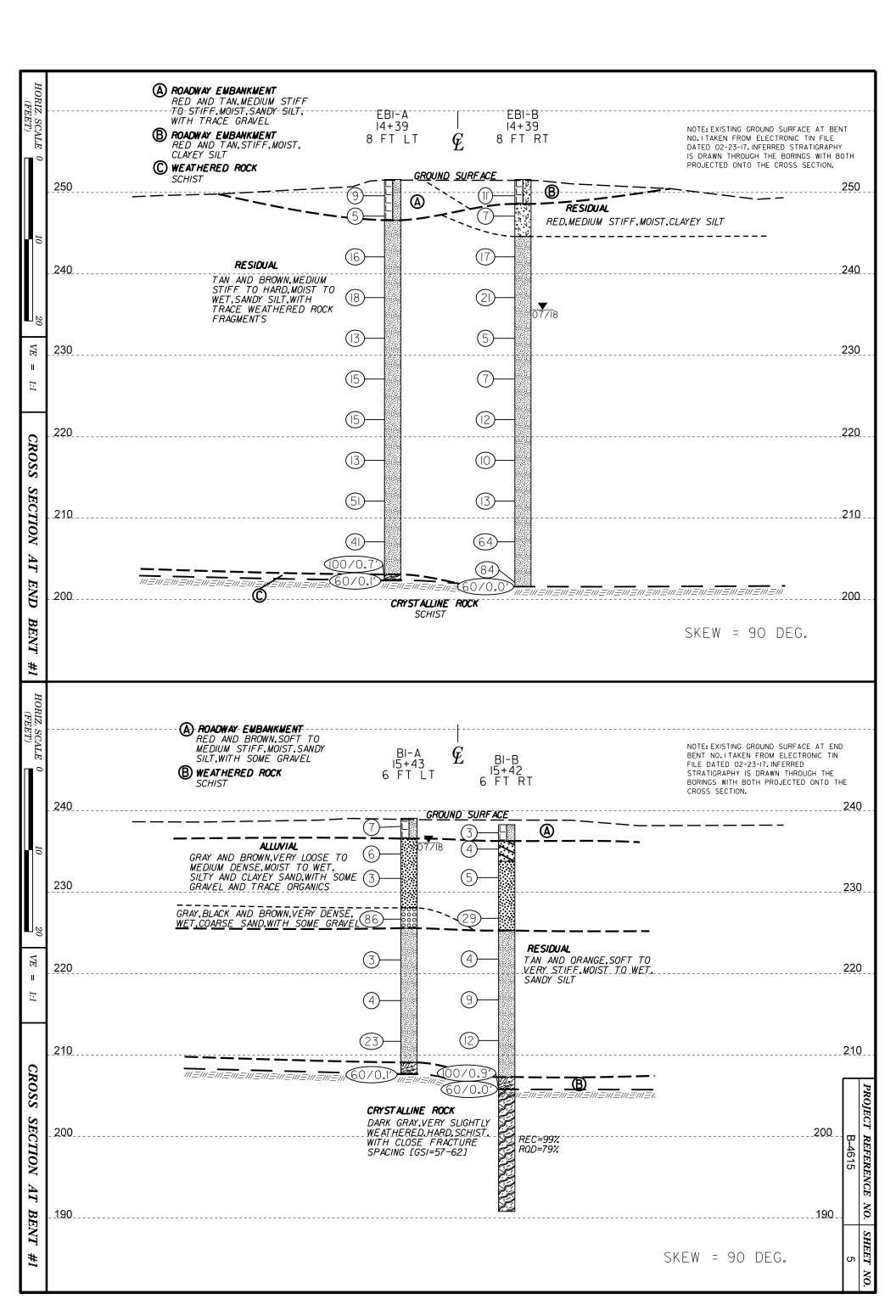
SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

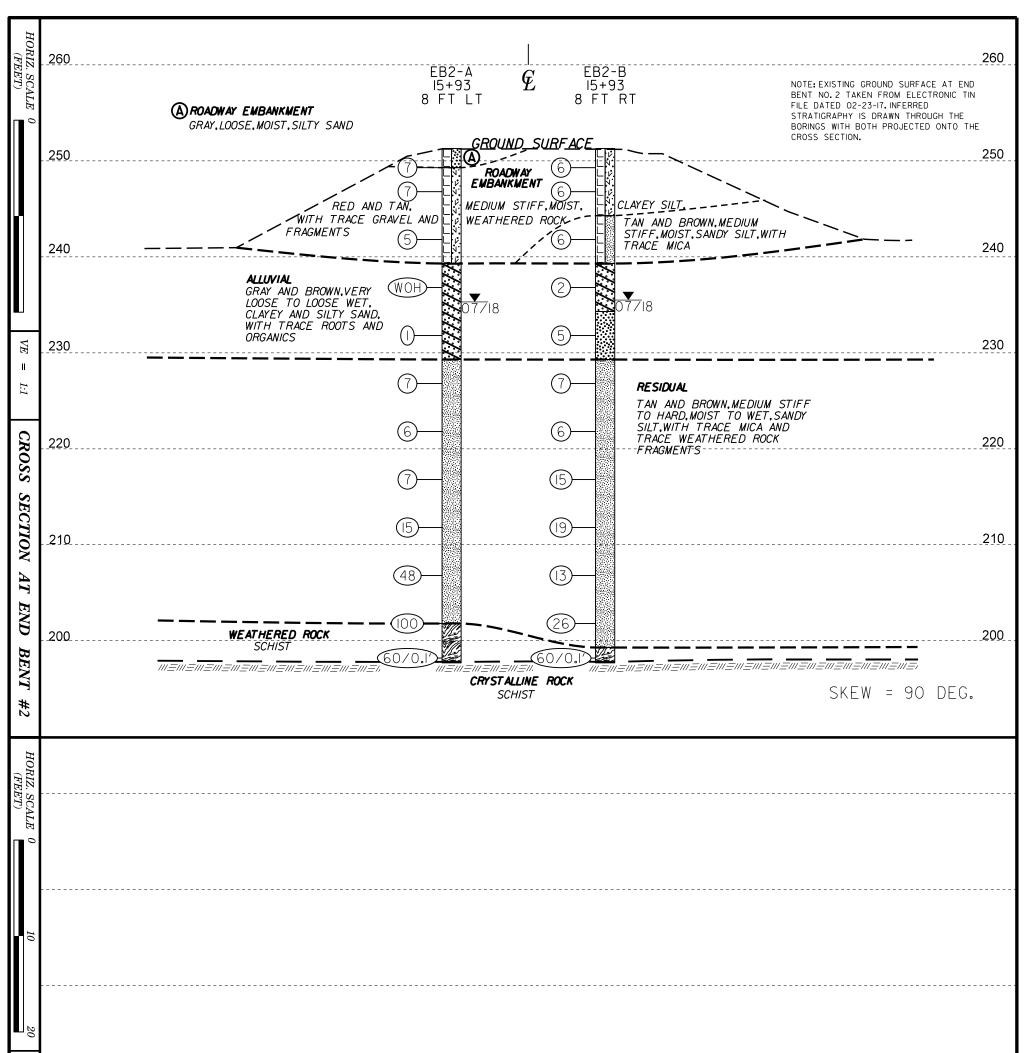
AASHTO LRFD Figure 10.4.6.4-1 $-$ Determination of GSI for Jointed F	Rock Mass (Marı	nos and Hoek,2	2000)			AASHTO LRFD Figure 10.4.6.4–2 $-$ Determination of GSI for Te
GEOLOGICAL STRENGTH INDEX (GSI)FOR JOINTED ROCKS (Hoek and Marinos,2000) From the lithology,structure and surface	faces	staıned		faces	faces Js	GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos. P and Hoek E., 2000) From a description of the lithology, structure and
conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.	VERY GOOD Very rough, fresh unweathered sur	<b>GOOD</b> Rough, slightly weathered, iron sta surfaces	<b>FAIR</b> Smooth, moderately weathered and altered surfaces	POOR Slickensided, highly weathered surf with compact coatings or fillings or angular fragments	<b>VERY POOR</b> Slickensided, highly weathered surf with soft clay coatings or fillings	surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the conditio of the discontinuities and estimate the average valu of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fail poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.
STRUCTURE		REASING SU	•		~	COMPOSITION AND STRUCTURE
INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities	90			N/A	N/A	A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.
BLOCKY - well interlocked un- disturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets		70 60				B. Sand- stone with thin inter-
VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets		5	50			layers of siltstone amounts
BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity			40	30		<b>C, D, E,</b> and <b>G</b> - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to <b>F</b> and <b>H</b> .
DISINTEGRATED - poorly inter- locked, heavily broken rock mass with mixture of angular and rounded rock pieces				20		G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers
LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes	N/A	N/A			10	Into small rock pu     Into small rock pu





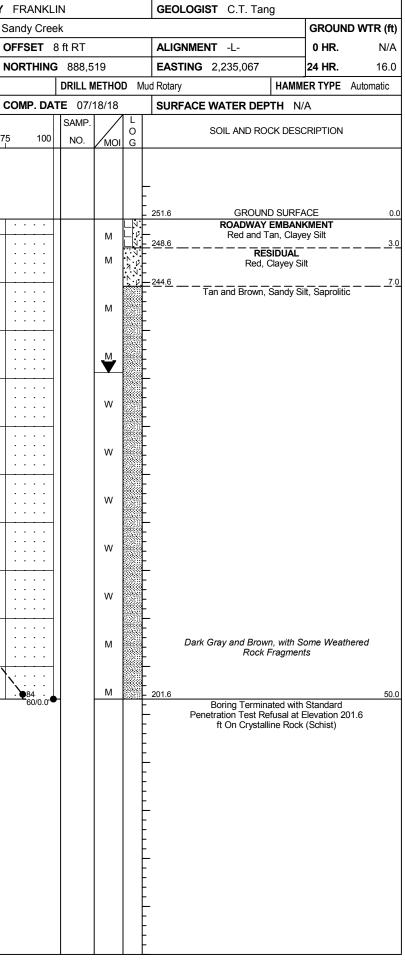






VE = 1:1		
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	B-4615	PROJECT REFERENCE
	6	NO. SHEET NO.

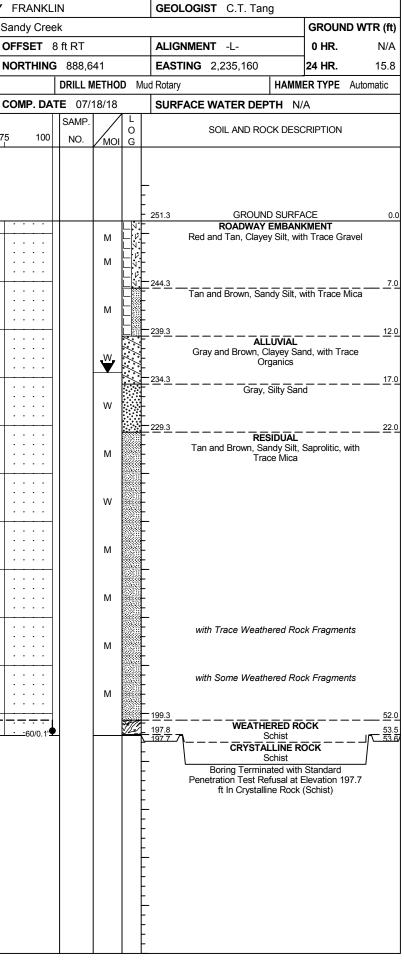
	38400					<b>IP</b> B-45				ry Fran					GEOL	LOGIST C.T. 1	ang	1		<b>S</b> 3840					<b>P</b> B-45			COUNT	
SITE	DESCR	RIPTION	Bric	dge No	b. 52 c	on SR 143	33 (Perso	on Ro	ad) ove	er Sandy (	Creek							GROUND WTR (	t) SIT	E DESCI	RIPTIO	N Brid	lge No	o. 52 o	n SR 14	33 (Perso	on Roa	ad) over	Sa
BORI	ING NO	. EB1-	-A		s	TATION	14+39			OFFSE	T 8 ft L	Γ			ALIG	NMENT -L-		0 HR. N/	A BO	RING NC	). EB1	-В		S	TATION	14+39			OF
COLL	LAR EL	<b>EV.</b> 25	51.6 ft		Т	OTAL DE	PTH 4	9.3 ft		NORTH	ING 88	8,528			EAST	<b>ING</b> 2,235,05	4	24 HR. FIA	D CO	LLAR EL	<b>EV.</b> 2	51.6 ft		Т	OTAL DI	EPTH 50	0.0 ft		NC
DRILL	RIG/HA	MMER E	FF./DA	ATE B	RI8284	CME 300 9	1% 02/26	/2018			DRIL	L MET	THOD	) М	lud Rotary		НАММ	ER TYPE Automatic	DRI	LL RIG/HA	MMER E	EFF./DA	TE BF	RI8284	CME 300	91% 02/26/2	2018		
DRIL	<b>LER</b> J	. Ander	son		S	TART DA	<b>TE</b> 07/	/19/18	3	COMP.	DATE (	)7/19/	/18		SURF	ACE WATER D	<b>EPTH</b> N	Ά	DR	LLER .	I. Ande	rson		S	TART D	<b>ATE</b> 07/ <sup>2</sup>	18/18		cc
LEV	DRIVE ELEV	DEPIR	BLC	ow co	UNT		BLC	OWS PE	ER FOO	Т	SAN	1P. 🔻		L O		SOIL AND	ROCK DES	RIPTION	ELE	/ DRIVE ELEV		H BLC	ow co	UNT		BLO	WS PE	ER FOOT	
(ft)	(ft)	(ft)	0.5ft	0.5ft	0.5ft	0	25	50	0	75	100 NC	). /r		G	ELEV. (fl			DEPTH	(ft)	(ft)	(ft)	0.5ft	0.5ft	0.5ft	0	25	50		75
255																			255		$\perp$								
		ł												ł	_						ł								
	250.6	- 1.0												-100	251.6		UND SURF		0.0	250.6	- 1.0								
250	250.6	T 1.0	2	4	5	<b>→</b> 9						1	мĽ	-8	_	Red and Tan, Sa			250	250.6	<u>+ 1.0</u>	2	4	7		1			+
-	248.1	3.5	1	2	3						.		M L	-8	-					248.1	3.5	2	3	4					.
245		ŧ				<b>•</b> 5			· · · · · ·	· · · · ·		'			- 246.6 -		RESIDUAL		5.0 245		Ŧ				. ( :			· · · · ·	
	243.1	8.5											1000		-	Tan and Brown,	Sandy Silt, v Saprolitic	vith Trace Mica,			+				\.				+
		+ <sup>0.5</sup>	4	8	8	-  · · ·       · · ♥	 16	· · ·	· · · · · ·	· · · · ·		1	М		-					243.1	+ <sup>0.5</sup>	3	6	11		• · · ·		· · · · ·	:
240		‡				· · ·		• •		· · · ·	•				-				240		‡					1	•••		·
	238.1	13.5							· · · · · ·	: : : :	:				-					238.1	13.5			40		1		· · · · ·	-
		ŧ	6	7	11		●18 · ·	· · ·	· · ·	· · · · ·			М		-						ŧ	5	9	12		• • • • • • • • • • • • • • • • • • •		· · · ·	-
235	-	ŧ				<del>j</del>									_				235		Ŧ								+
	233.1	18.5	4	5	8	-  ·· <b>/</b>			· · ·		.		м		-					233.1	18.5	2	2	3	. / ●5				
230		Ŧ													-				230		Ŧ								.
	228.1	23.5				· · ł					•		No.		-	with Trace We	athered Ro	ck Fragments		228.1	T 23.5								
		+	6	7	8	<b>  ::∳</b>			· · · · · ·	· · · · ·	.	1	М		-						-	2	2	5	· · · · · · · · · · · · · · · · · · ·			· · · · ·	
225	· -	‡					· · ·	•••		· · · ·	·		0.000		-				225		‡						•••		⊥.
	223.1	28.5	6	6	9		· · · ·	· · ·	· · · · · ·	· · · · ·	·				-					223.1	28.5	3	4	8	• \ •	· · ·		· · · · ·	-
		t		0	9	::•	15	· · ·	· · · ·	·   · · · ·   · · ·			М		-						ŧ		4	0	· • • 1 	2		· · · ·	
220	-	±													_				220		<u>+</u>								+
-	218.1	33.5	3	5	8	-   · · <b>/</b> ·		•••	· · ·	· · · · ·			м		-					218.1	<u> </u>	2	4	6					
215		ł					- I								-				215		+								.
	213.1	38.5						· · · ·			-				-					213.1	T 38.5								
		Ŧ	8	20	31				<b>5</b> 1 · ·			1	М		-						Ŧ	3	5	8		13.			
10		Ŧ						/	· · ·						-				210		Ŧ								+-
-	208.1	43.5	10	14	27			·/·	· · · ·		.	Ι,	м		-	with Some We	athered Ro	ck Fragments		208.1	43.5	3	20	44				· · · · ·	-
205		‡						<b>4</b> 1	· · · · · ·	· · · · ·	•	'	IVI		-				205		‡								
200		+						1.			-		1000		- 203 1			4		203.1	+ + 48.5								$\mathbf{x}$
	202.4	48.5 49.2			<u> </u>			<u>–</u> –	· <del>-</del>	100/			50	977	203.1 202.4 202.3	wea			3.5 9.2 9.3	203.1	т	8	14	70			· · · ·	· · · · ·	
		t	60/0.1							60/	0.1'			ł		CRYS	Schist				1	60/0.0	1						
		ŧ												ŀ	-	Boring Terr	Schist minated with	Standard			ŧ								
		ŧ												ł	-	Penetration Test	t Refusal at I	Elevation 202.3			ŧ								
	-	+												ł		it in Crys	talline Rock	(Schist)			+								
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WBS	38400	.1.FD2			Т	<b>P</b> B-45′	16	C	COUNT	Y FF	RANKL	IN			GEOLOG	GIST C.T	. Tang		
SITE	DESCR	IPTION	Brid	ge No	. 52 o	n SR 143	3 (Pers	on Roa	ad) over	r Sano	dy Cree	k						GROUN	D WTR (ft)
BOR	ING NO.	B1-A			S	TATION	15+43			OFF	SET (	6 ft LT			ALIGNM	ENT -L-		0 HR.	N/A
COL	AR ELE	<b>EV.</b> 23	39.1 ft		Т	OTAL DE	<b>PTH</b> 3	1.5 ft		NOF	RTHING	888,6	10		EASTING	<b>3</b> 2,235,1	118	24 HR.	3.0
DRILI	RIG/HAI	MMER E	FF./DA	TE BF	RI8284 (	CME 300 9	1% 02/26	/2018		1		DRILL N	IETHO	D Mu	ud Rotary				Automatic
	LER J.					TART DA				CON		<b>FE</b> 07/ <sup>-</sup>			1 .				
ELEV (ft)		DEPTH (ft)		0W COI 0.5ft	UNT				R FOOT		100	SAMP. NO.	моі	L O G	ELEV. (ft)		D ROCK DE		DEPTH (f
	ELEV (ft) 239.1 		L								100				- 239.1 - 236.6 	GF ROAD Red and Br Gray and B Tray, Black a Tan, Tan, Tan,	ROUND SUR WAY EMBA own, Sandy Gravel ALLUVIAI rown, Silty S: Organics Ind Brown, C Gravel RESIDUA Sandy Silt, S Sandy Silt, S Schist YSTALLINE Schist erminated wi	FACE INKMENT Silt, with Som and, with Trad oarse Sand, v Carse Sand, v Cars	0.

		BURELUG	·				
WBS 38400.1.FD2	TIP B-4516 C	COUNTY FRANKLIN	GEOLOGIST C.T. Tang	WBS 38400.1.FD2	TIP B-4516 COUN	TY FRANKLIN	GEOLOGIST C.T. Tang
SITE DESCRIPTION Bridge N	No. 52 on SR 1433 (Person Roa	ad) over Sandy Creek	GROUND WTR (ft)	SITE DESCRIPTION Bridge No. 5	52 on SR 1433 (Person Road) ov	er Sandy Creek	GROUND WTR (f
BORING NO. B1-B	STATION 15+42	OFFSET 6 ft RT	ALIGNMENT -L- 0 HR. N/A	BORING NO. B1-B	STATION 15+42	OFFSET 6 ft RT	ALIGNMENT -L- 0 HR. N/A
COLLAR ELEV. 238.3 ft	TOTAL DEPTH 47.5 ft	NORTHING 888,602	<b>EASTING</b> 2,235,128 <b>24 HR.</b> Caved	COLLAR ELEV. 238.3 ft	TOTAL DEPTH 47.5 ft	NORTHING 888,602	EASTING 2,235,128 24 HR. Caved
DRILL RIG/HAMMER EFF./DATE	BRI8284 CME 300 91% 02/26/2018	DRILL METHOD MU	Id Rotary HAMMER TYPE Automatic	DRILL RIG/HAMMER EFF./DATE BRI8	3284 CME 300 91% 02/26/2018	DRILL METHOD	Iud Rotary HAMMER TYPE Automatic
DRILLER J. Anderson	<b>START DATE</b> 07/17/18	COMP. DATE 07/17/18	SURFACE WATER DEPTH N/A	DRILLER J. Anderson	START DATE 07/17/18	COMP. DATE 07/17/18	SURFACE WATER DEPTH N/A
ELEV DRIVE DEPTH BLOW C				CORE SIZE NQ	TOTAL RUN 15.0 ft		
(ft) ELEV (ft) 0.5ft 0.5ft			SOIL AND ROCK DESCRIPTION ELEV. (tt) DEPTH (tt)				
				ELEV RUN ELEV (ft) (ft) (ft) DEPTH RUN (ft) DRILL RATE (Min/ft)	RUN REC. RQD (ft) (ft) NO. (ft) (ft) % %		DESCRIPTION AND REMARKS
240				205.8			Begin Coring @ 32.5 ft
238.3 0.0			- GROUND SURFACE 0.0	205 205.8 32.5 1.0 6:46/1.0	) (0.9) (0.6) (14.8) (11.8	B)205.8 Hard, Very Slightly	CRYSTALLINE ROCK 3
<b>†</b>   1   1	2 3	···· ···	ROADWAY EMBANKMENT		(3.9) $(3.9)$ $(2.4)$ $(3.9)$ $(2.4)$		y Weathered, Dark Gray, Schist, with Close Fracture [GSI = 57-62]
236.3 T 2.0 235 WOH 1		· · · · ·   · · · ·       M	Red and Brown, Sandy Silt 2.0	200.8 37.5 4:02/1.0 2:56/1.0			
232.8 5.5	1		233.8 Gray and Brown, Clayey Sand, with Trace 4.5 Organics		) (5.0) (4.3) ) 100% 85%		
232.8 + 5.5 4 2	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	м	Gray, Silty Sand, with Some Gravel	5:00/1.0	100% 85% RS-1		
230			-				
227.8 + 10.5 + 10.5					0 (5.0) (4.5) 0 100% 90%		
	) 9	· · · ·   · · · ·     M	225.3 13.0	3:57/1.0 4:59/1.0		190.8	
225				190.8 47.5 4:15/1.0			ed at Elevation 190.8 ft In Crystalline Rock (Schist)
222.8 15.5 2 2	2	· · · · ·   · · · ·       M	Orange and Tan, Sandy Silt, Saprolitic				
220	$ =  \left  \left  \P_{1}^{4} \cdots \right  \cdots \right  $						
217.8 + 20.5	1	· · · ·   · · · ·	-				
$\frac{217.8 + 20.5}{+}$ 3 4	$5$ $1 \cdot 1 \cdot 2 \cdot 1 \cdot $						
215			_				
212.8 - 25.5							
		· · · ·   · · · ·					
210 —			-				
207.8 30.5	2 88/0.4		207.3 31.0				
205 205.8 32.5 60/0.0			205.8 WEATHERED ROCK 32.5			I F	
			CRYSTALLINE ROCK				
			Hard, Very Slightly Weathered, Dark Gray, Schist, with Close Fracture				
200			[REC=99%, RQD=79%] - [GSI = 57-62]				
		· · · ·   · · · ·					
195			-				
	1 11 1						
			190.8 47.5				
			<ul> <li>Boring Terminated at Elevation 190.8 ft In Crystalline Rock (Schist)</li> </ul>				
			_				
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		F					
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			-			-	
‡							
		F					

DBLL B2         DBLL B1         DBLL B1         DBLL B2         DBLL B2 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>URE</th><th></th><th></th><th></th><th></th><th></th><th></th><th>-</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>												URE							-										
BORNE OD         FIATURE 1         OPFRET 85.1         FIATURE 1         DORME 000         BORNE 000         <																GEOL	OGIST C.T. Tang	- 1											
COLLAG ELEV. 25:0         OTAL DEPTH 53:0         Destination 498:0         Destination 220:17         Parker. 60         OCLAG ELEV. 25:0         OTAL DEPTH 53:0         Destination 220:17           DBULLBOINMENT FORCE SUBJECTIONE SUBJECTION					dge N					n Ro	ad) ove							`					lge No					toad) ov	
DBLL B2         DBLL B1         DBLL B1         DBLL B2         DBLL B2 <t< th=""><th>BOR</th><th>ING NO</th><th><b>).</b> EB2</th><th>-A</th><th></th><th>s</th><th>STATI</th><th>ION 1</th><th>15+93</th><th></th><th></th><th>OFFSET</th><th>8 ft LT</th><th></th><th></th><th>ALIGN</th><th>IMENT -L-</th><th>0 HR. N/A</th><th>BO</th><th>RING NO</th><th><b>).</b> EB2</th><th>-В</th><th></th><th>S<sup>-</sup></th><th>TATIO</th><th><b>N</b> 15</th><th>5+93</th><th></th><th>OF</th></t<>	BOR	ING NO	<b>).</b> EB2	-A		s	STATI	ION 1	15+93			OFFSET	8 ft LT			ALIGN	IMENT -L-	0 HR. N/A	BO	RING NO	<b>).</b> EB2	-В		S <sup>-</sup>	TATIO	<b>N</b> 15	5+93		OF
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	COL	LAR EL	. <b>EV</b> . 2	51.3 f	t	T	ΌΤΑ	L DEP	<b>TH</b> 53	3.6 ft		NORTHI	NG 888,6	651		EAST	NG 2,235,147	<b>24 HR.</b> 16.0	COI	LAR EL	<b>EV.</b> 2	51.3 ft		т	OTAL	DEPT	<b>H</b> 53.6	ft	NC
Dery       BLOW COUNT       BLOWS PER-EXCI       SOLE AD ACCLUDIGATION       BLOWS PER-EXCI         250	DRILI	L RIG/HA	MMER E	FF./D	ATE E	BRI8284	CME	300 91%	% 02/26/2	2018			DRILL	METHO	OD	Mud Rotary	HAN	IMER TYPE Automatic	DRII	L RIG/HA	MMER E	EFF./DA	TE BF	RI8284 (	CME 30	0 91%	02/26/2018	3	
(i) (ii) (ii) (iii) (iiii) (iii) (i	DRIL			son		S	TAR	T DAT	<b>E</b> 07/1	18/18	}	COMP. D	ATE 07	/18/18	3	SURF	ACE WATER DEPTH	N/A	DRI			rson		S	TART	DATE	07/18/	18	CC
(i) (ii) (ii) (iii) (iiii) (iii) (i	ELEV	DRIVE	DEPTH	' <b> </b>	_	-								· 🔻			SOIL AND ROCK DE	SCRIPTION	ELE	/ DRIVE	DEPTH	·——							
201         201         1.0         0         0         25/3         0.0         00000 SURACS         0           201         3.5         3         4         1<	(ft)		(ft)	0.5f	t 0.5f	t 0.5ft	0		25	50	)	75 10	0 NO.	Имо					(ft)		(ft)	0.5ft	0.5ft	0.5ft	0	2	5	50	75
201         201         1.0         0         0         25/3         0.0         00000 SURACS         0           201         3.5         3         4         1<	ł																												
280       203       10       0 <td>255</td> <td></td> <td>+</td> <td></td> <td>L</td> <td></td> <td></td> <td>255</td> <td></td> <td><math>\downarrow</math></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	255		+													L			255		$\downarrow$								
280       203       10       0 <td>ł</td> <td></td> <td>ŧ</td> <td></td> <td>È</td> <td></td> <td></td> <td></td> <td></td> <td>‡</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	ł		ŧ													È					‡								
3242         4         3         4         3         3         4         3         3           326         4         3         4         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3 <td>050</td> <td>250.2</td> <td>+ 10</td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td>· · ·</td> <td>•••</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>251.3</td> <td></td> <td></td> <td></td> <td>250.2</td> <td>+ 10</td> <td></td> <td></td> <td> '</td> <td>╫╌</td> <td><del></del></td> <td></td> <td><del></del></td> <td></td>	050	250.2	+ 10		_				· · ·	•••						251.3				250.2	+ 10			'	╫╌	<del></del>		<del></del>	
282       3       3       4       4       5       5       2       2       3       4       5       4       5       4       4       6       6       7	250		<u> </u>	6	3	4	11	7.	+					м		il .	Gray, Silty S	and <u>2</u>	0 250	200.3	Ŧ	4	3	3				+	
280       2		247.8	- 3.5	3	3	4		<b>I</b>	· · ·	· ·				М						247.8	<u> </u>	2	2	4				· · ·	:
202.6       8.6       - </td <td>245</td> <td></td> <td>±</td> <td></td> <td></td> <td></td> <td></td> <td>T'</td> <td></td> <td>245</td> <td></td> <td>ŧ</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>•</td>	245		±					T'											245		ŧ								•
20       2       2       3       4       -		242 8	1 85				į		· ·											242 8	1 85							· · ·	
220 227.2 13.5 Work Work Work 1 228 228 228 228 228 228 228 22			1	2	2	3	] ∳	5		· ·		.		м							1	1	2	4	6			· · ·	:
222       13.5       WOH       WOH       WOH       WOH       WOH       WOH       22.5       1.1       1 <td>240</td> <td></td> <td>Ŧ</td> <td></td> <td>2<u>39.3</u></td> <td></td> <td>12</td> <td>0 240</td> <td>-</td> <td>Ŧ</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>+</td> <td>-+-</td>	240		Ŧ													2 <u>39.3</u>		12	0 240	-	Ŧ							+	-+-
225     185     222     185     223     225     225     227.8     235     2     2     3     4       220     227.8     22.5     2     2     5     1 <td></td> <td>237.8</td> <td>13.5</td> <td>WO</td> <td>H WOH</td> <td>1 WOH</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</td> <td><u>*</u></td> <td>Brown and Gray, Clayey</td> <td>L Sand, with Trace</td> <td></td> <td>237.8</td> <td>13.5</td> <td>1</td> <td>1</td> <td></td> <td><math>\left\  \frac{1}{2} \right\ </math></td> <td></td> <td></td> <td></td> <td>•</td>		237.8	13.5	WO	H WOH	1 WOH									~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<u>*</u>	Brown and Gray, Clayey	L Sand, with Trace		237.8	13.5	1	1		$\left\  \frac{1}{2} \right\ $				•
228     135     WOH     WOH     1	235		Ŧ				•							Ŭ			Roots		235		Ŧ				$\left  \begin{array}{c} \P^2 \end{array} \right $				
230       221       23.5       2       2       5       -<		232.8	T 185				$ \Gamma$								/./.	\$ 				232.8	T 195				1.				
220		202.0	+ 10.5	WO	H WOH	1 1	₁					.		w	/./.	أحثوا				202.0	+ 10.5	2	2	3	∳₅.				
2213       233       2       2       3       4       7       12         2228       28.5       2       3       4       7       12         220       217.8       33.5       2       2       5       1	230		Ŧ					· · ·							/./.	229.3		2	0 230	-	Ŧ							+	
220 2228 28.5 2228 28.5 220 227.8 20 20 20 20 20 20 20 20 20 20		227.8	23.5	2	- 2	5	11											L		227.8	23.5	2	3		-] -    -] -				:
228       29       20       20       218       38       48       7       12       11       16       17       18       18       18       18       18       18       18       18       18       18       19       19       19       19       18 <t< td=""><td>225</td><td></td><td>Ŧ</td><td></td><td></td><td></td><td></td><td>∳7 · · •</td><td></td><td>•••</td><td></td><td>•   • • • •</td><td></td><td></td><td></td><td>- -</td><td></td><td>· •</td><td>225</td><td></td><td>ŧ</td><td></td><td>5</td><td>-</td><td><b>    •</b><sup>7</sup></td><td>, </td><td></td><td></td><td>:</td></t<>	225		Ŧ					∳7 · · •		•••		•   • • • •				- -		· •	225		ŧ		5	-	<b>    •</b> <sup>7</sup>	, 			:
220       2       3       3       4       6       9         217.8       33.5       - <t< td=""><td></td><td></td><td>‡</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td>8<b>-</b></td><td></td><td></td><td></td><td></td><td>‡</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></t<>			‡						1							8 <b>-</b>					‡							<u> </u>	
200 217.8 33.5 217.8 35.5 217.8 35.5 217.8 35.5 217.8 35.5 217.8 35.5 217.8 35.5 217.8 35.5 217.8 35.5 217.8 35.5 2		222.8	<u>+ 28.5</u> +	2	3	3		6 · · ·	· ·   · ·	•••				w		8– 8–				222.8	<u>+ 28.5</u> +	2	2	4		,			
215       2       2       5       1	220		‡					· · ·	· ·	• •						8 <b>-</b>			220	_	‡					· · ·	· · · ·	<u> </u>	·   ·
215       212.8       38.5       4       6       9         210       207.8       43.5       -		217.8	33.5					 								8- 8-				217.8	33.5				 	λ. I		· · ·   · · ·	:
210       212.8       38.5       4       6       9	215		‡	2	2	5	11.			· ·				M		8- 8-			215		‡	3	6	9		15	· · · ·	· · · ·	:
210       4       6       9	215		‡				11	<u>ì</u> .	1							8 <b>-</b> -			215	-	‡							<u> </u>	
207.8       43.5		212.8	<u>+ 38.5</u> +	4	6	9	<del> </del>  :			· ·	· · · · ·	·   · · · · ·		м						212.8	<u>+ 38.5</u> +	4	7	12	1 : :		· · · · 	· · · ·	•
205       11       16       32	210		‡				L:			•••						- -			210	_	‡						· · · ·	<u> </u>	•
205     -<		207.8	43.5				<u>  :</u>	· · ·												207.8	43.5				] ::		· · · ·	· · · ·	•
202.8       48.5       18       25       75 <ul> <li></li></ul>	205		‡	11	16	32	11		· ·   · ·	· • • • • • • • • • • • • • • • • • • •	<sup>18°</sup> · · · ·	.   .		M					205		‡	4	5	8		<b>(</b> 13	· · · ·	· · · ·	:
198.3       53.0			‡						+							- -			205		‡					\		+	
198.3       53.0		202.8	<u>+ 48.5</u> +	18	25	75			· ·   · ·	::¦	 <u></u>			м		201.8			5	202.8	<u>+ 48.5</u> +	14	18	8	1	۰ <b>۱</b>	26 • • •	· · · ·	•
198.3       53.0	200		‡				_:		· ·	• •		100/1						ROCK	200	_	‡					· · ·	<b>F</b>	<u> </u>	·
Boring Terminated with Standard Penetration Test Refusal at Elevation 197.7 ft In Crystalline Rock (Schist)		198.3	53.0	60/0	1			· · · · · ·	· · ·	· · · ·			1			197.8		53	5	198.3	53.0	60/0 1'	,			 	· <del>-</del>	<u></u>	
			ŧ	00/0.	<u>'</u>												CRYSTALLINE Schist		6/		‡	00/0.1	1						
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UNCONFINED COMPRESSIVE STRENGTH OF INTACT ROCK CORE SPECIMEN ASTM D7012

WBS No.:	38400.1.FD2
TIP No.:	B-4516
County:	Franklin

Test Date: 7/23/2018 Tested By: J. Evans

Description: Bridge No. 52 on SR 1433 (Person Road) over Sandy Creek

Test No.	1		
Boring ID	B1-B		
Station	15+42		
Sample ID	RS-1		
Sample Depth, ft	39.3		
Core Length #1, in.	4.032		
Core Length #2, in.	4.041		
Core Length #3, in.	4.040		
Avg. Core Length, in.	4.038		
Core Dia. #1, in.	1.967		
Core Dia. #2, in.	1.967		
Avg. Core Dia., in.	1.967		
Length/Dia. Ratio	2.05		
X-Sectional Area, in <sup>2</sup>	3.04		
Weight, lb	1.22		
Unit Weight, pcf	171.75		
Break Type	2		
Load at Failure, lb	16,390		
Correction Factor	1.00		
Comp. Strength, psi	5,391		
Comp. Strength, ksf	776		

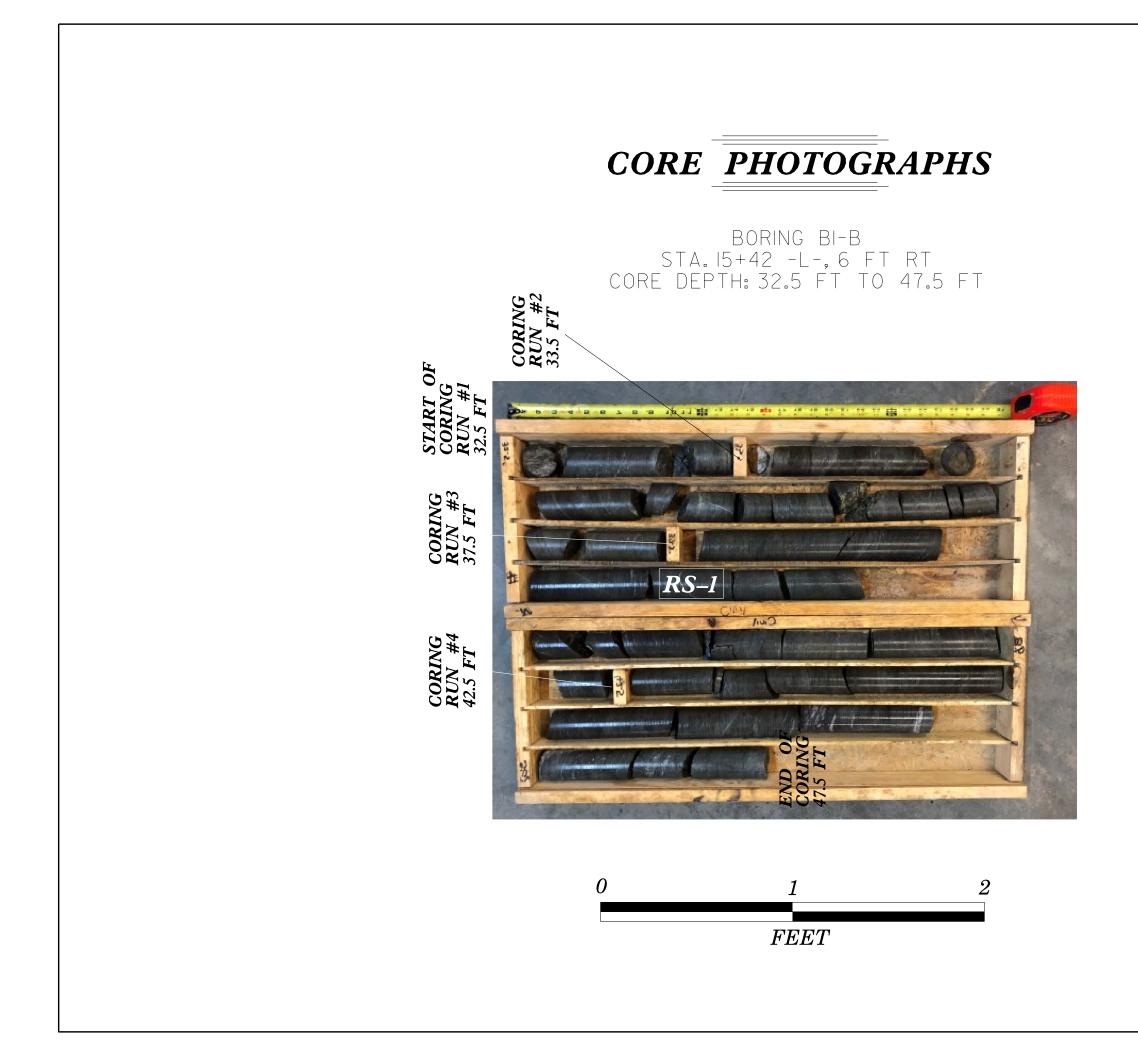
Rock Descriptions:

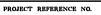
Test 1 : Dark Gray, Very Slight Weathered, Hard, Schist, with Close Fracture Spacing

Break Types:













PHOTOGRAPH NO.1.: VIEW LOOKING NORTH.





DATE: 9-15-14