

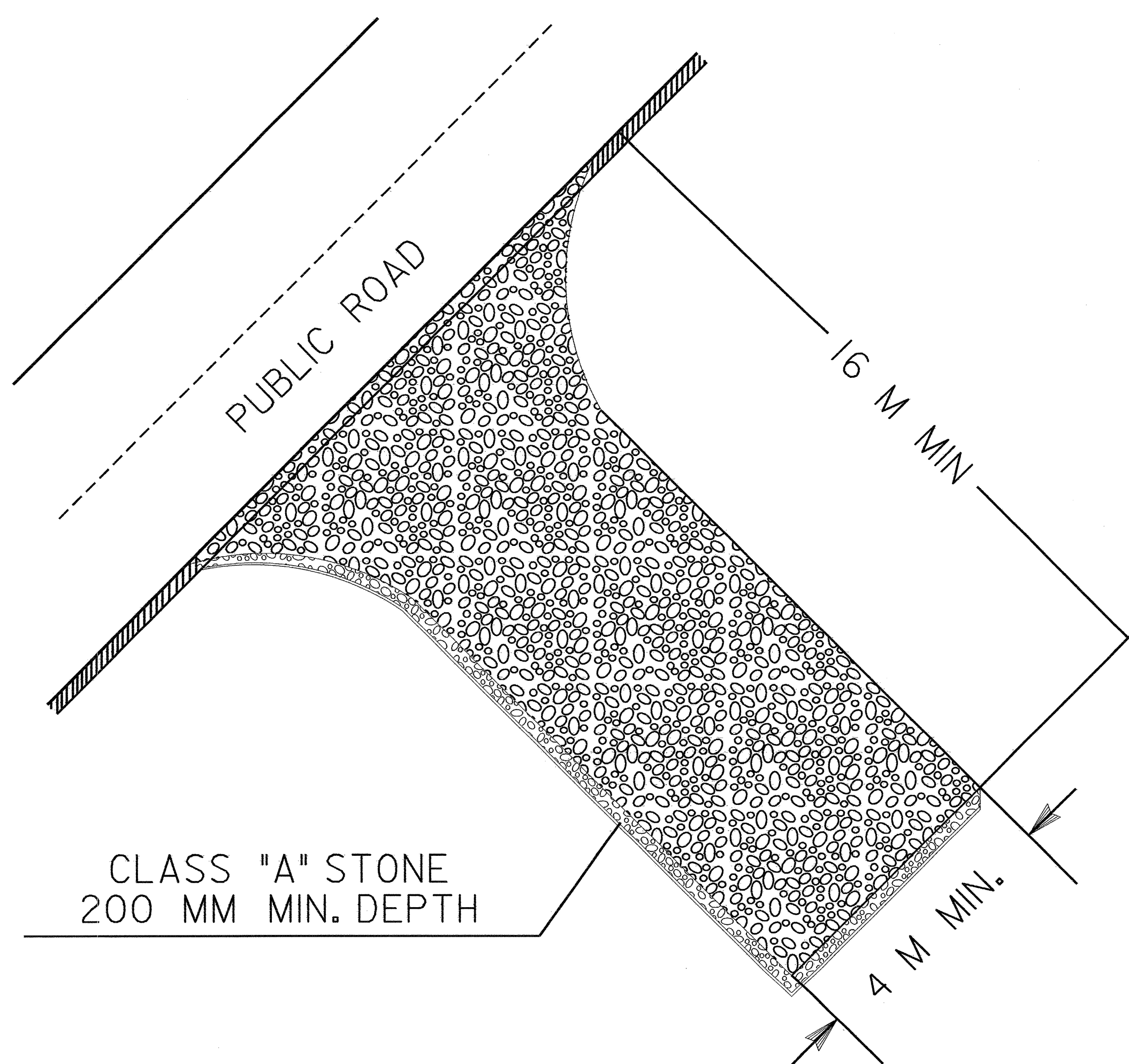


PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-2
R / W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

TEMPORARY GRAVEL CONSTRUCTION ENTRANCE

NOTES:

1. TURNING RADIUS SUFFICIENT TO ACCOMODATE LARGE TRUCKS SHALL BE PROVIDED.
2. ENTRANCE(S) SHOULD BE LOCATED TO PROVIDE FOR UTILIZATION BY ALL CONSTRUCTION VEHICLES.
3. MUST BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING OR DIRECT FLOW OF MUD ONTO STREETS. PERIODIC TOPDRESSING WITH STONE WILL BE NECESSARY.
4. ANY MATERIAL TRACKED ONTO THE ROADWAY MUST BE CLEANED UP IMMEDIATELY.
5. GRAVEL CONSTRUCTION ENTRANCE SHALL BE LOCATED AT ALL POINTS OF INGRESS AND EGRESS UNTIL SITE IS STABILIZED. FREQUENT CHECKS OF THE DEVICE AND TIMELY MAINTENANCE MUST BE PROVIDED.
6. NUMBER AND LOCATION OF CONSTRUCTION ENTRANCES TO BE DETERMINED BY THE ENGINEER

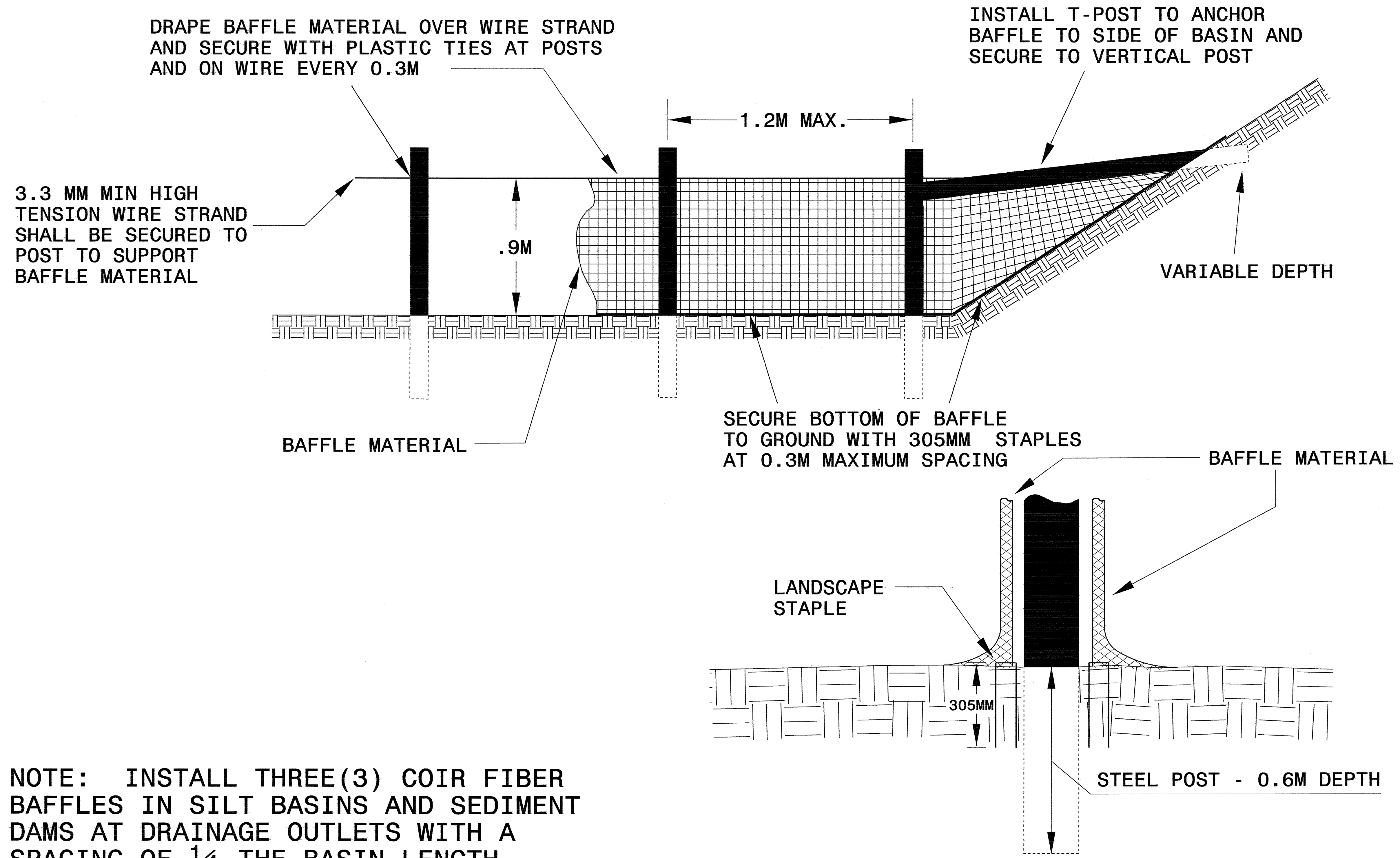


NOTE: FILTER FABRIC TO BE PLACED BENEATH STONE



PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-2A
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER


COIR FIBER BAFFLE DETAIL

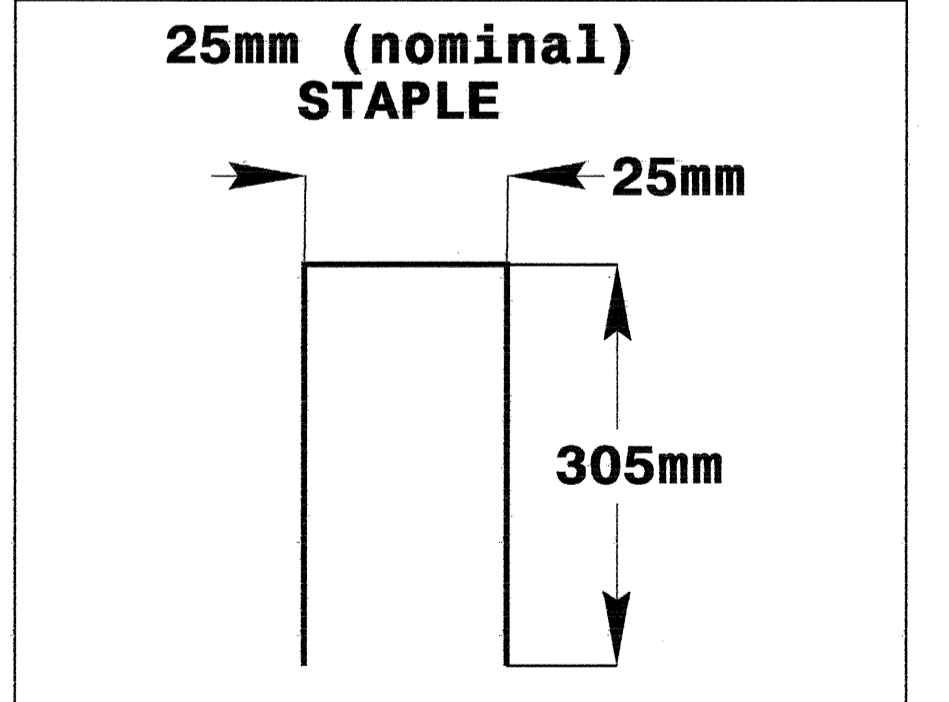
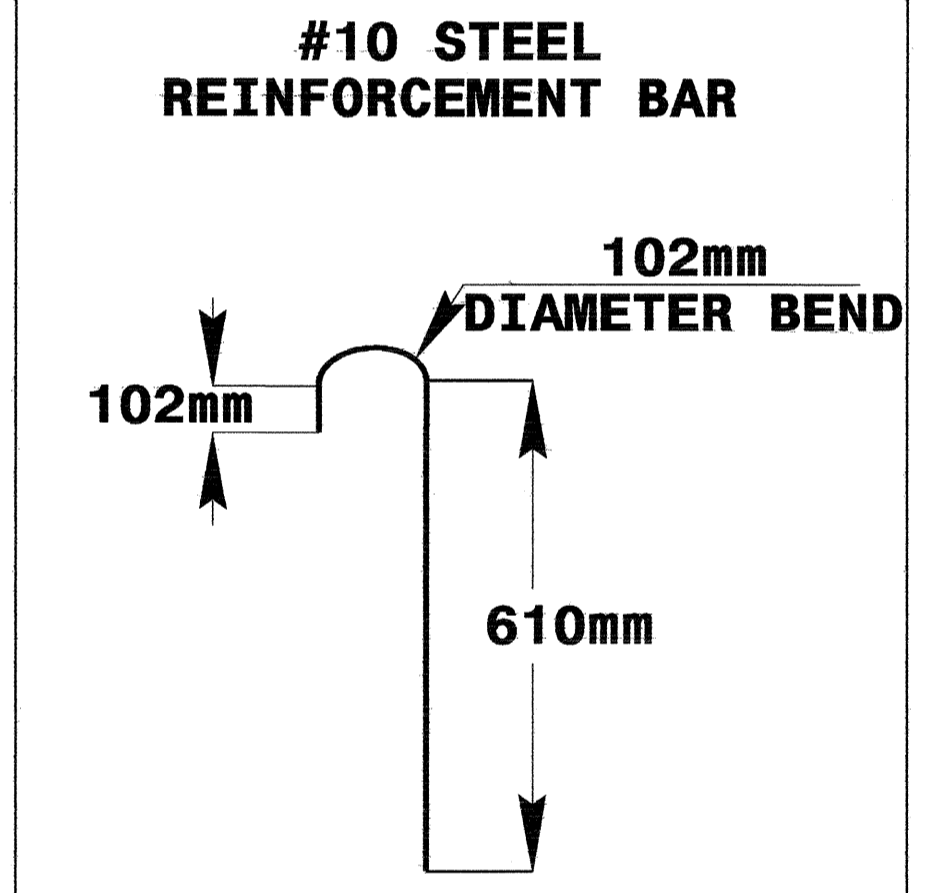
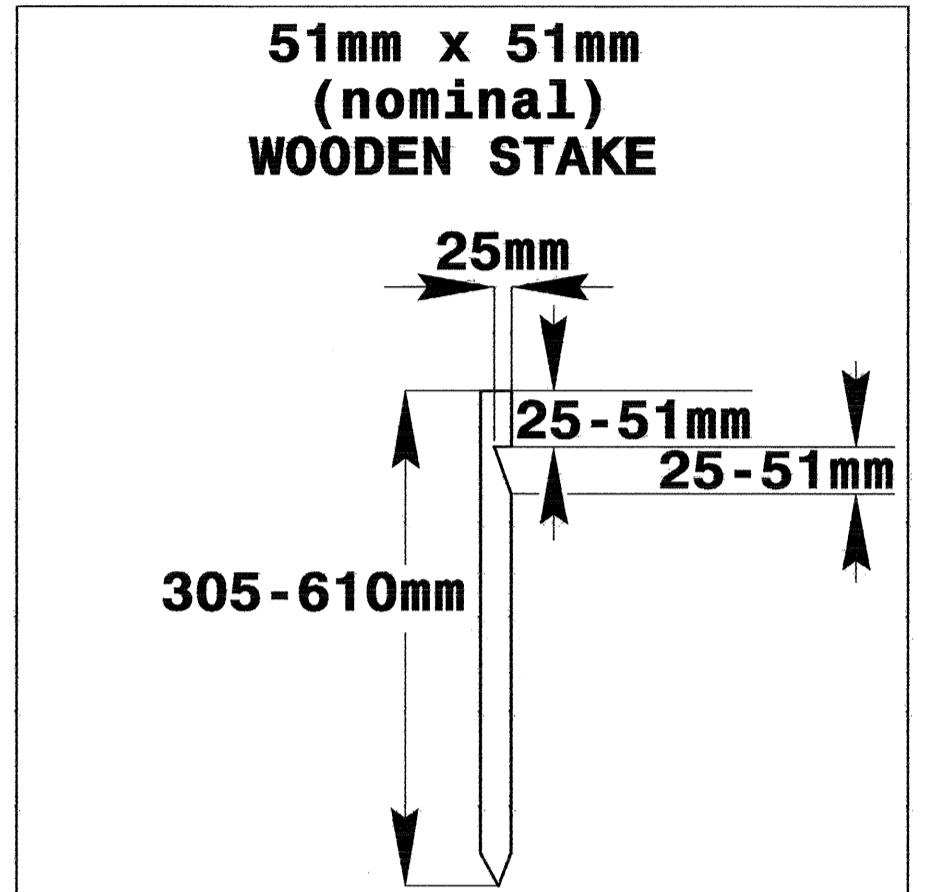
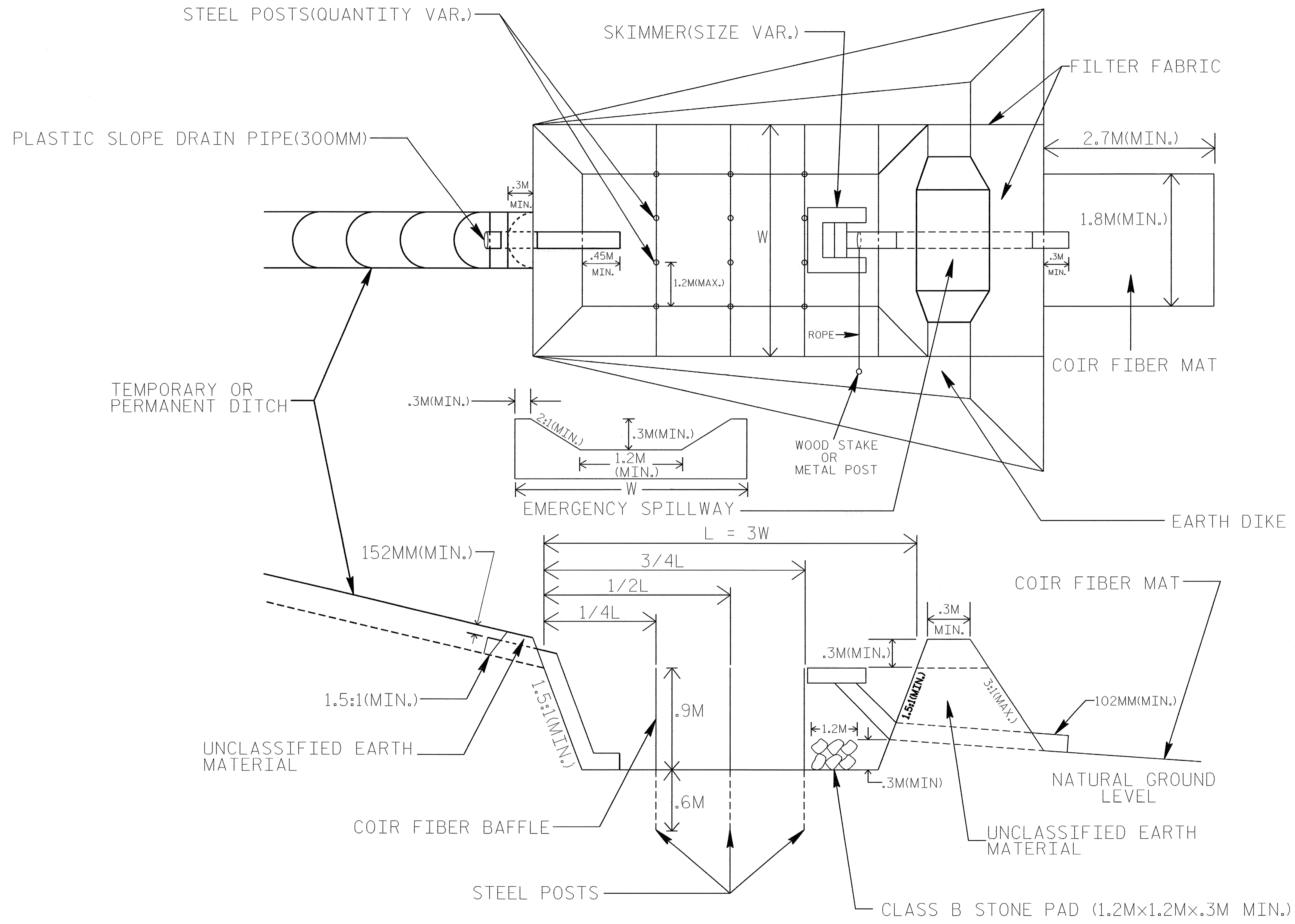


NOTE: INSTALL THREE(3) COIR FIBER BAFFLES IN SILT BASINS AND SEDIMENT DAMS AT DRAINAGE OUTLETS WITH A SPACING OF $\frac{1}{4}$ THE BASIN LENGTH. TWO(2) COIR FIBER BAFFLES CAN BE INSTALLED IN SILT BASINS AND DAMS LESS THAN 6 M IN LENGTH WITH A SPACING OF $\frac{1}{3}$ THE BASIN LENGTH.

BAFFLE MATERIAL SHALL BE SECURED TO THE BOTTOM AND SIDES OF BASIN USING 305MM LANDSCAPE STAPLES

SKIMMER BASIN WITH BAFFLES DETAIL

		PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-2B
ROADWAY DESIGN ENGINEER		HYDRAULICS ENGINEER	



COIR FIBER MAT ANCHOR OPTIONS

NOTES

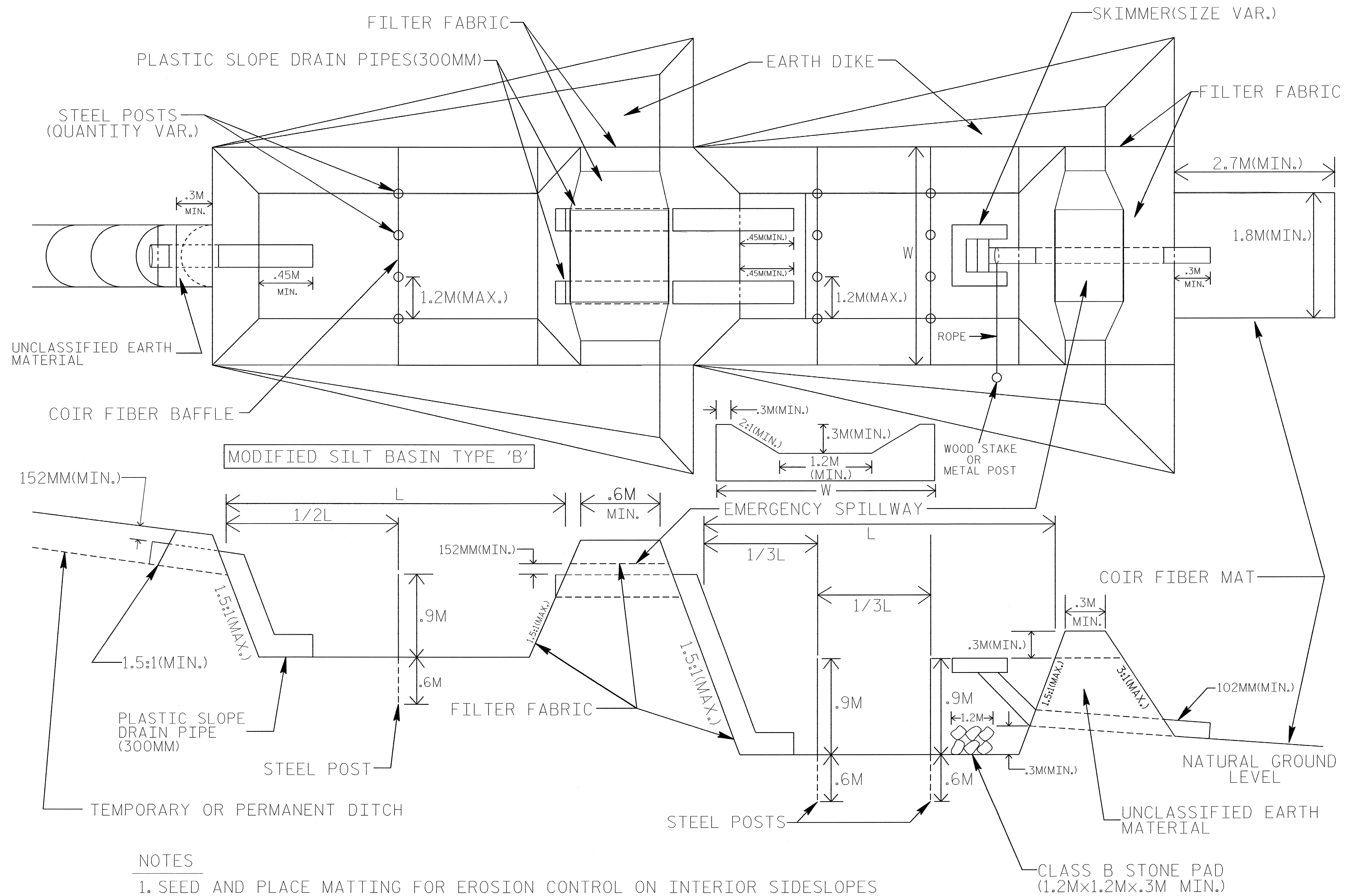
1. SEED AND PLACE MATTING FOR EROSION CONTROL ON INTERIOR SIDESLOPES.
2. LIMIT EARTH DIKE HEIGHT TO 1.5M.
3. MINIMUM BASIN WIDTH SHALL BE 3M.
4. DETERMINE EMERGENCY SPILLWAY LENGTH (M) USING $Q/0.074$, WHERE Q IS FLOW RATE (CMS) INTO BASIN.

NOT TO SCALE

TIERED SKIMMER BASIN DETAIL

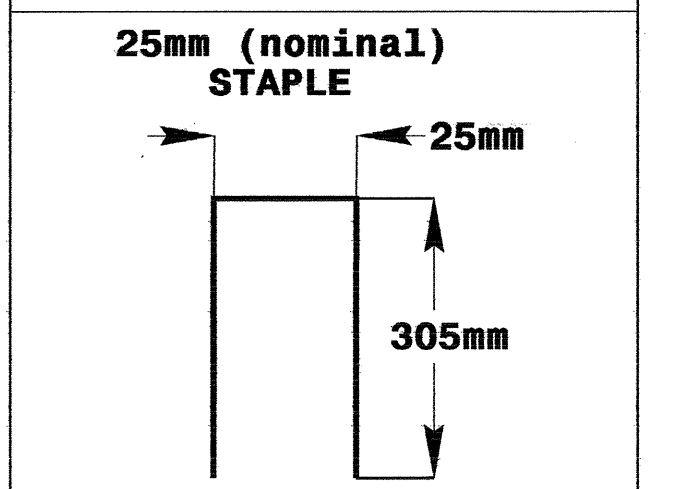
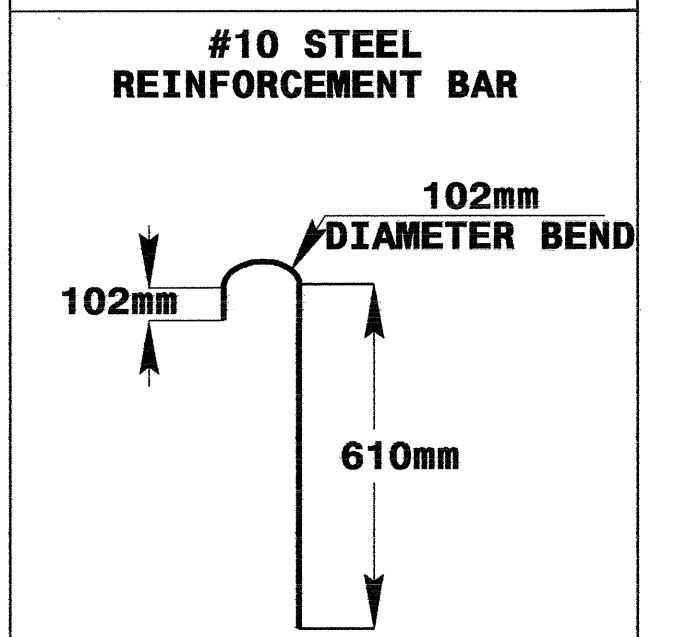
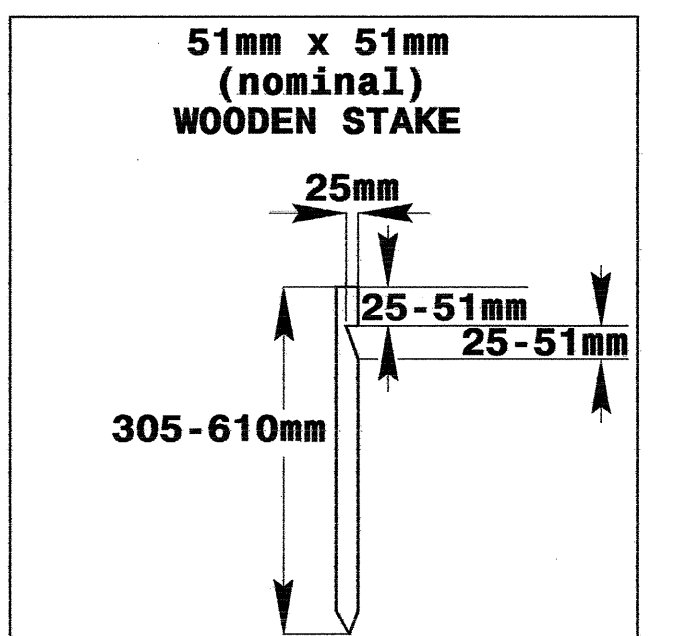


PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-2C
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



NOTES

1. SEED AND PLACE MATTING FOR EROSION CONTROL ON INTERIOR SIDESLOPES OF BASINS.
2. LIMIT HEIGHT OF EARTH DIKES TO 1.5M.
3. ADDITIONAL MODIFIED SILT BASINS TYPE 'B' MAY BE NEEDED DEPENDING ON SLOPE.
4. THE MINIMUM BASIN WIDTHS SHALL BE 3M.
5. DETERMINE EMERGENCY SPILLWAY LENGTHS (M) USING $Q/0.074$, WHERE Q IS FLOW RATE (CMS) INTO UPPER BASIN.



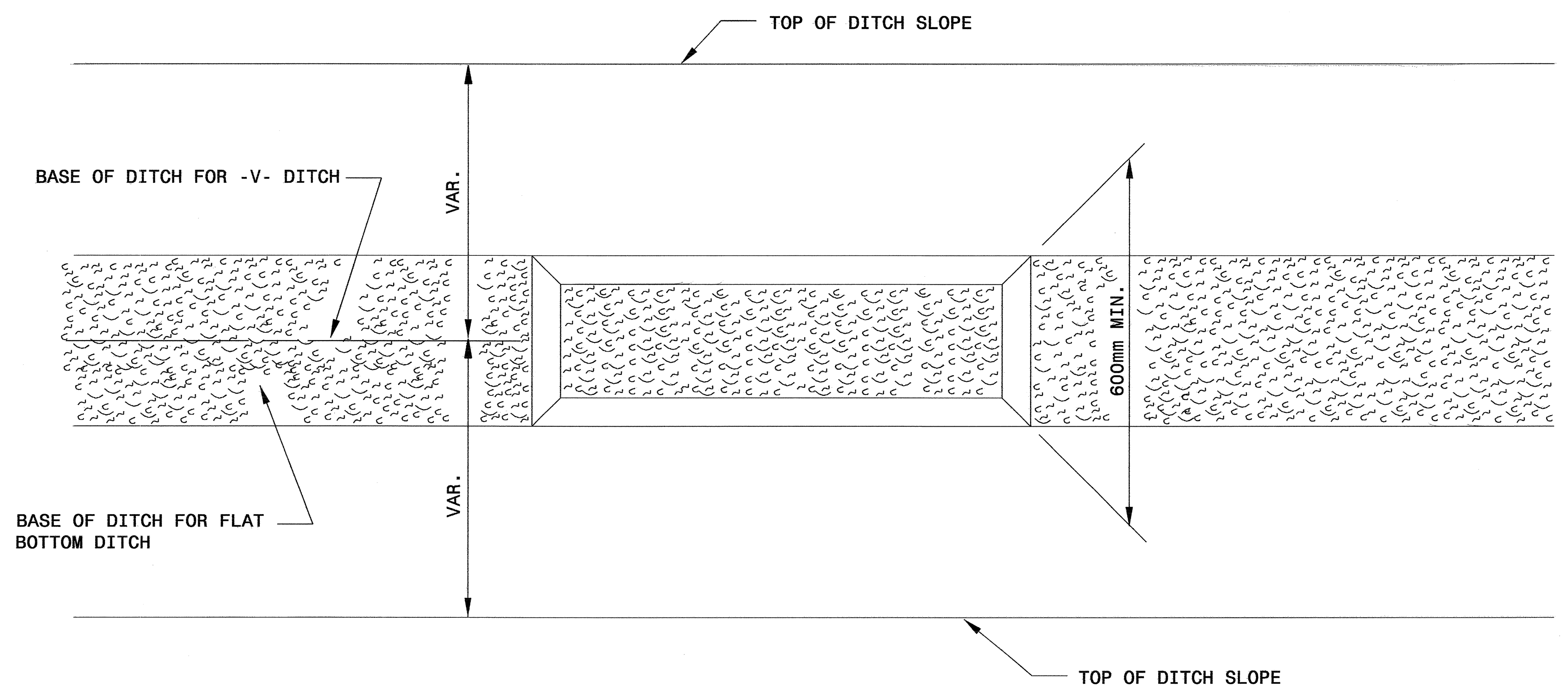
COIR FIBER MAT ANCHOR OPTIONS

NOT TO SCALE

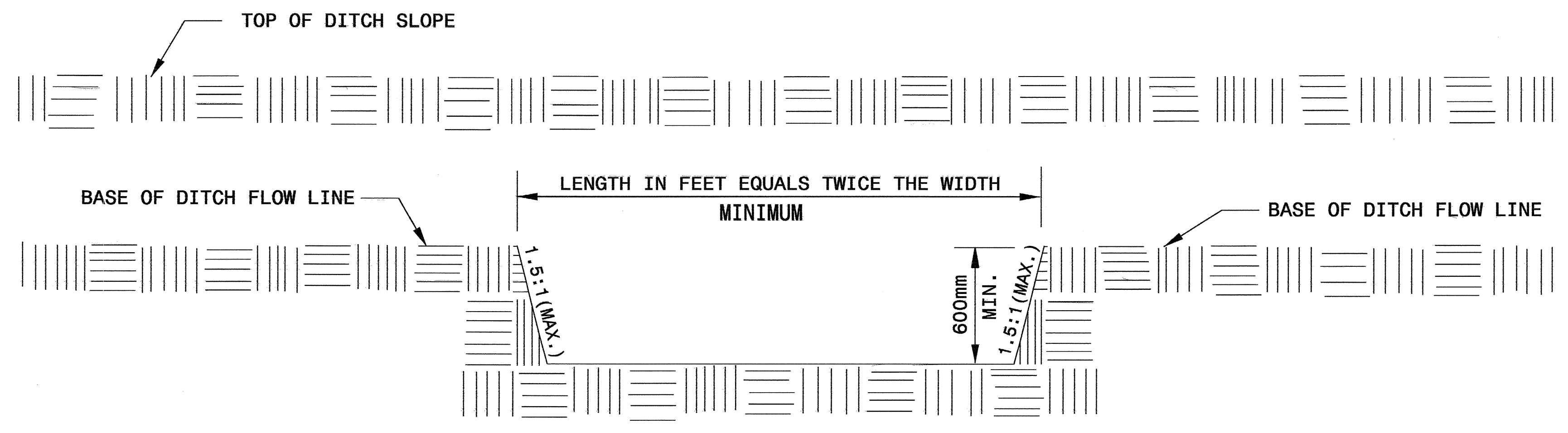


PROJECT REFERENCE NO.	SHEET NO.
X-0002B	EC-2D
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

SILT BASIN 'B' DETAIL



PLAN

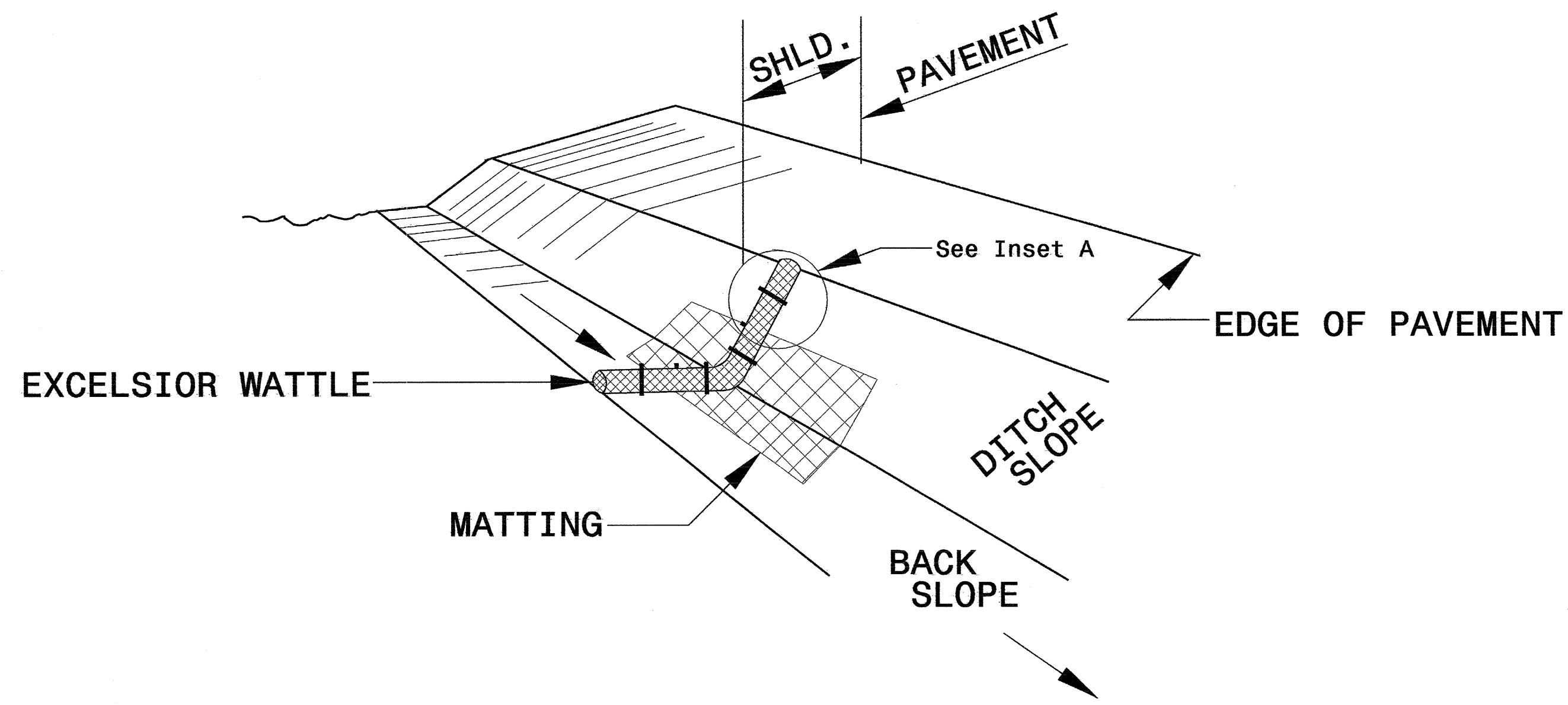


ELEVATION

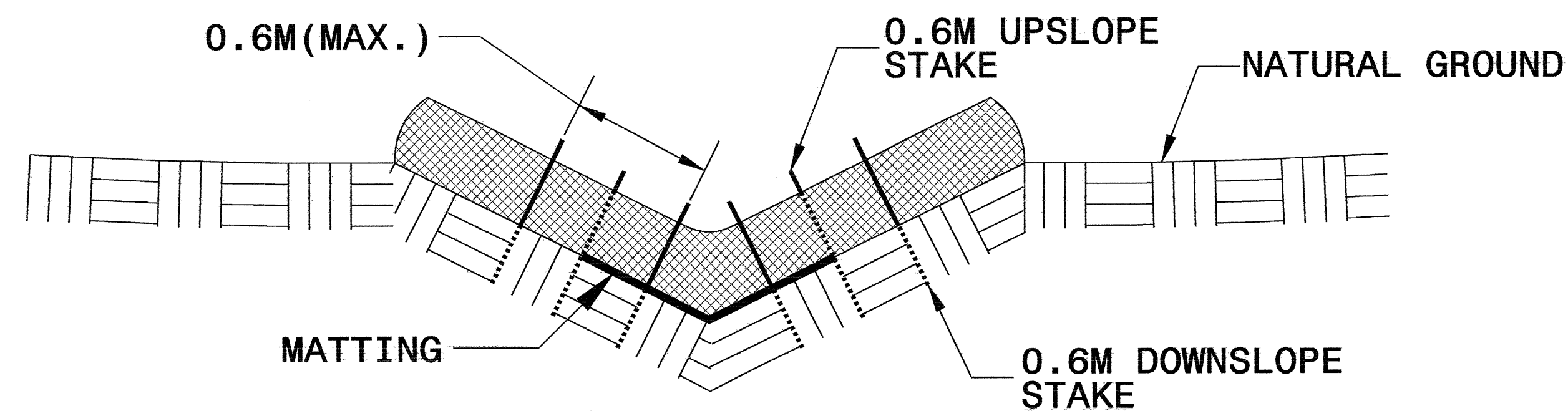
WATTLE WITH POLYACRYLAMIDE DETAIL



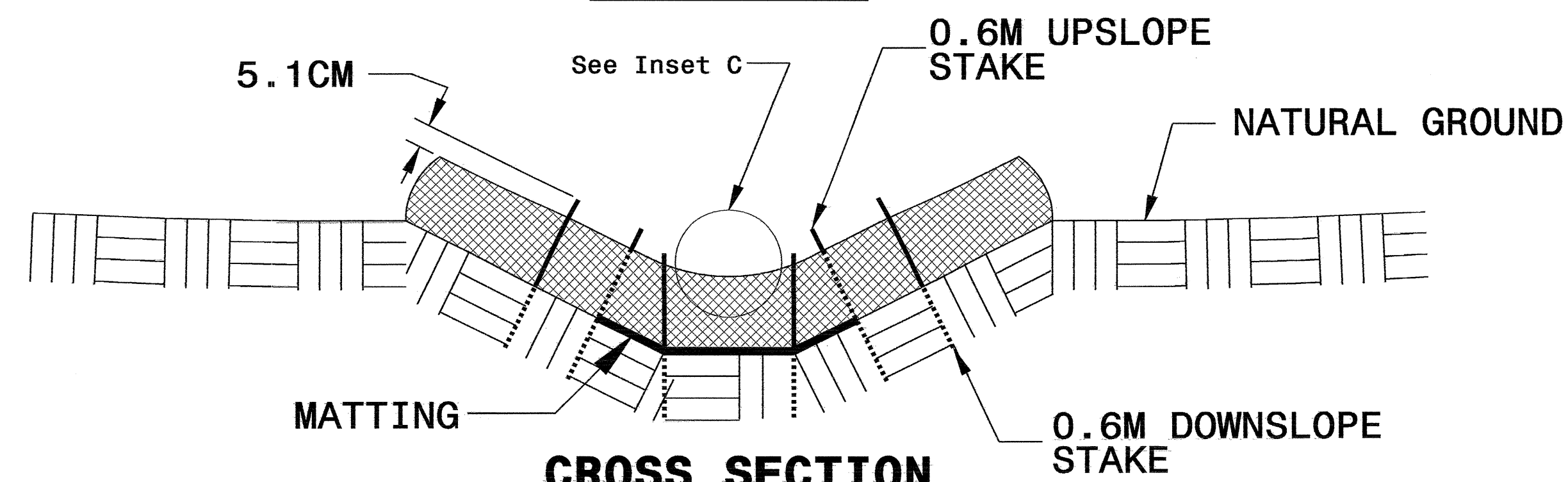
PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-2E
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



ISOMETRIC VIEW



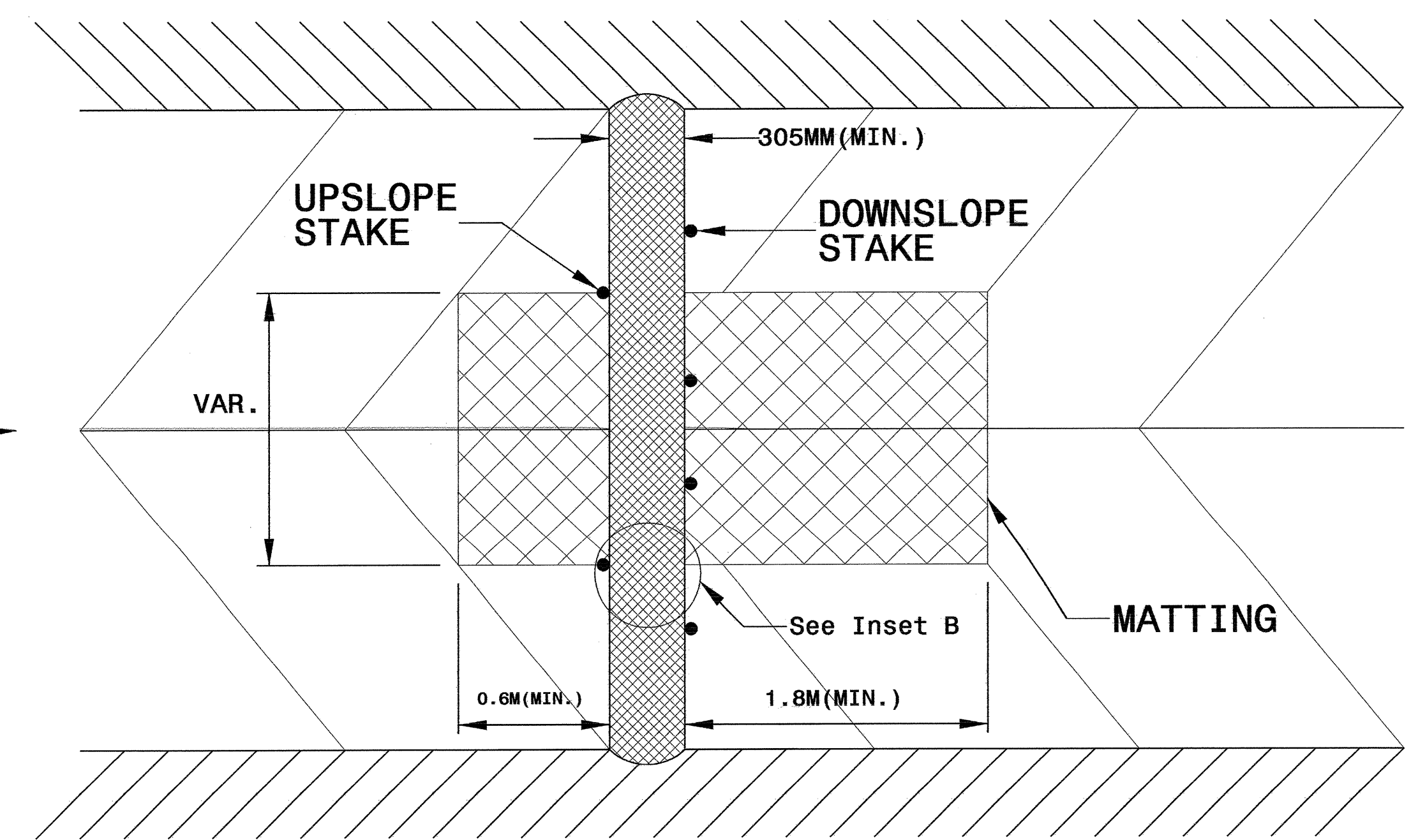
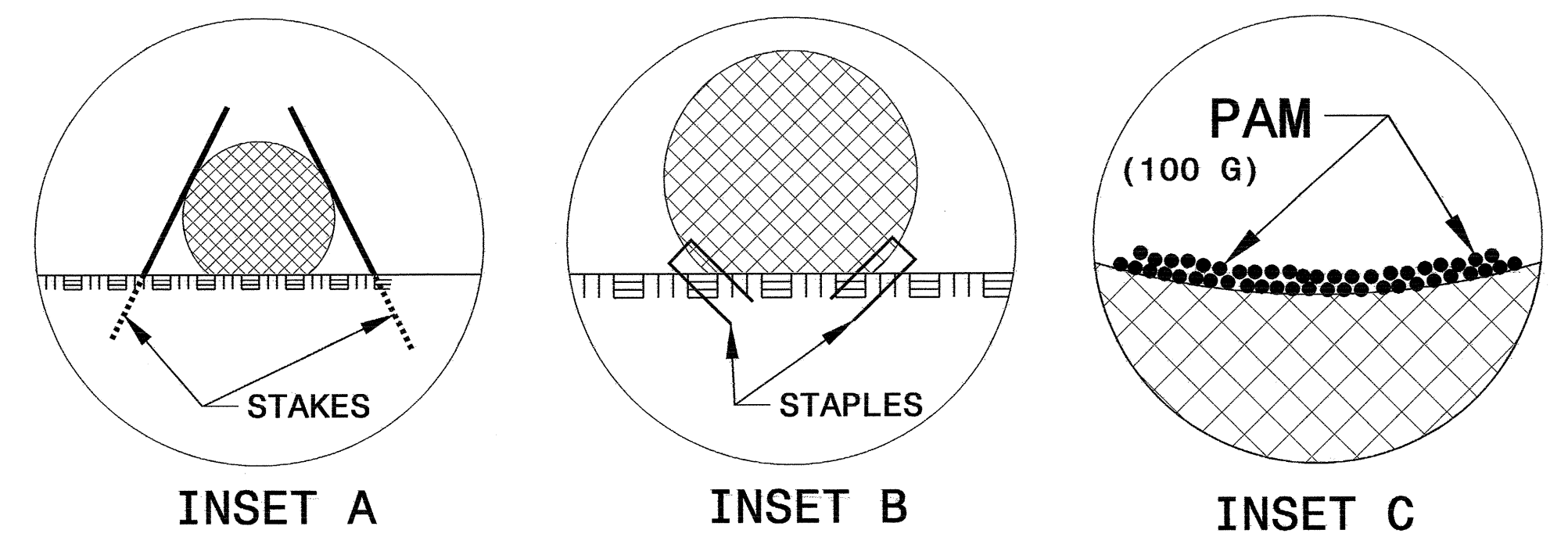
CROSS SECTION VEE DITCH



CROSS SECTION TRAPEZOIDAL DITCH

NOTES:

- USE MINIMUM 305 MM DIAMETER EXCELSIOR WATTLE.
- USE 0.6 M WOODEN STAKES WITH A 5.1 CM BY 5.1 CM CROSS SECTION.
- INSTALL A MINIMUM OF 2 UPSLOPE STAKES AND 4 DOWNSLOPE STAKES AT AN ANGLE TO WEDGE WATTLE TO BOTTOM OF DITCH.
- PROVIDE STAPLES MADE OF 3 MM DIAMETER STEEL WIRE FORMED INTO A U SHAPE NOT LESS THAN 305 MM IN LENGTH.
- INSTALL STAPLES APPROXIMATELY EVERY 0.3 LINEAR METER ON BOTH SIDES OF WATTLE AND AT EACH END TO SECURE IT TO THE SOIL.
- INSTALL MATTING IN ACCORDANCE WITH SECTION 1631 OF THE STANDARD SPECIFICATIONS.
- INITIALLY APPLY 100 GRAMS OF ANIONIC OR NEUTRALLY CHARGED POLYACRYLAMIDE (PAM) OVER WATTLE WHERE WATER WILL FLOW AND AFTER EVERY RAINFALL EVENT THAT IS EQUAL TO OR EXCEEDS 6 MM.

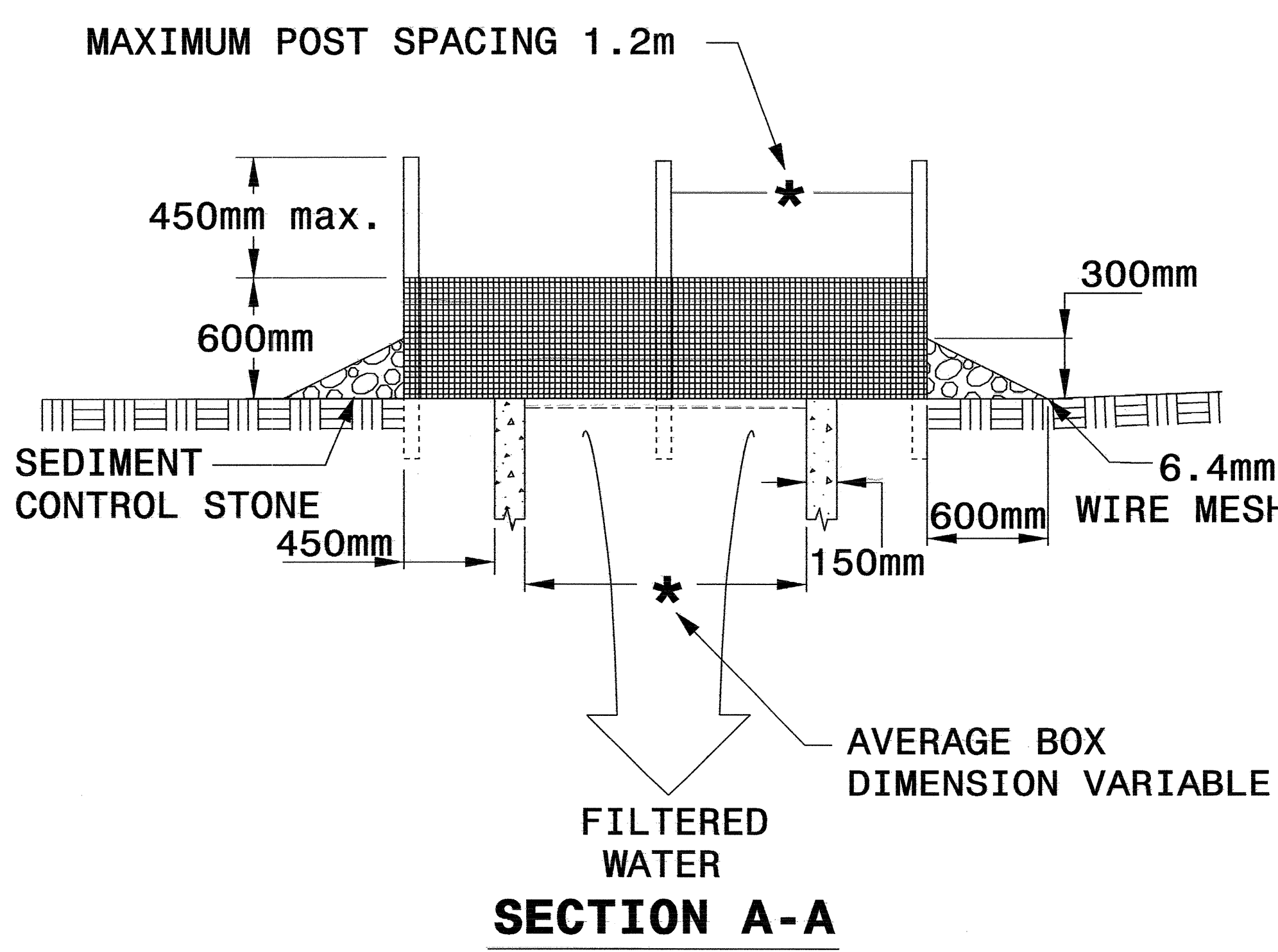
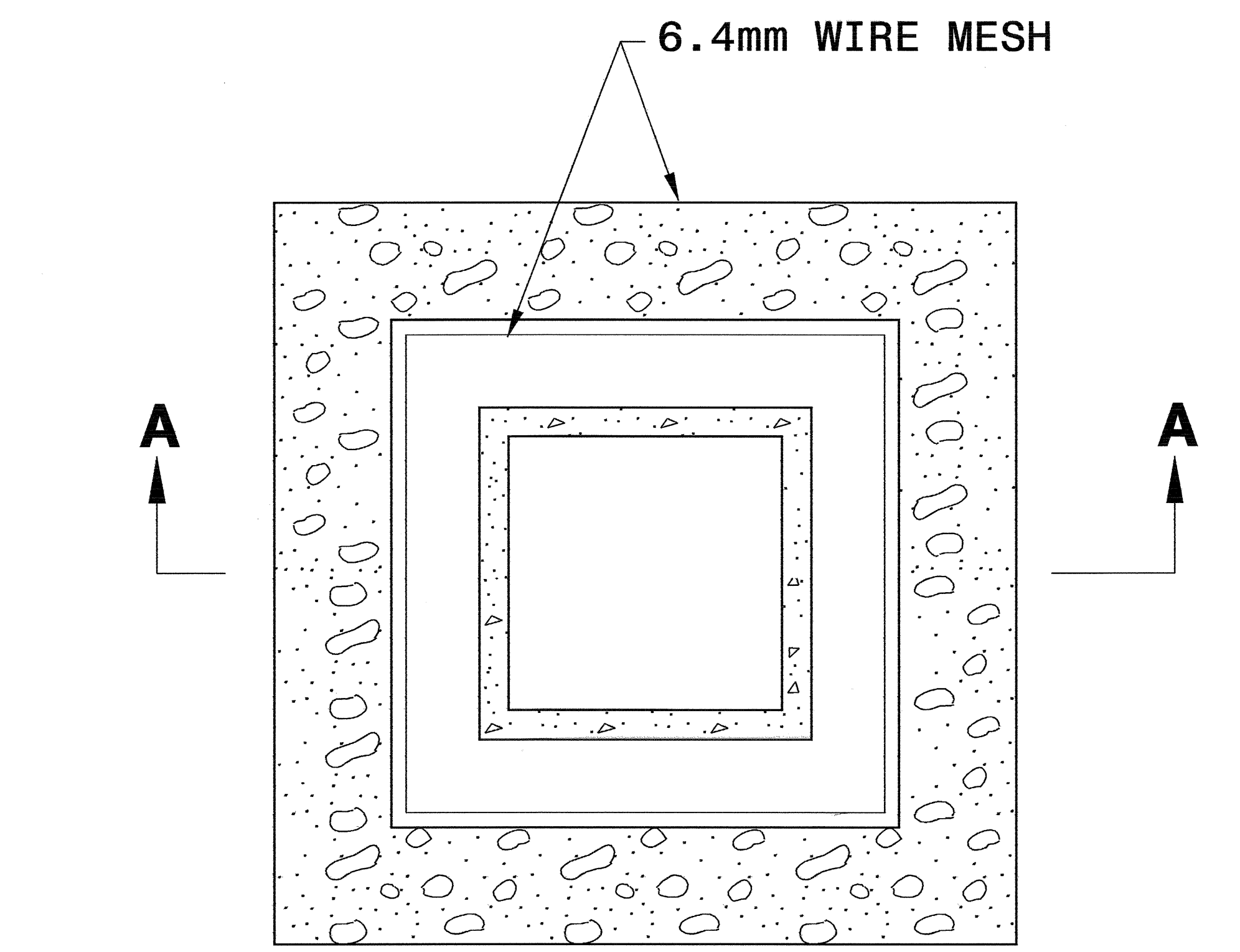


TOP VIEW



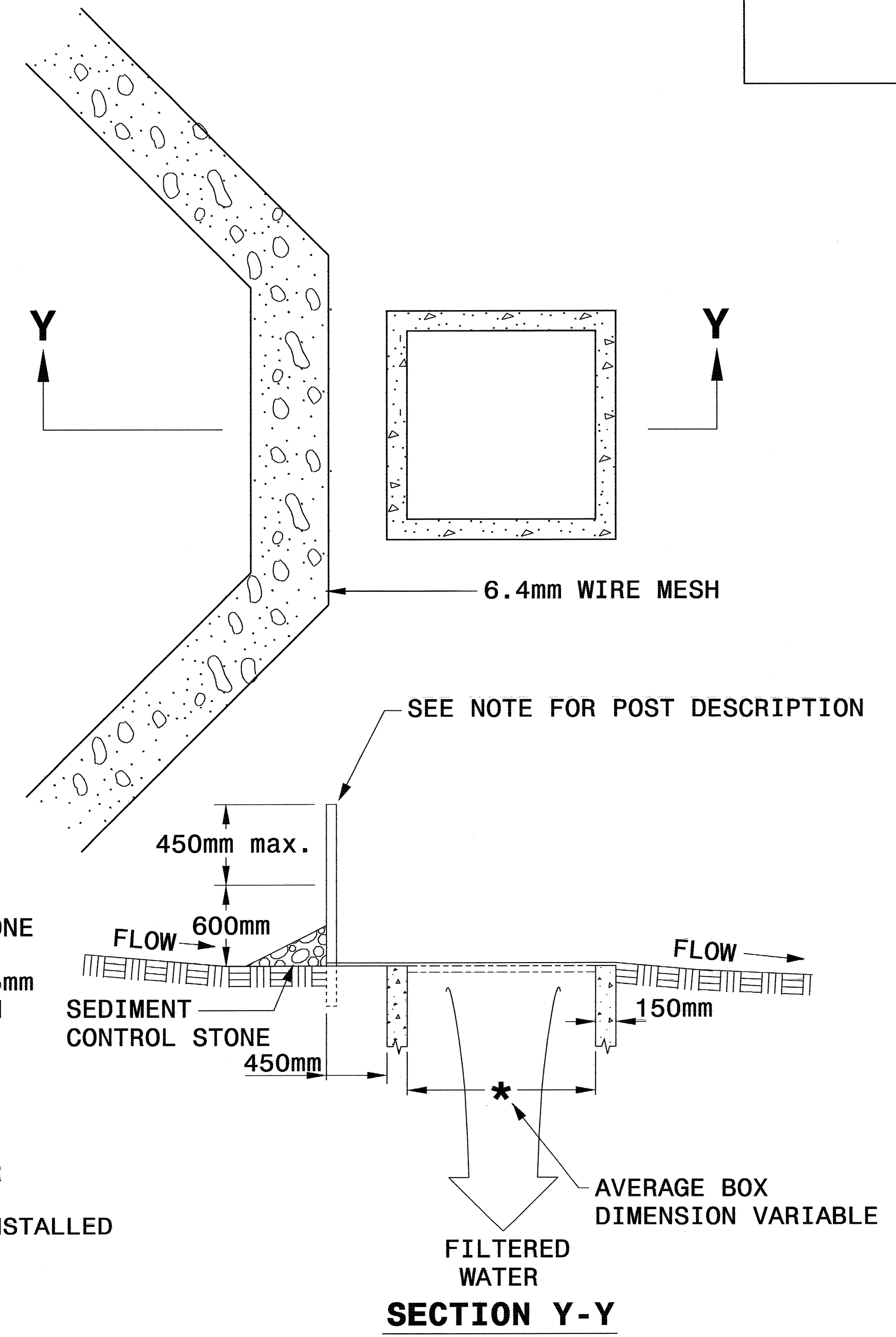
PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-2F
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

ROCK INLET SEDIMENT TRAP TYPE 'C' DETAIL



MULTI-DIRECTIONAL FLOW

NOTE
 USE NO. 5 OR NO. 57 STONE FOR SEDIMENT CONTROL.
 USE HARDWARE CLOTH 0.65mm WIRE MESH WITH 6.4mm MESH OPENINGS.
 PLACE TOP OF WIRE MESH A MINIMUM OF 300mm BELOW THE SHOULDER OR ANY DIVERSION POINT.
 INSTALL WIRE MESH UNDER SEDIMENT CONTROL STONE.
 USE 1.5m STEEL POST, INSTALLED 450mm DEEP MINIMUM, AND OF THE SELF-FASTENER ANGLE STEEL TYPE.
 SPACE POST A MAXIMUM OF 1.2m.



SINGLE-DIRECTIONAL FLOW



PROJECT REFERENCE NO. <i>X-0002B</i>	SHEET NO. <i>EC-26</i>
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

SPECIAL SEDIMENT CONTROL FENCE DETAIL

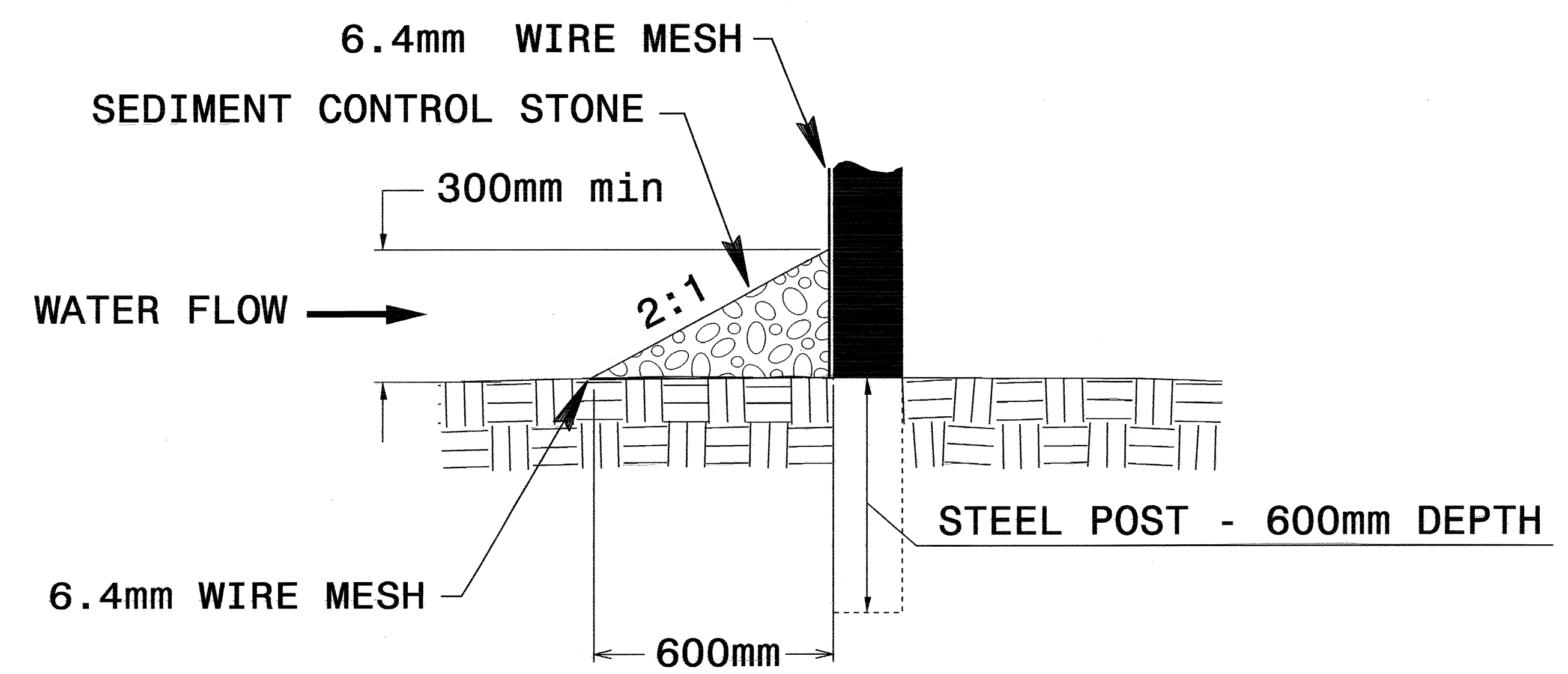
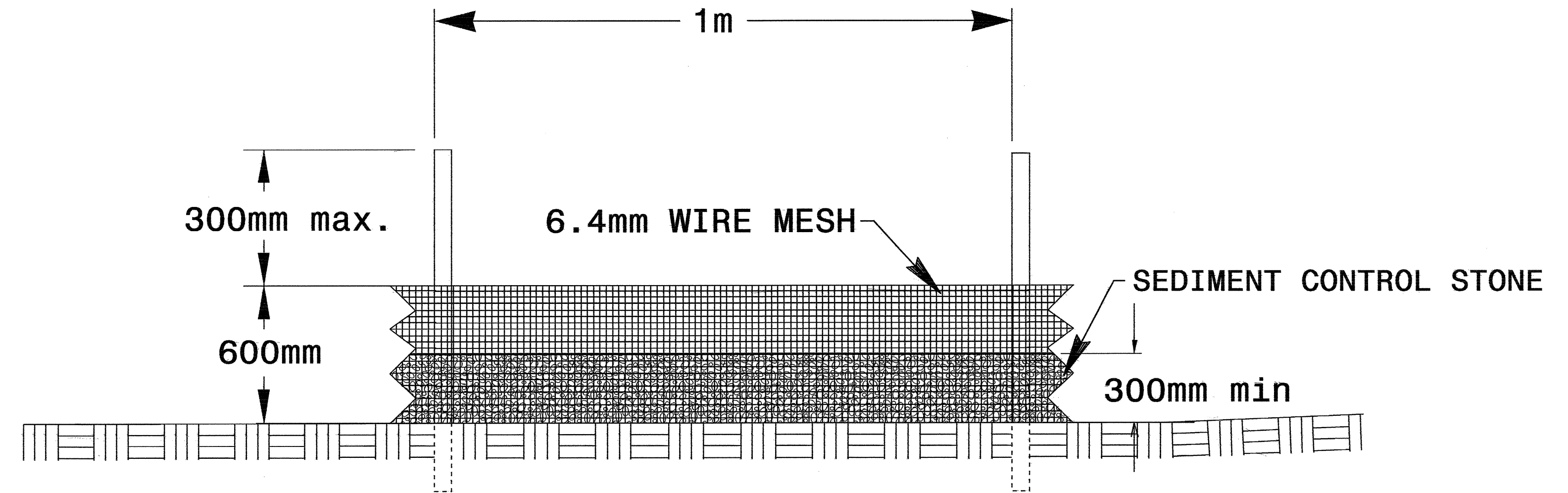
GENERAL NOTES:

USE NO. 5 OR NO. 57 STONE FOR SEDIMENT CONTROL.

USE 0.65mm HARDWARE CLOTH WIRE MESH WITH 6.4 mm MESH OPENINGS.

INSTALL 1.5m SELF FASTENER ANGLE STEEL POST 600mm DEEP MINIMUM.

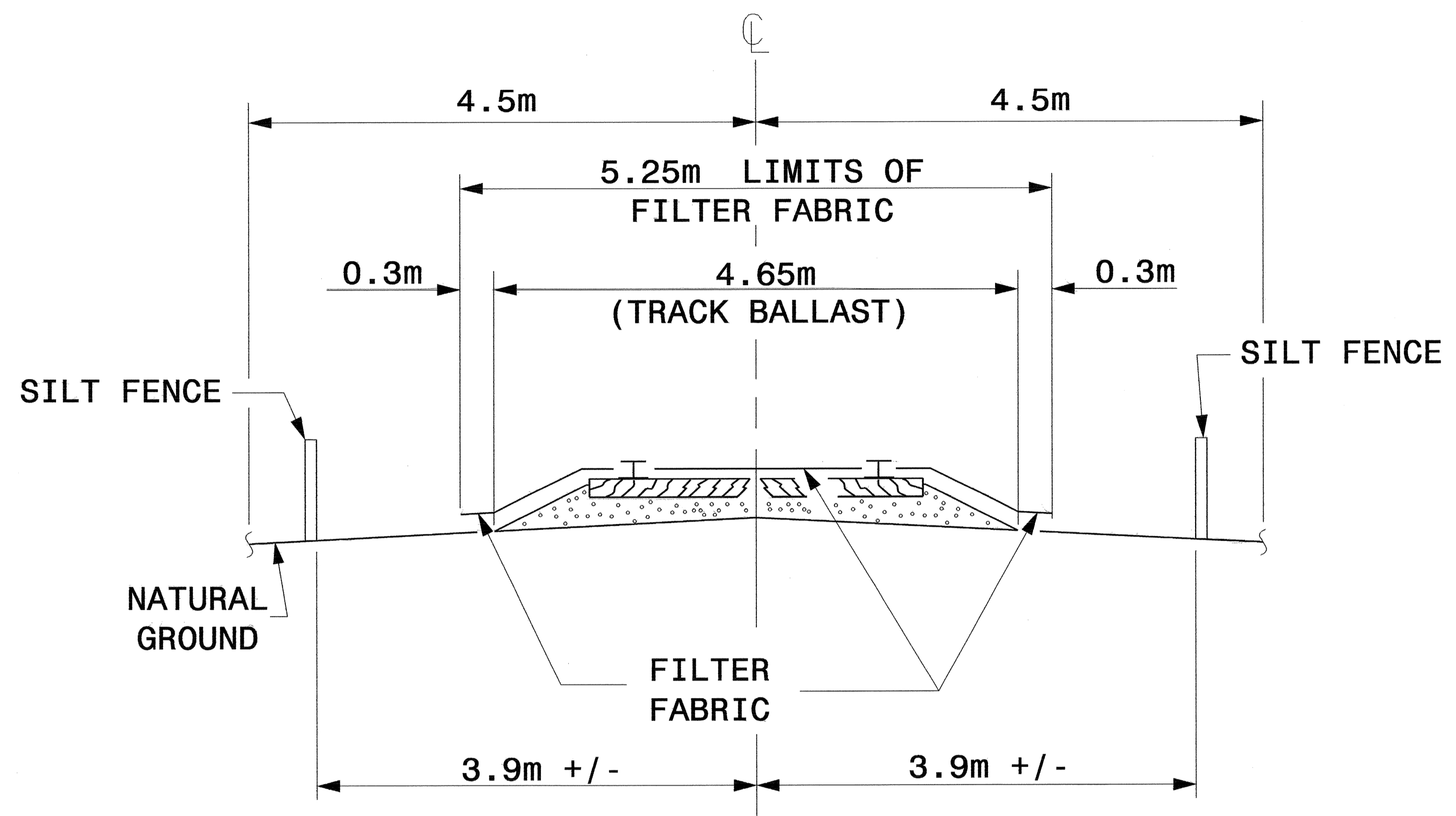
SPACE POST A MAXIMUM OF 1m.





PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-2H
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

RAILROAD EROSION CONTROL DETAIL



NOTES

INSTALL RAILROAD EROSION CONTROL MEASURES PRIOR TO PERFORMING ANY WORK IN THE RAILROAD RIGHT-OF-WAY.

ADDITIONAL EROSION CONTROL MEASURES FOR PROTECTION OF RAILROAD DITCHES MAY BE REQUIRED AS DIRECTED BY THE ENGINEER.

MAKE NO SEPARATE PAYMENT FOR RAILROAD EROSION CONTROL MEASURES.

EXTEND LIMITS OF SILT FENCE AND FILTER FABRIC PARALLEL TO RAILROAD A MINIMUM OF 3m OUTSIDE EDGE OF SUPERSTRUCTURE OR TOE OF SLOPE ON CONSTRUCTION. A GREATER LENGTH OF SILT FENCE OR FILTER FABRIC MAY BE REQUIRED IF SO DIRECTED BY THE ENGINEER.

NAIL FILTER FABRIC TO TIMBER RAIL TIES WITH PRIME SOURCE "GRIP CAP" OR EQUIVALENT. SECURE FILTER FABRIC ON SHOULDER AS DIRECTED BY THE ENGINEER AND RAILROAD.

NOTE: UTILIZE SKIMMER BASIN AS STILLING BASIN WHERE APPLICABLE.

NOTE: PLACE TEMPORARY ROCK SEDIMENT DAMS TYPE-B AND TEMPORARY ROCK SILT CHECKS TYPE-A AT DRAINAGE OUTLETS.

CLEARING AND GRUBBING EROSION CONTROL FOR CONSTRUCTION SHEET 07

METRIC

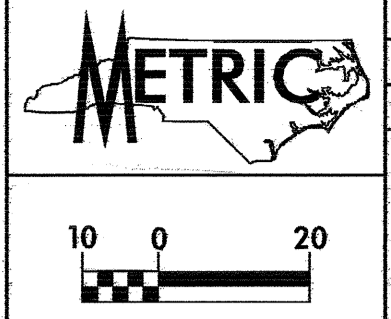
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CONST. REV.

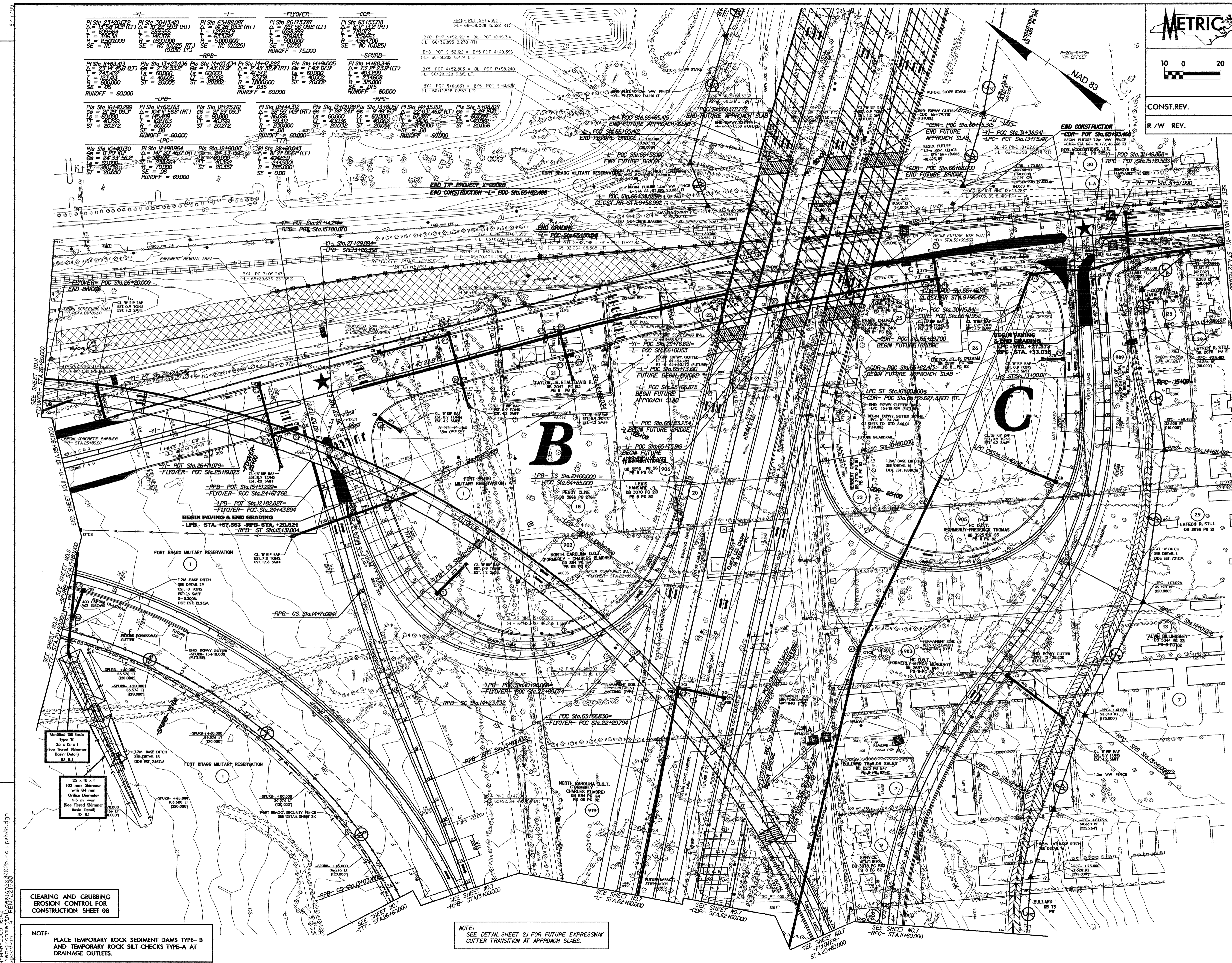
R/W REV.

PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-07/CONST.07
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

Pile Sta 12+94.904 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 14+38.835 $\Delta = 17.17$ $L = 246.34$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 16+68.249 $\Delta = 9.5$ $L = 1000.000$ $ST = 20.001$ $SE = 0.025$ $RUNOFF = 60.000$	Pile Sta 18+13.787 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 20+58.292 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 22+02.795 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 23+47.298 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 24+91.801 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 26+36.304 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 27+80.807 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 29+25.310 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 30+69.813 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 32+14.316 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 33+58.819 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 35+03.322 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 36+47.825 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 37+92.328 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 39+36.831 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 40+81.334 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 42+25.837 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 43+70.340 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 45+14.843 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 46+59.346 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 48+03.849 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 49+48.352 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 50+92.855 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 52+37.358 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 53+81.861 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 55+26.364 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 56+70.867 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 58+15.370 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 59+59.873 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 61+04.376 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 62+48.879 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 64+93.382 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 66+37.885 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 67+82.388 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 69+26.891 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 70+71.394 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 72+15.897 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 73+60.400 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 75+04.903 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 76+49.406 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 77+93.909 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 79+38.412 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 80+82.915 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 82+27.418 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 83+71.921 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 85+16.424 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 86+60.927 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 88+05.430 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 89+49.933 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 90+94.436 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 92+38.939 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 93+83.442 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 95+27.945 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 96+72.448 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 98+16.951 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 99+61.454 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 101+05.957 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 102+50.460 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 103+94.963 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 105+39.466 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 106+83.969 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 108+28.472 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 109+72.975 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 111+17.478 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 112+61.981 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 114+06.484 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 115+50.987 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 116+95.490 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 118+39.993 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 119+84.496 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 121+28.999 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 122+73.502 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 124+18.005 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 125+62.508 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 127+07.011 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 128+51.514 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 130+96.017 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 132+40.520 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 133+85.023 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 135+29.526 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 136+74.029 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 138+18.532 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 139+63.035 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 141+07.538 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 142+52.041 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 143+96.544 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 145+41.047 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 146+85.550 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 148+30.053 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 149+74.556 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 151+19.059 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 152+63.562 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 154+08.065 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 155+52.568 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 156+97.071 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 158+41.574 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 159+86.077 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 161+30.580 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 162+75.083 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 164+19.586 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 165+64.089 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 167+08.592 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 168+53.095 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 170+97.598 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 172+42.101 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 173+86.604 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 175+31.107 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 176+75.610 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 178+20.113 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 179+64.616 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 181+09.119 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 182+53.622 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 184+98.125 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 186+42.628 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 187+87.131 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 189+31.634 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 190+76.137 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC (0.025)$	Pile Sta 192+20.640 $\Delta = 12.52$ $L = 64.182$ $R = 1000.000$ $SE = NC 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---	---	--	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	-----------------------------------



PROJECT REFERENCE NO.	SHEET NO.
X-0002B	EC-08/CONST.08
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
CONST. REV.	
R/W REV.	



REVISIONS

CLEARING AND GRUBBING
EROSION CONTROL FOR
CONSTRUCTION SHEET 08

NOTE:
PLACE TEMPORARY ROCK SEDIMENT DAMS TYPE-B
AND TEMPORARY ROCK SILT CHECKS TYPE-A AT
DRAINAGE OUTLETS.

NOTE:
SEE DETAIL SHEET 2J FOR FUTURE EXPRESSWAY
GUTTER TRANSITION AT APPROACH SLABS.

FUTURE GRADING AND PAVING

04-MAR-2009 16:42
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NOTE:
PLACE TEMPORARY ROCK SEDIMENT DAMS TYPE-B AND TEMPORARY ROCK SILT CHECKS TYPE-A AT DRAINAGE OUTLETS.

CLEARING AND GRUBBING EROSION CONTROL FOR CONSTRUCTION SHEET 11

-FLYOVER-			-SPURB-		
PI Sta 26+73.787	PIs Sta 28+17.847	PIs Sta 29+07.836	PI Sta 30+25.909	PI Sta 14+88.346	PIs Sta 16+77.054
$\Delta = 125^{\circ} 56' 09.8" (LT)$	$\Delta = 4^{\circ} 17' 49.9"$	$\Delta = 2^{\circ} 08' 54.9"$	$\Delta = 13^{\circ} 58' 42.8" (RT)$	$\Delta = 73^{\circ} 21' 23.9" (LT)$	$\Delta = 5^{\circ} 27' 24.3"$
$L = 1098.999$	$Ls = 75.000$	$Ls = 60.000$	$L = 195.178$	$L = 403.299$	$68 Ls = 60.000$
$T = 979.953$	$LT = 50.015$	$LT = 40.003$	$T = 98.076$	$T = 234.608$	$68 LT = 40.019$
$R = 500.000$	$ST = 25.013$	$ST = 20.003$	$R = 800.000$	$R = 315.000$	$ST = 20.017$
$SE = 0.05$			$SE = 0.04$	$SE = 0.075$	
$RUNOFF = 75.000$			$RUNOFF = 60.000$	$RUNOFF = 60.000$	

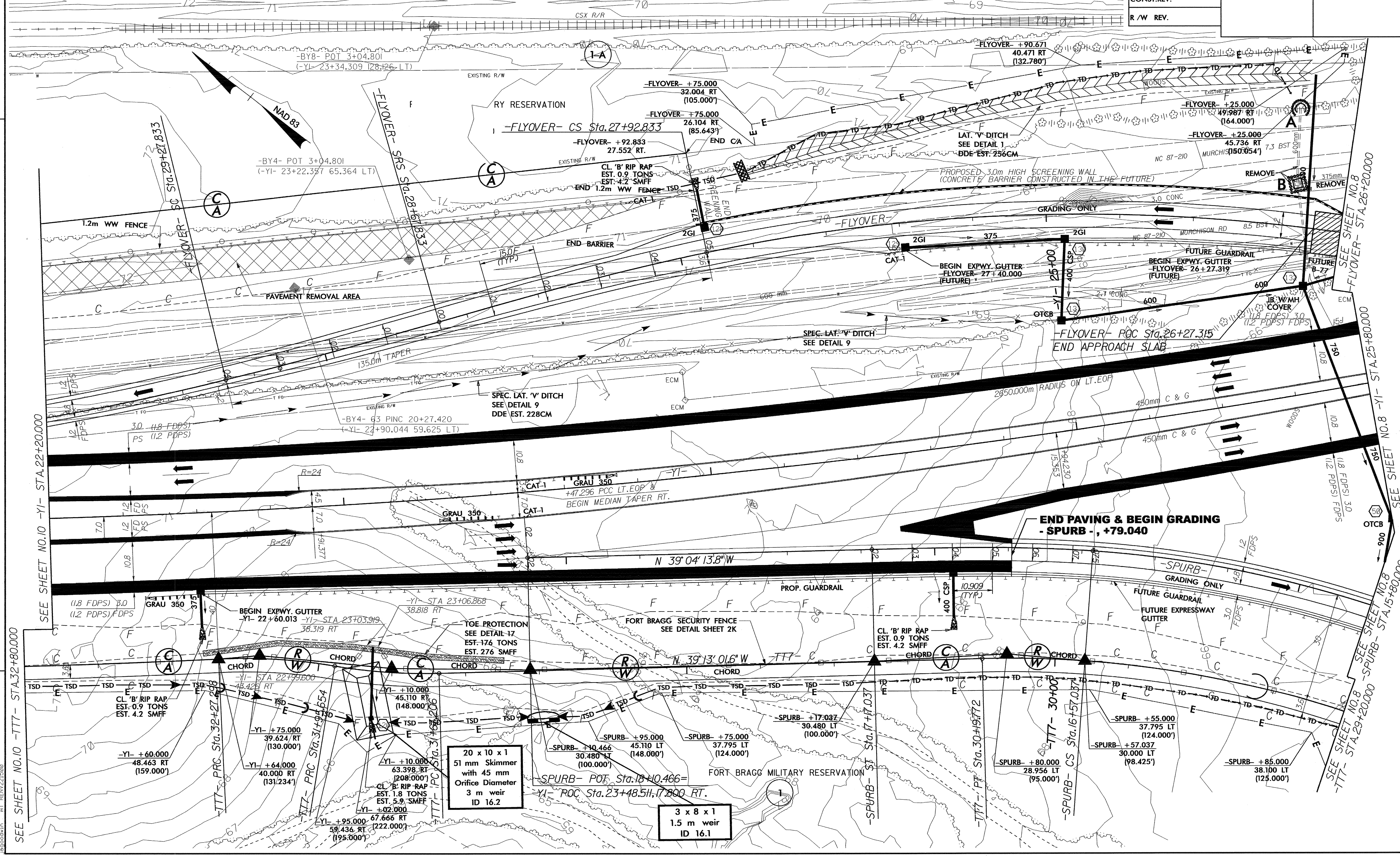
METRIC

5 0 10

CONST. REV.

R/W REV.

PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-II/CONST.II
R/W SHEET NO.	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	



REVISIONS

SEE SHEET NO. 10 -YI- STA. 22+20.000

SEE SHEET NO. 10 -TT7- STA. 32+80.000

SEE SHEET NO. 8 -FLYOVER- STA. 26+20.000

SEE SHEET NO. 8 -SPURB- STA. 15+80.000

20 x 10 x 1
51 mm Skimmer
with 45 mm
Orifice Diameter
3 m weir
ID 16.2

3 x 8 x 1
1.5 m weir
ID 16.1

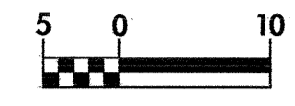
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NOTE:
PLACE TEMPORARY ROCK SEDIMENT DAMS TYPE-B
AND TEMPORARY ROCK SILT CHECKS TYPE-A AT
DRAINAGE OUTLETS.

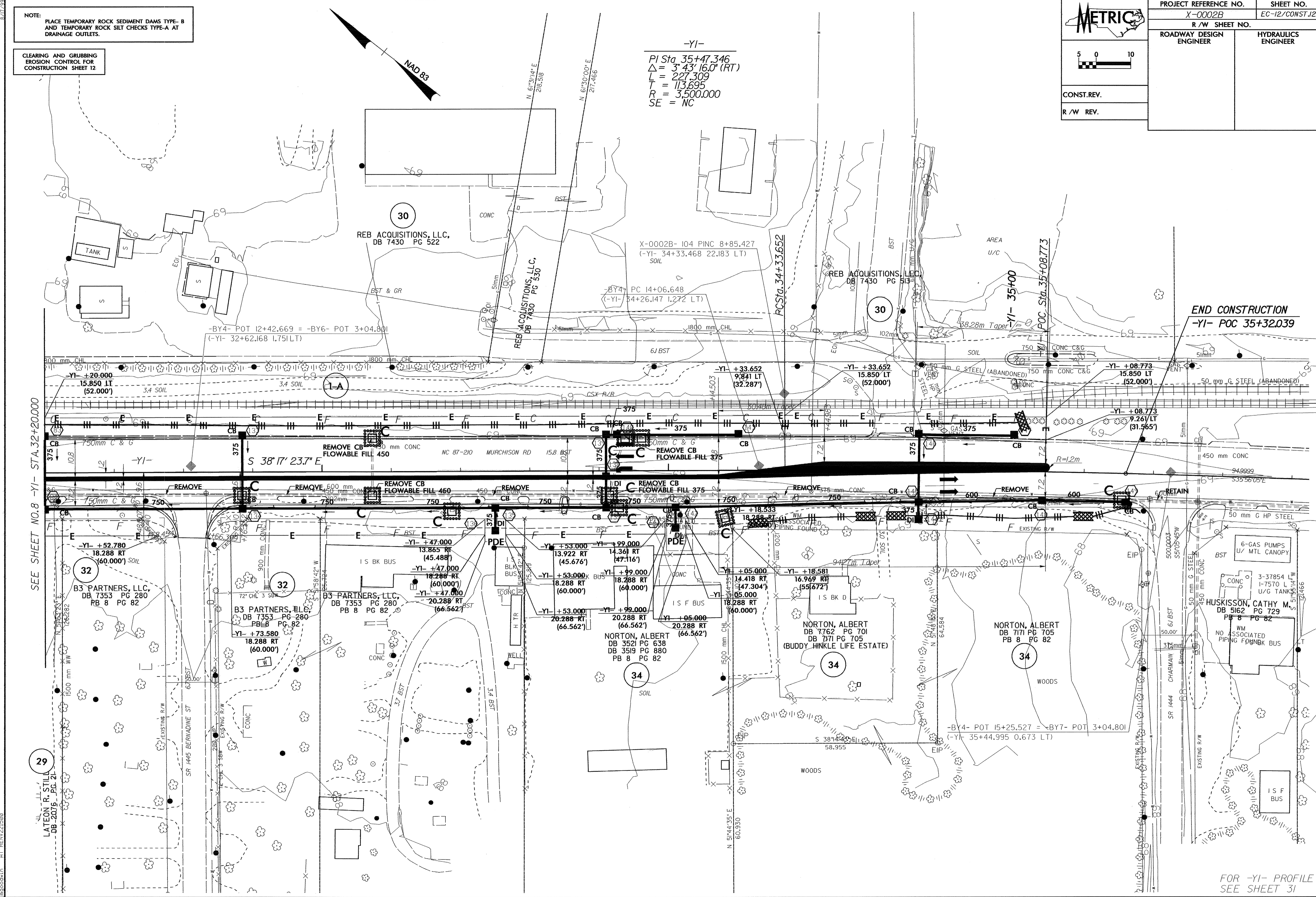
CLEARING AND GRUBBING
EROSION CONTROL FOR
CONSTRUCTION SHEET 12



PROJECT REFERENCE NO. X-0002B	SHEET NO. EG-12/CONST.12
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
CONST. REV.	
R/W REV.	



-Y1-
PI Sta. 35+47.346
 $\Delta = 3^{\circ}43'16.0''$ (RT)
L = 227.309
T = 113.695
R = 3,500.000
SE = NC



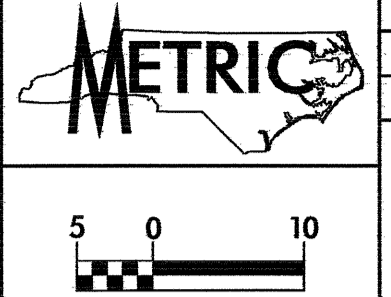
SEE SHEET NO. 8 -Y1- STA. 32+20.000

29
LATEON R. STILL
DB 2076 PG 21

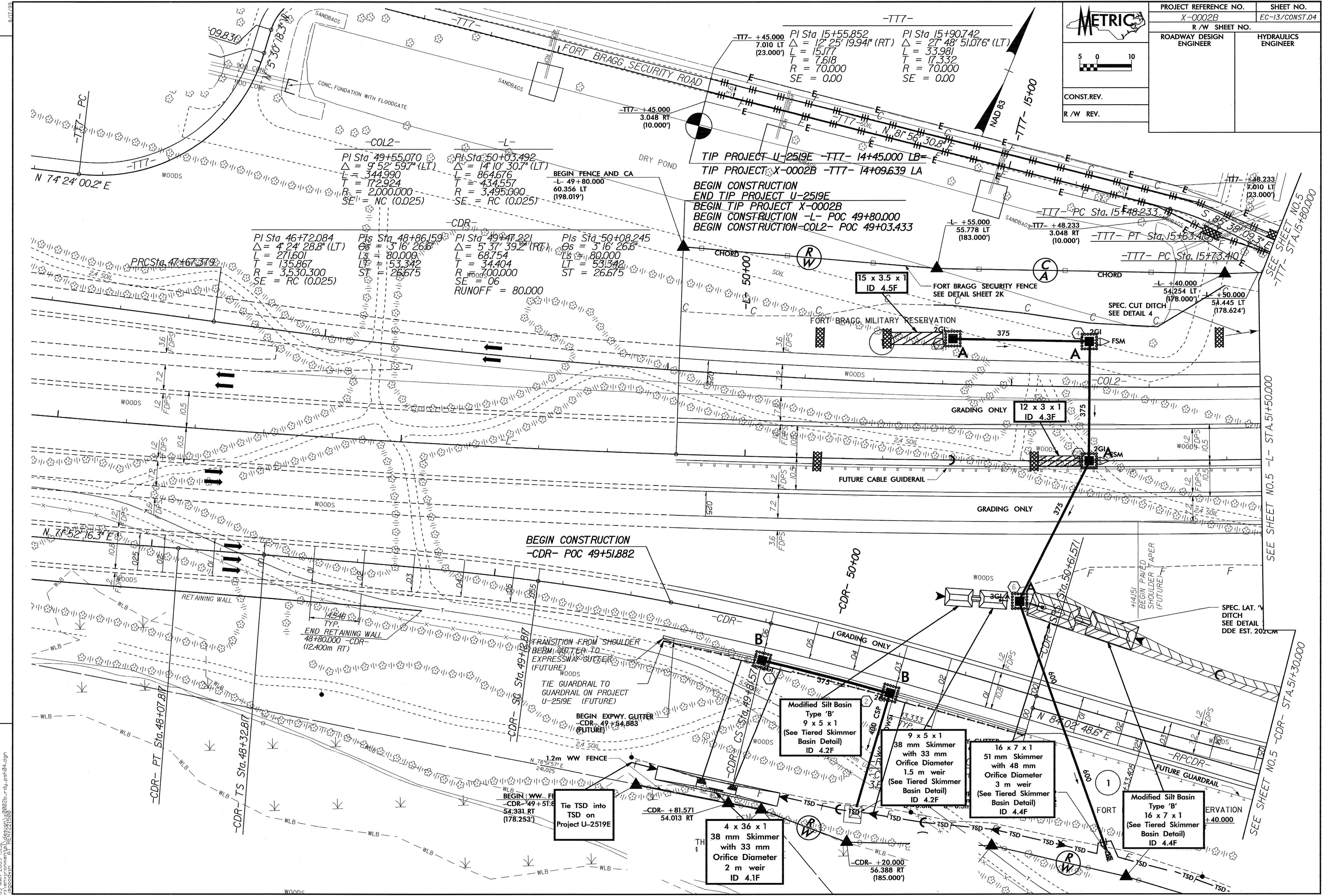
END CONSTRUCTION
-Y1- POC 35+32.039

FOR -Y1- PROFILE
SEE SHEET 31

03-MAR-2009 14:15
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 Association



PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-13/CONST.04
R/W SHEET NO.	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	
CONST. REV.	
R/W REV.	



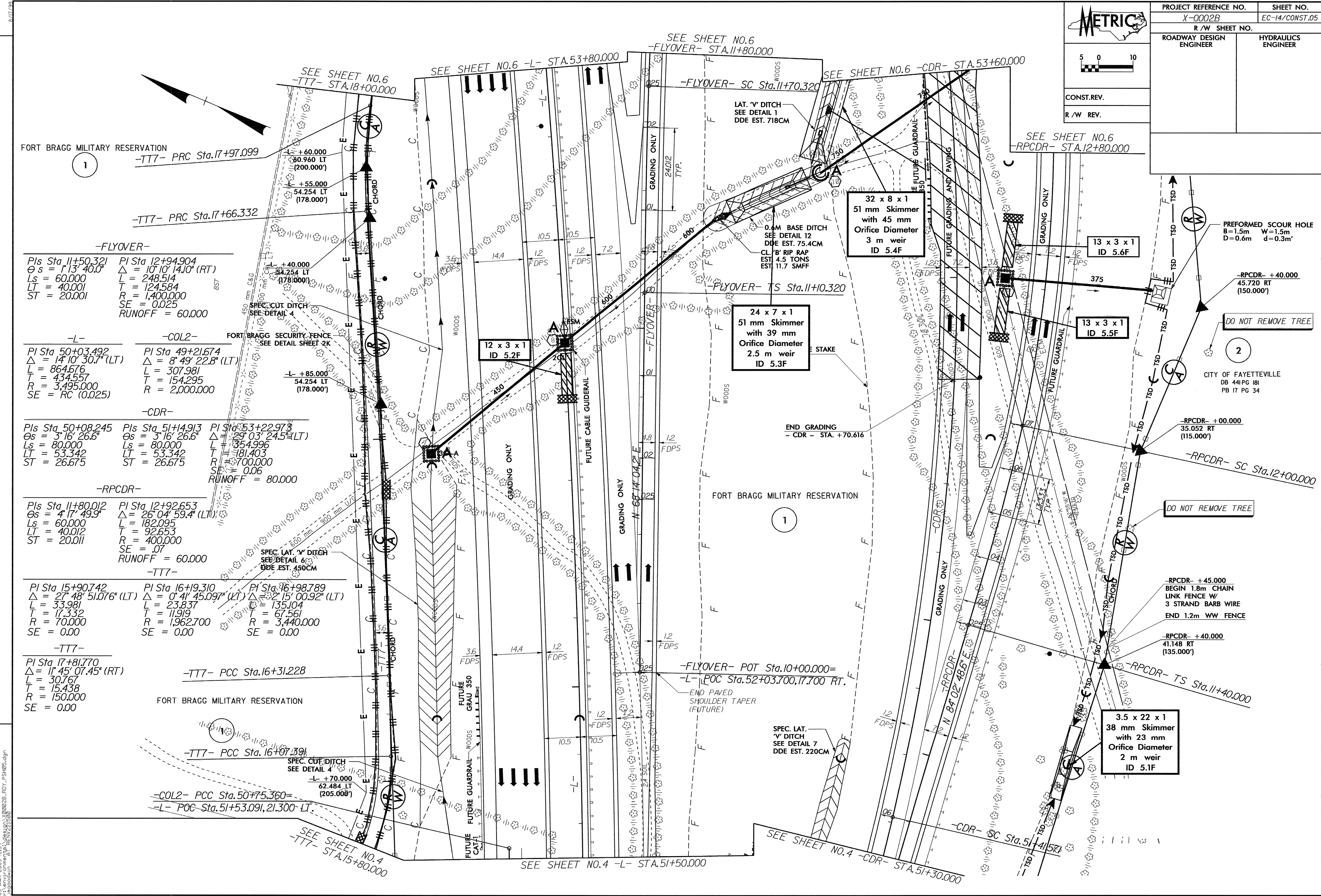
REVISIONS

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METRIC

CONST. REV.
R/W REV.

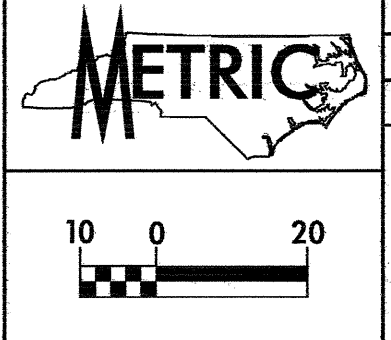
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R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER



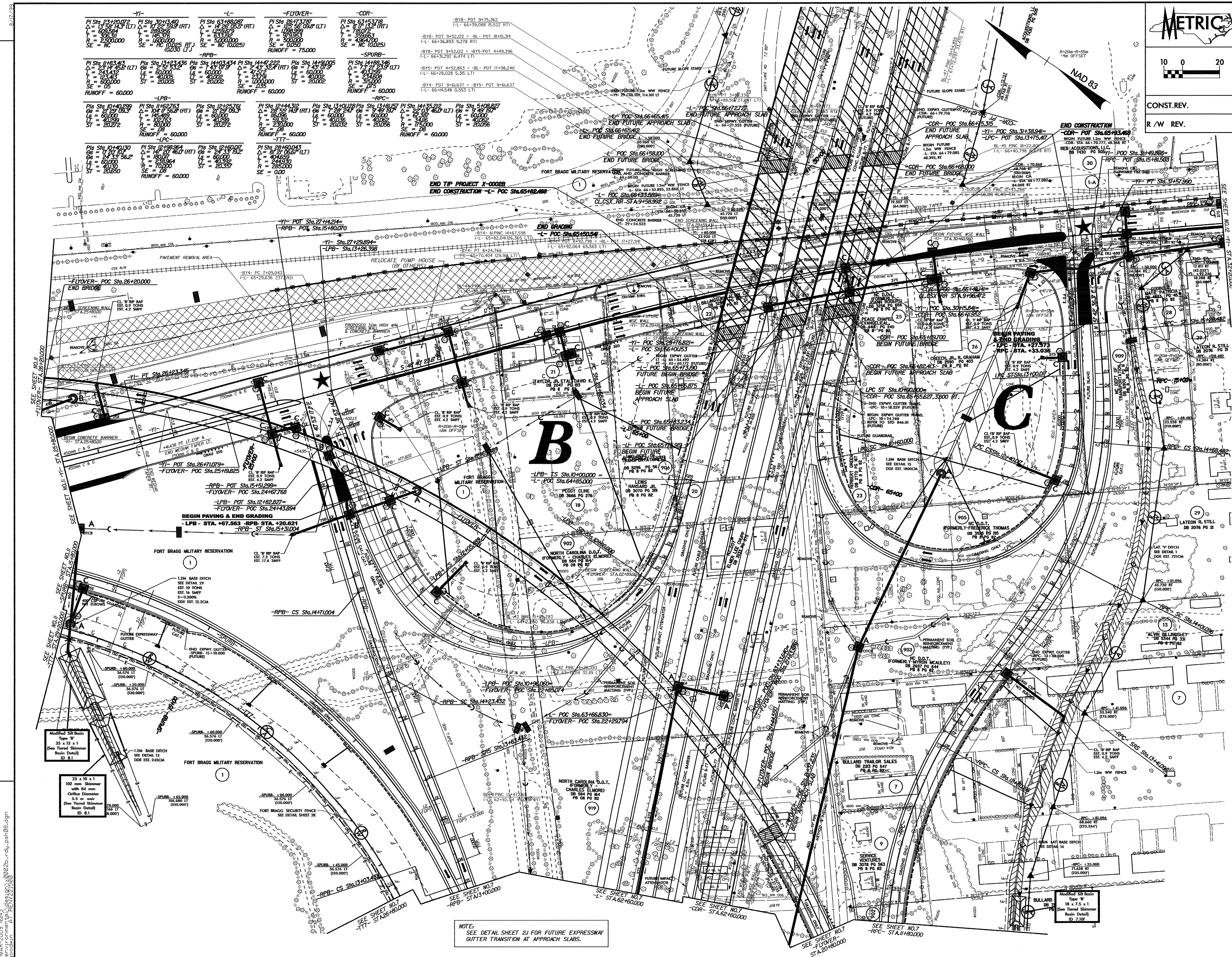
-FLYOVER-		
PIs Sta 11+50.321 Δs = 1°13'40.0"	PI Sta 12+94.904 Δ = 10°10'14.0" (RT)	
Ls = 60.000 LT = 40.001 ST = 20.001	L = 248.514 T = 124.584 R = 1,400.000 SE = 0.025 RUNOFF = 60.000	
-L-		
PI Sta 50+03.492 Δ = 14°10'30.7" (LT)	PI Sta 49+21.674 Δ = 8°49'22.8" (LT)	
L = 864.676 T = 434.557 R = 3,495.000 SE = RC (0.025)	L = 307.981 T = 154.295 R = 2,000.000	
-COL2-		
PIs Sta 50+08.245 Δs = 3°16'26.6"	PIs Sta 51+14.913 Δ = 29°03'24.5" (LT)	PIs Sta 53+22.973 Δ = 32°15'00.92" (LT)
Ls = 80.000 LT = 53.342 ST = 26.675	Ls = 80.000 T = 181.403 R = 700.000 SE = 0.06 RUNOFF = 80.000	L = 354.996 T = 170.000 R = 3,440.000 SE = 0.00
-RPCDR-		
PIs Sta 11+80.012 Δs = 4°17'49.9"	PI Sta 12+92.653 Δ = 26°04'59.4" (LT)	
Ls = 60.000 LT = 40.012 ST = 20.011	L = 182.095 T = 92.653 R = 400.000 SE = .07 RUNOFF = 60.000	
-TT7-		
PI Sta 15+90.742 Δ = 27°48'51.076" (LT)	PI Sta 16+19.310 Δ = 0°41'45.097" (LT)	PI Sta 16+98.789 Δ = 32°15'00.92" (LT)
L = 33.981 T = 17.332 R = 70.000 SE = 0.00	L = 23.837 T = 11.919 R = 1,962.700 SE = 0.00	L = 135.104 T = 67.561 R = 3,440.000 SE = 0.00
-TT7-		
PI Sta 17+81.770 Δ = 11°45'07.45" (RT)		
L = 30.767 T = 15.438 R = 150.000 SE = 0.00		

REVISIONS

05-MAR-2009 15:51
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10/25/08



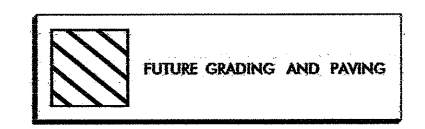
PROJECT REFERENCE NO.	SHEET NO.
X-002B	EC-17/CONST.08
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER




REVISIONS

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NOTE:
 SEE DETAIL SHEET 2J FOR FUTURE EXPRESSWAY
 GUTTER TRANSITION AT APPROACH SLABS.

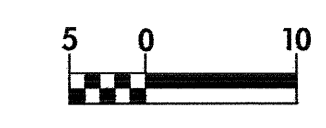
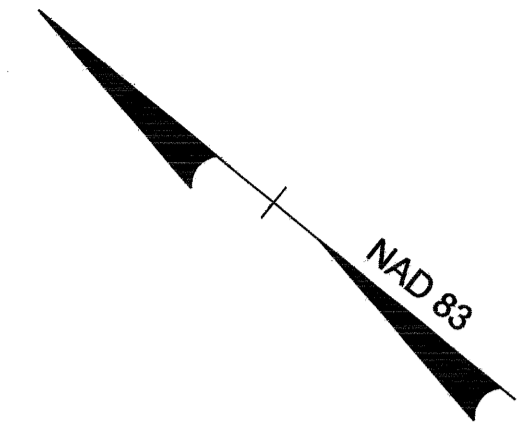


FUTURE GRADING AND PAVING

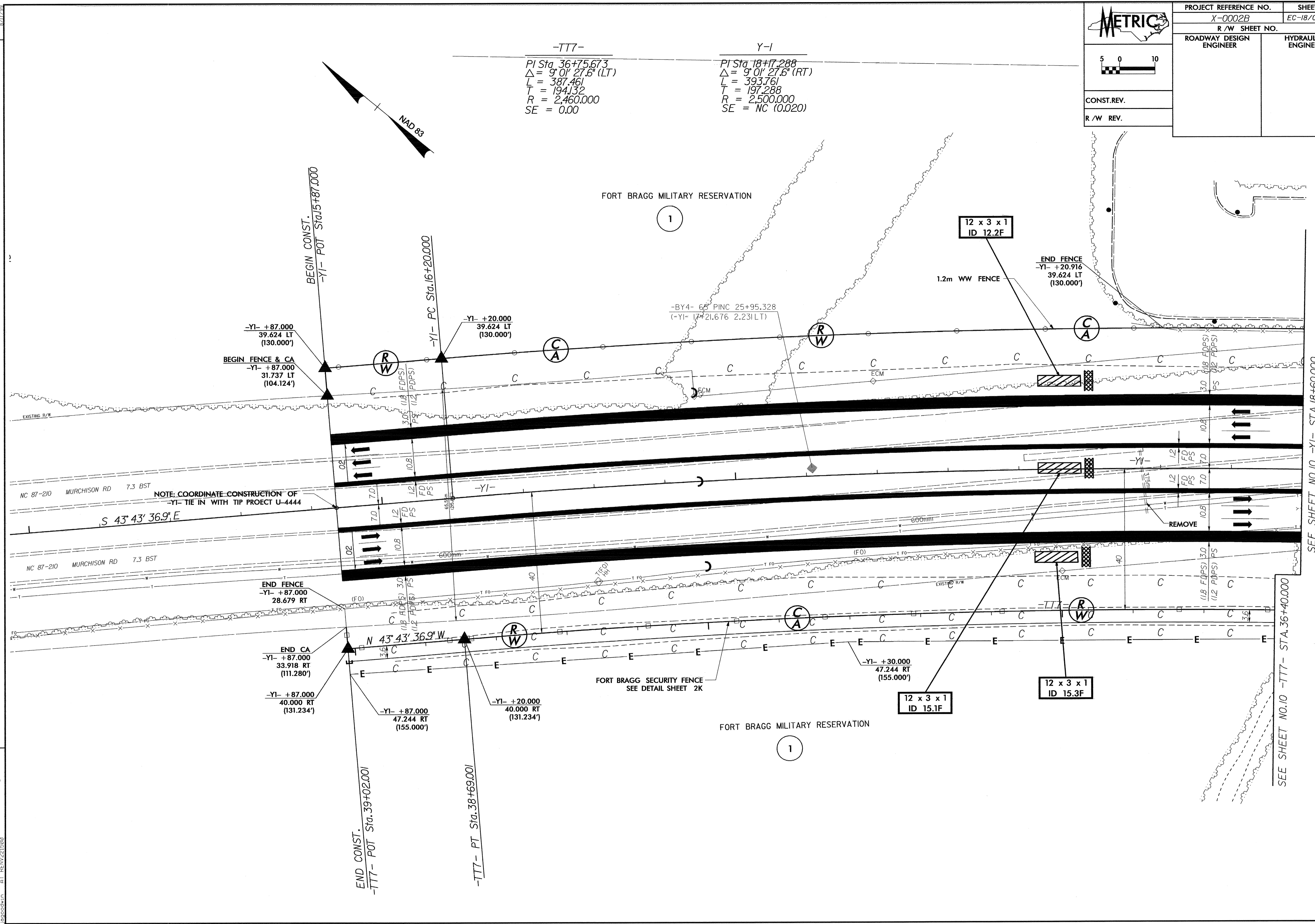
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	X-0002B	EC-18/CONST.09
ROADWAY DESIGN ENGINEER	R/W SHEET NO.	
	HYDRAULICS ENGINEER	
CONST. REV.		
R/W REV.		

-TT7-
 PI Sta. 36+75.673
 $\Delta = 9^{\circ} 01' 27.6''$ (LT)
 L = 387.461
 T = 194.132
 R = 2,460.000
 SE = 0.00

Y-I
 PI Sta. 18+7.288
 $\Delta = 9^{\circ} 01' 27.6''$ (RT)
 L = 393.761
 T = 197.288
 R = 2,500.000
 SE = NC (0.020)



REVISIONS



SEE SHEET NO. 10 -YI- STA. 18+60.000

SEE SHEET NO. 10 -TT7- STA. 36+40.000

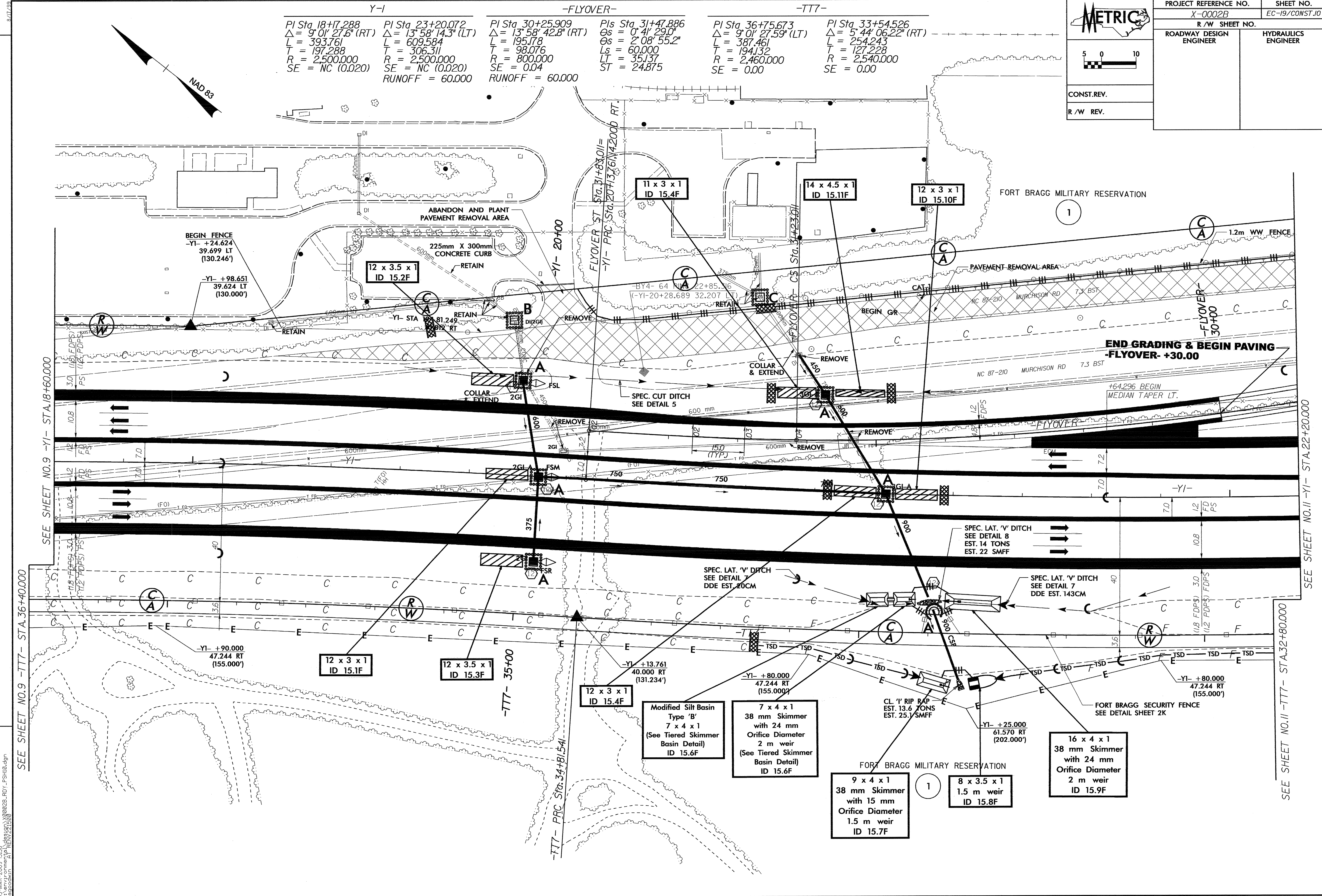
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METRIC

CONST. REV.
R/W REV.

PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-19/CONST.10
R/W SHEET NO.	HYDRAULICS ENGINEER
ROADWAY DESIGN ENGINEER	

Y-1		-FLYOVER-		-TT7-	
PI Sta. 18+17.288	PI Sta. 23+20.072	PI Sta. 30+25.909	PIs Sta. 31+47.886	PI Sta. 36+75.673	PI Sta. 33+54.526
$\Delta = 9^{\circ} 01' 27.6''$ (RT)	$\Delta = 13^{\circ} 58' 14.3''$ (LT)	$\Delta = 13^{\circ} 58' 42.8''$ (RT)	$\Theta_s = 0^{\circ} 41' 29.0''$	$\Delta = 9^{\circ} 01' 27.59''$ (LT)	$\Delta = 5^{\circ} 44' 06.22''$ (RT)
L = 393.761	L = 609.584	L = 195.178	$\Theta_s = 2^{\circ} 08' 55.2''$	L = 387.461	L = 254.243
T = 197.288	T = 306.311	T = 98.076	Ls = 60.000	T = 194.132	T = 127.228
R = 2,500.000	R = 2,500.000	R = 800.000	LT = 35.137	R = 2,460.000	R = 2,540.000
SE = NC (0.020)	SE = NC (0.020)	SE = 0.04	ST = 24.875	SE = 0.00	SE = 0.00
RUNOFF = 60.000		RUNOFF = 60.000		SE = 0.00	



REVISIONS

SEE SHEET NO.9 -YI- STA.18+60.000

SEE SHEET NO.9 -TT7- STA.36+40.000

SEE SHEET NO.11 -YI- STA.22+20.000

SEE SHEET NO.11 -TT7- STA.32+80.000

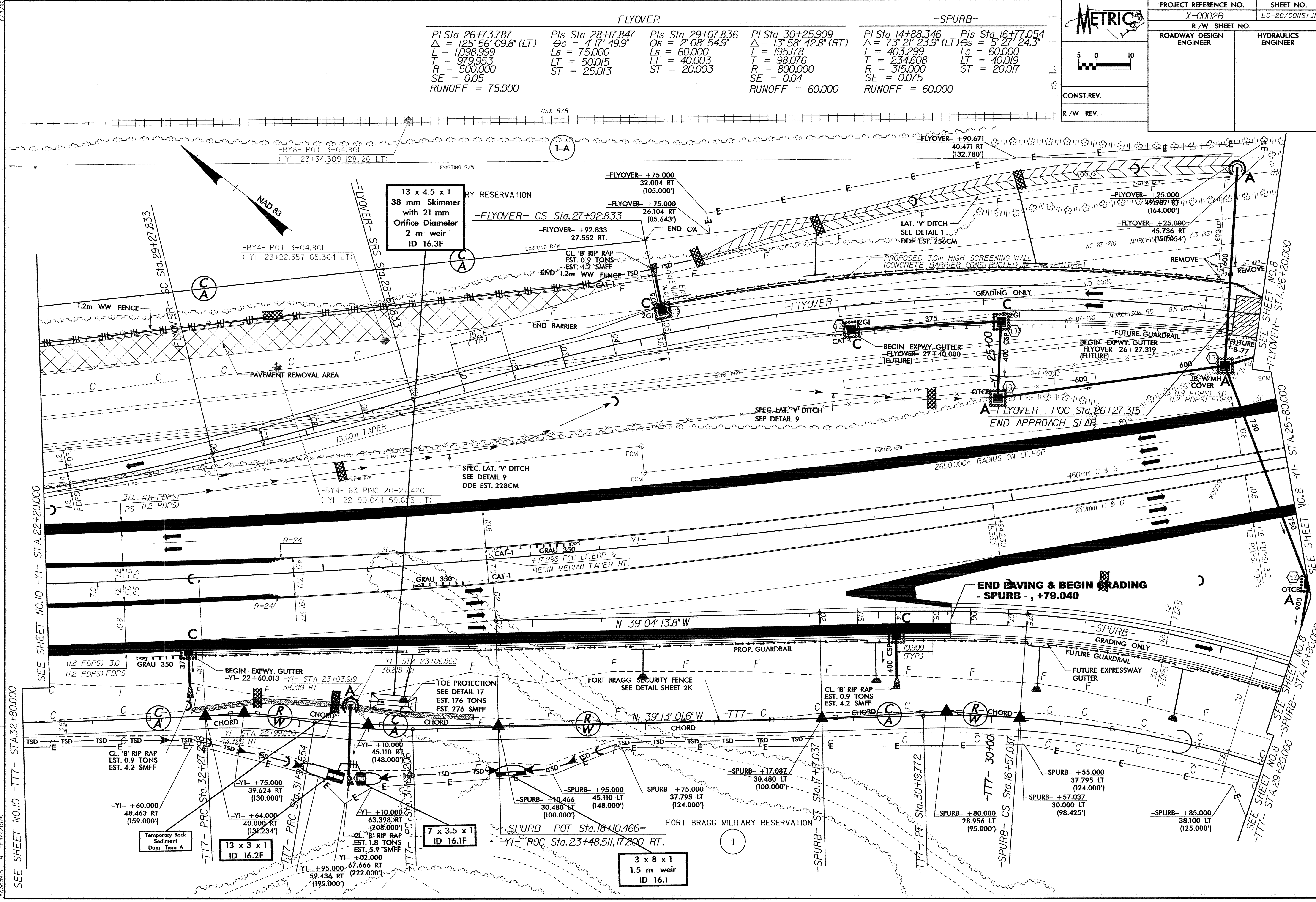
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METRIC

CONST. REV.
R/W REV.

PROJECT REFERENCE NO. X-0002B	SHEET NO. EC-20/CONST.11
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER

-FLYOVER-			-SPURB-		
PI Sta 26+73.787	PIs Sta 28+17.847	PIs Sta 29+07.836	PI Sta 30+25.909	PI Sta 14+88.346	PIs Sta 16+77.054
$\Delta = 125^{\circ}56'09.8"$ (LT)	$\Delta s = 4^{\circ}17'49.9"$	$\Delta s = 2^{\circ}08'54.9"$	$\Delta = 13^{\circ}58'42.8"$ (RT)	$\Delta = 73^{\circ}21'23.9"$ (LT)	$\Delta s = 5^{\circ}27'24.3"$
L = 1,098.999	Ls = 75.000	Ls = 60.000	L = 195.178	L = 403.299	Ls = 60.000
T = 979.953	LT = 50.015	LT = 40.003	T = 98.076	T = 234.608	LT = 40.019
R = 500.000	ST = 25.013	ST = 20.003	R = 800.000	R = 315.000	ST = 20.017
SE = 0.05			SE = 0.04	SE = 0.075	
RUNOFF = 75.000			RUNOFF = 60.000	RUNOFF = 60.000	



REVISIONS

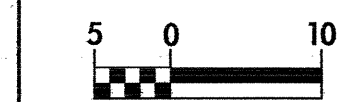
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SEE SHEET NO.10 -TT7- STA.32+80.000

SEE SHEET NO.8 -FLYOVER- STA.26+20.000
SEE SHEET NO.8 -SPURB- STA.15+80.000
SEE SHEET NO.8 -TT7- STA.29+20.000

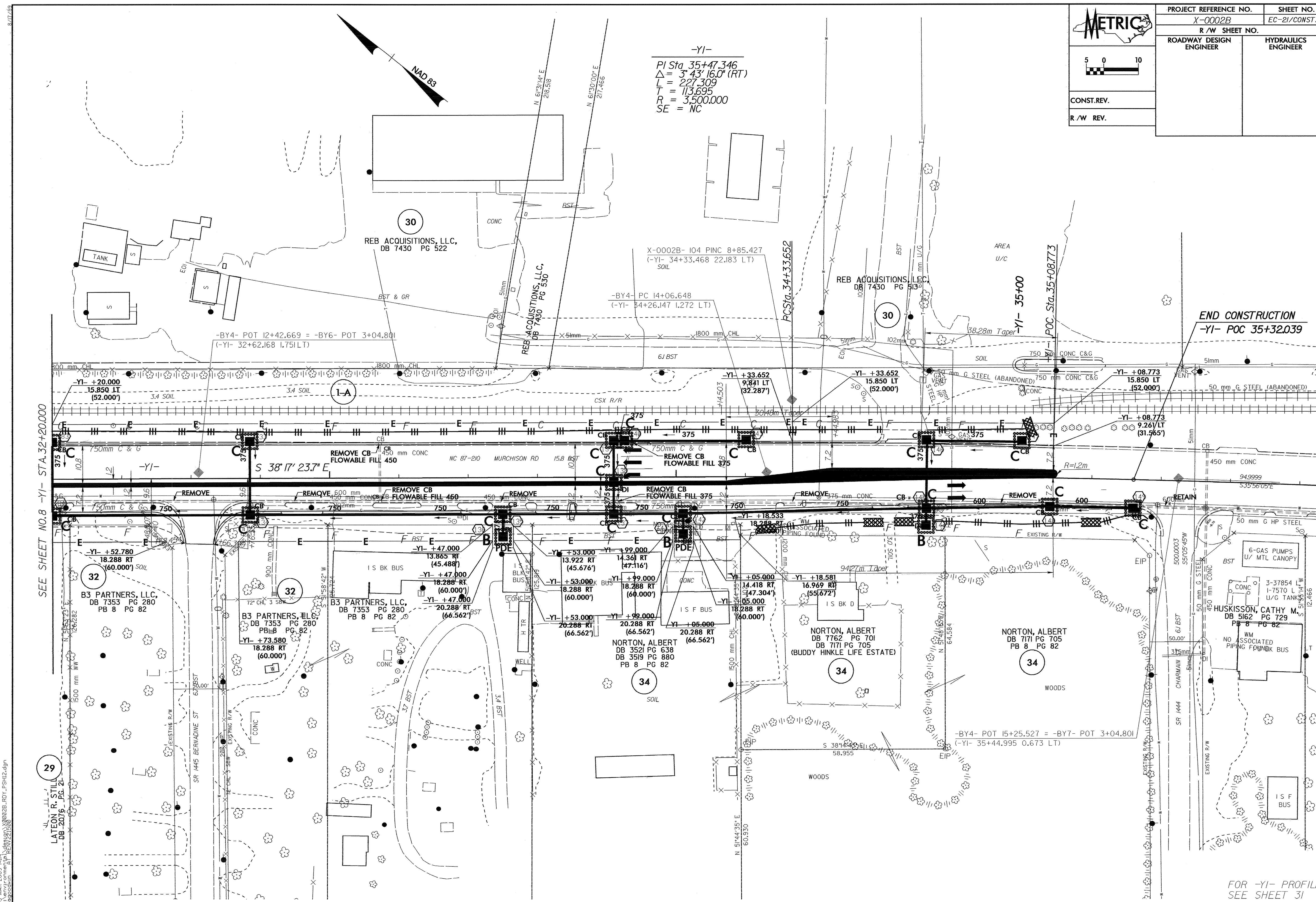
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Association



PROJECT REFERENCE NO.	SHEET NO.
X-0002B	EC-21/CONST.12
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
CONST. REV.	
R/W REV.	



-Y1-
 PI Sta. 35+47.346
 $\Delta = 3' 43'' 16.0''$ (RT)
 $L = 227.309$
 $T = 113.695$
 $R = 3,500.000$
 $SE = NC$



SEE SHEET NO. 8 -Y1- STA. 32+20.000

FOR -Y1- PROFILE SEE SHEET 31

05-MAR-2009 14H
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