

NOTE: SEE SHEET 2A FOR PLAN SHEET LAYOUT AT TIME OF INVESTIGATION

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STATE	STATE PROJECT REFERENCE NO.	SHEET	TOTAL
N.C.	P-5208E	1	35
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
50000.1.STR207B		P.E.	
		R/W & UTIL.	

CONTENTS

LINE	STATION	PLAN	PROFILE	XSECT
-L-	9+62.43-75+30.00	4-9	10-12	X-6, X-7, X-8 X-10, X-11 X-16, X-17 X-21, X-22 X-26, X-29 X-30, X-33 X-35, X-36 X-39, X-40 X-41, X-42
-YI-	10+00.00-17+00.00	8	12	NA

ROADWAY
SUBSURFACE INVESTIGATION

PROJ. REFERENCE NO. P-5208E F.A. PROJ. _____
COUNTY MECKLENBURG & CABARRUS
PROJECT DESCRIPTION CALDWELL PARK DRIVE EXTENSION
ON NEW LOCATION FROM CHOCHRANE FARM PROPERTY
TO EXISTING CALDWELL PARK DRIVE
INVENTORY

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF PREPARING THE SCOPE OF WORK TO BE INCLUDED IN THE REQUEST FOR PROPOSAL. THE VARIOUS FIELD BORING LOGS, ROCK CORES, AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT 1919 TOL-6850. THE SUBSURFACE PLANS, FIELD BORING LOGS, ROCK CORES, AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

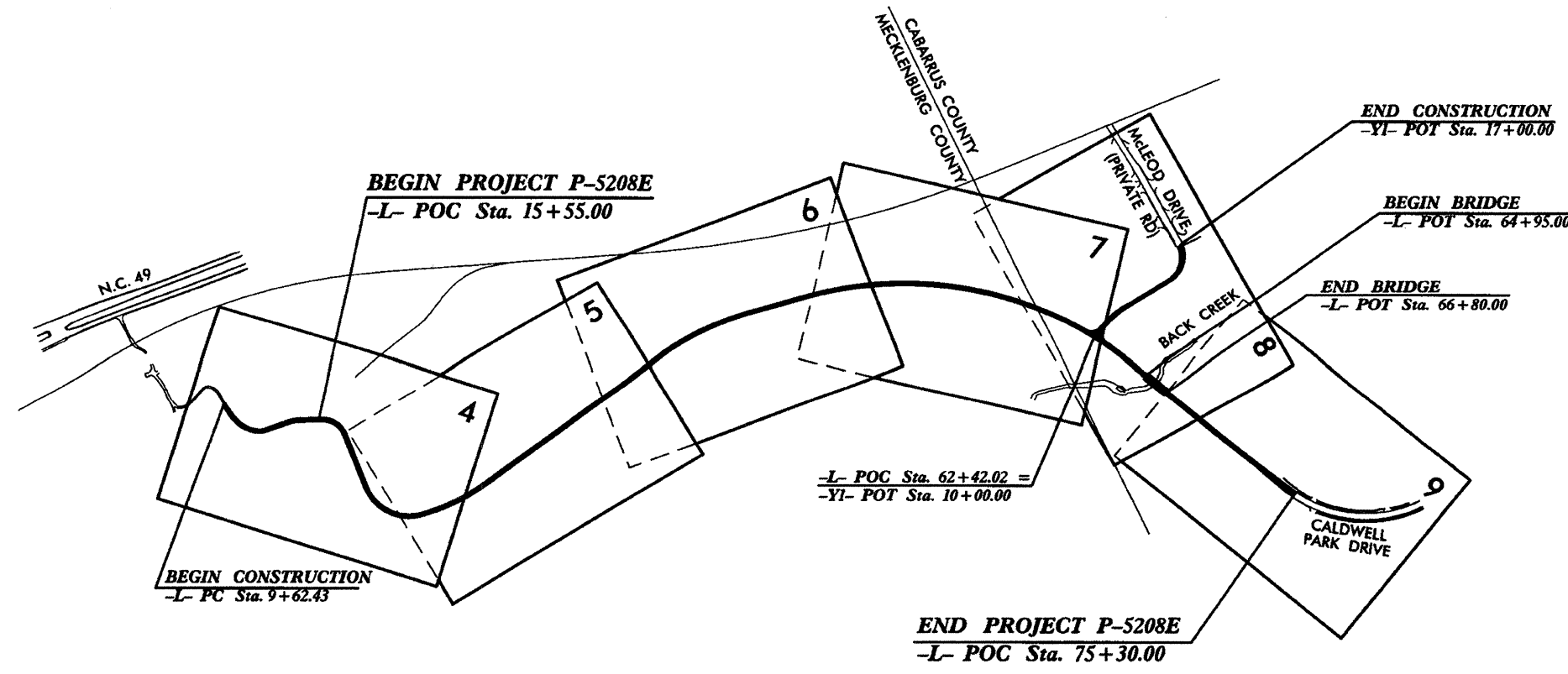
SOIL AND ROCK BOUNDARIES WITHIN A BOREHOLE ARE BASED ON GEOTECHNICAL INTERPRETATION UNLESS ENCOUNTERED IN A SAMPLE. INTERPRETED BOUNDARIES MAY NOT NECESSARILY REFLECT ACTUAL SUBSURFACE CONDITIONS BETWEEN SAMPLED STRATA AND BOREHOLE INFORMATION MAY NOT NECESSARILY REFLECT ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS, INCLUDING TEMPERATURES, PRECIPITATION, AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, OR THE OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

NOTE - THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N.C. DEPARTMENT OF TRANSPORTATION AS BEING ACCURATE NOR IS IT CONSIDERED TO BE PART OF THE PLANS, SPECIFICATIONS, OR CONTRACT FOR THE PROJECT.

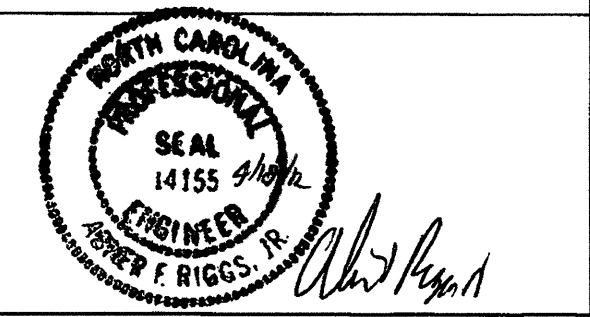
NOTE - BY HAVING REQUESTED THIS INFORMATION THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

CONTRACT: ID: P-5208E



- PERSONNEL
- J. BRANDSEN
 - M. B. MOSLEY
 - M. G. MOSLEY
 - A. F. RIGGS JR.

DRAWN BY B. RATTI
DRAWN BY _____
INVESTIGATED BY S&ME, INC.
CHECKED BY A. F. RIGGS JR.
SUBMITTED BY S&ME, INC.
DATE APRIL 19, 2012



NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION		GRADATION	ROCK DESCRIPTION		TERMS AND DEFINITIONS																																																																															
<p>SOIL IS CONSIDERED TO BE THE UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 180 BLOWS PER FOOT ACCORDING TO STANDARD PENETRATION TEST (ASTM D-1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY SHALL INCLUDE: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. EXAMPLE:</p> <p style="font-size: small; font-weight: bold;">VERY STIFF, GR. SILTY CL. W/ INT. INTERBEDDED FINE SAND LAYERS. HIGH PLAST. A-1-5</p>		<p>WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORM - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. (ALSO POORLY GRADED)</p> <p>GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLES OF TWO OR MORE SIZES.</p>	<p>HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT IF TESTED, WOULD YIELD SPT REFUSAL. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPEND SAMPLER EQUAL TO OR LESS THAN 50 BLOWS PER FOOT IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK.</p> <p>ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:</p>		<p>ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.</p> <p>ADUIFIER - A WATER BEARING FORMATION OR STRATA.</p> <p>ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.</p> <p>ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, AS SHALE, SLATE, ETC.</p> <p>ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.</p> <p>CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.</p> <p>COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.</p> <p>CORE RECOVERY (REC_c) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.</p> <p>DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.</p> <p>DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.</p> <p>DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.</p> <p>FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.</p> <p>FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.</p> <p>FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.</p> <p>FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.</p> <p>FORMATION (FM₁) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.</p> <p>JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.</p> <p>LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.</p> <p>LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.</p> <p>MOTTLED (MOTL) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLED IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.</p> <p>PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.</p> <p>RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.</p> <p>ROCK QUALITY DESIGNATION (ROQ) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.</p> <p>SAPROLITE (SAP) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.</p> <p>SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.</p> <p>SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.</p> <p>STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS IN OR BPF OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH DIAMETER SPT SPEND SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 50 BLOWS PER FOOT.</p> <p>STRATA CORE RECOVERY (SREC_c) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.</p> <p>STRATA ROCK QUALITY DESIGNATION (SRQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.</p> <p>TOPSOIL (TS) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.</p>																																																																															
		<p>ANGULARITY OF GRAINS</p> <p>THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.</p>		<p>WEATHERED ROCK (WR)</p> <p>CRYSTALLINE ROCK (CR)</p> <p>NON-CRYSTALLINE ROCK (NCR)</p> <p>COASTAL PLAIN SEDIMENTARY ROCK (CPI)</p> <p>WEATHERING</p> <p>FRESH VERY SLIGHT (V SL)</p> <p>SLIGHT (SL)</p> <p>MODERATE (MOD)</p> <p>MODERATELY SEVERE (MOD SEV)</p> <p>SEVERE (SEV)</p> <p>VERY SEVERE (V SEV)</p> <p>COMPLETE</p>																																																																																
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PL - PLASTIC LIMIT	- WET - (W)	SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE																																																																																		
OM - OPTIMUM MOISTURE	- MOIST - (M)	SOLID; AT OR NEAR OPTIMUM MOISTURE																																																																																		
SL - SHRINKAGE LIMIT	- DRY - (D)	REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE																																																																																		
PLASTICITY		EQUIPMENT USED ON SUBJECT PROJECT				BEDDING																																																																														
<table border="1" style="width:100%; font-size: x-small;"> <tr> <th>NONPLASTIC</th> <th>PLASTICITY INDEX (PI)</th> <th>DRY STRENGTH</th> </tr> <tr> <td>LOW PLASTICITY</td> <td>0-5</td> <td>VERY LOW</td> </tr> <tr> <td>MED. PLASTICITY</td> <td>6-15</td> <td>SLIGHT</td> </tr> <tr> <td>HIGH PLASTICITY</td> <td>16-25</td> <td>MEDIUM</td> </tr> <tr> <td></td> <td>26 OR MORE</td> <td>HIGH</td> </tr> </table>		NONPLASTIC	PLASTICITY INDEX (PI)	DRY STRENGTH	LOW PLASTICITY	0-5	VERY LOW	MED. PLASTICITY	6-15	SLIGHT	HIGH PLASTICITY	16-25	MEDIUM		26 OR MORE	HIGH	<p>EQUIPMENT USED ON SUBJECT PROJECT</p> <p>ADVANCING TOOLS:</p> <p><input type="checkbox"/> CLAY BITS <input type="checkbox"/> 6" CONTINUOUS FLIGHT AUGER <input type="checkbox"/> B' HOLLOW AUGERS <input type="checkbox"/> HARD FACED FINGER BITS <input type="checkbox"/> TUNG. CARBIDE INSERTS <input type="checkbox"/> CASING <input type="checkbox"/> W/ ADVANCER <input type="checkbox"/> TRICONE * STEEL TEETH <input type="checkbox"/> TRICONE * TUNG. CARB. <input type="checkbox"/> CORE BIT</p> <p>HAMMER TYPE: <input checked="" type="checkbox"/> AUTOMATIC <input type="checkbox"/> MANUAL</p> <p>CORE SIZE: <input type="checkbox"/> B <input type="checkbox"/> N <input type="checkbox"/> H</p> <p>HAND TOOLS:</p> <p><input type="checkbox"/> POST HOLE DIGGER <input type="checkbox"/> HAND AUGER <input type="checkbox"/> SOUNDING ROD <input type="checkbox"/> VANE SHEAR TEST</p>				<p>VERY THICKLY BEDDED</p> <p>THICKLY BEDDED</p> <p>THINLY BEDDED</p> <p>VERY THINLY BEDDED</p> <p>THICKLY LAMINATED</p> <p>THINLY LAMINATED</p>																																																															
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	26 OR MORE	HIGH																																																																																		
COLOR		INDURATION				BENCH MARK																																																																														
<p>DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.</p>		<p>FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF THE MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.</p> <p>FRITABLE</p> <p>MODERATELY INDURATED</p> <p>INDURATED</p> <p>EXTREMELY INDURATED</p>				<p>BENCH MARK: R/R SPIKE SET IN FIRST JOINT OF CONC. C&G AT EOP ON EAST SIDE OF PRIVATE DRIVE STA 360+18.91 163.38' RT -BL- ELEVATION: 664.51 FT.</p> <p>NOTES: BRIDGE BORINGS EB1-A, EB1-B, BI-A, BI-B, EB2-A AND EB2-B TO BE SUBMITTED IN BRIDGE INVENTORY REPORT UNDER SEPARATE COVER.</p>																																																																														

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	P-5208E	2A	
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
50000.1.STR20TIB		P.E.	

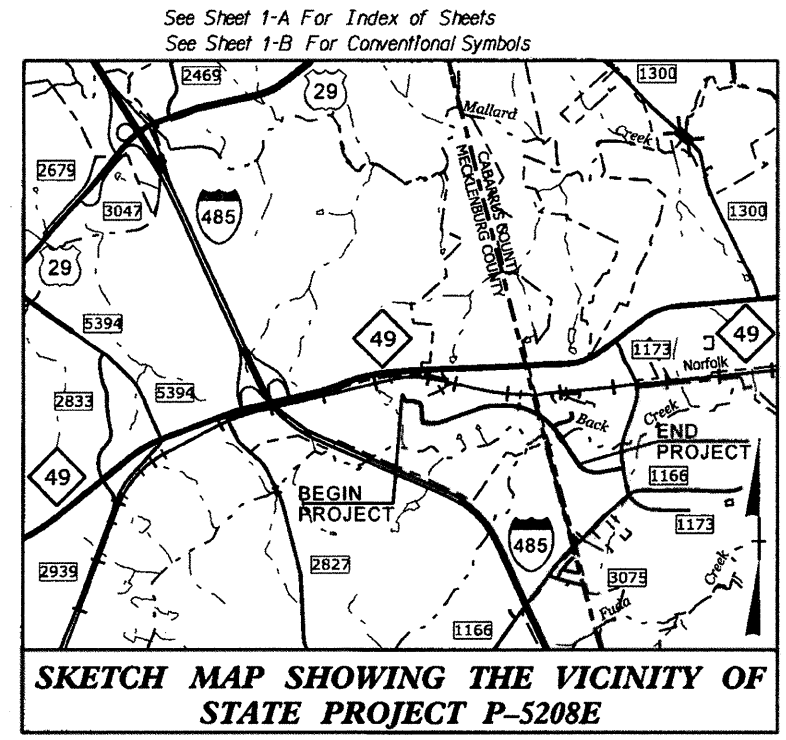


STATE OF NORTH CAROLINA
NCDOT RAIL DIVISION

**MECKLENBURG & CABARRUS
COUNTIES**

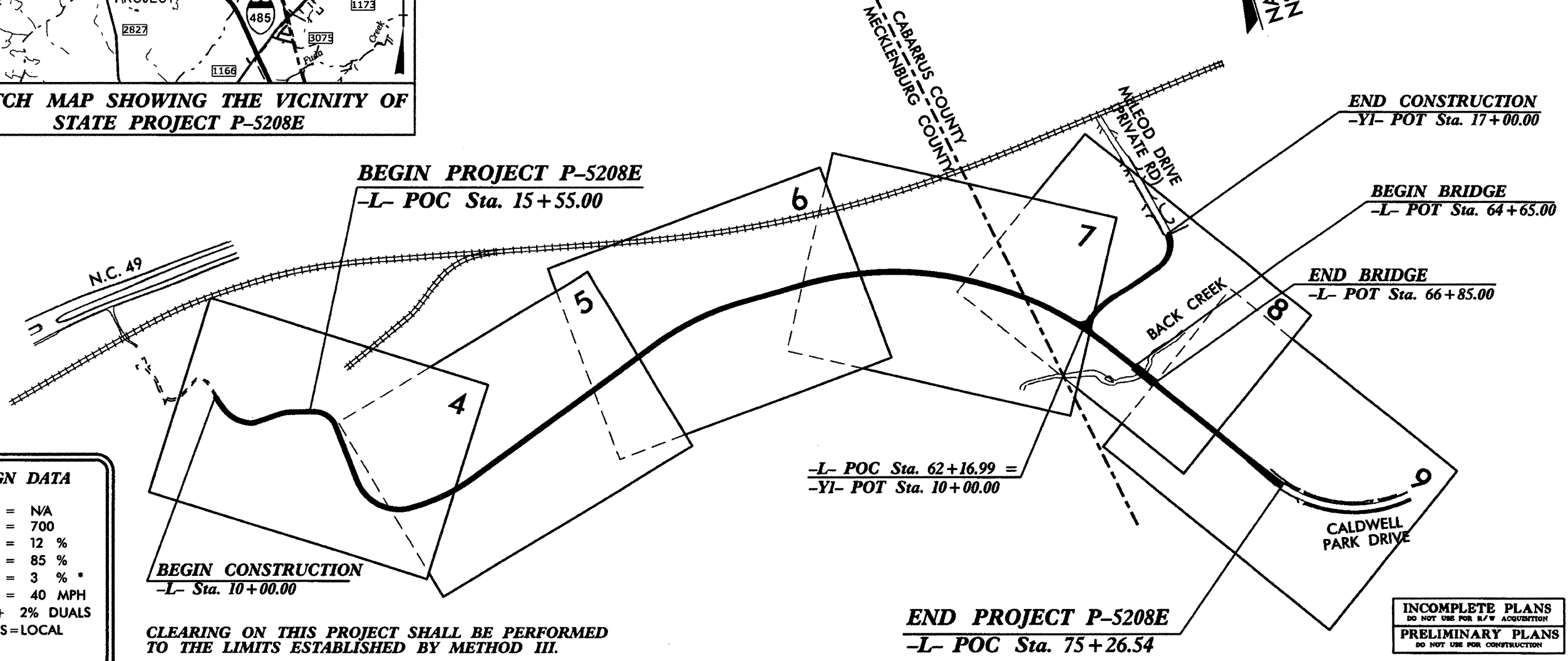
**LOCATION: CALDWELL PARK DRIVE EXTENSION
ON NEW LOCATION FROM COCHRANE
FARM PROPERTY TO EXISTING CALDWELL
PARK DRIVE**

TYPE OF WORK: GRADING, DRAINAGE, PAVING, AND STRUCTURES



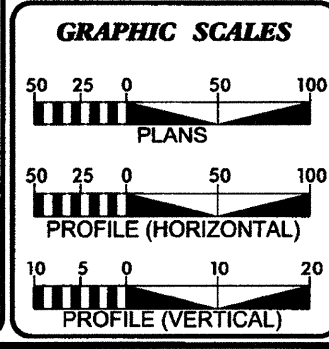
SKETCH MAP SHOWING THE VICINITY OF
STATE PROJECT P-5208E

TIP PROJECT: P-5208E



DESIGN DATA

ADT 2012 = NA
ADT 2035 = 700
DHV = 12 %
D = 85 %
T = 3 % *
V = 40 MPH
* 1% TTST + 2% DUALS
FUNC CLASS = LOCAL



PROJECT LENGTH

LENGTH ROADWAY TIP PROJECT P-5208E = 1.096 MILES
LENGTH STRUCTURES TIP PROJECT P-5208E = 0.035 MILES
TOTAL LENGTH TIP PROJECT P-5208E = 1.131 MILES

SUBMITTAL: 25% PLANS
DATE: NOVEMBER 17, 2011

Prepared In the Office of:

Florence & Hutcheson
CONSULTING ENGINEERS
3121 Kipling Way, Suite 100 Raleigh, NC 27607
NC License No. T-0228

2012 STANDARD SPECIFICATIONS

DAVID C. WALLER, PE
PROJECT ENGINEER

LETTING DATE: APRIL 16, 2013
RIGHT OF WAY DATE: APRIL 16, 2012

ROADWAY DESIGN ENGINEER

SIGNATURE: _____ P.E.

HYDRAULICS ENGINEER

SIGNATURE: _____ P.E.

NC DEPARTMENT OF
TRANSPORTATION
RAIL DIVISION

ENGINEERING AND SAFETY BRANCH
CAPITAL TASK
MS MARSH SERVICE CENTER
RALEIGH, NC 27601

INCOMPLETE PLANS
DO NOT USE FOR R/W ACQUISITION
PRELIMINARY PLANS
DO NOT USE FOR CONSTRUCTION

B:\APR-2012_09-13
S:\PROJECTS\2011\11-285_CaldwellRd_P-5208E\Standard DOT Structure\GEO TECH\DOT\Cadd Files\TIP\P5208E.GEO.RDWY\CADD_GEO TECH\PlanPro\Fp5208e_rdy_tsh.dgn
BRGHT AT BRAT 11-13-2011

Earthwork Balance Sheet

Volumes in Cubic Yards

PROJECT: P-5208E

COUNTY: Cabarrus / Mecklenburg

DATE: 2/12/2013

COMPILED BY: DCW

SHEET 3 OF 35 SHEETS

STATION	STATION	EXCAVATION					EMBANKMENT				BORROW	WASTE			
		TOTAL UNCLASS.	ROCK	UNDERCUT	UNCLAS. UNSUIT.	SUITABLE UNCLASS.	TOTAL	ROCK	EARTH	EMBANK. +20%		ROCK	SUITABLE	UNCLAS. UNSUIT.	TOTAL
-L- 9+63.43	-L- 30+00.00	4,914	59	1,018	170	4,685	6,455	59	6,382	7,717	2,973			1,188	1,188
	SUBTOTAL	4,914	59	1,018	170	4,685	6,455	59	6,382	7,717	2,973			1,188	1,188
-L- 30+00.00	-L- 64+95.00	81,207	33	2,257	4,915	76,259	38,821	33	38,780	46,569		29,723	7,172	36,895	
-Y1- 10+50.00	-Y1- 17+00.00	466				466	13,783		13,783	16,540	16,074				
	SUBTOTAL	81,673	33	2,257	4,915	76,725	52,604	33	52,563	63,109	16,074		29,723	7,172	36,895
-L- 66+80.00	-L- 75+30.00	640		2,478	396	244	15,792		15,792	18,950	18,706			2,874	2,874
	SUBTOTAL	640		2,478	396	244	15,792		15,792	18,950	18,706			2,874	2,874
	TOTAL	87,227	91	5,753	5,481	81,655	74,851	91	74,737	89,776	37,753		29,723	11,234	40,957
MATERIAL FOR SHOULDER CONSTRUCTION							500		500	600	600				
LOSS DUE TO CLEARING & GRUBBING		-10,680				-10,680					10,680				
ADDITIONAL UNDERCUT				8,200			8,200		8,200	9,840	9,840			8,200	8,200
ROCK WASTE TO REPLACE BORROW															
ADJUST FOR ROCK WASTE															
WASTE IN LIEU OF BORROW											-29,723		-29,723		-29,723
PROJECT TOTAL		76,547	91	13,953	5,481	70,975	83,551	91	83,437	100,216	29,150			19,434	19,434
EST. 5% TO REPLACE TOP SOIL ON BORROW PIT											1,457				
GRAND TOTAL		76,547	91	13,953	5,481	70,975	83,551	91	83,437	100,216	30,607			19,434	19,434
SAY		76,560		13,960							30,650				

Approx. quantities only. Borrow, fine grading, clearing & grubbing and removal of existing pavement will be paid for at the lump sum price for "Grading".

EST. DDE = 1000 CUBIC YARDS

SHOULDER BORROW = 500 CUBIC YARDS

EST. SHALLOW UNDERCUT = 750

EST. SHALLOW UNDERCUT BY STATIONS = 0

TOTAL SHALLOW UNDERCUT = 750

CLASS IV SUBGRADE STABILIZATION = 2,200 TONS

PER GEOTECH RECOMMENDATION, ESTIMATED 8,200 CUBIC YARDS OF UNDERCUT TO BE USED IN THE DISCRETION OF THE RESIDENT ENGINEER.

TO: Simpson Engineers & Associates
5520 Dillard Drive, Suite 120
Cary, North Carolina 27518

ATTENTION: Mr. Andy Batts, P.E.

FROM: S&ME, Inc.
3201 Spring Forest Road
Raleigh, North Carolina 27616

STATE PROJECT: 50000.1.STR20T1B
FEDERAL PROJECT: N/A
TIP NUMBER: P-5208E
COUNTY: Mecklenburg and Cabarrus
S&ME PROJECT NO. 1051-11-285
DESCRIPTION: Caldwell Park Drive Extension Grade Separation
SUBJECT: Roadway Subsurface Investigation – Inventory Report

Project Description

S&ME, Inc. has completed the authorized roadway inventory report for the above referenced project. This report was performed in accordance with our Subconsultant Agreement for Professional Services between Simpson Engineers & Associates and S&ME, Inc. dated September 16, 2011 and the terms and conditions stated within. This project is located southwest of Harrisburg, North Carolina in Mecklenburg and Cabarrus County. The proposed project consists of extending Caldwell Park Drive, on new location, from Chochrane farm property to existing Caldwell Park Drive. The roadway will consist of a two lane roadway with curb and gutter. A new bridge will be constructed along the new Caldwell Park Drive alignment between (Stations 65+00 to 66+85 -L-) over Back Creek.

A geotechnical investigation was conducted between January 31, 2012 and February 9, 2012 by performing soil test borings. Drilling consisted of advancing 3-1/4 inch diameter hollow stem augers with standard penetration testing by a Diedrich D-50 drill rig mounted on an all-terrain carrier. The Diedrich D-50 drill rig is equipped with an automatic hammer. The roadway was investigated with thirty-three (33) soil test borings (B-1 through B-27, B-21A, B-23A and B-27A -L-) and (B-28 through B-30 -Y1-) including borings EB1-B, B1-B and EB2-B at the proposed bridge location. The borings were advanced to depths ranging from about 6.0 to 35.0 feet (elevations 675.4 to 598.4 feet) at collar elevations ranging from about 685.4 to 606.4 feet. Representative split-spoon soil samples were collected for visual classification and selected soil samples were submitted for laboratory analysis. Laboratory testing was performed in accordance with the AASHTO Soil Classification System.

The following survey lines were investigated.

<u>Line</u>	<u>Station</u>
-L-	9+62.43 to 75+30
-Y1-	10+00 to 17+00

Areas of Special Geotechnical Interest

- 1) Highly Plastic Soils: Areas were identified that contain soils that have plasticity indices of 35 or higher within the upper 2 feet of proposed grade within the following locations:

<u>Line</u>	<u>Station</u>
-L-	15+00 to 19+00
-L-	21+50 to 24+00
-L-	31+50 to 34+00
-L-	60+85 to 61+50
-L-	72+50 to 75+30

- 2) Crystalline Rock: Crystalline rock was encountered at or near proposed roadway grades within the following locations:

<u>Line</u>	<u>Station</u>
-L-	29+00 to 29+40
-L-	60+00 to 60+70

- 3) Alluvial Soils : The following areas contain relatively soft or wet soils which have the potential for subgrade problems during construction. In addition, these soils may contain cohesive soils or organic materials which may cause embankment instability or long term settlement problems.

<u>Line</u>	<u>Station</u>
-L-	40+90 to 44+90
-L-	48+50 to 49+25
-L-	63+50 to 66+85

- 4) Artificial Fill: Poorly compacted artificial fill exist above existing underground utilities including unpaved roadways, sewer easements and in areas where previous grading has occurred. Artificial fill material was encountered at the following locations:

<u>Line</u>	<u>Station</u>
-L-	60+85 to 61+50
-Y1-	69+75 to 75+30

Physiography and Geology

The site is located within the Western Piedmont Physiographic and Geologic Province of North Carolina. The Piedmont Province is characterized by gently to steeply sloping topography with well-rounded hills and along rolling ridges with a northeast-southwest trend dissected by a moderate to well developed (mature) dendritic-type drainage system consisting of drainage swales, hollows, tributaries, streams and rivers.

More specifically, the site is located within the Charlotte Belt. Based on previous mapping (N.C. Geologic Map 1985) and our knowledge of the local geology, the parent rock is interpreted to be felsic metavolcanic rock. These rocks typically weather irregular with shallow to deep residual soils overlying saprolite to bedrock.

Soil Properties

Soils present on this project are separated into three major categories based on origin. These categories include artificial fill, alluvial and residual soils.

Artificial fill materials were found in association with previous construction, utility easements and unpaved roadways in borings B-23, B-26, B-27 and B-27A. The depth of the fill materials ranged from about 2 to 9.5 feet. The fill materials encountered consist of soft to medium stiff red-brown and tan-orange highly plastic fine sandy silty clay (A-7-5, A-7-6). The standard penetration test (SPT) N-values in these soils ranged from 3 to 13 blows per foot (bpf). These soils appeared to be moist.

Alluvial deposits were encountered at the ground surface within drainage features (B-13, B-14 and B-17), and within the Back Creek flood plain (EB1-B, B1-B and EB2-B) to depths ranging from about 3 to 7 feet beneath the ground surface. Typically, alluvial deposits encountered consist of medium dense brown, clayey fine to coarse sand (A-2-4) and soft to medium stiff red-brown and brown fine to coarse sandy silty clay (A-7-5 and A-6) and slightly clayey fine to coarse sandy silt (A-4). N-values for the alluvial soils encountered ranged from 1 to 18 bpf.

Residual soils were encountered at the ground surface in borings B-1 through B-12, B-15, B-16, B-18 through B-23A, B-24, B-25 and B-28, B-29, B-30, and beneath the artificial fill and alluvium in the remaining borings. The residual soils consist of medium stiff to hard tan, brown and green-gray fine sandy silt (A-4), medium stiff to hard red-orange, orange-tan low to highly plastic coarse to fine sandy silty clay (A-6, A-7-5) and dense tan-white silty fine to coarse sand (A-2-4). The SPT N-values for the residual soils ranged from 6 to 78 bpf. The residual soils transition to weathered rock in borings B-7, B-8, B-9, B-15, B-18, B-19, B-21, B-22, B-23A, B-24, EB1-B, B1-B, B-28, B-29, B-30 at depths ranging from about 3 to 18.5 feet (elevations 675.6 to 599.4 feet) and extend to the depth of boring termination. Borings B-19 and B-32 encountered 3.5 to 4.5 feet thick ledges of weathered rock within the highly weathered residual soils. N-values in the weathered rock exceed 100 blows per foot.

Auger refusal material on crystalline rock (Metavolcanic) was encountered in borings B-7, B-23A, B-24, EB1-B, B1-B, EB2-B and B-29 at depths of approximately 5 to 22.6 feet (elevations of 672.5 to 605.8 feet) beneath the ground surface.

Groundwater

Groundwater was encountered only in the borings located adjacent to drainage features and the Back Creek flood plain (B-17 and B1-B). Water levels at these locations were measured at depths of about 1 and 6.5 feet (elevations 639.0 to 599.9 feet) beneath the ground surface. The elevation of the Back Creek at the time of our investigation was at about elevation 601.9 feet. In the higher elevation portions of the site, groundwater generally occurs greater than 10 feet below proposed grades. The potential for perched water levels is likely in most of the upland areas where stiff to hard relatively impermeable clays and silts exist as the surface.

Geotechnical Descriptive Analysis

For descriptive purposes, the project has been divided into three segments. The division of the alignments into three segments is based on the near surface and subsurface materials.

Segment I

-L-	9+62.43 to 40+90
-L-	44+90 to 48+50
-L-	49+25 to 52+50
-L-	60+75 to 63+50
-L-	66+80 to 75+30
-Y1-	10+00 to 17+00

Segment I consists of areas near grade or requiring fill above residual soils and cut sections along the alignment which will require excavations of about 8 to 10 feet of residual soils to reach design grades. The majority of this section consists of residual soils as described in the Soil Properties section of this report. These sections consist of extending the existing roadway along the alignments with typical construction methods. Segment I makes up approximately 80 percent of the investigated alignment.

Segment II

-L-	40+90 to 44+90
-L-	48+50 to 49+25
-L-	63+50 to 64+85

Segment II consists of areas requiring 10 to 20 feet of embankment fill above soft alluvial soils. Approximately 8 percent of the investigation falls within Section II.

Segment III


-L- 52+50 to 60+75



Segment III consists of areas requiring excavation depths of 10 to 25 feet in very stiff to hard residual soils and weathered rock materials. Approximately 12 percent of the investigation falls within Section III.

S&ME appreciates the opportunity to be your geotechnical consultant on this project.
If you have any questions or need additional information in regard to this report, please contact us.

Very truly yours,

S&ME, Inc.

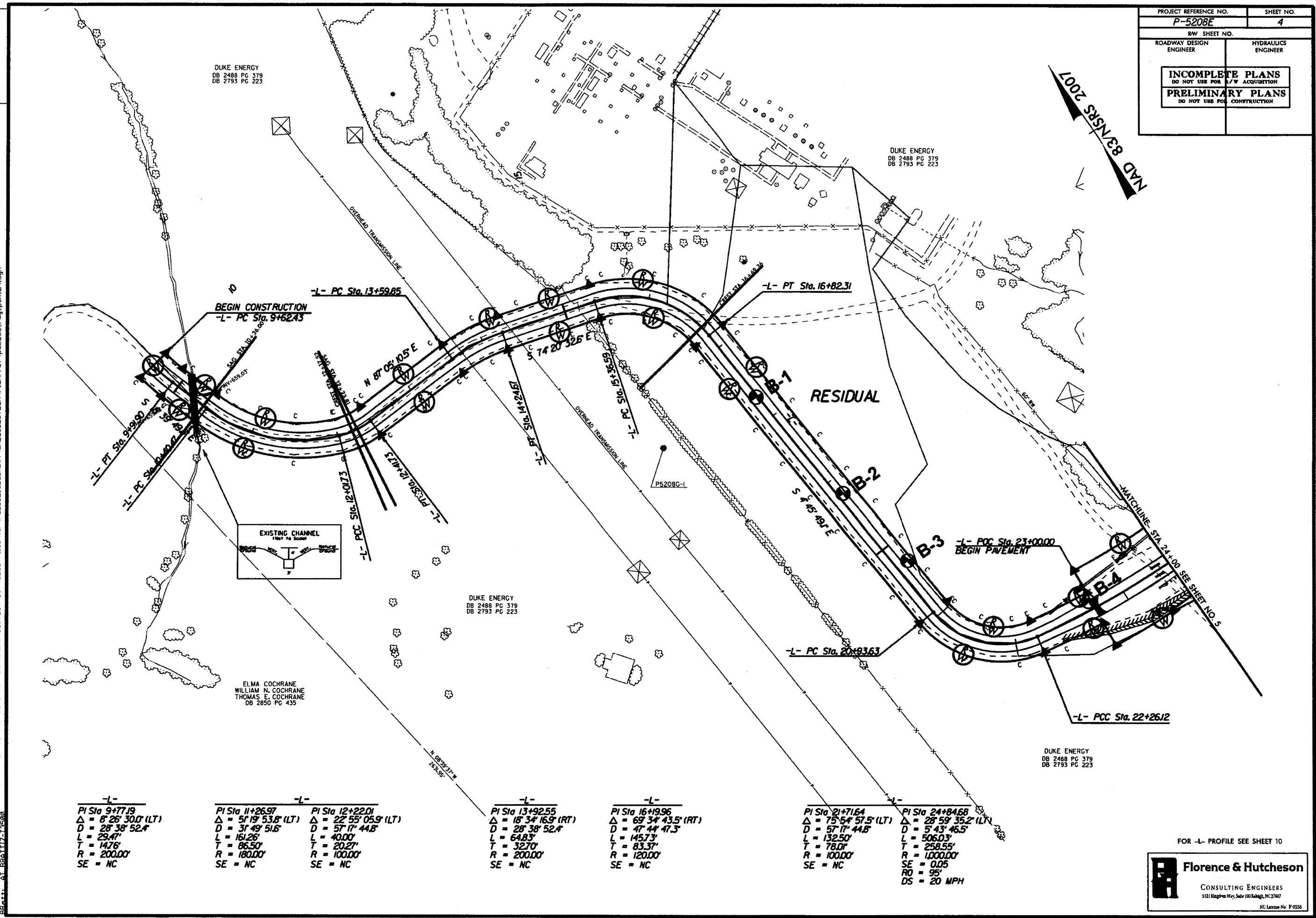

Nicole Bradley P.G.
Professional Geologist


Abner F. Riggs, Jr.,
Senior Geotechnical Engineer
N.C. Registration No. 14155


Attachments

S:\PROJECTS\2011\11-285Caldwell Park Drive Extension\Geotech DOT\Report\11-285 rpt Inventory.doc

PROJECT REFERENCE NO. P-5208E	SHEET NO. 4
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR A/W ACQUISITION PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	



I:\APR 2007\5208E\Standard DOT Structure\GEO TECH\DOT\Cadd Files\TIP\PS208E.GEO.RDW\CADD.GEOTECH\Plan\Prof\p5208e_rdy_psh_04.dgn

-L- PI Sta 9+77.19 $\Delta = 8^{\circ} 26' 30.0''$ (LT) $D = 28^{\circ} 38' 52.4''$ $L = 29.47'$ $T = 14.76'$ $R = 200.00'$ $SE = NC$	-L- PI Sta 11+26.97 $\Delta = 51^{\circ} 19' 53.8''$ (LT) $D = 31^{\circ} 49' 51.6''$ $L = 161.26'$ $T = 86.50'$ $R = 180.00'$ $SE = NC$	-L- PI Sta 12+22.01 $\Delta = 22^{\circ} 55' 05.9''$ (LT) $D = 57^{\circ} 17' 44.8''$ $L = 40.00'$ $T = 20.27'$ $R = 100.00'$ $SE = NC$	-L- PI Sta 13+92.55 $\Delta = 18^{\circ} 34' 16.9''$ (RT) $D = 28^{\circ} 38' 52.4''$ $L = 64.83'$ $T = 32.70'$ $R = 200.00'$ $SE = NC$	-L- PI Sta 16+19.96 $\Delta = 69^{\circ} 34' 43.5''$ (RT) $D = 47^{\circ} 44' 47.3''$ $L = 145.73'$ $T = 83.37'$ $R = 120.00'$ $SE = NC$	-L- PI Sta 21+71.64 $\Delta = 75^{\circ} 54' 57.5''$ (LT) $D = 57^{\circ} 17' 44.8''$ $L = 132.50'$ $T = 78.01'$ $R = 100.00'$ $SE = NC$	-L- PI Sta 24+84.68 $\Delta = 28^{\circ} 59' 35.2''$ (LT) $D = 5^{\circ} 43' 46.5''$ $L = 506.03'$ $T = 258.55'$ $R = 1000.00'$ $SE = 0.05$ $RO = 95'$ $DS = 20 MPH$
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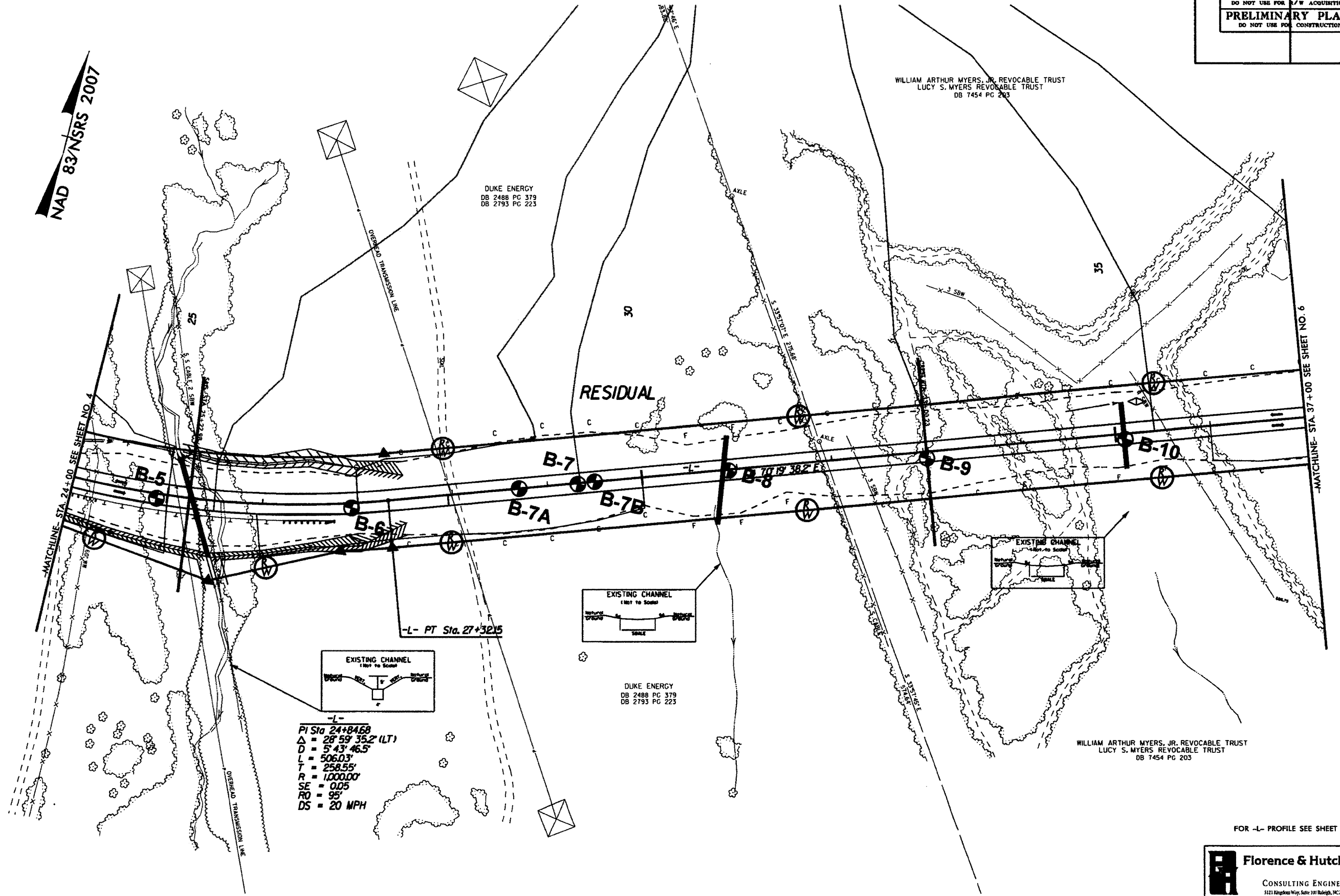
FOR -L- PROFILE SEE SHEET 10

Florence & Hutcheson
 CONSULTING ENGINEERS
 5121 Kingsley Way, Suite 100 Raleigh, NC 27607
 NC License No. P-0255

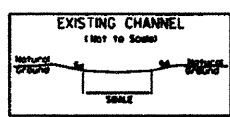
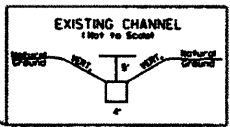
PROJECT REFERENCE NO. P-5208E	SHEET NO. 5
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR A/W ACQUISITION PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

NAD 83/NSRS 2007

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 11/11/12 10:50 AM
 11/11/12 10:50 AM



-L-
 PI Sta. 24+84.68
 $\Delta = 28^{\circ} 59' 35.2''$ (LT)
 $D = 5' 43.465''$
 $L = 506.03'$
 $T = 258.55'$
 $R = 1,000.00'$
 $SE = 0.05$
 $RO = 95'$
 $DS = 20$ MPH



DUKE ENERGY
 DB 2488 PG 379
 DB 2793 PG 223

WILLIAM ARTHUR MYERS, JR. REVOCABLE TRUST
 LUCY S. MYERS REVOCABLE TRUST
 DB 7454 PG 203

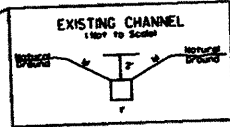
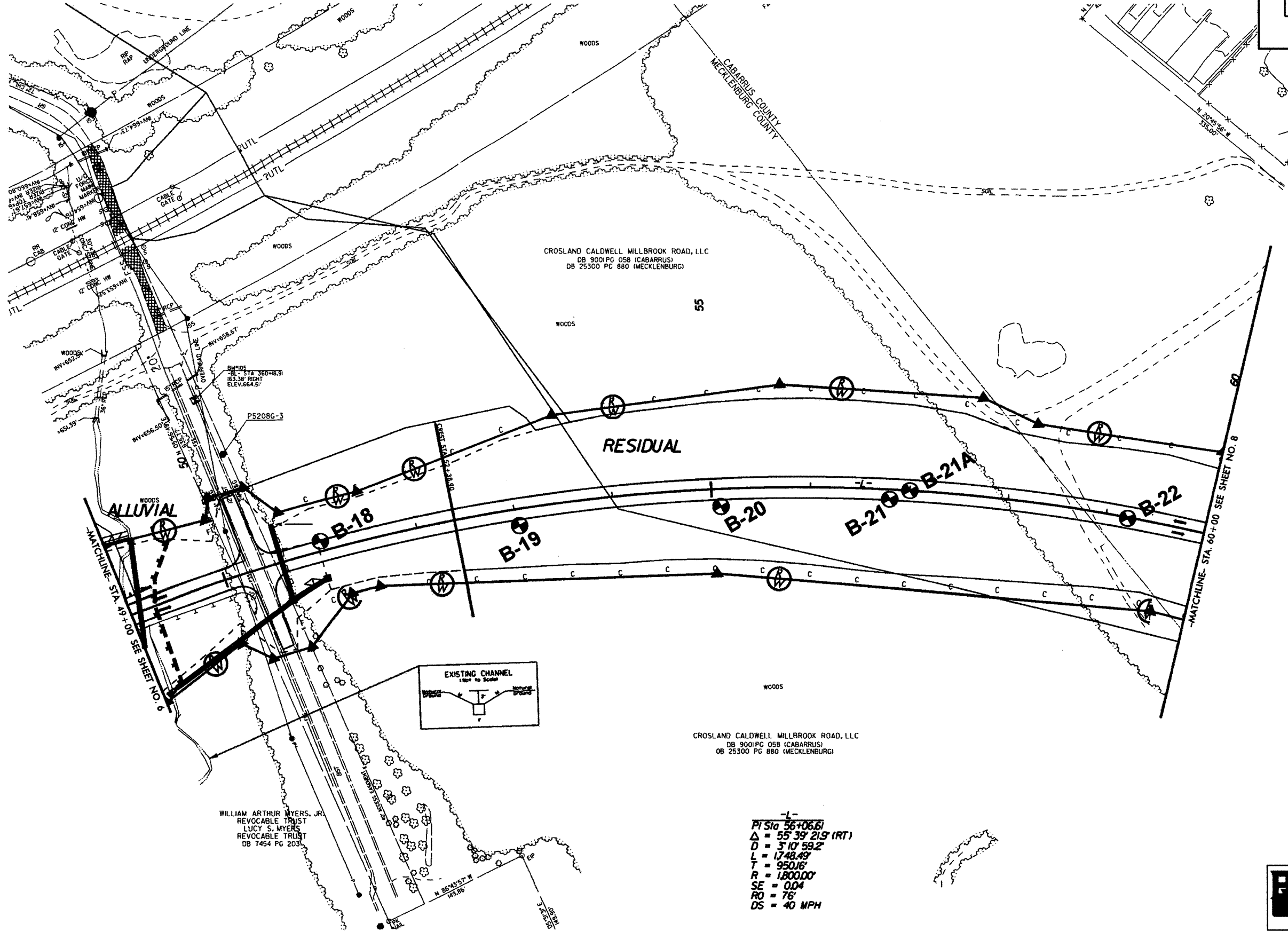
FOR -L- PROFILE SEE SHEET 10


Florence & Hutcheson
 CONSULTING ENGINEERS
 5121 Kingsley Way, Suite 101 Raleigh, NC 27607
 NC License No. F-0288

PROJECT REFERENCE NO. P-5208E		SHEET NO. 7	
RW SHEET NO.			
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION		PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

FOR DETAIL OF CROSSING CLOSURE, SEE SHEET NO. 2C

MAD 83/NBS 2007



CROSLAND CALDWELL MILLBROOK ROAD, LLC
DB 9001 PG 058 (CABARRUS)
DB 25300 PG 880 (MECKLENBURG)

-L-
PI Sta 56+06.61
 $\Delta = 55^{\circ} 39' 21.9'' (RT)$
D = 3' 10' 59.2"
L = 1748.49'
T = 950.16'
R = 1,800.00'
SE = 0.04
RO = 76'
DS = 40 MPH

WILLIAM ARTHUR MYERS, JR.
REVOCABLE TRUST
LUCY S. MYERS
REVOCABLE TRUST
DB 7454 PG 203

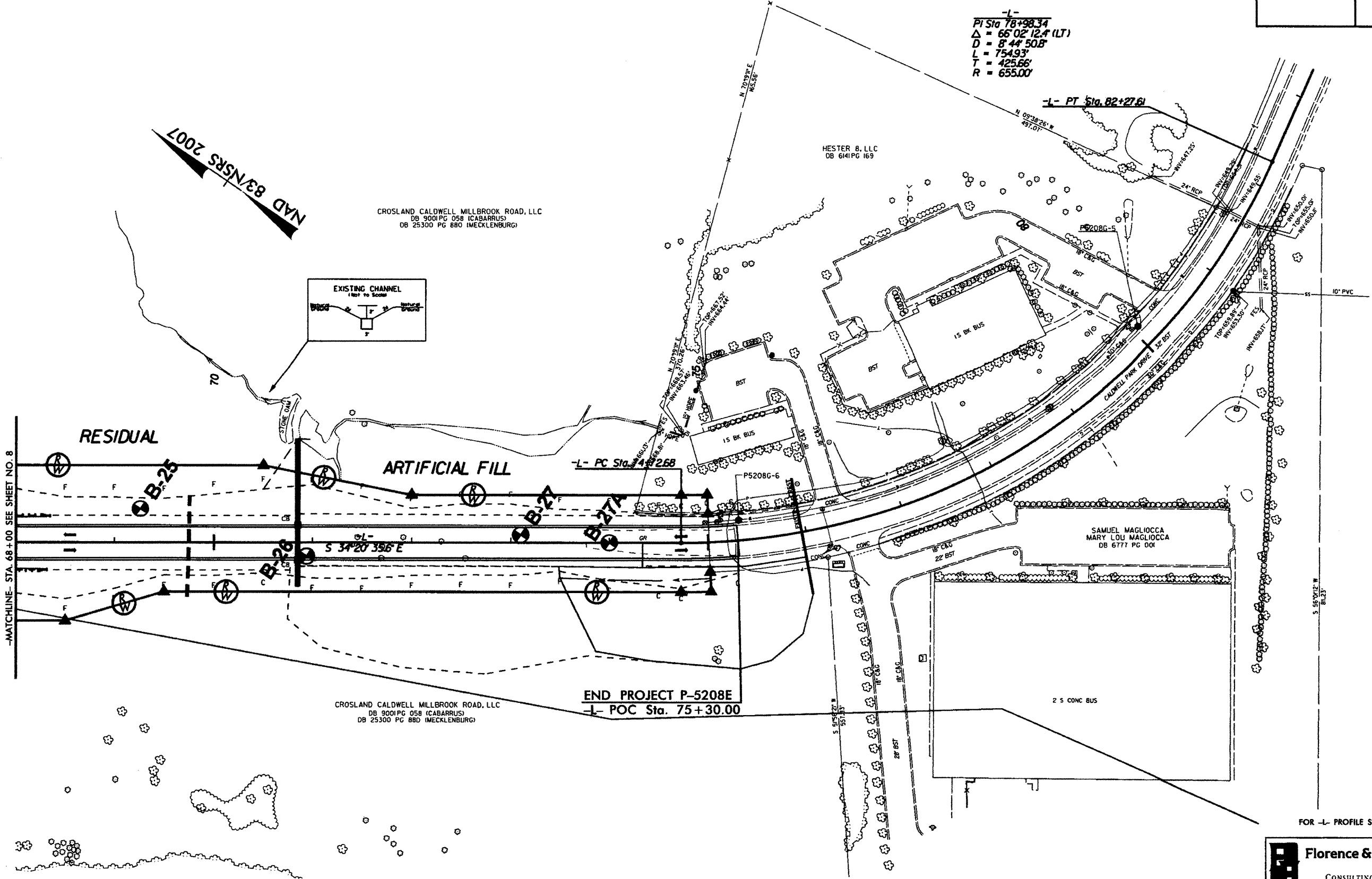
FOR -L- PROFILE SEE SHEET 11

Florence & Hutcheson
CONSULTING ENGINEERS
5121 Kipling Way, Suite 100 Raleigh, NC 27607
NC License No. F-0255

P:\5208E\Standard DOT Structure\GEO\TECH DOT\Cadd Files\TIP\5208E_GEO_RDVY\CADD_GEO\TECH\Plan\p5208e_rdy_psh_07.dgn

PROJECT REFERENCE NO. P-5208E	SHEET NO. 9
RW SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
INCOMPLETE PLANS DO NOT USE FOR ACQUISITION PRELIMINARY PLANS DO NOT USE FOR CONSTRUCTION	

$\Delta = 66^{\circ}02'12.4''$ (LT)
 $D = 8'44'50.8''$
 $L = 754.93'$
 $T = 425.66'$
 $R = 655.00'$



-MATCHLINE- STA. 68+00 SEE SHEET NO. 8

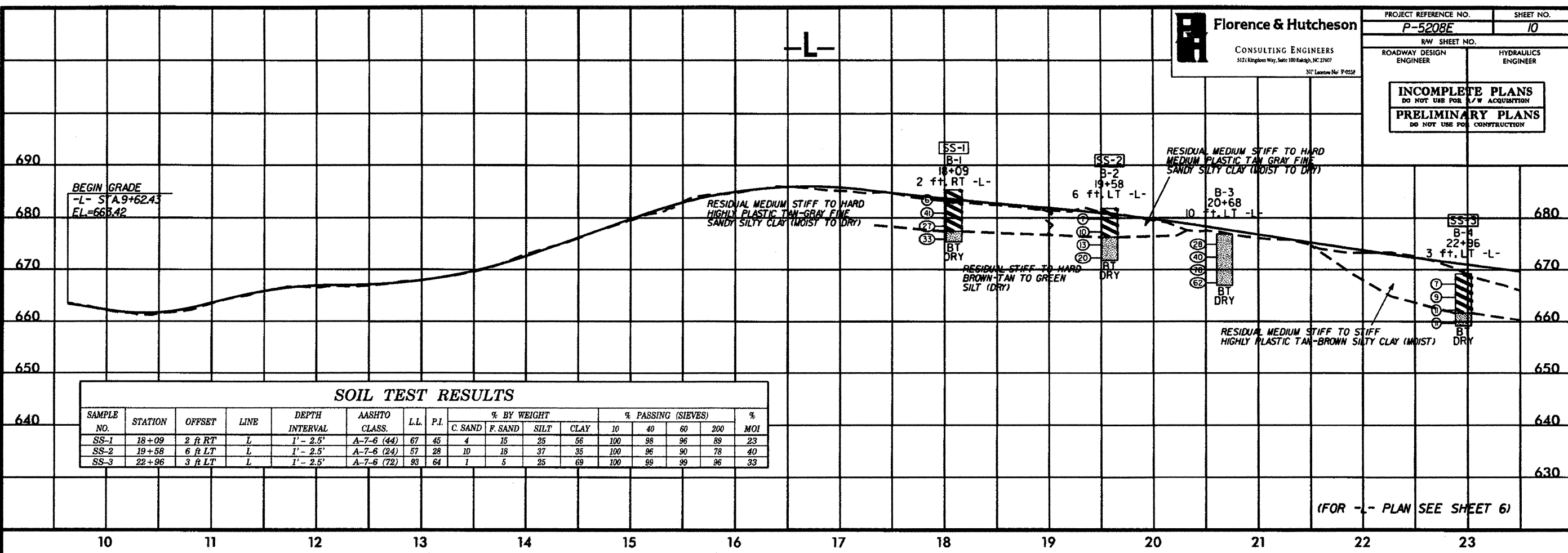
END PROJECT P-5208E
 -L- POC Sta. 75+30.00

FOR -L- PROFILE SEE SHEET 12

Florence & Hutcheson
 CONSULTING ENGINEERS
 3121 Kingston Way, Suite 100 Raleigh, NC 27607
 NC License No: F-0228

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INCOMPLETE PLANS
 DO NOT USE FOR ACQUISITION
PRELIMINARY PLANS
 DO NOT USE FOR CONSTRUCTION

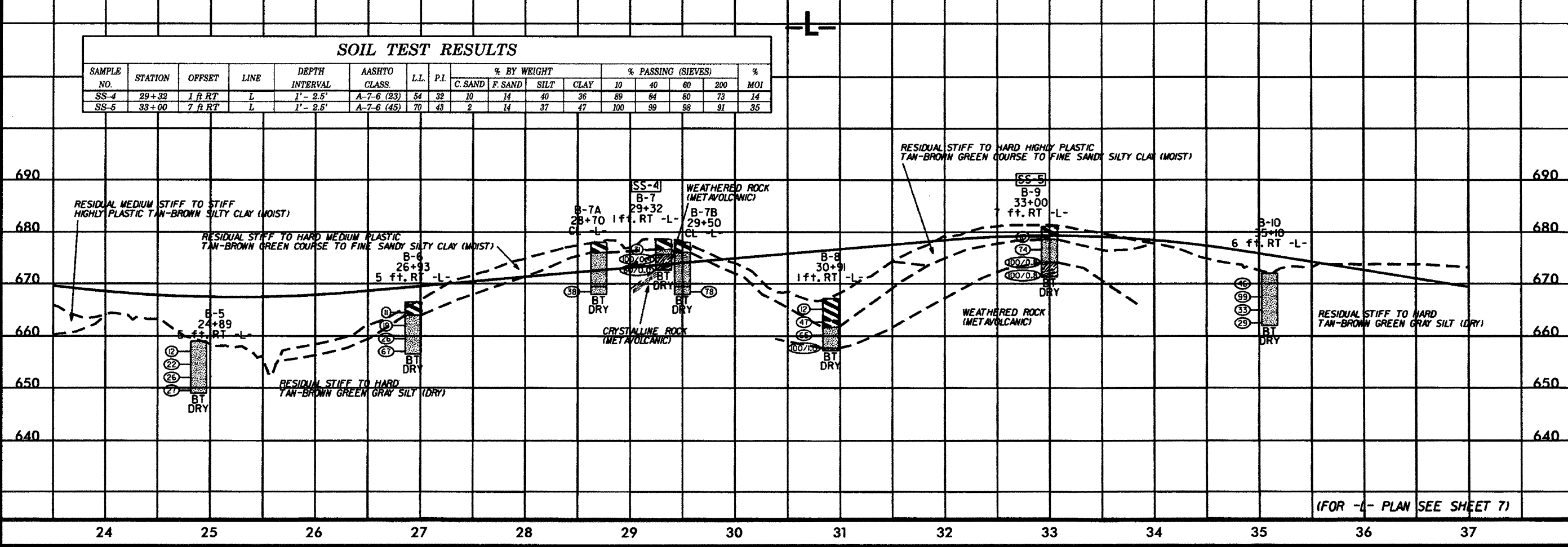


SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-1	18+09	2 ft RT	L	1' - 2.5'	A-7-6 (44)	67	45	4	15	25	56	100	98	96	89	23
SS-2	19+58	6 ft LT	L	1' - 2.5'	A-7-6 (24)	57	28	10	18	37	35	100	96	90	78	40
SS-3	22+96	3 ft LT	L	1' - 2.5'	A-7-6 (72)	93	64	1	5	25	69	100	99	99	96	33

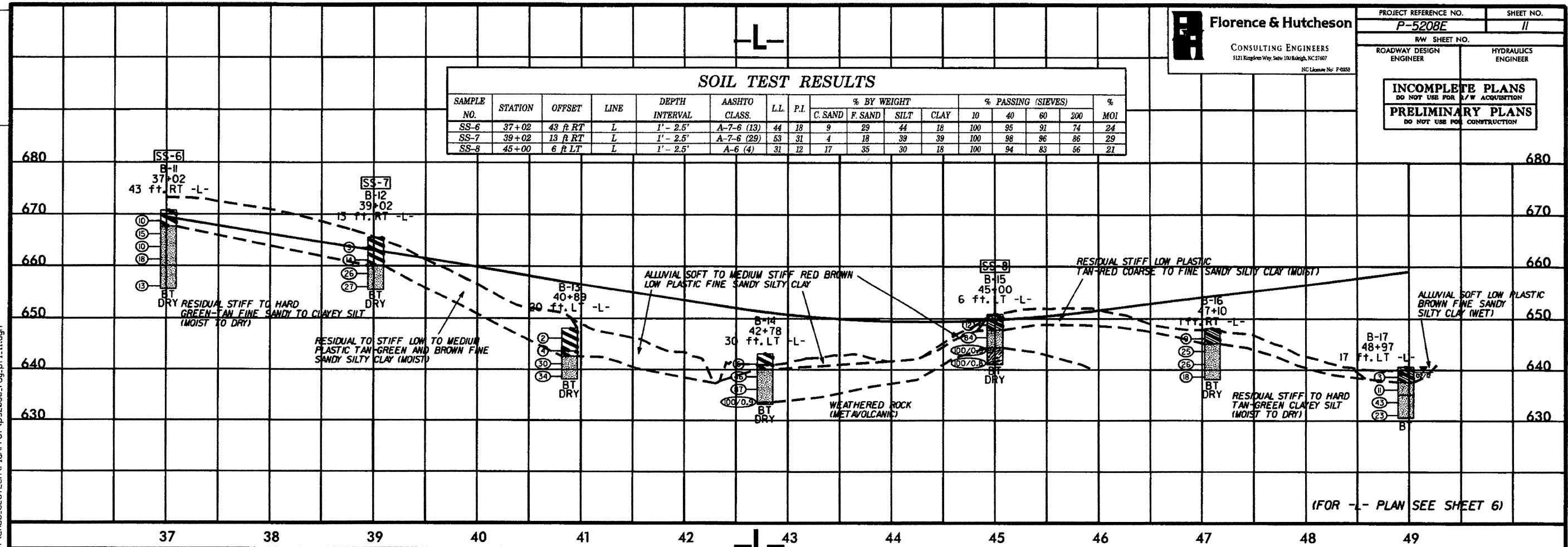
SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-4	29+32	1 ft RT	L	1' - 2.5'	A-7-6 (23)	54	32	10	14	40	36	89	84	80	73	14
SS-5	33+00	7 ft RT	L	1' - 2.5'	A-7-6 (45)	70	43	2	14	37	47	100	99	98	91	35

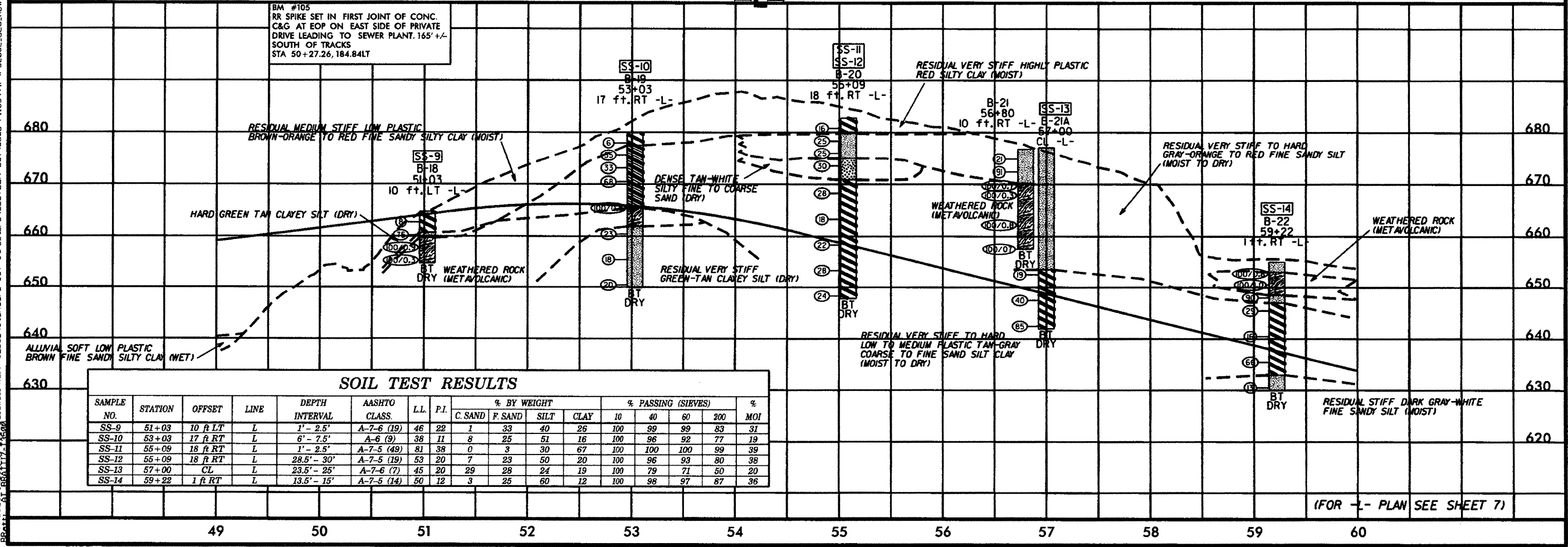


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SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-6	37+02	43 ft. RT	L	1' - 2.5'	A-7-6 (13)	44	18	9	29	44	18	100	95	91	74	24
SS-7	39+02	13 ft. RT	L	1' - 2.5'	A-7-6 (29)	53	31	4	18	39	39	100	98	96	86	29
SS-8	45+00	6 ft. LT	L	1' - 2.5'	A-6 (4)	31	12	17	35	30	18	100	94	83	56	21



(FOR -L- PLAN SEE SHEET 6)



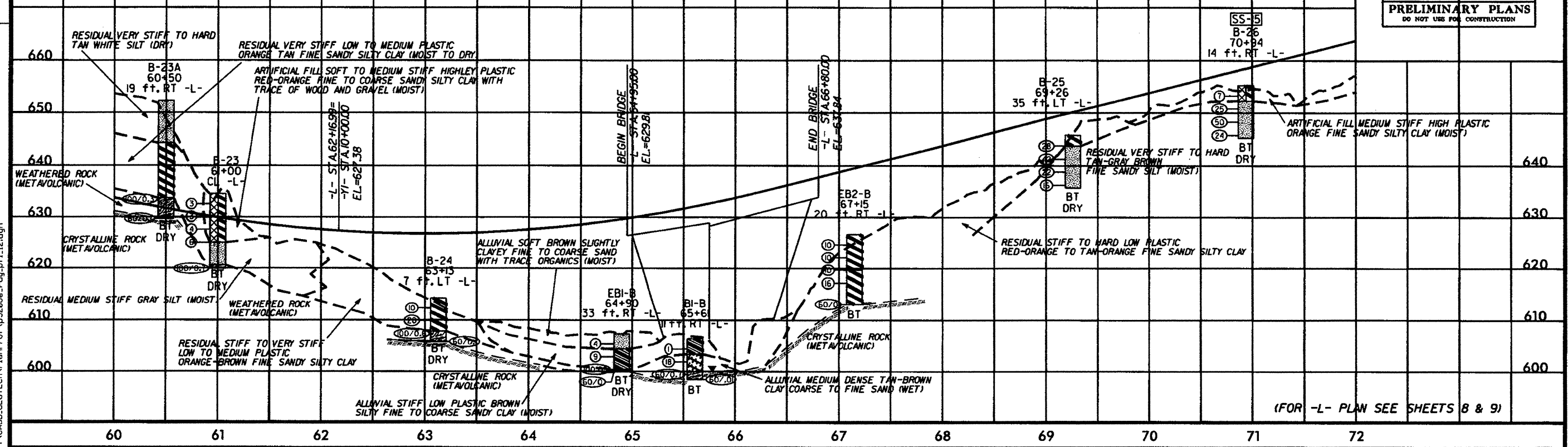
(FOR -L- PLAN SEE SHEET 7)

SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-9	51+03	10 ft. LT	L	1' - 2.5'	A-7-6 (19)	46	22	1	33	40	26	100	99	99	83	31
SS-10	53+03	17 ft. RT	L	6' - 7.5'	A-6 (9)	38	11	8	25	51	16	100	96	92	77	19
SS-11	55+09	18 ft. RT	L	1' - 2.5'	A-7-5 (49)	81	38	0	3	30	67	100	100	100	99	39
SS-12	55+09	18 ft. RT	L	28.5' - 30'	A-7-5 (19)	53	20	7	23	50	20	100	96	93	80	28
SS-13	57+00	CL	L	23.5' - 25'	A-7-6 (7)	45	20	29	28	24	19	100	79	71	50	20
SS-14	59+22	1 ft. RT	L	13.5' - 15'	A-7-5 (14)	50	12	3	25	60	12	100	98	97	87	36

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SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-15	70+94	14 ft. RT	L	1'-2.5'	A-7-6 (46)	71	43	1	12	32	55	100	100	99	92	36

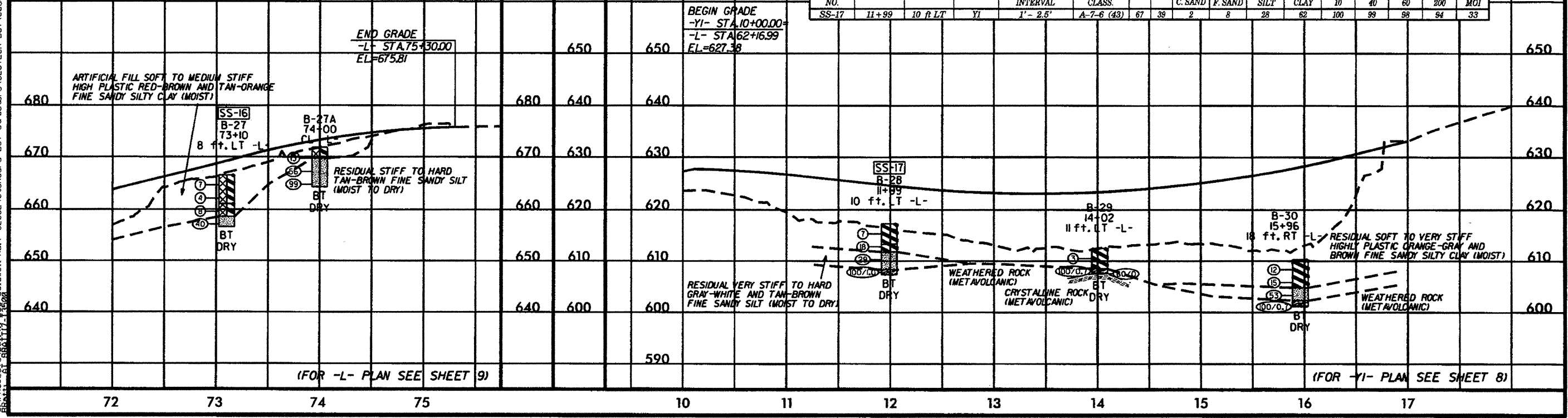


SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-16	73+10	8 ft. LT	L	3.5' - 5'	A-7-6 (52)	81	52	7	9	23	61	100	96	93	87	32

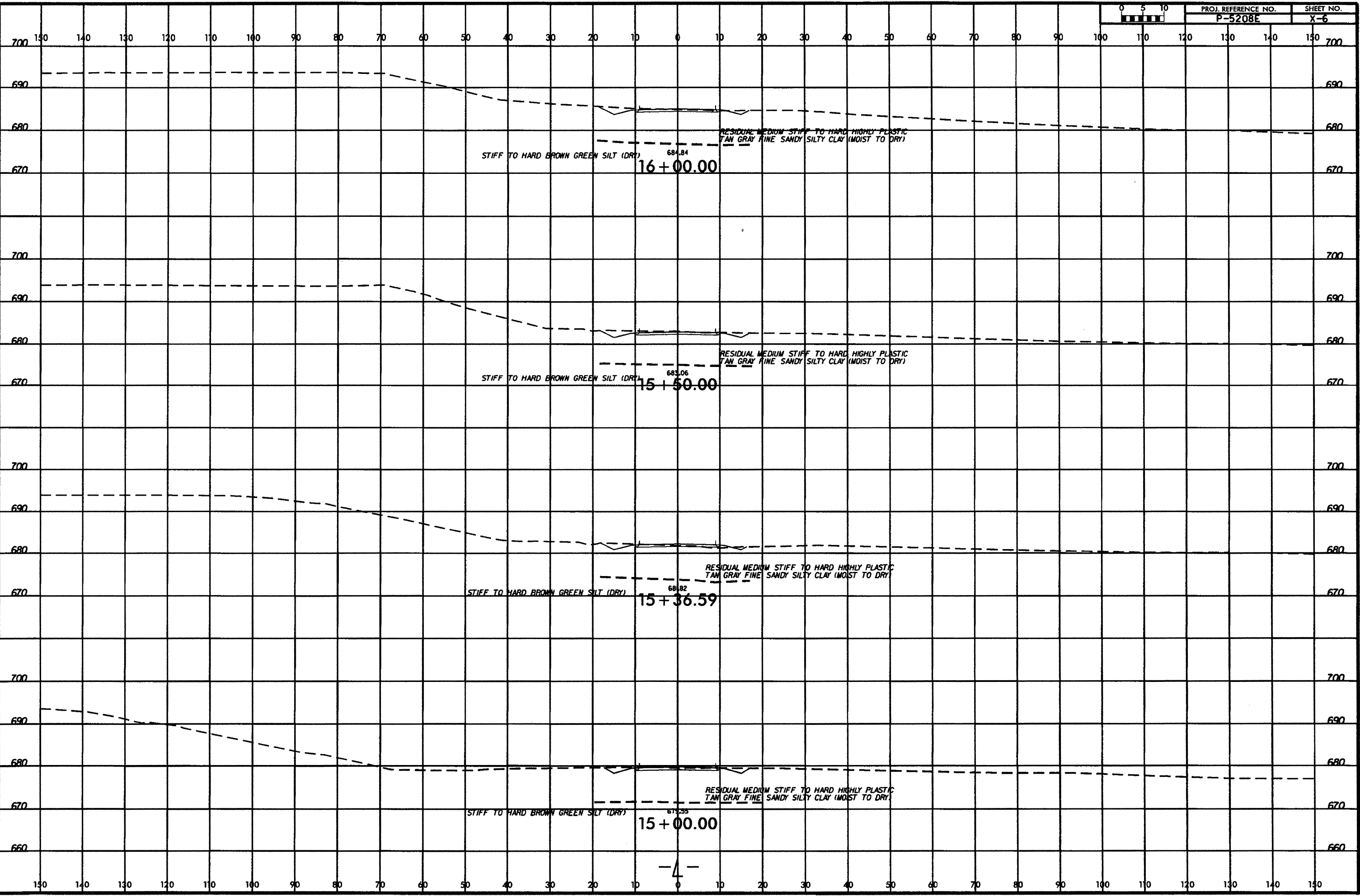
SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-17	11+99	10 ft. LT	Y1	1'-2.5'	A-7-6 (43)	67	39	2	8	28	62	100	99	98	94	33

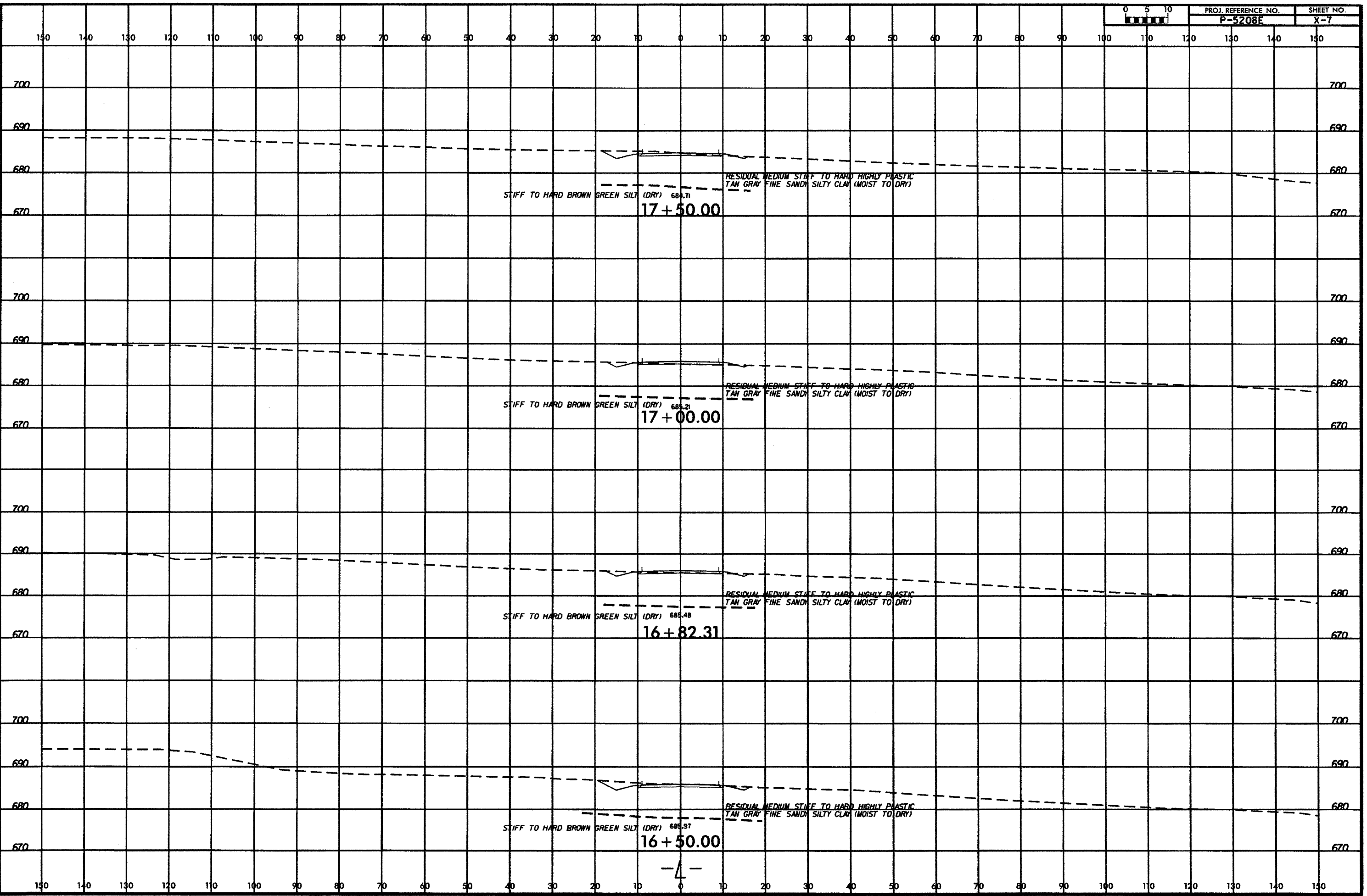


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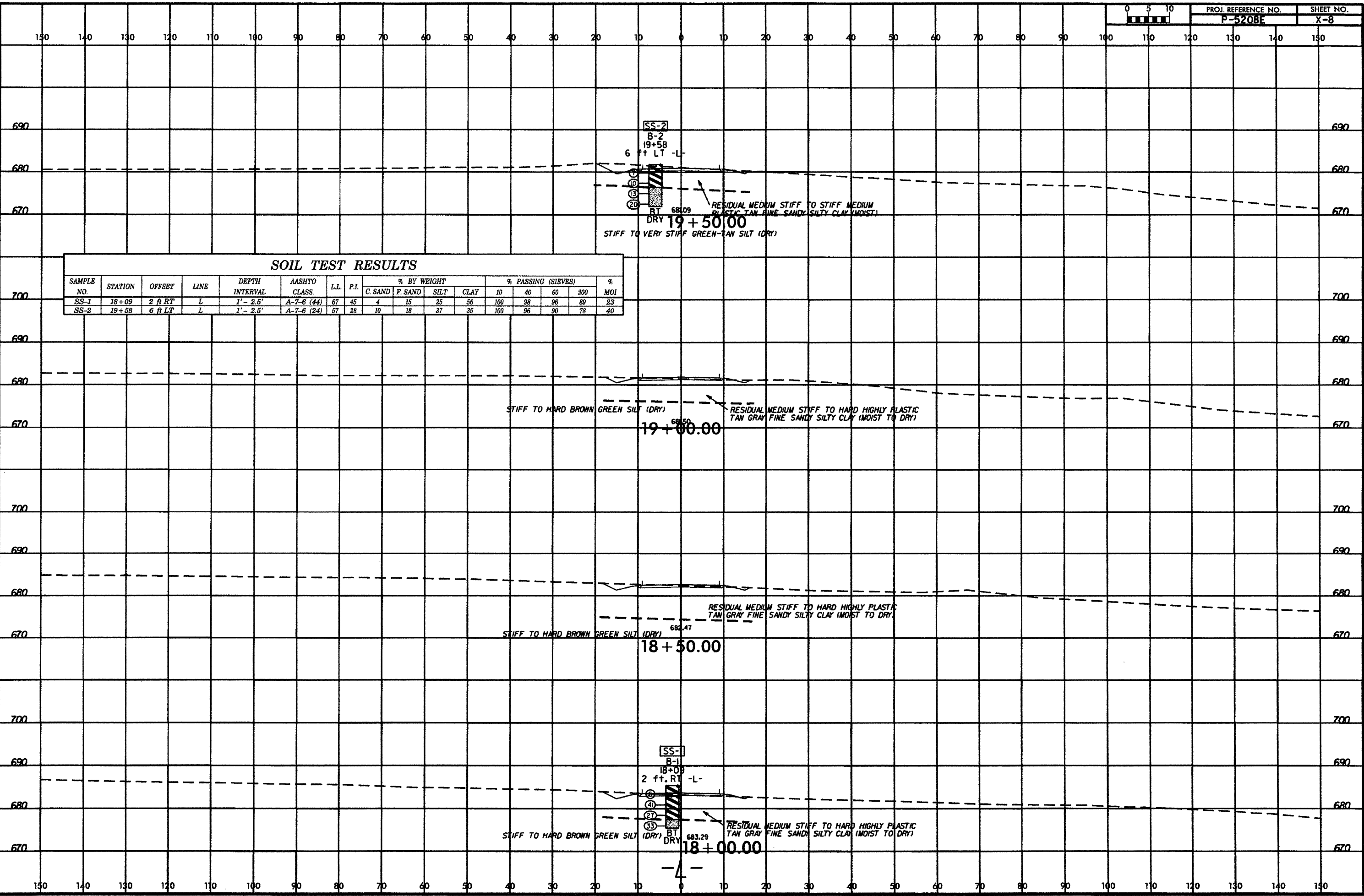
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 8/23/99



SOIL TEST RESULTS																
SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-1	18+09	2 ft RT	L	1' - 2.5'	A-7-6 (44)	67	45	4	15	25	56	100	98	96	89	23
SS-2	19+58	6 ft LT	L	1' - 2.5'	A-7-6 (24)	57	28	10	18	37	35	100	96	90	78	40

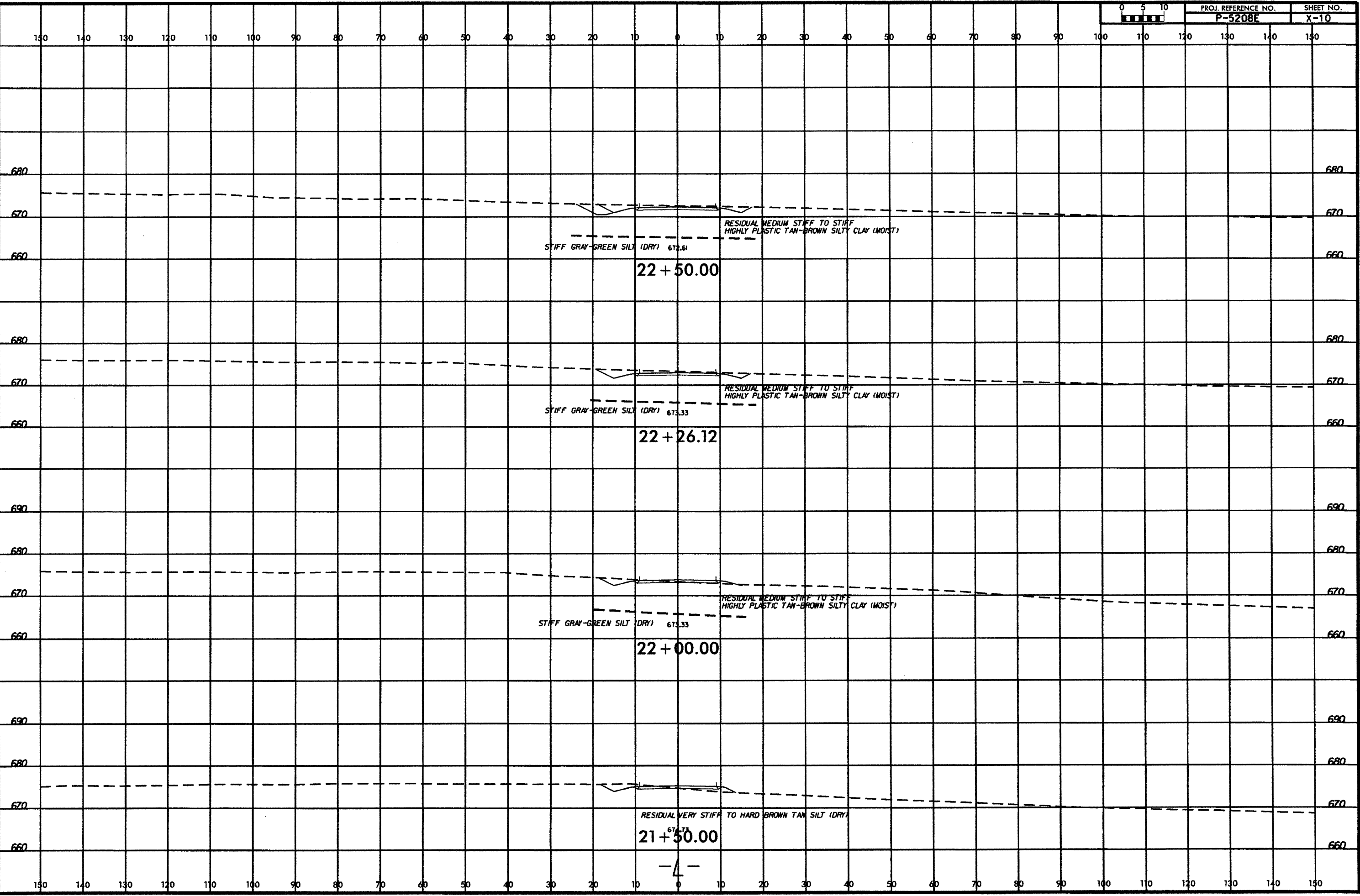
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 B-2
 19+58
 6 ft LT -L-
 RT 681.09
 DRY 19+50.00
 STIFF TO VERY STIFF GREEN-TAN SILT (DRY)
 RESIDUAL MEDIUM STIFF TO STIFF MEDIUM PLASTIC TAN FINE SANDY SILTY CLAY (MOIST)

STIFF TO HARD BROWN GREEN SILT (DRY)
 19+50.00
 RESIDUAL MEDIUM STIFF TO HARD HIGHLY PLASTIC TAN GRAY FINE SANDY SILTY CLAY (MOIST TO DRY)

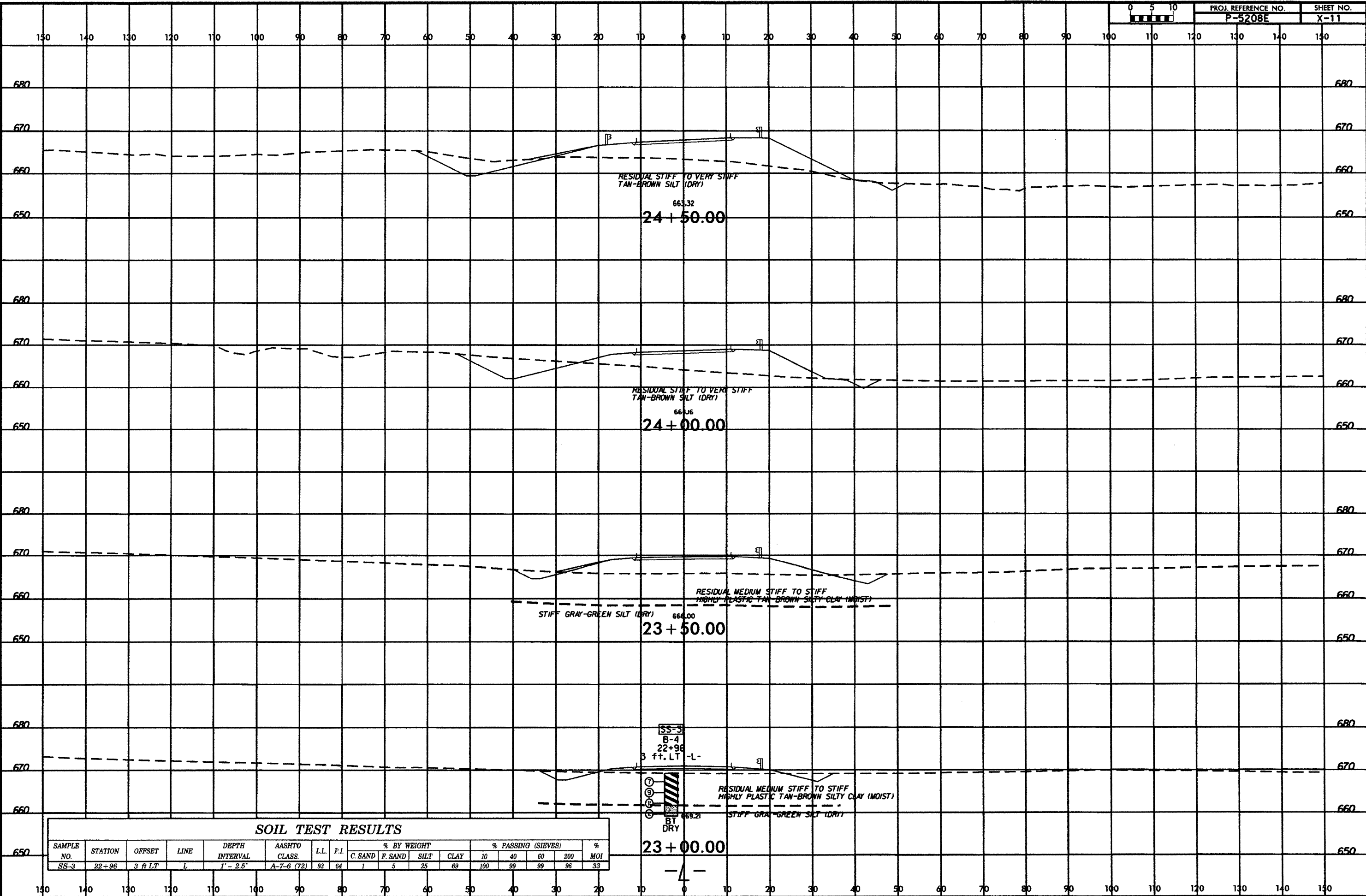
STIFF TO HARD BROWN GREEN SILT (DRY)
 18+50.00
 RESIDUAL MEDIUM STIFF TO HARD HIGHLY PLASTIC TAN GRAY FINE SANDY SILTY CLAY (MOIST TO DRY)

SS-1
 B-1
 18+09
 2 ft RT -L-
 RT 683.29
 DRY 18+00.00
 STIFF TO HARD BROWN GREEN SILT (DRY)
 RESIDUAL MEDIUM STIFF TO HARD HIGHLY PLASTIC TAN GRAY FINE SANDY SILTY CLAY (MOIST TO DRY)

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 Project: 21-13508



RESIDUAL STIFF TO VERY STIFF
 TAN-BROWN SILT (DRY)
 663.32
 24 + 50.00

RESIDUAL STIFF TO VERY STIFF
 TAN-BROWN SILT (DRY)
 664.16
 24 + 00.00

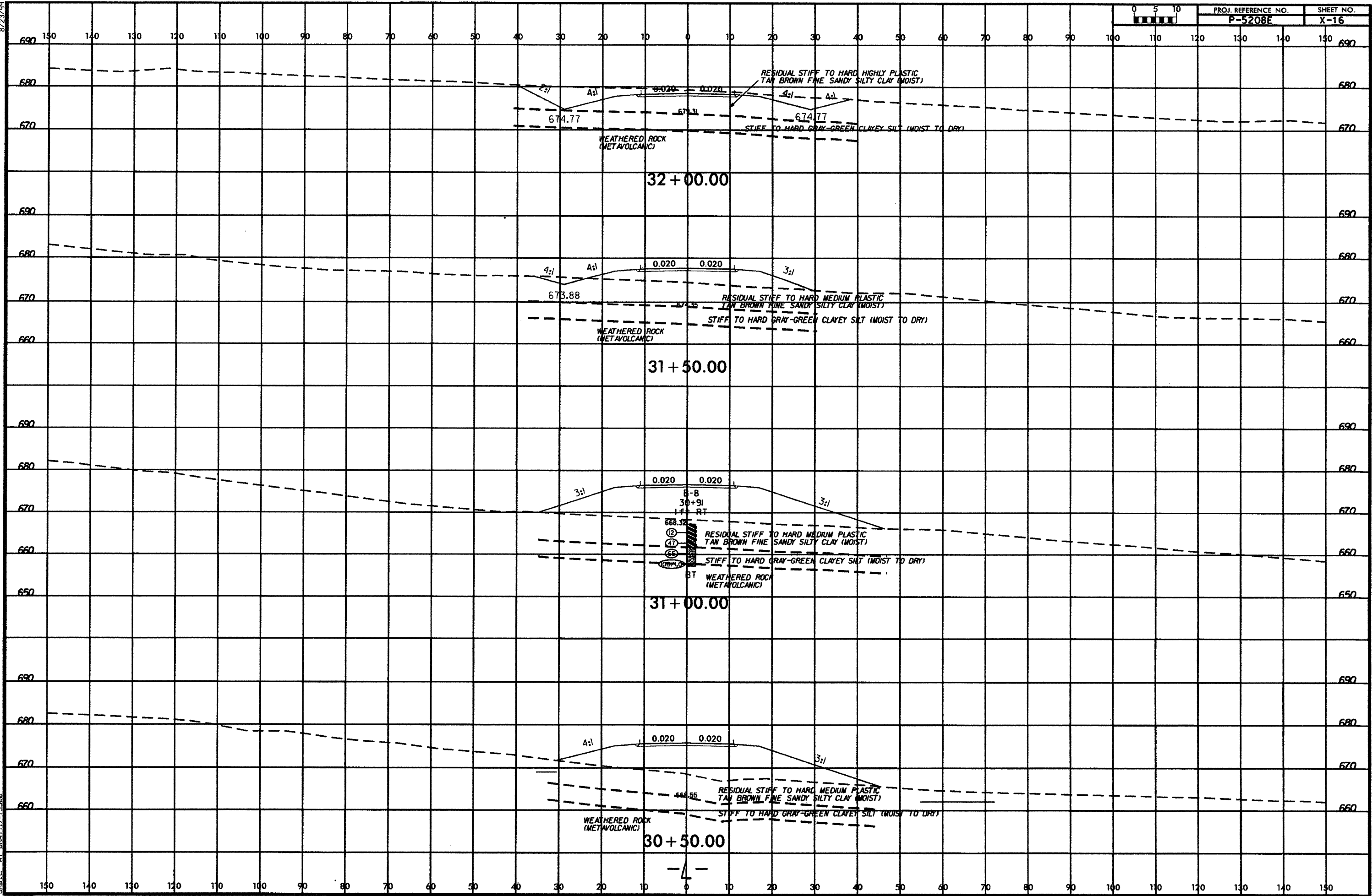
RESIDUAL MEDIUM STIFF TO STIFF
 HIGHLY PLASTIC TAN-BROWN SILTY CLAY (MOIST)
 STIFF GRAY-GREEN SILT (DRY)
 666.00
 23 + 50.00

SS-3
 B-4
 22+96
 3 ft. LT -L-
 BT
 DRY
 669.21
 23 + 00.00

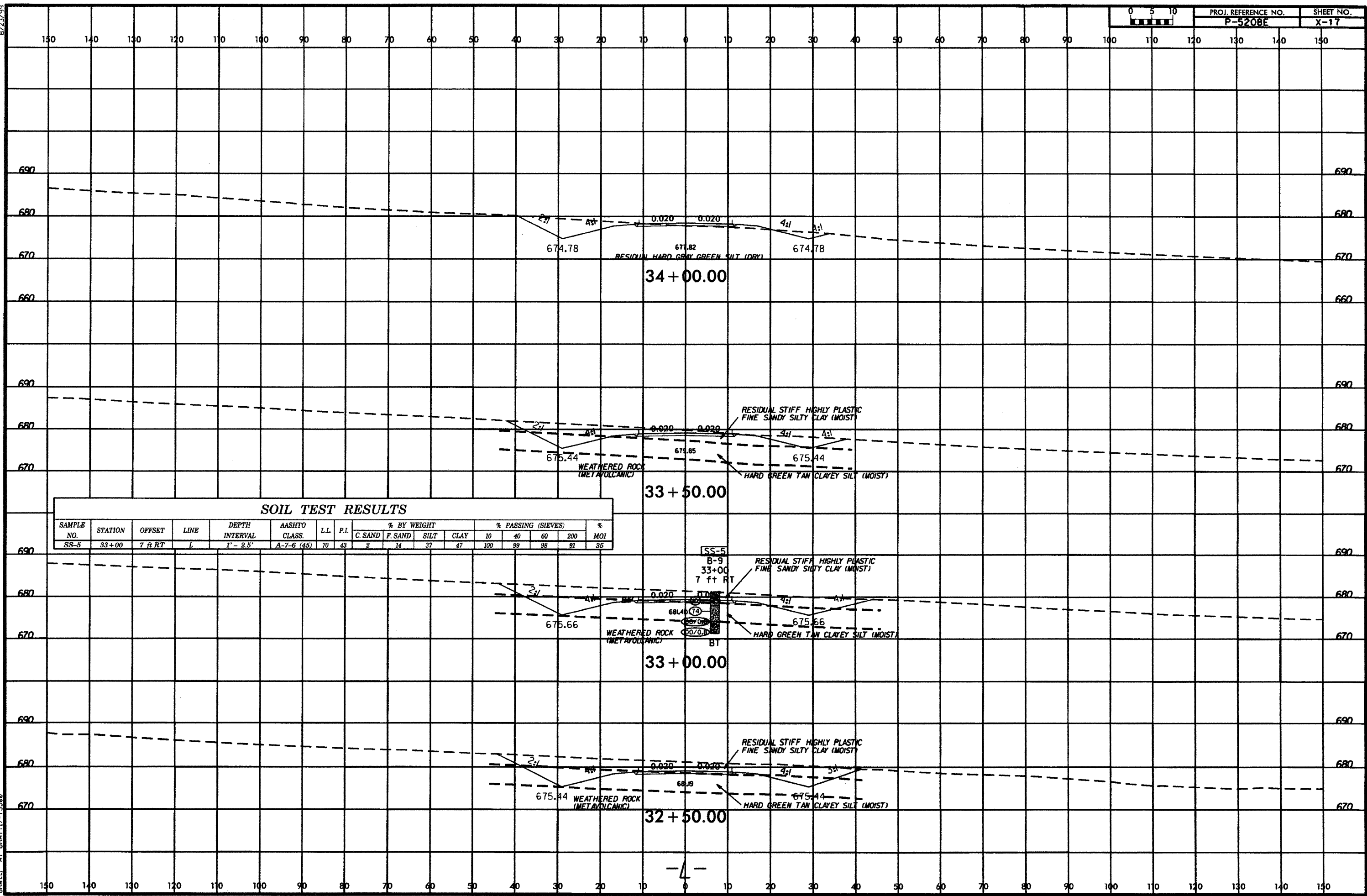
SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-3	22+96	3 ft. LT	L	1' - 2.5'	A-7-6 (72)	93	64	1	5	25	69	100	99	99	96	33

8/23/99
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BRATTI



8/23/99
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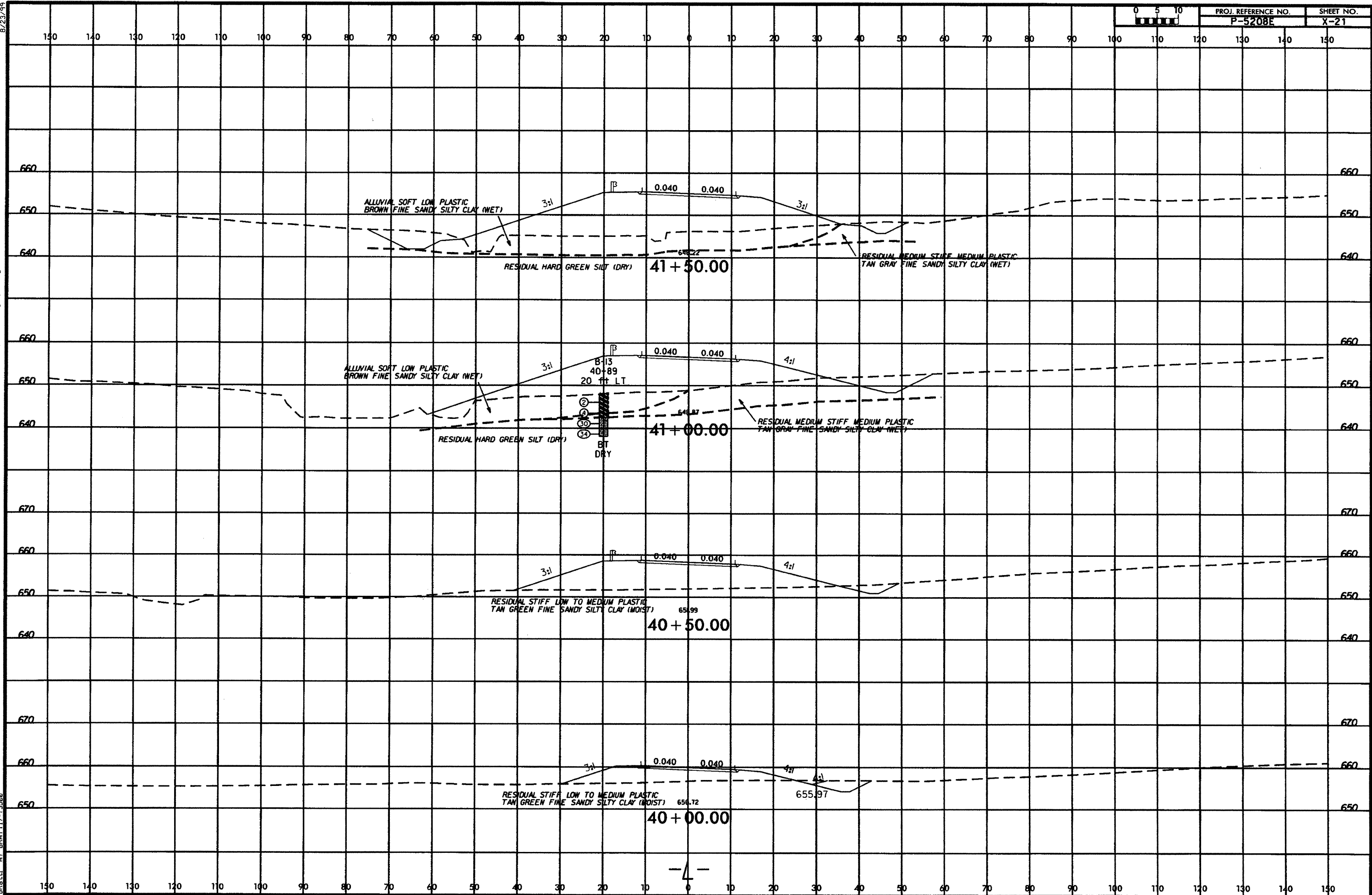


SOIL TEST RESULTS

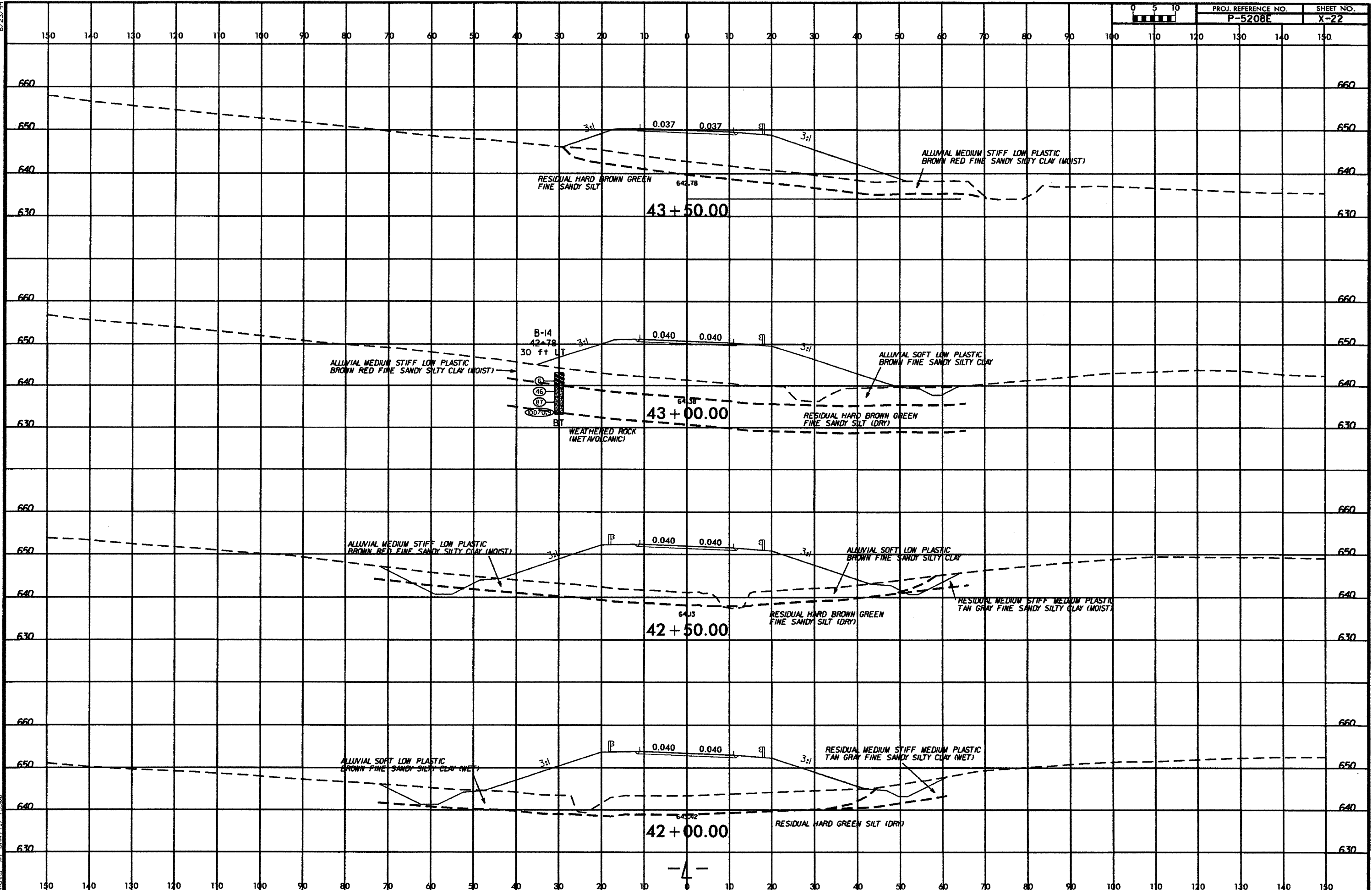
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								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-5	33+00	7 ft RT	L	1' - 2.5'	A-7-6 (45)	70	43	2	14	37	47	100	99	98	91	35

8/23/99
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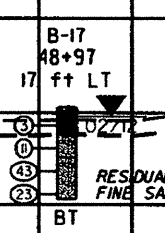
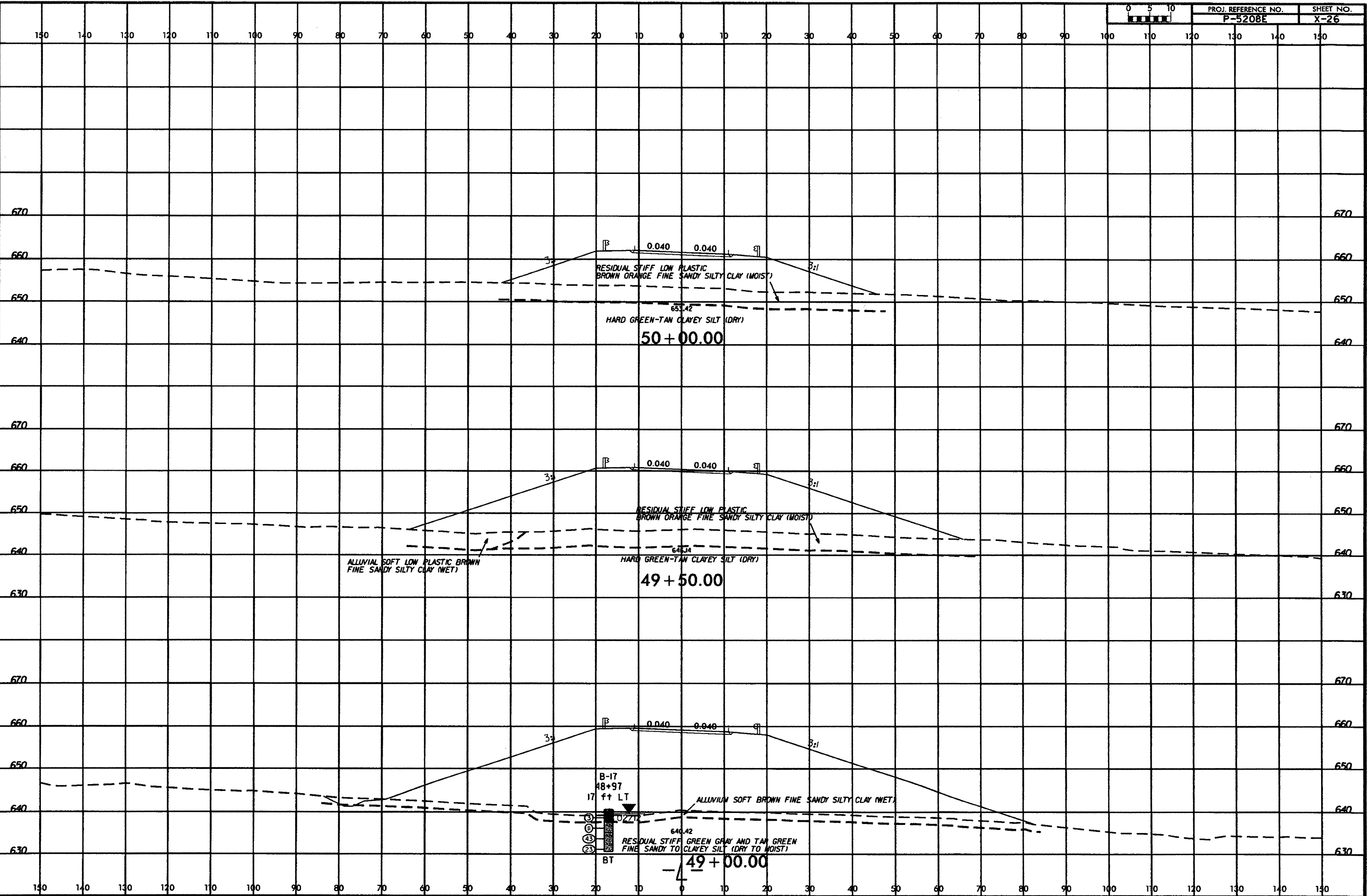
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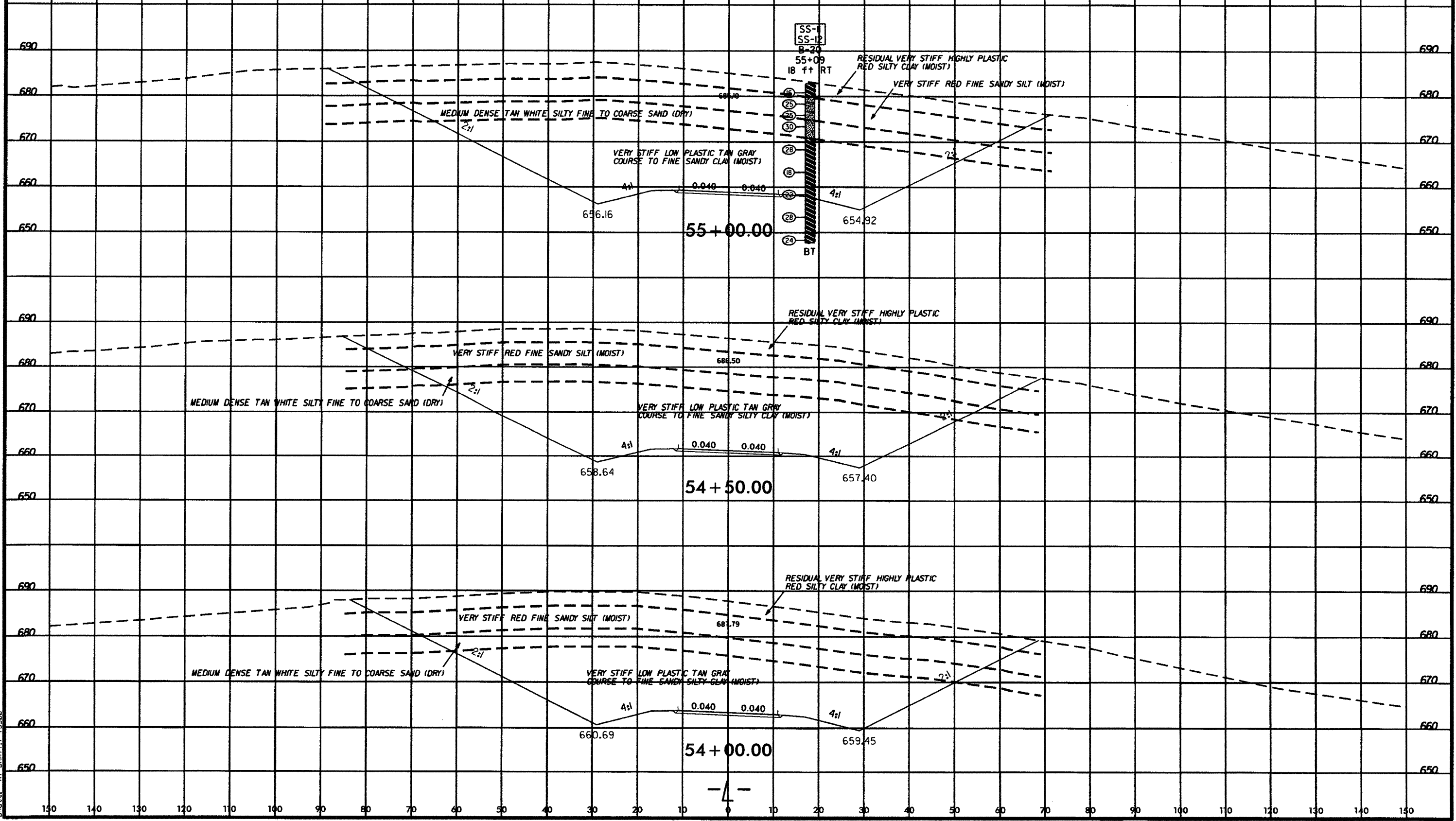


640.42
 RESIDUAL STIFF GREEN GRAY AND TAN GREEN
 FINE SANDY TO CLAYEY SILT (DRY TO MOIST)

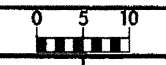
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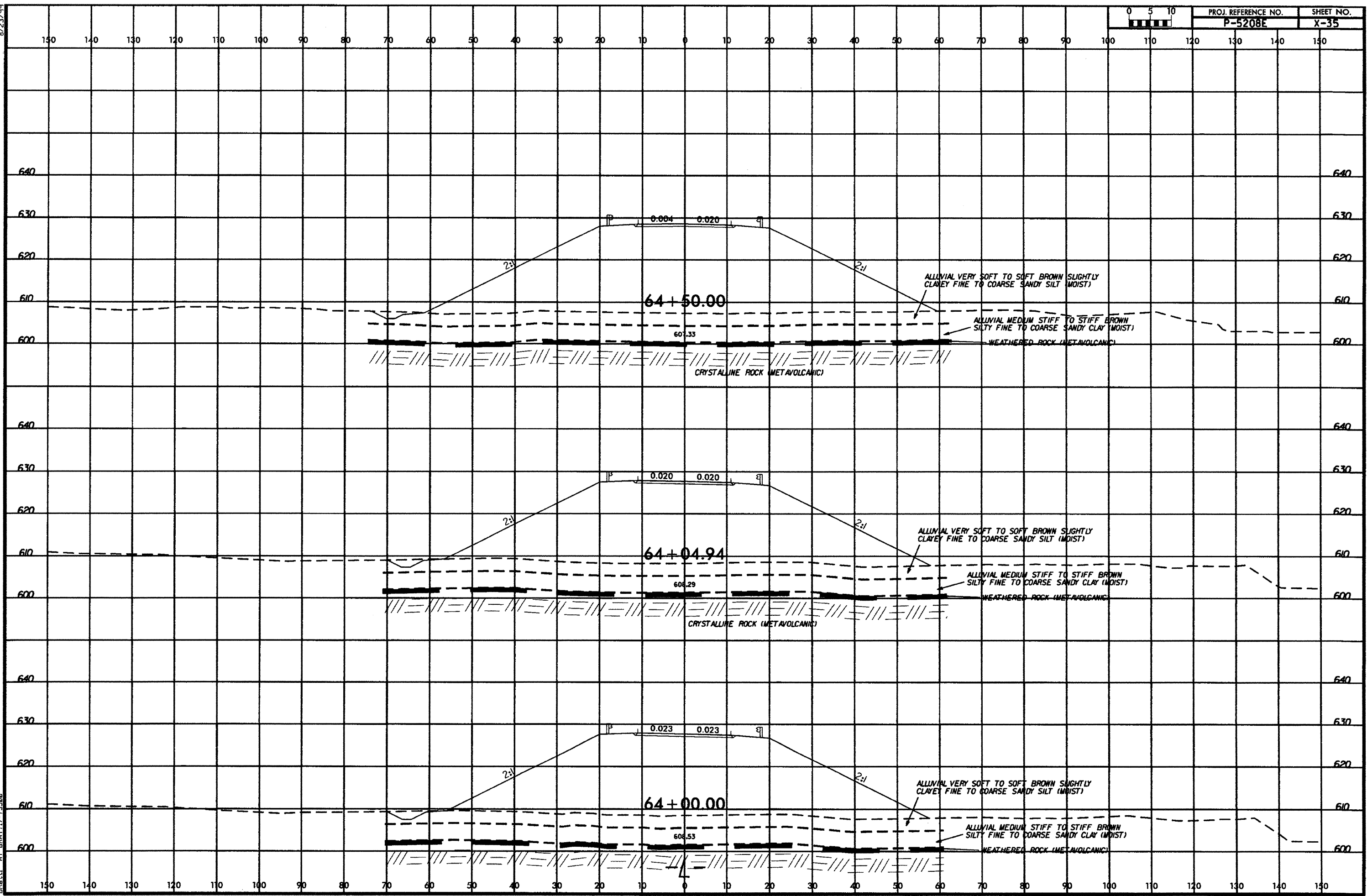
SOIL TEST RESULTS																
SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-11	55+09	18 ft RT	L	1' - 2.5'	A-7-5 (49)	81	38	0	3	30	67	100	100	100	99	39
SS-12	55+09	18 ft RT	L	28.5' - 30'	A-7-5 (19)	53	20	7	23	50	20	100	96	93	80	38



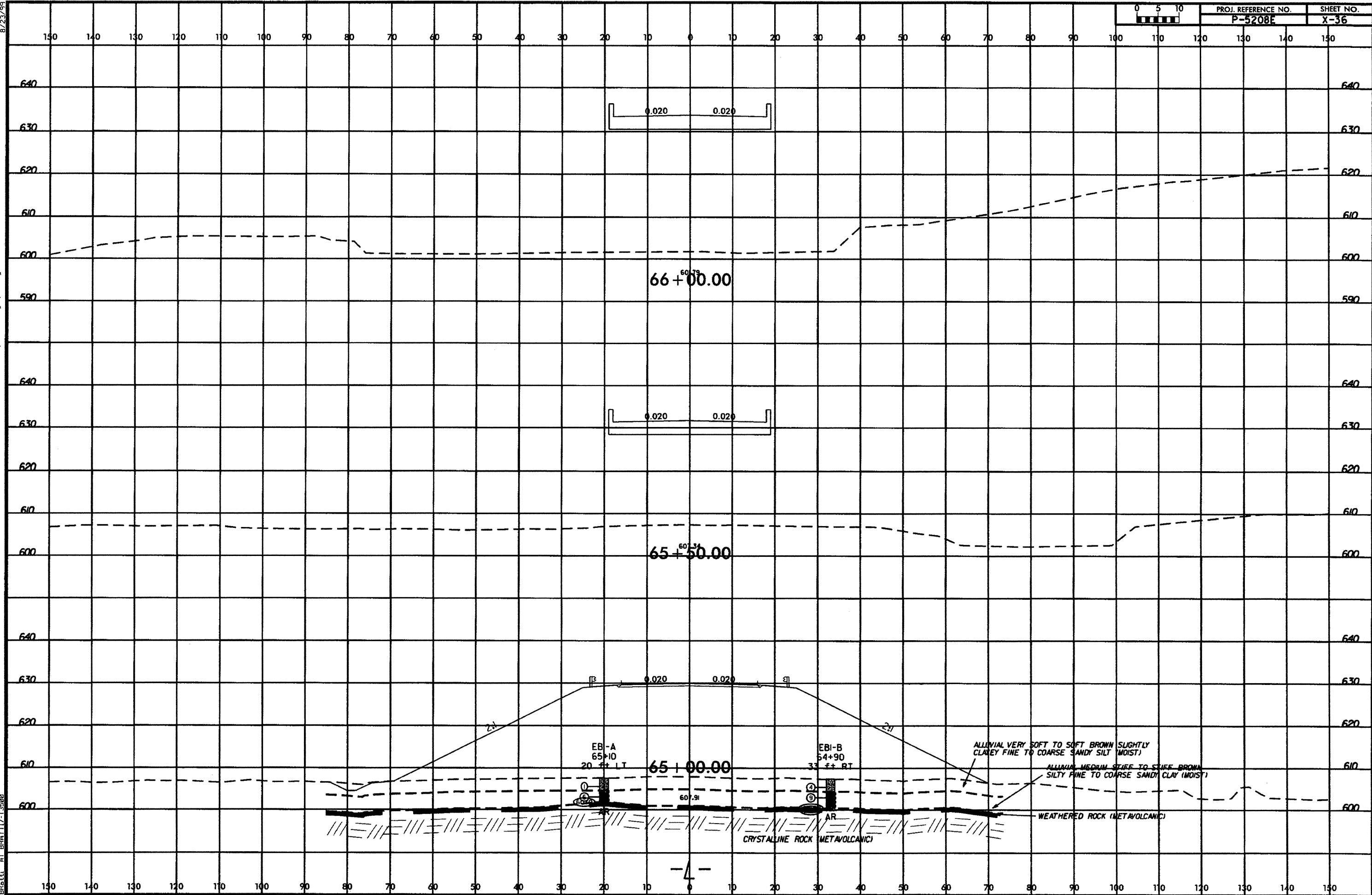
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 SAN FRANCISCO
 BRATTLEY
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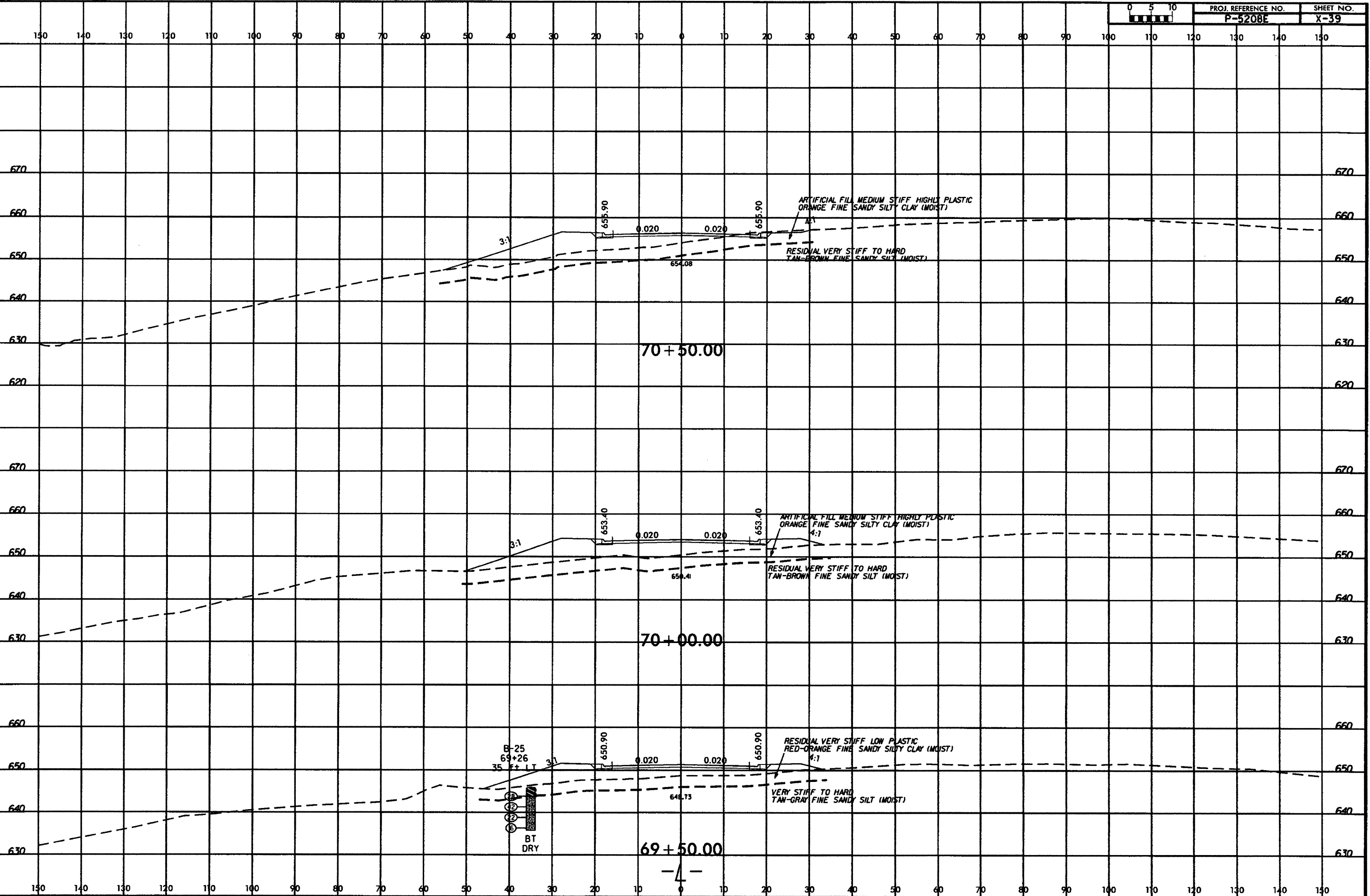


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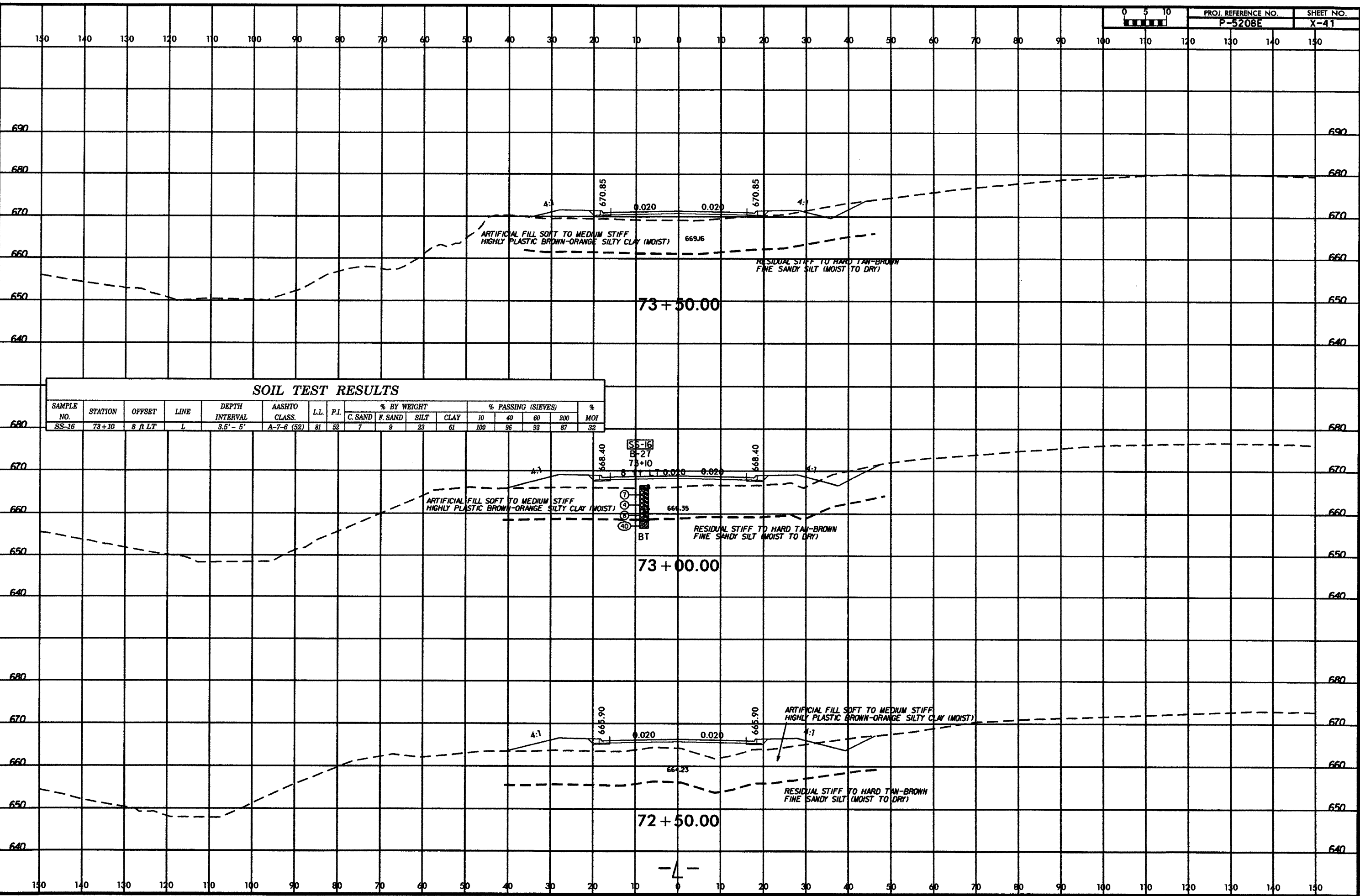


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8/23/99

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SHEET NO. X-39		



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 8/23/99



SOIL TEST RESULTS

SAMPLE NO.	STATION	OFFSET	LINE	DEPTH INTERVAL	AASHTO CLASS.	LL	P.I.	% BY WEIGHT				% PASSING (SIEVES)				% MOI
								C. SAND	F. SAND	SILT	CLAY	10	40	60	200	
SS-16	73+10	8 R LT	L	3.5' - 5'	A-7-6 (52)	81	52	7	9	23	61	100	96	93	87	32

