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REFERENCE

SEE SHEET 2A FOR PLAN SHEET LAYOUT AT TIME OF INVESTIGATION

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<u>LINE</u> -L- -LI- -YIREV-	<u>STATION</u> 10+00-43+69.04 10+00-15+28.38 10+00-25+46.29	<u>PLAN</u> 4-6 6 4	<u>PROFILE</u> 7-9 10 10
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SOIL LABORATORY RESULTS

26-27

STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS** GEOTECHNICAL ENGINEERING UNIT

ROADWAY SUBSURFACE INVESTIGATION

COUNTY JOHNSTON

PROJECT DESCRIPTION NOVO NORDISK ACCESS FROM SR 1905 (GORDON ROAD) TO PROPOSED NOVO NORDISK SITE

INVENTORY

NIA OIEC Ň

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STATE PROJECT REFERENCE NO. STATE SHEETS NO. 30 N.C R-5769 1

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY. PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOLI TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT 1991 707-6860. THE SUBSIFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

CENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSUFFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSUFFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DECREE OF RELIBULITY INHERENT IN THE SUBSUFFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THES SUBJFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THES WATER LEVELS OR SOL MOISTURE CONDITIONS MAY VARY CONSDERABLY WITH THE ACCOMPING OL CUNDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CALITORIED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPHIONO OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONSTRUCTIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDENSION OR FOR AN THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

NOTES:

- TES: THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N.C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT. BY HAVING REDUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

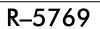
PERSONNEL TURNAGE, J. R. EKLUND, M.A. LEE, S. *LEE*, *B*. *C*. ALEXANDER, M. J. INVESTIGATED BY TERRACON CONSULTANTS FIELDS, W.D. DRAWN BY ALEXANDER, M. J. CHECKED BY SUBMITTED BY TERRACON CONSULTANTS JUNE 2016 DATE Docusigned by: Matthew J. Alexander OFBQRAREAPOICE A RO/ OFESSION T SEAL 040231 ALL J. ALL IN 8/22/2016 SIGNATURE DATE DOCUMENT NOT CONSIDERED FINAL UNLESS ALL SIGNATURES COMPLETED

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

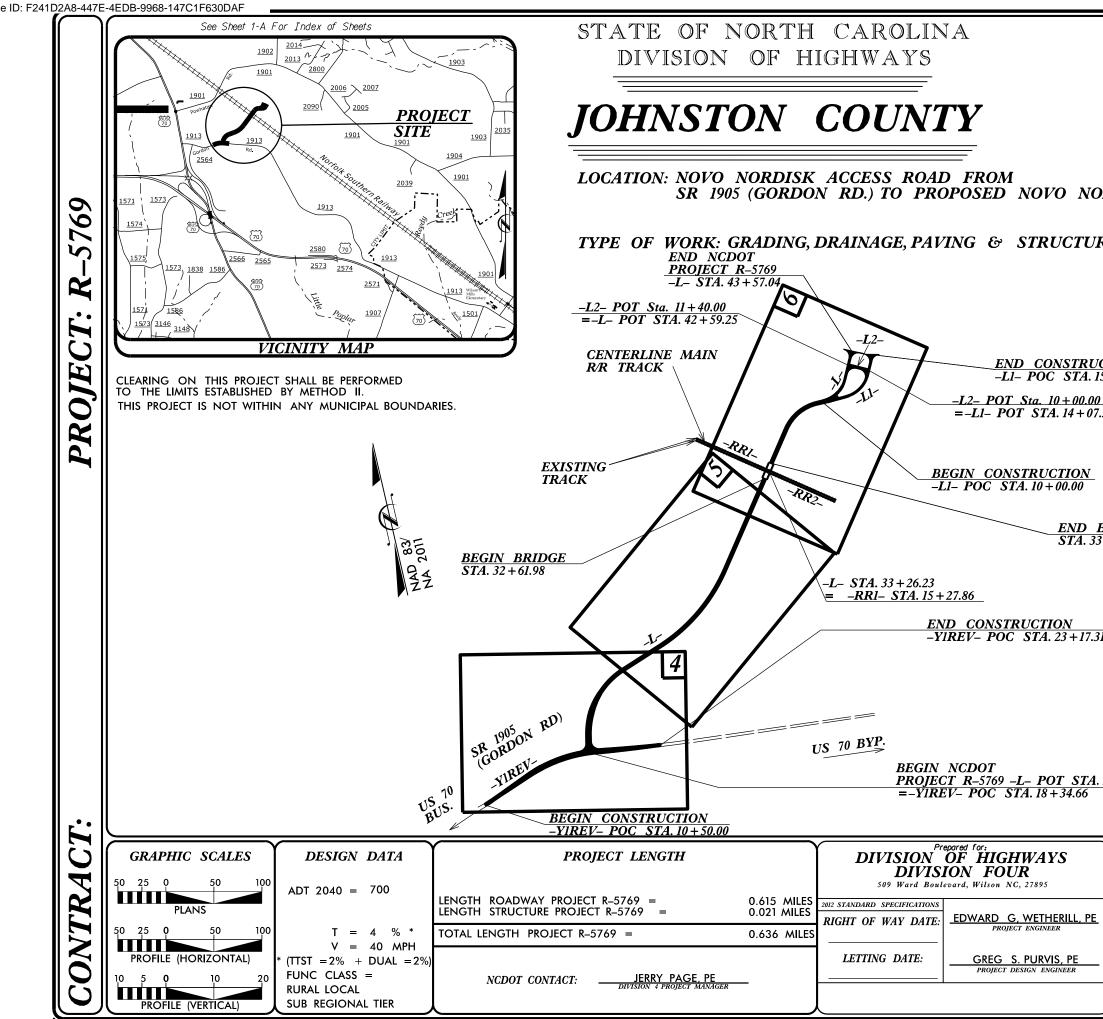
SOIL DESCRIPTION	GRADATION	ROCK DESCRIPTION
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM 01586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM, BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING;	WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.	HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTE ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD VIELD SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0,I BLOWS IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK
CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE,	ANGULARITY OF GRAINS	REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:
VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6	THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.	WEATHERED NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT
SOIL LEGEND AND AASHTO CLASSIFICATION	MINERALOGICAL COMPOSITION	ROCK (WR) 100 BLOWS PER FOOT IF TESTED.
GENERAL GRANULAR MATERIALS SILT-CLAY MATERIALS ORGANIC MATERIALS CLASS. (≤ 35% PASSING *200) (> 35% PASSING *200) ORGANIC MATERIALS	MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC.	CRYSTALLINE FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC RO ROCK (CR) FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC RO
GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5	ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.	
CLASS. A:1-9 A-1-6 A-2-4 A-2-5 A-2-6 A-2-7 A-7-6 A-3 A-6, A-7	COMPRESSIBILITY SLIGHTLY COMPRESSIBLE LL < 31	NON-CRYSTALLINE SEDIMENTARY ROCK THAT WOULD YELLD SPT REFUSAL IN ROCK (NCR)
	MODERATELY COMPRESSIBLE LL = 31 - 50 HIGHLY COMPRESSIBLE LL > 50	COASTAL PLAIN COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT SEDIMENTARY ROCK SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDS
7. PASSING •10 50 MX GRANULAR SILT-	PERCENTAGE OF MATERIAL	(CP) SHELL BEDS, ETC.
40 30 MX 50 MX 51 MN *200 JB MX 25 MX 10 MX 35 MX 35 MX 35 MX 36 MN 36 MN 36 MN 36 MN 36 MN	GRANULAR SILT - CLAY	WEATHERING
MATERIAL PASSING *40 LL 40 MX 41 MN 40 MX 41 MN 40 MX 41 MN 40 MX 41 MN 10 MX 11 MN 10 MX 11 MN 10 MX 11 MN 10 MX 11 MN	ORGANIC MATERIAL SOILS OTHER MATERIAL TRACE OF ORGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10% LITTLE ORGANIC MATTER 3 - 5% 5 - 12% LITTLE 10 - 26% MODERATELY ORGANIC 5 - 10% 12 - 26% SOME 20 - 35% HIGHLY ORGANIC 5 - 10% 12 - 26% SOME 20 - 35%	FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING, ROCK I HAMMER IF CRYSTALLINE. VERY SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY CC (V SLI) CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER H
PI 6 MX NP 10 MX 10 MX 11 MN 11 MN 10 MX 10 MX 11 MN 11 MN MODERATE OPENAL	GROUND WATER	OF A CRYSTALLINE NATURE.
GROUP INDEX Ø Ø Ø 4 MX 8 MX 12 MX IG MX NO MX AMOUNTS OF ONOHALC SOILS USUAL TYPES STONE FRAGS. FINE SILTY OR CLAYEY SILTY CLAYEY MATTER ORGANIC SOILS SOILS	✓ WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING ✓ STATIC WATER LEVEL AFTER 24 HOURS	SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO RO((SLI.) I INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOLD ROCKS SOME OCCASIONAL CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER
MATERIALS SANU	∇PW PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA	MODERATE SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS (MOD.) GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLA'
GEN. RATING EXCELLENT TO GOOD FAIR TO POOR POOR UNSUITABLE	Olle Spring or seep	DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH WITH FRESH ROCK.
PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ;PI OF A-7-6 SUBGROUP IS > LL - 30		MODERATELY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL F
	MISCELLANEOUS SYMBOLS	SEVERE AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE L((MOD. SEV.) AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND V
PRIMARY SOIL TYPE COMPACTNESS OR CONSISTENCY RANCE OF STANDARD PENETRATION RESISTENCE RANCE OF UNCONFINED COMPRESSIVE STRENGTH (N-VALUE) CENEDALUX VERY LOOSE < 4	ROADWAY EMBANKMENT (RE) 25/825 DIP & DIP DIRECTION WITH SOIL DESCRIPTION OF ROCK STRUCTURES	IF TESTED, WOULD YIELD SPT REFUSAL SEVERE ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED, ROCK FABRIC CLEAR AND E ISEV.) REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS A
CRANIL AP LOOSE 4 TO 10		TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF
Onnocent MEDIUM DENSE 10 TO 30 N/A MATERIAL (NON-COHESIVE) DENSE 30 TO 50 VERY DENSE > 50 VERY SOFT < 2	ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT 	VERY ALL ROCK EXCEPT QUARTZ DISCOLORED OF STAINED. ROCK FABRIC ELEMENTS AR SEVERE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF (V SEV.) REMAINING, SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT
GENERALLY SOFT 2 TO 4 0.25 TO 0.5 SILT-CLAY MEDIUM STIFF 4 TO 8 0.5 TO 1.0 MATERIAL STIFF 8 TO 15 1 TO 2	TEST BORING WOMITORING WELL	VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <u>IF TESTED, WOULD YIELD SPT N V</u> COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, ON DISCERNIBLE ONLY SCATTERED CONCENTRATIONS, OUARTZ MAY BE PRESENT AS DIKES OR STRINGERS
(COHESIVE) VERY STIFF 15 TO 30 2 TO 4 HARD > 30 > 4	TTTTT ALLUVIAL SOIL BOUNDARY A PIEZOMETER - SPT N-VALUE	ALSO AN EXAMPLE.
TEXTURE OR GRAIN SIZE	RECOMMENDATION SYMBOLS	ROCK HARDNESS
U.S. STD. SIEVE SIZE 4 10 40 60 200 270		VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.
OPENING (MM) 4.76 2.00 0.42 0.25 0.075 0.053 BOULDER COBBLE GRAVEL COARSE FINE SILT CLAY BOULDER COBBLE GRAVEL SAND SAND SAND SAND	SHALLOW UNCLASSIFIED EXCAVATION - UNCLASSIFIED EXCAVATION - UNCLASSIFIED EXCAVATION - UNDERCUT UNDERCUT OF BACKFILL	HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BL TO DETACH HAND SPECIMEN.
(BLUR.) (COB.) (CR.) (CSE. SD.) (F SD.) (SL.) (CL.) GRAIN MM 305 75 2.0 0.25 0.05 0.005	ABBREVIATIONS AR - AUGER REFUSAL MED MEDIUM VST - VANE SHEAR TEST	MODERATELY CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DE HARD EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DE BY MODERATE BLOWS.
SOIL MOISTURE - CORRELATION OF TERMS	BT - BORING TERMINATED MICA MICACEOUS WEA WEATHERED CL CLAY MOD MODERATELY γ' - UNIT WEIGHT CPT - CONE PENETRATION TEST NP - NON PLASTIC γ'_{d} - DRY UNIT WEIGHT	MEDIUM CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE O HARD CAN BE EXCAVATED IN SMALL CHIPS TO PEICES I INCH MAXIMUM SIZE BY HARD POINT OF A GEOLOGIST'S PICK.
SOIL MOISTURE SCALE (ATTERBERG LIMITS) FIELD MOISTURE DESCRIPTION GUIDE FOR FIELD MOISTURE DESCRIPTION - SATURATED - USUALLY LIQUID: YERY WET, USUALLY	CSE COARSE ORG ORGANIC DMT - DILATOMETER TEST PMT - PRESSUREMETER TEST SAMPLE ABBREVIATIONS DPT - DYNAMIC PENETRATION TEST SAP SAPROLITIC S - BULK e - VOID RATIO SD SAND, SANDY SS - SPLIT SPOON	SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POIN PIECES CAN BE BROKEN BY FINGER PRESSURE.
ILL LIQUID LIMIT (SAT.) FROM BELOW THE GROUND WATER TABLE	e - VOID RATIO SD SAND, SANDY SS - SPLIT SPOON F - FINE SL SILT, SILTY ST - SHELBY TUBE FOSS FOSSILIFEROUS SLI SLIGHTLY RS - ROCK FRAC FRACTURED, FRACTURES TCR - TRICONE REFUSAL RT - RECOMPACTED TRIAXIAL	VERY CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READLLY WITH POINT OF PICK. SOFT OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCH FINGERNALL.
RANGE < - WET - (W) SEMISOLID; REQUIRES DRYING TO (PI) ATTAIN OPTIMUM MOISTURE	FRAGS FRAGMENTS W - MOISTURE CONTENT CBR - CALIFORNIA BEARING	FRACTURE SPACING BEDDING
	HI HIGHLY V - VERY RATIO EQUIPMENT USED ON SUBJECT PROJECT	TERM SPACING TERM VERY WIDE MORE THAN 10 FEET VERY THICKLY BEDDED
OM OPTIMUM MOISTURE - MOIST - (M) SOLID; AT OR NEAR OPTIMUM MOISTURE SL SHRINKAGE LIMIT	DRILL UNITS: ADVANCING TOOLS: HAMMER TYPE: CME-45C CLAY BITS X AUTOMATIC MANUAL	WIDE 3 TO 10 FEET THICKLY BEDDED 1. MODERATELY CLOSE 1 TO 3 FEET THINLY BEDDED 0.1 CLOSE 0.16 TO 1 FOOT VERY THINLY BEDDED 0.6
- DRY - (D) REOUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE		. VERY CLOSE LESS THAN 0.16 FEET THICKLY LAMINATED 0.00 THINLY LAMINATED <
PLASTICITY	СИЛЕ -55 СОЛЕ -55 СО	INDURATION
PLASTICITY INDEX (PI) DRY STRENGTH	CME-550 HARD FACED FINGER BITS -N	FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HE
NON PLASTIC 0-5 VERY LOW SLIGHTLY PLASTIC 6-15 SLIGHT	VANE SHEAR TEST V CASING V ADVANCER	FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.
MODERATELY PLASTIC 16-25 MEDIUM HIGHLY PLASTIC 26 OR MORE HIGH	POST HOLE DIGGER	MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH ST BREAKS EASILY WHEN HIT WITH HAMMER.
	X D50 - (TER346)	INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL DIFFICULT TO BREAK WITH HAMMER.
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.	X D50 - (TER373) X TRICONE 3% STEEL TEETH VANE SHEAR TEST	EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE SAMPLE BREAKS ACROSS GRAINS.

PROJECT REFERENCE NO.



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	TERMS AND DEFINITIONS
D. AN INFERRED SPT REFUSAL.	ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
FOOT PER 60 IS OFTEN	ADUIFER - A WATER BEARING FORMATION OR STRATA.
	ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
	ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.
N VALUES >	ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT
СК ТНАТ	WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND
CLUDES GRANITE,	SURFACE.
L PLAIN	CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
IF TESTED.	COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.
MAY NOT YIELD TONE, CEMENTED	CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
	DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
RINGS UNDER	<u>DIP</u> - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.
DATINGS IF OPEN, AMMER BLOWS IF	DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
CK UP TO	FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
L FELDSPAR BLOWS.	SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTORE.
5. IN	FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM
Y. ROCK HAS	PARENT MATERIAL.
AS COMPARED	FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
ELDSPARS DULL	FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE
OSS OF STRENGTH	
WHEN STRUCK.	JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
VIDENT BUT	<u>LEDGE</u> - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.
RE KAOLINIZED	LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
E DISCERNIBLE	USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
STRONG ROCK	PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.
ONLY MINOR ALUES < 100 BPF	OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.)SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
IN SMALL AND	ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF
. SAPROLITE IS	ROCK SECHENTS EQUAL TO OR OREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
5 REQUIRES	$\underline{SAPROLITE}$ - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
LOWS REQUIRED	<u>SILL</u> - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
EP CAN BE	SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT
ETACHED	OR SLIP PLANE.
R PICK POINT. BLOWS OF THE	STANDARD PENETRATION TEST (PENETRATION RESISTANCE)(SPT) - NUMBER OF BLOWS (N OR BPF)OF A 140 LB.HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
FRAGMENTS T. SMALL, THIN	STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
PIECES 1 INCH	STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEOMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
ED READILY BY	TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
THICKNESS	BENCH MARK: SEE NOTES
4 FEET	ELEVATION: N/A FEET
.5 - 4 FEET .6 - 1.5 FEET	
3 - 0.16 FEET 18 - 0.03 FEET	NOTES:
0.008 FEET	FIAD - FILLED IN AFTER DRILLING
	PROJECT WAS DRAFTED USING PROVIDED TIN FILE (FILE: R5769_012616)
AT, PRESSURE, ETC.	
EEL PROBE;	
PROBE:	
NODL:	
	DATE: 8-15-14



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Date: TIP Number: County: Description:	June 2016 R-5796 Johnston Novo Nordisk Access Road from SR 1905 (Gordon Road) to Proposed Novo Nordisk Site
Subject:	Roadway Geotechnical Report - Inventory

Project Description

The project is located between Clayton and Wilsons Mills near the US 70 corridor in Johnston County, North Carolina. The proposed project consists of the construction of 0.6 miles of two-lane roadway on new location and the widening of an 800 feet long section of existing two-lane roadway to accommodate turn lanes. The new construction begins at SR 1905 (Gordon Road) and continues in a northeast direction through cultivated fields, wetlands, and woods before crossing two Norfolk Southern rail lines and ending at the proposed site of the new Novo Nordisk facility. The proposed access road will cross over the Norfolk Southern rail lines on a single span bridge with MSE walls proposed at the abutments. SR 1905 will be widened to the north to accommodate turn lanes to the proposed access road. The widening and new construction will be fill sections ranging from sliver fills on the existing SR 1905 embankments to 30 feet tall embankments at the bridge over the Norfolk Southern rail lines.

The geotechnical subsurface investigation was performed throughout March and April of 2016. Two Diedrich D-50 rotary drills were utilized to advance the soil test borings. Both of the rotary drill rigs utilized on this project were equipped with recently calibrated automatic Standard Penetration Test (SPT) hammers. A Pagani TG73-200 rig was utilized to push cone (CPT) and flat blade dilatometer (DMT) at the proposed bridge approach embankments. Pore water pressure dissipation tests were performed during selected CPT soundings.

The following alignments were investigated by soil testing and visual reconnaissance:

<u>Alignment</u>	<u>Stations</u>
-L-	10+00 to 43+57.04
-L1-	10+00 to 15+07.87
-Y1REV-	10+50 to 23+17.31

Physiography and Geology

The project is located near the western fringe of the Inner Coastal Plain Physiographic Province. The near surface soils consist of undivided upland coastal plain deposits. The coastal plain deposits are underlain by residual soils and weathered and crystalline rock within the depths of several soil test borings performed at the site. Where encountered in the SPT borings, the top of the residual soils and weathered rock is near Elevation 250 feet. SPT refusal on crystalline rock was encountered between Elevations 232 and 242 feet

near the Norfolk Southern rail lines. The crystalline rock encountered in the soil test borings was mica schist.

The existing elevations along the corridor range from approximately 279 feet to 295 feet. In general, the topography is rolling with gentle slopes. The existing Norfolk Southern rail lines are located near the highest point on the project. An area delineated as wetlands between -L- Stations 22+00 and 29+50 is believed to be a portion of a Carolina Bay.

Soil Properties

-Y1REV-

Roadway embankment soils were encountered in the hand augers performed along the shoulder of existing SR 1905 (-Y1REV-). The roadway embankment soils begin near -Y1REV- Station 14+75 and continue to Station 22+00. The roadway embankment soils consist of high plasticity silty clay (A-7-6) over silty sand (A-2-4), both containing little quartz gravel. The clay layer was approximately 2 feet thick and the sand extended to approximately 6 feet below existing grades where encountered in the hand augers. In the up station direction along -Y1REV-, the roadway embankment tapers from at grade and gets deeper as existing SR 1905 crosses a small jurisdictional stream channeled through a 30 inch RCP culvert at -Y1REV- Station 20+52. The maximum existing embankment height occurs near the existing RCP culvert and is approximately 6 feet. As the alignment continues up station, the roadway embankment soils taper out and meet undivided coastal plain again at -Y1REV- Station 22+00.

Alluvial soils were encountered beneath the roadway embankment on -Y1REV- between Stations 19+11 and 21+67. The alluvial soils encountered directly beneath the roadway embankment were organic sandy clay (A-6). This layer is approximately 1 foot thick and is underlain by a loose clean sand (A-3) to hand auger termination depths of 6.5 feet. The alluvial soils occur in the low lying area on the -Y1REV- alignment as described above and continue north along the jurisdictional stream floodplain toward the -L- alignment.

<u>-L- and -L1-</u>

Alluvial soils are present on the -L- alignment at the surface near the jurisdictional stream that continues south toward SR 1905 (-Y1REV-). These alluvial soils are present near the surface between -L- Stations 15+97 and 16+79. The alluvial soils consist of loose clean sand (A-3).

The coastal plain deposits along the corridor can be generalized into three layers. There are organic soils present within and surrounding the delineated wetlands. Outside of the wetland areas and beneath the organic soils is a relatively stiff crust. Beneath the stiff crust is a very soft layer that extends to the top of residual and weathered rock.

The organic soil layer was encountered at the surface within the delineated wetlands and near their boundaries between approximately -L- Stations 21+25 to 29+50 and 37+00 to 39+50. This layer consists of organic clayey sand (A-2-6) and organic sandy clay (A-6). These soils contain trace to little organics and extend to depths as deep as 9 feet where encountered.

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The second generalized coastal plain layer was encountered outside of the delineated wetlands and beneath the organic soils described previously. This layer is a medium stiff to hard layer that generally consists of silty clay (A-7-6) and sandy clay (A-6), although some samples from this layer also classify as a medium dense to dense clayey sand (A-2-6 or A-2-7) based on laboratory testing. This layer is notably stiffer / denser than the other coastal plain soils encountered along the project. This layer exhibits the highest SPT blow counts and in-situ moduli based on the CPT and DMT near the Norfolk Southern Railroad between approximately -L- Station 30+50 and 35+50, where the depth to groundwater is the deepest along the project. The layer extends from the surface to depths of up to 20 feet below existing site grades.

The third coastal plain layer exhibited very low SPT blow counts and was encountered once the SPT borings were advanced through the stiff crust layer along the project. The soft / loose layer consisted of wet to saturated high plasticity clay (A-7-6) with highly variable amounts of sand and gravel; saturated clayey sand (A-2-6 and A-2-7) with trace to little gravel; and clean, very loose to loose, sand and gravel (A-3 and A-1-a). The sandy and gravelly soils were typically encountered in the top 20 feet of the layer and the high plasticity clay was encountered below to the interface with the residual and weathered rock. Based on the in-situ testing and deeper SPT borings, the soft / loose layer extends to the top of residual and weathered rock which were encountered at depths ranging from 35 to 50 feet below existing site grades. The clay soils near the bottom of the layer also contained trace to little mica.

Residual soils were encountered in several of the deeper SPT borings advanced near the bridge and retaining wall structures at the Norfolk Southern Railroad. The residual soils were sampled as soft to stiff high plasticity clay (A-7-6) and dense to very dense silty sand (A-2-4) both of which contained trace to little mica.

Rock Properties

Weathered rock and crystalline rock along the project appear to be a micaceous schist based on the materials recovered in the split spoon sampler. Rock coring was not performed for the subsurface investigation along the project. The weathered rock and rock were encountered at depths of 40 to 60 feet below existing site grades. The weathered rock and crystalline rock at the site are not anticipated to have an impact on roadway construction.

Groundwater

The corridor generally drains to the delineated wetland areas which in turn drain to unnamed jurisdictional streams that run out of the corridor. The areas delineated as wetlands along the project were observed to retain water for several days following precipitation. In the suspected Carolina Bay, water depths of up to 3 feet were observed during a site visit to lay out boring locations. However, the site was revisited following a period of dry weather to begin the field investigation and the surface water had infiltrated or drained. Surface water depths of up to 1.5 feet were observed in the delineated wetland areas up station from the bridge over the Norfolk Southern Railroad. Similar to the suspected Carolina Bay, surface water was not observed when the site was revisited after a period of dry weather. Although surface water was not

observed following dry weather, groundwater was encountered during drilling and sampling in and near the delineated wetlands at depths of 0.5 to 1 foot below existing site grades.

Away from the wetland areas, the depth to groundwater ranged from approximately 3 to 10 feet below existing site grades. From the SR 1905 and access road intersection to approximately -L- Station 21+00, groundwater was encountered between 3 and 7.5 feet below existing site grades which corresponds to an elevation of 278 to 280 feet. Between -L- Stations 29+00 and 37+00 groundwater was encountered between 2 and 10 feet below existing site grades. Along this section of the project, the depths to groundwater correspond to an elevation of 284 to 285 feet.

Areas of Special Geotechnical Interest

1. High Plasticity Clay

High plasticity clay was encountered near proposed subgrade or in fill sections at the following locations:

Alignment

-Y1REV-

2. Organic Soils

Soils containing little organic matter were encountered at the following locations:

<u>Alignment</u> -L--L-

3. High Groundwater

Groundwater was encountered at the following locations within 6 feet of proposed grades:

Alignment	
-L-	
-L-	
-L1-	

4. Poor Drainage

The following areas are delineated as wetland and were observed to hold standing surface water for periods during the investigation:

<u>Alignment</u>
-L-
-L-
-L1-

PROJECT REFERENCE NO.	SHEET NO.
R-5769	ЗA

<u>Stations</u> 10+50 to 23+17.31

<u>Stations</u> 21+25 to 29+50 37+00 to 39+50

<u>Stations</u> 21+25 to 24+00 41+25 to 43+57.04 10+50 to 15+07.87

> <u>Stations</u> 21+25 to 29+50 37+56 to 43+57.04 10+00 to 15+07.87

<u>Closing</u>

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report, or if we may be of further service, please contact us at your convenience.

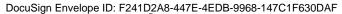
Sincerely, Terracon Consultants, Inc.

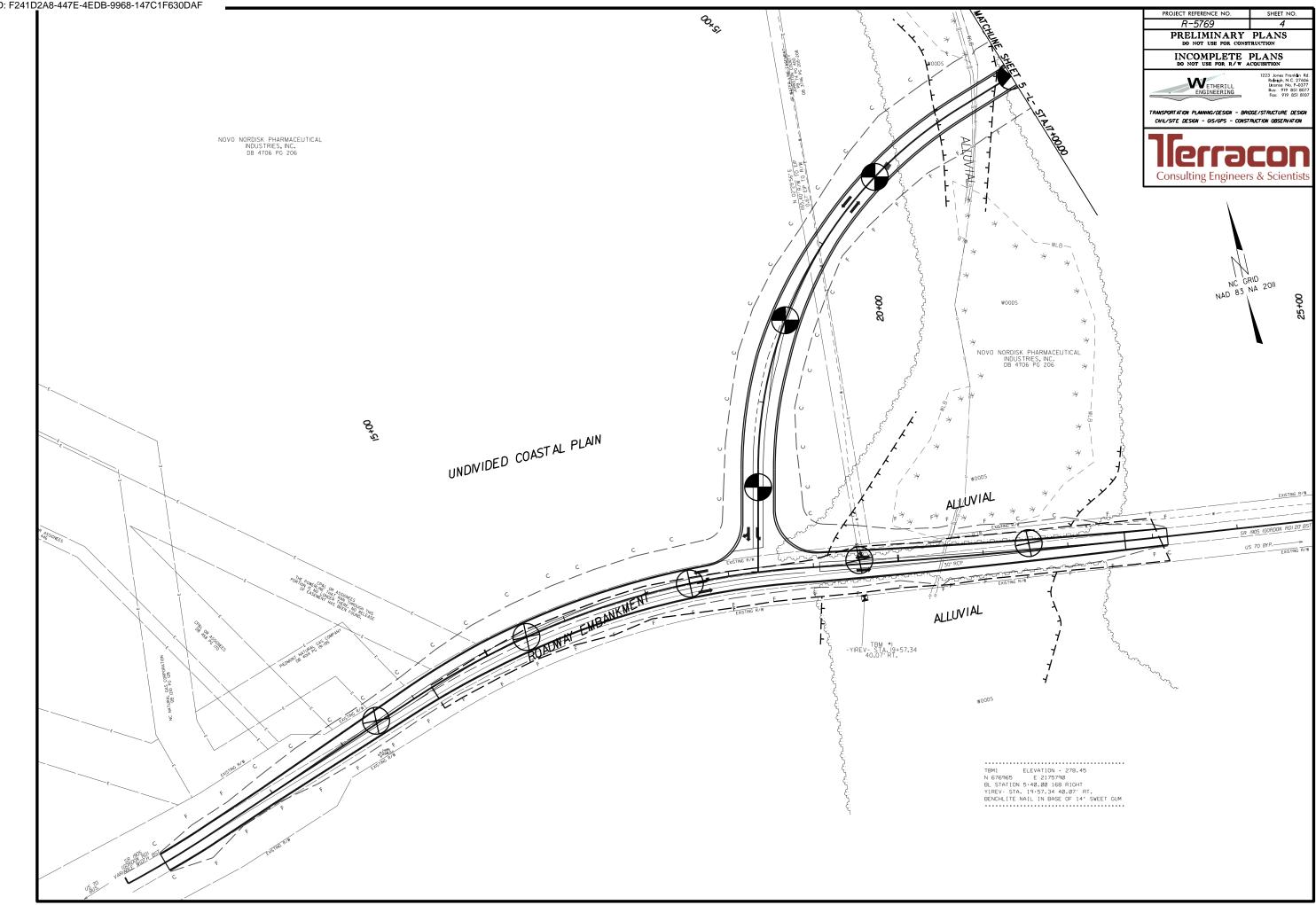
Matthew J. Alexander, PE Project Geotechnical Engineer

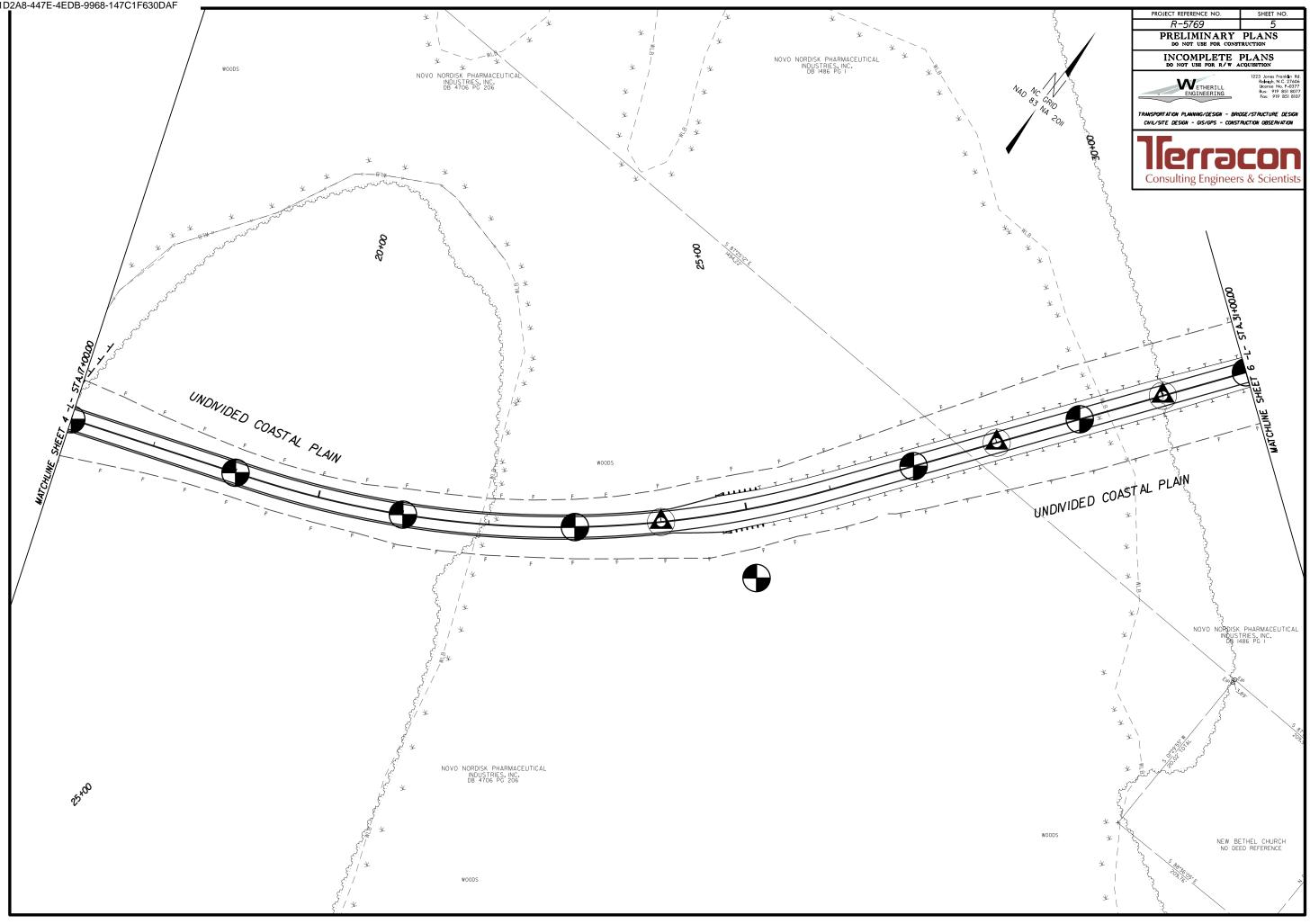
ANDREN NASH

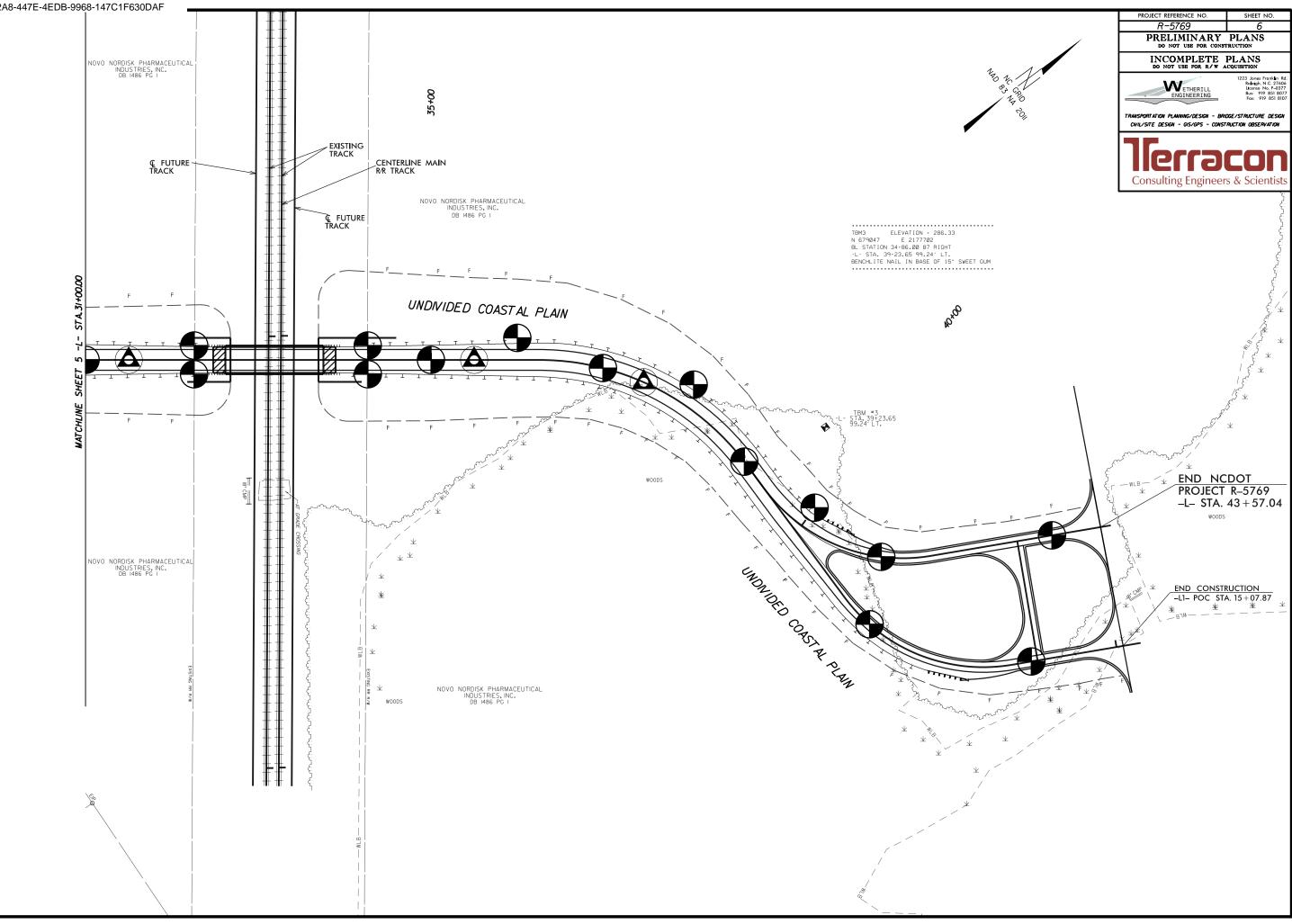
Andrew A. Nash, PE Geotechnical Department Manager

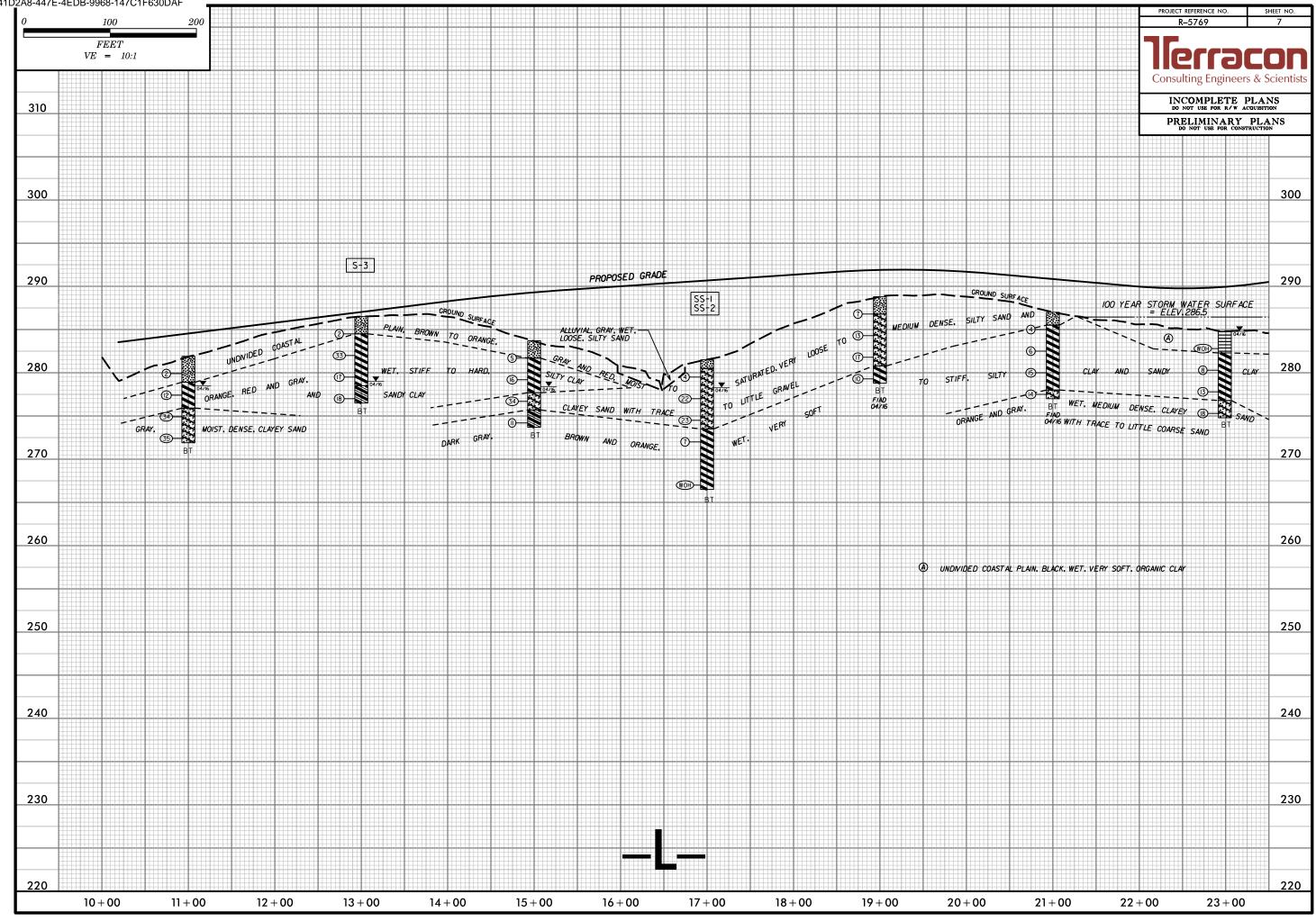
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R-5769	3B

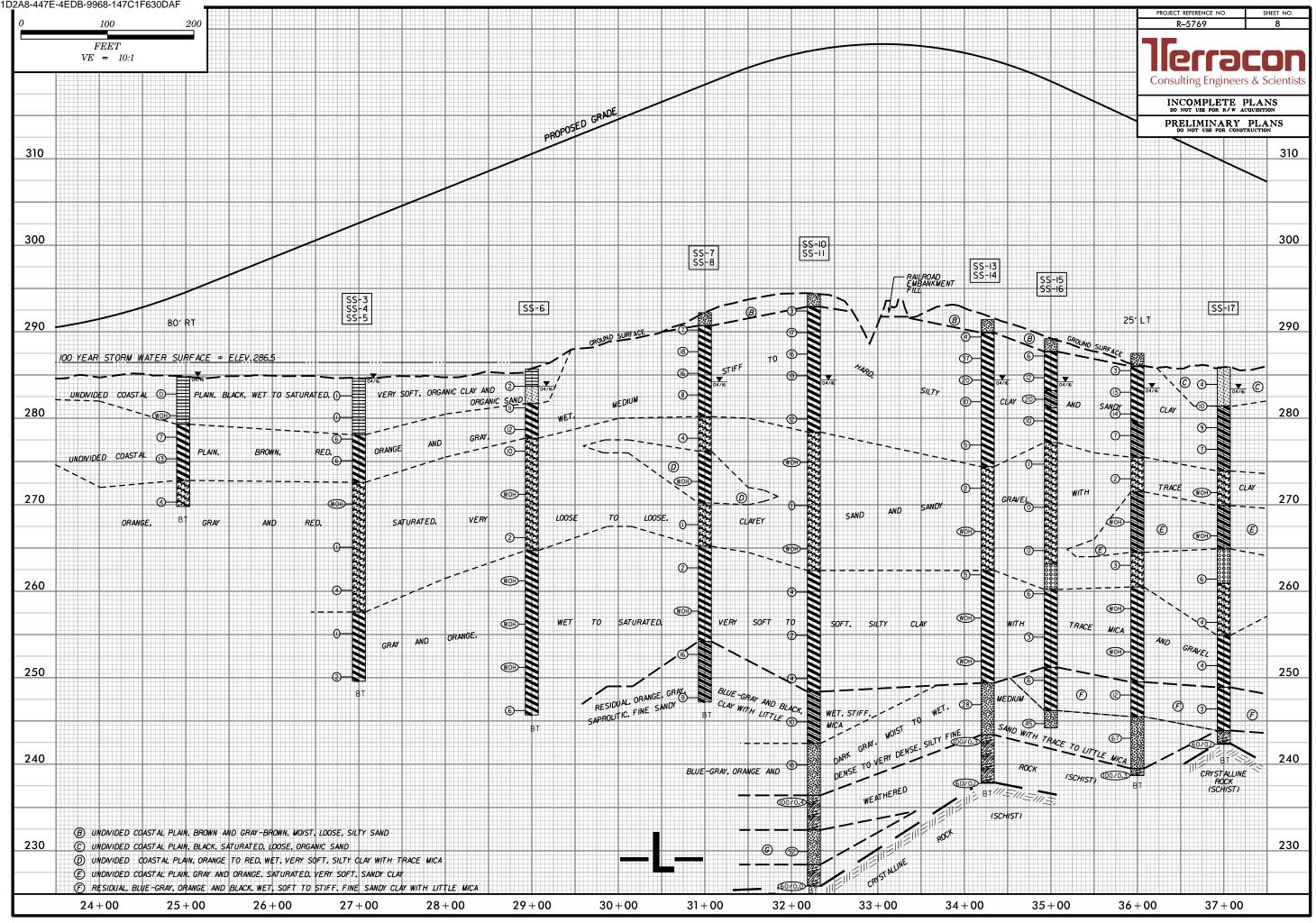


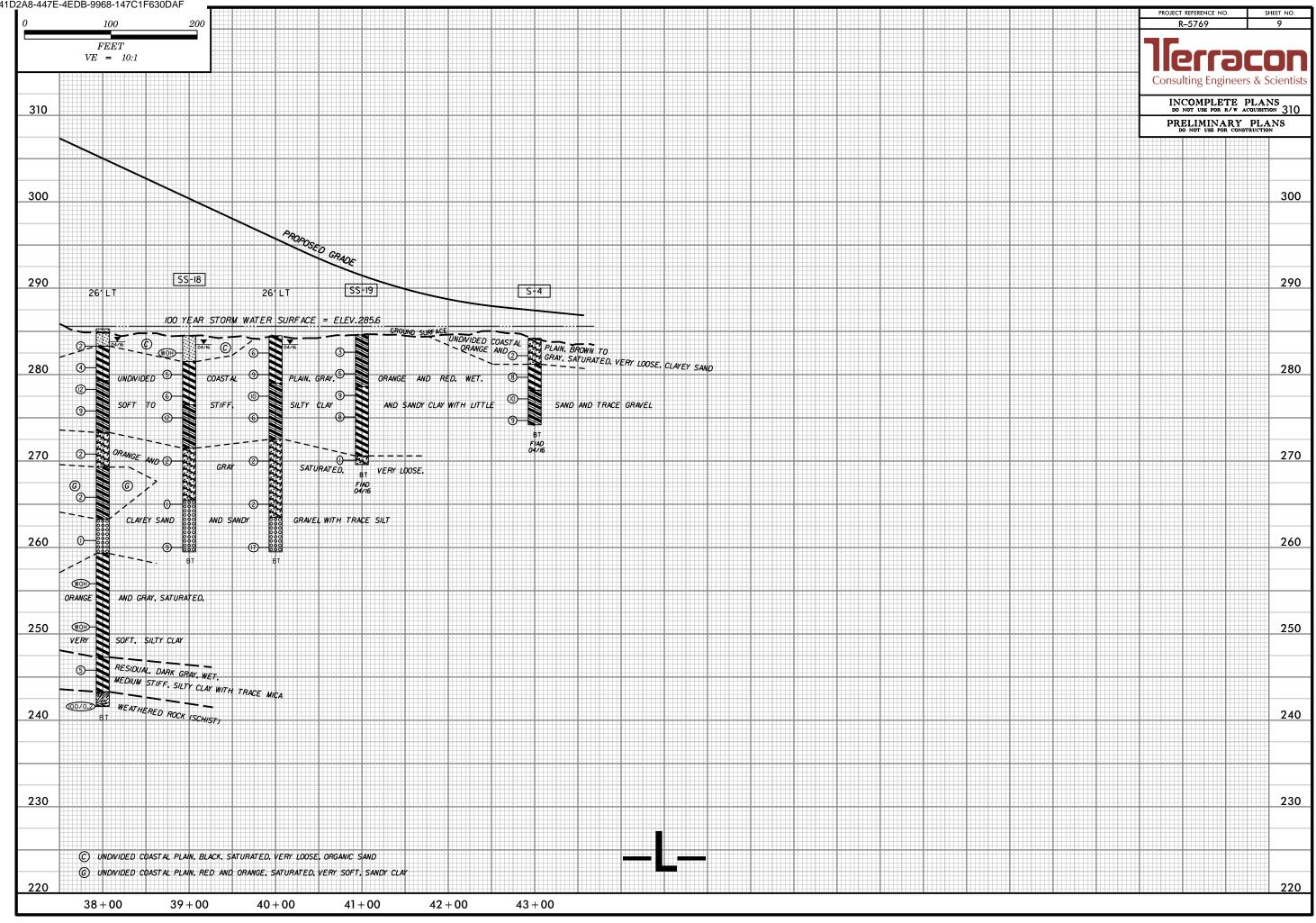


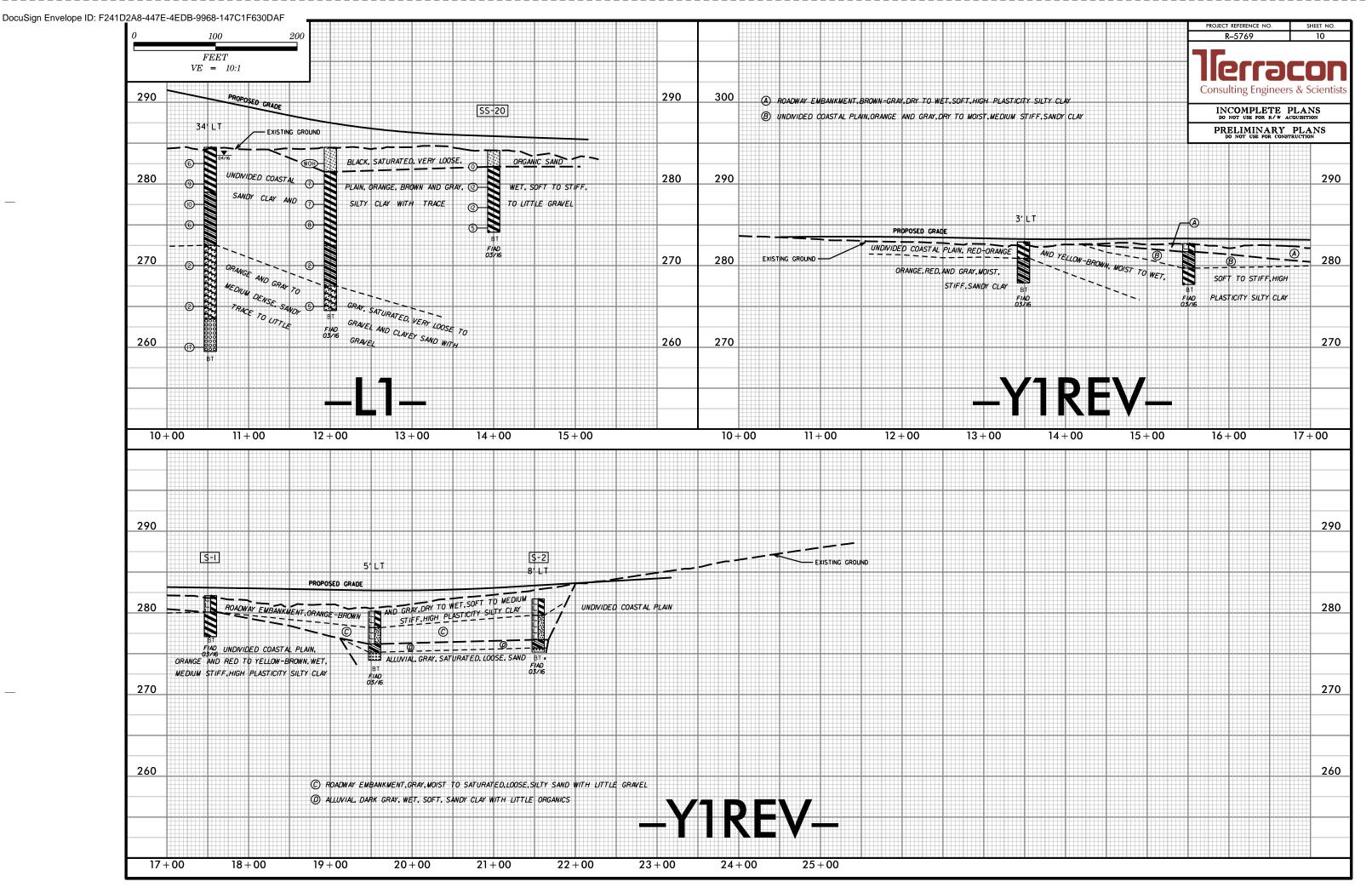


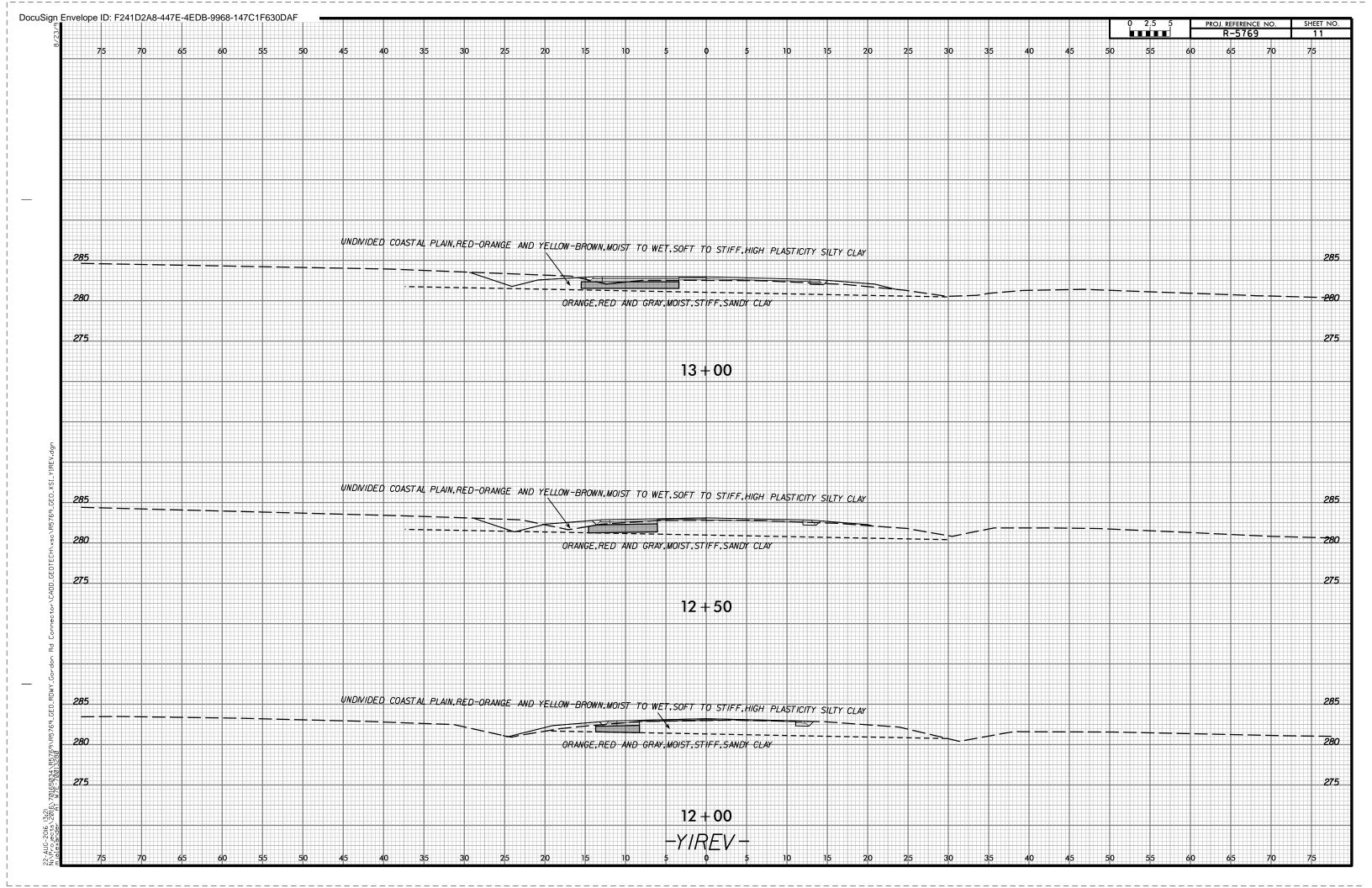


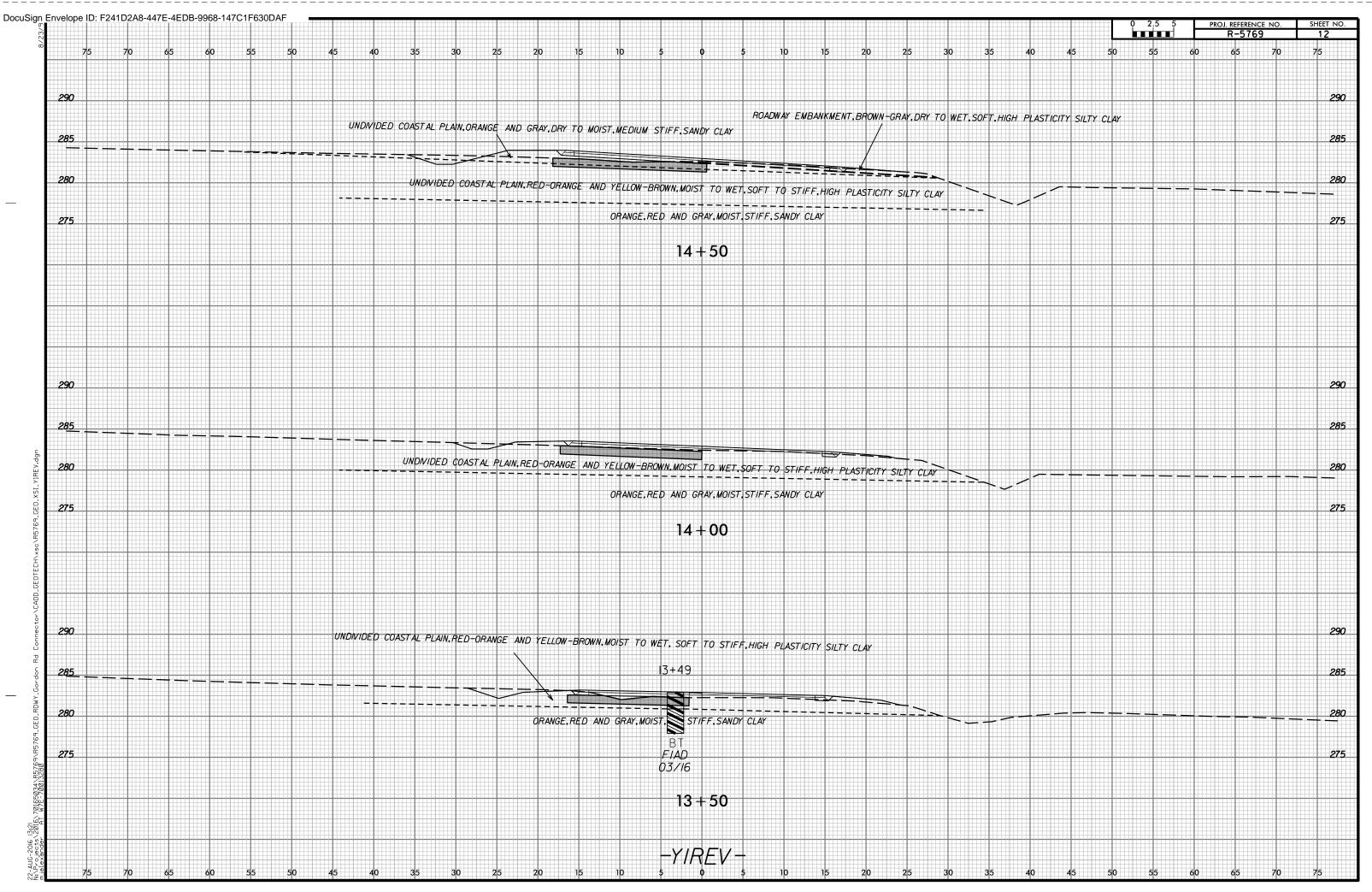


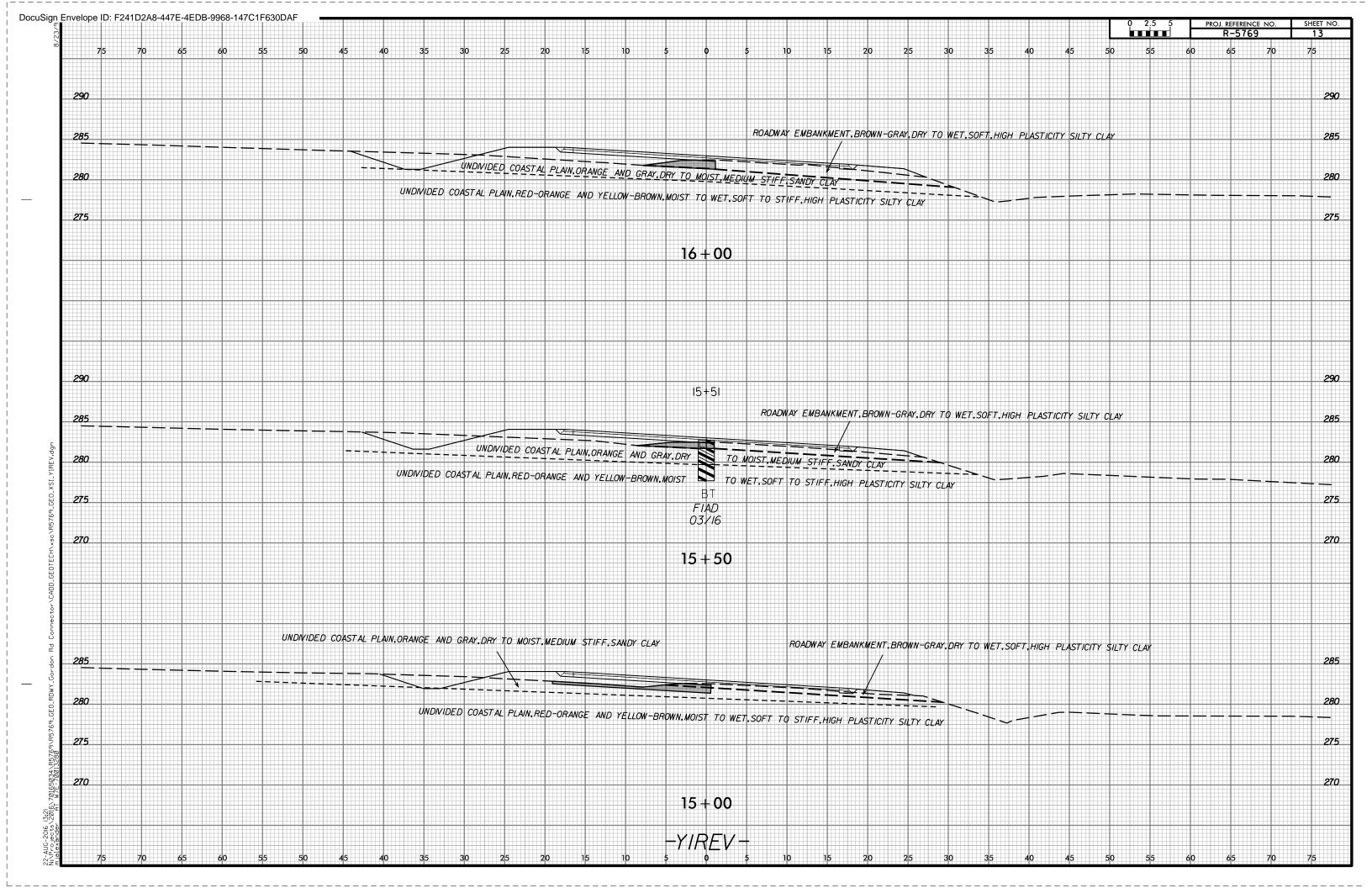


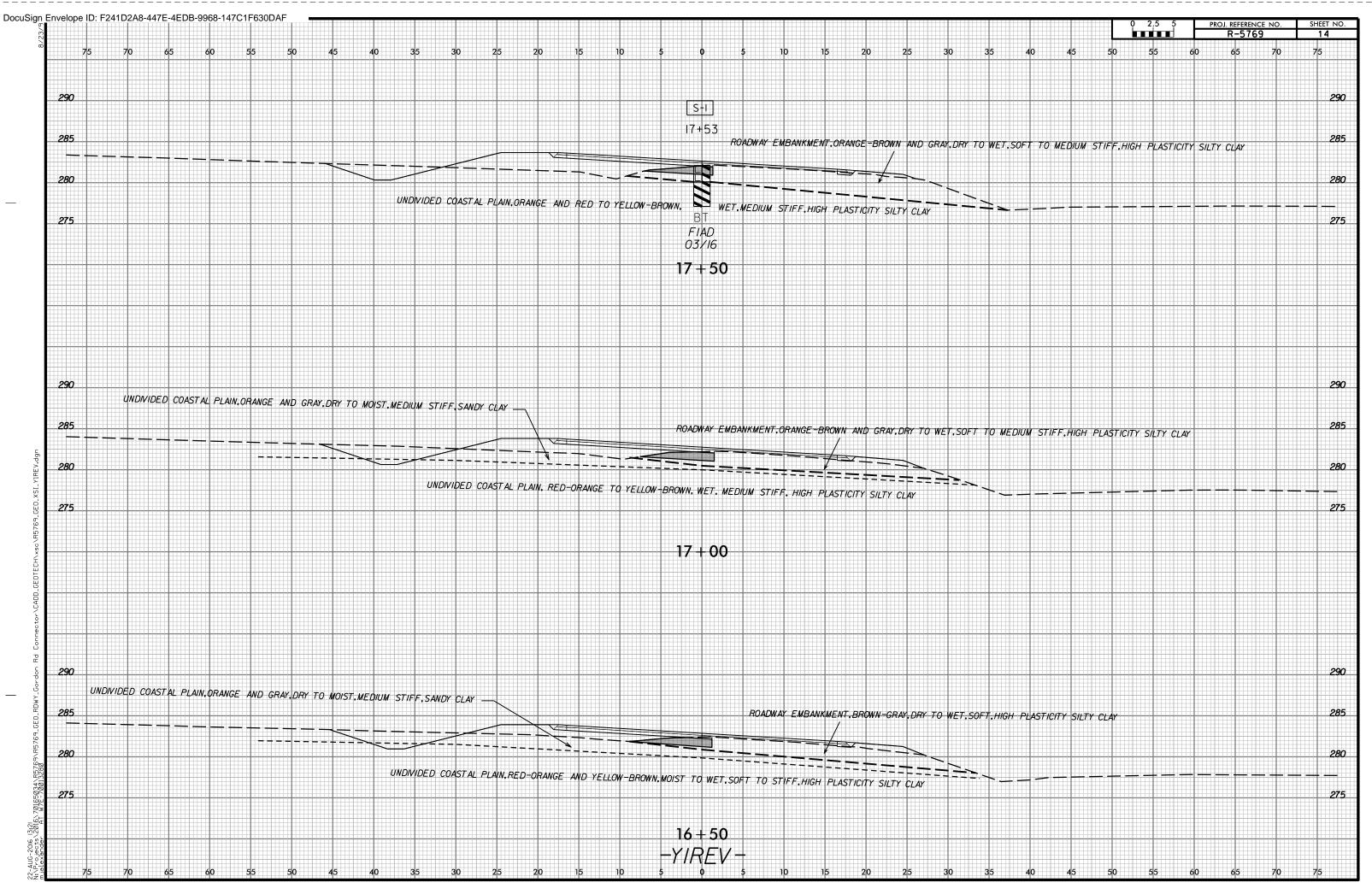


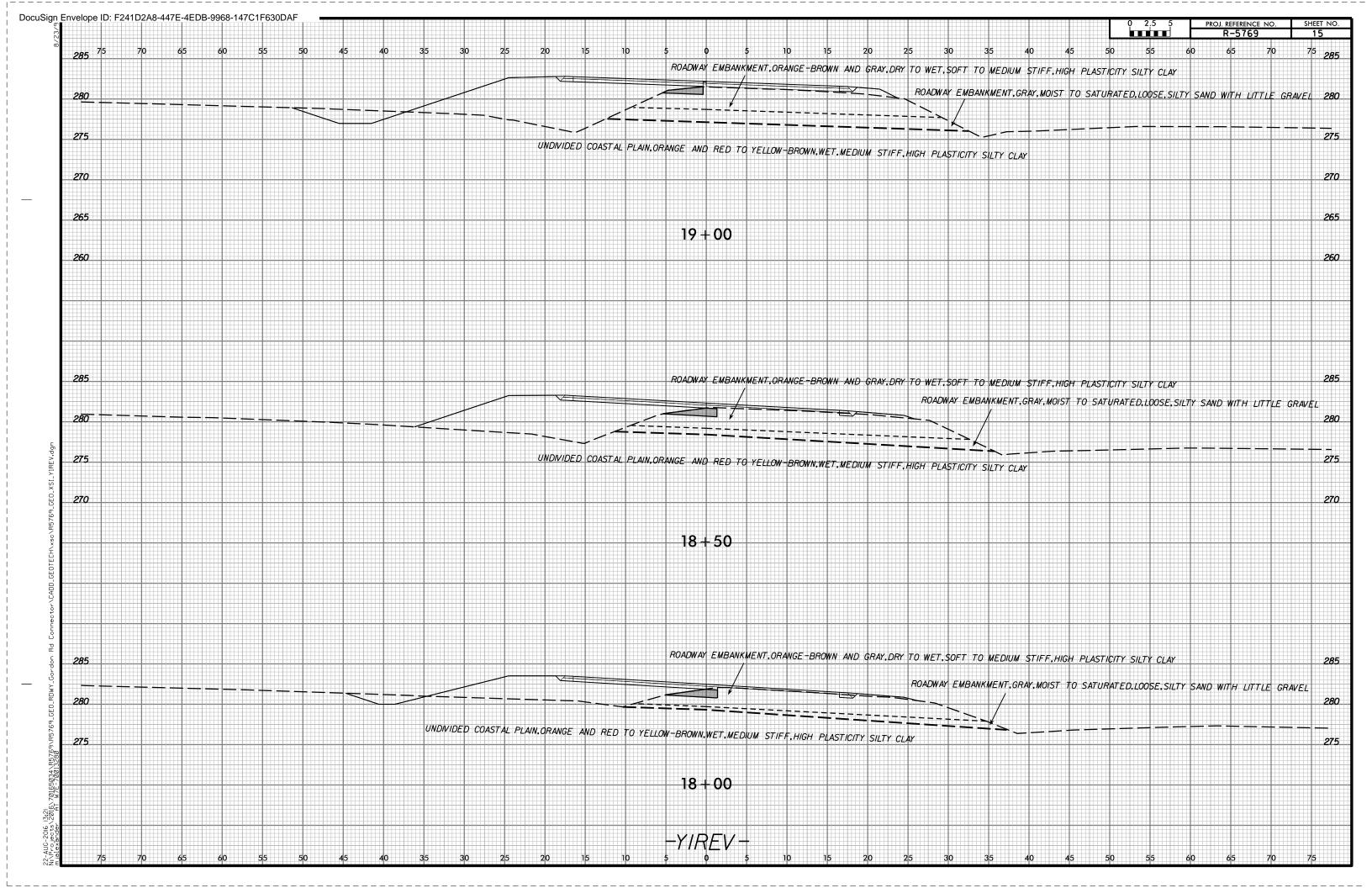


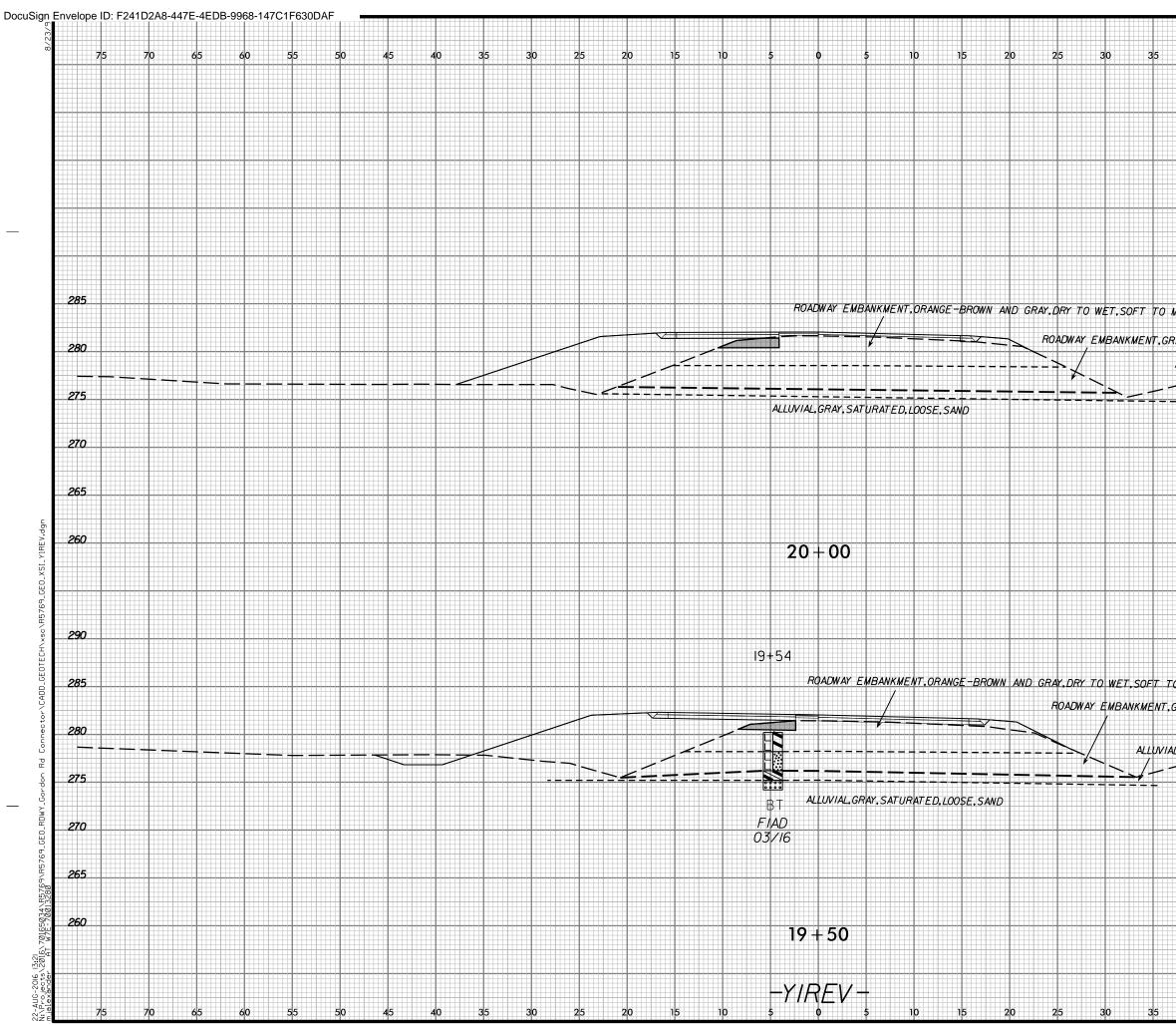




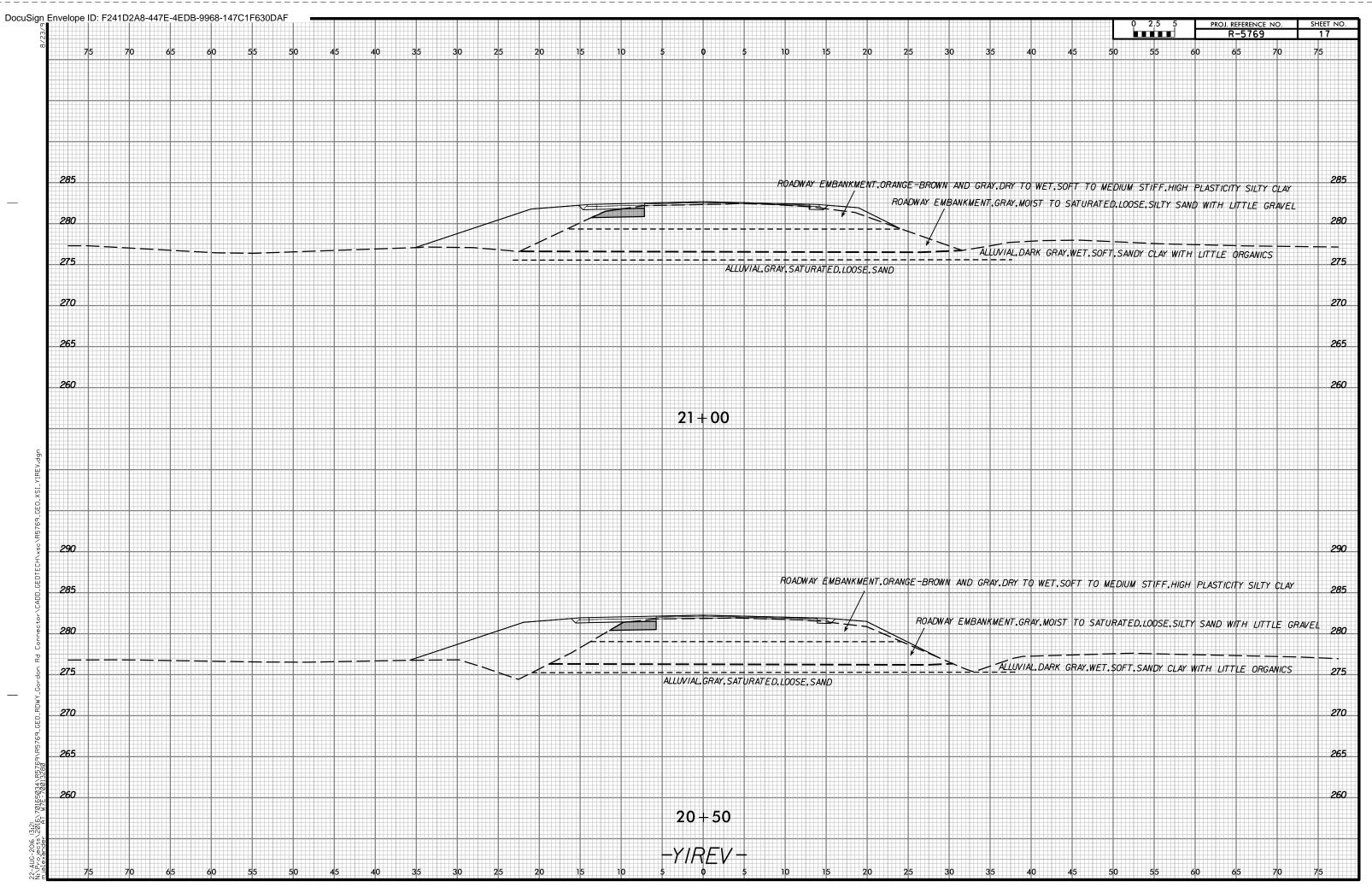


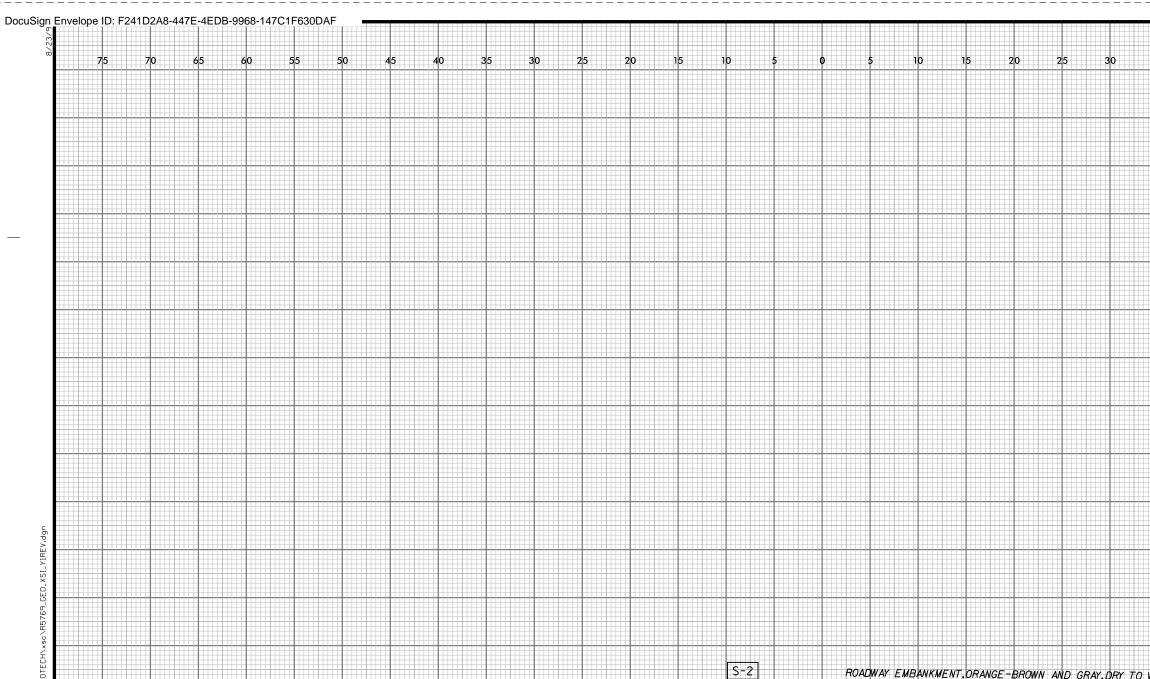


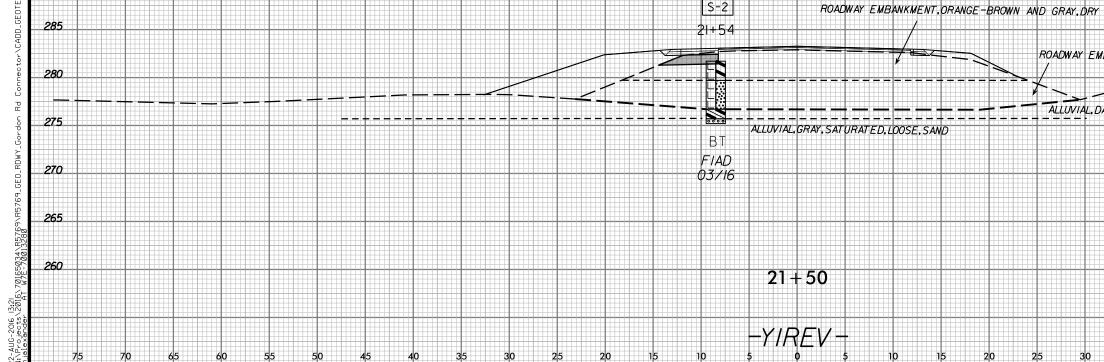


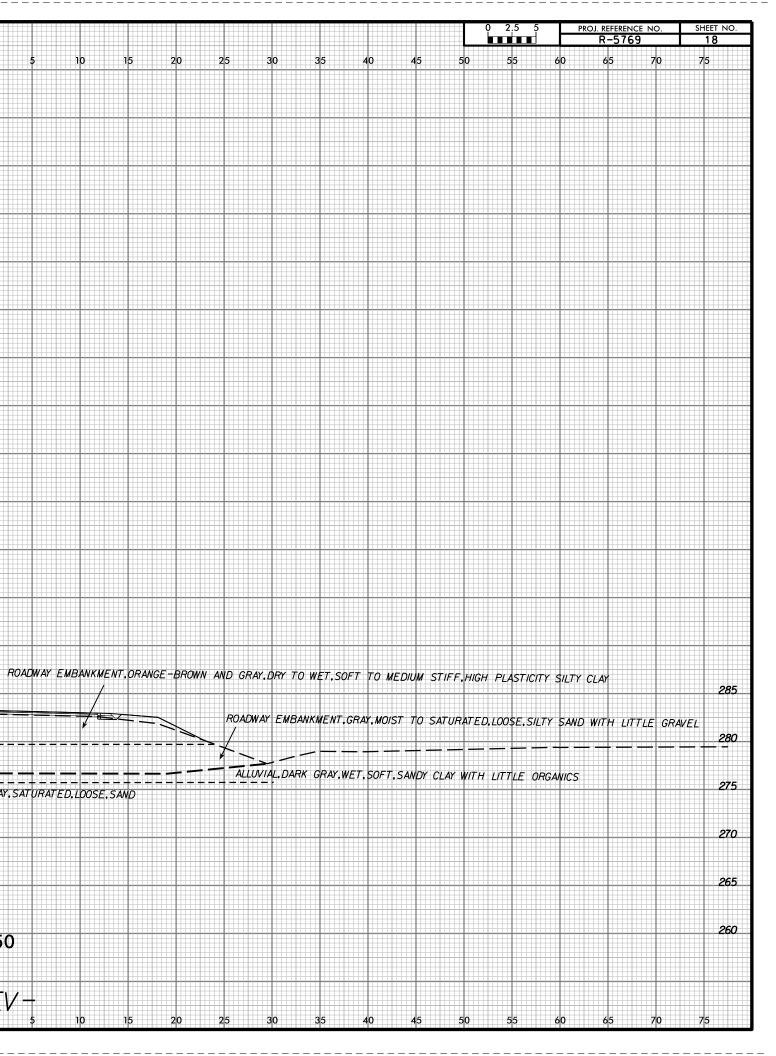


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40 4	5 5	0 55	60		5	70	75
							285
ÆDIUM STIFF.	HIGH PLA	STICITY SIL	TY CLAY				205
AY.MOIST TO S	SATURATE	D.LOOSE.SIL	TY SANE	WITH I	ITTLE G	RAVEL	900
ALLUVIAL.DARK							280
<i>{</i>							
							275
							270
							265
							260
							290
) MEDIUM STIF	F,HIGH I	PLASTICITY	SILTY CL	AY			285
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							280
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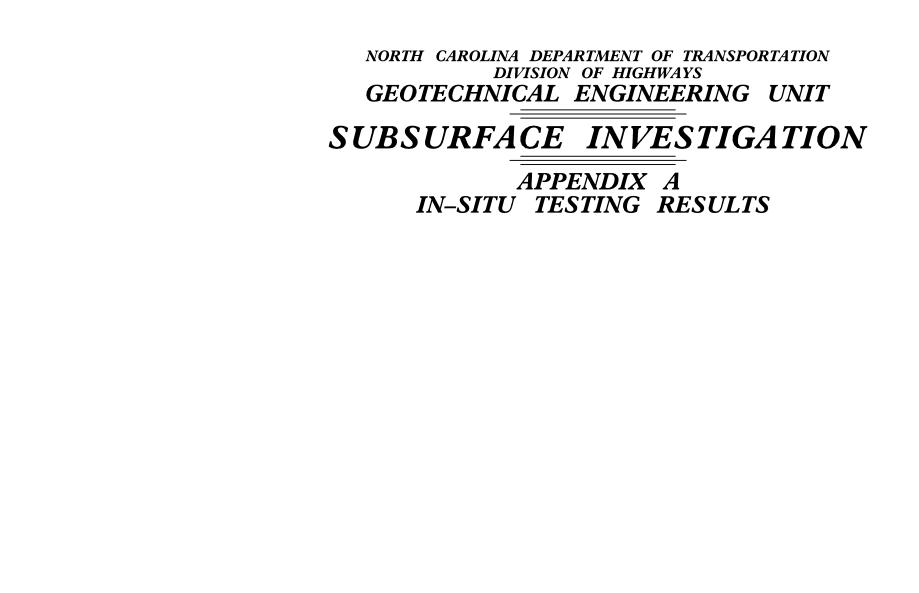




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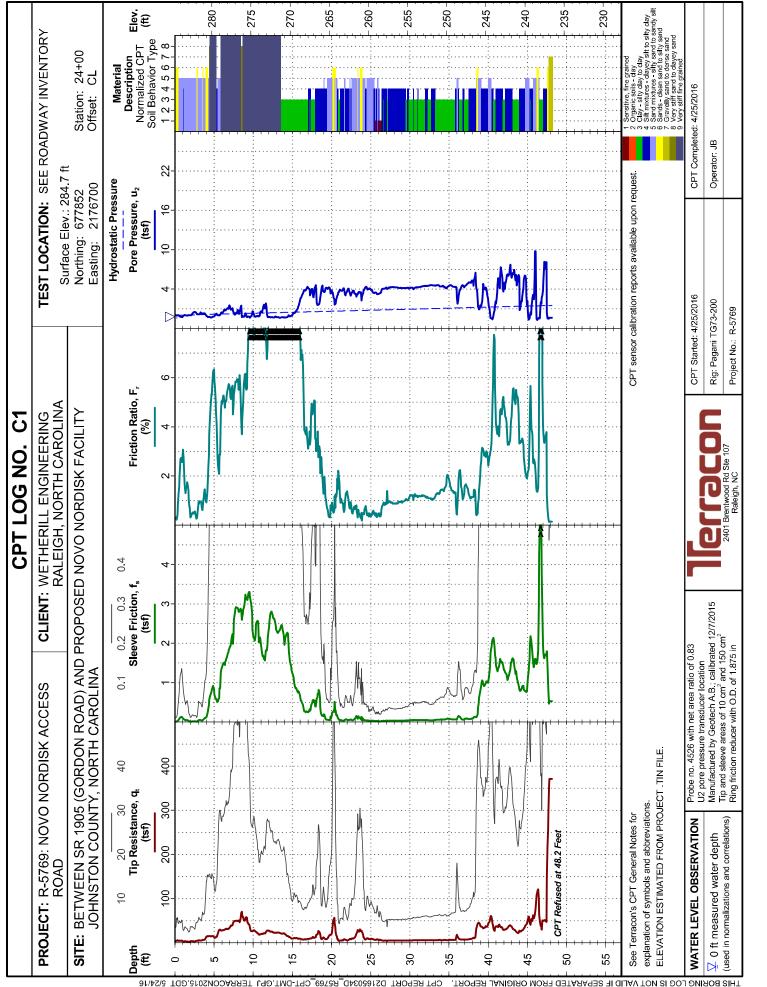


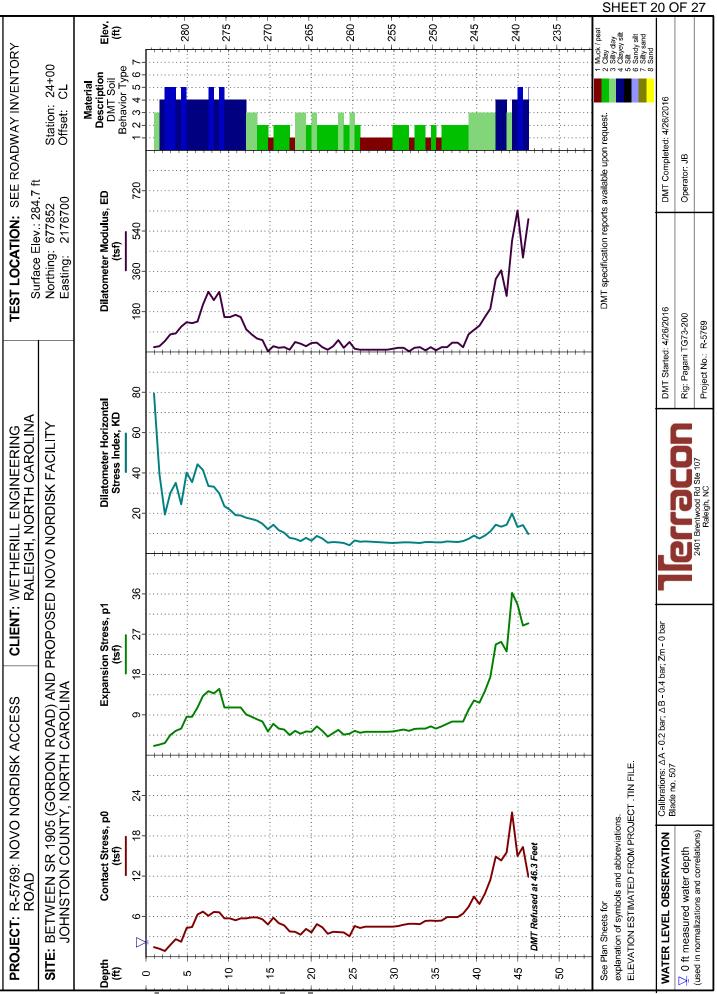




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INITIALS

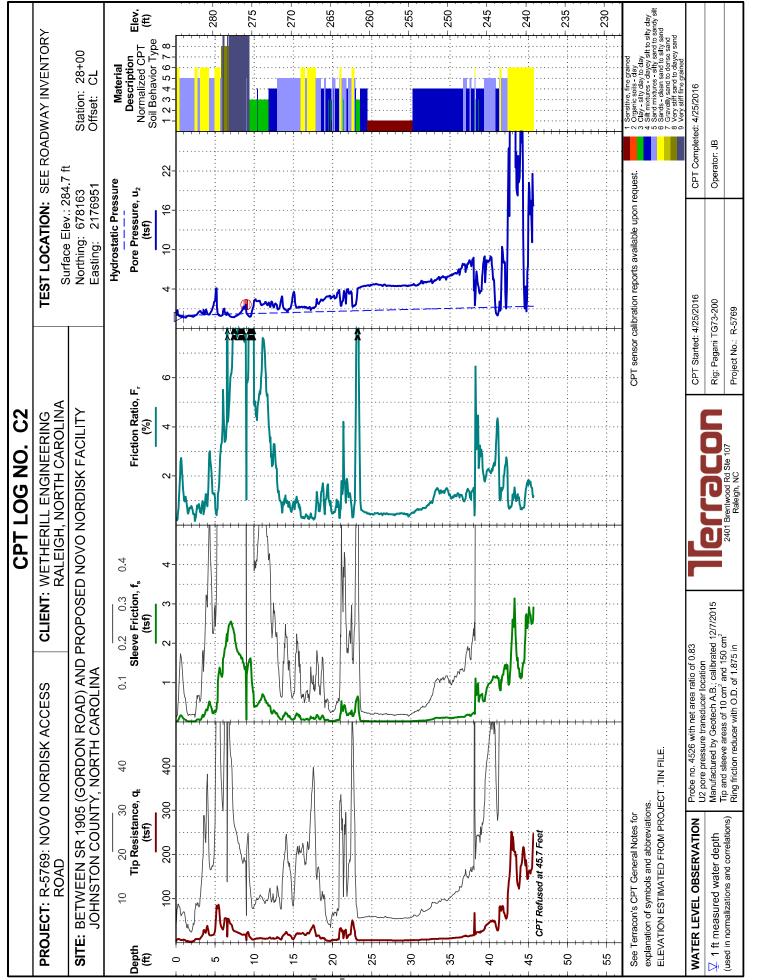


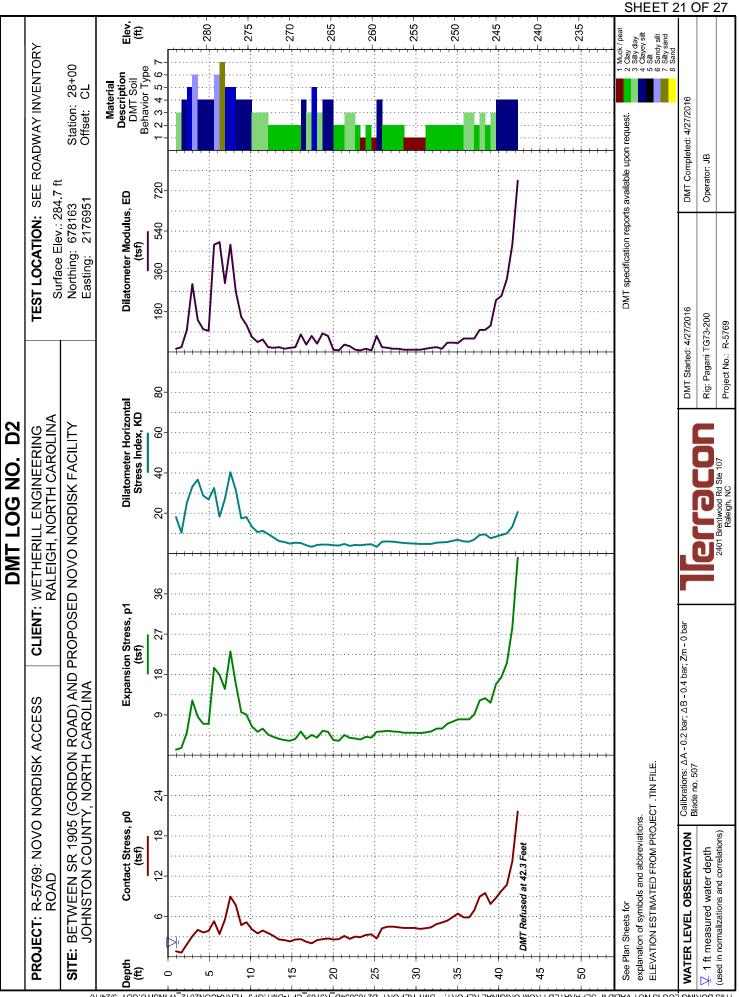


4/16 THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CPT REI

DMT LOG NO. D1

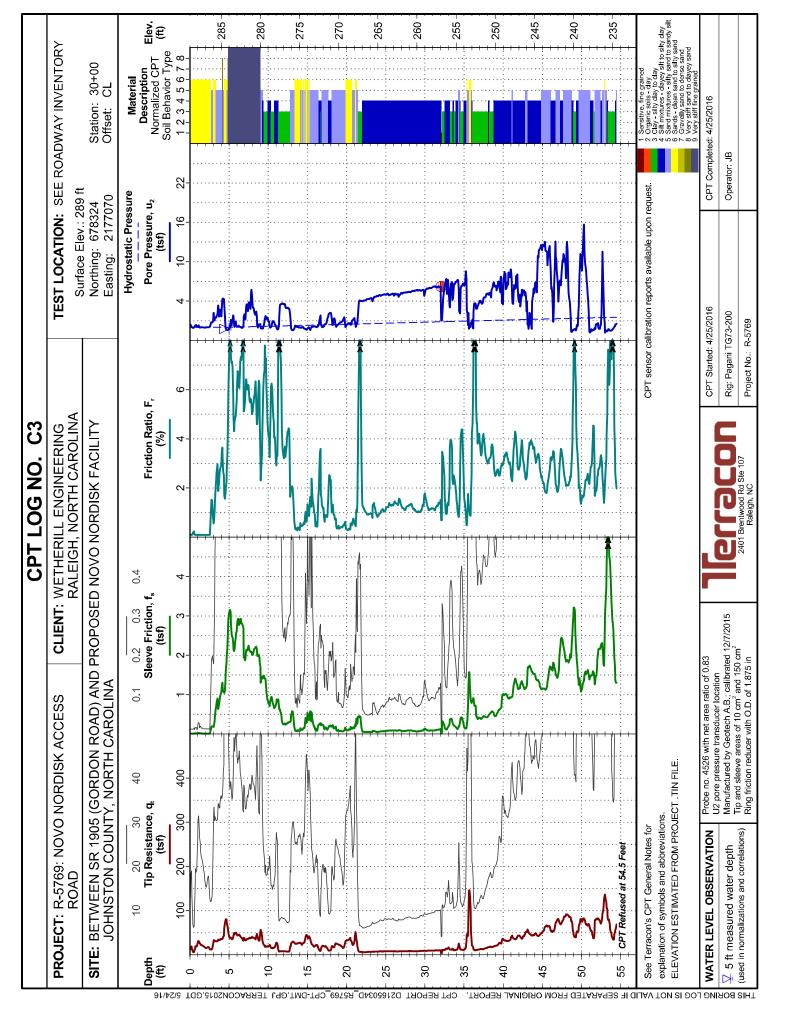
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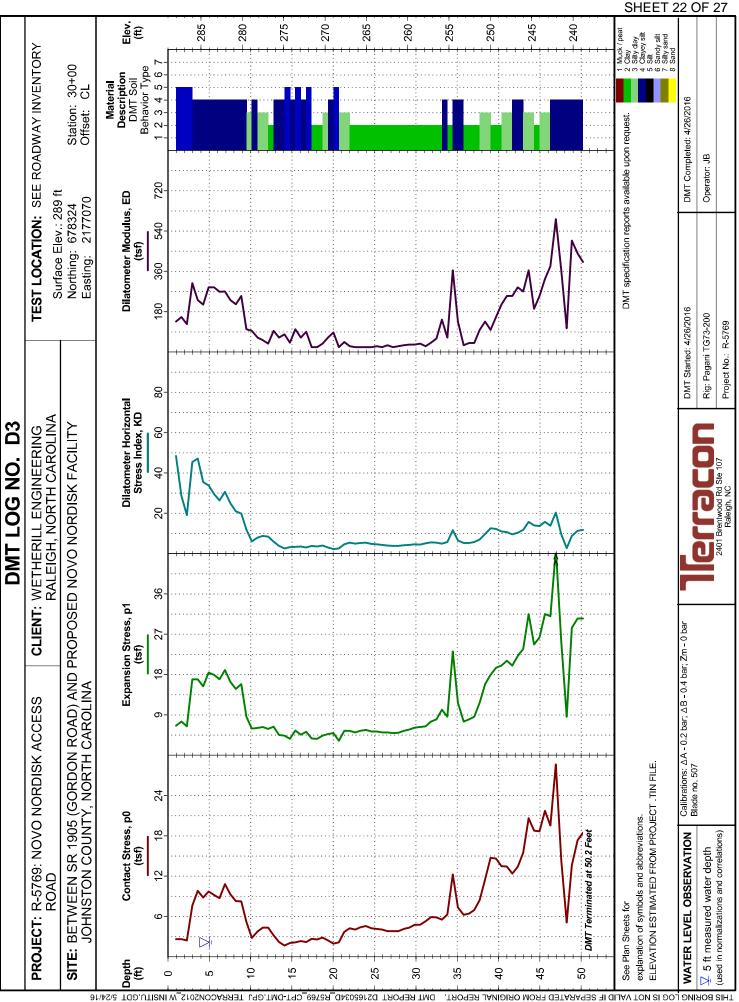


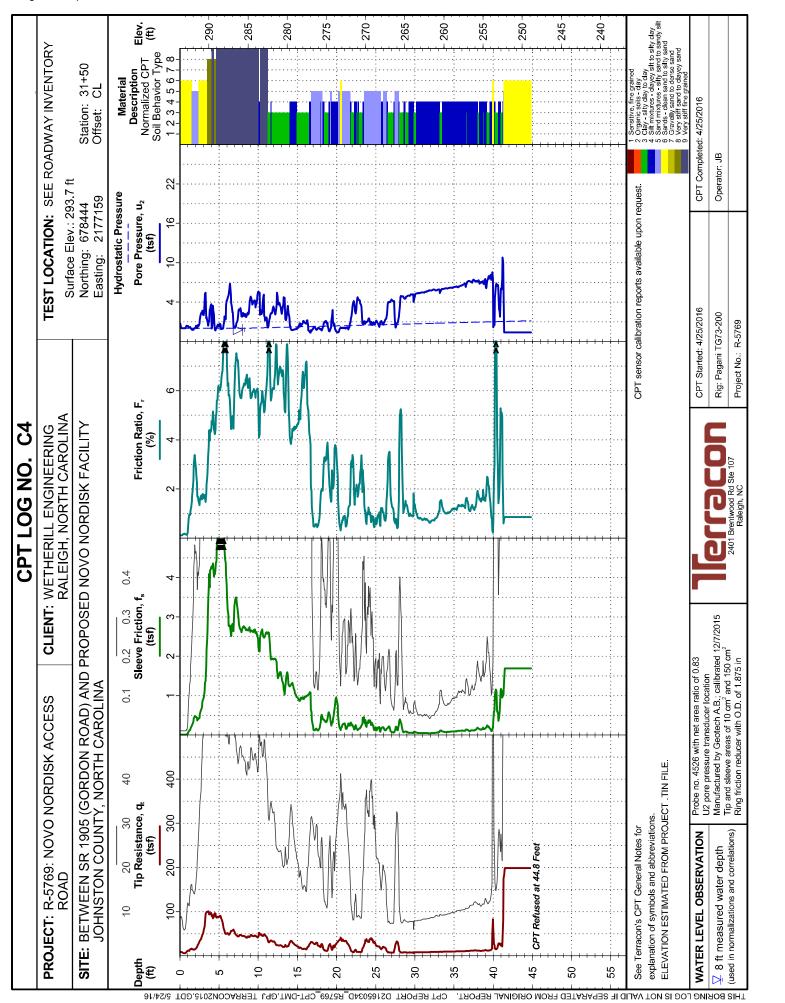


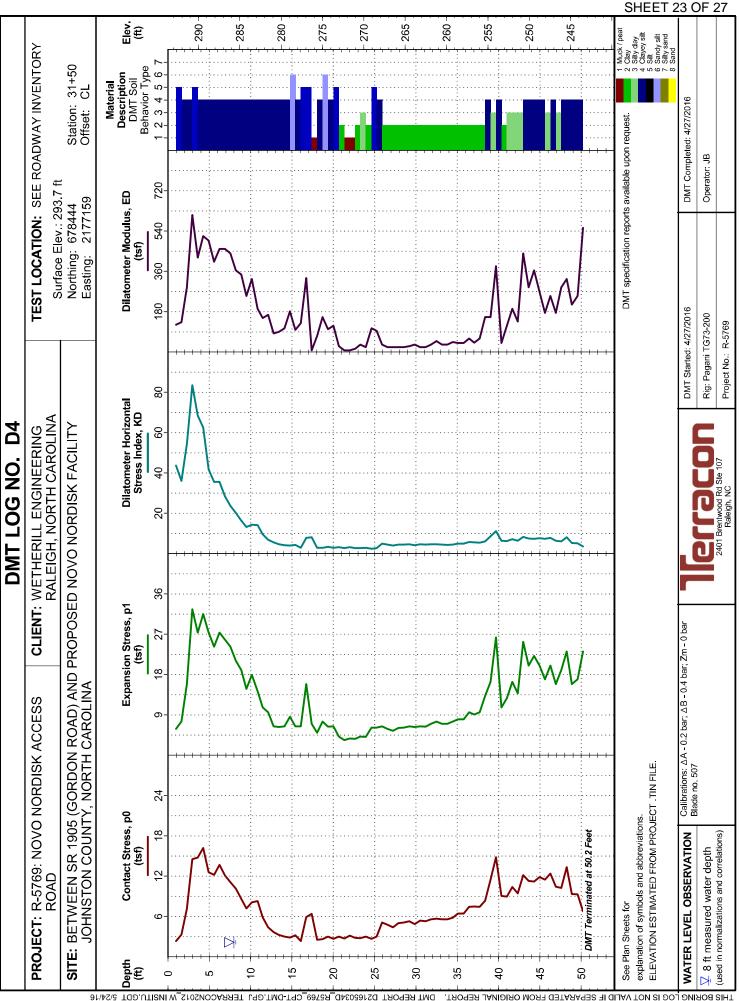
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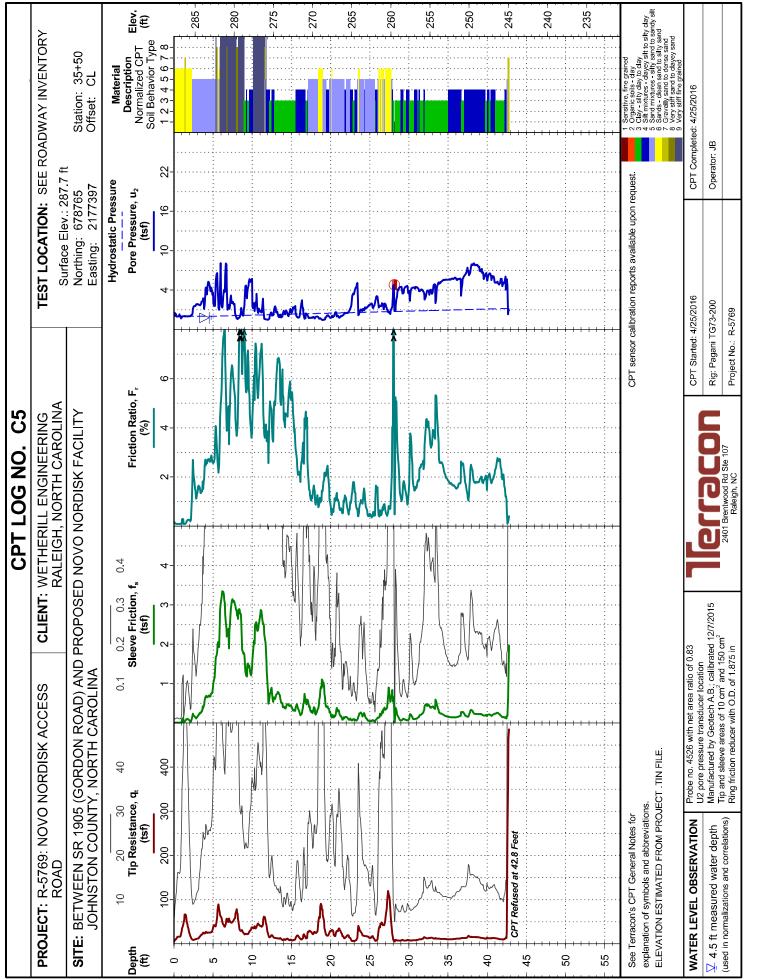
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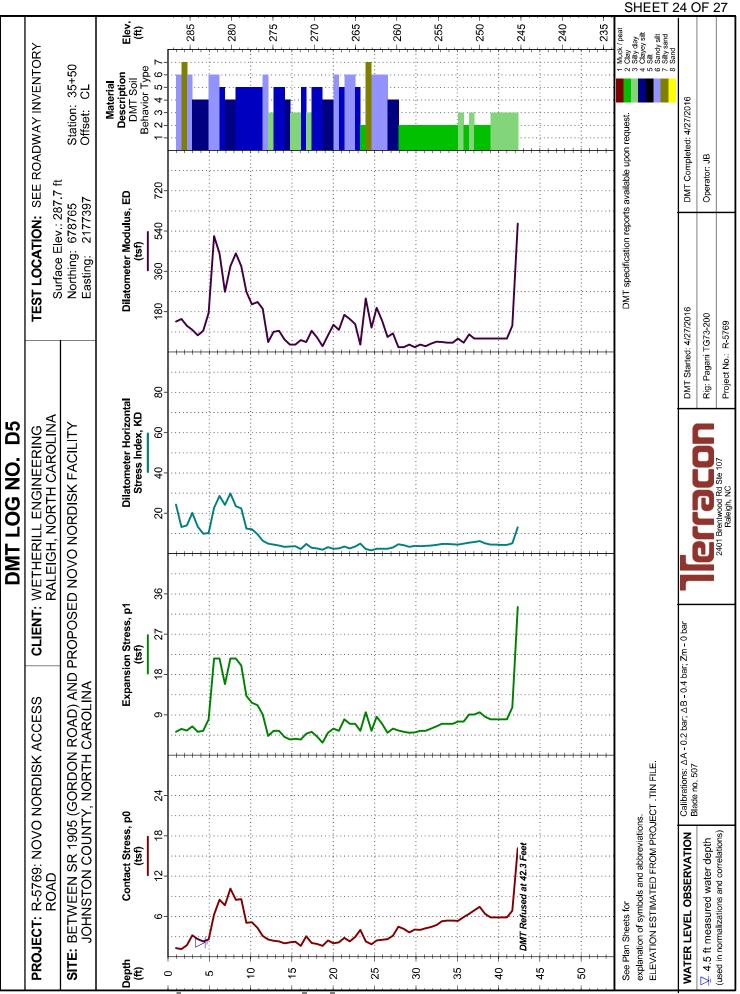






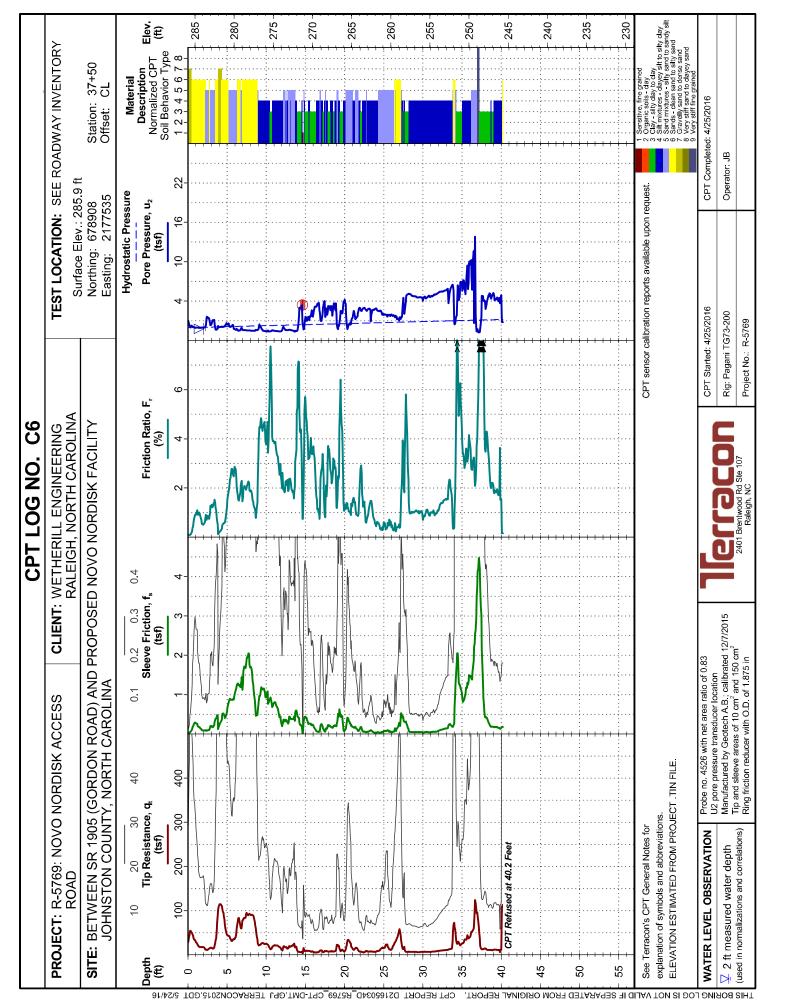


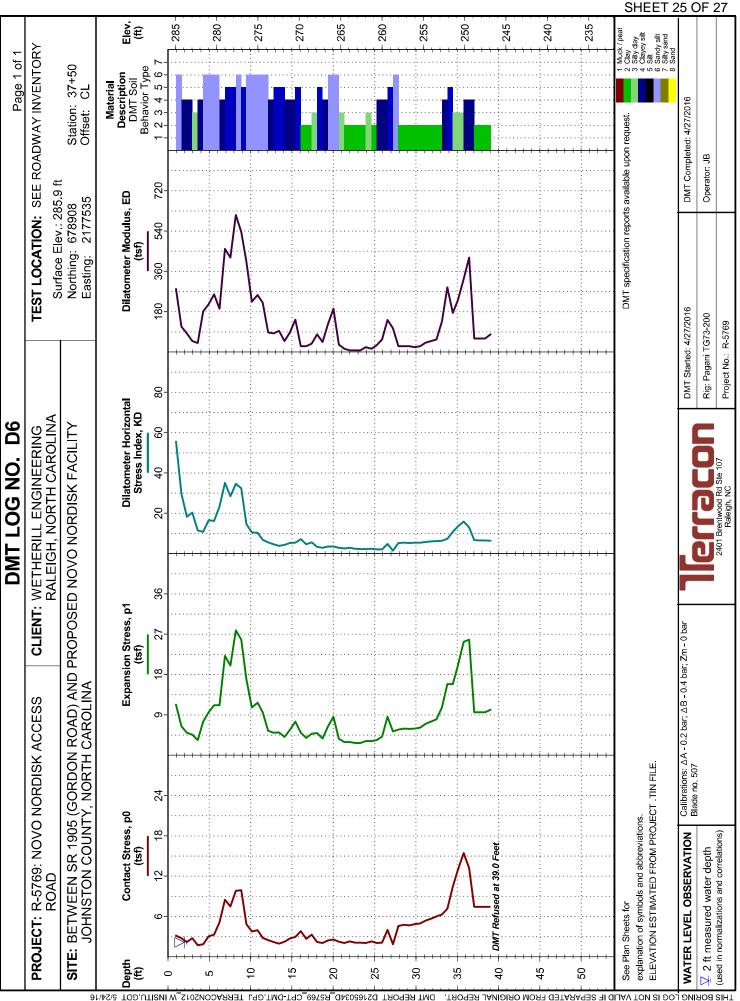




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REFERENCE: R-5769







INITIALS

SOIL LABORATORY TESTING SUMMARY

PROJECT NUMBER:

N/A

ID (TIP): R-5769

COUNTY:

DESCRIPTION: NOVO NORDISK ACCESS ROAD FROM SR 1905 (GORDON ROAD) TO PROPOSED NOVO NORDISK FACILITY

Boring No.	Sample No.	Alignment	Station	Offset (feet)	Depth Interval (feet)	AASHTO Class.	L.L.	P.I.	% by Weight				%	% Passing (sieves)				
									Coarse Sand	Fine Sand	Silt	Clay	Retained #4 Sieve	#10	#40	#200	% Moisture	° Organi
Y1REV_1753	S-1	-Y1REV-	17+53	CL	1.0 - 2.0	A-7-6 (7)	43	28	34.9	22.4	5.8	36.9	1	96	74	44	19.6	-
Y1REV_2154	S-2	-Y1REV-	21+00	9 LT	1.0 - 2.0	A-7-6 (8)	48	26	23.7	26.1	7.7	42.5	10	83	69	46	17.1	-
L_1300	S-3	-L-	13+00	CL	1.0 - 6.0	A-7-6 (7)	47	23	35.1	18.9	4.8	41.2	0	98	76	47	-	-
L_4300	S-4	-L-	43+00	CL	1.0 - 6.0	A-2-6 (1)	34	20	48.7	21.0	2.6	27.7	2	94	65	30	-	-
L 1700	SS-1	-L-	17+00	CL	3.5 - 5.0	A-2-6 (0)	39	23	53.7	15.3	4.6	26.4	15	73	43	24	10.6	-
L_1700	SS-2	-L-	17+00	CL	6.0 - 7.5	A-2-7 (0)	54	36	40.2	19.4	5.2	35.2	35	57	41	24	11.7	-
 L_2700	SS-3	-L-	27+00	CL	1.0 - 2.5	A-6 (4)	35	11	21.8	26.7	27.1	24.4	0	99	86	58	34.5	8.0
L_2700	SS-4	-L-	27+00	CL	13.5 - 15.0	A-2-7 (0)	51	33	66.4	7.8	1.6	24.2	10	81	36	22	21.9	-
 L_2700	SS-5	-L-	27+00	CL	23.5 - 25.0	A-2-6 (0)	25	14	68.2	13.4	2.0	16.4	43	41	21	8	14.7	-
L_2900	SS-6	-L-	29+00	CL	8.5 - 10.0	A-2-7 (2)	71	50	63.3	8.5	0.9	27.3	1	94	42	27	20.3	-
L_3100	SS-7	-L-	31+00	CL	6.0 - 7.5	A-7-6 (9)	55	36	46.5	12.5	2.5	38.5	0	100	77	42	24.4	-
L_3100	SS-8	-L-	31+00	CL	28.5 - 30.0	A-7-6 (8)	42	19	0.5	58.3	9.8	31.4	0	100	100	55	40.9	-
EB1-A	SS-9	-L-	32+26	17 LT	38.5 - 40.0	A-7-6 (12)	44	18	0.6	47.5	17.6	34.3	0	100	100	68	44.5	-
EB1-B	SS-10	-L-	32+26	17 RT	8.5 - 10.0	A-7-6 (13)	56	38	29.6	24.7	5.0	40.7	0	100	82	49	22.4	-
EB1-B	SS-11	-L-	32+26	17 RT	18.5 - 20.0	A-2-7 (2)	62	45	64.9	8.6	0.3	26.2	1	97	52	27	28.4	-
EB2-A	SS-12	-L-	34+27	17 LT	33.5 - 35.0	A-7-6 (7)	43	21	0.8	61.3	9.8	28.1	0	100	100	49	46.1	-
EB2-B	SS-13	-L-	34+27	17 RT	6.0 - 7.5	A-7-6 (12)	79	54	54.8	5.9	0.5	38.8	1	96	50	39	20.5	-
EB2-B	SS-14	-L-	34+27	17 RT	23.5 - 25.0	A-2-7 (1)	51	38	63.8	8.6	2.0	25.6	2	93	43	27	29.8	-
L_3500	SS-15	-L-	35+00	CL	23.5 - 25.0	A-2-6 (0)	34	22	51.6	22.2	1.0	25.2	13	81	54	23	25.0	-
L_3500	SS-16	-L-	35+00	CL	38.5 - 40.0	A-7-6 (28)	54	38	3.5	34.2	35.2	27.1	2	96	93	76	42.1	-
L_3700	SS-17	-L-	37+00	CL	18.5 - 20.0	A-6 (7)	38	26	25.8	32.8	8.6	32.8	2	97	86	45	30.5	-
L_3900	SS-18	-L-	39+00	CL	13.5 - 15.0	A-2-7 (0)	72	56	77.8	4.2	0.3	17.7	0	99	31	18	30.6	-
L_4100	SS-19	-L-	41+00	CL	1.0 - 2.5	A-6 (3)	33	18	31.6	28.8	6.6	33.0	0	99	87	41	20.4	-
L1_1400	SS-20	-L-	14+00	CL	1.0 - 2.0	A-6 (3)	34	20	41.1	21.9	6.5	30.5	2	95	71	37	25.6	-
EB2-A	ST-1	-L-	34+27	17 LT	33.5 - 36.0	A-7-6 (7)	42	17	0.2	57.2	16.4	26.2	0	100	100	55	-	-
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ST-1 TESTED BY GEOTECHNICS



JOHNSTON

Stephanie H. Huffman

Certified Lab Technician Signature

114-01-1203 Certification Number