

**LOCHNER**

SHEET

PROJECT: **BONNER BRIDGE - OREGON INLET NORTH CAROLINA**

JMJ Aug-06

SUBJECT: **SLAB ANALYSIS**

WDB Aug-06

SUBJECT: **PRESTRESSED GIRDER SECTIONS - BASED ON PLAN DIMENSIONS**

**SLAB DESIGN**

**INPUT**

Girder Type (prestressed or steel): **prestressed**

Slab Thickness	<b>7.25</b>	In.	No. of Beams	<b>4.00</b>
Top Bar Clearance	<b>1.875</b>	In.	Top Flange Width	= <b>1.33</b> Ft.
Bot. Bar Clearance	<b>1.500</b>	In.	Live Load	= <b>11</b> Kips
Future Wearing Surf.	<b>0.00</b>	Lbs./FT. <sup>2</sup>	f <sub>c</sub>	= <b>3.00</b> Ksi
Beam Spacing	<b>8.000</b>	Ft.	f <sub>y</sub>	= <b>40.00</b> Ksi
Effective Slab Span	=	8.00 - 1.33		= <b>6.67</b> Ft.

**Dead Load**

Slab	=	(7.25 / 12.00) x 0.15	<b>0.091</b>
FWS	=	(0.00 / 1000) x 1.00	<b>0.000</b>
		W <sub>DL</sub>	= <b>0.091</b> Kips / Ft.

**Moments**

M <sub>DL</sub>	=	0.091 x (6.67) <sup>2</sup> / 8.00 x 0.8	= <b>0.403</b> Ft. - Kips
M <sub>LL+I</sub>	=	(6.67 + 2.00) / 32.00 x 11.0 x 0.8 x 1.3	= <b>3.098</b> Ft. - Kips
M <sub>W</sub>	=	0.403 + 3.098	= <b>3.501</b> Ft. - Kips
M <sub>U</sub>	=	(1.30 x (0.403 + (1.67 x 3.098)))	= <b>7.250</b> Ft. - Kips

**Top Slab Reinforcement**

d	=	7.25 - 1.88 - 0.313	= <b>5.06</b> In.
R <sub>U</sub>	=	(7.250 x 12.00) / (0.90 x 12.0 x (5.063) <sup>2</sup> )	= <b>0.314</b>
ω	=	0.85 x (1.00 - {1.00 - (2.0 x 0.314 / 0.85 x 3.00)} <sup>0.5</sup> )	= <b>0.1122</b>
ρ Req.	=	0.112 x 3.00 / 40.00	= <b>0.0084</b>
β <sub>1</sub>	=		= <b>0.85</b>
ρ Max	=	0.75 x (0.85 x 0.85 x 3000 / 40000) x {87000 / (87000 + 40000)}	= <b>0.0278</b>
A <sub>S</sub> Req.	=	0.0084 x 12.00 x 5.06	= <b>0.51</b> Sq. In.

<b>Bar Size</b>	<b>5</b>	d <sub>C</sub> =	2.188	In.
<b>Spacing</b>	<b>6.50</b> in	d <sub>C'</sub> =	2.188	In.
<b>A<sub>S</sub></b>	<b>0.57</b> Sq. In.	d =	5.063	In.

A	=	2.00 x 6.50 x 2.19	=	28.44	
f <sub>S</sub> Allow	=	130.00 / (28.44 x 2.19) <sup>0.33</sup>	=	32.81 Ksi	36 Max.
a	=	(0.57 x 40.00) / 0.85 x 3.00 x 12.00	=	0.740 In.	
jd	=	5.0625 - 0.74 / 2.00	=	4.69	
f <sub>S</sub> Act	=	(3.50 x 12.00) / 0.57 x 4.69	=	15.81 Ksi	
θM <sub>N</sub>	=	0.90 x 0.57 x 40.00 x 4.69 / 12	=	7.97 Ft. Kips	

**f<sub>S</sub> Act = 15.81 < 32.81 OK**

**θM<sub>N</sub> = 7.97 > 7.25 OK**

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**Bottom Slab Reinforcement**

d	=	7.25 - 0.5 - 1.50 - 0.313	=	4.94 In.
R <sub>U</sub>	=	(7.250 x 12.00) / 0.90 x 12.0 x (4.938)^2	=	0.330
ω	=	0.85 x (1.00 - {1.00 - (2.0 x 0.330 / 0.85 x 3.00)}^0.5)	=	0.1184
ρ Req.	=	0.118 x 3.00 / 40.00	=	0.0089
ρ Max	=		=	0.0278
A <sub>S</sub> Req.	=	0.0089 x 12.00 x 4.94	=	0.53 Sq. In.

<b>Bar Size</b>	<b>5</b>		d <sub>C</sub> =	1.813 In.
<b>Spacing</b>	<b>6.50</b>	in	d <sub>C</sub> ' =	1.813 In.
A <sub>S</sub>	<b>0.57</b>	Sq. In.	d =	4.938 In.

A	=	2.00 x 6.50 x 1.81	=	23.56
f <sub>S</sub> Allow	=	130.00 / (23.56 x 1.81)^0.33	=	37.20 Ksi      36.0 Max
a	=	(0.57 x 40.00) / 0.85 x 3.00 x 12.00	=	0.740 In.
jd	=	4.9375 - 0.74 / 2.00	=	4.57
f <sub>S</sub> Act	=	(3.50 x 12.00) / 0.57 x 4.57	=	16.24 Ksi
θM <sub>N</sub>	=	0.90 x 0.57 x 40.00 x 4.57 / 12	=	7.76 Ft. Kips

**f<sub>S</sub> Act = 16.24 < 36.00 OK**

**θM<sub>N</sub> = 7.76 > 7.25 OK**

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PROJECT: **BONNER BRIDGE - OREGON INLET NORTH CAROLINA**

JMJ

Aug-06

SUBJECT: **SLAB ANALYSIS**

NTBC

Aug-06

SUBJECT: **PRESTRESSED GIRDER SECTIONS - BASED ON FIELD DATA, ASSUME NO BOTTOM COVER**

**SLAB DESIGN**

**INPUT**

Girder Type (prestressed or steel): **prestressed**

Slab Thickness	<b>5.75</b>	In.	No. of Beams	=	<b>4.00</b>	
Top Bar Clearance	<b>1.875</b>	In.	Top Flange Width	=	<b>1.33</b>	Ft.
Bot. Bar Clearance	<b>0.000</b>	In.	Live Load	=	<b>11</b>	Kips
Future Wearing Surf.	<b>0.00</b>	Lbs./FT. <sup>2</sup>	f <sub>c</sub>	=	<b>4.50</b>	Ksi
Beam Spacing	<b>8.000</b>	Ft.	f <sub>y</sub>	=	<b>40.00</b>	Ksi
Effective Slab Span	=	8.00 - 1.33		=	<b>6.67</b>	Ft.

**Dead Load**

Slab	=	(5.75 / 12.00) x 0.15		<b>0.072</b>
FWS	=	(0.00 / 1000) x 1.00		<b>0.000</b>
			W <sub>DL</sub>	= <b>0.072</b> Kips / Ft.

**Moments**

M <sub>DL</sub>	=	0.072 x (6.67) <sup>2</sup> / 8.00 x 0.8	=	<b>0.319</b> Ft. - Kips
M <sub>LL+I</sub>	=	(6.67 + 2.00) / 32.00 x 11.0 x 0.8 x 1.3	=	<b>3.098</b> Ft. - Kips
M <sub>W</sub>	=	0.319 + 3.098	=	<b>3.418</b> Ft. - Kips
M <sub>U</sub>	=	(1.30 x (0.319 + (1.67 x 3.098)))	=	<b>7.142</b> Ft. - Kips

**Top Slab Reinforcement**

d	=	5.75 - 1.88 - 0.313	=	<b>3.56</b> In.
R <sub>U</sub>	=	(7.142 x 12.00) / (0.90 x 12.0 x (3.563) <sup>2</sup> )	=	<b>0.625</b>
ω	=	0.85 x (1.00 - {1.00 - (2.0 x 0.625 / 0.85 x 4.50)} <sup>0.5</sup> )	=	<b>0.1527</b>
ρ Req.	=	0.153 x 4.50 / 40.00	=	<b>0.0172</b>
β <sub>1</sub>	=		=	<b>0.83</b>
ρ Max	=	0.75 x (0.85 x 0.83 x 4500 / 40000) x {87000 / (87000 + 40000)}	=	<b>0.0405</b>
A <sub>S</sub> Req.	=	0.0172 x 12.00 x 3.56	=	<b>0.73</b> Sq. In.

<b>Bar Size</b>	<b>5</b>		d <sub>C</sub> =	2.188	In.
<b>Spacing</b>	<b>6.50</b>	in	d <sub>C'</sub> =	2.188	In.
<b>A<sub>S</sub></b>	<b>0.57</b>	Sq. In.	d =	3.563	In.

A	=	2.00 x 6.50 x 2.19	=	<b>28.44</b>	
f <sub>S</sub> Allow	=	130.00 / (28.44 x 2.19) <sup>0.33</sup>	=	<b>32.81</b> Ksi	36 Max.
a	=	(0.57 x 40.00) / 0.85 x 4.50 x 12.00	=	<b>0.494</b> In.	
jd	=	3.5625 - 0.49 / 2.00	=	<b>3.32</b>	
f <sub>S</sub> Act	=	(3.42 x 12.00) / 0.57 x 3.32	=	<b>21.84</b> Ksi	
θM <sub>N</sub>	=	0.90 x 0.57 x 40.00 x 3.32 / 12	=	<b>5.63</b> Ft. Kips	

**f<sub>S</sub> Act = 21.84 < 32.81 OK**

**θM<sub>N</sub> = 5.63 < 7.14 27% OVERSTRESSED**

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**Bottom Slab Reinforcement**

d	=	5.75 - 0.5 - 0.00 - 0.313	=	4.94 In.
R <sub>U</sub>	=	(7.142 x 12.00) / 0.90 x 12.0 x (4.938) <sup>2</sup>	=	0.326
ω	=	0.85 x (1.00 - {1.00 - (2.0 x 0.326 / 0.85 x 4.50)} <sup>0.5</sup> )	=	0.0757
ρ Req.	=	0.076 x 4.50 / 40.00	=	0.0085
ρ Max	=		=	0.0405
A <sub>S</sub> Req.	=	0.0085 x 12.00 x 4.94	=	0.50 Sq. In.

<b>Bar Size</b>	<b>5</b>		d <sub>C</sub> =	0.313 In.
<b>Spacing</b>	<b>6.50</b>	in	d <sub>C</sub> ' =	0.313 In.
A <sub>S</sub>	<b>0.57</b>	Sq. In.	d =	4.938 In.

A	=	2.00 x 6.50 x 0.31	=	4.06
f <sub>S</sub> Allow	=	130.00 / (4.06 x 0.31) <sup>0.33</sup>	=	120.06 Ksi      36.0 Max
a	=	(0.57 x 40.00) / 0.85 x 4.50 x 12.00	=	0.494 In.
jd	=	4.9375 - 0.49 / 2.00	=	4.69
f <sub>S</sub> Act	=	(3.42 x 12.00) / 0.57 x 4.69	=	15.44 Ksi
θM <sub>N</sub>	=	0.90 x 0.57 x 40.00 x 4.69 / 12	=	7.97 Ft. Kips

**f<sub>S</sub> Act = 15.44 < 36.00 OK**

**θM<sub>N</sub> = 7.97 > 7.14 OK**