## **CONTENTS**

361

2

316

**DESCRIPTION** TITLE SHEET LEGEND SITE PLAN **PROFILES** BORE LOG & CORE REPORTS SCOUR REPORT

CORE PHOTOGRAPHS

### STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS** GEOTECHNICAL ENGINEERING UNIT

# STRUCTURE SUBSURFACE INVESTIGATION

| ROJ. REFERENCE NO.   | 33167.1.1 (B–3619) | F.A. PROJ. <i>BRZ-3439(1)</i> |
|----------------------|--------------------|-------------------------------|
| COUNTY BUNCOMBI      | Ξ                  |                               |
| ROJECT DESCRIPTION . | BRIDGE NO. 56 ON   | SR-3439                       |
|                      | OVER BILL MOORE    | CREEK                         |
|                      |                    |                               |
| SITE DESCRIPTION     |                    |                               |
| ,                    |                    |                               |
|                      |                    |                               |

| ST'A | TE STAT | E PROJECT | REFERENCE NO | SHEET | SHEETS |
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| N.   | .C. 33  | 167.1.1   | (B-3619)     | 1     |        |
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THE SUBSUPFACE HERMATION AND THE SUBSUPFACE HIVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLAINING, AND DESIGN, AND HOT FOR COMSTRUCTION OR PAY PURPOSES. THE VARBOUS FRELD BORNIC COOS, RCCY CIRES, AND SOUL TEST DATA AVAILABLE MAY BE PURLIED OR MISPECTED IN RALFION BY CONTACTING THE N.C. OPPARTMENT OF TRANSPORTATION. GEOISCHMICAL ENGINEERING LIMIT AT 1900/250-4088, HEITHER THE SUBSURFACE PLANS AND PEPORTS, NOR THE FIELD BORNS LOOS, ROCK COPES, OR SOIL TEST DATA ARE PART OF THE CONTRACT.

CEMERAL SOIL AND FOR STRAIA DESCRIPTIONS AND DESCRIPT BORRCAPES ARE BASED ON A CHOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSIDERACE DATA AND MAY NOT INTERSSARILY REFLECT THE ACTUAL SUBSIDERACE CONDITIONS DECEMBED OR BETWEN SAMPLED STRAIA WITHIN THE BOREHOLE THE LABORATION SAMPLE DATA AND THE INTERPRETATION PLAYER THAT CAN BE RELIED ON DULLY TO THE DESCRED OF RELIEBLIT, MERCENT IN THE STANDARD TEST MATING. OF THE PROPERTY WATER LEVELS ON SOU, MOSTURE COMPUTIONS MORE ARE ON THE SUBSEPPACE MYSTERIES AND FOR THE THE THE PROPERTY WATER LEVELS OR SOU MOSITURE COMPUTIONS MORE AS PECONDED AT THE THAT OF THE PROPERTY OF LABORATIC COMPUTIONS MORE THAT STANDARD THE STANDARD WATER LEVELS OR SOU MOSITURE COMPUTIONS MORE ASSOCIATED AND AND THE STANDARD THE ST

THE BIDDER OF CONTRACTOR IN CAUTIONED THAT DETAILS SHOWN ON THE SUBSUIPFACE PLAIS ARE DEFENDENCE OF AND IN MAIN FACES THE FINAL DESIGN DETAILS ARE DEFERRENT, FOR BIDDWIN AND CONSTRUCTION PRAIS AND DECEMENTS FOR BROWN AND CONSTRUCTION OF THE PROJECT. THE DEPARTMENT DOES NOT WARRANT OR CONFARON OF THE SUFFICIENCY OR ACCURACY OF THE WYESTIGATION MADE, MOR THE WITEFRETATIONS MADE, OR OPENION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONSTRUCTIONS TO BE EMPORTURED OF CONTRACTOR IS CAUTIONED TO MAKE SUCH REPERIORENT SUBJURACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATIST MAGELER AS TO CONDITIONS TO BE DECONSTRUCTED ON THIS PRODUCT, THE CONTRACTOR SHALL HAVE NO CLAIM FOR ACCURACY COMPENSATION OF FOR AN EXPENSION OF TIME FOR MAY REASON RESULTING THOM THE ACTUAL CONTRACTOR SHALL HAVE NO CLAIM FOR ACCURACY COMPENSATION OF FOR AN EXPENSION OF TIME FOR MAY REASON RESULTING THOM THE ACTUAL CONTRACTOR SHALL HAVE NO CLAIM FOR ACCURACY COMPENSATION OF FOR AN EXCENSION OF TIME FOR MAY REASON RESULTING THOM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE NOICE THE SUBSURFACE IMPORMATION.

|                  | T B DANIEL   |
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|                  | M M HAGER    |
| · .              | D 0 CHEEK    |
|                  | G K ROSE     |
|                  | C J COFFEY   |
|                  | R D CHILDERS |
|                  | _            |
|                  | _            |
|                  |              |
| INVESTIGATED BY_ | C A DUNNAGAN |
|                  | W D FRYE, Jr |
|                  | W D FRYE, Jr |
| DATE             |              |
|                  |              |

PERSONNEL

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NOTE - BY HAVING REQUESTED THIS INFORMATION THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

DRAWN BY: C A DUNNAGAN

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 PROJECT REFERENCE NO.
 SHEET NO.

 33167.1.1 (B-3619)
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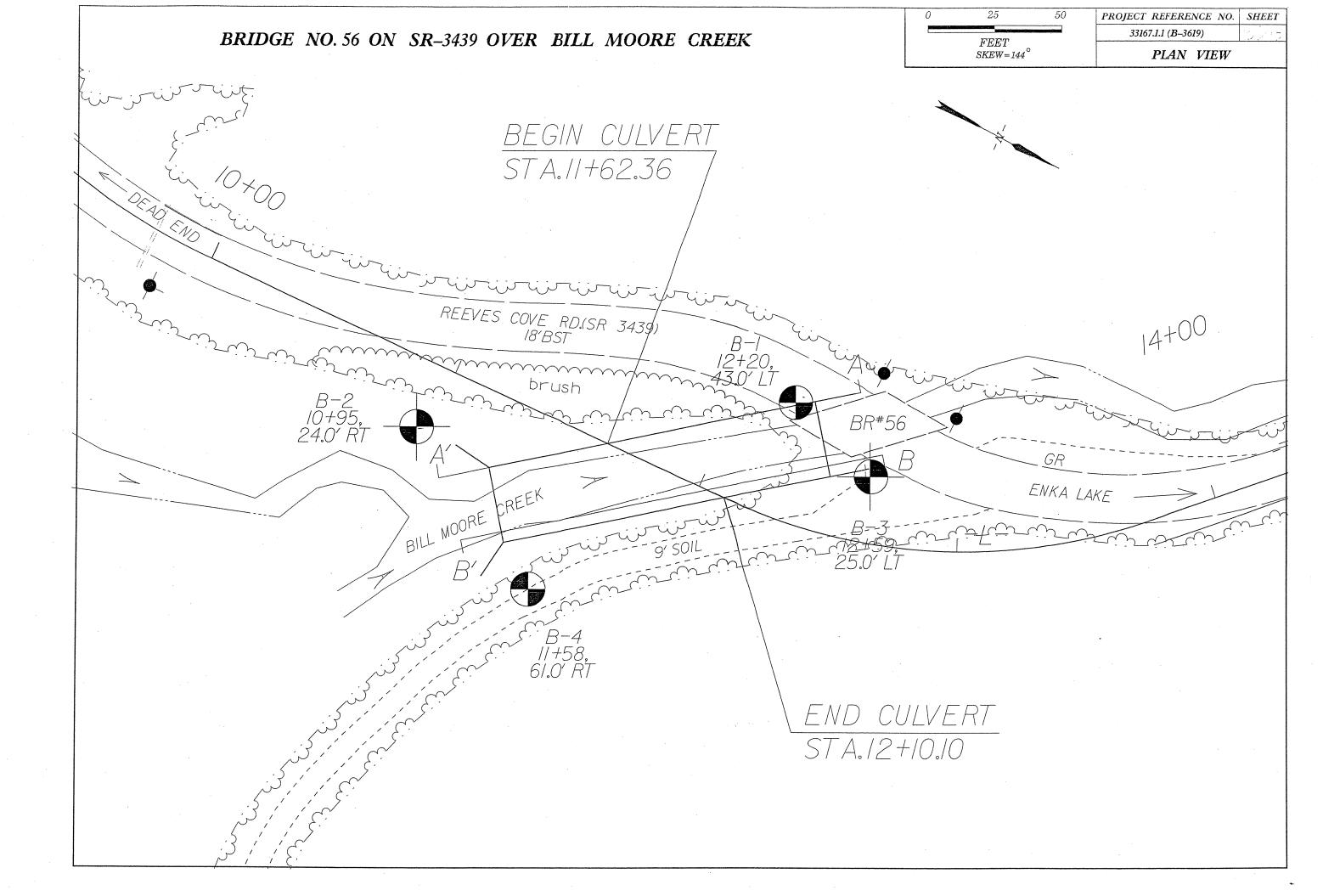
### DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

### SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

|   |   |   |   | SOIL AND RO   | CK LEGEND, TERM                           | is, symbo                    | LS, AND ABBRE   | VIATIONS   |                                   |  |
|---|---|---|---|---|---|------------------------------|---|--|-----------------------------------|--|
|   | SOIL DESCRIPTION  |   |   | GRADATION   |   |                              |   | CK DESCRIPTION   |                                   | TERMS AND DEFINITIONS  |
|   | DISOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED I  |   | UNIFORM - INDICATES THAT S                              | GOOD REPRESENTATION OF PARTICLE SIZES I<br>OIL PARTICLES ARE ALL APPROXIMATELY TH | FROM FINE TO COARSE.<br>E SAME SIZE.(ALSO | ROCK LINE IN                 | DICATES THE LEVEL AT WHICH                                  | THAT IF TESTED, WOULD YIELD SPT R<br>NON-COASTAL PLAIN MATERIAL WOULD  | YIELD SPT REFUSAL.                | ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.   |
| 100 BLOWS PER FOOT ACCORDING TO S                         | INTINUOUS FLIGHT POWER AUGER, AND YIELD LESS<br>STANDARD PENETRATION TEST (AASHTO T206, ASTM                        | 1 D-1586). SOIL                               | POORLY GRADED) GAP-GRADED - INDICATES A M               | IXTURE OF UNIFORM PARTICLES OF TWO OR   | MORE SIZES.                               |                              |   | POON SAMPLER EQUAL TO OR LESS THE<br>SITION BETWEEN SOIL AND ROCK IS OF  |                                   | AQUIFER - A WATER BEARING FORMATION OR STRATA.   |
| CONSISTENCY, COLOR, TEXTURE, MOISTUR                      | SHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY SH<br>RE, AASHTO CLASSIFICATION, AND OTHER PERTINENT                      | HALL INCLUDE:<br>T FACTORS SUCH               |   | ANGULARITY OF GRAINS  |   | OF WEATHERE                  | D ROCK.<br>ALS ARE TYPICALLY DIVIDED AS                     |  |                                   | ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.  ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS,                     |
| AS MINERALOGICAL COMPOSITION, ANGU                        | JLARITY, STRUCTURE, PLASTICITY, ETC. EXAMPLE:<br>CLAY, NOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7 |   | THE ANGULARITY OR ROUNDNE<br>SUBANGULAR, SUBROUNDED, OF | SS OF SOIL GRAINS IS DESIGNATED BY THE  | TERMS: ANGULAR,                           | WEATHERED                    | SPIREIA   | AL PLAIN MATERIAL THAT WOULD YIEL  | O SPT N VALUES > 1000             | OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, AS SHALE, SLATE, ETC.   |
|   | ND AND AASHTO CLASSIFICATIO   |   | OCCUPATION DECISION OF                                  | MINERALOGICAL COMPOSITION   | N.  | ROCK (WR)                    | BLUWS PER   | FOOT IF TESTED.  |                                   | ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE                      |
| GENERAL GRANULAR MATER                                    | DIALC CILT-CLAY MATERIALS   |   |   | RTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE                                       |   | CRYSTALLINE<br>ROCK (CR)     | KINT WOULD YIE  | DARSE GRAIN IGNEOUS AND METAMORPH<br>LD SPT REFUSAL IF TESTED, ROCK TYP  |                                   | GROUND SURFACE.  |
| CLASS. (≤ 35% PASSING                                     | "200) (> 35% PASSING "200)  | ORGANIC MATERIALS                             | WHENEVER THEY ARE CONSIDER                              |   |   |                              | CINE TO C   | BBRO, SCHIST, ETC.<br>DARSE GRAIN METAMORPHIC AND NON-CO   | DASTAL PLAIN                      | CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.  |
| GROUP A-1 A-3 CLASS. A-1-0 A-1-b A-2-4 A                  | A-2 A-4 A-5 A-6 A-7 A-1, A-2-5 A-2-6 A-2-7 A-1  | A-2 A-4, A-5<br>3 A-6, A-7                    | OL LOUTE V. GOLIDOTO                                    | COMPRESSIBILITY   |   | NON-CRYSTALLIN<br>ROCK (NCR) | SEDIMENTA   | RY ROCK THAT WOULD YELD SPT REFU<br>PHYLLITE, SLATE, SANDSTONE, ETC.   | SAL IF TESTED. ROCK TYPE          | COLLUYIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.  |
| SYMBOL SYMBOL SYMBOL                                      |   | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\        | SLIGHTLY COMPRESS<br>MODERATELY COMPR                   | ESSIBLE LIQUID LIMIT  | LESS THAN 31<br>EQUAL TO 31-50            | COASTAL PLAIN                | COASTAL P   | LAIN SEDIMENTS CEMENTED INTO ROCK.   |                                   | CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL  |
| % PASSING   |   |   | HIGHLY COMPRESSIE                                       | PERCENTAGE OF MATERIA   | GREATER THAN 50                           | SEDIMENTARY RO               | LK SPT REFUS<br>SHELL BED                                   | AL. ROCK TYPE INCLUDES LIMESTONE.S<br>S.ETC.   | SANDSTONE, CEMENTED               | LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.  |
| * 10 50 MX  | GRANU   |   | ORGANIC MATERIAL  | GRANULAR SILT - CLAY  | <del></del>                               |                              |   | WEATHERING   |                                   | DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.   |
| * 40 30 MX 50 MX 51 MN<br>* 200 15 MX 25 MX 10 MX 35 MX 3 | 35 MX 35 MX 35 MX 36 MN 36 MN 36 MN 36 MN   | S SOILS PEAT                                  | TRACE OF ORGANIC MATTER                                 | SOILS SOILS<br>2 - 3% 3 - 5% TRO  | OTHER MATERIAL  ACE 1 - 10%               |                              |   | EW JOINTS MAY SHOW SLIGHT STAINING   | G. ROCK RINGS UNDER               | DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE  |
| LIQUID LIMIT 40 MY 4                                      | 41 MN 48 MX 41 MN 48 MX 41 MN 48 MX 41 MN   |   | LITTLE ORGANIC MATTER<br>MODERATELY ORGANIC             | 3 - 5% 5 - 12% LIT  | TTLE 10 - 20%                             | 1                            | AMMER IF CRYSTALLINE.                                       | STAINED, SOME JOINTS MAY SHOW THIN   | CLAY COATINGS IF OPEN             | HORIZONTAL.  |
| 1                   | or and a row by can be any fee covering the case of   | OILS WITH ITTLE OR HIGHLY                     | HIGHLY ORGANIC  | 5 - 10% 12 - 20% SOI<br>>10% >20% HIC   | ME 20 - 35%<br>GHLY 35% AND ABOVE         | (V SLI.) CF                  | RYSTALS ON A BROKEN SPECIME                                 | N FACE SHINE BRIGHTLY. ROCK RINGS  |                                   | DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.  |
| GROUP INDEX Ø Ø Ø   |   | ODERATE ORGANIC                               |   | GROUND WATER  |   | 1                            | F A CRYSTALLINE NATURE.                                     | STAINED AND DISCOLORATION EXTENDS  | INTO ROCK UP TO                   | FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE   |
|   | Y OR CLAYEY SILTY CLAYEY OF   | RGANIC  | WATER LI  | EVEL IN BORE HOLE IMMEDIATELY AFTER I   | DRILLING                                  | (SLI.) I                     | INCH. OPEN JOINTS MAY CONTAI                                | N CLAY. IN GRANITOID ROCKS SOME OC   | CASIONAL FELDSPAR                 | SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.  FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.   |
| MATERIALS SAND SAND GRAV                                  | /EL AND SAND SOILS MA   | ATTER   | STATIC V  | ATER LEVEL AFTER 24 HOURS   |   | 1                            |   | DRED. CRYSTALLINE ROCKS RING UNDER<br>SHOW DISCOLORATION AND WEATHERING  |                                   | FISSILE - A PROPERTY OF SPLITTING ALONG CLUSELY SPACED PARALLEL PLANES.  FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM                             |
| GEN. RATING AS A EXCELLENT TO G                           | GOOD FAIR TO POOR FAIR  |   | ∇ PW     PERCHED  | WATER, SATURATED ZONE, OR WATER BEAR!   | ING STRATA                                | (MOD.) GF                    | RANITOID ROCKS, MOST FELDSPAI                               | RS ARE DULL AND DISCOLORED, SOME S   | HOW CLAY. ROCK HAS                | PARENT MATERIAL.   |
| SUBGRADE  | POOF  | н   | OM SPRING O   | R SEEP  |   |                              | ULL SOUND UNDER HAMMER BLOV<br>ITH FRESH ROCK.              | S AND SHOWS SIGNIFICANT LOSS OF S  | THENGTH AS COMPARED               | FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY  |
| ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~                   | S ≤ LL - 30; PI OF A-7-6 SUBGROUP IS<br>NSISTENCY OR DENSENESS  | 5 > LL - 30                                   | O 00 S  | MISCELLANEOUS SYMBOLS   |   |                              |   | ORED OR STAINED. IN GRANITOID ROCK   |                                   | THE STREAM.  FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN   |
| COMPACT   | THESE OF RANGE OF STANDARD RAN  | NGE OF UNCONFINED                             |   | 707 vea   |   | (MOD. SEV.) AN               | ND CAN BE EXCAVATED WITH A                                  | GEOLOGIST'S PICK. ROCK GIVES *CLUNK*   |                                   | THE FIELD.   |
|   | STENCY PENETRATION RESISTENCE COM   | MPRESSIVE STRENGTH<br>(TONS/FT <sup>2</sup> ) | ROADWAY EMBANK  |   | NG DESIGNATIONS                           | 1                            | TESTED, WOULD YIELD SPT REI                                 | <del></del>  |                                   | JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.   |
| GENERALLY VERY L  |   |   | SOIL SYMBOL   | AUGER BORING  | S - BULK SAMPLE                           | (SEV.) IN                    | STRENGTH TO STRONG SOIL. I                                  | LORED OR STAINED. ROCK FABRIC CLEAR<br>N GRANITOID ROCKS ALL FELDSPARS AF  |                                   | LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.  |
| GRANULAR LOUS   | SE 4 TO 10<br>4 DENSE 10 TO 30  | N/A   | ARTIFICIAL FILL   | <b>D</b>  | SS - SPLIT SPOON<br>SAMPLE                | EX                           | XTENT. SOME FRAGMENTS OF ST<br>F TESTED, YIELDS SPT N VALUE |  |                                   | LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.  |
| MATERIAL DENS (NON-COHESIVE) VERY D                       | SE 30 TO 50   |   | THAN ROADWAY E  |   | ST - SHELBY TUBE                          |                              |   | ORED OR STAINED. ROCK FABRIC ELEM  | ENTS ARE DISCERNIBLE BUT          | MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN  |
| VERY S  |   | 10.05   | INFERRED SOIL B   | OUNDARY HW  | SAMPLE                                    |                              |   | ED TO SOIL STATUS, WITH ONLY FRAGM   |                                   | SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.  PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN                           |
| GENERALLY SOFT  | T 2 TO 4  | <0.25<br>0.25 TO 0.50                         | INFERRED ROCK L   | INE MONITORING WE   | RS - ROCK SAMPLE                          |                              |   | FABRIC REMAIN. IF TESTED, YIELDS   |                                   | INTERVENING IMPERVIOUS STRATUM.  |
| SILT-CLAY MEDIUM<br>MATERIAL STIF                         | F 8 TO 15   | 0.5 TO 1.0<br>1 TO 2                          | TTTTT ALLUVIAL SOIL B                                   | DUNDARY A PIEZOMETER INSTALLATION   | RT - RECOMPACTED TRIAXIAL                 |                              |   | BRIC NOT DISCERNIBLE, OR DISCERNIBLE   |                                   | RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.   |
| (COHESIVE) VERY S   |   | 2 TO 4  | •   | SLOPE INDICATO  | SAMPLE<br>DR CRD - CAN ISCRIMA BEARING    |                              | SO AN EXAMPLE.  | RTZ MAY BE PRESENT AS DIKES OR ST  | HINGERS. SAPROLITE IS             | ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND    |
|   | EXTURE OR GRAIN SIZE  |   | 25/025 DIP & DIP DIRECT ROCK STRUCTURES                 | 5   | CBR - CALIFORNIA BEARING<br>RATIO SAMPLE  |                              | Ri  | OCK HARDNESS   |                                   | EXPRESSED AS A PERCENTAGE.   |
| U.S. STO. SIEVE SIZE                                      |   | 70  | SOUNDING ROD  | SPT N-VALUE   |   |                              |   | OR SHARP PICK, BREAKING OF HAND  | SPECIMENS REQUIRES                | SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.  |
|   | 4 10 40 60 200 27<br>4.76 2.00 0.42 0.25 0.075 0.0  |   | 2 220,000 100   | ADDREVIATIONS   |   | ·                            | SEVERAL HARD BLOWS OF THE G<br>CAN BE SCRATCHED BY KNIFF OF | EOLOGIST'S PICK.<br>R PICK ONLY WITH DIFFICULTY. HARD F  | NAMMER BLOWS REGIMEED             | SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND  |
| BOULDER COBBLE G  | GRAVEL COARSE FINE  | SILT CLAY                                     | AR - AUGER REFUSAL                                      | ABBREVIATIONS HI HIGHLY   | w - MOISTURE CONTENT                      |                              | O DETACH HAND SPECIMEN.                                     | TOK ONE! WITH DIFFICULTS. MARU P   | HENDER DEUTS REGUIRED             | RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.   |
|   | (GR.) SAND SAND (CSE. SD.) (F SD.)  | (SL.) (CL.)                                   | BT - BORING TERMINATED                                  | MED MEDIUM  | V - VERY                                  |                              |   | PICK, GOUGES OR GROOVES TO 0.25  |                                   | SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR  |
| GRAIN MM 305 75   | 2.0 0.25 0.0  | Ø5 Ø.005                                      | CL CLAY CPT - CONE PENETRATION                          | MICA MICACEOUS<br>TEST MOD MODERATELY   | VST - VANE SHEAR TEST<br>WEA WEATHERED    | E                            | BY MODERATE BLOWS.  | GEOLOGIST'S PICK. HAND SPECIMENS   |                                   | SLIP PLANE.  |
| SIZE IN. 12 3   | TUDE  |   | CSE COARSE  | NP - NON PLASTIC  | 7 - UNIT WEIGHT                           |                              |   | 55 INCHES DEEP BY FIRM PRESSURE OF   |                                   | STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH |
| SOIL MOIST  | TURE - CORRELATION OF TERMS   |   | DMT - DILATOMETER TEST<br>DPT - DYNAMIC PENETRATION     |   | 76- DRY UNIT WEIGHT                       | F                            | POINT OF A GEOLOGIST'S PICK.                                |  |                                   | A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.   |
| (ATTERBERG LIMITS)  | DESCRIPTION GUIDE FOR FIELD   | MOISTURE DESCRIPTION                          | e - VOID RATIO<br>F - FINE                              | SAP SAPROLITIC<br>SD SAND, SANDY  | WOH-WEIGHT OF HAMMER                      |                              |   | DILY BY KNIFE OR PICK. CAN BE EXCA<br>IN SIZE BY MODERATE BLOWS OF A F   |                                   | STRATA CORE RECOVERY ISRECJ - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH  |
|   |   | VERY WET, USUALLY                             | FOSS FOSSILIFEROUS                                      | SL SILT, SILTY  | FIAD-FILLED IMMEDIATELY AFTER DRILLING    | F                            | PIECES CAN BE BROKEN BY FINO                                | ER PRESSURE.   |                                   | OF STRATUM AND EXPRESSED AS A PERCENTAGE.  |
| LL LIOUID LIMIT   | (SAT.) FROM BELOW THE   | GROUND WATER TABLE                            | FRAC FRACTURED, FRACTU<br>FRAGS FRAGMENTS               | RES SLI SLIGHTLY TCR - TRICONE REFUSAL  |   |                              |   | N BE EXCAVATED READILY WITH POINT BROKEN BY FINGER PRESSURE, CAN BE  |                                   | STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE        |
| PLASTIC RANGE   | SEMISOLID; REQUIR   | RES DRYING TO                                 |   |   |   | F                            | INGERNAIL.  |  |                                   | TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.  TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.  |
| (PI) PLASTIC LIMIT  | - WET - (W) ATTAIN OPTIMUM I  |   | EQU   | IPMENT USED ON SUBJECT P  | T   |                              | CTURE SPACING   | BEDD:  |                                   |  |
|   |   |   | DRILL UNITS:  | ADVANCING TOOLS:  | HAMMER TYPE:                              | TERM<br>VERY WIDE            | <u>SPACING</u><br>MORE THAN 10 FEET                         | TERM  VERY THICKLY BEDDED  | THICKNESS > 4 FEET                | BENCH MARK: BM#2-8 INCH SPIKE IN 12 INCH WHITE OAK   |
| OM OPTIMUM MOISTURE SL SHRINKAGE LIMIT                    | - MOIST - (M) SOLID: AT OR NEA  | AR OPTIMUM MOISTURE                           | MODILE D  | CLAY BITS   | X AUTOMATIC MANUAL                        | WIDE                         | 3 TO 10 FEET  | THICKLY BEDDED THINLY BEDDED   | 1.5 - 4 FEET<br>0.16 - 1.5 FEET   | 65.7 FEET RIGHT OF -BL- STA 12+28.89  ELEVATION: 2172.54 FT.   |
| SL _ SHRINKAUE LIMIT                                      | REQUIRES ADDITIO  | INAL WATER TO                                 | MOBILE B  | 6' CONTINUOUS FLIGHT AUGER  | CORE SIZE:                                | MODERATELY<br>CLOSE          | 0.16 TO 1 FEET  | VERY THINLY BEDDED .   | 0.03 - 0.16 FEET                  | NOTES:   |
| 1 .   | - DRY - (D) ATTAIN OPTIMUM N  |   | BK-51   | _ 8' HOLLOW AUGERS  |   | VERY CLOSE                   |   | THICKLY LAMINATED THINLY LAMINATED   | 0.008 - 0.03 FEET<br>< 0.008 FEET | INOTES:  |
|   | PLASTICITY  |   | CME-45C   | HARD FACED FINGER BITS  | X -N XWL                                  |                              |   | INDURATION   |                                   |  |
|   | PLASTICITY INDEX (PI) DRY   | STRENGTH                                      |   | TUNGCARBIDE INSERTS   |   | FOR SEDIMENTARY              | ROCKS, INDURATION IS THE HA                                 | RDENING OF THE MATERIAL BY CEMENT  | ING, HEAT, PRESSURE, ETC.         |  |
| NONPLASTIC<br>LOW PLASTICITY                              |   | RY LOW .                                      | X CME-550   | X CASING X W/ ADVANCER  | н   | FRIAB                        |   | BING WITH FINGER FREES NUMEROUS G  |                                   |  |
| MED. PLASTICITY   | 16-25 M   | EDIUM   | PORTABLE HOIST  | TRICONE STEEL TEETH   | HAND TOOLS:                               |                              |   | INS CAN BE SEPARATED FROM SAMPLE   |                                   |  |
| HIGH PLASTICITY   |   | HIGH  | L LOUINDER HOIST  |   | POST HOLE DIGGER  HAND AUGER              | MODER                        |   | INS CAN BE SEPARATED FROM SAMPLE<br>AKS EASILY WHEN HIT WITH HAMMER.   | WITH SIEEL PHUBE:                 |  |
|   | COLOR   | · · · · · · · · · · · · · · · · · · ·         |   |   | SOUNDING ROD                              | INDURA                       |   | NINS ARE DIFFICULT TO SEPARATE WITH  | H STEEL PROBE;                    |  |
| 1   | OR COLOR COMBINATIONS (TAN, RED. YELLOW-I   |   |   | CORE BIT  | VANE SHEAR TEST                           |                              |   | FICULT TO BREAK WITH HAMMER.   |                                   |  |
| PODIFICAS SUCH HS CIUMI, DAKE                             | N, STITEMEN, ETC. HIE USED TO DESCRIBE APP  | FEMNANCE.                                     | LEJ =   | L =   | <u> </u>                                  | EXTRE                        |   | RP HAMMER BLOWS REQUIRED TO BREA<br>IPLE BREAKS ACROSS GRAINS.   | K SAMPLE;                         |  |
|   |   |   |   | <u> </u>  | <u> </u>                                  | J                            |   | The second secon |                                   | 1  |



|      | 1           |   | <br>                                    |   |   | -1<br>-1                                | 4<br>- 4<br>                            |                                       |  | 20                                     | 33167.1.1 (B-3     |   |
|------|-------------|---|---|---|---|---|---|---------------------------------------|--|--|--------------------|---|
|      | PR          | OFILE   | THRO                                    | <i>OUGH</i>                             | A A                                     | $ND A^2$                                |   |                                       | VE = 2                                 |  | PRO                | FILE                                    |
|      |             | i<br>i<br>i                                   | 1 1 1 1                                 |   | 1                                       | 1                                       |   | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |  | ************************************** |                    | 2<br>2<br>1<br>1                        |
|      | ;<br>;      |   |   |   |   | ,<br>;<br>;                             |   | 1                                     | ;<br>;<br>;                            | :<br>:<br>:<br>:<br>:                  |                    | 1                                       |
| ;    | 1           | 1 1 1   | 1 | 1                                       | 1<br>,<br>(                             | 1                                       | :                                       | 1 1 1                                 | 1                                      | !<br>!<br>!                            |                    | t<br>!                                  |
|      |             |   |   | 1 |   | 1                                       |   | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | :<br>:<br>:<br>:<br>:                  | :<br>:                                 | ;<br>;<br>;<br>(1) |   |
|      | :<br>!<br>! | 1<br>1<br>1<br>2                              |   | · · · · · · · · · · · · · · · · · · ·   | i<br>i                                  | 1 |   | ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! | 1<br>;<br>1<br>1                       | <br>                                   |                    | 1<br>1<br>1<br>1                        |
|      |             |   | 1                                       |   | <u> </u>                                | <br>                                    | £                                       | 1 1                                   |  | D                                      | 9                  | 1                                       |
|      | 1           |   | 4                                       | B–1<br>12+20,                           | )<br>,<br>,<br>,                        | 1<br>1<br>1<br>1                        | -L-                                     | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 1                                      | $A$ , $\frac{10}{240}$                 | -2<br>-95,         | )<br>:<br>:                             |
|      | .           | 1   | -                                       | 43.0° LT                                | f                                       | !<br>!<br>!                             | STA 11                                  | +62                                   | · (                                    | $A^{\prime}$ 24.0                      | KI .               |   |
| 2160 |             |   |   |   | <br>                                    | <br>                                    | 1                                       | EXI                                   | STING GROUND                           |  |                    |   |
|      | F           | M'D A NIKMFNIT. D                             | POWAI                                   |   | 1<br>1<br>1                             | 1<br>1<br>1                             | 1 |                                       |  |  | 1                  | 1                                       |
|      | TRACE O     | MBANKMENT: B<br>SILTY SAND W<br>DF GRAVEL AND | NITH<br>D BOULDERS                      | L   S   S   S   S   S   S   S   S   S   |   | ALLUVIU                                 | JM: GRAY AND                            | BROWN SILTY                           |  | 2/06                                   | SA<br>BR           | PROLITE:<br>OWN SIL                     |
| 2150 |             | <br>  | 2/0                                     | 2 09 00 2                               | SAND                                    | WITH TRACE                              | OF ORGANIC                              | BROWN SILTY<br>MATTER, MICA A         | $\stackrel{ND}{-}\stackrel{GRAVEL}{-}$ |  | 24)                | SAND                                    |
|      |             |   | 1                                       | 100/0.7                                 | WEATHERED                               | ROCK OF GNI                             | EISS                                    | 1                                     | =///=///                               |  | WEAT               | HERED I                                 |
|      |             |   | /=///                                   | 60/0.0                                  | /=//=//                                 | <u> </u>                                | 4<br>1<br>4<br>1                        |                                       | =///- 1//                              | BT<br>FIAD                             |                    | ł<br>                                   |
| 2140 |             | CRYSTA  | LLINE ROCK:<br>ITE-GNEISS               | BT                                      | 1<br>2<br>1                             | 1 | 1                                       | 1                                     | CRYSTALLINE<br>BIOTITE: GN             | ROCK:<br>VEISS                         |                    | 1<br>1<br>1                             |
|      |             | BIOT.   | ITEGNEISS                               | 1                                       |   |   |   |                                       |  | !<br>!<br>!                            |                    |   |
| 1    |             |   |   | ;<br>;<br>;                             |   |   | 1                                       |                                       | 1,<br>1<br>1<br>1                      | 1<br>1<br>1<br>1                       |                    | 1<br>1<br>1                             |
|      |             |   | 1 1 1                                   | 1                                       |   |   | 1                                       |                                       | ;<br>1<br>1<br>1                       | 1<br>1<br>1 ·<br>1                     |                    | 1 |
| 2130 |             | <br>  | ;<br>;<br>;                             | i<br>                                   | 1                                       | 1                                       | ;<br>;<br>;                             |                                       |  |  |                    | ;<br>;<br>;                             |
|      | <br>        |   | ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;   | 1<br>1<br>1                             | 1 | ;<br>1<br>1<br>4<br>3                   | t<br>t                                  |                                       | !                                      | 1<br>1<br>1                            |                    | 1 1 1                                   |
|      |             |   | 1 I I I I I I I I I I I I I I I I I I I | 1<br>8<br>7<br>1                        | 1 1 1 1                                 | 1                                       | ;<br>;<br>;                             |                                       |  | 1                                      |                    | 1                                       |
| 2120 |             |   |   | !<br>!<br>!                             | 1<br>1<br>1                             | 1<br>1<br>1<br>1                        | 1 |                                       |  |  |                    |   |
|      |             |   |   | <br>                                    | 1 1 1 1 1 1 1 1                         | 1<br>1<br>1<br>1                        | 1<br>1<br>1                             |                                       | !<br>!<br>!                            | ;<br>;<br>;                            |                    | ;<br>!<br>!                             |
|      |             |   | 1                                       |   | 1 | 1<br>f<br>l                             | 1<br>1<br>1<br>1                        | 1                                     | ;<br>1<br>1<br>1                       | ;<br>;<br>;                            |                    | * 1<br>* 1<br>* 1                       |
| 2110 |             |   | 1                                       |   |   | 1 | t<br>t<br>t                             |                                       | 1<br>1<br>1<br>1                       | <br>                                   |                    |   |
|      |             | 1 1 1   |   | <del></del>                             |   | ;<br>;<br>;                             | :<br>:                                  | 1                                     | 1 1                                    | 1 1                                    | <br>               | 1                                       |
|      |             |   | 1 |   |   | 1<br>                                   | :<br>                                   | 1                                     | 1 ·<br>1<br>1<br>1                     | . !                                    |                    | 1<br>1<br>1<br>1                        |
|      |             | ;<br>;<br>;<br>;                              | 1<br>1<br>1<br>1                        |   |   | ,<br>1<br>4<br>1<br>1                   | ,<br>1<br>1<br>1<br>1                   |                                       | 1<br>1<br>1<br>1                       | 1                                      |                    | # # # # # # # # # # # # # # # # # # #   |
|      |             |   |   |   | :<br>                                   | ;<br>;<br>;                             | )<br>                                   | 1                                     |  |  |                    | 1<br>1                                  |
|      | · !         | 1 1 1   | 1                                       |   | :<br>:<br>:<br>!                        | :<br>!                                  | 1                                       | 1                                     | <br>                                   | 1                                      | ;<br>;<br>;        | 1                                       |
|      |             | 1       | 1<br>1<br>1<br>1                        |   | ,<br>                                   |   | · · · · · · · · · · · · · · · · · · ·   | 1                                     | !<br>!<br>!                            |  |                    | :                                       |
|      |             | 1   |   |   | :<br>1<br>1                             | 1                                       | 1                                       |                                       | 1 1                                    |  |                    |   |

|                          | ;<br>;<br>                        |   |  | 0 20                        | 40 PROJECT REFERENCE NO. S<br>33167.1.1 (B-3619) |
|--------------------------|-----------------------------------|---|--|-----------------------------|--|
| 1 1<br>1 1<br>1 1<br>1 1 | PROFILE TH                        | ROUGH B ANI   | $\mathbf{R}^{\prime}$  | VE = 2 	 SKEW = 14          |  |
|                          |                                   |   |  | 12 - 2 SVEW - 13            |  |
|                          |                                   |   |  |                             |  |
|                          |                                   |   |  |                             |  |
|                          |                                   |   |  | B-4<br>11+58,               |  |
|                          | R                                 | <u>E</u>  |  | 61.0'RT R'                  |  |
|                          | B-3                               | <i>−L−</i><br>STA 12+05   | EMBANKMENT RED SIL<br>SAND AND GRAY SAND A                       |                             |  |
| 2160                     | 2+59,                             | OWN   | GRAVEL SAPROLITE: GRAY SILTY SAN                                 |                             |  |
|                          | 5.0° LT FILL: RED-BR<br>SILTY SAN | TD EXISTIN  | G GROUND WITH TRACE OF ROCK FRAGMENTS  WEATHERED ROCK OF GNEISS. | WATER SURFACE 2/09          |  |
| 2150                     |                                   | VIUM: BROWN SANDY SILT WITH TRACE DRGANIC MATTER AND BASAL GRAVEL | <del></del>  | 7/1                         |  |
|                          |                                   | // <u>=///=</u> ///=///=  | ODYOM  | DRY                         |  |
|                          | CRYSTALLINE R<br>BIOTITE GNEI     | OCK.<br>SS  | BIO  | ALLINE ROCK:<br>TITE GNEISS |  |
| 2140                     | $BT \ FIAD$                       |   |  |                             |  |
|                          |                                   |   |  |                             |  |
| 2130                     |                                   |   |  |                             |  |
|                          |                                   |   |  |                             |  |
|                          |                                   |   |  |                             |  |
| 2120                     |                                   |   |  |                             |  |
|                          |                                   |   |  |                             |  |
| 2110                     |                                   |   |  |                             |  |
|                          |                                   |   |  |                             |  |
| 2                        |                                   |   |  |                             |  |
|                          |                                   |   |  |                             |  |
|                          |                                   |   |  |                             |  |
|                          |                                   |   | i  | i i i                       | 1  |

# NCDOT GEOTECHNICAL ENGINEERING UNIT

SHEET

|      | JECT N        |                   |              |        |     |     | B-3619    |             |           |          | VTY   | Bunco   | mbe   |              |                   | GEOLOGIST H                                   | ager, M. M.         |   |
|------|---------------|-------------------|--------------|--------|-----|-----|-----------|-------------|-----------|----------|-------|---------|-------|--------------|-------------------|---|---------------------|---|
| SITE | DESCR         | IPTIO             | <b>N</b> Bri | dge No | 56  | on  | n SR-3439 | over BIII N | loore Cre | ek       |       |         |       |              |                   |   | GROUND W            | VTR (ft                                 |
| BOR  | ING NO.       | . B-1             |              |        |     | ST  | TATION 1  | 2+20        |           | OFFS     | ET 4  | 43ft LT |       |              | ALIGNM            | IENT -L-                                      | 0 HR.               | 4.8                                     |
| COL  | LAR ELI       | E <b>V</b> . 2    | ,157.4       | ft     |     | TC  | OTAL DEP  | ΓΗ 11.3 f   |           | NORT     | HING  | 663,    | 385   |              | EASTIN            | <b>G</b> 913,427                              | 24 HR.              | 5.2                                     |
| DRIL | L MACH        | IINE              | CME-5        | 550    |     | DF  | RILL METH | OD NW       | Casing w  | SPT      |       |         |       |              |                   | HAMMER TYP                                    | E Automatic         |   |
| STA  | RT DATE       | E 02/             | 12/09        |        |     | CC  | OMP. DATE | 02/12/0     | 9         | SURF     | ACE   | WATE    | R DEP | гн г         | V/A               | DEPTH TO RO                                   | OCK N/A             |   |
| ELEV | DRIVE<br>ELEV | DEPTH             | <b>'</b>     | ow co  | ,   |     |           |             | PER FOOT  |          |       | SAMP    | . V   | L            |                   | SOIL AND ROCK DE                              | SCRIPTION           | *************************************** |
| (ft) | (ft)          | (ft)              | 0.5ft        | 0.5ft  | 0.5 | ift | 0 :       | 25 5        | 50<br>1   | 75<br>1  | 100   | NO.     | МО    |              | ELEV. (ft)        | - COIL / WE TOOK DE                           |                     | DEPTH (f                                |
|      |               |                   |              |        |     | ı   |           |             |           |          |       |         |       |              |                   |   |                     |   |
| 2160 | _             | _                 |              |        |     |     |           |             |           |          |       |         |       |              |                   |   |                     |   |
|      | -             | -                 | 1.           |        |     |     |           |             |           |          |       |         |       |              | -<br>- 2,157.4    | GROUND SUR                                    | REACE               | 0.                                      |
| 2155 | -             |                   |              |        |     | T   |           | ::::        |           |          |       |         | 1     | H            | -                 | ROADWAY EMBA<br>Brown silty sand with tra-    | NKMENT              |   |
| 100  | 2,153.5-      | -<br>- 3.9        |              |        |     | -   | <u> </u>  |             |           | 1        |       |         |       | Ηğ           | <del></del><br>-  | boulders.                                     |                     |   |
|      | 1             | -                 | WOH          | WOH    | 2   |     | <b>2</b>  |             |           | : :      |       |         | M     |              | 2,152.5           | ALLUVIA                                       | I                   | 4.                                      |
| 150  | _             |                   |              |        |     |     | <u> </u>  |             |           | <u> </u> |       |         |       | 1011         | 2,150.2 Gr        | ay silty sand with trace of and mica.         | of organic material | 7.                                      |
|      | 2,148.5       | - 8.9<br>-        | 14           | 86/0.2 |     |     |           |             |           |          |       |         |       |              | . \               | WEATHERED                                     | ROCK                | /                                       |
| 145  | 2,146.1       | 11.3              | 60/0.0       |        |     | _   | <u> </u>  | <u> </u>    | • • • •   | 1        | 0/0.7 |         | ļ     |              | 2,146.1           | Weathered rock o                              | -                   | 11.                                     |
| 143  | 1             | <del>-</del><br>- | 00/0.0       |        |     |     |           |             |           | Ū.       | 0,0.0 |         |       |              |                   | Boring Terminated with Penetration Test Refus | al at Elevation     |   |
|      | 1             | -                 |              |        |     |     |           |             |           |          |       |         |       |              |                   | 2,146.1 ft in biotite                         | e gneiss.           |   |
| 140  |               | -                 |              |        |     | l   |           |             |           |          |       | ŀ       |       |              | ,<br><del>-</del> |   |                     |   |
|      | 1             | - ·               |              |        |     |     |           |             |           |          |       |         |       |              |                   |   |                     |   |
| 125  | ‡             | -                 |              |        |     |     |           |             |           |          |       |         |       |              | ,<br>,            |   |                     |   |
| 35   | 1             | -<br>-            |              |        |     |     |           |             |           |          |       |         |       | ŀ            | -                 |   |                     |   |
|      | ‡             |                   |              |        |     |     |           |             |           |          |       |         |       |              |                   |   |                     |   |
| 30   | 1             |                   |              |        |     |     |           |             | *         |          |       |         |       | E            |                   |   |                     |   |
|      | 1             |                   |              |        |     |     |           |             |           |          |       |         |       | F            |                   |   |                     |   |
| 0.5  | 1             |                   |              |        |     |     |           |             |           |          |       |         |       | $\mathbb{E}$ |                   |   |                     |   |
| 125  | +             | •                 |              |        |     |     |           |             |           |          |       |         |       | -            | -                 |   |                     |   |
|      | ‡             |                   |              |        |     |     |           |             |           |          |       |         |       | E            |                   |   |                     |   |
| 20   | #             |                   |              |        |     |     |           |             |           |          |       |         |       | E            | _                 |   |                     |   |
|      | ‡             |                   |              |        |     |     |           |             |           |          |       |         |       | E            |                   |   | •                   |   |
| 15   | ‡             |                   |              | 1      |     |     |           |             |           |          |       |         |       | E            |                   |   |                     |   |
| 13   | +             |                   |              |        |     |     |           |             |           |          |       |         |       | F            | =                 |   |                     |   |
|      | ‡             |                   |              |        |     |     |           |             |           |          |       |         |       | E            |                   |   |                     |   |
| 10   | #             |                   | l            |        |     |     |           |             |           |          |       |         |       | E            | _                 |   |                     |   |
|      | ‡             |                   |              | 1      |     | 1   |           |             |           |          |       |         | 1     | F            |                   |   |                     |   |
| 05   | ‡             |                   | l            |        |     |     |           |             |           |          | l     |         |       | E            |                   |   |                     |   |
|      | +             | l                 |              |        |     |     |           |             |           |          |       |         |       | -            | •                 |   |                     |   |
|      | ‡             | I                 | 1            | l      |     |     |           |             |           |          |       |         |       | E            |                   |   |                     |   |
| 00   | #             |                   |              |        |     |     |           |             |           |          | 1     |         |       | E            |                   |   |                     |   |
|      | ‡             | .                 |              |        |     |     |           |             |           |          | l     |         |       | Ł            |                   |   |                     |   |
| 95   | ‡             |                   |              |        |     |     | •         |             |           |          |       |         | -     | F            |                   |   |                     |   |
|      | ‡             |                   |              |        |     |     |           |             |           |          |       |         | l     | F            |                   |   |                     |   |
|      | ‡             |                   |              |        |     |     |           |             |           |          |       | 1       |       | F            |                   |   |                     |   |
| 90   | ‡             |                   |              |        |     |     |           |             | •         |          |       | l       | .     | L            |                   |   |                     |   |
|      | ‡             |                   |              |        |     |     |           |             |           |          |       |         |       | E            |                   |   |                     |   |
| 35   | ‡             | I                 |              |        |     |     |           |             |           |          |       | l       |       | F            |                   |   |                     |   |
| ~    | ‡             |                   |              |        |     |     |           |             |           |          |       |         |       | F            |                   |   |                     |   |
|      | ‡             |                   |              |        |     |     |           |             |           |          |       |         |       | E            |                   |   |                     |   |
| 80   | +             |                   |              |        |     |     |           |             |           |          |       |         |       | F            |                   |   |                     |   |



SHEET

10

| PRO.                         | JECT N                  | <b>3</b> 3    | 167.1.       | 1      | ID.          | B-3619  | )     |           |              | cou    | NTY    | Buncon       | nbe  |             |                       |             | GEOLOGIST +  | lager, M. M.             |             |        |
|------------------------------|-------------------------|---------------|--------------|--------|--------------|---------|-------|-----------|--------------|--------|--------|--------------|------|-------------|-----------------------|-------------|--|--------------------------|-------------|--------|
| SITE                         | DESCR                   | IPTION        | l Bric       | ige No | . 56 o       | n SR-34 | 39 ov | er BIII M | loore Cr     | eek    |        |              |      |             |                       |             |  | GROUND                   | WTR (       | (ft)   |
| BOR                          | ING NO.                 | B-4           |              |        | S            | TATION  | 11+   | ·58       |              | OFF    | SET 6  | 31ft RT      |      |             | ALIGN                 | IMENT       | F-   | 0 HR.                    | N           | √A/A   |
| COLI                         | LAR ELE                 | <b>EV.</b> 2, | 164.0        | ft     | T            | OTAL D  | EPTH  | 9.1 ft    |              | NOR    | THING  | 663,3        | 27   |             | EASTI                 | <b>NG</b> 9 | 13,533   | 24 HR.                   | D           | Ory    |
| DRIL                         | L MACH                  | IINE (        | CME-5        | 50     | D            | RILL ME | ТНО   | D NW      | Casing       | w/ SPT |        |              |      |             |                       |             | HAMMER TYP   | E Automatic              | •           |        |
| STAF                         | RT DATE                 |               |              |        | С            | OMP. DA | ATE   | 02/12/0   | 9            | SUR    | ACE    | WATER        | DEPT | 1 H         | N/A                   |             | DEPTH TO RO  | OCK N/A                  | <del></del> |        |
| ELEV<br>(ft)                 | DRIVE<br>ELEV<br>(ft)   | DEPTH<br>(ft) | BLC<br>0.5ft | 0.5ft  | UNT<br>0.5ft | 0       | 25    | BLOWS F   | PER FOO      | 75     | 100    | SAMP.<br>NO. | MOI  | L<br>O<br>G | ELEV. (ft)            |             | OIL AND ROCK DI  | ESCRIPTION               | DEPTH       | H (ft) |
| 2165                         | _                       | -             |              |        |              |         |       |           |              | -      |        |              |      |             | 2,164.0               |             | GROUND SUI<br>ROADWAY EMBA<br>Red silty sa                       | ANKMENT                  |             | 0.0    |
| 2160                         | 2,159.6-                | - 4.4<br>-    | 8            | 21     | 18           |         |       | 39        |              |        |        |              |      |             | 2,160.3               | Grav        | ROADWAY EMBA<br>Gray sand and<br>SAPROLI<br>to white silty sand  | ANKMENT<br>gravel.<br>TE |             | 3.7    |
| 04.55                        | -                       | <u> </u>      |              |        |              | : : :   |       | · · !     | <del> </del> | ∄÷     |        |              |      | 1100        | <u>- 2,156.7</u>      |             | fragment   | S.                       |             | 7.3    |
| 2155                         | 2,154.9                 | 9.1           | 60/0.0       | -      | ļ            | L       |       | ****      | <u> </u>     |        | 60/0.0 | -            |      | 1           | 2,154.9               |             | WEATHERED<br>Weathered   | rock.                    |             | 9.1    |
| 2150                         | -                       |               |              |        |              |         |       |           |              |        |        |              |      |             | -<br>-<br>-<br>-      | B<br>Pen    | oring Terminated v<br>netration Test Refu<br>2,154.9 ft in bioti | sal at Elevation         |             |        |
| 2145                         | -                       | -             |              |        |              |         |       |           |              |        |        |              |      |             | -<br><br>-<br>-       |             |  |                          |             |        |
| 2140                         | -                       |               |              |        |              | -       |       |           |              |        |        |              |      |             | <br>                  |             |  |                          |             |        |
| 2135                         | -                       | -<br>-        |              |        |              |         |       |           |              |        |        |              |      |             | -<br>-<br>-           |             |  |                          |             | ·      |
| 2130                         | -<br>-<br>-             |               | ,            |        |              |         |       |           |              |        |        |              |      |             | -<br>-<br>-<br>-<br>- |             |  |                          |             |        |
| 2125                         |                         | -<br>-<br>-   |              |        |              |         |       |           |              |        |        |              |      |             | -<br><br>-<br>-       |             |  |                          |             |        |
| 2120                         | +                       | -<br>-<br>-   |              |        |              |         |       |           |              |        |        |              |      |             | -<br><br>-<br>-       |             |  | •                        |             |        |
| 2115                         | <u>+</u><br>+<br>+<br>+ | -<br>-<br>-   |              |        |              |         |       |           |              |        |        |              |      |             | -<br><br>-<br>-       |             |  |                          |             |        |
| 2110                         | <del> </del>            | •<br>•<br>•   |              |        |              |         | •     |           |              |        |        |              |      |             | -<br>-<br>-<br>-      |             |  |                          |             |        |
| 2105                         | <del> </del>            | -<br>-<br>-   |              |        |              | -       |       |           |              |        |        |              |      |             | -<br>-<br>-<br>-      |             | • .  |                          |             |        |
| 2105<br>2100<br>2095<br>2090 | +                       | -             |              |        |              |         |       |           |              |        |        | ***          |      |             | -<br>-<br>-<br>-      |             |  | • • •                    |             |        |
| 2095                         |                         |               |              |        |              |         |       |           |              |        |        |              |      |             | -<br>-<br>-<br>-<br>- |             |  |                          |             |        |
| 2090                         | +                       | -             |              |        |              |         |       |           |              |        |        |              |      | -           | <u>-</u><br>•<br>•    |             |  |                          |             |        |

# NCDOT GEOTECHNICAL ENGINEERING UNIT

SHEET

| PRO          | JECT N                |               |               |          |              | <b>G R</b> B-36 |       |        |             |         | CO       | UNTY  | Bunco       | mbe          |     |                    |          | GEOLOGIȘT [                               | Daniel, T. B.                         |          |
|--------------|-----------------------|---------------|---------------|----------|--------------|-----------------|-------|--------|-------------|---------|----------|-------|-------------|--------------|-----|--------------------|----------|---|---------------------------------------|----------|
| SITE         | DESCR                 | RIPTIO        | <b>N</b> Brid | dge No   | 56 (         | on SR-3         | 439 c | over B | III Mo      | ore Cr  | eek      |       |             |              |     |                    |          |   | GROUND                                | WTR (ft  |
| BOR          | ING NO                | . B-2         |               |          |              | OITATE          | N 10  | )+95   |             |         | OFF      | SET   | 24ft RT     | •            |     | ALIG               | NMEN.    | r -L-                                     | .0 HR.                                | 2.6      |
|              | LAR EL                |               |               |          |              | TOTAL           |       |        |             |         | ٠        |       | 663,        | 264          |     | EAST               | ING :    | 913,499                                   | 24 HR.                                | FIAD     |
|              | L MACH                |               |               | 550      |              | ORILL N         |       |        |             | asing v |          |       | ······      |              |     | ····               |          |   | PE Automatic                          | ;<br>    |
| STA          | RT DATI               | E 02/         | <del></del>   |          |              | OMP. I          | DATE  |        |             |         |          | RFACE | WATE        |              | TH  | N/A                |          | DEPTH TO R                                | OCK 7.8 ft                            |          |
| ELEV<br>(ft) | DRIVE<br>ELEV<br>(ft) | DEPTI<br>(ft) | 0.5ft         | 0.5ft    | <del>,</del> |                 | 2     |        | NS PE<br>50 | R FOO   | Γ<br>75  | 100   | SAMF<br>NO. | 17           | 0   |                    |          | OIL AND ROCK D                            | ESCRIPTION                            |          |
|              | (10)                  |               | 10.011        | 0.51     | 0.010        |                 | 1     | Ĺ      |             |         |          |       | 110.        | V MO         | ) G | ELEV. (fi          |          |   | ·                                     | DEPTH (f |
| 2160         |                       |               |               |          |              |                 |       |        |             |         |          |       |             |              |     |                    |          |   |                                       |          |
| 2100         | -                     | †             |               |          |              |                 |       |        |             |         |          |       |             |              |     | -                  |          |   |                                       |          |
|              | -                     | <u> </u>      | -             | <u> </u> |              | <del> </del>    |       | ····   |             |         | · T ·    |       | -           | <del> </del> | -   | 2,157.2            |          | GROUND SU<br>ALLUVI                       |                                       | 0.       |
| 2155         | _                     | -             |               |          |              |                 | - 1   |        |             |         | <u> </u> |       |             | $\nabla$     |     | _                  | Bre      | own silty sand with                       |                                       |          |
|              | 2,152.1               | 5.1           |               |          |              |                 |       |        |             |         |          |       | 1.          |              |     | -<br>- 2,151.6     |          |   |                                       | 5.0      |
| 2150         | -                     | E             | 4             | 14       | 10           |                 |       | 24 • • |             |         |          |       |             | Sat.         |     | 2,150.1<br>2,149.4 |          | SAPROL                                    |                                       | 7.       |
|              | -                     | E             |               |          |              | ::              | : -   |        | -           |         |          |       |             |              |     | 2,149.4<br>2,147.8 | \        | Brown silty:<br>WEATHERED                 | ROCK                                  | 9.4      |
|              | -                     |               |               |          |              |                 |       |        |             |         |          |       |             |              |     | _                  | <u> </u> | Weathered rock<br>CRYSTALLINI             | E ROCK                                | -        |
| 2145         | -                     | Ė             |               |          |              |                 |       |        |             |         |          |       |             |              |     | -                  | Boring   | ray biotite gneiss w<br>Terminated at Ele | ith muscovite.<br>vation 2,147.8 ft i | l<br>in  |
|              | -                     | -             |               |          |              |                 |       |        |             |         |          |       |             |              |     | _<br>-             | •        | biotite gne                               | iss.                                  |          |
| 2140         | \ _                   | _             |               |          |              |                 |       | •      |             |         |          |       |             |              |     |                    |          |   |                                       |          |
|              | -                     | -             |               |          |              |                 |       |        |             |         |          |       |             |              |     | <del>-</del>       |          |   |                                       | ė        |
| 2135         |                       | -             |               |          |              |                 |       |        |             |         |          |       |             |              |     | -                  |          |   |                                       |          |
| -            |                       |               |               |          |              |                 |       |        |             |         |          |       |             |              |     | _                  |          |   |                                       |          |
|              |                       |               |               |          |              |                 |       |        |             |         |          |       |             |              |     | -                  |          |   |                                       |          |
| 2130         | -                     |               |               |          |              |                 |       |        |             |         |          |       |             |              |     | <del>-</del>       |          |   |                                       |          |
|              |                       | _             |               |          |              |                 |       |        |             |         |          |       |             |              |     | -                  |          |   |                                       |          |
| 2125         | _                     | -             |               |          |              |                 |       |        |             |         |          |       |             |              |     | -                  |          |   |                                       |          |
| - 1          | 1                     | _             |               |          |              |                 |       |        |             |         |          |       |             | ŀ            |     | -<br>-             |          |   |                                       |          |
| 2120         | ‡                     | -             |               |          |              |                 |       |        |             |         |          |       |             |              |     | <b>-</b>           |          |   |                                       | *        |
| -120         | 7                     | -             |               |          |              |                 |       |        |             |         |          |       |             |              |     | <del>-</del>       |          |   |                                       |          |
|              | ‡                     | -             |               |          |              |                 |       |        |             |         |          |       |             | 1            |     | -                  |          |   |                                       |          |
| 2115         | +                     | -             |               |          |              |                 |       |        |             |         |          |       |             |              |     | -                  |          | *   |                                       |          |
|              | $\frac{1}{1}$         |               |               |          |              |                 |       |        |             |         |          |       |             |              | F   | -                  |          |   |                                       |          |
| 2110         | $\pm$                 | -<br>-        |               |          |              |                 |       |        |             |         |          |       |             |              | [   | •<br>•             |          |   |                                       |          |
|              | +                     |               |               |          |              |                 |       |        |             |         |          |       |             |              | 1   | •                  |          |   |                                       |          |
| 2105         | ‡                     |               |               |          |              |                 |       |        |             |         |          |       |             |              |     |                    |          |   |                                       |          |
| 2105         | 1                     | -             |               |          |              |                 |       |        |             |         |          |       |             |              |     | <b>-</b> ·         |          |   |                                       |          |
|              | ‡                     |               |               |          |              |                 |       |        |             |         |          |       |             |              |     |                    |          |   |                                       |          |
| 2100         | #                     |               |               |          |              |                 |       |        |             |         |          |       |             |              |     |                    |          |   |                                       |          |
|              | Ŧ                     |               |               |          |              |                 |       |        |             |         |          |       |             |              |     | •                  |          |   |                                       |          |
| 2095         | $\exists$             |               |               | l        |              |                 |       |        |             |         |          |       |             |              |     |                    |          |   |                                       |          |
|              | 1                     |               | İ             |          |              |                 |       |        |             |         |          |       |             |              |     | <del></del><br>-   |          |   |                                       |          |
| .000         | ‡                     |               |               |          |              |                 |       |        |             |         |          |       |             |              |     | •                  |          |   |                                       |          |
| 090          | +                     | .             |               |          |              |                 |       |        |             |         |          |       |             |              | E   | <del>-</del>       |          |   |                                       |          |
|              | ‡                     |               | .             |          |              |                 |       |        |             |         |          |       |             |              |     |                    |          |   |                                       |          |
| 085          | ‡                     |               |               | •        |              |                 |       |        |             |         |          |       |             |              |     | <del>-</del>       |          |   |                                       |          |
| -            | ‡                     |               |               | •        |              |                 |       |        |             |         |          |       |             |              |     |                    |          |   |                                       |          |
| 080          | ‡                     |               | 1             | 1        |              |                 |       |        |             |         |          |       |             |              | E   |                    |          |   | *                                     |          |



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| PRO   | JECT N         |                   |       |               | I <b>D.</b> B-    |                  |          |                          |           | co  | UNTY Buncon                      | nbe            |                   | GEOLOGIST D                          | aniel T B                             |           |
|-------|----------------|-------------------|-------|---------------|-------------------|------------------|----------|--------------------------|-----------|-----|----------------------------------|----------------|-------------------|--------------------------------------|---------------------------------------|-----------|
|       |                |                   |       |               |                   |                  | 9 over B | III Moo                  | re Cre    | 1   |                                  |                |                   |                                      | GROUND                                | WTR (ft)  |
|       | ING NO.        |                   |       |               | T                 |                  | 10+95    |                          |           |     | FSET 24ft RT                     |                | ALIGNMEN          | IT -L-                               | 0 HR.                                 | 2.6       |
|       | LAR ELI        |                   | 157.2 | ft            | TOTA              | AL DE            | PTH 9.4  | 1 ft                     |           |     | RTHING 663,2                     | 64             | EASTING           | 913,499                              | 24 HR.                                | FIAD      |
| DRIL  | L MACH         | INE (             | CME-5 | 50            | DRIL              | L MET            | HOD N    | W Ca                     | sing w    | /SP | Γ Core                           |                |                   | HAMMER TYP                           | E Automatic                           |           |
| STA   | RT DATE        | 02/2              | 20/06 |               | СОМ               | P. DA            | TE 02/2  | 0/06                     |           | su  | RFACE WATER                      | DEPTH          | N/A               | DEPTH TO RO                          | OCK 7.8 ft                            |           |
| COR   | E SIZE         | NXWI              | <     |               | TOTA              | AL RUI           | N 1.6 ft |                          |           | DR  | LLER Coffey,                     | Jr., C.        |                   |                                      | · · · · · · · · · · · · · · · · · · · | ****      |
| ELEV  | RÚN<br>ELEV    | DEPTH             | RUN   | DRILL<br>RATE | REC.              | JN<br>RQD        | SAMP.    | STF<br>REC.<br>(ft)<br>% | RQD       | L   |                                  |                | DESCRIPTION       | AND REMARKS                          |                                       |           |
| (ft)  | (ft)           | (ft)              | (ft)  | (Min/ft)      | REC.<br>(ft)<br>% | RQD<br>(ft)<br>% | NO.      | (ft)<br>%                | (ft)<br>% | Ğ   | ELEV. (ft)                       |                | DECONII TION      |                                      |                                       | DEPTH (ft |
| 149.3 | 2 149 4-       | - 78              | 1.6   |               | (1.6)             | (1.4)            |          |                          |           |     | 7 2 4 4 0 4                      |                | Begin Cori        | ng @ 7.8 ft<br>LINE ROCK             |                                       | 7.8       |
|       | 2;149:8        | - 7.8<br>- 9.4    | 1.0   |               | 100%              | 88%              |          | <u> </u>                 |           | 5   | 2,149.4<br>- 2,147.8<br>- Gray b | oiotite gneiss | with muscovite.   | Fresh; hard. Well foli<br>intervals. | ated with trace of                    |           |
| 2145  | -              | _                 |       |               |                   |                  |          |                          |           |     |                                  |                | a) Join           | ts @ 20°.                            |                                       | J         |
|       |                | -                 |       |               |                   |                  |          |                          |           |     |                                  | Boring Fer     | minated at Elevat | ion 2,147.8 ft in biotil             | te gneiss.                            |           |
| 2140  |                | -                 |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
| 2140  | -              | -                 |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
|       | -              | -                 |       |               |                   |                  |          |                          |           |     | <u>.</u>                         |                | •                 |                                      |                                       |           |
| 2135  |                | _                 |       | ·             |                   |                  |          |                          |           |     | ·<br>                            |                |                   |                                      |                                       |           |
|       |                | -                 |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
| 2130  | ]              |                   |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
|       |                | _                 |       |               |                   |                  |          |                          |           |     | -<br>-                           |                |                   |                                      |                                       |           |
|       | -              | -                 |       |               |                   |                  |          |                          |           |     |                                  |                |                   |                                      |                                       |           |
| 2125  |                | -                 |       |               |                   |                  |          |                          |           |     | <del></del>                      |                |                   |                                      |                                       |           |
|       | 1              | -                 |       |               |                   |                  |          |                          |           |     |                                  |                |                   |                                      |                                       |           |
| 2120  | _              |                   |       |               |                   |                  |          |                          |           |     | <del></del>                      |                |                   |                                      |                                       |           |
|       | -              | <del>-</del><br>- |       |               |                   |                  |          |                          |           |     |                                  |                |                   |                                      |                                       |           |
| 2115  |                | -                 |       |               |                   |                  |          |                          |           |     | • •                              |                |                   |                                      | •                                     |           |
|       |                | -                 |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
|       | 1              | -                 |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
| 2110  | $-\frac{1}{2}$ | -                 |       |               |                   |                  |          |                          |           |     | ·<br>                            |                |                   |                                      |                                       |           |
|       | 1              |                   |       |               |                   |                  |          |                          |           |     |                                  |                |                   |                                      |                                       |           |
| 2105  | 1              |                   |       |               |                   |                  |          |                          |           |     | ·                                |                |                   |                                      |                                       |           |
|       | 1              |                   |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
| 2100  |                |                   |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
| 2100  | †              |                   |       |               |                   |                  |          |                          |           |     | <del>-</del><br>·                |                |                   |                                      |                                       |           |
|       | 1              |                   |       |               |                   |                  |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
| 2095  | 1              | -                 |       |               |                   |                  |          |                          |           |     | ·<br><del>-</del>                |                |                   |                                      |                                       |           |
|       | 1              |                   |       |               |                   | 1                |          |                          |           |     | •                                |                |                   |                                      |                                       |           |
| 2090  | $\pm$          |                   |       |               |                   |                  |          |                          |           | l   | •                                |                | ,                 |                                      |                                       |           |
|       | I              |                   |       |               |                   |                  |          |                          |           |     | <del>-</del>                     |                |                   |                                      |                                       |           |
|       | 1              |                   |       |               |                   |                  |          |                          |           |     |                                  |                |                   | • .                                  |                                       |           |
| 2085  | +              | <b>-</b>          |       |               |                   |                  |          |                          |           |     | <del>-</del>                     |                |                   |                                      |                                       |           |
|       | ‡              |                   |       |               |                   |                  |          |                          |           |     |                                  |                |                   |                                      |                                       | •         |
| 2080  | ‡              |                   |       |               |                   |                  |          |                          |           |     | <del>-</del>                     |                | ,                 |                                      | •                                     | •         |
|       | ‡              |                   |       |               |                   |                  |          |                          |           |     |                                  |                |                   |                                      | ,                                     |           |
| 2075  | +              |                   |       |               |                   |                  |          |                          |           |     |                                  |                |                   | •                                    | , ,                                   |           |
| 2075  | +              |                   |       |               |                   |                  |          |                          |           |     | <del>-</del>                     |                |                   |                                      | . '                                   |           |
|       | ‡              |                   |       |               |                   |                  |          |                          |           |     |                                  |                |                   | •                                    | •                                     |           |
| 2070  | #              |                   |       |               |                   |                  |          |                          |           |     | -                                |                |                   | •                                    |                                       |           |



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| PRO  | JECT N                                  | <b>O.</b> 33                                 | 167.1. | 1      | ID.   | . E     | 3-3619     |             |           | COUNTY       | Bunco         | mbe        |            |                                       | G            | EOLOGIST Dar                              | iel, T. B.               |          |
|------|---|--|--------|--------|-------|---------|------------|-------------|-----------|--------------|---------------|------------|------------|---------------------------------------|--------------|---|--------------------------|----------|
| SITE | DESCR                                   | IPTIO  | N Brid | dge No | 56    | on :    | SR-3439    | over BIII N | Moore Cre | ek           |               |            |            | · · · · · · · · · · · · · · · · · · · |              |   | GROUND V                 | /VTR (f  |
| BOR  | ING NO.                                 | B-3  |        |        |       | STA     | ATION 12   | 2+59        |           | OFFSET       | 25ft LT       |            |            | ALIGNI                                | MENT         | -L-                                       | 0 HR.                    | 2.       |
| COL  | AR ELE                                  | <b>EV</b> . 2                                | 154.9  | ft     | 7     | TOT     | TAL DEPT   | H 12.3 f    | t         | NORTHIN      | <b>G</b> 663, | 414        |            | EASTIN                                | <b>IG</b> 91 | 3,440                                     | 24 HR.                   | FIA      |
| DRIL | L MACH                                  | IINE (                                       | CME-5  | 50     | 1     | DRI     | ILL METH   | OD NW       | Casing w  | SPT Core     | )             |            | ····       |                                       | T            | HAMMER TYPE                               | Automatic                |          |
| STAF | RT DATE                                 | 02/2   | 20/06  |        |       | CON     | MP. DATE   | 02/20/0     | 6         | SURFACE      | WATER         | R DEP      | TH         | N/A                                   |              | DEPTH TO ROC                              |                          |          |
| LEV  | DRIVE                                   | DEPTH  | BLC    | ow co  | UNT   | П       |            | BLOWS       | PER FOOT  |              | SAMP          | <b>V</b> / | 1          | <u> </u>                              | L            |   |                          |          |
| (ft) | ELEV<br>(ft)                            | (ft)   | 0.5ft  | 0.5ft  | 0.5ft |         | 0 2        | 5           | 50        | 75 100       | NO.           | MO         | O<br>OI G  | ELEV. (ft)                            | SO           | IL AND ROCK DESC                          |                          | DEPTH    |
|      |   |  |        |        |       |         |            |             |           |              |               |            |            |                                       |              |   |                          | <u> </u> |
| 2155 |   |  |        |        |       |         |            |             |           |              |               |            |            | 2,154.9                               |              | GROUND SURFA                              | ACE.                     |          |
|      | 2,153.2                                 | 1.7  |        |        |       | $\prod$ |            |             |           |              |               | $\nabla$   | X          | - 2,153.4                             |              | ARTIFICIAL FIL                            | L                        |          |
|      | 1                                       | -  | 2      | 2      | 2     |         | <b>4</b> 4 |             | : : : :   |              |               | ├-w-       |            | - 2,151.6                             |              | Red-brown silty sa<br>ALLUVIAL            | *·····                   | <i></i>  |
| 150  | 4                                       | -  |        |        |       | 1       |            |             | T         | <del> </del> | 1             |            |            | 2,150.7                               | Dark b       | rown sandy silt with matter, and trace of | trace organic<br>gravel. |          |
| l    | 1                                       | -  |        |        |       |         |            |             |           |              |               |            |            | -                                     |              | ALLUVIAL<br>Alluvial gravel.              |                          | 1        |
| 145  | 1                                       | •  |        |        |       |         |            |             | : : : :   |              |               |            |            | - L<br>-                              |              | CRYSTALLINE RO                            | OCK                      | J        |
|      | 7                                       | •  |        |        |       |         |            |             |           | · · · ·      | 11            |            |            | <del>-</del>                          | Gray         | biotite gniess with r                     | nuscovite.               |          |
| ŀ    | ‡                                       | <u>.                                    </u> |        |        |       | ╫       |            |             | 1         | 1            | 4             | -          | كأبخ       | - 2,142.6<br>- Bo                     | oring Te     | rminated with Stand                       | ard Penetration          | 1        |
| 140  | 4                                       | •  |        |        |       |         |            |             |           |              |               |            |            |                                       |              | usal at Elevation 2,14<br>gneiss.         |                          |          |
|      | ‡                                       |  |        |        |       |         |            |             |           |              |               |            |            | <del>-</del><br>-                     |              | g31001                                    |                          |          |
| 35   | ‡                                       |  |        |        |       |         |            |             |           |              |               |            |            | -<br>-                                |              |   |                          |          |
|      | ‡                                       | <del>.</del>                                 |        |        |       |         |            |             |           |              |               |            |            | <del>-</del>                          |              |   |                          |          |
|      | ‡                                       | •  |        |        |       |         |            |             |           |              |               |            |            |                                       |              |   |                          |          |
| 30   | #                                       | •  |        |        |       |         |            |             |           |              |               |            |            | •                                     |              |   |                          |          |
| ĺ    | ‡                                       |  |        |        |       |         |            |             |           |              |               |            |            |                                       |              |   |                          |          |
| 25   | ‡                                       |  |        |        |       |         |            |             | •         |              |               |            |            |                                       |              |   |                          |          |
| 25   | +                                       |  |        | .      |       |         |            |             |           |              |               |            | 1 1        |                                       |              |   |                          |          |
|      | ‡                                       |  |        |        |       |         |            |             |           |              |               |            | lE         |                                       |              |   |                          |          |
| 20   | #                                       |  |        |        |       |         |            |             |           |              |               |            |            |                                       |              |   |                          |          |
|      | • ‡                                     |  | l      |        |       |         |            |             |           |              |               |            |            |                                       |              |   |                          |          |
| 15   | ‡                                       |  | l      | l      |       |         |            |             |           |              |               |            |            | •                                     |              |   |                          |          |
| 15   | +                                       |  | l      | - 1    |       |         |            |             |           |              |               |            |            | _                                     |              |   |                          |          |
|      | 1                                       | l  |        |        |       |         |            |             |           |              |               |            | -          |                                       |              |   |                          |          |
| 10   | 1                                       | ļ  |        |        |       |         |            |             |           |              |               |            |            |                                       |              |   |                          |          |
|      | <u></u>                                 | l  |        | l      |       |         | •          |             |           |              |               |            |            | -                                     |              |   |                          |          |
|      | <u></u>                                 | l  | l      | - 1    |       |         |            |             |           |              |               |            | F          |                                       |              |   |                          |          |
| 05   | $\pm$                                   |  | 1      | 1      |       |         |            |             |           |              |               |            | F          | -                                     |              |   |                          |          |
|      | ±                                       |  | l      | 1      |       |         |            |             |           |              |               |            | F          |                                       |              |   |                          |          |
| 00   | <u></u>                                 |  | l      |        |       |         |            |             |           |              |               |            | F          |                                       |              |   |                          |          |
|      | ±                                       |  |        |        |       |         |            |             |           |              |               |            | F          | -                                     |              |   |                          |          |
|      | Ī                                       |  |        |        | -     |         |            |             |           |              |               | l          | F          |                                       |              |   |                          |          |
| 95   | Ŧ                                       | l  |        | ]      |       |         |            |             |           |              |               |            | F          | -                                     |              |   |                          |          |
|      | I                                       |  |        | .      |       |         |            |             |           |              |               | .          | F          |                                       |              |   |                          |          |
| 0    | Ŧ                                       |  |        |        |       |         |            |             |           |              |               |            | þ          |                                       |              |   |                          |          |
| 7    | Ŧ                                       |  |        |        |       |         |            |             |           |              | 1             |            | -          | •                                     |              |   |                          |          |
|      | Ŧ                                       |  |        |        |       |         |            |             |           |              |               |            |            |                                       |              |   |                          |          |
| 5    | ‡                                       |  |        |        |       |         |            |             |           |              |               |            | L          |                                       |              |   |                          |          |
|      | ‡                                       |  |        |        |       |         | *          |             |           |              |               | l          | . <u> </u> |                                       |              |   |                          |          |
|      |   |  |        |        |       |         |            |             |           |              |               |            |            |                                       |              |   |                          |          |
| 10   | ‡                                       |  |        |        |       |         |            |             |           |              |               |            | E          |                                       |              |   |                          |          |
| 30   | +++++++++++++++++++++++++++++++++++++++ |  |        |        |       |         |            |             |           |              |               |            | E          |                                       |              |   |                          |          |



SHEET

|               | JECT N              |                  |               |                  | ID. B        |                  |              |                          |                  | 1                                      | UNTY Buncombe                |   | GEOLOGIST D                               | aniel, T. B.     |
|---------------|---------------------|------------------|---------------|------------------|--------------|------------------|--------------|--------------------------|------------------|--|------------------------------|---|---|------------------|
|               |                     |                  | <b>V</b> Brid | dge No. 5        | <del></del>  |                  |              | III Mod                  | re Cre           |  |                              |   |   | GROUND WTR (1    |
|               | ING NO              |                  |               |                  | +            |                  | 12+59        |                          | ····             | <del> </del>                           | FSET 25ft LT                 | ALIGNMEN                                |   | 0 HR. 2.         |
|               | LAR EL              |                  |               | ~~~~             | <del> </del> |                  | PTH 12       |                          |                  | ــــــــــــــــــــــــــــــــــــــ | RTHING 663,414               | EASTING                                 |   | 24 HR. FIA       |
|               | L MAC               |                  |               | 550              | <del> </del> |                  | THOD N       |                          | sing w           |  |                              |   | HAMMER TYPI                               |                  |
|               | RT DAT              |                  |               |                  | <del>}</del> |                  | TE 02/2      |                          |                  | <del> </del>                           | RFACE WATER DEPTH            | N/A                                     | DEPTH TO RO                               | CK 4.2 ft        |
|               | E SIZE              | T                | Т             | DRILL            | TOTA         | AL RU            | N 8.1 ft     |                          | ΣΔΤΔ             | <del> </del>                           | ILLER Coffey, Jr., C.        |   |   |                  |
| ELEV<br>(ft)  | RUN<br>ELEV<br>(ft) | DEPTH<br>(ft)    | RUN<br>(ft)   | RATE<br>(Min/ft) | REC.         | RQD<br>(ft)<br>% | SAMP.<br>NO. | STF<br>REC.<br>(ft)<br>% | RQD<br>(ft)<br>% | L<br>0<br>G                            | ELEV. (ft)                   | DESCRIPTION A                           | AND REMARKS                               | DEPTH            |
| 150.7<br>2150 | 2,150.7             | 1-42             | 3.1           |                  | (0.7)        | (0.7)            |              | ļ                        | ļ                |  |                              | Begin Corin                             |   |                  |
|               | 2,147.6             | +                | 3.1           |                  | (2.7)<br>87% | (2.7)<br>87%     | ·            |                          |                  |  | 2,150.7<br>- Grey biotite gn | eiss with muscovite                     | LINE ROCK and small garnets. Fr           | esh; hard. Well  |
|               | 2,141.0             | <del>T 7.3</del> | 5.0           |                  | (4.4)        | (4.4)            |              |                          |                  |  | •<br>•                       |   | of massive intervals.  y foliation @ 50°. |                  |
| 2145          | -                   | Ŧ                |               |                  | 88%          | 88%              |              |                          |                  |  | <del>-</del><br><del></del>  |   |   |                  |
|               | 2,142.6             | 12.3             |               |                  |              |                  |              |                          |                  |  | - 2,142.6                    |   |   | 12               |
| 2140          |                     | Ŧ                |               |                  |              |                  |              |                          |                  |  | - Boring Termina             | ated with Standard P<br>2,142.6 ft in I | enetration Test Refu<br>biotite gneiss.   | sal at Elevation |
|               | _                   | Ŧ                |               |                  |              |                  |              |                          |                  |  | <del></del> ·                |   |   |                  |
|               |                     | Ŧ                |               |                  |              |                  | ,            |                          |                  |  | •<br>•                       |   |   |                  |
| 2135          | -                   | Ŧ                |               |                  |              |                  |              |                          |                  |  | -<br>-                       |   |   |                  |
|               |                     | Ī                |               |                  |              |                  |              |                          |                  |  |                              |   |   |                  |
| 2130          |                     | Ŧ                |               |                  |              |                  |              |                          |                  |  | •                            |   |   |                  |
|               |                     | Ŧ.               |               |                  |              |                  |              |                          |                  |  | <del>-</del><br>·            |   |   |                  |
|               |                     | Ŧ                |               |                  |              |                  |              |                          |                  |  | •                            |   |   | *                |
| 125           | _                   | Ŧ                |               |                  |              |                  |              |                          |                  |  | ·<br><del>-</del>            |   |   |                  |
|               |                     | Ŧ                |               |                  |              |                  |              |                          |                  |  | •                            |   |   |                  |
| 120           |                     | Ŧ                |               |                  |              |                  |              |                          |                  | ŀ                                      | •                            |   |   |                  |
|               |                     | F                |               |                  |              |                  |              |                          |                  |  | <del>-</del><br>·            |   |   |                  |
|               |                     | F                |               |                  |              |                  |              |                          |                  |  | •<br>•                       |   |   |                  |
| 115           | _                   | F                |               |                  |              |                  |              |                          |                  |  | <del>-</del>                 |   |   |                  |
|               |                     | F                |               |                  |              | .                |              |                          |                  |  |                              |   | •   |                  |
| 110           |                     | F                |               |                  |              |                  |              |                          |                  | F                                      |                              | ٠.,                                     |   |                  |
|               | -                   | F                |               |                  |              |                  |              |                          |                  | ļ                                      | <del>-</del>                 |   |   |                  |
| .             | -                   |                  |               |                  |              | l                |              |                          |                  | F                                      |                              |   |   |                  |
| 2105          | _                   |                  |               |                  |              | 1                |              |                          |                  | F                                      | <del>-</del>                 |   |   |                  |
|               | -                   |                  |               |                  |              | l                |              |                          |                  | F                                      |                              |   |   |                  |
| 100           | -                   |                  |               |                  |              | l                |              | ,                        |                  | F                                      |                              |   |   |                  |
|               | -                   | _                |               |                  |              |                  |              |                          |                  | F                                      | -                            |   |   |                  |
|               | -                   |                  |               |                  |              |                  |              |                          |                  | F                                      |                              |   |   |                  |
| 095           | _                   |                  |               |                  |              | İ                |              |                          |                  | F                                      |                              |   |   |                  |
|               | -                   | _                |               |                  |              |                  |              |                          | l                | F                                      |                              |   |   |                  |
| 090           | _                   |                  |               |                  | 1            |                  |              |                          |                  | F                                      |                              |   |   |                  |
|               | -                   | -                |               |                  | 1            |                  |              |                          | ĺ                | F                                      | •                            |   |   |                  |
| l             | -                   | -                |               |                  | l            |                  |              |                          | 1                | F                                      |                              |   |   |                  |
| 085           |                     | -                |               |                  |              |                  |              |                          |                  | F                                      | -                            |   |   |                  |
|               | ]                   |                  |               |                  |              |                  |              |                          | Ì                | F                                      |                              |   |   |                  |
| 080           | _]                  | -                |               |                  |              |                  |              |                          |                  | F                                      |                              |   |   |                  |
|               | 7                   | _                |               |                  |              |                  |              |                          |                  | F                                      | -                            |   |   |                  |
|               | 1                   | - 1              |               |                  |              |                  |              |                          |                  | F                                      |                              |   | •   |                  |
| 075           | -                   | -                |               | .                |              |                  |              |                          |                  | F                                      | -                            |   |   |                  |
|               | . 1                 | -                |               |                  |              |                  |              |                          |                  | F                                      |                              |   |   |                  |
|               |                     |                  |               |                  |              |                  |              | l                        |                  | 上                                      |                              |   |   |                  |

Template Revised 02/07/06

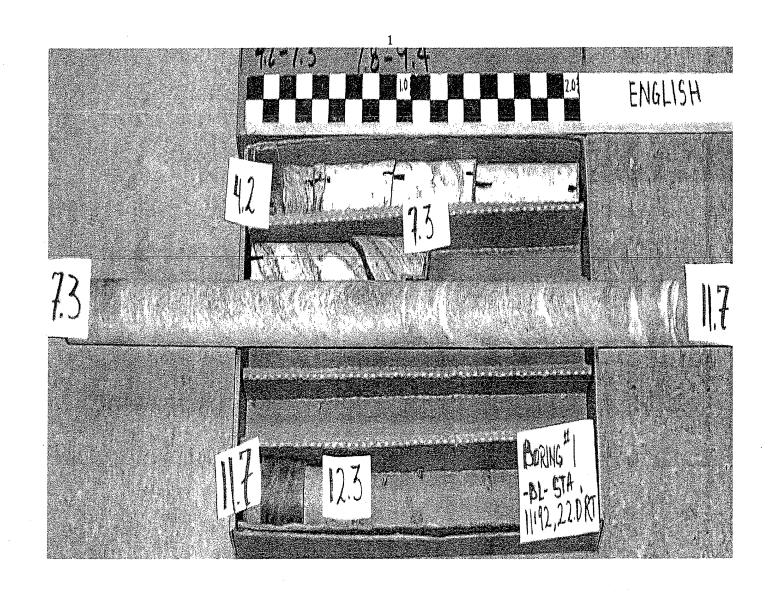
# FIELD SCOUR REPORT

| WBS:  | 33167.1.1                       | TIP:                       | B-3619          |           | COUNTY: Buncombe    |                        |  |  |  |  |  |
|---|---------------------------------|----------------------------|-----------------|-----------|---------------------|------------------------|--|--|--|--|--|
| DESCRIPTION(1): Bridge No. 56 on SR-3439 over Bill Moore Creek        |                                 |                            |                 |           |                     |                        |  |  |  |  |  |
| EXISTING BRIDGE   |                                 |                            |                 |           |                     |                        |  |  |  |  |  |
| Information from:   | Field In Other                  | nspection _<br>(explain) _ | X N             | Microfilm | n (reel po          | os:)                   |  |  |  |  |  |
| Bridge No.:<br>Foundation Type: _                                     | 56 Length                       | :                          | Total Bents:    | 3         | Bents in Channel: 1 | Bents in Floodplain: 2 |  |  |  |  |  |
| EVIDENCE OF S Abutments or E  | COUR(2)                         |                            |                 |           |                     |                        |  |  |  |  |  |
| Interior Bents: I   |                                 |                            |                 |           |                     |                        |  |  |  |  |  |
| Channel Bed: 1  | None noted.                     |                            |                 |           |                     |                        |  |  |  |  |  |
| Channel Bank: 1   | lone noted.                     |                            |                 |           |                     |                        |  |  |  |  |  |
| EXISTING SCOU<br>Type(3): <u>F</u>                                    | R PROTECTIO<br>Pile and panel e |                            | lls.            |           |                     |                        |  |  |  |  |  |
| Extent(4): Walls extend 2 feet beyond edge of bridge, on either side. |                                 |                            |                 |           |                     |                        |  |  |  |  |  |
| Effectiveness(5): (   |                                 |                            |                 |           |                     |                        |  |  |  |  |  |
| Obstructions(6): _  | imber debris or                 | upstream                   | side of interio | or bent.  |                     |                        |  |  |  |  |  |

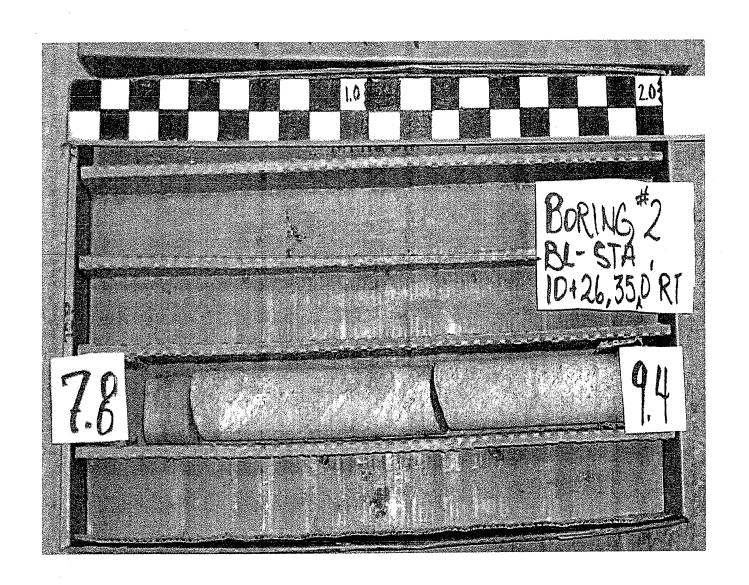
#### **INSTRUCTIONS**

- 1 Describe the specific site's location, including route number and body of water crossed.
- 2 Note scour evidence at existing end bents or abutments (e.g. undermining, sloughing, degradations).
- 3 Note existing scour protection (e.g. rip rap).
- 4 Describe extent of existing scour protection.
- 5 Describe whether or not the scour protection appears to be working.
- 6 Note obstructions such as dams, fallen trees, debris at bents, etc.
- 7 Describe the channel bed material based on observation and/or samples. Include any lab results with report.
- 8 Describe the channel bank material based on observation and/or samples. Include any lab results with report.
- 9 Describe the material covering the banks (e.g. grass, trees, rip rap, none).
- 10 Determine the approximate floodplain width from field observation or a topographic map.
- 11 Describe the material covering the floodplain (e.g. grass, trees, crops).
- 12 Use professional judgement to specify if the stream is degrading, aggrading, or static.
- 13 Describe potential and direction of the stream to migrate laterally during the bridge's life (approx. 100 years).
- Give the design scour elevation (DSE) expected over the life of the bridge (approx. 100 years). This elevation can be given as a range across the site, or for each bent. Discuss the relationship between the Hydraulics Unit theoritical scour and the DSE. If the DSE is dependent on scour counter measures, explain (e.g. rip rap armoring on slopes). The DSE is based on the erodability of materials, giving consideration to the influence of joints, foliation, bedding characteristics, % core recovery, % RQD, differential weathering, shear strength, observations at existing structures, other tests deemed appropriate, and overall geologic conditions at the site.

| a,   |  |                   |              |             | NFORM     |          | <u>N</u> |   |        |          |             |  |
|--|--|-------------------|--------------|-------------|-----------|----------|----------|---|--------|----------|-------------|--|
| Channel Bed I                                | Material(7): <u>S</u>                  | Sand, gra         | vel, col     | obles an    | nd boulde | ers.     |          |   |        |          |             |  |
| Channel Bank I                               | nel Bank Material(8): Sand and gravel. |                   |              |             |           |          |          |   |        |          |             |  |
| Channel Banl                                 | < Cover(9): _S                         | Shrubs.           |              |             |           |          |          |   |        |          |             |  |
|  | Width(10): <u>L</u>                    |                   |              |             |           |          |          |   |        |          |             |  |
| Floodplain                                   | Cover(11): <u>T</u>                    | rees and          | shrub        | S.          |           | ,        |          |   |        |          |             |  |
| Stream is(12): Aggrading Degrading _X Static |  |                   |              |             |           |          |          |   |        |          |             |  |
| hannel Migration Ten                         |  |                   |              |             |           |          |          |   |        |          |             |  |
| Observations and C                           | ther Comme                             | nts: <u>Inter</u> | ior ben      | ıt added    | relativel | y recent | tly.     |   |        |          |             |  |
| Reported by: C A Dunnagan Date: 2/11/2009    |  |                   |              |             |           |          |          |   |        |          |             |  |
| Reported by: C A Dunnagan Date: 2/11/2009    |  |                   |              |             |           |          |          |   | .000   |          |             |  |
| DESIGN SCOUR ELEVATIONS(14)                  |  |                   |              |             | Feet      |          |          |   | Meters |          |             |  |
|  |  |                   |              |             |           |          |          |   |        |          |             |  |
|  |  |                   |              |             |           |          |          |   |        |          |             |  |
|  |  |                   |              |             |           |          |          |   |        |          |             |  |
|  | -                                      |                   |              |             | ļ         |          |          |   |        |          |             |  |
|  |  |                   |              |             |           |          |          |   |        |          |             |  |
|  |  |                   |              |             |           |          |          |   |        |          |             |  |
| Comparison of DSE There were no scou         |  |                   |              |             |           | an Pane  | ort      |   |        |          |             |  |
| dated 17 April 2009.                         |  | resemed           | in the       | пушаш       | iics Desi | gii Nepi | JIL      |   |        |          |             |  |
| DSE determined by: Date:                     |  |                   |              |             |           |          |          |   |        |          |             |  |
|  |  |                   |              |             |           |          |          |   |        |          |             |  |
| SOIL ANALYSIS RE                             | SULTS FRO                              | OM CHAI           | NEL E        | BED AN      | D BANK    | MATE     | RIAL     |   |        | <u> </u> | <del></del> |  |
| Bed or Bank Sample No.                       |  |                   | <del> </del> |             |           |          |          |   |        |          |             |  |
| Retained #4                                  |  |                   | <b> </b>     |             |           |          |          |   |        |          |             |  |
| Passed#10                                    |  |                   |              |             |           |          |          |   |        |          |             |  |
| Passed#40                                    |  |                   | ļ            | ·           |           |          |          |   |        |          |             |  |
| Passed #200                                  |  |                   | <del> </del> |             |           |          |          |   |        | <u> </u> |             |  |
| Coarse Sand<br>Fine Sand                     |  |                   | <b>-</b>     |             |           |          |          |   |        |          |             |  |
| Silt   |  |                   | <b> </b>     |             |           |          |          |   |        |          |             |  |
| Clay   |  |                   | <del> </del> |             |           |          |          |   |        |          |             |  |
| LĹ   |  |                   | 1            |             |           |          |          |   |        |          |             |  |
| PI   |  |                   |              |             |           |          |          |   |        |          |             |  |
| AASHTO                                       |  |                   | ļ            |             |           |          |          |   |        |          |             |  |
| Station Offset                               |  |                   | <del> </del> | <del></del> |           |          | 4        | _ |        | <b></b>  |             |  |
| Depth  |  |                   | <del> </del> |             |           |          |          |   |        |          |             |  |
| Dopui  |  |                   |              |             |           |          |          |   |        | l        |             |  |



33167.1.1 (B-3619)
Buncombe County
Bridge No. 56 on SR-3439
over Bill Moore Creek.
B-1
Box 1 of 1



33167.1.1 (B-3619)
Buncombe County
No. 56 on SR-3439
over Bill Moore Creek.
B-2
Box 1 of 1