STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT

CONTENTS

SHEET	DESCRIPTION
1	TITLE SHEET
2	LEGEND
3	GEOTECHNICAL REPORT
4	SITE PLAN
5	PROFILE(S)
6–7	BORE LOG
8	SOIL SAMPLES TEST RESULTS
9	SCOUR REPORT
10	SITE PHOTOGRAPH(S)

STRUCTURE SUBSURFACE INVESTIGATION

PROJ. REFERENCE NO. 33521.1.1 (B-4174) F.A. PROJ. BRZ-1515 (3)

COUNTY LENOIR

PROJECT DESCRIPTION BRIDGE NO. 128 OVER MOSELEY CREEK

ON SR 1515 AT -L- STATION 16+12.50

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING, AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARBOUS FELD BORING LOGS, ROCK CORES, AND SOLI TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (1919) 250-4088. NETHER THE SUBSURFACE PLANS AND REPORTS, NOR THE FIELD BORING LOGS, ROCK CORES, OR SOLI TEST DATA ARE PART OF THE CONTRACT.

CEMERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A CECTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORNIOS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE, THE LABORATORY SAMPLE DATA AND THE IN STILL (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION, THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MOISTURE CONDITIONS TO CLIMATIC CONDITIONS TO CLIMATIC CONDITIONS TO CLIMATIC CONDITIONS TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION, AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT, FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCLMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEFARTMENT DOES NOT MARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOT THE INTERPRETATIONS MADE, OR OPINION OF DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSIFIED ON THIS PROJECT, THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS TO BE ENCOUNTERED ON THIS PRODUCT, THE HOLD OF THE PROMET OF THE SUBSURFACE INFORMATION.

PERSONNEL

JLS

MMH

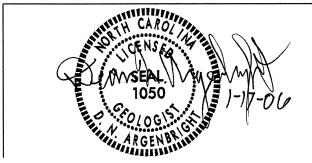
INVESTIGATED BY K. B. QUICK

CHECKED BY D. N. ARGENBRIGHT

SUBMITTED BY D. N. ARGENBRIGHT

DATE JANUARY 2006

WNC



NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

PROJECT REFERENCE NO.

33521.1.1 (B-4174)

SHEET NO.

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

	SOIL AND R	OCK LEGEND, TERM	is, symbols, an	ND ABBREV	IATIONS	
SOIL DESCRIPTION	GRADATION		ROCK	DESCRIPTION	TERMS AND DEFINITIONS	
SOIL IS CONSIDERED TO BE THE UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FILIDIT POWER AUGUER, AND YIELD LESS THAN 180 BLOWS PER FOOT ACCORDING TO STANDARD PENETRATION TEST (ARSHID T206, STIM D-1506), SOIL CLASSIFICATION IS BASED ON THE ARSHID SYSTEM BASIC DESCRIPTIONS GENERALLY SHALL INCLUDE: CONSISTENCY, COLOR, TEXTURE, MOSTOL CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. EXAMPLE:	WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZE UNIFORM - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY POORLY GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLES OF TWO OF CAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLES OF TWO OF CAP-GRADED - INDICATES AND THE ANGULARITY OF GRAIN THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE ANGULARITY OF THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE ANGULARITY OF THE A	THE SAME SIZES (ALSO R MORE SIZES. S	ROCK LINE INDICATES TH SPT REFUSAL IS PENETRA IN NON-COASTAL PLAIN N OF WEATHERED ROCK. ROCK MATERIALS ARE TY	STAL PLAIN MATERIAL THA HE LEVEL AT WHICH NON- RATION BY A SPLIT SPOOM MATERIAL, THE TRANSITI YPICALLY DIVIDED AS FOL	AT IF TESTED, WOULD YIELD SPT REFUSAL, AN INFERRED COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. N SAMPLER EQUAL TO OR LESS THAN OL FOOT PER 60 BLOWS, ON BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZOI	ALLUVIUM (ALLUV) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS.
VERY STOPF, GRAN, SOLTY CLAN, LOOST WITH MITEREEDOED FINE SAND LAVERS, HIGHLY PLASTIC, A-T-6 SOIL LEGEND AND AASHTO CLASSIFICATION	SUBANGULAR, SUBROUNDED, OR ROUNDED.	TON	RDCK (WR)	BLOWS PER FOR	PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 OT IF TESTED.	OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL
GENERAL GRANULAR MATERIALS SILT-CLAY MATERIALS CONCAUSE MATERIALS	MINERAL OGICAL COMPOSIT MINERAL NAMES SUCH AS DUARTZ, FELDSPAR, MICA, TALC, KADLIN, ETC. ARI		CRYSTALLINE ROCK (CR)		E GRAIN IGNEOUS AND METAMORPHIC ROCK THAT PT REFUSAL IF TESTED, ROCK TYPE INCLUDES GRANITE.	AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
CLASS. (≤ 35% PASSING *200) (> 35% PASSING *200) UNDAMIC MATERIALS GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5	WHENEVER THEY ARE CONSIDERED OF SIGNIFICANCE. COMPRESSIBILITY		NON-CRYSTALLINE	GNEISS, GABBRO	B SCHIST, ETC. E GRAIN METAMORPHIC AND NON-COASTAL PLAIN	CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
CLASS. A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-7-6 A-3 A-6, A-7	SLIGHTLY COMPRESSIBLE LIQUID LIM	4IT LESS THAN 31 4IT EQUAL TO 31-50	ROCK (NCR)	SEDIMENTARY R INCLUDES PHYLI	OCK THAT WOULD YEILD SPT REFUSAL IF TESTED. ROCK TYPE LITE, SLATE, SANDSTONE, ETC.	COLLUYIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.
SYMBOL B0000B0000B000B000B000B000B000B000B000		IT GREATER THAN 50	COASTAL PLAIN SEDIMENTARY ROCK (CP)	SPT REFUSAL, F	SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED	CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
* 10 50 MX SILT- MUI	GRANULAR SILT - CLAY	OTHER MATERIAL			ATHERING	DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
* 200 15 MX 25 MX 10 MX 35 MX 35 MX 35 MX 35 MX 36 MN 36 MN 36 MN 36 MN 36 MN 50 MN	TRACE OF ORGANIC MATTER 2 - 3% 3 - 5%	TRACE 1 - 10%	FRESH ROCK FRESH, I HAMMER IF CE	CRYSTALS BRIGHT, FEW J	TOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER	DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.
L10JID L1MIT PLASTIC INDEX 6 MX NP 18 MX 19 MX 10 MX 11 MN 10 MX 10 MX 11 MN 1	MODERATELY ORGANIC 5 - 10% 12 - 20% HIGHLY ORGANIC >10% >20%	LITTLE 10 - 20% SOME 20 - 35% HIGHLY 35% AND ABOVE	(V SLI.) CRYSTALS ON	ALLY FRESH, JOINTS STAIN N A BROKEN SPECIMEN FA ALLINE NATURE.	NED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN, ICE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF	DIP DIRECTION ODP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
USUAL TYPES STONE FRAGS. OF MAJOR GRAVEL, AND GAND GRAVEL	✓ WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER	R DRILLING	SLIGHT ROCK GENERAL (SLI.) 1 INCH. OPEN	ALLY FRESH, JOINTS STAII I JOINTS MAY CONTAIN CL	NED AND DISCOLORATION EXTENDS INTO ROCK UP TO AY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR	FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
GEN. RATING	STATIC WATER LEVEL AFTER 24 HOURS PERCHED WATER SATURATED ZONE OR WATER BEI		MODERATE SIGNIFICANT	PORTIONS OF ROCK SHOW	. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS. DISCOLORATION AND WEATHERING EFFECTS. IN	FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM
AS A EXCELLENT TO GOOD FAIR TO POOR POOR UNSUI	BLE TENDED WATER SHICK HILL ZONE, ON WHIER BEI	ARING STRATA	DULL SOUND (UNDER HAMMER BLOWS AN	RE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS ND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED	PARENT MATERIAL.
PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30 CONSISTENCY OR DENSENESS	SPRING OR SEEP MISCELLANEOUS SYMBOI		WITH FRESH F MODERATELY ALL ROCK EXC	CEPT QUARTZ DISCOLOREI	D OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL	FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
PRIMARY SOIL TYPE COMPACTNESS OR RANGE OF STANDARD RANGE OF UNCONFINED	ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION ST CPT SET CPT S		(MOD. SEV.) AND CAN BE E	EXCAVATED WITH A GEOL	DW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH OGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK.	FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.
(N-VALUE) (TONS/FT ²)	⊣ Ψ	S - BULK SAMPLE	SEVERE ALL ROCK EX	<i>I<mark>OULD YIELD SPT REFUSAL</mark></i> XCEPT QUARTZ DISCOLORE	D OR STAINED ROCK FABRIC CLEAR AND EVIDENT BUT REDUCE:	JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
GENERALLY LOOSE 4 TO 10 GRANULAR MEDIUM DENSE 10 TO 30 N/A	SOIL SYMBOL AUGER BORING ARTIFICIAL FILL (AF) OTHER	SS - SPLIT SPOON	EXTENT. SOME	E FRAGMENTS OF STRONG	ANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME ROCK USUALLY REMAIN.	LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.
(NON-COHESIVE) DENSE 30 TO 50 VERY DENSE >50	THAN ROADWAY EMBANKMENT - CORE BORING	SAMPLE ST - SHELBY TUBE	VERY SEVERE ALL ROCK EXC		D OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT	LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTTLING IN
VERY SOFT <2 (0.25 GENERALLY SOFT 2 TO 4 (2.25 TO 4.25 TO 4.26 TO 4.2	INFERRED SOIL BOUNDARY MONITORING	SAMPLE WELL PAR PECT TENT MODIFIES	REMAINING. SA	SAPROLITE IS AN EXAMPLE	TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK E OF ROCK WEATHERED TO A DEGREE SUCH THAT ONLY MINOR	SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN
SULT	INFERRED ROCK LINE A PIEZOMETER INSTALLATION INSTALLATION	RM - RESILIENT MODULUS SAMPLE	COMPLETE ROCK REDUCED	D TO SOIL. ROCK FABRIC	RIC REMAIN. IF TESTED, YIELDS SPT N VALUES < 100 BPF NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND	INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
(COHESIVE) VERY STIFF 15 TO 30 2 TO 4 HARD >30 >4	25/825 DIP & DIP DIRECTION OF SLOPE INSTALLATION	RS - ROCK SAMPLE	SCATTERED CO ALSO AN EXAM	ONCENTRATIONS. QUARTZ	MAY BE PRESENT AS DIKES OR STRINGERS, SAPROLITE IS	ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO DR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND
TEXTURE OR GRAIN SIZE	ROCK STRUCTURES SPT N-VALUE	SAMPLE			HARDNESS	EXPRESSED AS A PERCENTAGE.
U.S. STD. SIEVE SIZE 4 10 40 60 200 270 DPENING (MM) 4.76 2.00 0.42 0.25 0.075 0.053	SOUNDING ROD REE SPT REFUSAL	CBR - CALIFORNIA REARING	VERY HARD CANNOT BE S SEVERAL HAR	SCRATCHED BY KNIFE OR ARD BLOWS OF THE GEOLO	SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES GIST'S PICK.	SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
BOULDER COBBLE GRAVEL COARSE FINE SILT CLAY	ABBREVIATIONS AR - AUGER REFUSAL HI HIGHLY	ω − MOISTURE CONTENT	TO DETACH F	HAND SPECIMEN.	CK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED	<u>SILL</u> - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
GRAIN MM 305 75 2.0 0.25 0.05 0.005 SIZE IN. 12 3	BT - BORING TERMINATED MED MEDIUM CL CLAY MICA MICACEOUS CPT - CONE PENETRATION TEST MOD MODERATELY	V - VERY VST - VANE SHEAR TEST WEA WEATHERED	HARD EXCAVATED E BY MODERATE	BY HARD BLOW OF A GEO TE BLOWS.	CK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE DLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED	SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
SOIL MOISTURE - CORRELATION OF TERMS	CSE COARSE NP - NON PLASTIC DMT - DILATOMETER TEST ORG ORGANIC DPT - DYNAMIC PENETRATION TEST PMT - PRESSUREMETER TEST	γ - UNIT WEIGHT $\gamma_{ m d}$ - DRY UNIT WEIGHT	HARD CAN BE EXCA	CAVATED IN SMALL CHIPS	ICHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. TO PEICES I INCH MAXIMUM SIZE BY HARD BLOWS OF THE	STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 148 LB. HAMMER FALLING 38 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER, SPT REFUSAL IS PENETRATION EQUAL TO OR LESS
SOIL MOISTURE SCALE FIELD MOISTURE GUIDE FOR FIELD MOISTURE DESCRIPTION	DPT - DYNAMIC PENETRATION TEST		SOFT CAN BE GROV	GEOLOGIST'S PICK. OVED OR GOUGED READILY	BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS	THAN 0.1 FOOT PER 60 BLOWS.
- SATURATED - USUALLY LIDUID; VERY WET, USUALLY (SAT.) FROM BELOW THE GROUND WATER TAB	FOSS FOSSILIFEROUS SL SILT, SILTY		PIECES CAN	BE BROKEN BY FINGER P		STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
LL LIOUID LIMIT PLASTIC SEMISOLID: REQUIRES DRYING TO	FRAGS FRAGMENTS TCR - TRICONE REFUSAL		VERY CAN BE CARV SOFT OR MORE IN FINGERNAIL.	THICKNESS CAN BE BROK	EXCAVATED READILY WITH POINT OF PICK, PIECES 1 INCH EN BY FINGER PRESSURE, CAN BE SCRATCHED READILY BY	STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
(PI) PLASTIC LIMIT ATTAIN OPTIMUM MOISTURE	EQUIPMENT USED ON SUBJECT	PROJECT HAMMER TYPE:	FRACTURE S	SPACING SPACING	BEDDING TERM THICKNESS	IOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
OM OPTIMUM MOISTURE - MOIST - (M) SOLID; AT OR NEAR OPTIMUM MOISTU		X AUTOMATIC X MANUAL	VERY WIDE	MORE THAN 10 FEET 3 TO 10 FEET	VERY THICKLY BEDDED > 4 FEET THICKLY BEDDED 1.5 - 4 FEET	BENCH MARK: B.M. *1 R/R SPIKE SET IN 18* GUM -L- STA. 18+58.87 OFFSET 70.94' RT
SL SHRINKAGE LIMIT	6 CONTINUOUS FLIGHT AUGER	CORE SIZE:	MODERATELY CLOSE 1	1 TO 3 FEET 0.16 TO 1 FEET	THINLY BEDDED 0.16 - 1.5 FEET VERY THINLY BEDDED 0.03 - 0.16 FEET	ELEVATION: 82.07 FT.
- DRY - (D) ATTAIN OPTIMUM MOISTURE	BK-51 8 HOLLOW AUGERS	□-в		LESS THAN 0.16 FEET	THICKLY LAMINATED 0.008 - 0.03 FEET THINLY LAMINATED < 0.008 FEET	NOTES:
PLASTICITY PLASTICITY INDEX (P1) DRY STRENGTH	☐ CME-45C ☐ HARD FACED FINGER BITS		FOR SEDIMENTARY ROCKS, IND		URATION ING OF THE MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.	<u></u>
NONPLASTIC	CME-550 TUNG,-CARBIDE INSERTS X CASING W/ ADVANCER		FRIABLE	RUBBING	WITH FINGER FREES NUMEROUS GRAINS:	
MED. PLASTICITY 16-25 MEDIUM HIGH PLASTICITY 26 OR MORE HIGH	PORTABLE HOIST X TRICONE 21% STEEL TEETH	HAND TODLS: POST HOLE DIGGER	MODERATELY INDUF		BLOW BY HAMMER DISINTEGRATES SAMPLE. CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE:	
COLOR	TRICONE TUNGCARB.	HAND AUGER		BREAKS	EASILY WHEN HIT WITH HAMMER.	
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY).	CORE BIT	SOUNDING ROD VANE SHEAR TEST	INDURATED		ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; LT TO BREAK WITH HAMMER.	
MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.	OTHEROTHER	OTHER	EXTREMELY INDURA		HAMMER BLOWS REQUIRED TO BREAK SAMPLE; BREAKS ACROSS GRAINS.	
						REVISED 03/07/05



STATE OF NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

MICHAEL F. EASLEY
GOVERNOR

P.O. BOX 25201, RALEIGH, N.C. 27611-5201

LYNDO TIPPETT

SECRETARY

January 12, 2006

STATE PROJECT:

33521.1.1 B-4174

F.A. PROJECT:

BRZ-1515 (3)

COUNTY:

Lenoir

DESCRIPTION:

Bridge No. 128 Over Moseley Creek on SR 1515

SUBJECT:

Geotechnical Report - Bridge Foundation Investigation for

SR 1515 over Moseley Creek at -L- Sta. 16+12.50

Site Description

The proposed bridge site is located in La Grange at the existing SR 1515 bridge over Moseley Creek. The replacement structure will be constructed along the existing alignment. Based on the proposed design, the new bridge will have two spans having a total length of 85 feet. The bents will have a skew of 90 degrees.

One Standard Penetration Test (SPT) boring was made at or near each proposed bent location to provide subsurface information relative to foundation design. The borings were made with an ATV mounted CME 45B drill machine along with a truck mounted Mobile B-47. All were advanced by rotary drill methods using bentonite drilling fluid.

The bridge site is located in the Coastal Plain Physiographic Province and is underlain by recent alluvial deposits and Cretaceous marine sediments of the Peedee Formation. Moseley Creek is a slow flowing stream typically 15± feet wide and 3 to 5 feet deep. Topography along the project is nearly flat to gently sloping. Elevations at the site range from 73± feet along the streambed to 82± feet along the existing SR 1515 embankment. The existing approach embankments are bordered by a 400± foot wide flood plain lying at elevations ranging from 75± to 78± feet.

The bridge is situated in an area characterized by artesian water levels. Artesian flow was noted in all borings drilled at the site where the hydrostatic head was measured at an elevation of 79 feet. The water surface of Moseley Creek was measured to an elevation of 76.3 feet at the time of this investigation. All borings were sealed after completion.

(3)

Soil Description

Surficial soils consist of 4 to 7.5 feet of very loose to loose alluvial moderately organic silty sand with wood (A-2-4) and muck. Approximately 5 to 13 feet of very loose to medium dense alluvial sand (A-2-4, A-3, A-1-b) underlie these soils. In borings EB1-A and EB2-B, 2 to 3 feet of soft alluvial sandy clay was encountered at an elevation of 64± feet. Soils belonging to the Cretaceous age Peedee Formation underlie the alluvial deposits at elevations ranging from 62± to 53± feet. The initial 3 to 12 feet of Peedee soils consists of very loose to loose sand (A-2-4, A-3, A-1-b) with weathered limestone. Below an elevation of 50± feet the Peedee Formational soils grade to a stiff to hard sandy silt (A-4) with some mica and shell fragments. In boring B1-A, a 5 foot thick discontinuous layer of stiff sandy clay (A-6) was encountered overlying the silt layer. At an elevation ranging from 30± to 25± feet the Cretaceous soils consist of very loose to very dense silty sand and sand (A-2-4, A-3) with shell fragments, mica, and phosphate. A hard sandy silt (A-4) layer was encountered in boring B1-A at an elevation of 9 feet.

Based on the proposed design, the existing grade will be raised approximately $1\pm$ foot at the bridge site. The existing fill at the end bent sites consists of stiff silty clay (A-7-6) at End Bent 1 and loose to medium dense silty sand (A-2-4) at End Bent 2. Some additional fill will be required for construction of the end bent and side slopes. Borrow meeting Coastal Plain criteria is available in nearby areas.

This Geotechnical Foundation Report is based on the Bridge Survey and Hydraulic Design Report for Moseley Creek dated August 5, 2005. If significant changes are made in the design or location of the proposed structure, the subsurface information should be reviewed and modified as necessary.

Prepared By:

Kyle B. Quick

Engineering Geologist

Hyl Quick

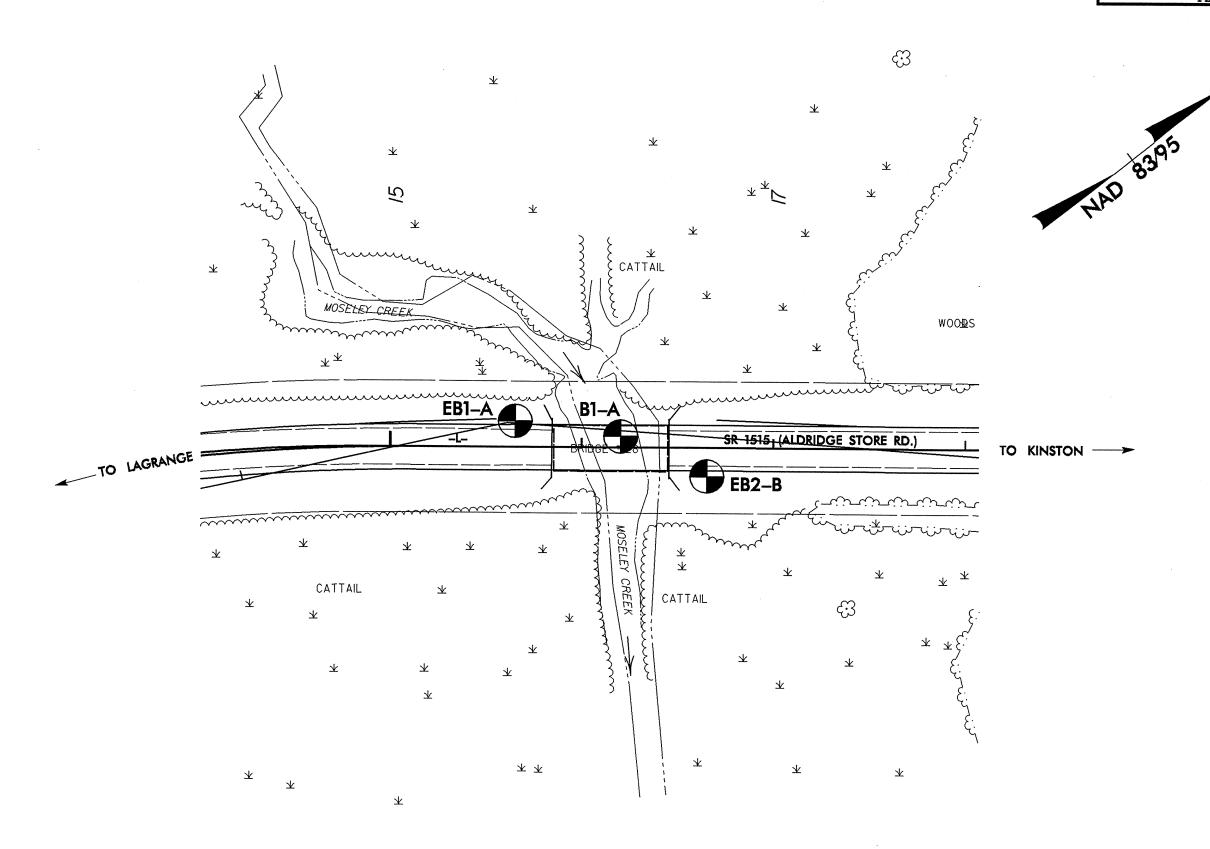
PROJECT REFERENCE NO. SHEET

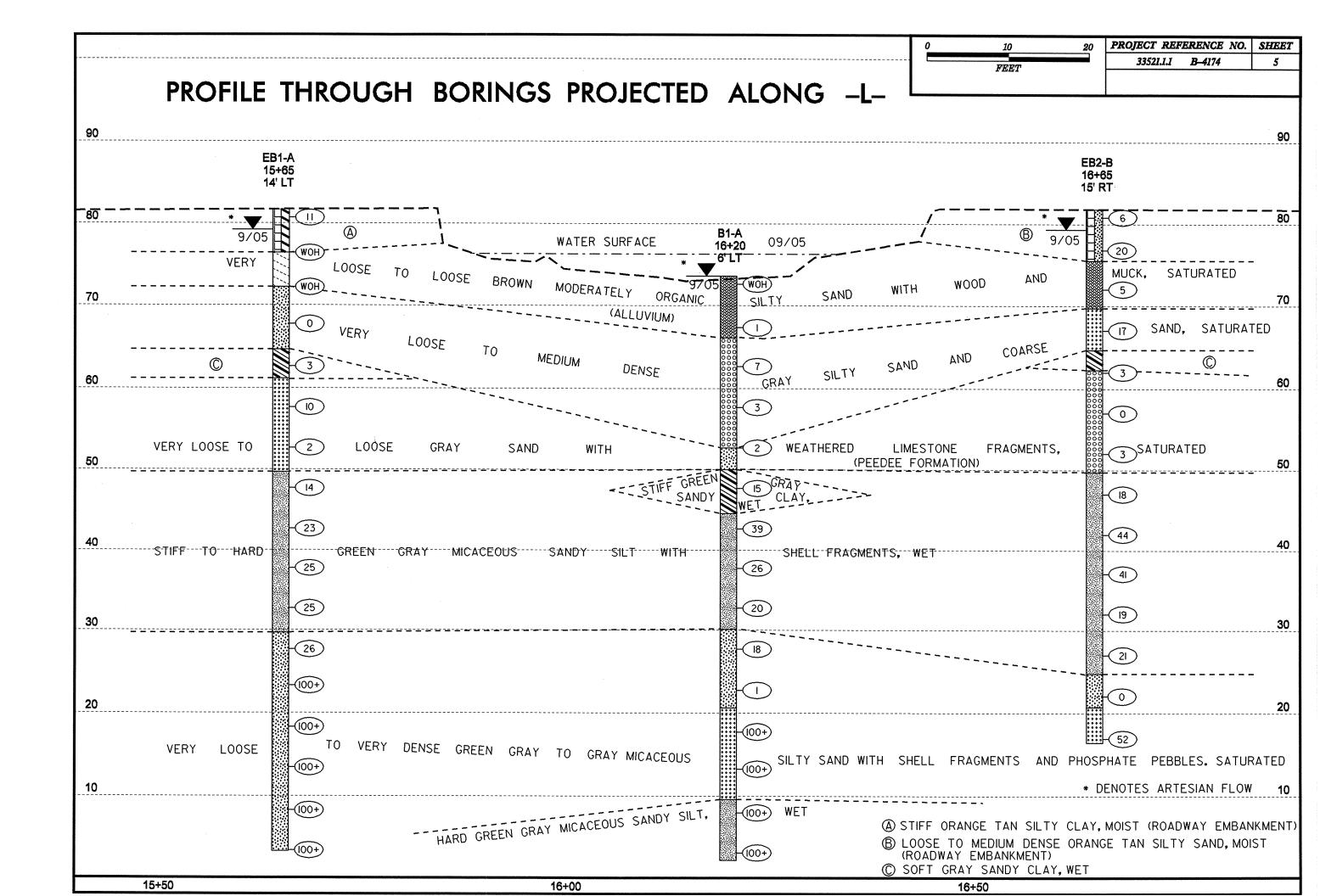
33521.1.1 (B-4174) 4

SITE PLAN

0 50 100

FEET





north carolina department of transportation — north carolina department of transportation GEOTECHNICAL UNIT BORING LOG

GEOTECHNICAL UNIT BORING LOG

DROTEON NO. 7750111 ID D 4174 CONTROL	ENOID GRALAGE	OFF AA AA HAOFD	TOP A TOP TO THE TOP T					SUBSTITUTE OF THE SUBSTITUTE O
PROJECT NO. 33521.1.1 ID. B-4174 COUNTY L SITE DESCRIPTION BRIDGE NO. 128 OVER MOSELEY CRE	ENOIR GEOLOGI		PROJECT NO. 33521.1.1				OLOGIST	J.L. STONE
		ENT -L- OHR. NM	BORING NO. BI-A		R MOSELY CREEK ON	· · · · · · · · · · · · · · · · · · ·	TOTAL PROPERTY.	GROUND WATER
COLLAR ELEVATION 81.7' NORTHING	EASTING			BORING LOCATION 3.6' NORTHIN	16+20 OFFSET		IGNMENT -	
	LL METHOD ROTARY W/MU		TOTAL DEPTH 71.4'	DRILL MACHINE M	· · · · · · · · · · · · · · · · ·	EASTING HOD ROTARY V	M / MILID	2/ HR, ARTESIAN
START DATE 07/15/03 COMPLETION DATE 07/15/03		N/A DEPTH TO ROCK N/A	START DATE 09/20/			REACE WATER DEP		HAMMER TYPE MANUAL DEPTH TO ROCK N/A
DEPTHIBLOW COUNTIDEN BLOWS PER FOOT	SAMPLE V	SOIL AND ROCK	DEPTHIBL OW		BLOWS PER FOOT	SAMPLE V	111 1.4 11	SOIL AND ROCK
ELEV. (FT.) 0.510.510.51(FT.) 0 25 50 75	NUMBER MOL G	DESCRIPTION		0.510.5 (FT.) P		NUMBER MOI	0	DESCRIPTION
+			73.6 ± 0.0 WOHW			1001		
81.7 ± 0.0 1 3 8 1 1 <u>XIII</u>		ODANOS TAN CILTY						MUCK, SATURATED
80.0 +		ORANGE TAN SILTY CLAY, MOIST	70.0 + 5.7 (2.1)					
	SS-I	(ROADWAY EMBANKMENT)	5.3 WOHW	VUH 1 1	-+	SS-15		(ALLUVIUM)
75.0 +		BROWN ORGANIC	65.0 +				000	
# 8.5 WOHWOHWOH I X 0 1		SILTY SAND, SATURATED	1 9.9 1	3 4 1 7		SS-16	000	
70.0 +		(ALLUVIUM)	60.0 ±				G	RAY COARSE SAND,
13.0 1 0 0 1 2	SS-2 SS-2	BROWN-GRAY SILTY SAND	14.9 1	1 2 1 *3		SS-17	000	SATURATED
65.0 +		WITH WOOD, SATURATED					200 000 000	
18.0 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		GRAY SANDY CLAY, WET	55.0 + 19.9 1	1 1 1 1 2-			000	
		ONAT SANDT CEAT, WET	1 1			SS-18	GR/	AY SAND, SATURATED
60.0 + 23.0 4 5 5 1 - 1 - 1 - 1 - 1	SS-3	GRAY SAND, SATURATED	50.0 + 24.9 2	6 9 1 1		SS-19 34%	(1	PEEDEE FORMATION)
		GRAT SAND, SATURATED			19	33-19 34%		REEN GRAY SANDY
55.0 + 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		(PEEDEE FORMATION)	45.0 +					CLAY, WET
28.0 WOH 1 1 1 2 - 1			29.9 6	12 27 1		SS-20		
50.0 +			40.0 ‡					
33.0 3 7 7 1 1 4	SS-4		34.9 6	12 14 1	- *26		GREE	EN GRAY SANDY SILT
45.0 45.0			_{75.0}				WI WI	TH SHELLS, WET
38.0 5 8 15 -			35.0 + 39.9 5	9 11 1	X 20		(D	CEDEC EODMATIONS
		GREEN GRAY SANDY						EEDEE FORMATION)
40.0 + 43.0 6 8 17 1 *25	==== SS-5	SILT WITH SHELLS, WET	30.0 ± 44.9 6	9 9 1 1	++	SS-2I		
		SILT WITH SHEELS, WET		´ ´ ` - <i> </i>	<u> </u>	33 21	G	REEN GRAY SILTY
35.0 + 48.0 8 10 15			25.0 + 40.0	(0)			S/	AND WITH SHELLS,
+ 40.0 0 10 13 1 1 425			49.9 1 W	VOH 1 I X = -				SATURATED
30.0 +			20.0 +					
53.0 7 12 14 1 *26	SS-6		± 54.9 11 3	34 66 0.9	_	SS-22	G	REEN GRAY SAND
25.0 +	·		15.0 +					
± 58.0 100 0.4 ± = = ± = = ± = = = = = = = = = = = =	<u>0</u> 0+x		59.9 100	0.4			WII	TH SOME MICA, WET
20.0 ‡		GRAY SILTY SAND			_		• • • •	TO SATURATED
20.0	00+*	·-	10.0 ± 64.9 61 3	39 0.7 =	-+	SS-23		DEEN ODAY CANDY
		WITH MICA AND					1945 (A)	REEN GRAY SANDY
15.0 + 68.0 100 0.2	 00+-x	DUOCDUATE MOIST	5.0 + 69 9 72	20 06				SILT WITH SOME
+ 55.01.00		PHOSPHATE, MOIST	69.9 72 2	28 0.6	_ <u> </u>			MICA, WET
10.0 + 1	00+X 00+X 00+X 00+X 00+X		0.0 ‡	BOF	RING_TERMINATED_AT_			
73.0 100 0.5 BORING TERMINATED	00+-*			1 1 1	ELEVATION 2.21 IN			
5.0 + DENSE			1 = 1	>	VERY DENSE SAND			
	00+*		-5.0 +					

PROJ SITE BORIL COLL TOTA STAR
82. 80.
75.
70.
65.0
60.0
55.0
50.0
45.0
40.0
35.0
30.0
25.0
20.0
15.0
10.0
5.0

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION GEOTECHNICAL UNIT BORING LOG SHEET 7 OF 1

PROJECT	ר אח כ	3521				B-4174		COUNT	ואוש		MU			L(O)				OF 10
	SCRIPTION			FN		8 OVER				VOIR	CD IEIE		GEOLG	OGIST	M. M.	HAGEF		
BORING		32-B					16+65			FFSET			AI ICN	MENT	-L-		GKOUI O HR.	VD WATE
COLLAR	ELEVATI	ON				NORTHING				11001	EASTIN		ALIUI	INIDIA I			-1 `	NM ARTESIA
	DEPTH 6				MACH	IINE MOBIL	E B-4	17	DRILL	METH	IOD ROTA	-	W/N	MUD	НАММ	ER TYP	E MAN	
START I	DATE 04				COMP	LETION DA	TE O	4/23	/04		FACE WAT			N/A		TH TO		N/A
ELEV.	DEPTH	1						PER I			SAMPLE		16			AND		
	(FT.)	0.5	<u> 10.5</u>	<u> 10.5</u>	(FT.)	0 2	5 	50	75	100	NUMBER	M)I. Ğ			SCRIPT		
82.1	+ 0.0	2		3	.													
80.0	± 0.0	-			'	-/							H	OPA	NGE T	- A NI C	II TV	CAND
00.0	‡ 4.0	7	11	9		-	0	3==			SS-7					MOIS:	Τ	
75.0	土					/		. ‡==	_					(RC)ADWA	Y EME	BANKM	ENT)
15.0	Ŧ 8.8	1	1	4		X5-					SS-8				MUCK,	SATI	IRATFI	D
70.0	‡		-					===			33-0					LLUVII		_
70.0	13.8	3	7	10				==			66.0		***					
	Ţ 13.0		′	10				1			SS-9		• • • •	GR.	AY SA	ND, SA	ATURA	TED
65.0 -	18.8	2	1	2	.	<u></u>		===						0.0				
	± 10.0	~	1	~		1		==		= =			000	GRA	AY SA	NDY (JLAY,	WEI
60.0 -	± ,,, ,	١.	_	_		F-]					0000	C	RAY C	COARC	E	٦D
	¥ 23.8	1	Ø	Ø		* 0 +					SS-IO		0000		AND W			עוי
55.0 -	\pm					#===#			_				000		MESTO			TED
	<u> 28.8</u>	2	1	2		X-3		==			SS-II		000		(PEEDE			
50.0 -	‡							<u> </u>					000				WIA II	0147
	‡ 33.8	4	8	10		X 18		·										
45.0 -	Ξ					[}												
15.0	‡ 38 . 8	5	23	21		F===}	 	44			SS-I2							
40.0	‡						‡	<u> </u>			33 12				GREEN	GRAY	Y SAN	DY
40.0	43.8	4	17	24	1	+	t,	:			CC 17							
	‡	'	1	2. 1	•		-/-: -/-:	<u> </u>			SS-13			SILT	WITH	SOME	E MICA	A, WET
35.0 -	+ 48.8	5		11			<u> </u>	<u> </u>										
-	± 40.0	O	8	11	1 [:		 								
30.0	<u>+ </u>	_		.		E = 3 1]			l							
-	53 . 8	5	9	12	1	X2	'L	 										
25.0	<u> </u>					F <i>-</i> /+.		 										
-	58.8	1	Ø	Ø		K Q==]	= = = =		SS-14				GRAY S			
20.0	<u> </u>							<u> </u>						WITH	SHEL SAT	L FRA URATI		IIS,
-	63.8	15	27	25	1	+		X-52					• • • •	GRA	Y SAN			
15.0			$\neg \dagger$			BORING	ĪĒR	MIN A	LED V	 			1		. 541	, JA	ONA	
-	‡	İ				ELEVAT		1	1									
10.0	‡					1			SAND-									
10.0	Fl					====		1										
	‡					F		<u> </u>										
5.0 -	 -																	
	I	1	1	,	1 1	1		ı	1	1 1	i		1 1					

B-4174 Lenoir County Bridge No. 128 over Moseley Creek on SR 1515

HOLE NO.	SAMPLE NO.	PASS 10	PASS 40	PASS 200	CSESAND	FINESAND	SI	CL	LL	PI	CLASS	DEPTH	MOIST.	ORG.
EB1-A	SS-1	100	99	92	2.6	7.5	55.3	34.6	48	23	A-7-6(15)	4.3-5.3		
	SS-2	88	63	17	51.7	31.6	10.3	6.4	31	NP	A-2-4(0)	13.0-14.5		
	SS-3	97	52	2	89.5	8.7	1.4	0.4	20	NP	A-3(0)	23.0-24.5		
	SS-4	84	83	58	4.8	58.4	22.3	14.5	40	7	A-4(5)	33.0-34.5		
	SS-5	100	100	63	0.4	66.0	19.1	14.5	30	1	A-4(5)	43.0-44.5		
	SS-6	100	99	22	3.2	80.3	10.1	6.4	23	NP	A-2-4(0)	53.0-54.5		
EB2-B	SS-7	82	62	12	51.9	35.2	4.4	8.5	15	NP	A-2-4(0)	4.0-5.5		
	SS-8	87	67	24	37.0	40.7	15.9	6.4	30	NP	A-2-4(0)	8.8-10.3		
	SS-9	87	51	6	69.0	25.2	1.4	4.4	17	NP	A-3(0)	13.8-15.3		
	SS-10	89	46	8	79.7	12.1	1.8	6.4	21	NP	A-1-b(0)	23.8-25.3		
	SS-11	64	34	7	75.5	14.4	1.6	8.5	27	NP	A-1-b(0)	29.5-30.3		
	SS-12	95	94	69	3.0	58.4	20.1	18.5	39	9	A-4(7)	38.8-40.3		
	SS-13	100	99	71	1.6	59.2	24.7	14.5	34	4	A-4(7)	43.8-45.3		
	SS-14	98	74	20	41.4	43.7	4.4	10.5	21	NP	A-2-4(0)	58.8-60.3		
B1-A	SS-15	100	81	55	29.1	18.6	27.9	24.3	Not	Enough	Material	5.3-6.8		27.8%
	SS-16	81	48	6	66.3	28.0	5.3	0.4	25	NP	A-1-b(0)	9.9-11.4		
	SS-17	93	44	4	87.6	8.7	1.3	2.4	18	NP	A-1-b(0)	14.9-16.4		
	SS-18	88	67	12	48.4	37.8	5.8	8.0	27	NP	A-2-4(0)	20.9-21.4		
	SS-19	97	95	72	3.2	53.1	29.2	14.5	40	12	A-6(8)	24.9-26.4	33.9%	
	SS-20	100	99	75	2.4	51.3	26.2	20.1	35	7	A-4(8)	29.9-31.4		
	SS-21	100	99	25	4.4	76.8	10.8	8.0	27	2	A-2-4(0)	44.9-46.4		
	SS-22	100	73	6	74.0	21.7	4.3	0.0	19	NP	A-3(0)	54.9-56.4		
	SS-23	98	87	53	22.7	24.5	52.8	0.0	22	NP	A-4(4)	64.9-65.6		

GEOTECHNICAL UNIT FIELD SCOUR REPORT

PROJECT: 33521.1.1 ID: B-4174 COUNTY: Lenoir
DESCRIPTION(1): Bridge No. 128 over Moseley Creek on SR 1515
INFORMATION ON EXISTING BRIDGE ✓ field inspection Information obtained from: ☐ microfilm (Reel:Pos:) ✓ other: Bridge Hydro Report
BR. NO.: 128 BR. LENGTH: 61.2 ft. NO. BENTS: 3 NO. BENTS IN: CHANNEL: 1 FLOODPLAIN: 2
FOUNDATION TYPE: timber piles
EVIDENCE OF SCOUR(2):
ABUTMENTS OR END BENT SLOPES: none noted
INTERIOR BENTS: none noted
CHANNEL BED:none noted
CHANNEL BANKS: some slumping along channel banks
EXISTING SCOUR PROTECTION:
TYPE(3): wooden end walls
EXTENT(4): 10-15 ft. outside edge of bridge
EFFECTIVENESS(5): seems effective
OBSTRUCTIONS(6) (DAMS,DEBRIS,ETC.): none noted
DESIGN INFORMATION
CHANNEL BED MATERIAL(7): Muck (SS-15)
CHANNEL BANK MATERIAL(8): Muck
CHANNEL BANK COVER(9): grasses
FLOOD PLAIN WIDTH(10): 400 ft.
FLOOD PLAIN COVER(11): grasses and trees

	SHEET 9 OF 10
ESIGN INFORMATION CONT.	
TREAM IS: X DEGRADING AGGRADINGE	EQUILIBRIUM (12)
THER OBSERVATIONS AND COMMENTS: stream is channelized do	own stream of the bridge
site	
HANNEL MIGRATION TENDENCY (13): North migration toward End Ber	nt 2 is unlikely due to channelization
EOTECHNICALLY ADJUSTED SCOUR ELEVATIONS(14):	
Geotechnical analysis agrees with the scour elevations as outlined in	the Bridge Survey and
Hydraulic Design. The scour elevation at Bent 1 is 64 feet.	
•	
REPORTED BY: Myle Quiel	DATE: 09/19/05
THE OTTED BT. Page Touce	DATE: <u>09/19/05</u>
CTIONIC	
 CTIONS GIVE THE DESCRIPTION OF THE SPECIFIC SITE, INCLUDING ROUTE NUMBER A NOTE ANY EVIDENCE OF SCOUR AT THE EXISTING END BENTS OR ABUTMENT SCOUR LOCATIONS, DEGRADATIONS, ETC.) NOTE ANY EXISTING SCOUR PROTECTION (RIR RAP, ETC.) DESCRIBE THE EXTENT OF ANY EXISTING SCOUR PROTECTION. 	AND BODY OF WATER CROSSED. 'S (UNDERMINING, SLOUGHING,

INSTRUC

- DESCRIBE WHETHER OR NOT THE SCOUR PROTECTION APPEARS TO BE WORKING.
- NOTE ANY DAMS, FALLEN TREES, DEBRIS AT BENTS, ETC.
- DESCRIBE THE CHANNEL BED MATERIAL BASED ON OBSERVATION AND/OR SAMPLES.
- DESCRIBE THE CHANNEL BANK MATERIAL BASED ON OBSERVATION AND/OR SAMPLES.
- DESCRIBE THE BANK COVERING (GRASS, TREES, RIP RAP, NONE, ETC.)
- (10) GIVE THE APPROXIMATE FLOOD PLAIN WIDTH (ESTIMATE).
- (11) DESCRIBE THE FLOOD PLAIN COVERING (GRASS, TREES, CROPS, ETC.)
- (12) CHECK THE APPROPRIATE SPACE AS TO WHETHER THE STREAM IS DEGRADING OR AGGRADING.
- (13) DESCRIBE THE POTENTIAL OF THE BODY OF WATER TO MIGRATE LATERALLY DURING THE LIFE OF THE BRIDGE (APPROXIMATELY 100 YEARS).
- GIVE THE GEOTECHNICALLY ADJUSTED SCOUR ELEVATION EXPECTED OVER THE LIFE OF THE BRIDGE (APPROXIMATELY 100 YEARS). THIS CAN BE GIVEN AS AN ELEVATION RANGE ACROSS THE SITE, OR ON A BENT BY BENT BASIS WHERE VARIATIONS EXIST. DISCUSS THE RELATIONSHIP BETWEEN THE HYDRAULICS THEORETICAL SCOUR AND THE GEOTECHNICALLY ADJUSTED SCOUR ELEVATION. IF THE GEOTECHNICALLY ADJUSTED SCOUR ELEVATION IS DEPENDENT ON SCOUR COUNTER MEASURES, EXPLAIN. (RIPRAP ARMORING ON SLOPES, ETC.) THE GEOTECHNICALLY ADJUSTED SCOUR ELEVATION IS BASED ON THE ERODABILITY OF MATERIALS WITH CONSIDERATION FOR JOINTING, FOLIATION, BEDDING ORIENTATION AND FREQUENCY, CORE RECOVERY PERCENTAGE, PERCENTAGE RQD, DIFFERENTIAL WEATHERING, SHEAR STRENGTH, OBSERVATIONS AT EXISTING STRUCTURES, OTHER TESTS DEEMED APPROPRIATE, AND OVERALL GEOLOGIC CONDITIONS AT THE SITE.

33521.1.1 B-4174 Lenoir Co.

Bridge No. 128 on SR 1515 Over Moseley Creek



Looking South West Toward End Bent 1